



Article

Analysis of Power Quality Signals Using An Adaptive Time-Frequency Distribution

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Abstract: Spikes frequently occur in power quality (PQ) disturbance signals due to various causes such as switching of the inductive loads and the energization of the capacitor bank. Such signals are difficult to analyze using existing time-frequency (TF) methods as these signals have two orthogonal directions in a TF plane. To address this issue, this paper proposes an adaptive TF distribution (TFD) for the analysis of PQ signals. In the proposed adaptive method, the smoothing kernel's direction is locally adapted based on the direction of energy in the joint TF domain, and hence an improved TF resolution can be obtained. Furthermore, the performance of the proposed adaptive technique in analyzing electrical PQ is thoroughly studied on both synthetic and real world electrical power signals with the help of extensive simulations. The simulation results (specially for empirical data) indicate that the adaptive TFD method achieves high energy concentration in the TF domain for signals composed of tones and spikes. Moreover, the local adaptation of smoothing kernel in the adaptive TFD enables the extraction of TF signature of spikes from TF images, which further helps in measuring the energy of spikes in a given signal. This new measure can be used to both detect the spikes as well as to quantify the extent of distortion caused by the spikes in a given signal.

Keywords: Time-Frequency, power quality, power signals, smoothing, distribution.

1. Introduction

Electric power quality (PQ) is a broad term which covers various aspects in the areas concerning electrical power transmission to its distribution to consumers. Different types of PQ issues are usually encountered in power systems including the voltage sag, swell, harmonics and transients. All these PQ issues arise due to the non-linear behavior of load on the transmission distribution system. These disturbing loads cause a deviation in the voltage and current waveforms which lead to significant degradation in the performance of power systems. Besides, there are multiple sources of different PQ disturbances appearing simultaneously, thus making it a challenging task to detect them individually. PQ also affects the performances of end user equipments which are connected to the power system. Due to such degradation in the performance of electric power systems, PQ has become a major area of concern for the utility companies. In order to improve the PQ, utilities must first record the information about the statistical behavior of the voltage and current in a power system and subsequently analyze that information for the occurrence of disturbance in order to avoid any

29 damage to the equipment. These requirements have sparked a lot of interest in the development of
30 signal processing algorithms for the analysis of electrical PQ [1–9].

31 Due to non-stationary characteristics of power signals, time-frequency (TF) signal processing
32 techniques are preferred tools for both analysis and the automated classification of these signals
33 [10]. TF signal analysis methods can be broadly categorized into linear methods and quadratic
34 methods [10]. Linear methods such as short time-Fourier transform are simple to implement, but
35 suffer from low resolution [10]. Quadratic TF methods, on the other hand, offer relatively higher
36 TF resolution as compared to the linear TF methods. The Wigner Villie distribution (WVD) is the
37 underlying TF distribution (TFD) for all quadratic TFDs. It provides ideal energy concentration for
38 mono-component signals but suffers from cross-term interference for multi-component signals [11].
39 The effects of cross-terms can be reduced by employing a two dimensional (2D) smoothing kernel,
40 but this also degrades the energy concentration of auto-terms [12]. Another alternative method for
41 reducing cross-terms in the WVD is to compute the Gabor Wigner transform, which is defined as the
42 multiplication of Gabor transform with the WVD [13]. This Gabor Wigner transform provides the
43 combined advantages of both the WVD and short time-Fourier transform, by offering high energy
44 concentration of auto-terms and by also removing cross-terms.

45 Spikes/transients are frequently observed in electrical PQ signals. They are caused by switching
46 of high inductive loads, and due to capacitor bank energization [14]. When an electric spike occurs,
47 high surge of voltage/current passes through electric equipment and can cause damage to electric
48 appliances. Specifically, transients/spikes can cause electrical devices to operate erratically, such as
49 micro-jogging in motors and it may also lead to a failure of the lighting equipment. Therefore, it is
50 imperative to detect the power quality issues [15–18].

51 Multi-resolution signal analysis methods such as the S-transform and the Hilbert transform are
52 also commonly used for the analysis and classification of PQ signals [19],[20],[21]. S-transform is
53 particularly useful for the analysis of signals with spikes as the shape of its analysis window is
54 frequency dependent. It provides high energy concentration for signals composed of spikes and
55 low frequency content. The Hilbert-Huang transform is also an effective tool for the analysis of
56 non-stationary signals [22]. However, it is only suitable for signals that can be modelled as amplitude
57 modulated and frequency modulated signals.

58 Recently, an adaptive time frequency based method (ADTFD) has been proposed which adapts
59 the direction of smoothing kernel locally on point-by-point basis for the analysis and the parameter
60 estimation of frequency modulated signals [23,24]. This method outperforms other TFD in terms
61 of its ability to resolve closely placed signal components and has found applications in areas such
62 as pattern recognition, direction of arrival estimation and signal classification [25,26]. The ADTFD
63 method, however, focuses mainly on the analysis of non-stationary frequency modulated signals. For
64 such signals, the direction of smoothing kernel can be from the set of all possible directions (covering
65 the whole range of θ) in the TF plane. In this work, our focus has been on the PQ disturbance signals
66 where spikes and sinusoids are the main disturbances. Therefore, we have modified the method
67 given in [23,24] so that it could be effectively used for the detection of spikes in the PQ signals. That
68 is achieved by limiting the directions of the smoothing kernel to only two angles, $\theta = 0$ and $\theta = 90$
69 degrees, which correspond to the horizontal and vertical axes of the TF plane where sinusoids and
70 spikes reside respectively. The performance of the proposed method is compared against the state
71 of the art TF based methods in terms of its ability to analyse PQ signals. Finally, a new metric is
72 presented which can be used to separate the signature of spikes from that of the tones in the PQ
73 signals.

74 The rest of this paper is organized as follows: signal model for the PQ signals is described in
75 Section II. Section III presents a review of the commonly used time-frequency methods and discusses
76 the drawbacks of these methods for analyzing PQ signals. Section IV discusses the proposed
77 adaptive TFD method in consideration for the analysis of the PQ signals. A detailed numerical
78 analysis considering both synthetic and real world electrical signals is presented in Section V. Finally,

79 concluding remarks on the proposed technique and the obtained simulation results are presented in
80 Section VI.

81 2. Signal Model for Power Quality Signals

82 A PQ signal without any distortion is a pure tone (i.e., sinusoid), which can be expressed as

$$x(t) = \cos(2\pi f_0 t), \quad (1)$$

83 where f_0 is the fundamental frequency of a signal. The PQ signals are sometimes corrupted by the
84 harmonics related to the fundamental frequency and can be represented as

$$x(t) = \sum_{k=1}^N \cos(2\pi k f_0 t). \quad (2)$$

85 In some cases, a PQ signal is corrupted by sudden transients or spikes. Therefore, a more general
86 model of PQ can be written as

$$x(t) = \sum_{k=1}^N \cos(2\pi k f_0 t) + \sum_{k=1}^M \delta(t - T_k), \quad (3)$$

87 where $\delta(t - T_k)$ is an impulse shifted at T_k seconds in time. One such PQ signal obtained by the
88 combination of tones and impulses is illustrated in Fig. 1.

89 3. Review of Time-frequency distributions

90 3.1. Quadratic Time-Frequency Distributions

91 The WVD is a core distribution of the quadratic class of TFDs. It can be obtained by taking
92 Fourier transform of the instantaneous auto-correlation function in the following way [12]

$$W_z(t, f) = \int w(\tau) z(t + \frac{\tau}{2}) z^*(t - \frac{\tau}{2}) e^{-j2\pi f \tau} d\tau, \quad (4)$$

93 where $w(\tau)$ is a time lag window, $z(t)$ is the analytic associate of a real signal $s(t)$, and $W_z(t, f)$ is the
94 WVD. The problem with the WVD is that it suffers from cross-terms interference for multi-component
95 signals due to its quadratic nature [12]. Cross-terms have oscillatory characteristics and the rate of
96 oscillation depends on the distance between two auto-terms [11]. The cross-terms of the WVD are
97 suppressed by employing a 2D smoothing kernel [12]. All TFDs belonging to the quadratic class,
98 including the Spectrogram, can be obtained by smoothing the WVD as follows

$$\rho(t, f) = \gamma(t, f) \underset{(t, f)}{**} W_z(t, f), \quad (5)$$

99 where $\rho(t, f)$ is a quadratic TFD, $\gamma(t, f)$ is a 2D smoothing filter, $**_{(t, f)}$ represents 2D convolution along
100 time and frequency axes.

101 Quadratic TFDs suffer from inherent compromise between suppression of cross-terms and the
102 energy concentration of auto-terms. Intensive smoothing results in almost removal of cross-terms,
103 e.g., in case of Spectrogram. However, such smoothing results in blurring of auto-terms thus affecting
104 the resolution capability of a quadratic TFD. Previous studies have shown that separable kernel TFDs,
105 i.e., TFDs whose smoothing kernel can be represented as the product of two smoothing functions:
106 $\gamma(t, f) = g(t)G(f)$, offer better compromise in cross-term suppression and auto-term preservation
107 [12]. This gain is achieved due the flexibility to independently adjust the smoothing along time and
108 frequency axes, which is not available in case of the commonly used Spectrogram [12].

109 3.2. Linear Short Time Fourier Transform

110 One alternative to the quadratic class of TFDs is linear time-frequency representations. One
111 popular distribution of this class is short time-Fourier transform and is defined as:

$$STFT(t, f) = \int w(\tau)z(t + \tau)e^{-j2\pi f\tau} d\tau, \quad (6)$$

112 where $w(\tau)$ is an analysis window. The short time-Fourier transform is a linear method. Hence, it
113 does not suffer from the cross-term interference problem commonly observed in quadratic methods.
114 The performance of this transform depends on the selection of an analysis window [10]. A wide
115 window offers good resolution along the frequency axis but poor resolution along the time axis;
116 while a narrow window provides good resolution along the time axis and poor resolution along the
117 frequency axis [10]. This limitation can be overcome to an extent by using the wavelet transform
118 [10], that offer high resolution along time and frequency axes for higher and lower frequencies,
119 respectively. However, the performance of the wavelet transform also depends on the selection
120 of mother wavelet that needs to be optimized manually for each signal to obtain an optimal
121 performance.

122 In case of power quality disturbance signals, we can have both spikes and tones in a single
123 composite signals. For such signals, it is impossible to select a single window that achieves high
124 energy concentration for both spikes and tones. A short window would result in good energy
125 concentration of the spikes but would deteriorate the energy concentration of the tones and vice
126 versa.

127 3.3. Gabor Wigner Transform: A Combination of Linear and Quadratic Methods

128 The short time-Fourier transform does not suffer from cross-term interference problem but
129 suffers from poor energy concentration of auto-terms. On the other hand, the WVD offers high
130 energy concentration of auto-terms but suffers from cross-term interference problem. One way to
131 combine the advantages of linear and quadratic time-frequency method, i.e., to obtain a TFD with
132 high energy concentration of auto-terms with the elimination of cross-terms is to simply multiply
133 a short time-Fourier transform with the WVD [13]. The TFD obtained as a multiplication of short
134 time-Fourier transform and WVD is called the Gabor Wigner transform (GWT) and is defined as [13]:

$$GWT(t, f) = GT(t, f)W_z(t, f), \quad (7)$$

135 where $GT(t, f)$ is simply a short time-Fourier transform with a Gaussian window. The GWT has
136 emerged as a powerful tool for the analysis of a number of real-life signals due to its ability to achieve
137 high energy concentration of auto-terms with significant cross-term suppression including power
138 quality disturbance signals [8,27].

139 The Gabor Wigner transform, however, fails to achieve optimal energy concentration in the
140 situations when auto-terms overlap with cross-terms [28,29]. Such a situation emerges when signal
141 components have very close components that ordinary short time Fourier transform fails to resolve.
142 In the case of PQ signals, such a situation appears when a given signal is corrupted by a train of
143 closely spaced spikes.

144 4. Proposed Methodology

145 This section presents the proposed method for the analysis of power quality signals.

146 4.1. Adaptive TFD for PQ Signals

147 An adaptive time frequency distribution for the analysis of power quality signals is presented in
148 this subsection. This method suppresses the interference terms of the WVD using adaptive directional
149 smoothing. Note that any quadratic TFD can be selected for the adaptive method, but we have

150 selected the WVD due its high resolution. Furthermore, this method exploits the fact that aligning
 151 the smoothing kernel in parallel to the direction of auto-terms can lead to a high resolution TF
 152 representation [30]. Such TFDs with the directional smoothing kernels can be expressed as [30]:

$$\rho(t, f) = \gamma_{\theta}(t, f) \underset{(t, f)}{**} W_z(t, f), \quad (8)$$

153 where γ_{θ} is a kernel whose direction depends on angle θ . Such TFDs achieve good performance
 154 for signals having one direction of energy distribution in the TF domain [30]. This global alignment
 155 of the smoothing kernel is not possible for the PQ spike signals as they can have two orthogonal
 156 directions: one parallel to the time-axis due to sinusoidal nature of power signals and other parallel
 157 to the frequency axis due to spikes. For such signals, the smoothing kernel's direction should be
 158 adapted locally as [24]

$$\rho(t, f) = \gamma_{\theta(t, f)}(t, f) \underset{(t, f)}{**} W_z(t, f), \quad (9)$$

159 where $\theta(t, f)$ denotes the direction angles which have been adapted locally based on the input signal
 160 characteristics. In general, the PQ signals are usually modeled either as the summation of pure tones
 161 or the summation of tones and spikes. Therefore, the cross-terms appearing in the WVD of PQ signals
 162 possess the following characteristics:

- 163 1. Cross-terms appear as ridges in the joint TF domain with their major axis being parallel to the
 164 direction of their oscillation [12].
- 165 2. The direction of cross-terms' oscillation, caused by the interaction of tones (fundamental
 166 frequency) and harmonics, is parallel to the time axis.
- 167 3. The direction of cross-terms' oscillation, caused by the interaction of spikes, is parallel to the
 168 frequency axis.

169 Note that the last two observations can be deduced from the established mathematical fact that
 170 the direction of cross-terms' oscillation is orthogonal to the direction of a line joining components
 171 [11]. These observations indicate that the smoothing kernel should be adapted along the following
 172 two directions: 1) along the direction parallel to the time axis to suppress the cross-terms appearing
 173 due to tones, 2) along the direction parallel to the frequency axis to suppress cross-terms appearing
 174 due to spikes. This implies that the smoothing kernel should be aligned locally with the cross-terms'
 175 major-axis at each TF point, which is the same direction as of the cross-terms' oscillation. If we use
 176 the absolute value of a WVD, the oscillatory characteristics of the cross-terms are removed. Then, the
 177 smoothing kernel's direction for each point in the TF plane is obtained by maximizing its correlation
 178 with the absolute value of the WVD as follows [24]

$$\theta(t, f) = \arg \max_{\theta} \left| |W_z(t, f)| \underset{(t, f)}{**} \gamma_{\theta}(t, f) \right|. \quad (10)$$

179 The above equation needs to be optimized only for two values of θ that are $\theta = 0$ and $\theta = \pi/2$ as
 180 the cross-terms are either parallel to the frequency or the time axis. Once $\theta(t, f)$ is estimated, we can
 181 obtain the adaptive TFD using the (9).

182 For the selection of the smoothing kernel, we use double derivative directional Gaussian kernel
 183 in this study, which is defined as:

$$\gamma_{\theta(t, f)}(t, f) = \frac{ab}{2\pi} \frac{d^2}{df_{\theta}^2} e^{-a^2 t_{\theta}^2 - b^2 f_{\theta}^2}, \quad (11)$$

184 where $t_{\theta} = t \cos(\theta) + f \sin(\theta)$, $f_{\theta} = -t \sin(\theta) + f \cos(\theta)$, θ is the rotation angle with respect to the
 185 time-axis, $\gamma_{\theta(t, f)}(t, f)$ is the directional Gaussian filter. The parameter a controls the smoothing of
 186 filter along the major axis while the parameter b controls the smoothing along the minor axis. Usually

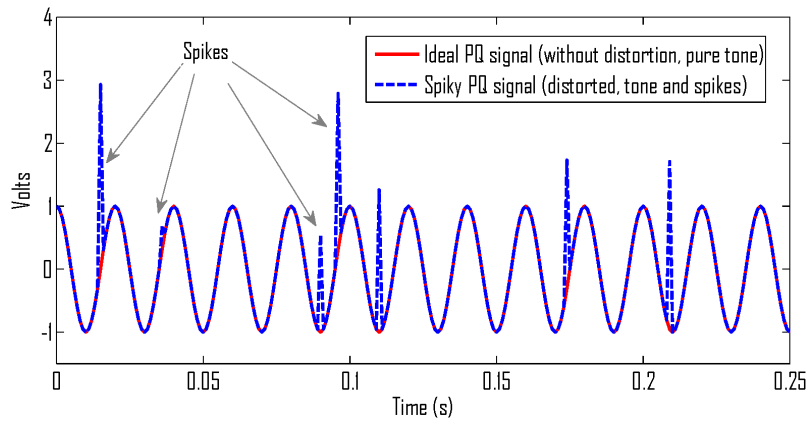


Figure 1. A synthetic PQ signal having both tones and spikes.

187 a is assigned a small value to have extensive smoothing along the major axis of cross-terms and b is
 188 assigned a large value to have less intensive smoothing along the minor axis to avoid the merging of
 189 close signal components [24]. Further details regarding the automatic optimization of parameters can
 190 be found in [23]. The main features of the employed kernel are highlighted below.

- 191 1. It has a low pass characteristics response when it is aligned in parallel to ridges, that is, along
 192 the major axis of auto- or cross-terms. This low pass characteristics results in the reduction of
 193 cross-terms and signal to noise ratio enhancement of auto-terms.
- 194 2. The response of this kernel becomes zero when it becomes orthogonal to the major axis of
 195 auto-terms. This characteristics of the smoothing kernel avoids spreading of signal energy for
 196 TF points where no signal is present.

197 4.2. Feature Extraction Using the Adaptive TFD

198 The key advantages of the adaptive TFD are: 1) it allows high energy concentration for both
 199 spikes and tones, 2) it can be used to detect spikes in a given PQ signal, by retaining TF points for
 200 which the direction of smoothing kernel is $\pi/2$. Let us define a spike TF image that retains only those
 201 points that are parallel to the direction of spikes in the following way

$$\rho_s(t, f) = \begin{cases} \rho(t, f) & ; \theta(t, f) = \frac{\pi}{2}, \\ 0 & ; \text{otherwise.} \end{cases} \quad (12)$$

202 where $\rho_s(t, f)$ is a spike TF image.

203 Similarly, we can define a tone TF image that retains only those points that are parallel to the
 204 direction of tones as follows

$$\rho_T(t, f) = \begin{cases} \rho(t, f) & ; \theta(t, f) = 0, \\ 0 & ; \text{otherwise.} \end{cases} \quad (13)$$

205 where $\rho_T(t, f)$ is a tone TF image.

206 Based on the energy of TFDs of these two images, we can compute the ratio of power consumed
 207 in spikes versus the power consumed in delivering power at 50 Hz along with the harmonics.

$$E_r = \int \int \frac{\rho_s(t, f)}{\rho_T(t, f)} dt df, \quad (14)$$

208 where E_r represents the ratio of energy consumed in spikes to the energy consumed in tones.

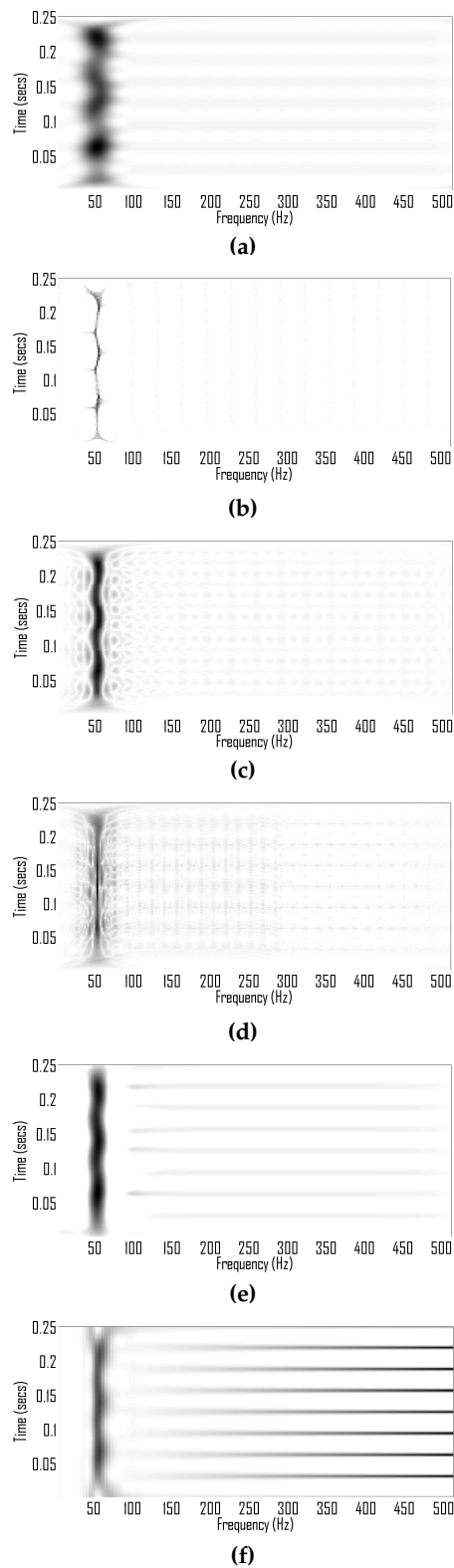


Figure 2. TF plots of the synthetic signal, given by (15), (a) Spectrogram (hamming window of length 45), (b) Reassigned Spectrogram. (c) MBD ($\beta = 0.1$ and lag window of length 64), (d) Gabor Wigner transform (Gabor transform of window length 45 is used), (e) The adaptive TFD ($a = 3$ and $b = 8$), (f) The S-transform.

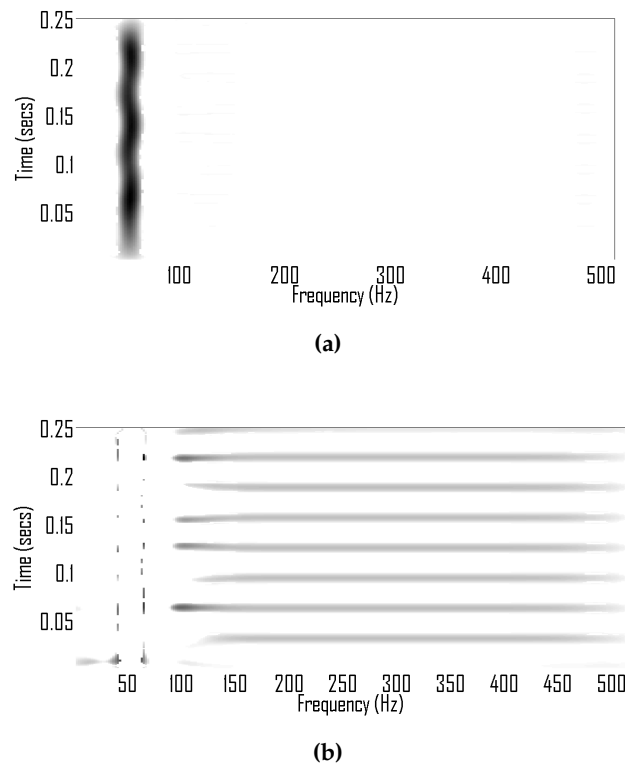


Figure 3. Separation of TF representations of tone and spike using direction of signal energy (a) TF representation of tone, (b) TF representation of spikes.

209 5. Numerical Analysis

210 To demonstrate the efficacy of the adaptive TFD method in analyzing electrical PQ, extensive
211 simulations for both synthetic and real world electrical power signals are performed.

212 5.1. Synthetic Signals

213 Let us simulate a scenario when a given signal has both tones and spikes.

$$s(t) = s_{\text{tone}} + s_{\text{spike}}, \quad (15)$$

214 where the tone part is defined as,

$$s_{\text{tone}} = \cos(100\pi t), \quad (16)$$

and the spike part is given as,

$$s_{\text{spike}} = \sum_{k=0}^N \delta(t - kT), \quad (17)$$

215 where $T = 1/32$ s. The given signal was sampled at 1024 Hz. The time-domain representation of the
216 signal is illustrated in Fig. 1.

217 The signal was analyzed using the state of the art TFDs including the Spectrogram, reassigned
218 Spectrogram [31], modified B distribution a Separable kernel TFD [12], Gabor Wigner Transform [13]
219 (or marked WVD), S-transform and the proposed adaptive method; the TF plots obtained from all
220 those methods are shown in Fig. 2. It is observed that the Spectrogram and reassigned Spectrogram
221 fail to concentrate signal energy for spikes due to its poor energy concentration. The WVD is hard to

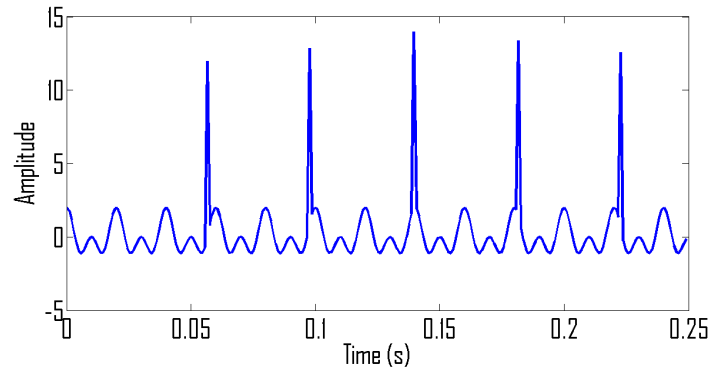


Figure 4. A synthetic PQ signal composed of two tones and spikes.

222 interpret due to the presence of cross-terms. The MBD suppresses cross-terms to certain extent, but it
 223 is difficult to separate cross-terms from spikes. The Gabor Wigner transform fails to clearly represent
 224 spikes due to overlapping of auto-terms and cross-terms in the WVD.

225 The S-transform due to its frequency dependent analysis window and the adaptive TFD, due
 226 to its locally adaptive smoothing kernel, achieves high concentration of energy for the given signal.
 227 Another benefit of the proposed approach is that it can separate TF signatures of spikes and tones
 228 using (12) and (13), as indicated in Fig. 3.

229 In order to demonstrate the performance of the proposed method on a more complicated and
 230 practical scenario, we consider a signal consisting of multiple tones in addition to spikes at random
 231 and multiple instances. Let us denote such a signal by $s(t)$ which is given by

$$s(t) = s_{\text{tone}} + s_{\text{spike}}, \quad (18)$$

where the tone part is defined as

$$s_{\text{tone}} = \cos(100\pi t) + \cos(200\pi t), \quad (19)$$

and the spike part is given as

$$s_{\text{spike}} = \sum_{k=0}^N \delta(t - kT), \quad (20)$$

232 where $T = \frac{1}{24}$ s. The given signal was sampled at 1024 Hz. The time-domain representation of
 233 the signal is illustrated in Fig. 4. The signal was analyzed using the same set of TFDs that were
 234 used in the earlier example; the TF plots obtained from all those methods are shown in Fig. 5. It
 235 is observed that the spectrogram and reassigned spectrogram fails to concentrate signal energy in
 236 the case of spikes. The MBD is hard to interpret due to the presence of cross-terms. The Gabor
 237 Wigner transform fails to clearly represent spikes due to overlapping of auto-terms and cross-terms
 238 in the WVD. The S-transforms achieves high energy concentration for spikes but fails to achieve high
 239 energy concentration for tones. The TFD spectrogram obtained from the proposed method, however,
 240 not only resolves close tones but achieves a clear representation of spikes (Fig. 5(e)).

241 5.2. Real World Signals

242 Let us now repeat the above experiment for a real world power signal acquired from the
 243 soldering iron. The signal is sampled at 2500 Hz and the total duration of signal is 0.1 s. The
 244 time-domain representation of the signal given in Fig. 7 indicates that the signal has both sinusoidal
 245 and spiky characteristics. The given signal is analyzed from the same set of TFDs that were used in
 246 the earlier experiment as shown in Fig. 6. The Spectrogram results in a blurred TF representation.
 247 The reassigned Spectrogram fail to concentrate energy for spikes. The poor performance of the WVD,

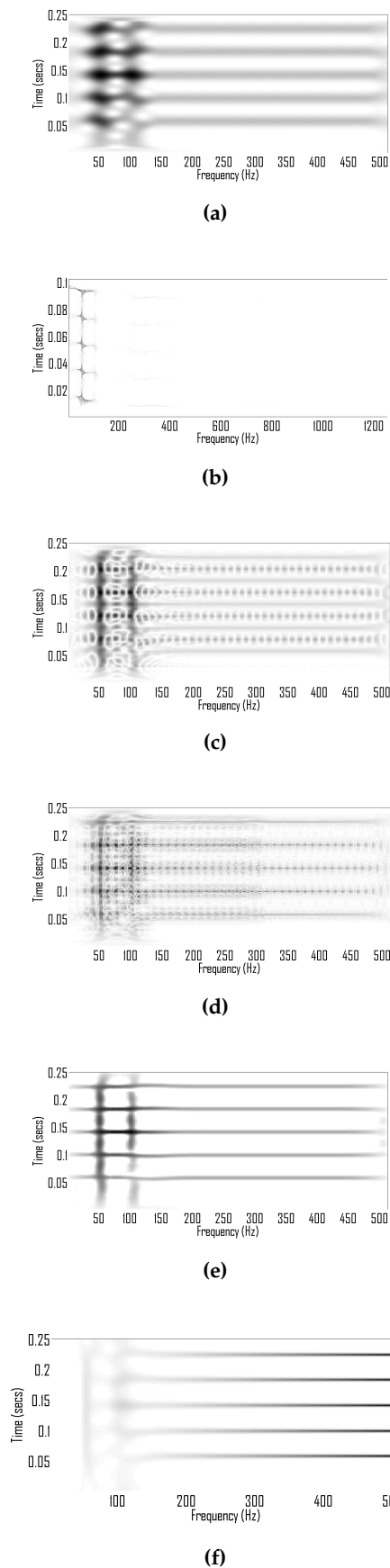
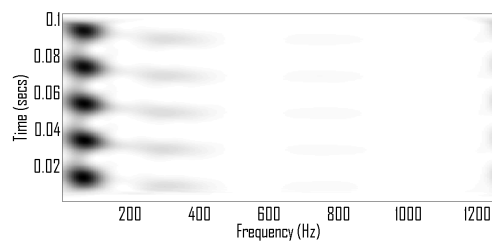
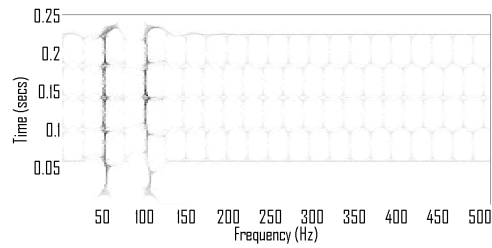


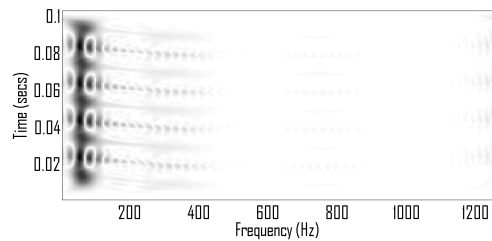
Figure 5. TF plots of the synthetic signal, given by (18), (a) Spectrogram (hamming window of length 45), (b) Reassigned Spectrogram, (c) MBD ($\beta = 0.1$ and lag window of length 64), (d) Gabor Wigner transform (Gabor transform of window length 45 is used), (e) The adaptive TFD ($a = 3$ and $b = 8$), (f) The S-transform



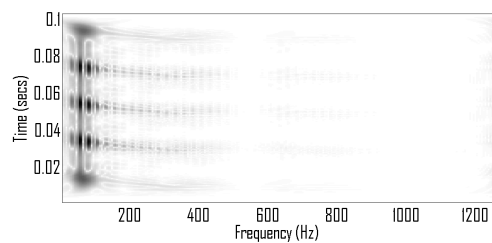
(a)



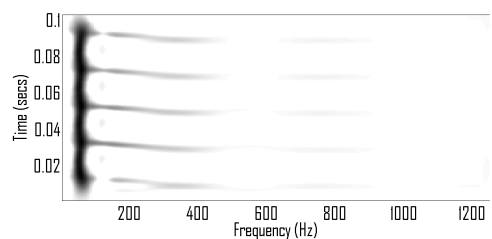
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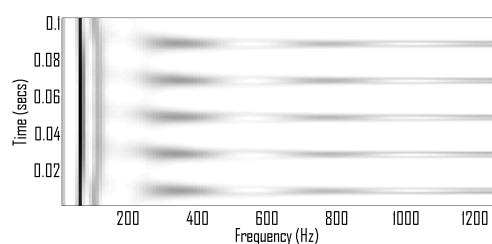
(c)



(d)



(e)



(f)

Figure 6. TF plots of a real world signal acquired from iron having spikes. (a) Spectrogram (hamming window of length 45). (b) Reassigned Spectrogram. (c) MBD ($\beta = 0.1$ and lag window of length 64). (d) Gabor Wigner transform (Gabor transform of window length 45 is used). (e) The adaptive TFD ($a = 3$ and $b = 8$). (f) The S-transform.

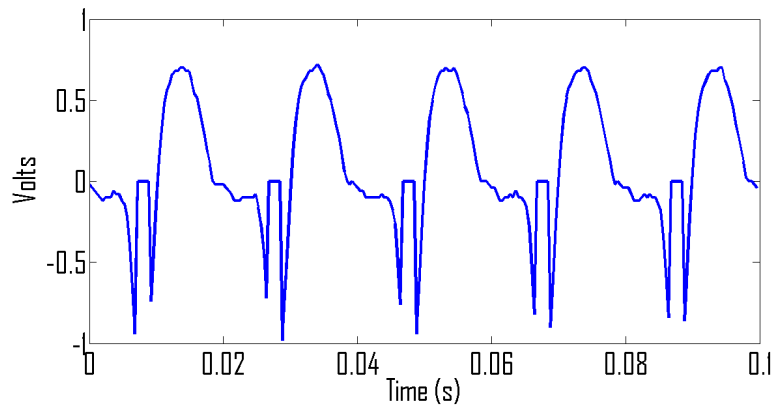


Figure 7. A real world PQ signal showing both tones and spikes.

248 MBD and Spectrogram is due to their fixed smoothing kernels that cannot be adapted locally. The
249 Gabor Wigner transform, which is otherwise a useful tool for PQ signals also fails to achieve high
250 energy concentration. The poor performance of the Gabor Wigner transform is due to the overlapping
251 of cross-terms with auto-terms in the WVD. The proposed TFD due to its local adaptation achieves
252 high energy concentration for all signal components. Similarly, the S-transform due to frequency
253 dependent window adaptation achieves good energy concentration for both tone and spikes.

254 Experimental results confirm that the adaptive TFD and S-transform outperforms its
255 counterparts in terms of preservation of signal energy for both spikes and tones. However, the
256 adaptive TFD provides additional benefit, i.e. using (12) and (13), we can separately observe TF
257 points belonging to tones and spikes as illustrated in Fig. 8. The ratio of spike energy versus tone
258 energy for this experiment is now obtained as: 0.538. This ratio can also stand as an unanimous
259 quantifier to measure the distribution of energy along spikes for the monitoring of PQ signals.

260 6. Conclusions

261 An effective method for the analysis of PQ signals with spiky characteristics has been developed.
262 Extensive computer simulations have been performed to study the performance of the proposed
263 technique in analyzing electrical PQ on both synthetic and real world electrical power signals. The
264 proposed method has been observed to outperform the existing signal analysis techniques including
265 Gabor Wigner transform in terms of its ability to give a clear representation for both spikes and
266 tones. Based on the proposed analysis, it has been concluded that the ratio between the signal energy
267 consumed in spikes and the tone energy is a useful quantifier for the effective monitoring of PQ in
268 electrical power signals. That feature can be integrated with the rest of the features developed as part
269 of other studies for the automatic classification of PQ signals.

270 **Author Contributions:** N.A.K, F.B. and S.J.N conceived and designed the experiments; N.A.K. and F.B.
271 performed the experiments; S.J.N. and N.R. analyzed the data; N.A.K., N.R., and S.K.S. contributed in analysis
272 on the results and writing of the paper.

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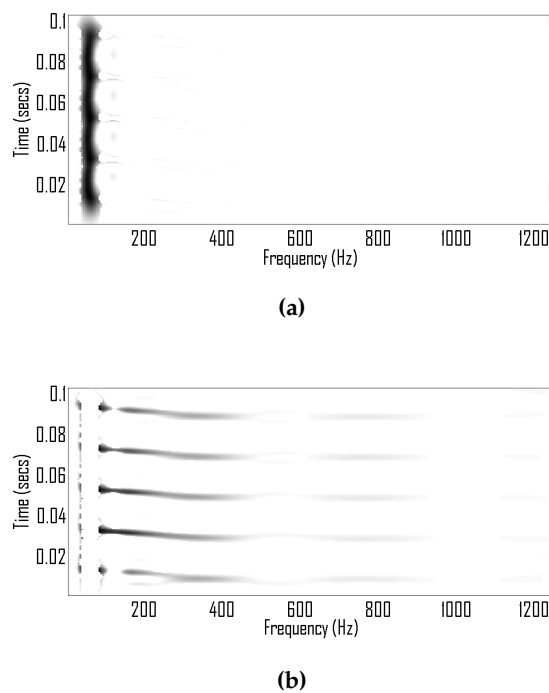


Figure 8. Separation of TF representation of tones and spikes using the direction of signal energy (a) TF representation of tones, (b) TF representation of spikes.

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