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ATTENUATION OF SOUND IN LINED CIRCULAR DUCTS

by

Young-chung Cho  
K. Uno Ingard

GTL Report No. 120

April 1975

Addendum to  
GTL Report No. 119



GAS TURBINE LABORATORY  
MASSACHUSETTS INSTITUTE OF TECHNOLOGY  
CAMBRIDGE, MASSACHUSETTS

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## PREFACE

This is an addendum to Gas Turbine Laboratory Report No. 119. It covers additional work on sound propagation in lined ducts which was started under DOT Grant Agreement DOT-OS-30011 and continued under Supplement Agreements to the same grant.

The work is being monitored by Dr. Gordon Banerian, Office of Noise Abatement, Department of Transportation.

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## A1. ATTENUATION OF SOUND IN LINED CIRCULAR DUCTS

In the previous report, we have used approximate expressions for the wall impedance for the discussion of sound attenuation in lined circular ducts. For instance, Eq. (2.5) has been used for the wall impedance of a circular duct lined with a resonator with a resistive screen, and Eq. (2.8) for a circular duct lined with a porous material.

If the ratio of the duct radius to the liner thickness ( $D/L$ ) is large and the sound frequency is large, the impedance given in Eq. (2.5) or Eq. (2.8) is a good approximation for a lined circular duct. However, when either one of these conditions is not fulfilled, the radial spread of the wave in the liner imposes some effects on the sound attenuation, whereas no wave spreading takes place in the liner of a rectangular duct.

In this addendum we derive expressions for the wall impedance of lined circular ducts, accounting for the cylindrical spreading of the waves within the liner. The assumption of a locally reacting surface is still made. On the basis of the impedance thus obtained, the attenuation characteristics of a circular lined duct are computed for a wide range of parameters.

For direct comparison, the numerical results are presented in figures numbered similarly to the previous report. For example, "Figure 3.66" in the previous report is replaced by "Figure A3.66" for plotting the octave band TL vs  $kL$  in a circular duct lined with a porous material with the duct parameters:  $\theta = 0.5$ ,  $D/L = 1.094$  and area ratio = 1. (See page 124 and page A

### A1.1 Resonator Liner

In the case of locally reacting duct walls, the sound propagation in the liner is negligible in the axial direction. Thus the pressure field in the liner is written as

$$p_L = A \left\{ H_0^{(1)}(kr) + \alpha H_0^{(2)}(kr) \right\}, \quad (A1.1)$$

where the H's are Hankel functions and A and  $\alpha$  are constants.

The velocity field is then

$$\vec{u} = \hat{r} \frac{1A}{\rho c} \left\{ H_1^{(1)}(kr) + \alpha H_1^{(2)}(kr) \right\}, \quad (A1.2)$$

where  $\hat{r}$  is the radial unit vector.

Since  $u_r = 0$  at  $r = b + L$ , from Eq. (A1.2),

$$\alpha = - \frac{H_1^{(1)}[k(b + L)]}{H_1^{(2)}[k(b + L)]}. \quad (A1.3)$$

The normalized wall reactance due to the cavity is

$$\chi_c = \left. \frac{p}{\rho c u_r} \right|_{r=b} = -i \frac{H_0^{(1)}(kb) + \alpha H_0^{(2)}(kb)}{H_1^{(1)}(kb) + \alpha H_1^{(2)}(kb)}. \quad (\text{A1.4})$$

If  $kb \gg 1$  and  $L \ll b$ , this equation reduces to

$$\chi_c \cong i \cot(kL). \quad (\text{A1.5})$$

This is the same as the cavity reactance in a rectangular duct lined with a resonator (cf. Eq. 2.5).

The total normalized impedance is

$$\zeta = \theta - i \left( kt' + \frac{H_0^{(1)}(kb) + \alpha H_0^{(2)}(kb)}{H_1^{(1)}(kb) + \alpha H_1^{(2)}(kb)} \right), \quad (\text{A1.6})$$

where  $\theta$  is the dynamic resistance of the screen,  $kt'$  the reactance accounting for the inertia of the air in the screen, and  $\alpha$  is given in Eq. (A1.3).

#### A1.2. Porous Liner

When the porous material is isotropic and homogeneous, the pressure field in the porous medium of an annular shape as shown in Fig. 2.20 is

$$p_L = A \left\{ H_0^{(1)}(qr) + \alpha H_0^{(1)}(qr) \right\}, \quad (\text{A1.7})$$

where  $q$  is defined in Eqs. (2.9) and (2.10).

The velocity field is then

$$\vec{u}_L = \hat{r} \frac{ikA}{\rho cq} \left\{ H_1^{(1)}(qr) + \alpha H_1^{(2)}(qr) \right\}. \quad (\text{A1.8})$$

It follows from  $u_r|_{r=b+L} = 0$  that



$$\alpha = - \frac{H_1^{(1)}[q(b + L)]}{H_1^{(2)}[q(b + L)]} . \quad (\text{A1.9})$$

The normalized wall impedance is

$$\zeta = \frac{p_2}{\rho c u_r} \Big|_{r=b} = - \frac{i q}{k} \frac{H^{(1)}(qb) + \alpha H_0^{(2)}(qb)}{H_1^{(1)}(qb) + \alpha H_1^{(2)}(qb)} . \quad (\text{A1.10})$$

If  $qb \gg 1$  and  $b \gg L$ , this equation reduces to

$$\zeta \rightarrow \frac{i q}{k} \cot(qL) . \quad (\text{A1.11})$$

This is the same as Eq. (2.8).

Figures A2.16 - A2.19: Real and imaginary parts of  $k_z$  for circular ducts lined with a resistive screen type resonator liner. The real part of  $k_z$  is normalized by division by  $k$ . The imaginary part of  $k_z$  is presented in terms of  $8.6859 \cdot \text{Im}(k_z)D$ , which is the transmission loss in dB of a pure tone in a length  $D$  of the duct. Each figure corresponds to a different value of  $D/L$ . Each curve in a figure corresponds to a different value of the flow resistance  $\theta$  (in units of  $\rho c$ ) of the screen.

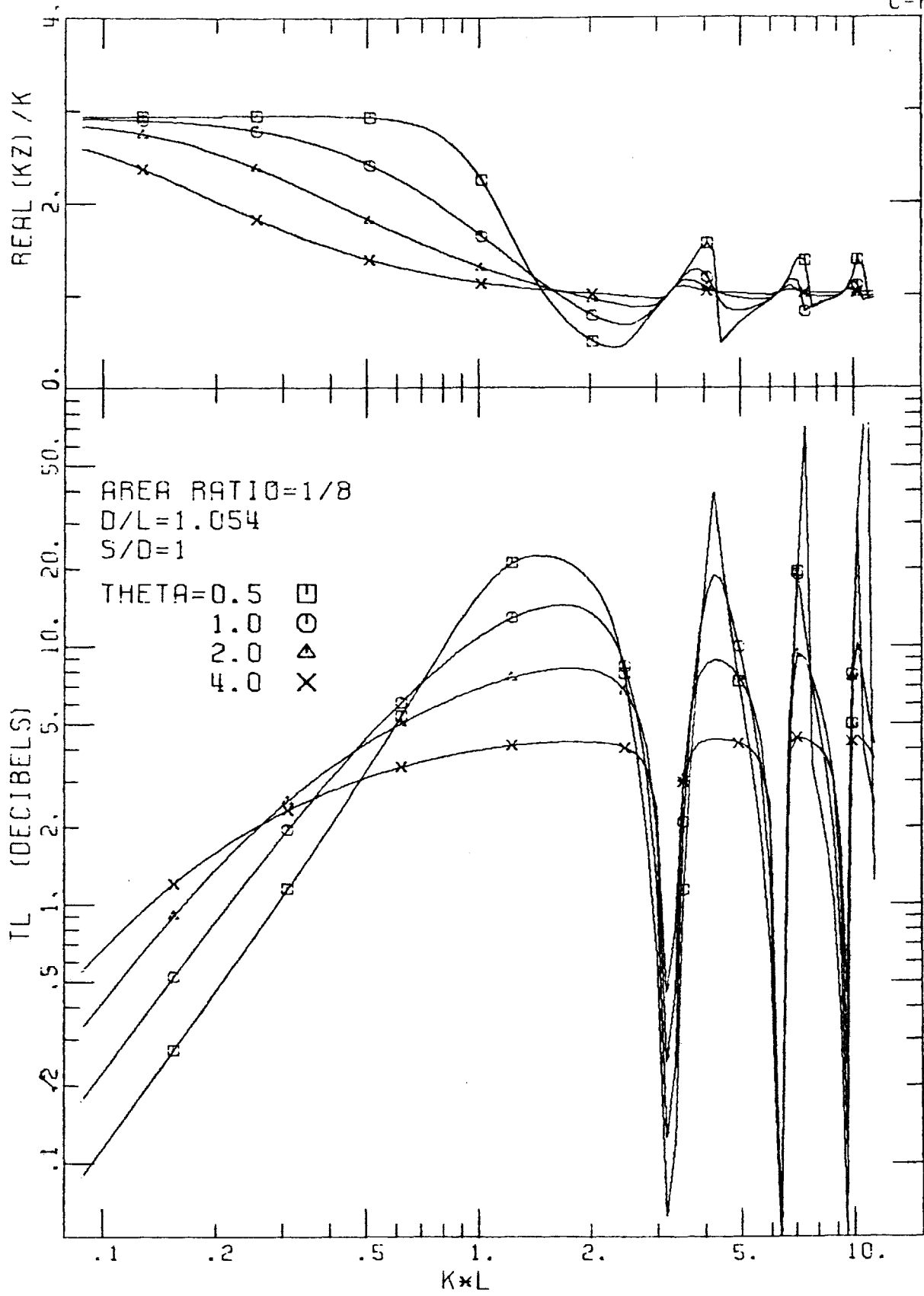


Figure A2.16

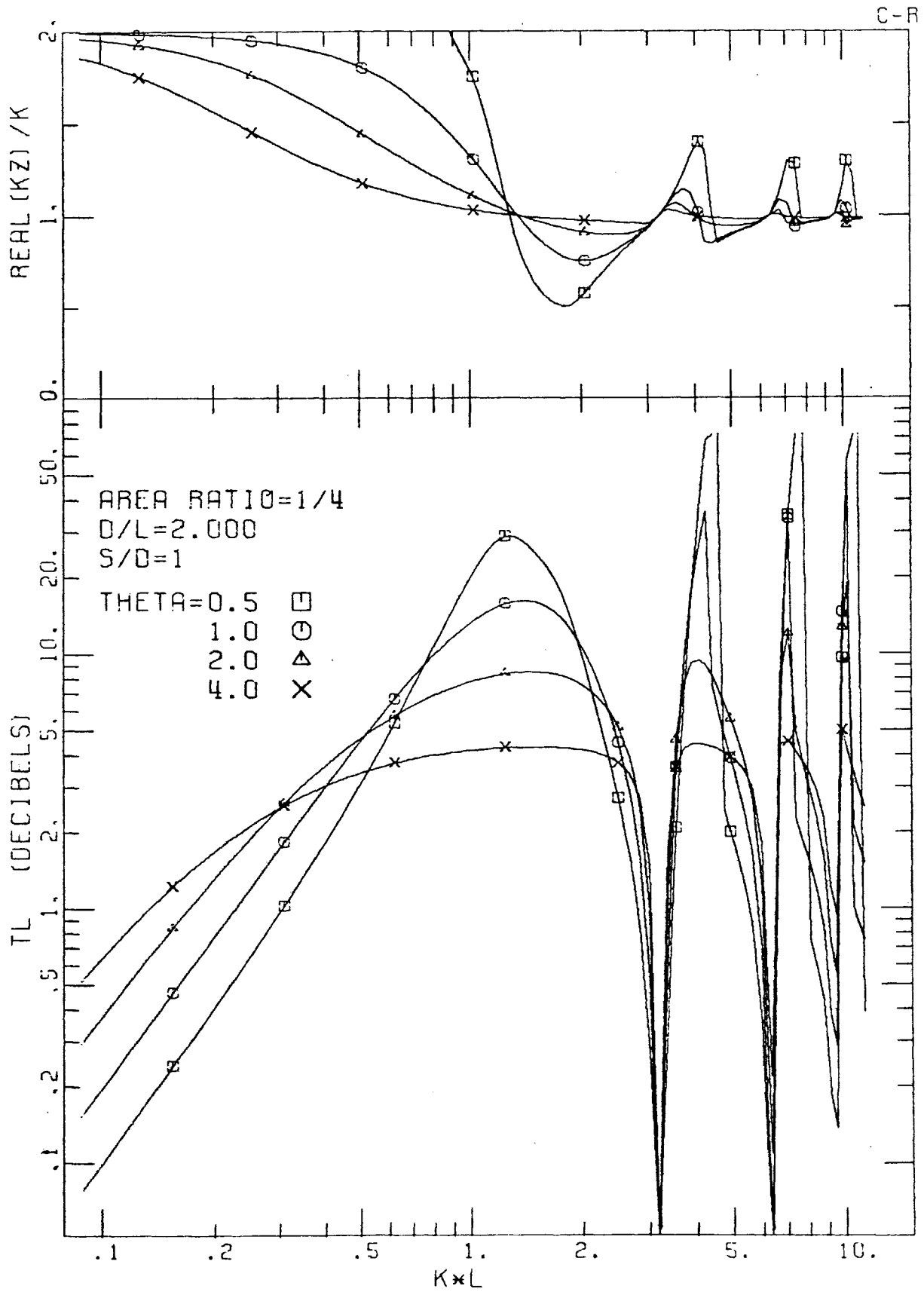


Figure A2.17

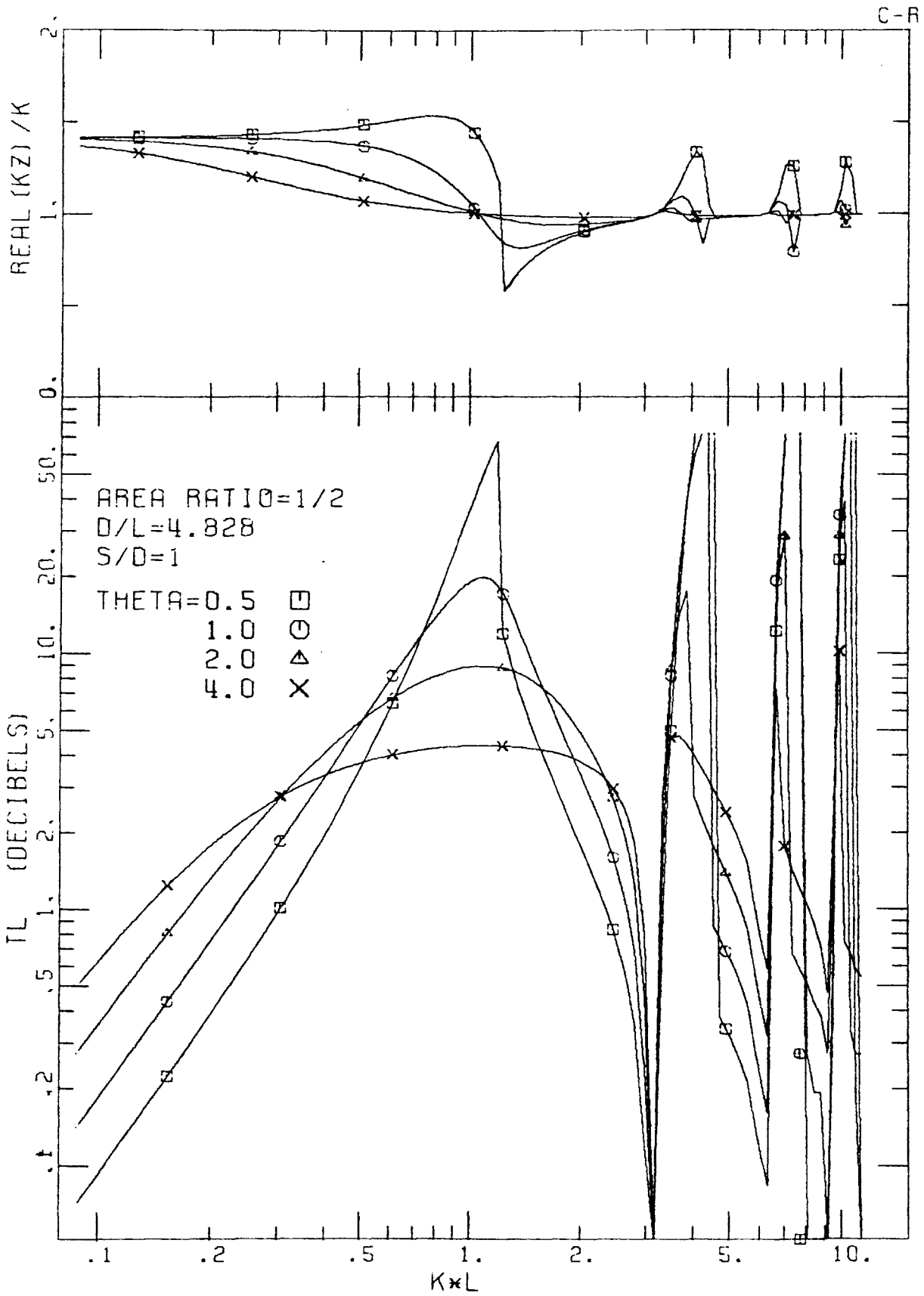


Figure A2.18

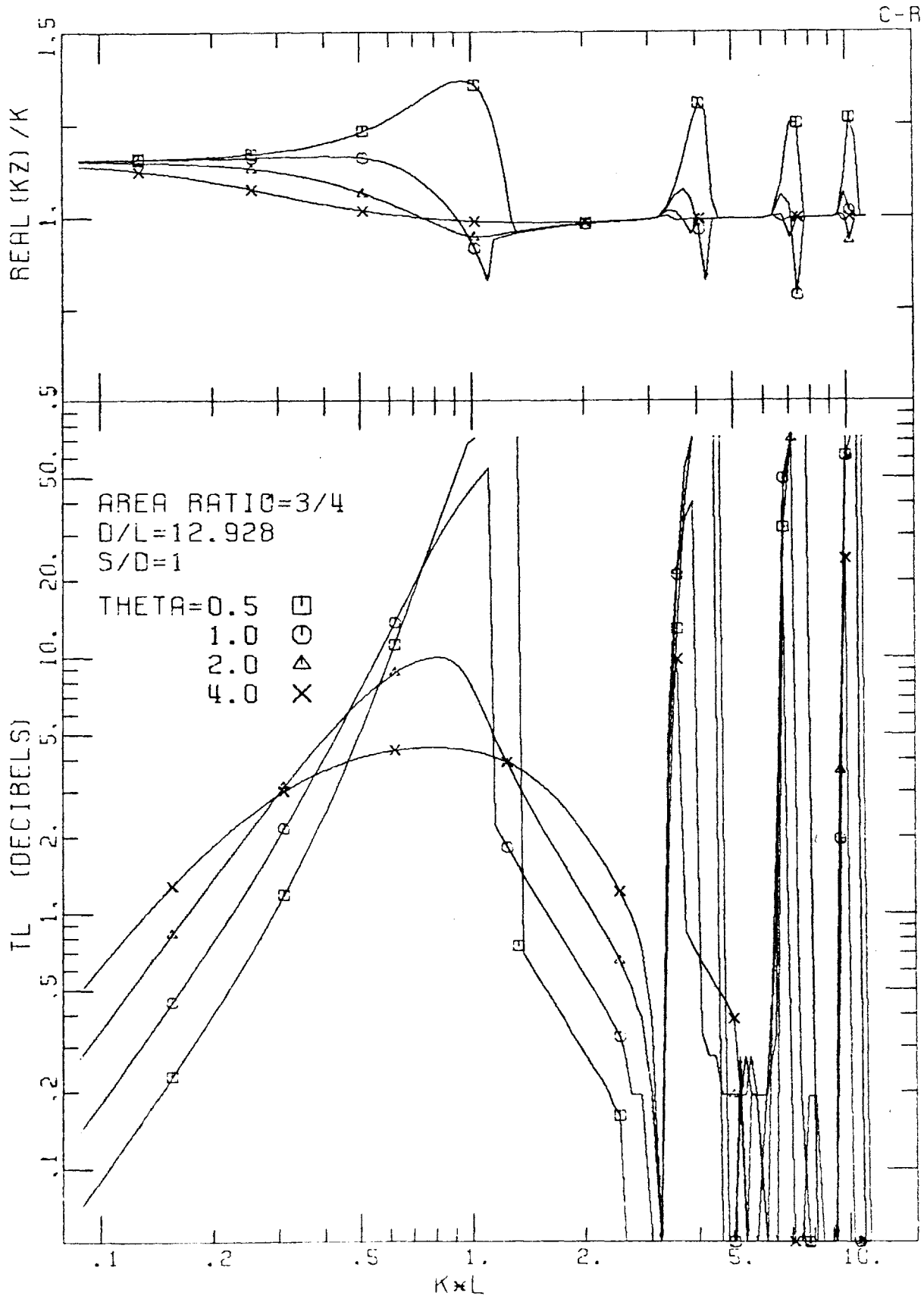


Figure A2.19

Figures A2.21 - A2.28: Real and imaginary parts of  $k_z$  for circular ducts lined with a porous liner. The format is the same as in Figures A2.16 - A2.19.

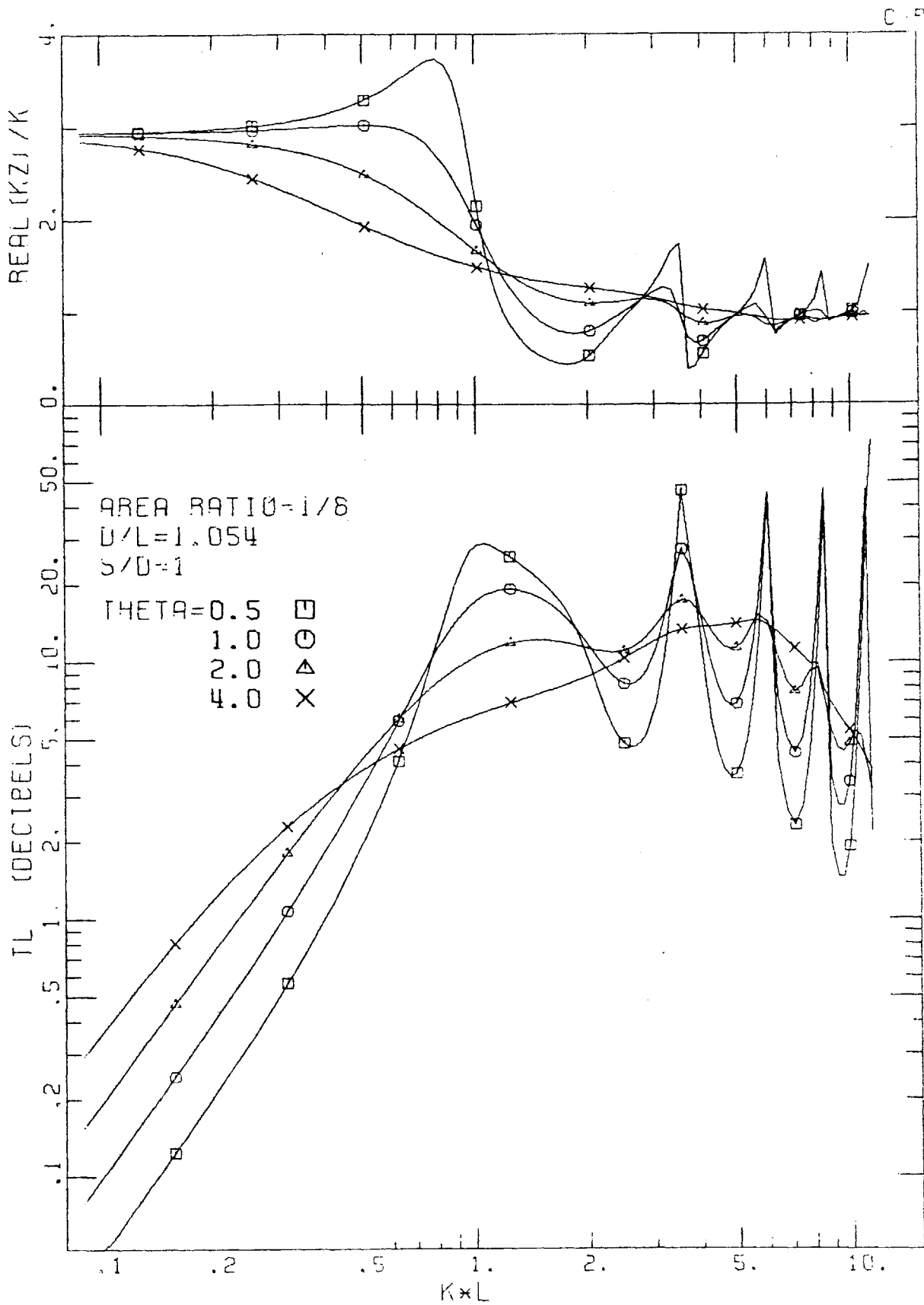


Figure A2.21



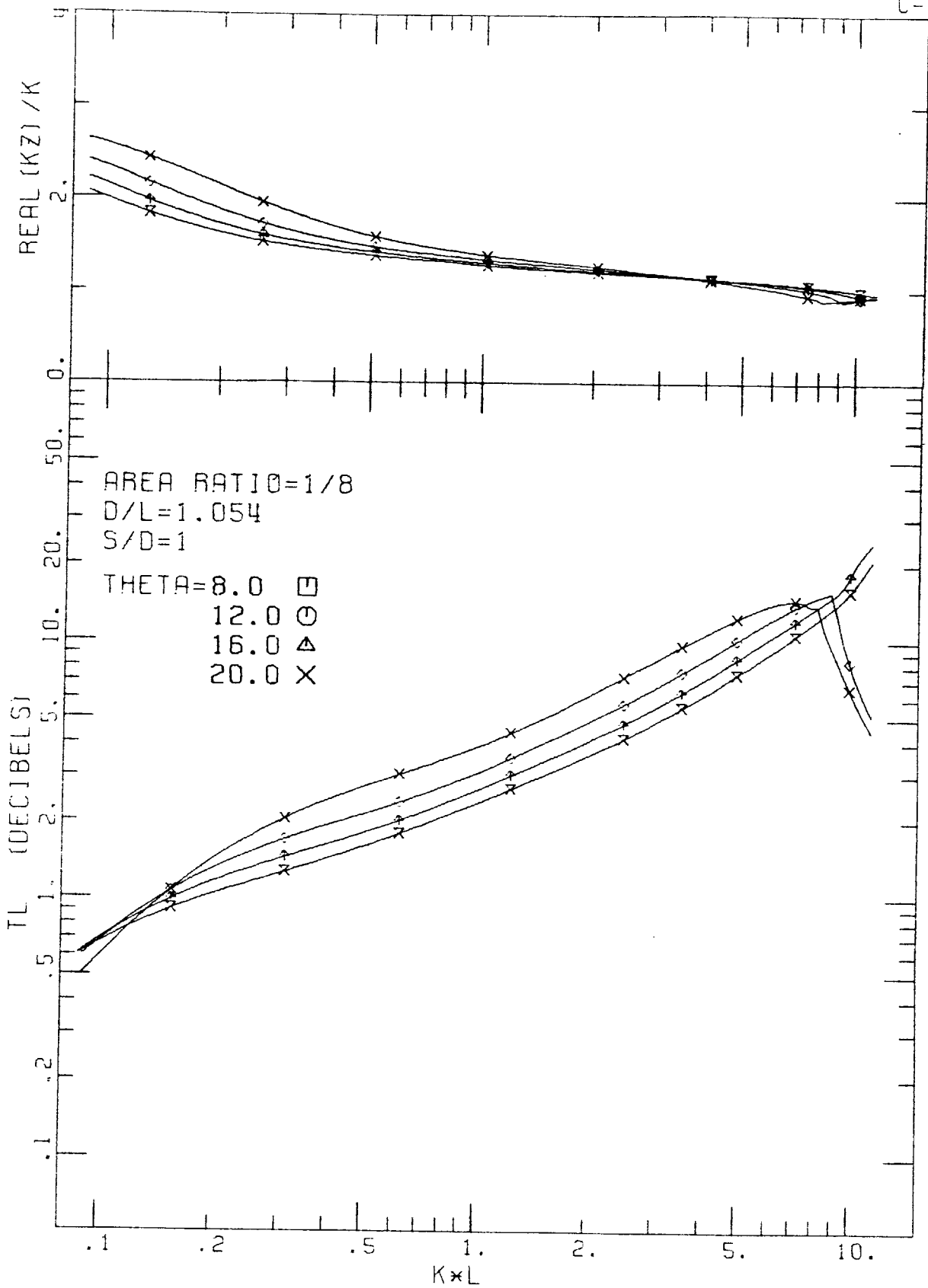


Figure A2.22

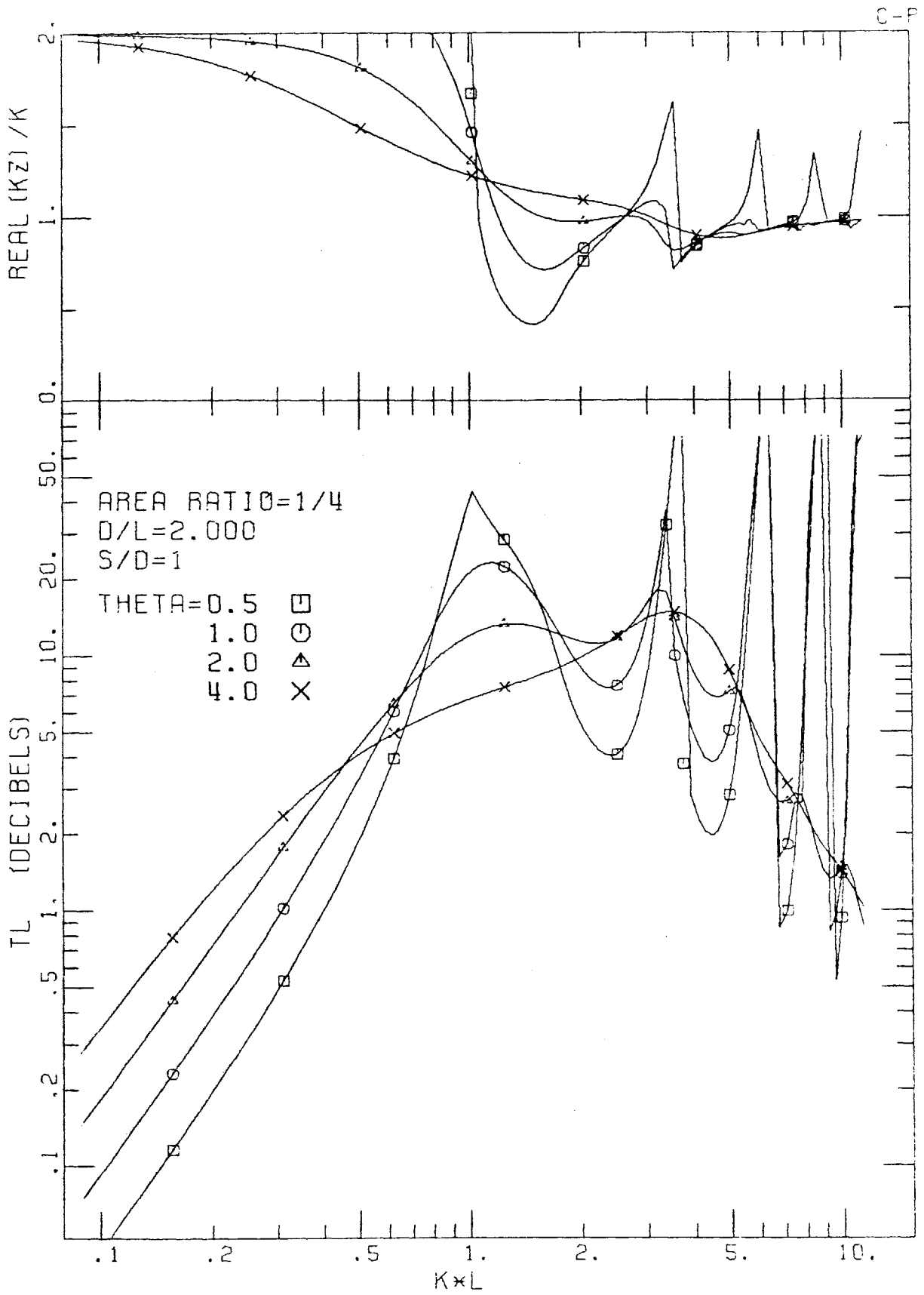


Figure A2.23

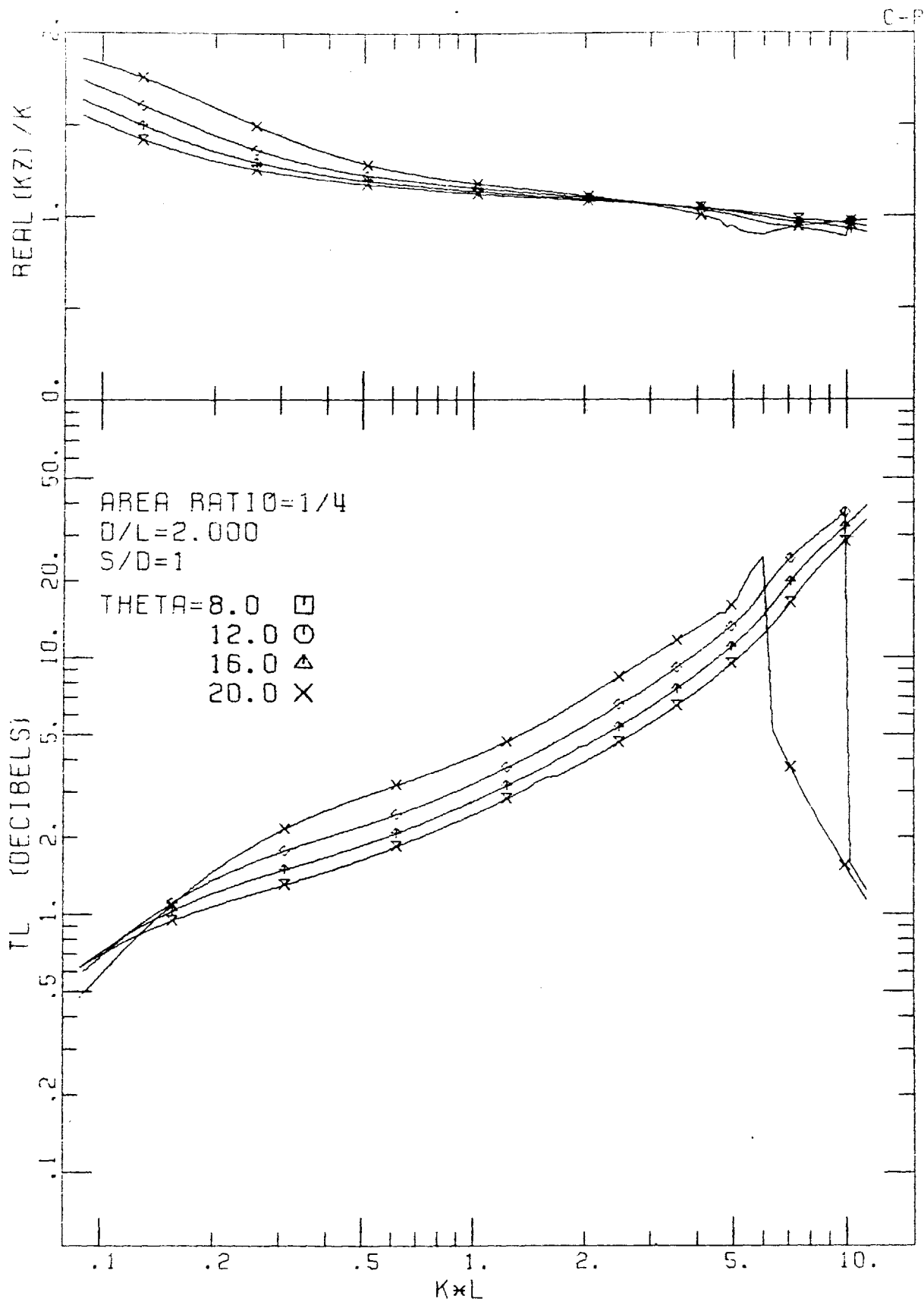


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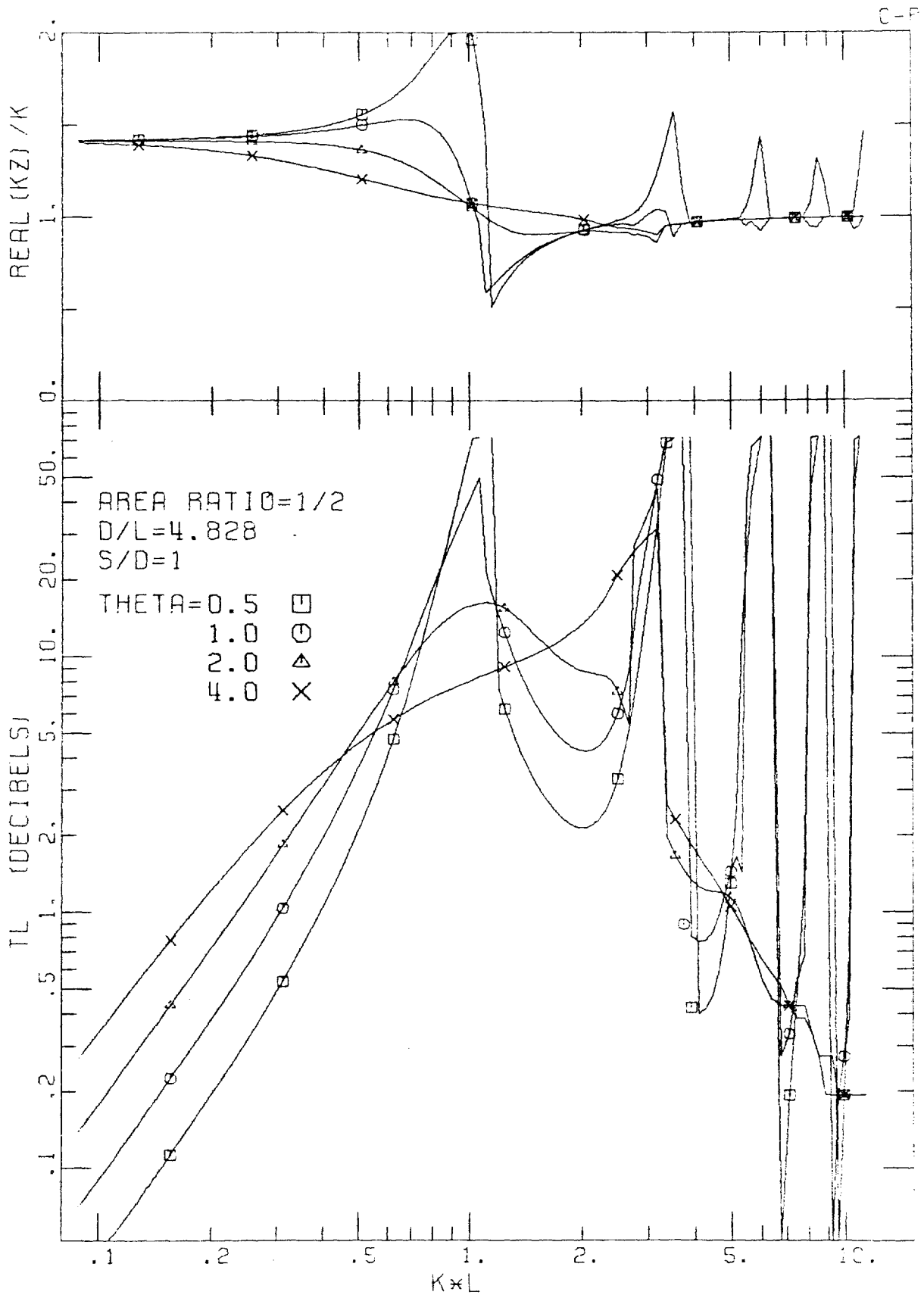


Figure A2.25

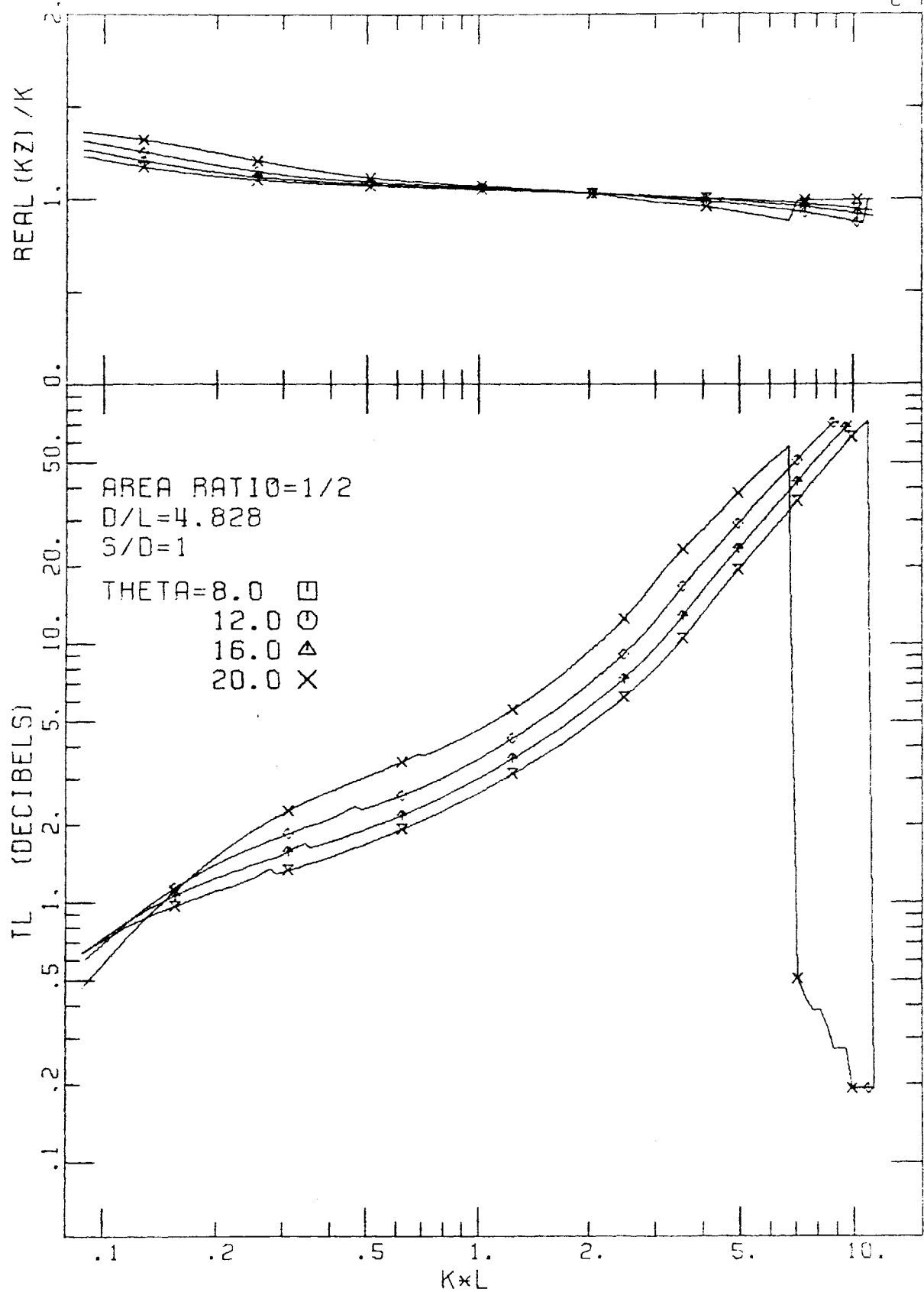


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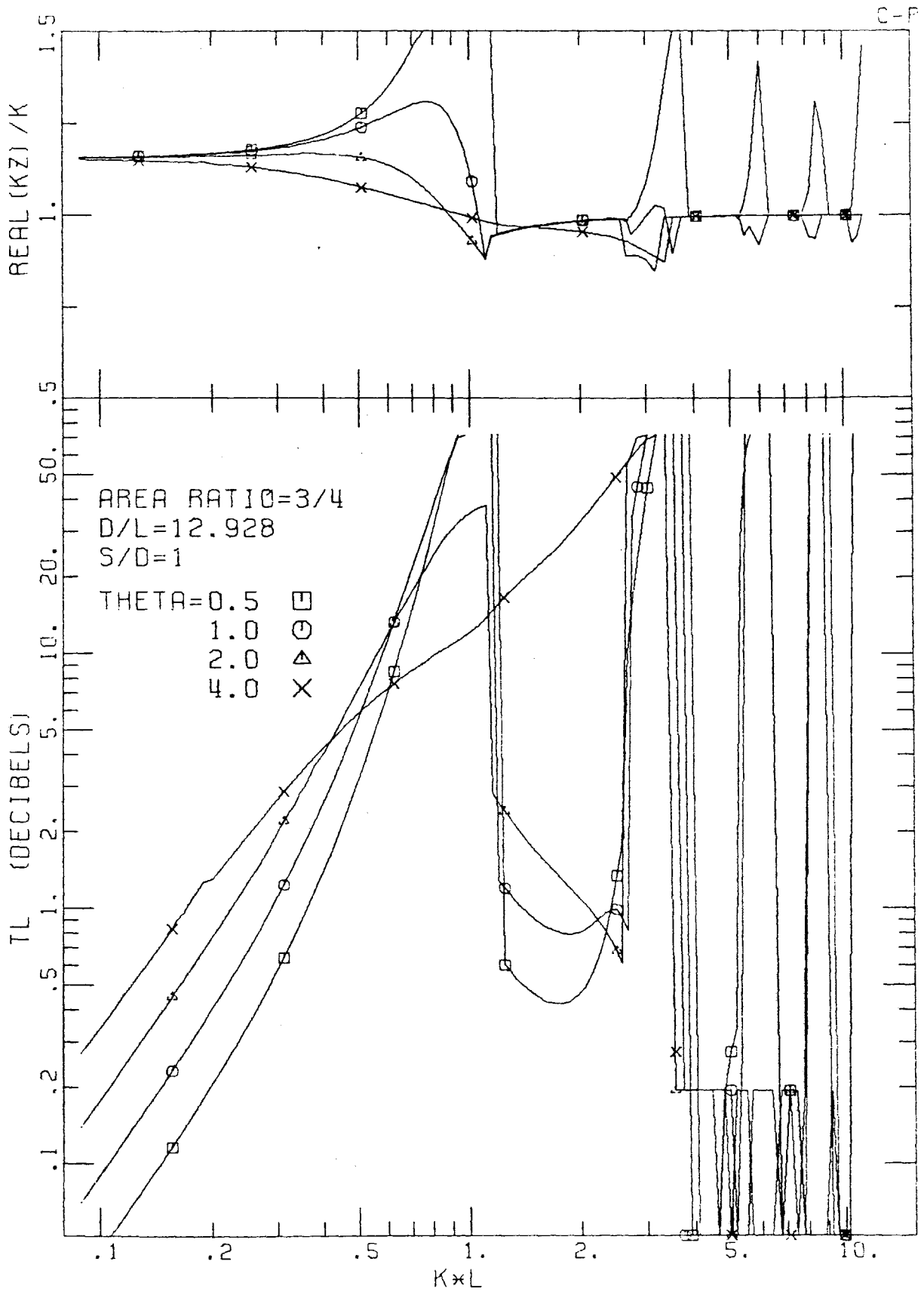


Figure A2.27

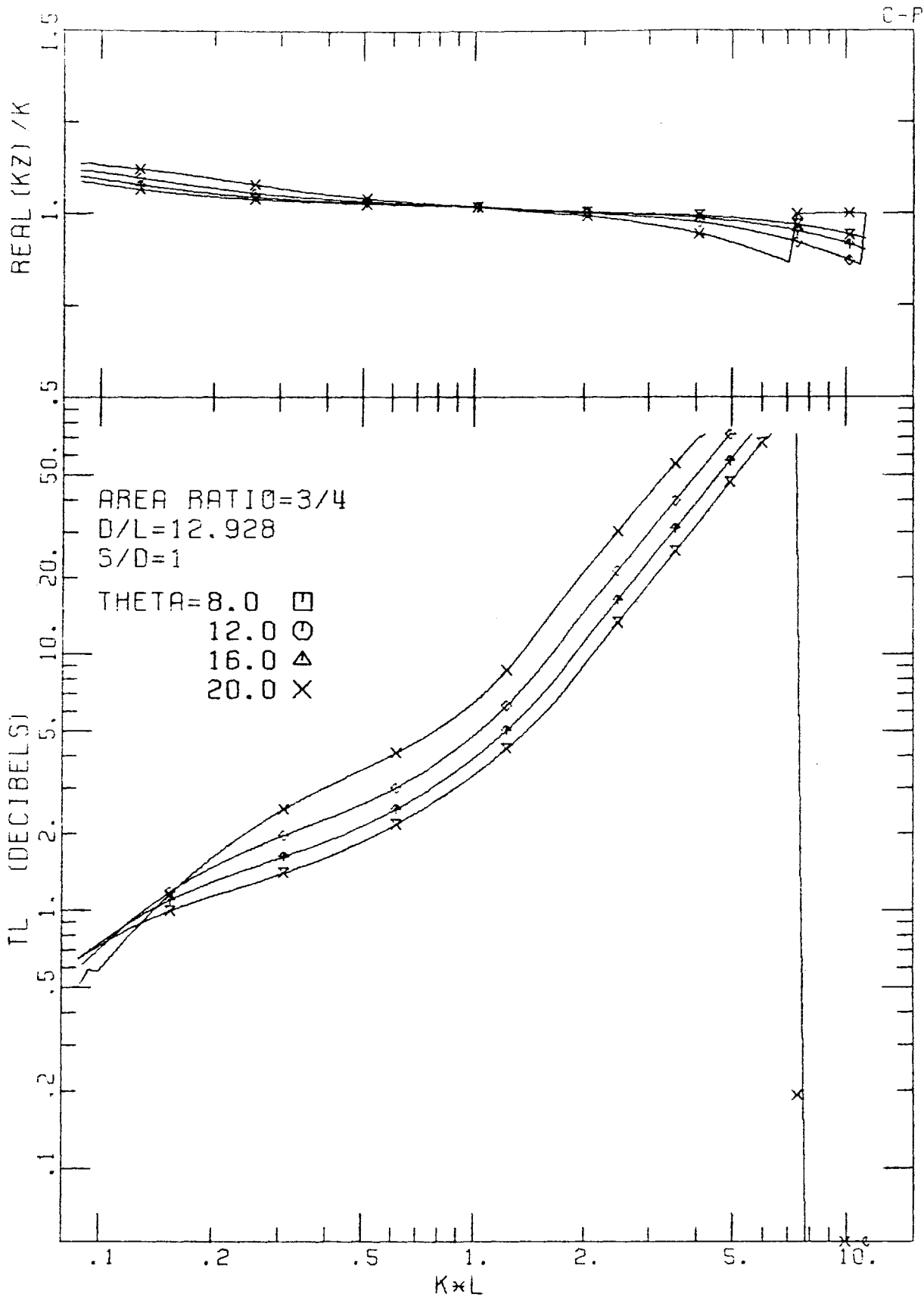


Figure A2.28

Figures A3.50 - A3.65: Octave band TL vs  $kL$  in circular ducts lined with a resistive screen type resonator liner. Each figure corresponds to a different combination of values of the screen resistance  $\theta$  and  $D/L$ . Each figure contains three frames corresponding to different spectra of the incident wave as indicated by  $N$ . In each frame five curves are given corresponding to five values of the duct length parameter  $S/D$ , which are given at the corner of each figure.



Figure A3.50

THETA=0.5  
D/L=1.094  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

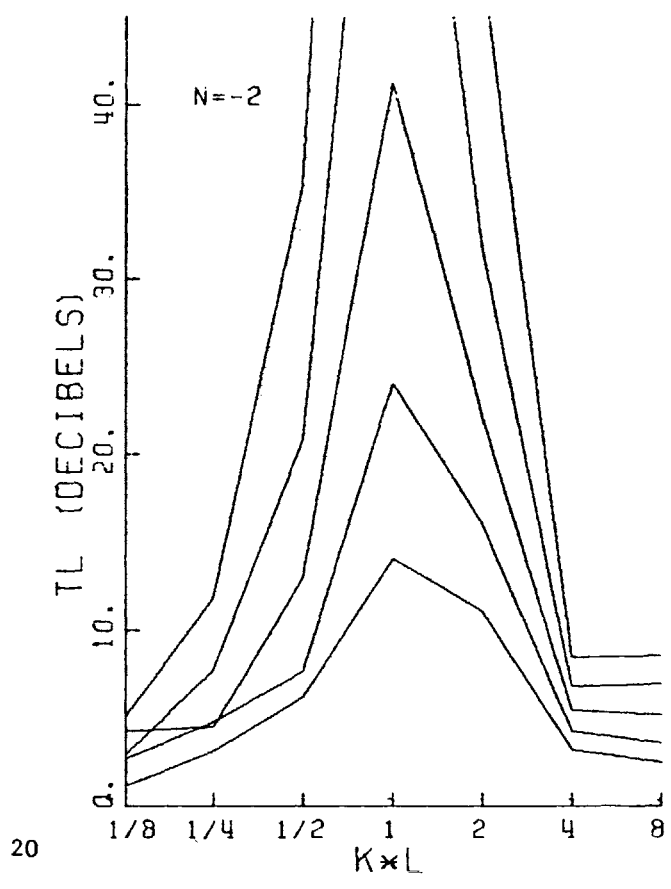
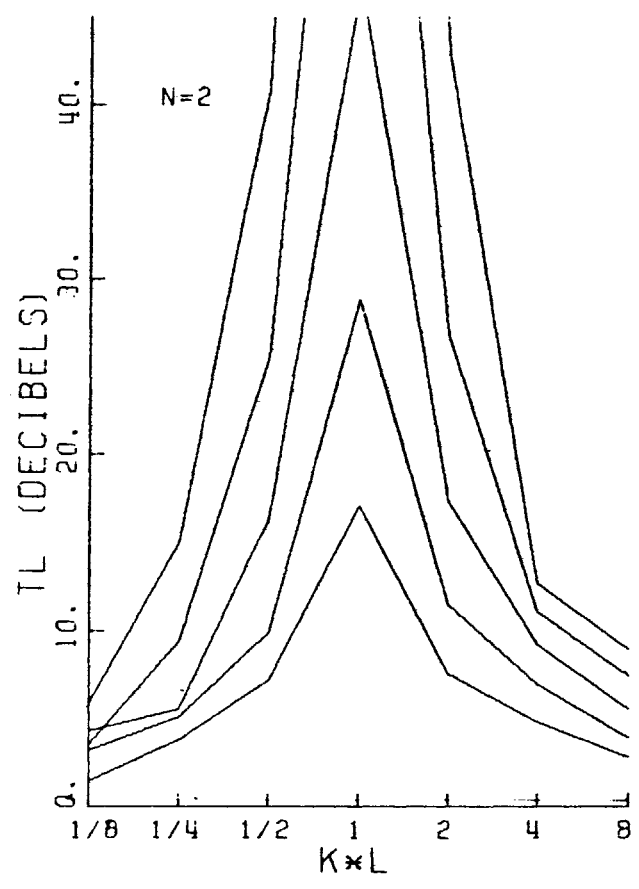
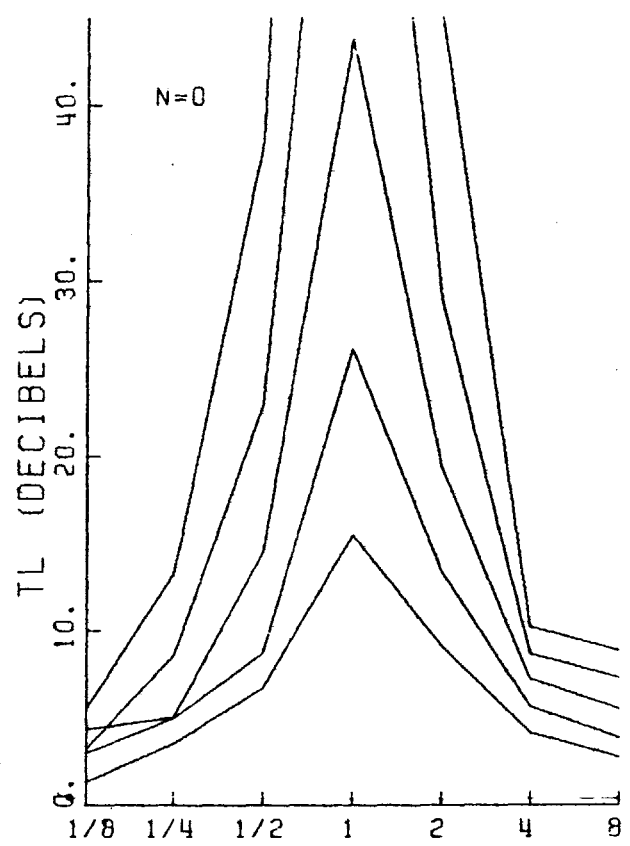


Figure A3.51

THETA=0.5  
 D/L=2.000  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

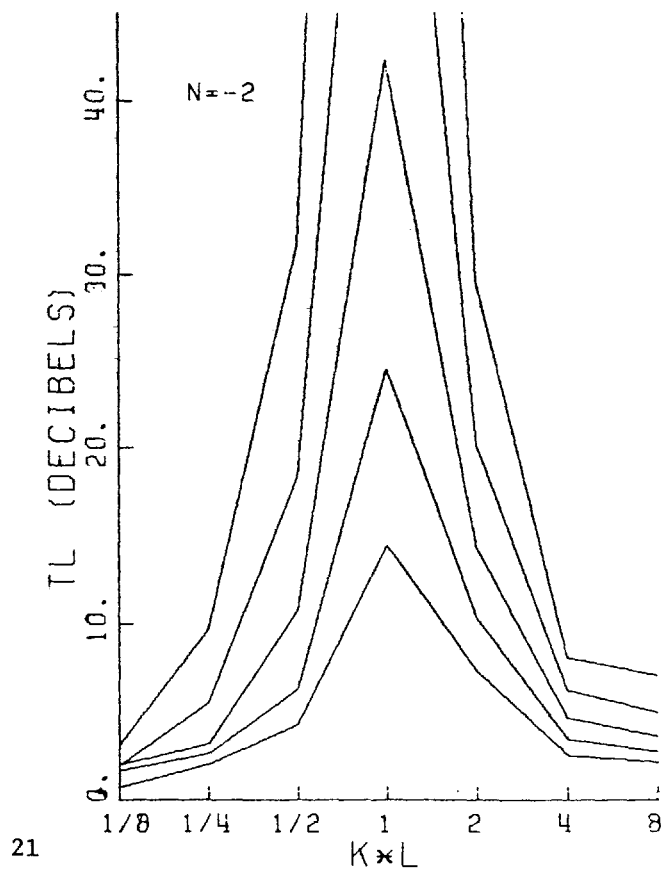
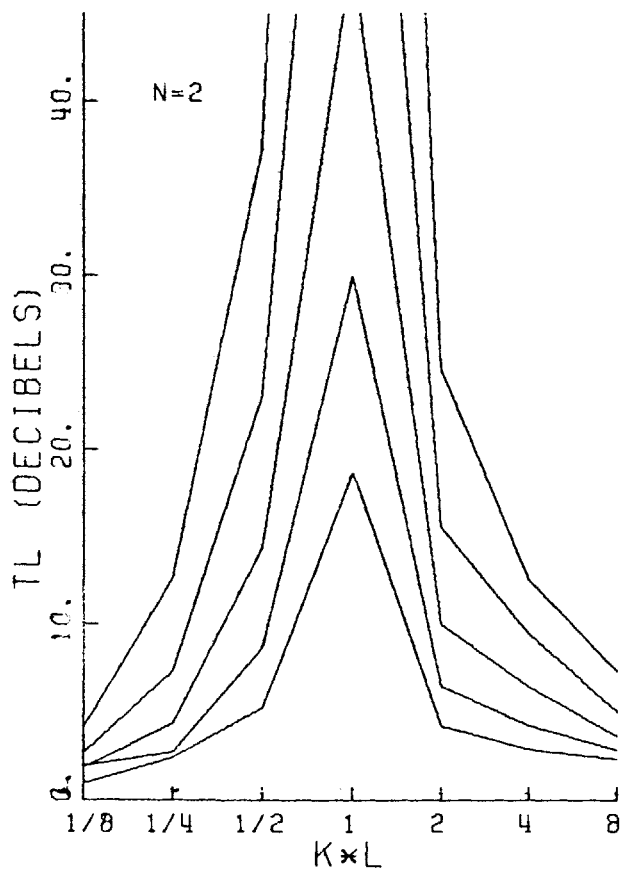
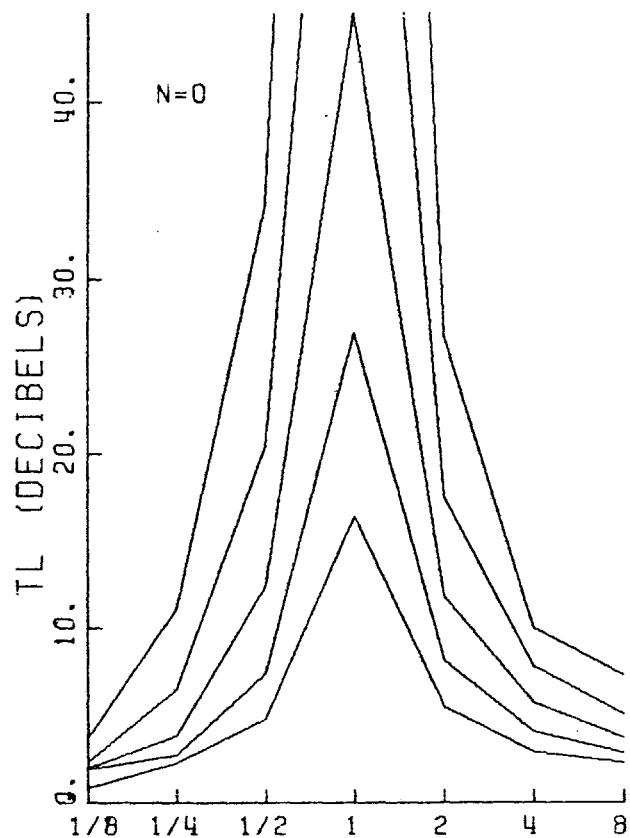


Figure A3.52

THETA=0.5  
D/L=4.828  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

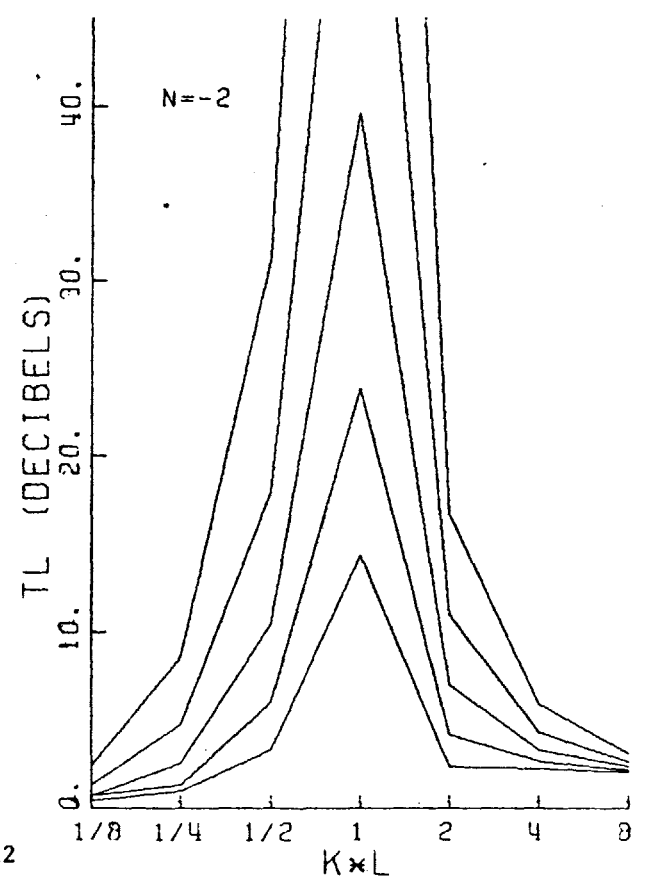
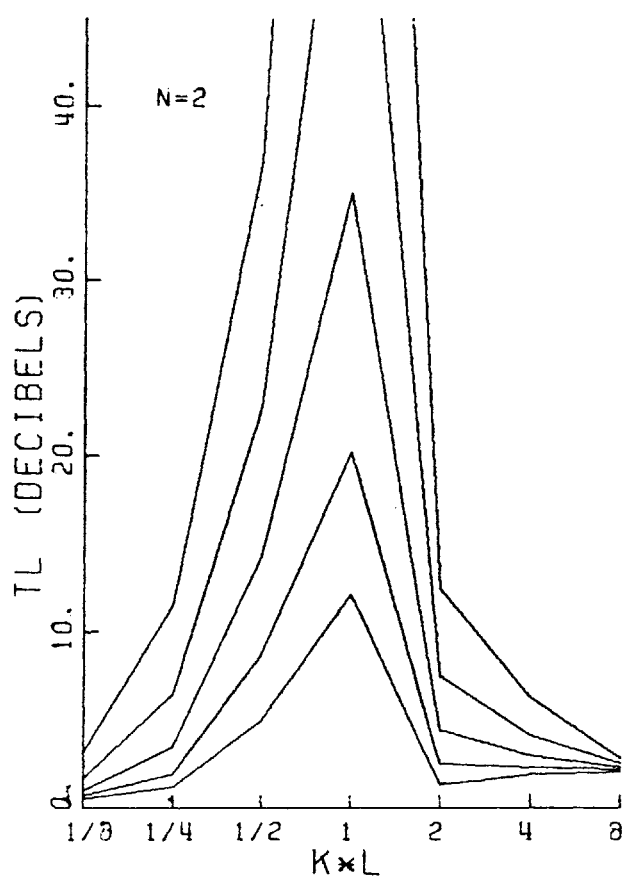
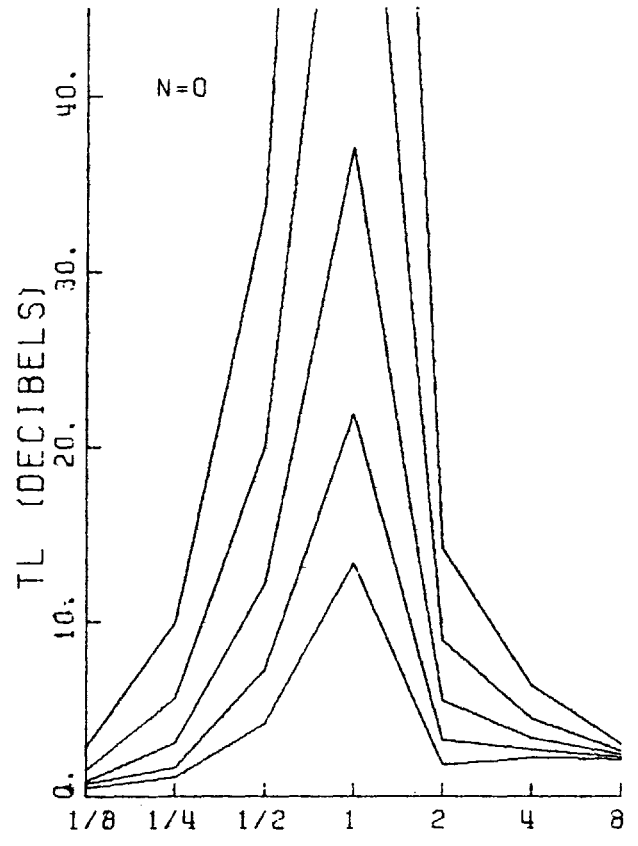


Figure A3.53

THETA=0.5  
D/L=12.928  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

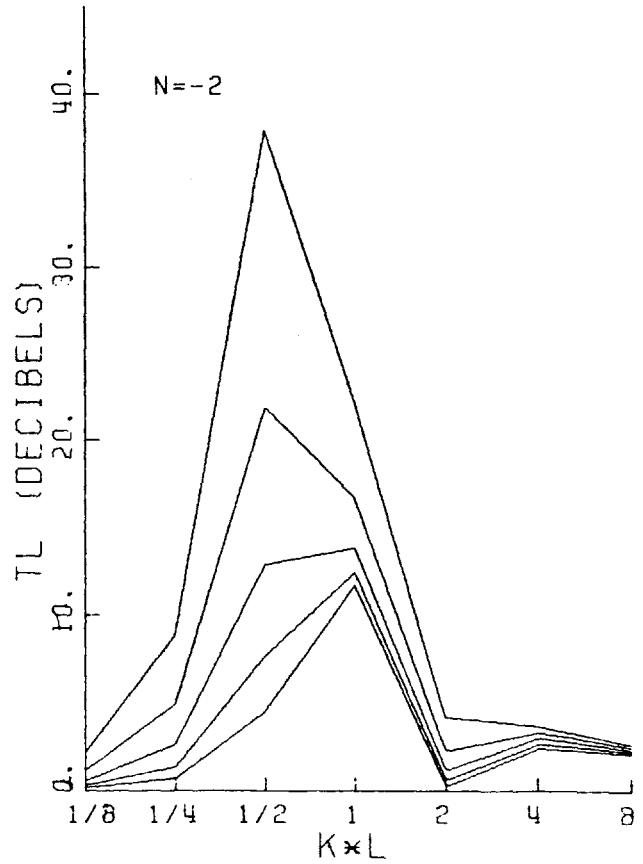
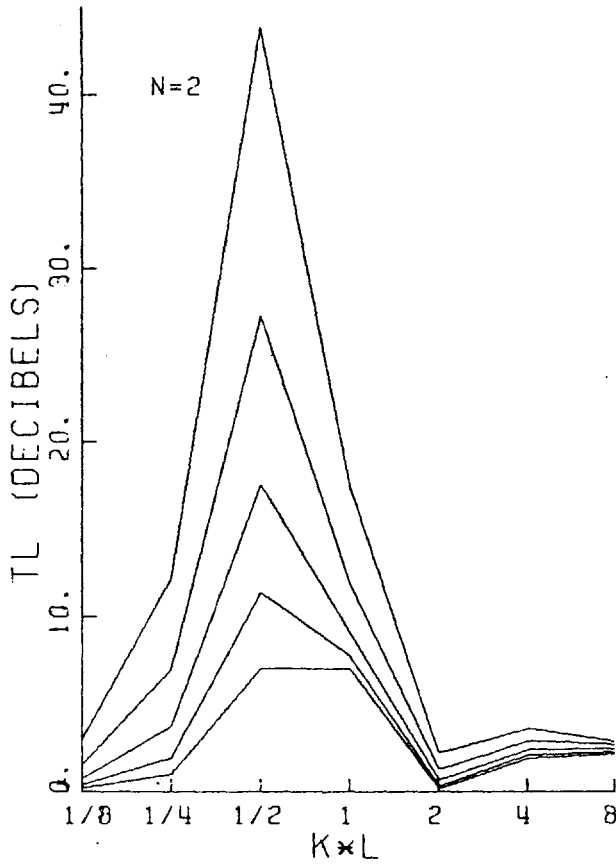
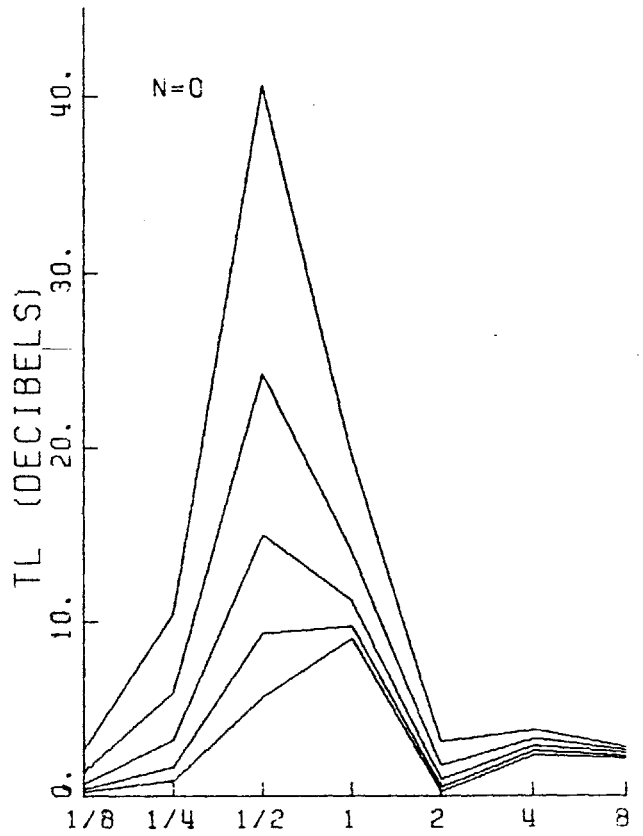


Figure A3.54

THETA=1.  
 D/L=1.094  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

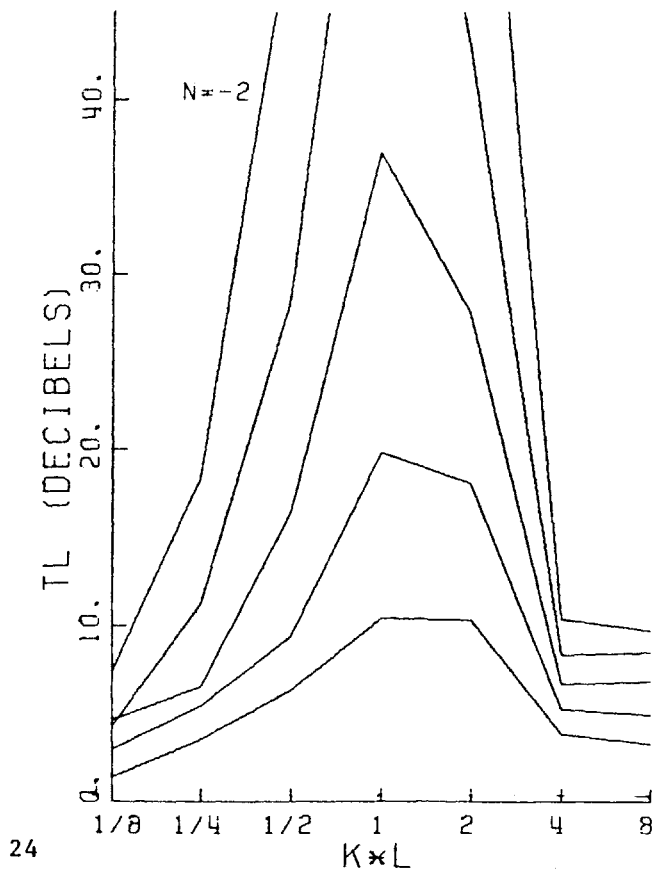
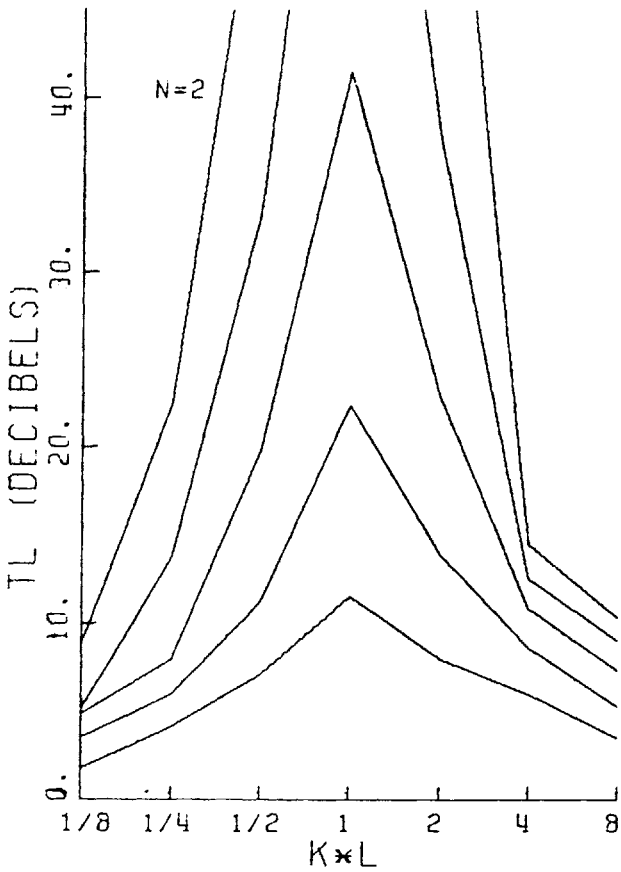
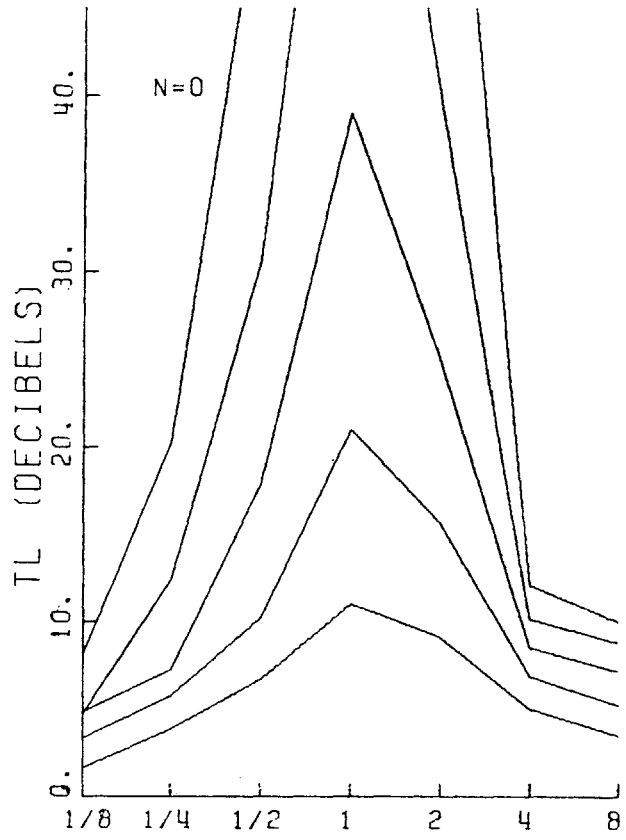


Figure A3.55

THETA=1.  
D/L=2.000  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

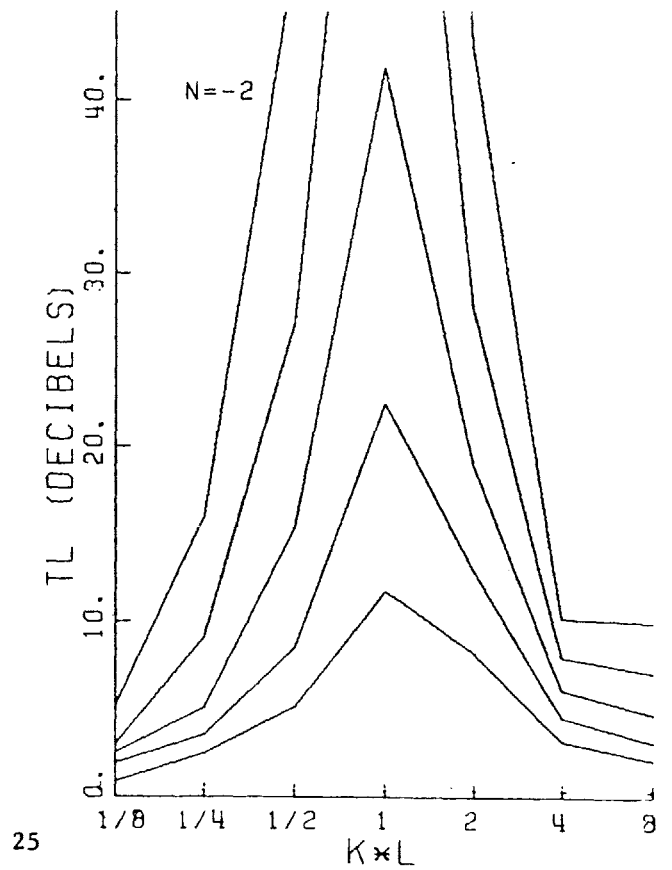
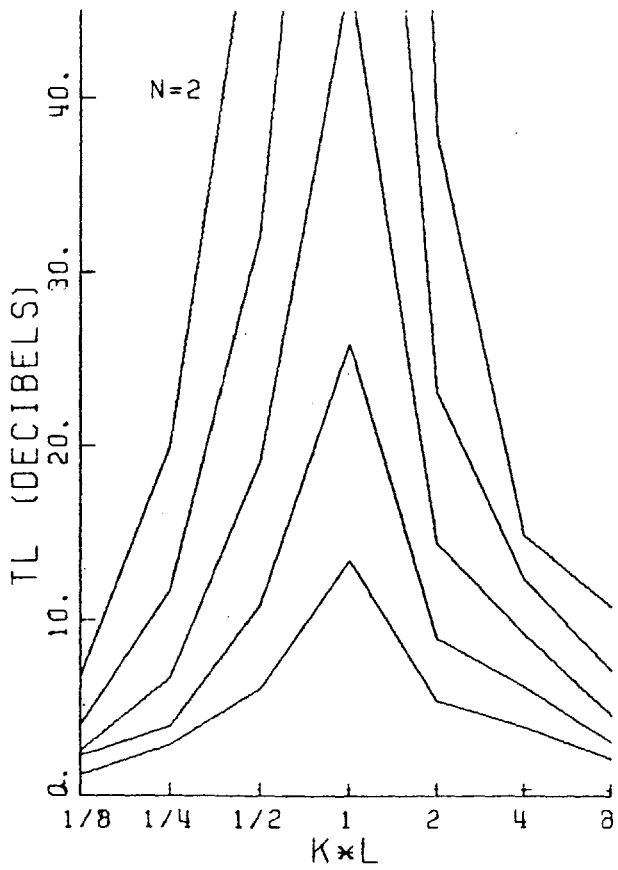
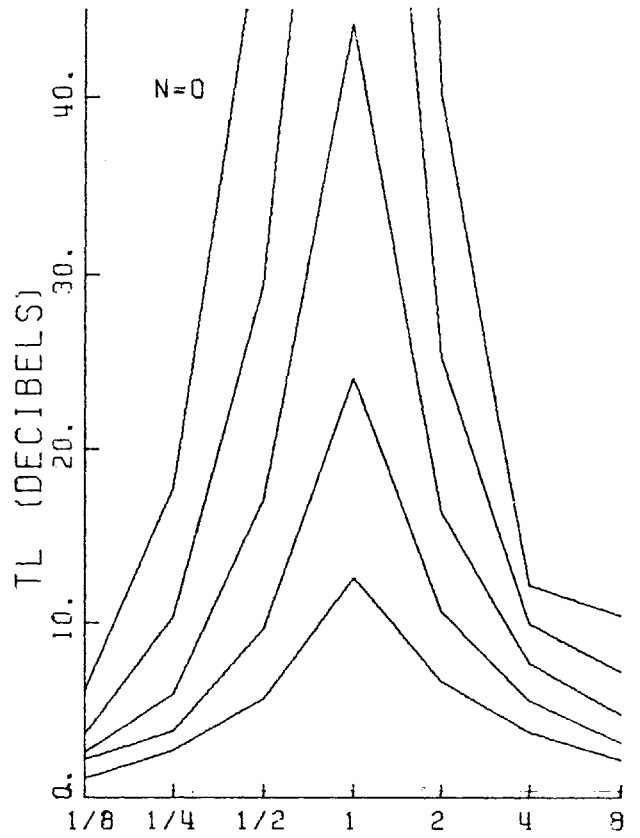


Figure A3.56

THETA=1.  
 D/L=4.828  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

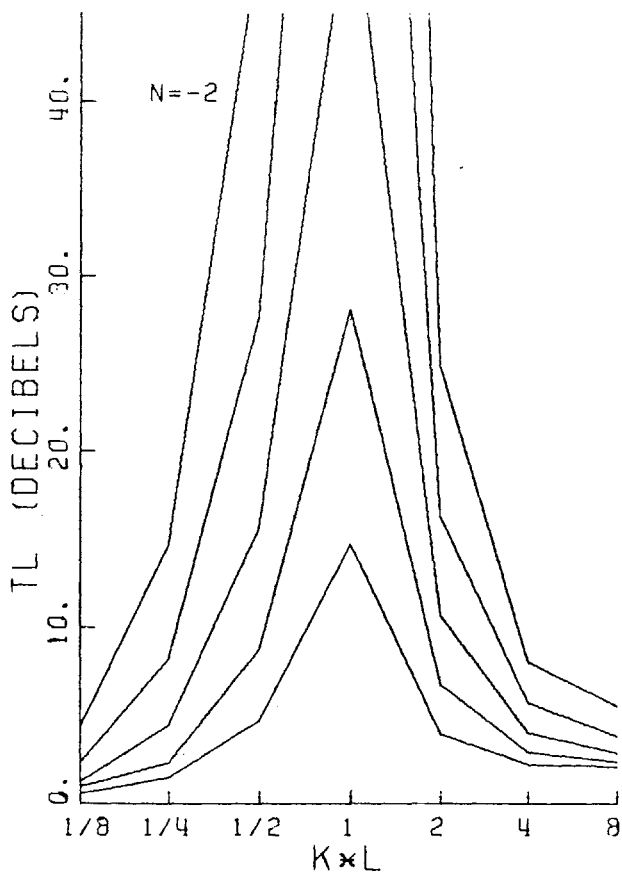
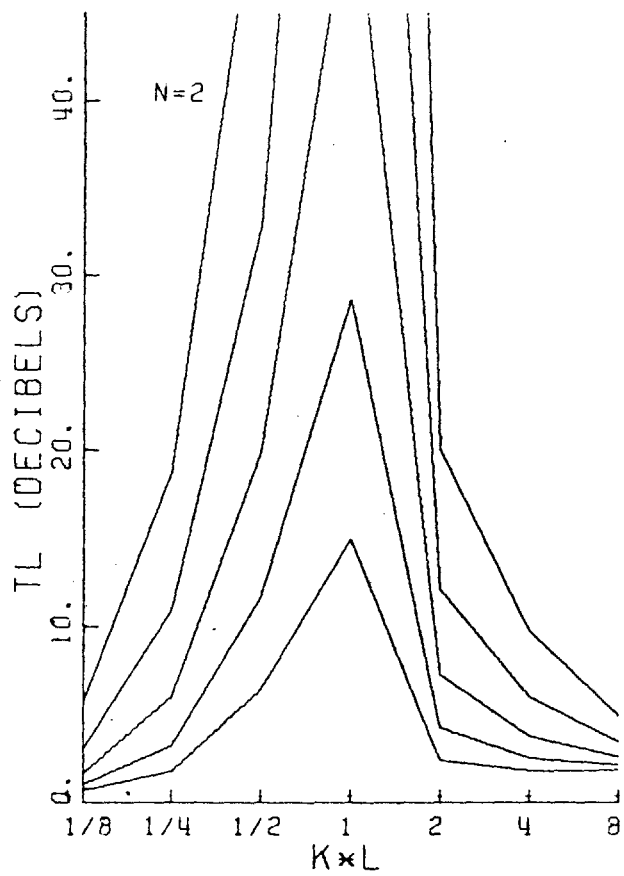


Figure A3.57

THETA=1.  
 D/L=12.928  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

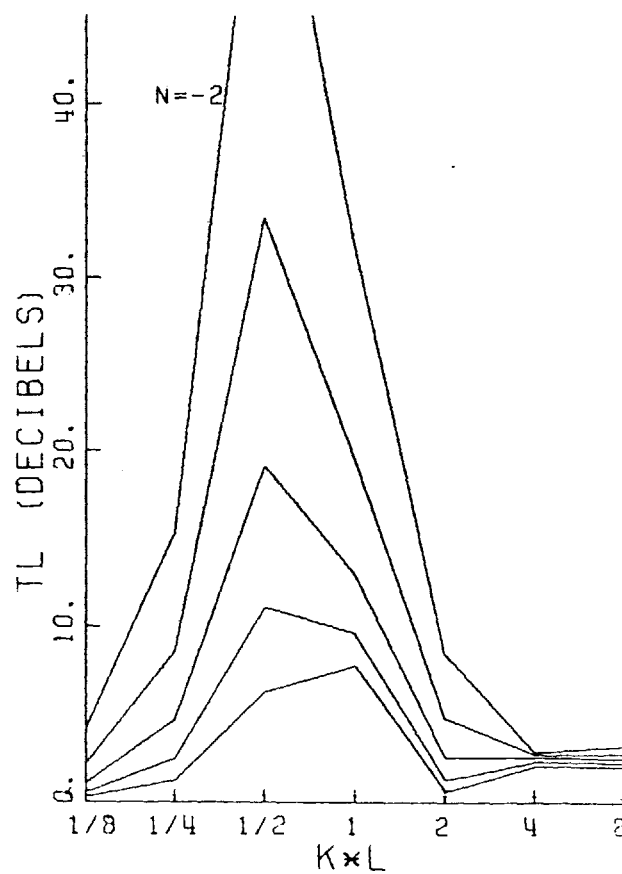
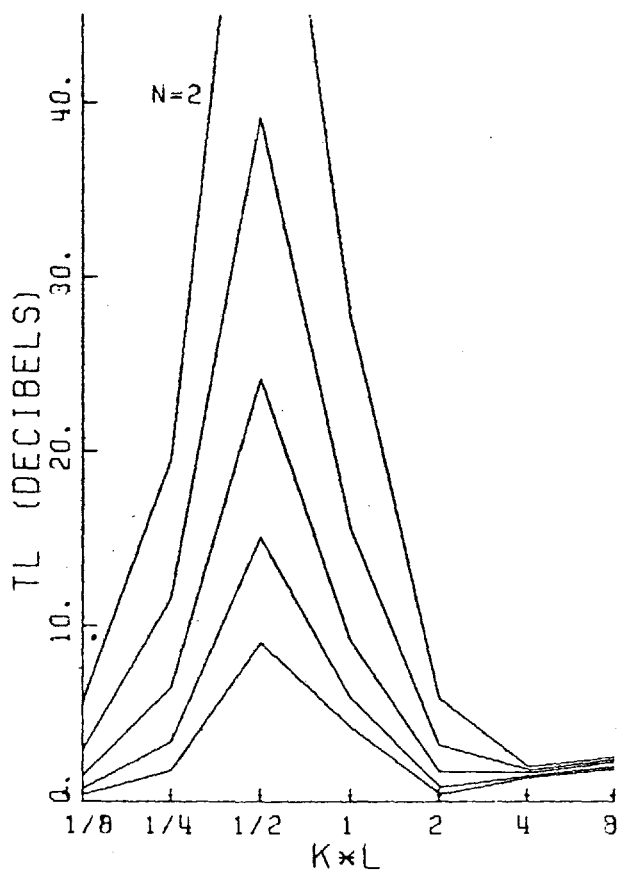




Figure A3.58

THETA=2.  
 D/L=1.094  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

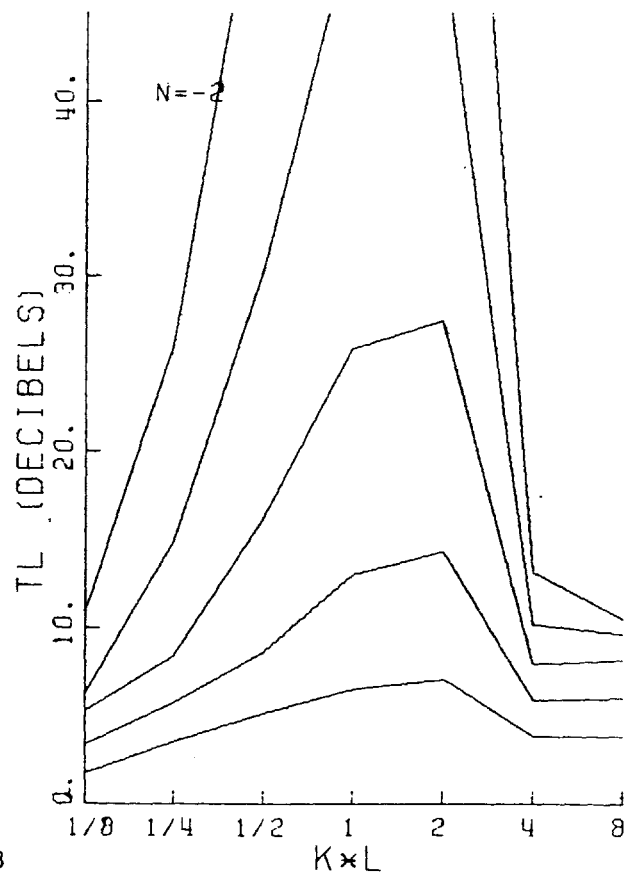
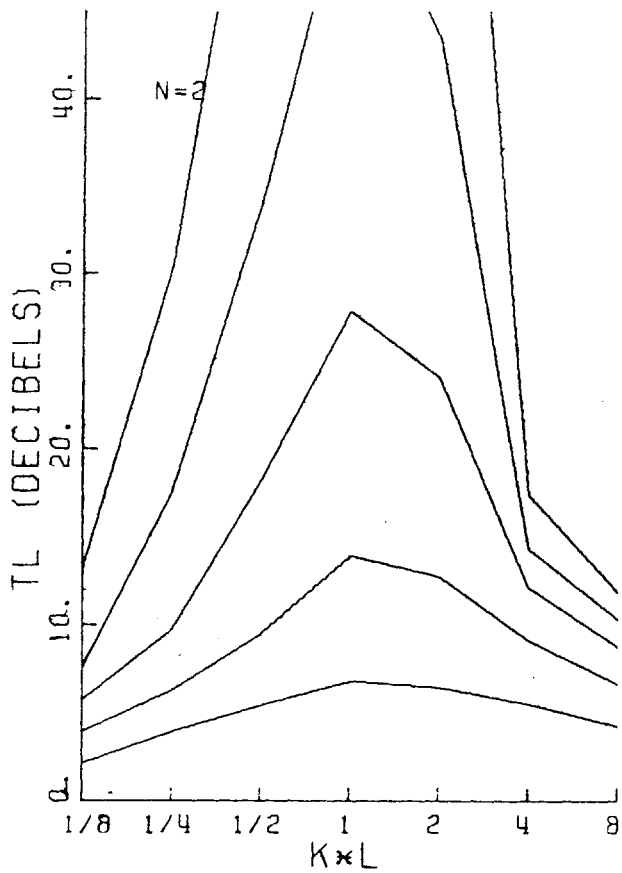
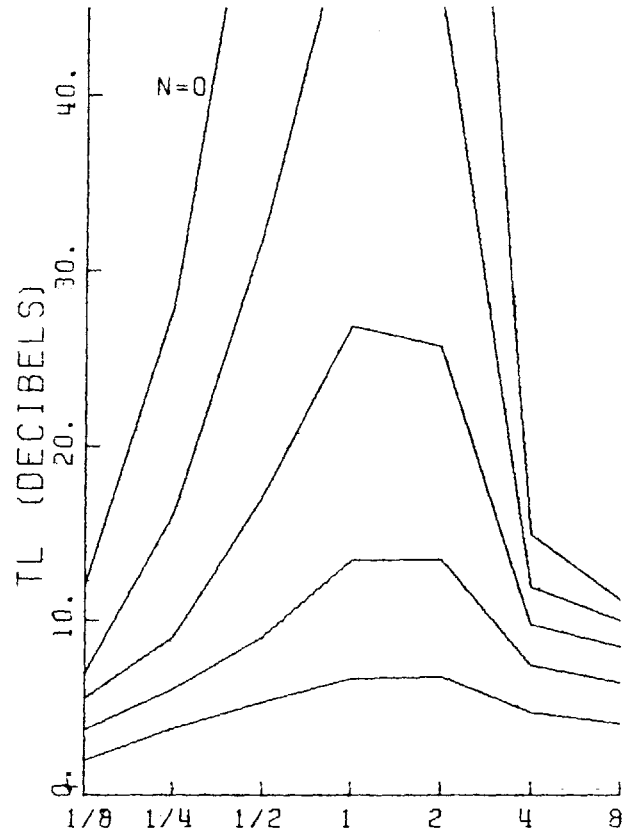


Figure A3.59

THETA=2.  
 D/L=2.000  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

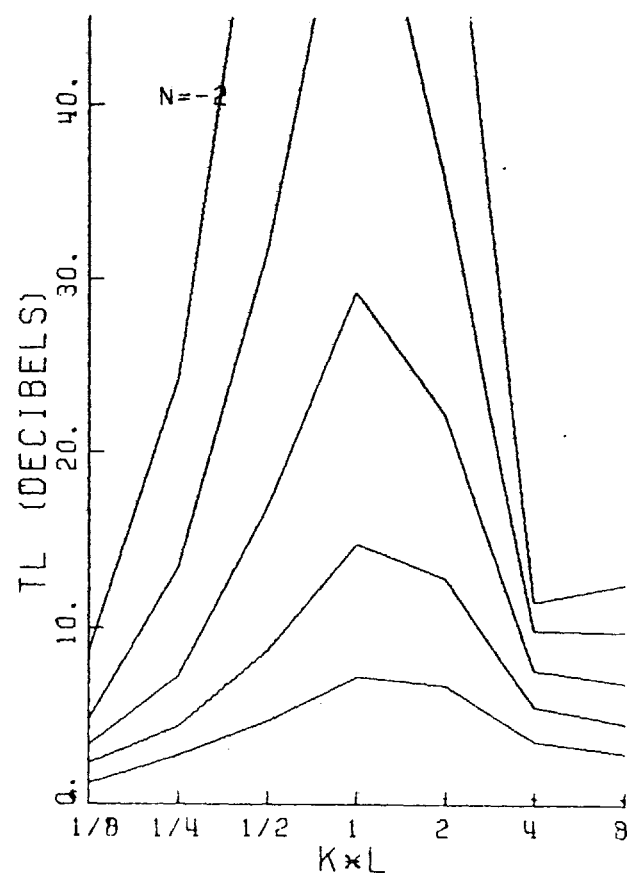
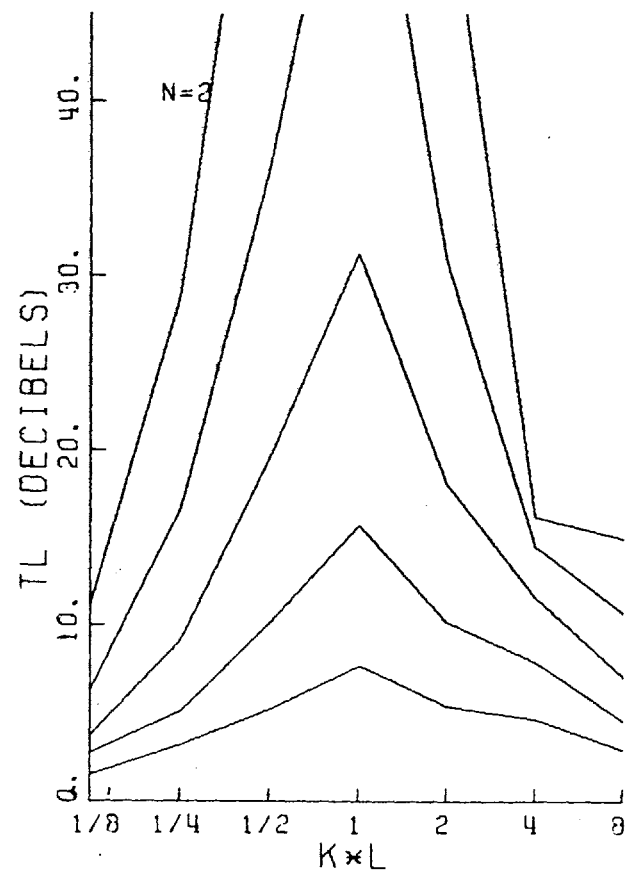
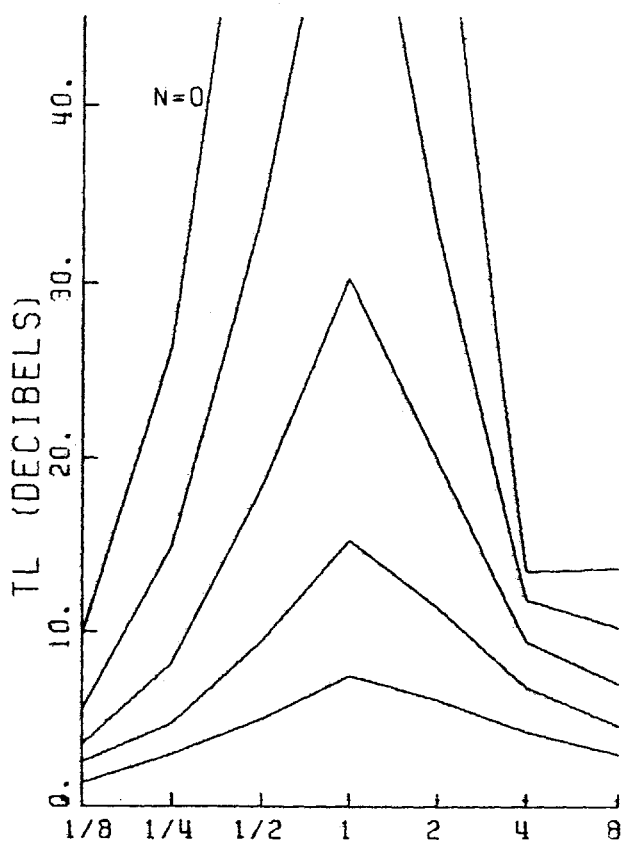


Figure A3.60

THETA=2.  
 D/L=4.828  
 AREA RATIO=1  
 S/D=16  
       8  
       4  
       2  
       1

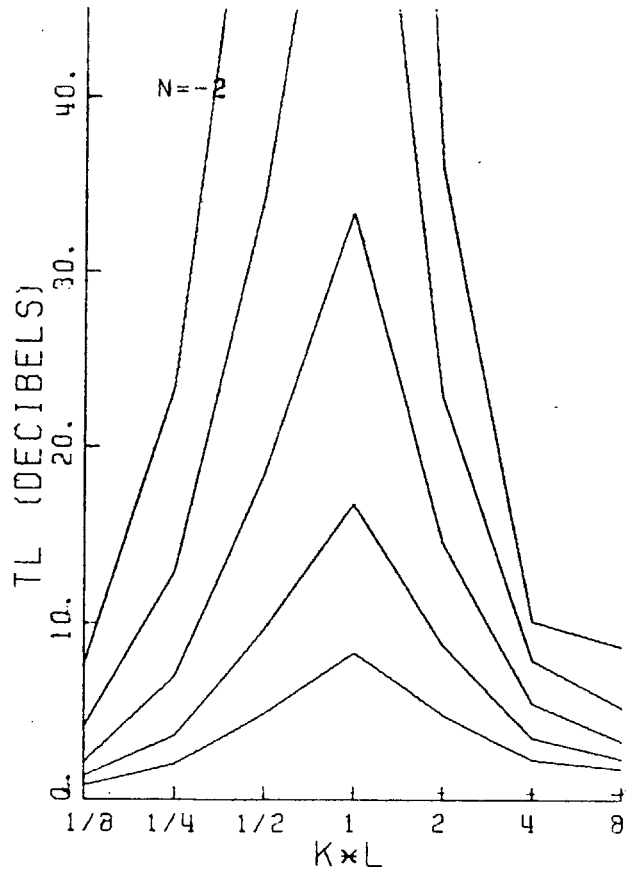
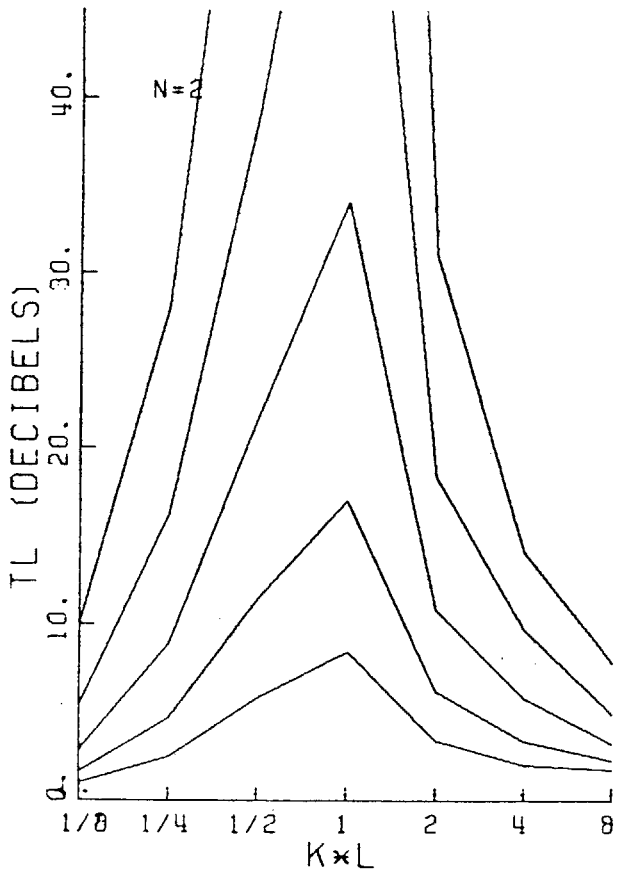
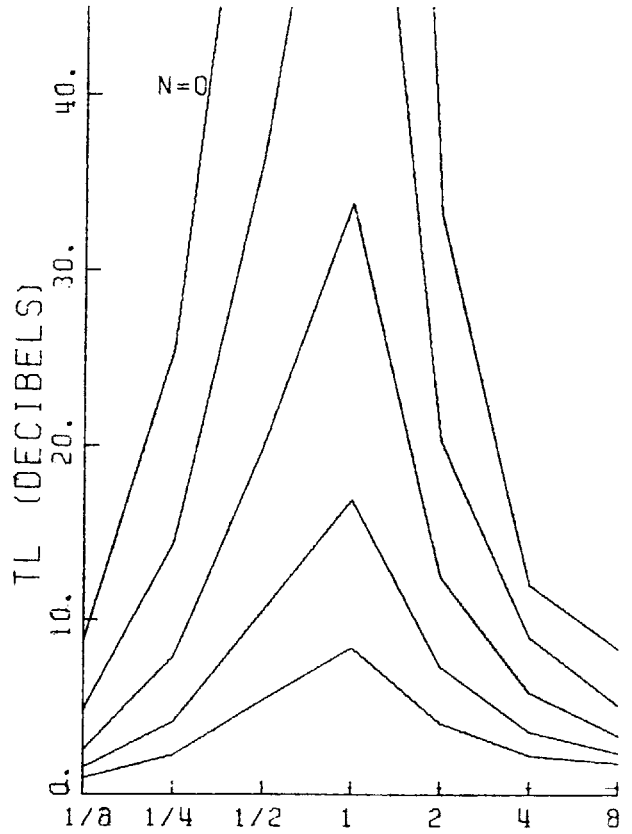


Figure A3.61

THETA=2.  
D/L=12.928  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

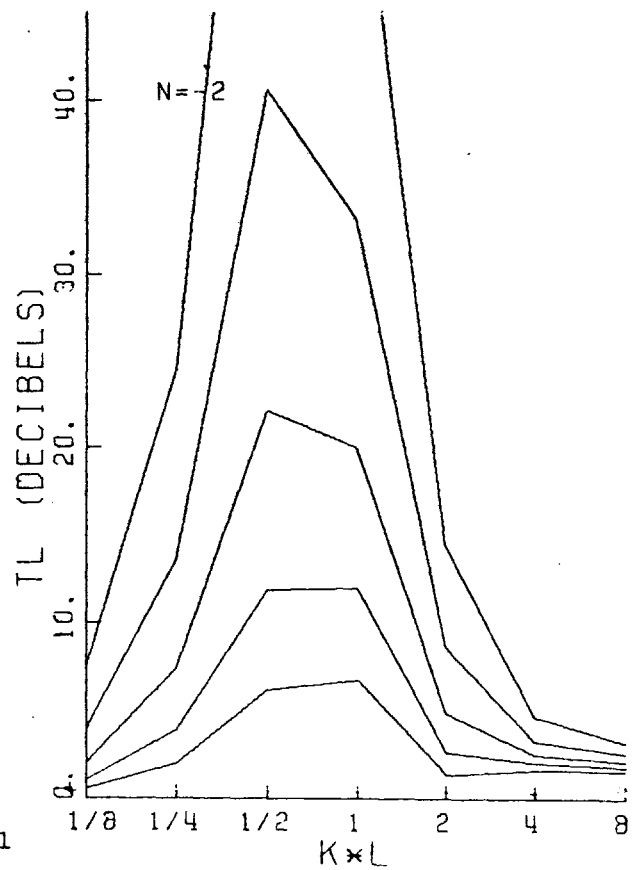
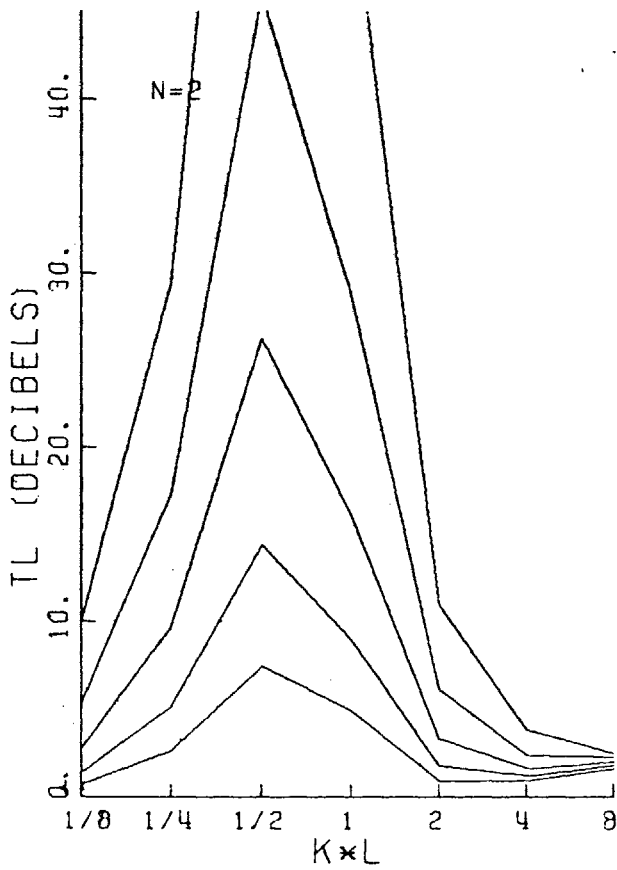
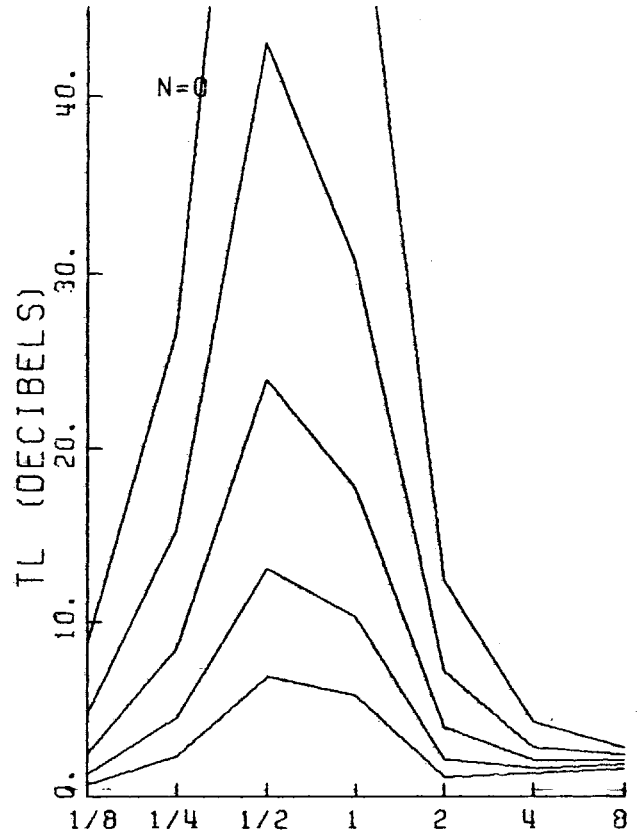


Figure A3.62

THETA=4.  
 D/L=1.094  
 AREA RATIO=1

S/D=16

8

4

2

1

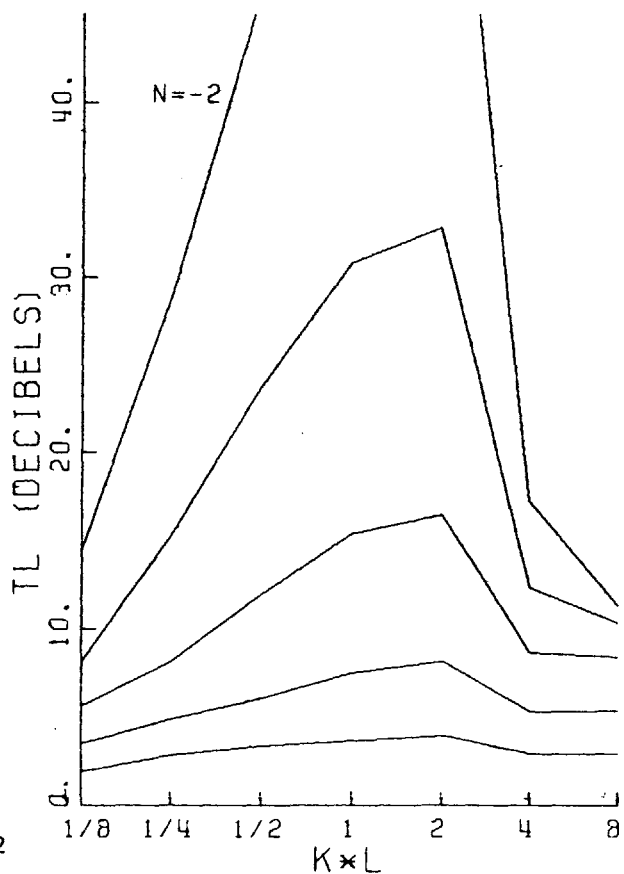
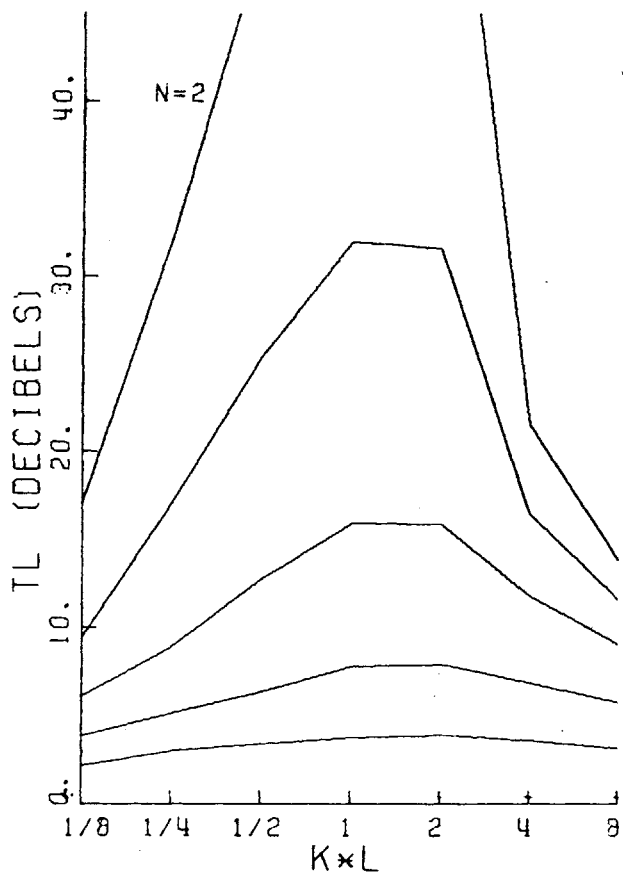
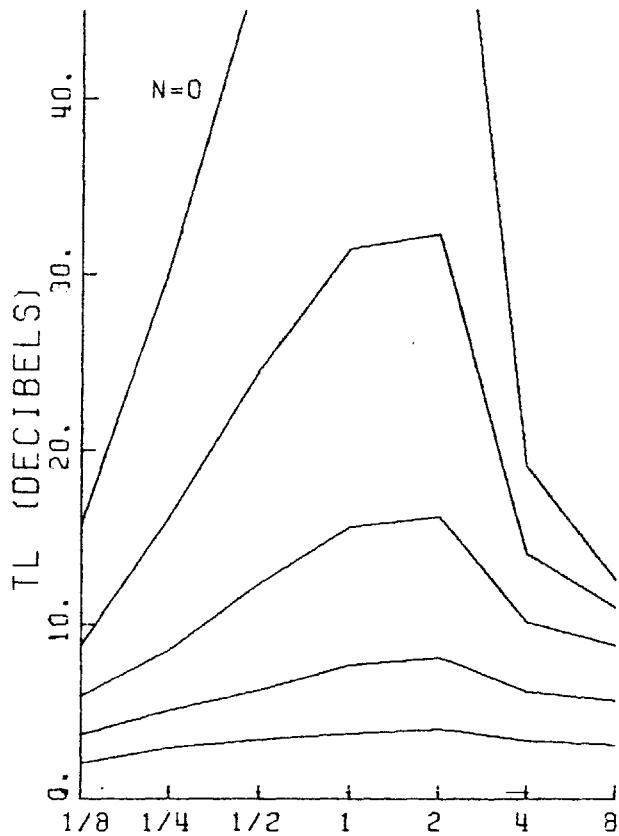


Figure A3.63

THETA=4.  
D/L=2.000  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

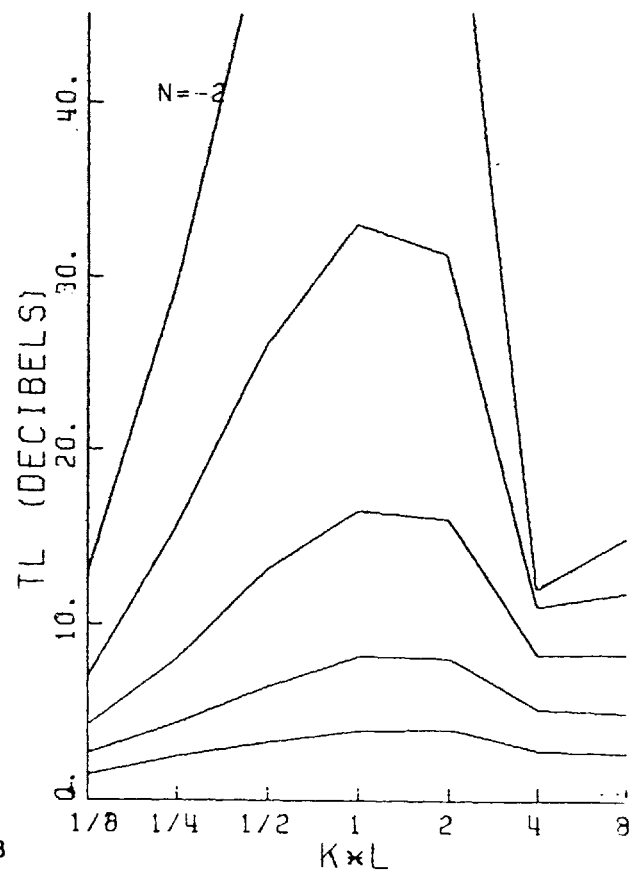
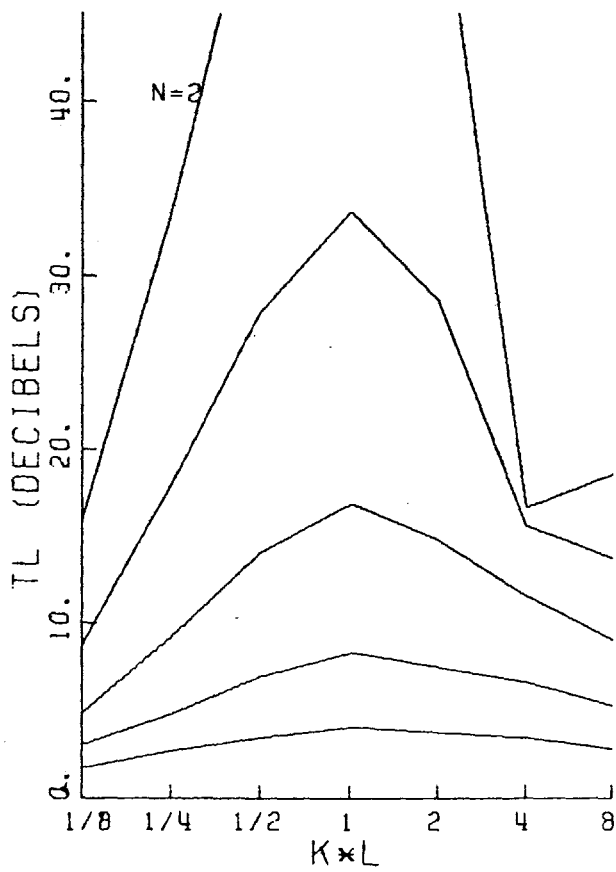
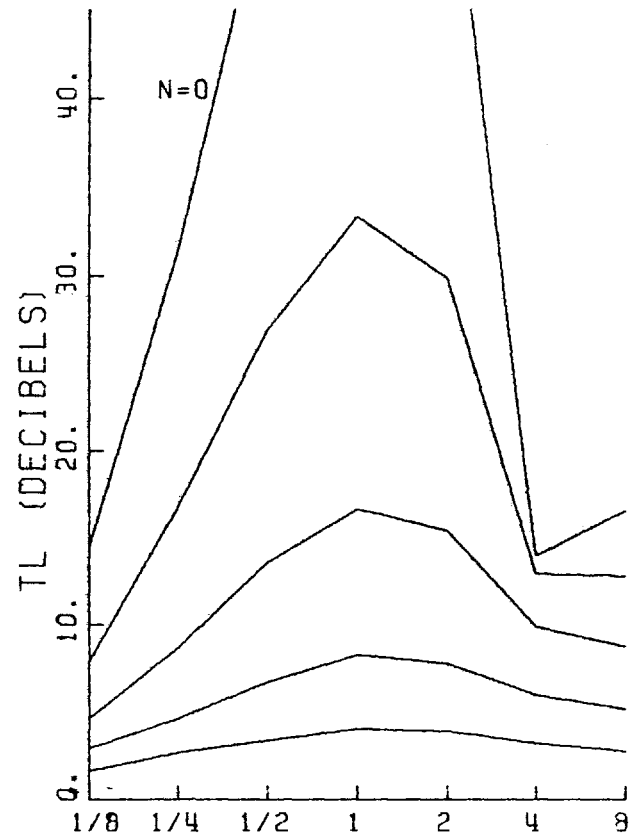


Figure A3.64

THETA=4.  
D/L=4.828  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

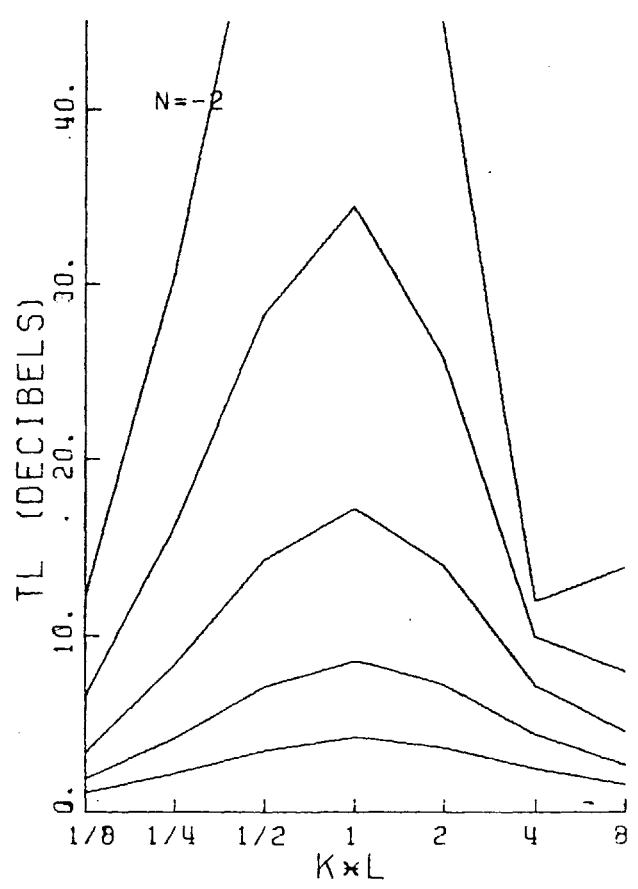
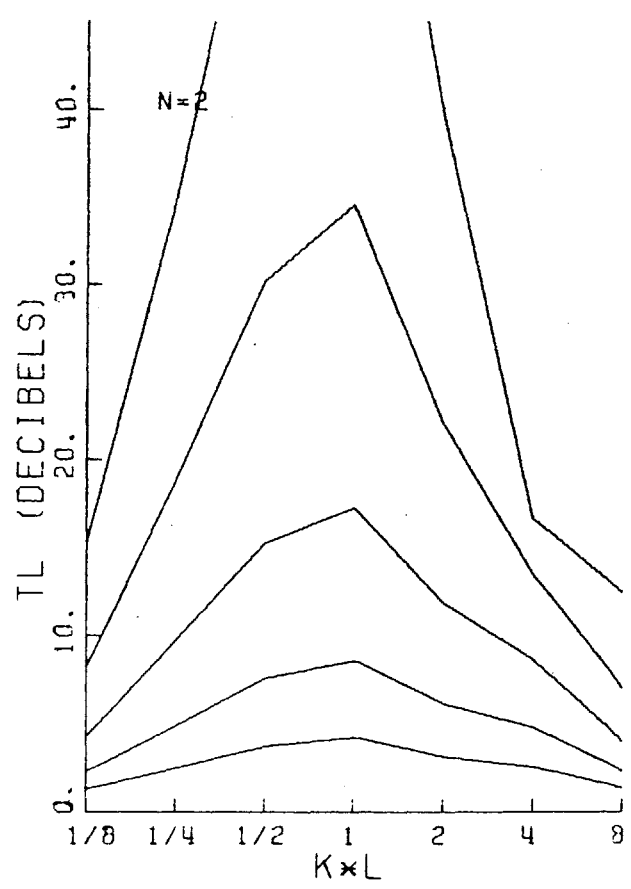
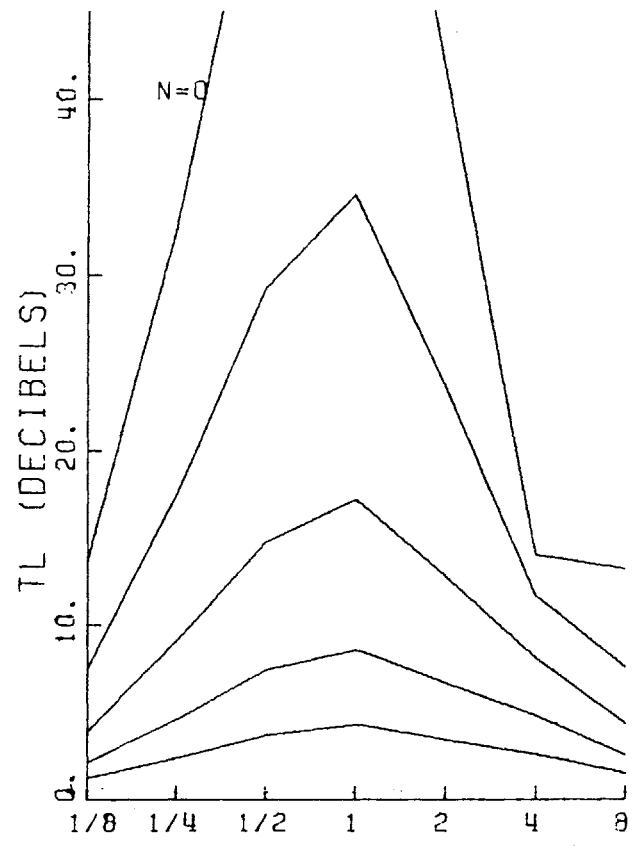
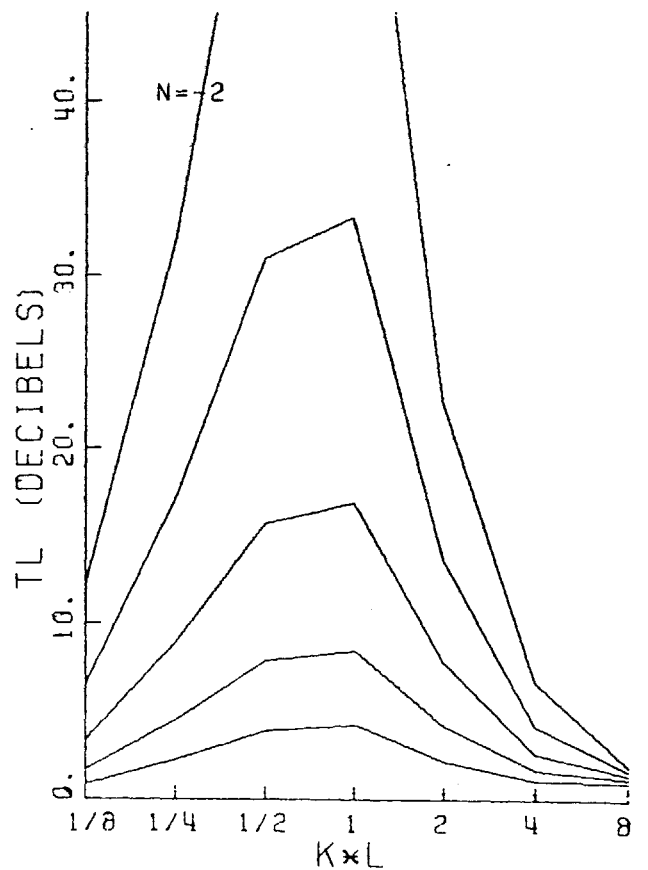
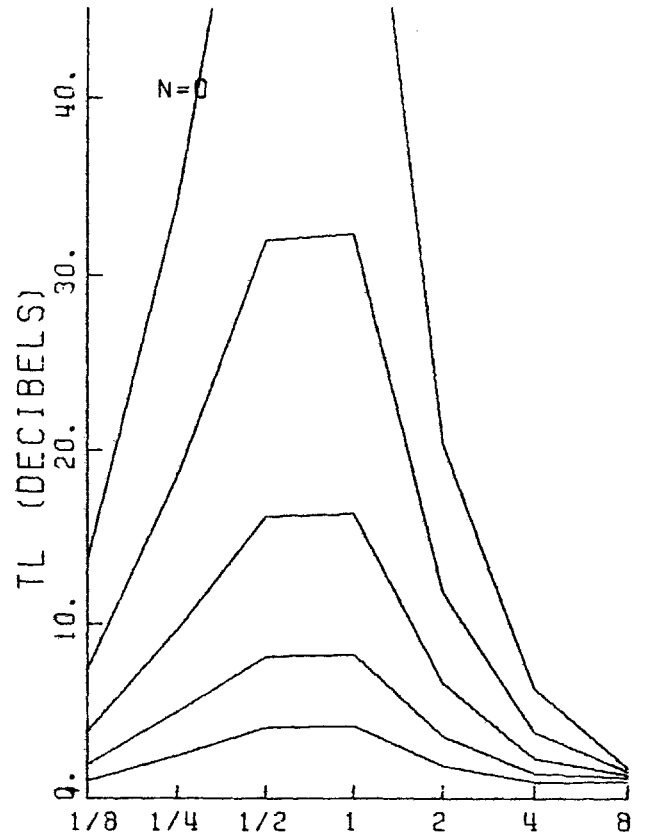


Figure A3.65

THETA=4.  
D/L=12.928  
AREA RATIO=1

S/D=16  
8  
4  
2  
1





Figures A3.66 - A3.97: Octave band TL vs  $kL$  for a circular duct lined with a porous liner. The format is the same as in Figures A3.50 - A3.65.

Figure A3.66

THETA=0.5  
D/L=1.094  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

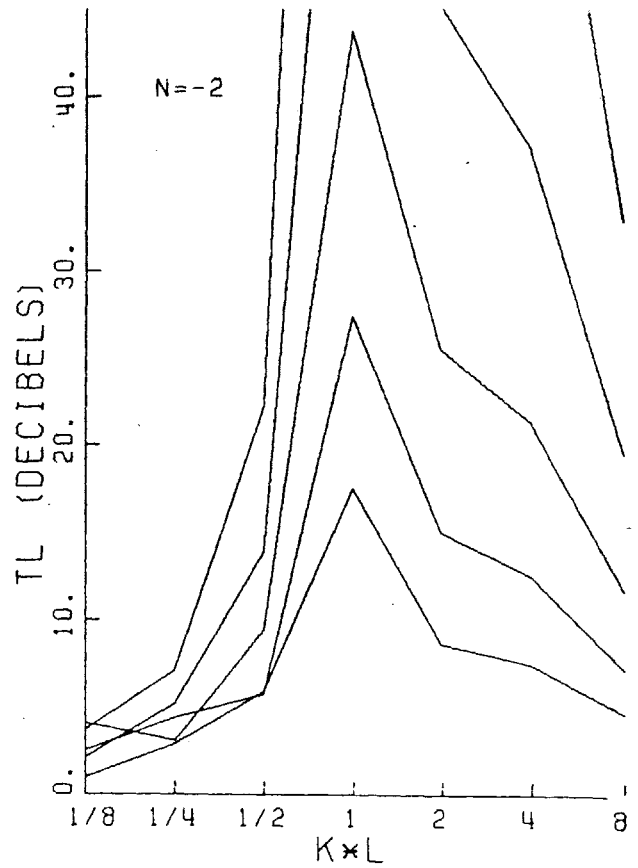
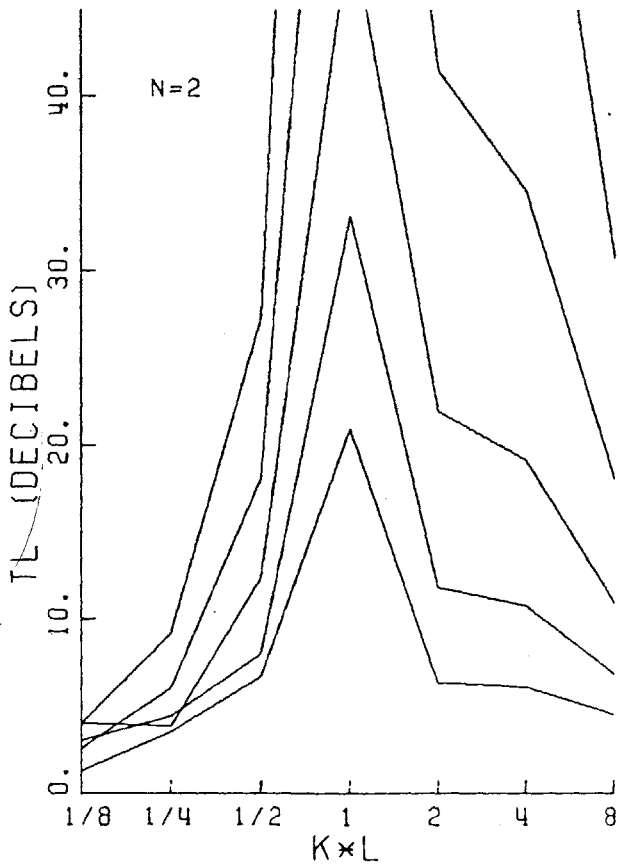
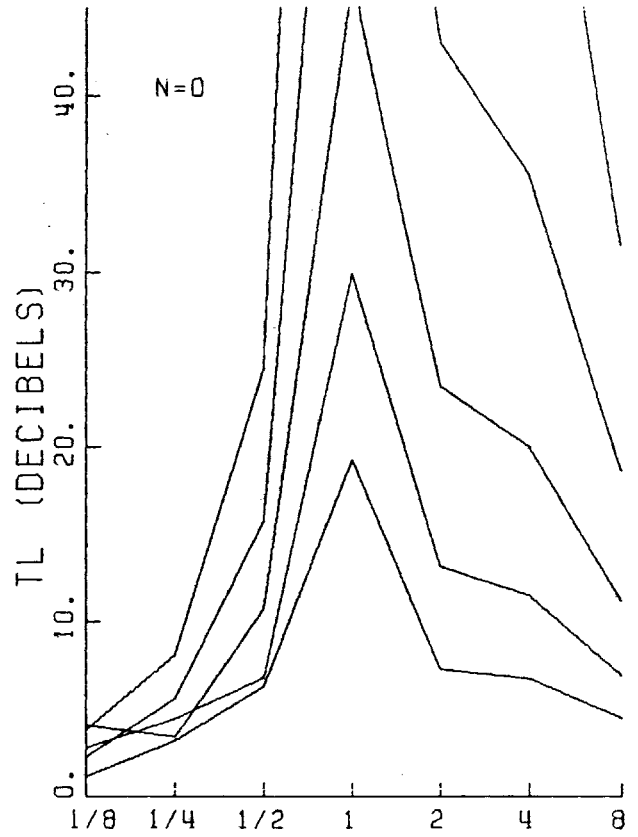


Figure A3.67

THETA=0.5  
D/L=2.000  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

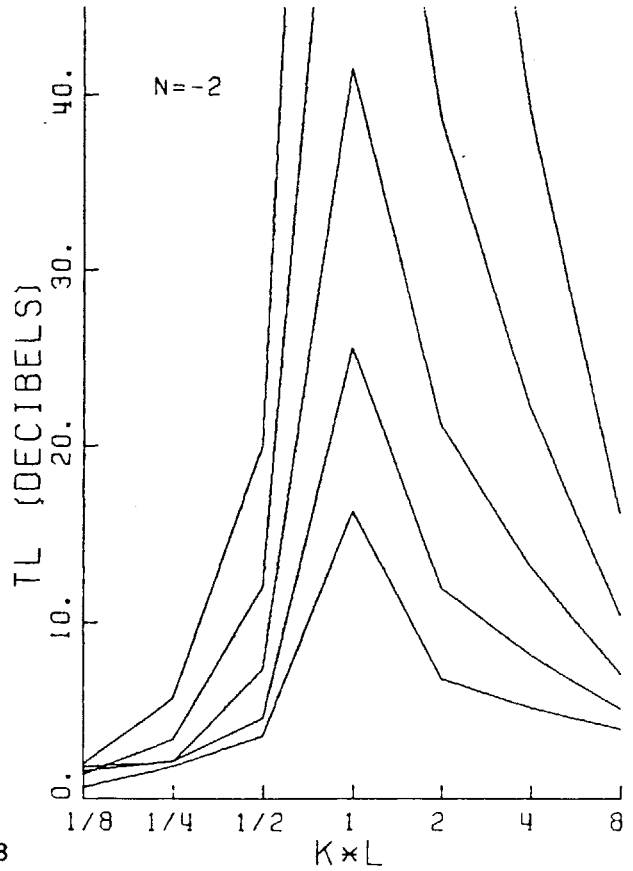
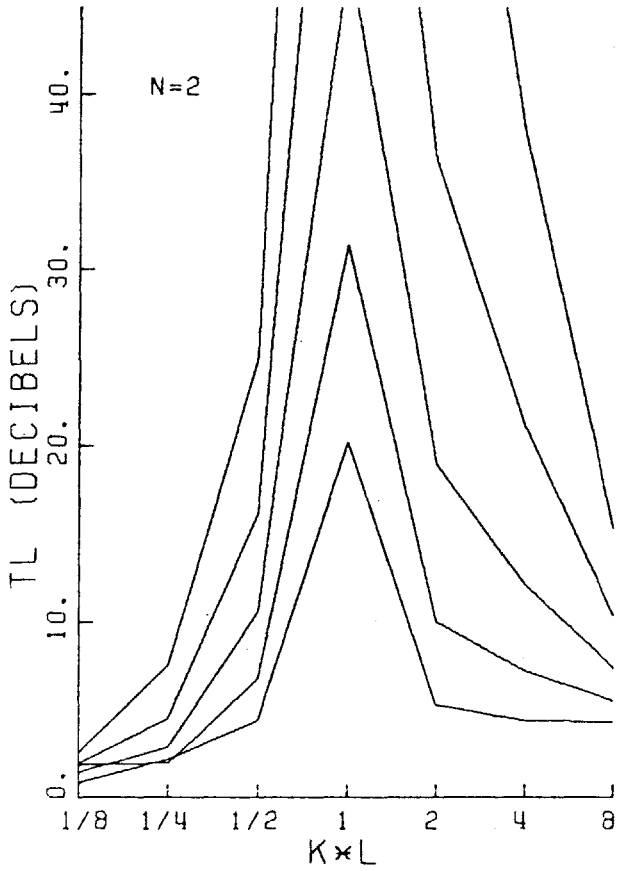
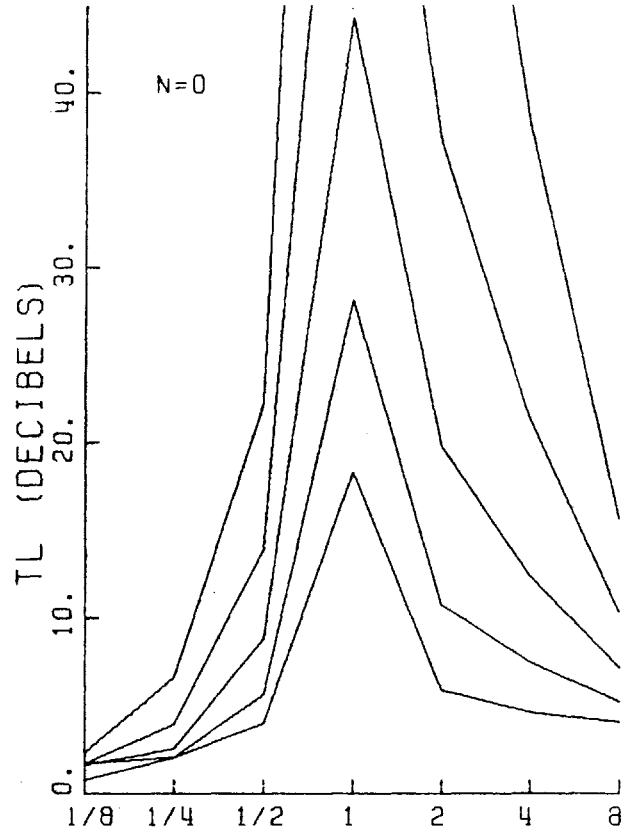


Figure A3.68

THETA=0.5  
D/L=4.828  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

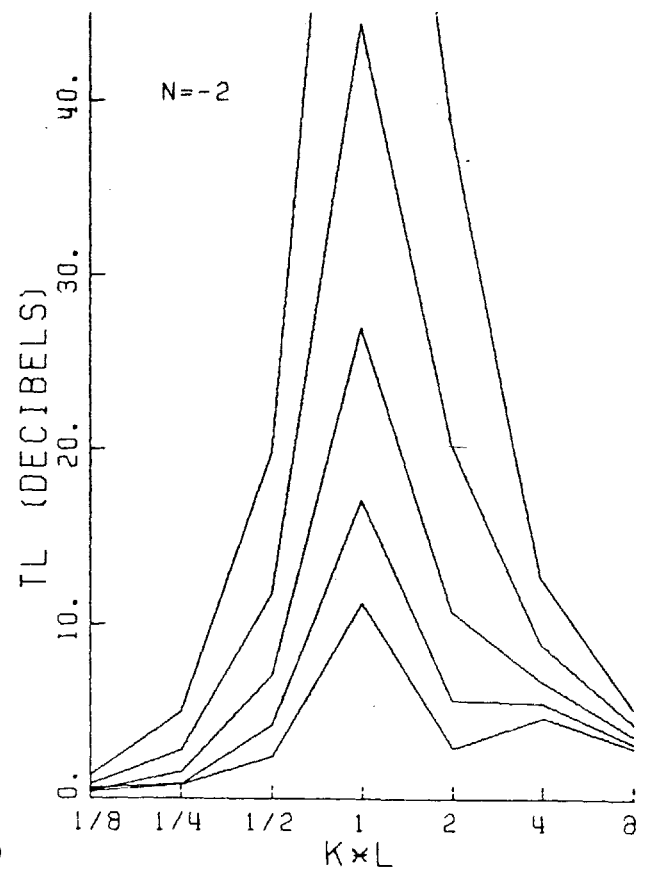
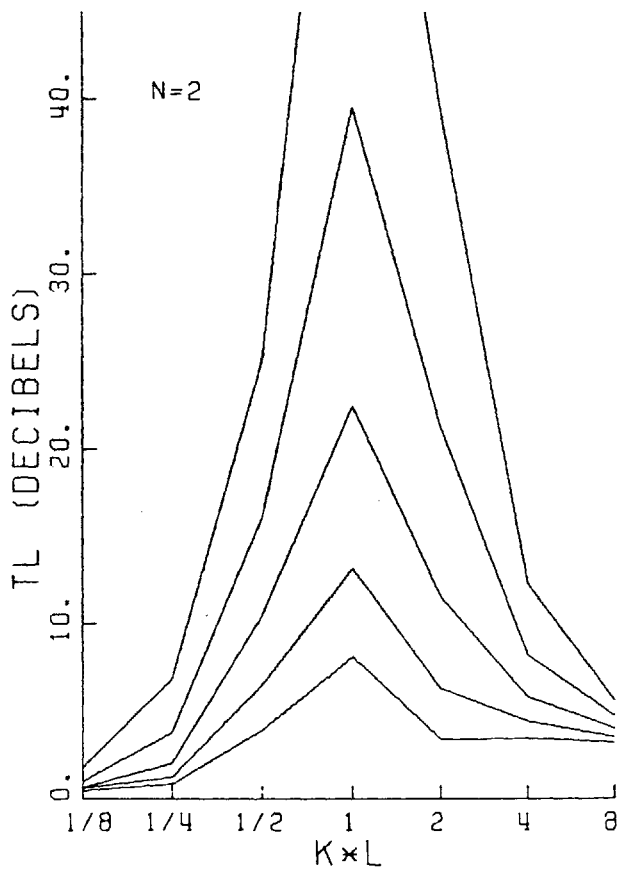
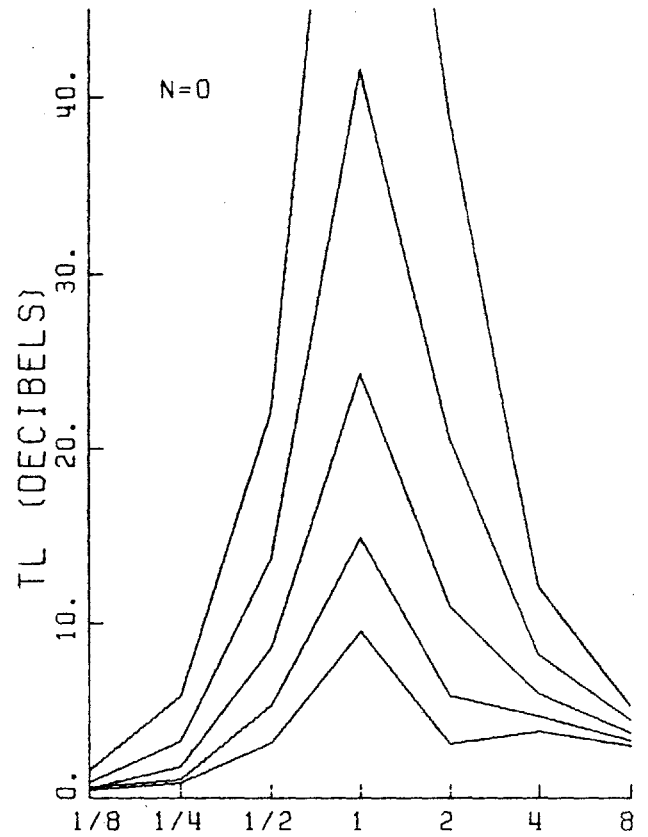


Figure A3.69

THETA=0.5  
D/L=12.928  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

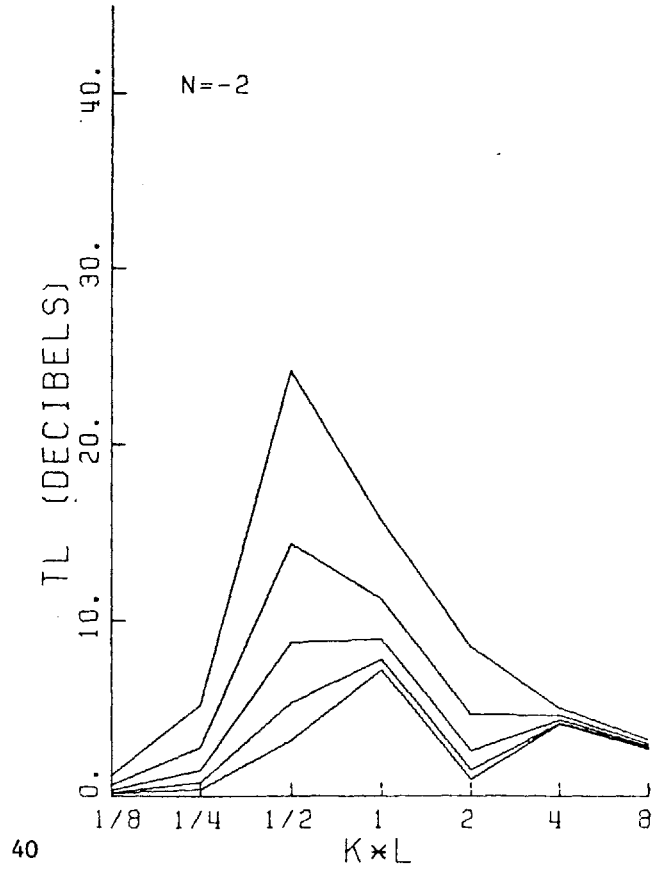
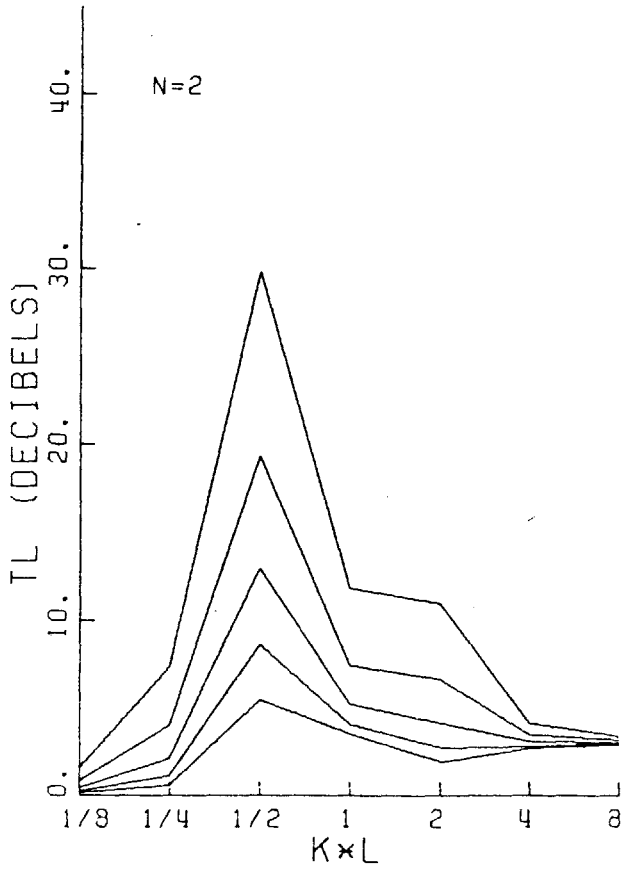
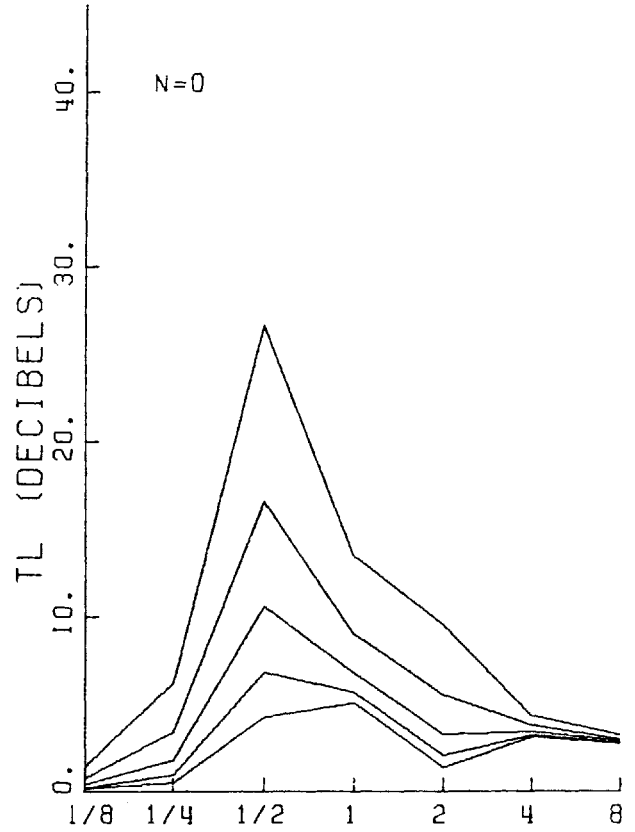


Figure A3.70

THETA=1.  
D/L=1.094  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

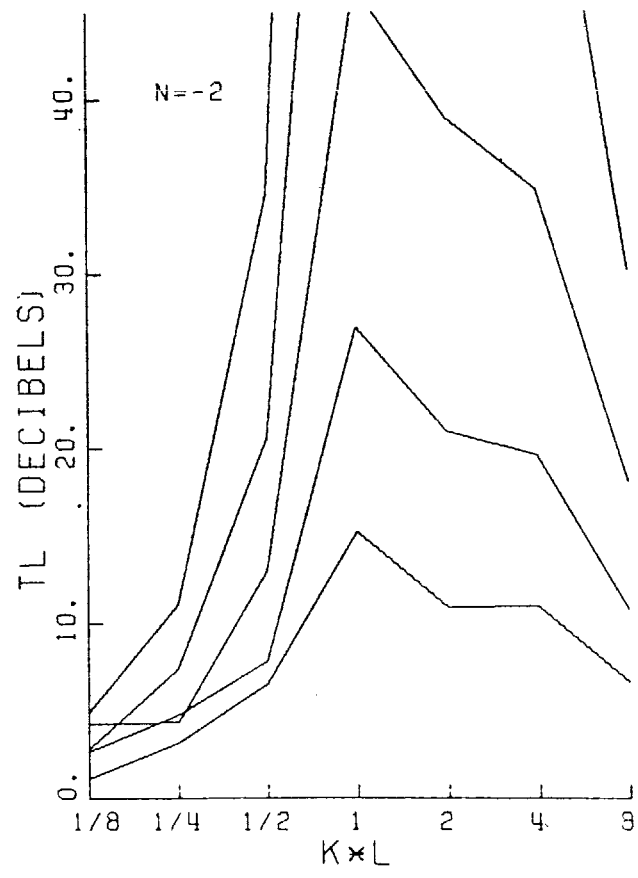
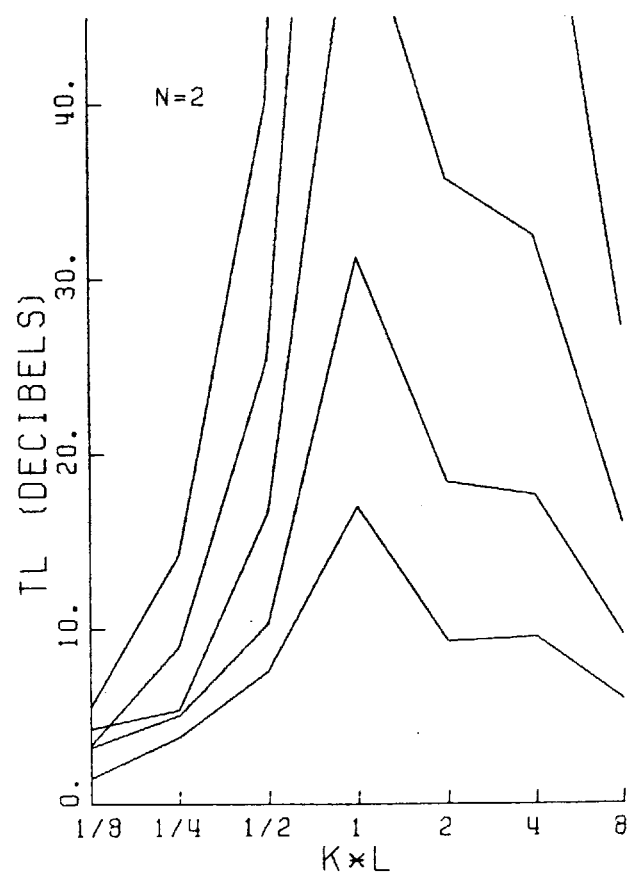
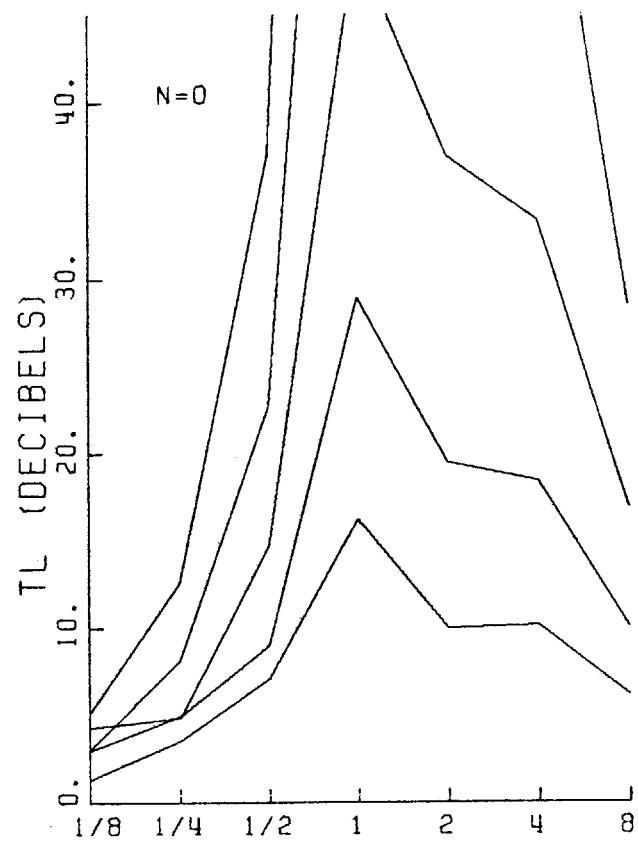


Figure A3.71

THETA=1.  
 D/L=2.000  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

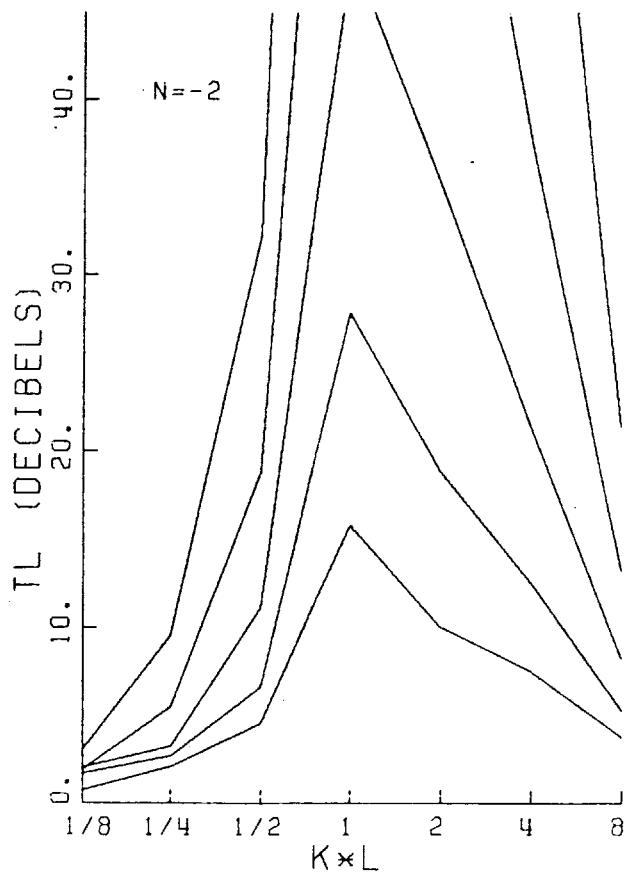
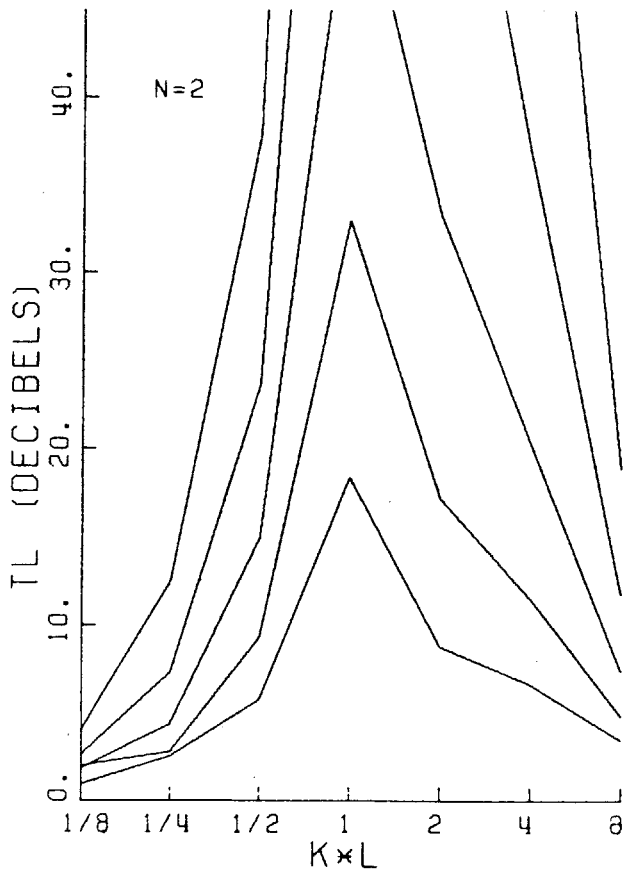
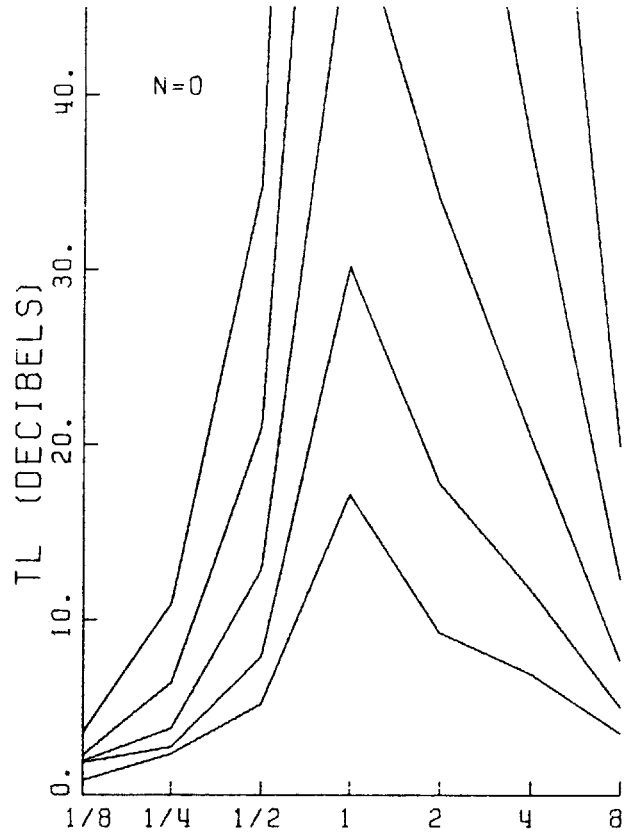


Figure A3.72

THETA=1.  
 D/L=4.828  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

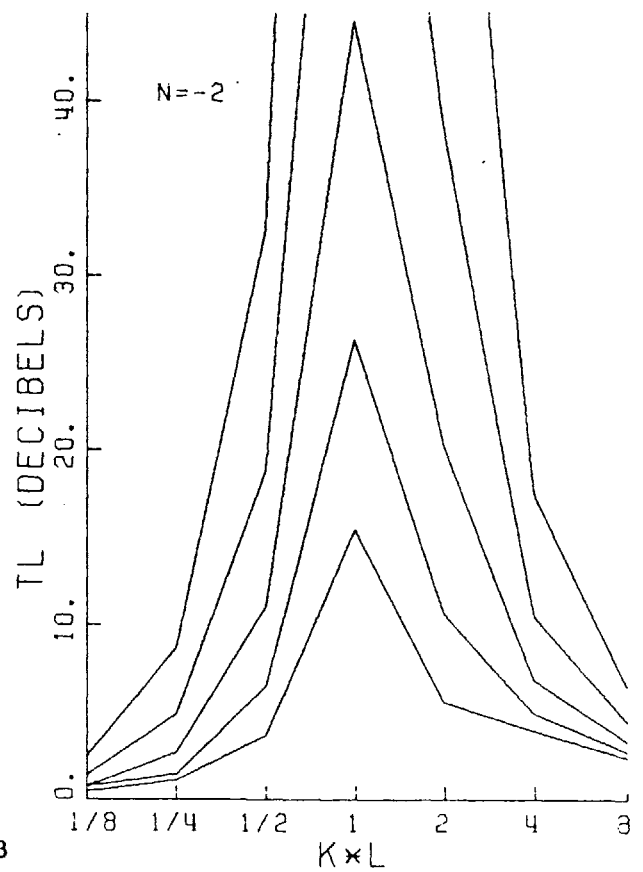
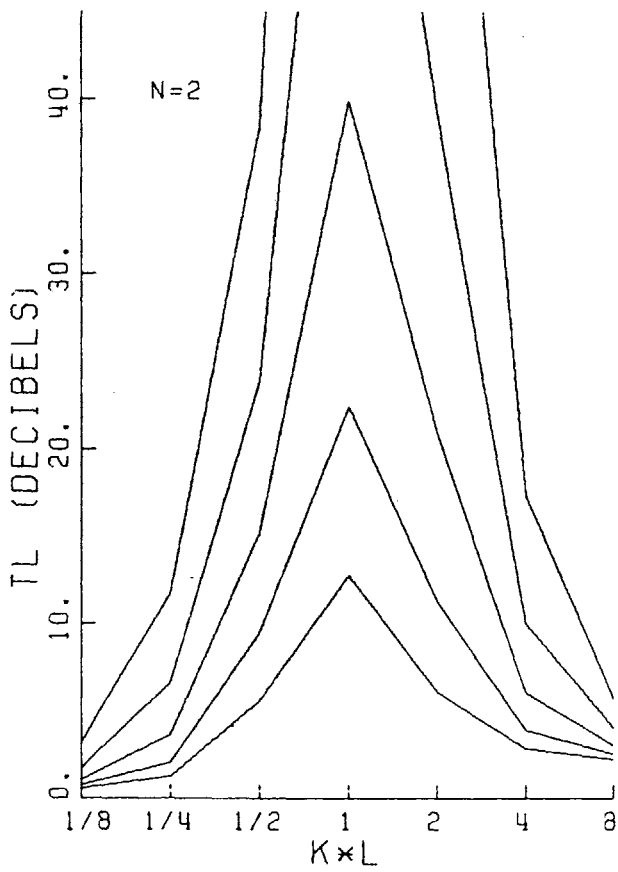
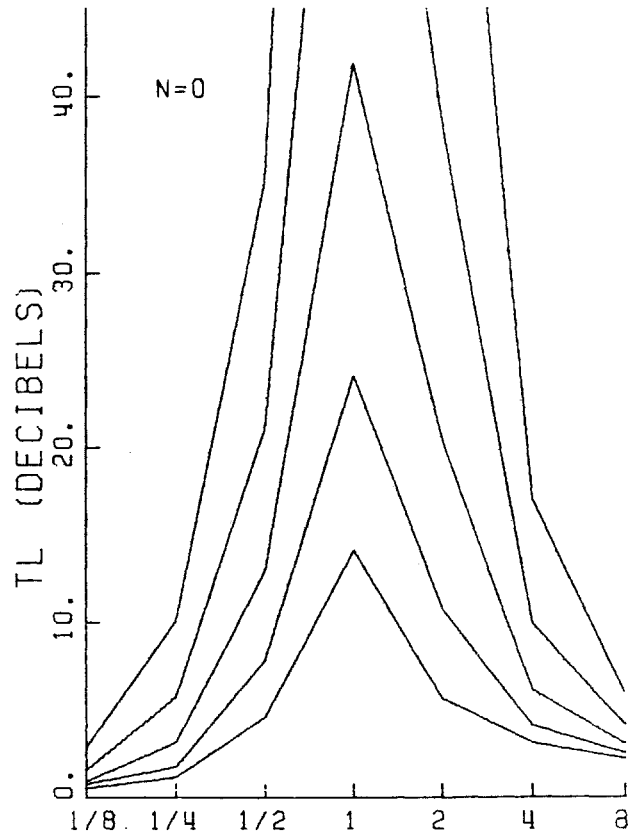




Figure A3.73

THETA=1.  
 D/L=12.928  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

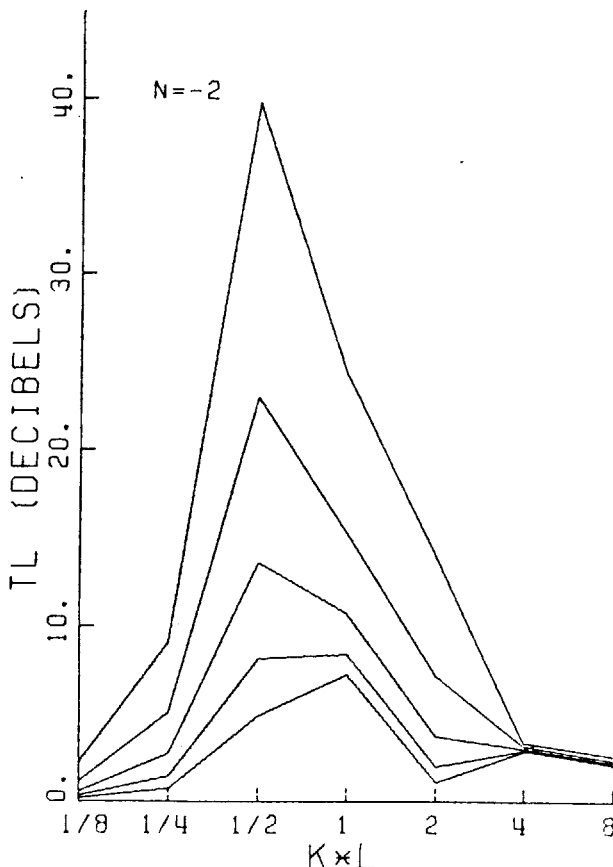
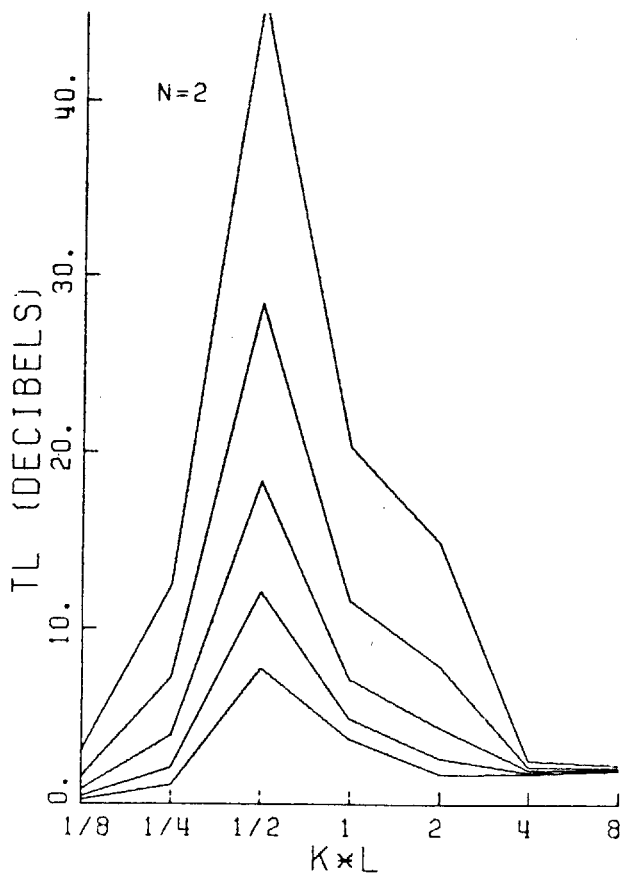
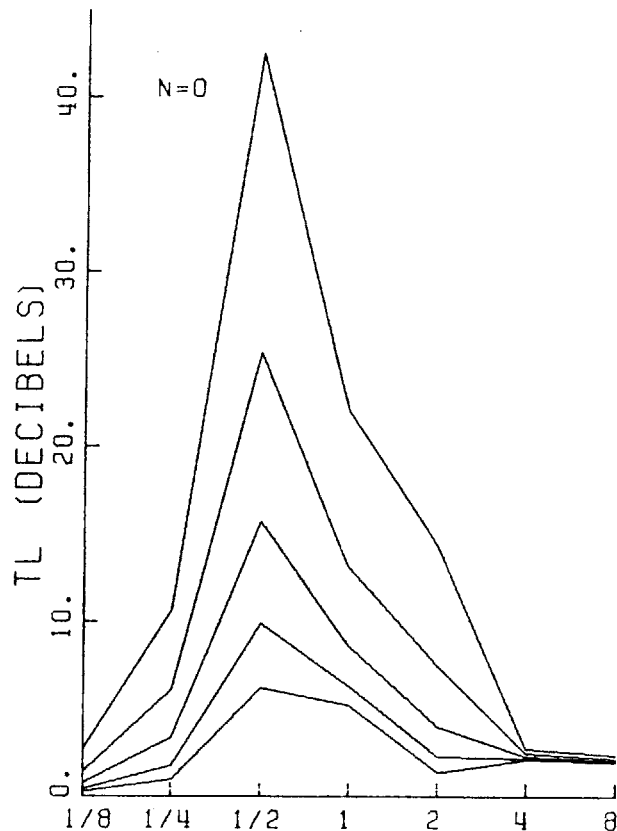


Figure A3.74

THETA=2.  
 D/L=1.094  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

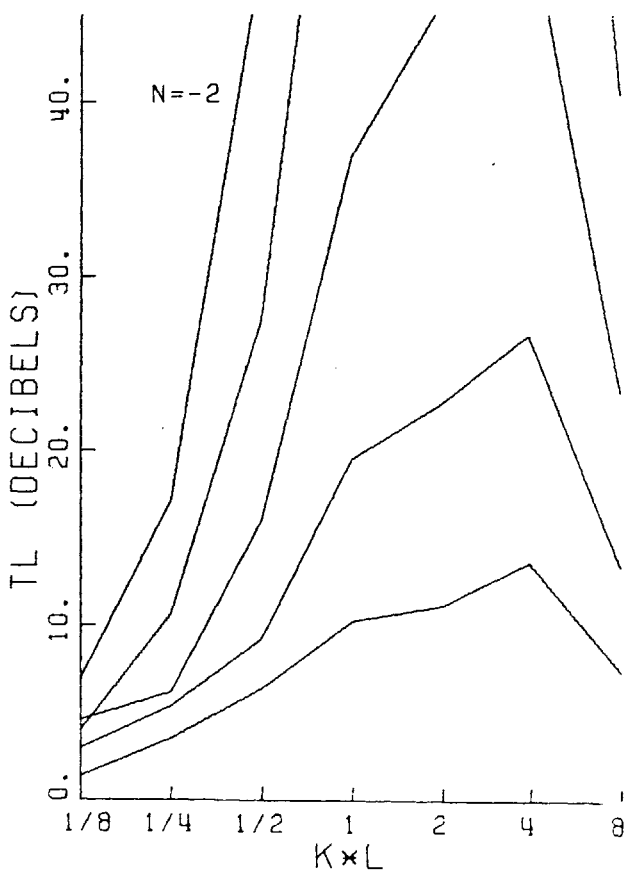
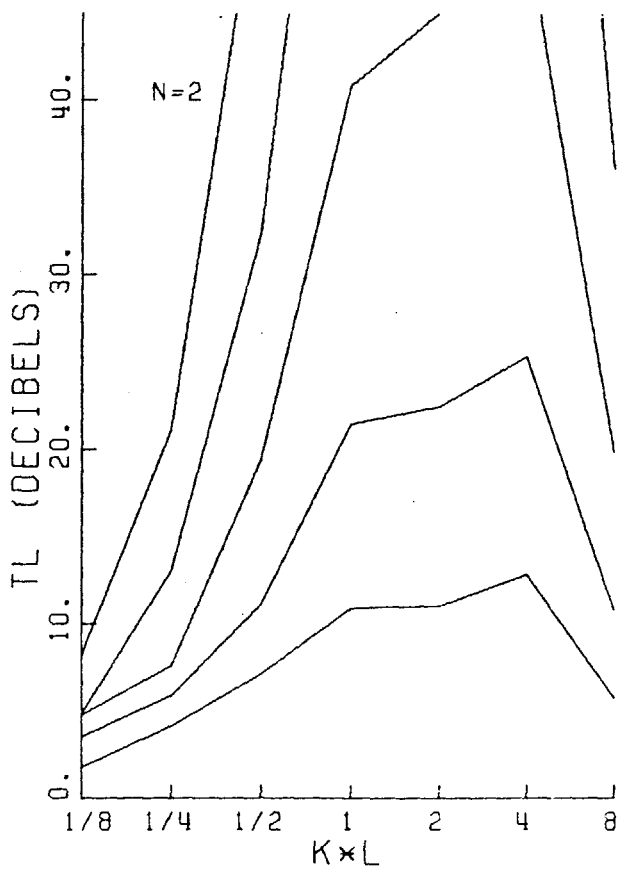
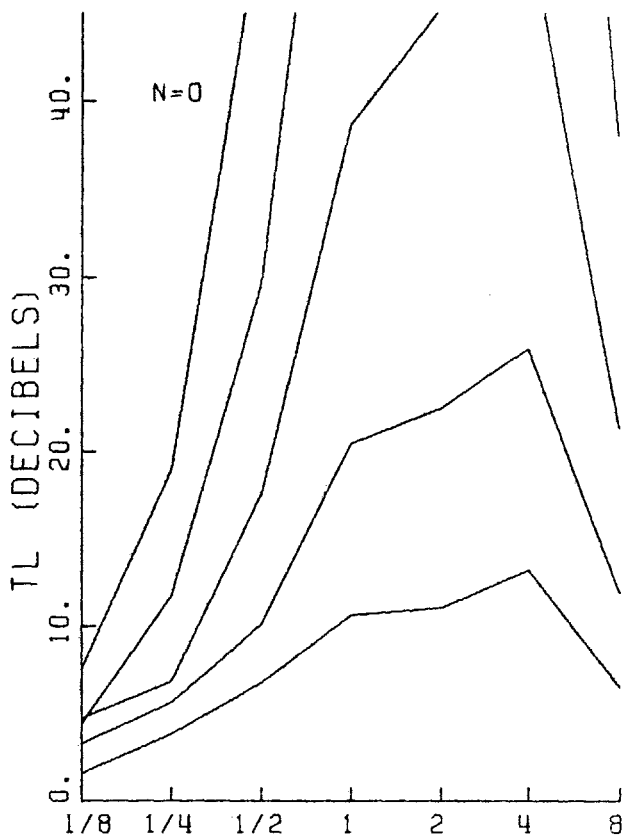


Figure A3.75

THETA=2.  
 D/L=2.000  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

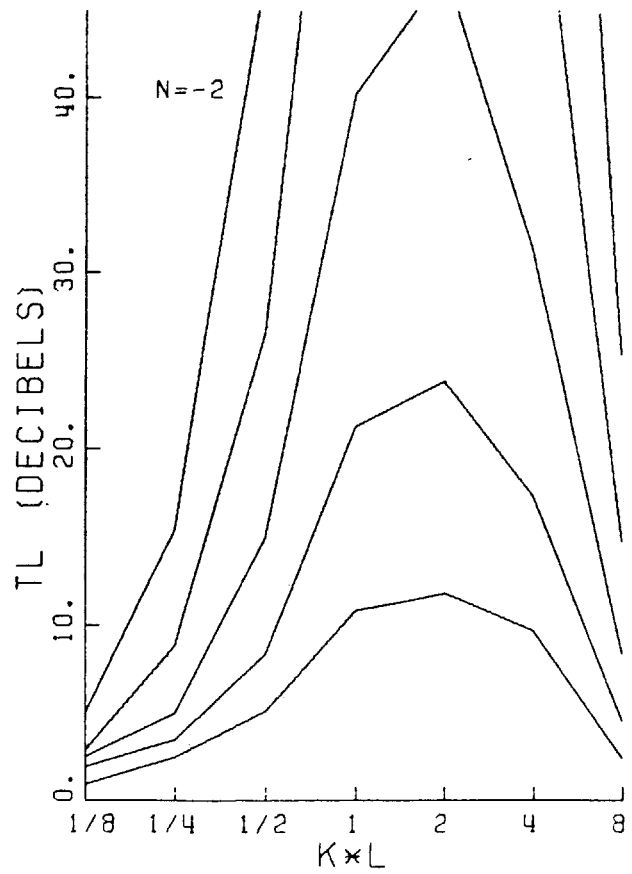
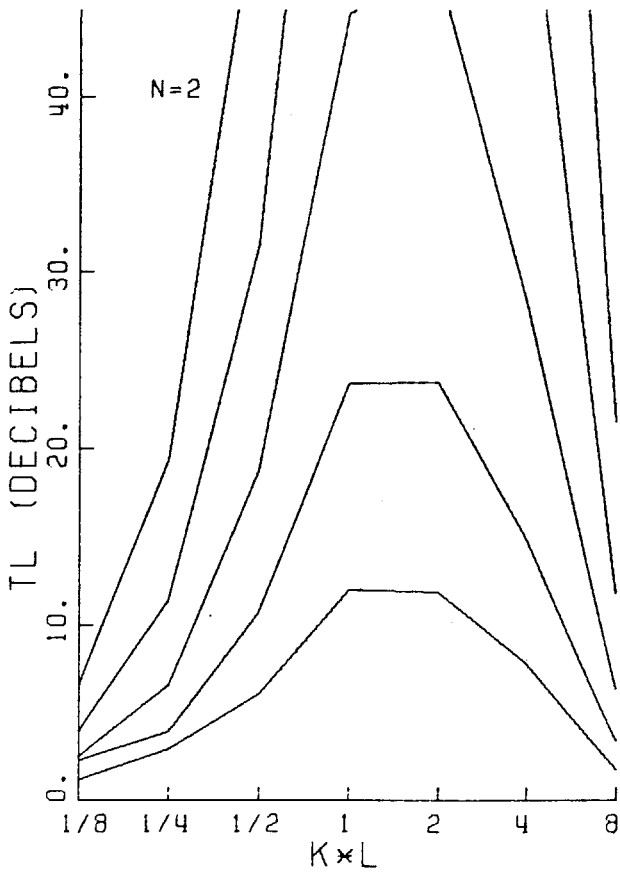
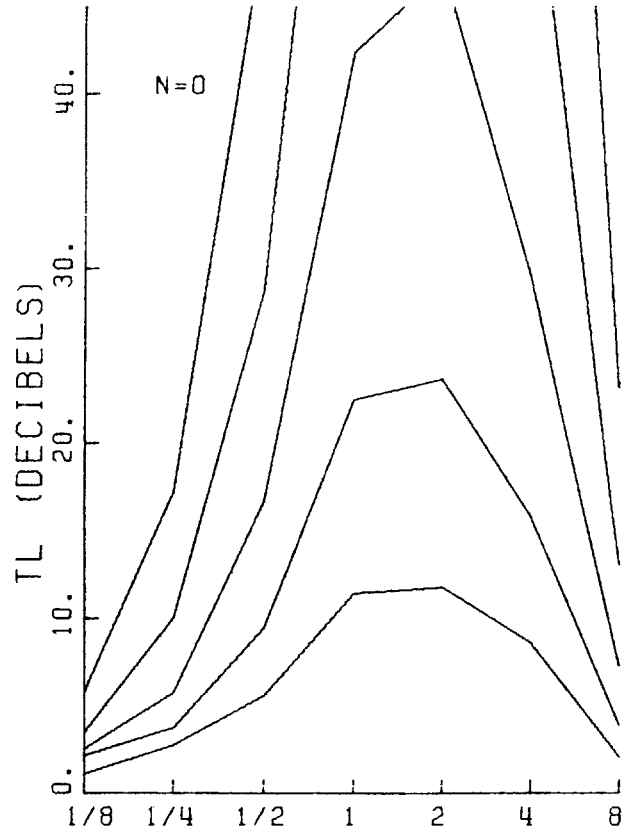


Figure A3.76

THETA=2.  
 D/L=4.828  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

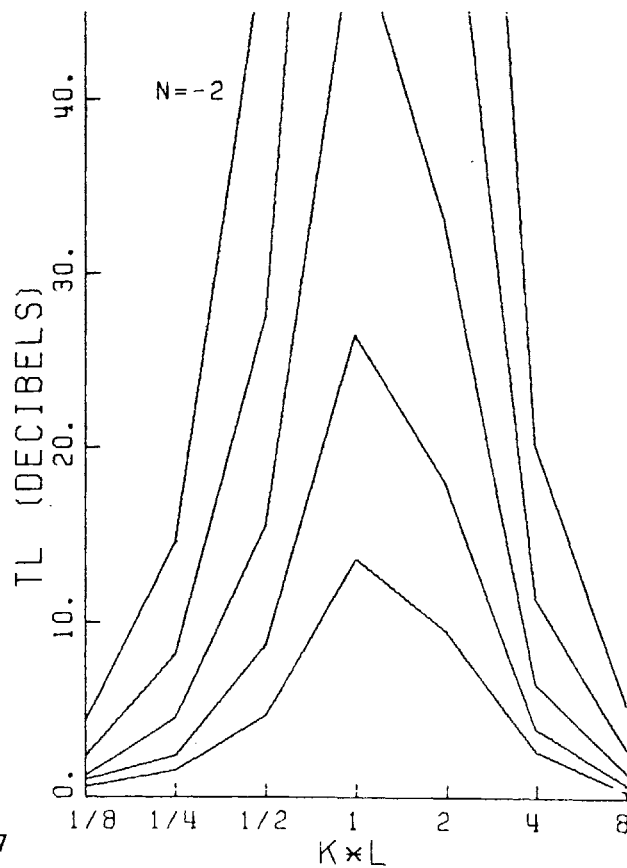
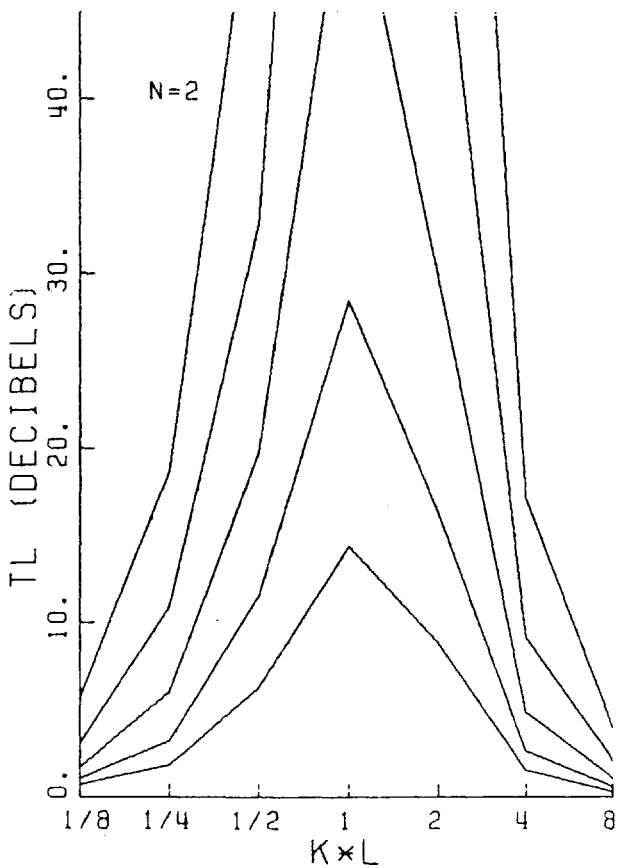
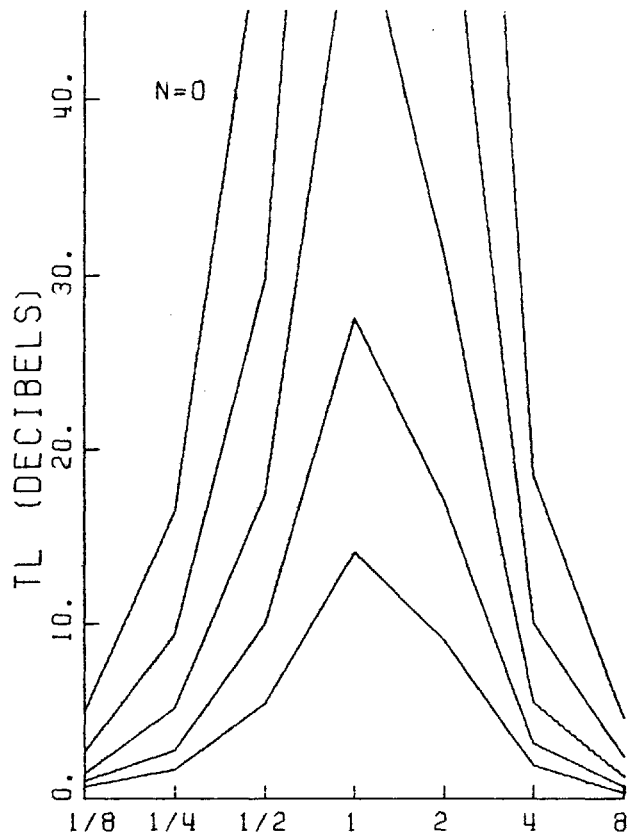


Figure A3.77

THETA=2.  
 D/L=12.928  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

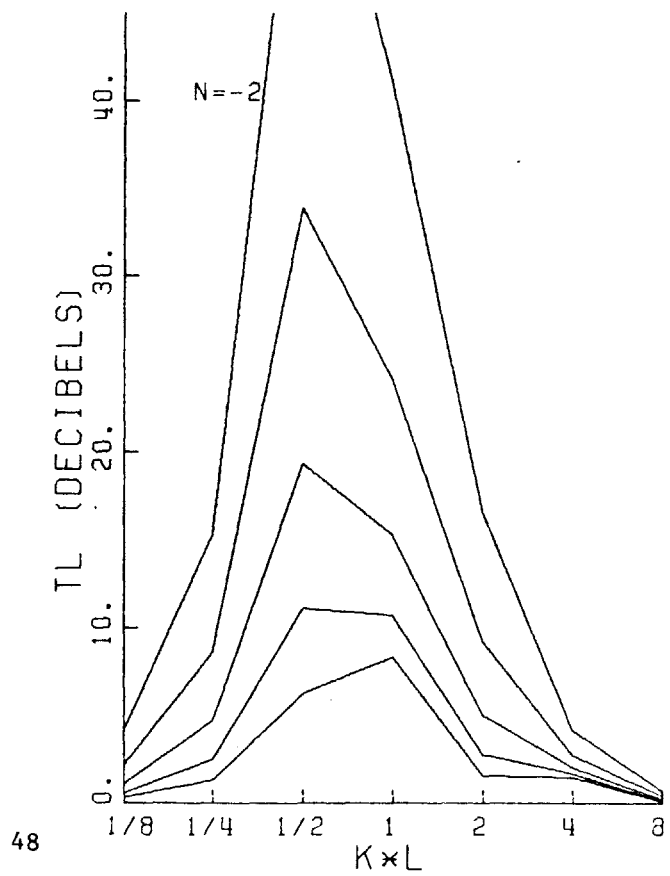
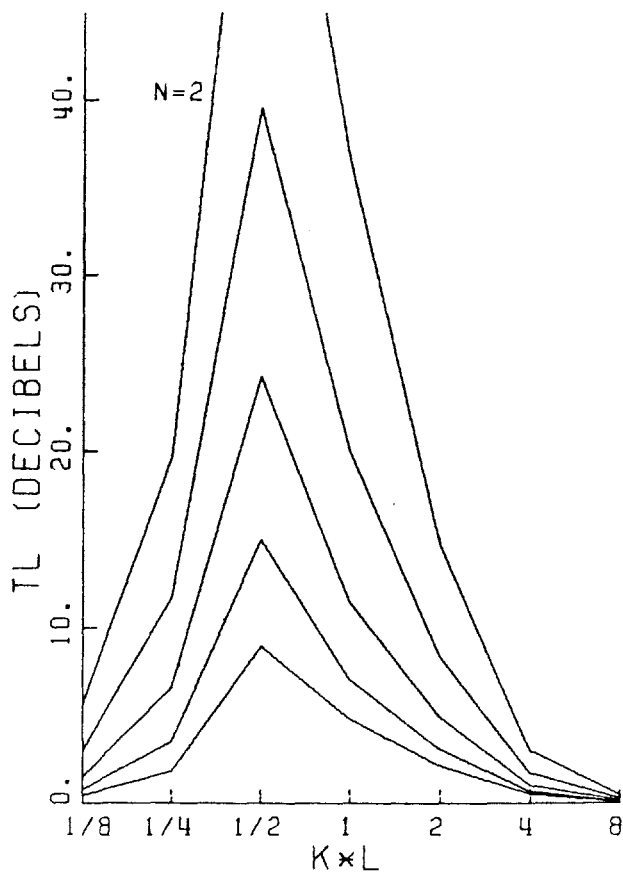


Figure A3.78

THETA=4.  
D/L=1.094  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

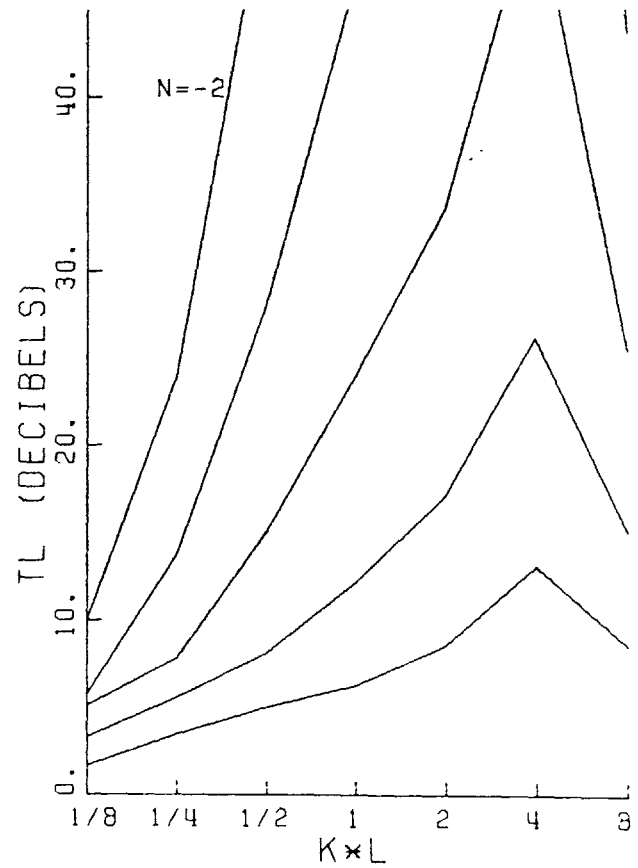
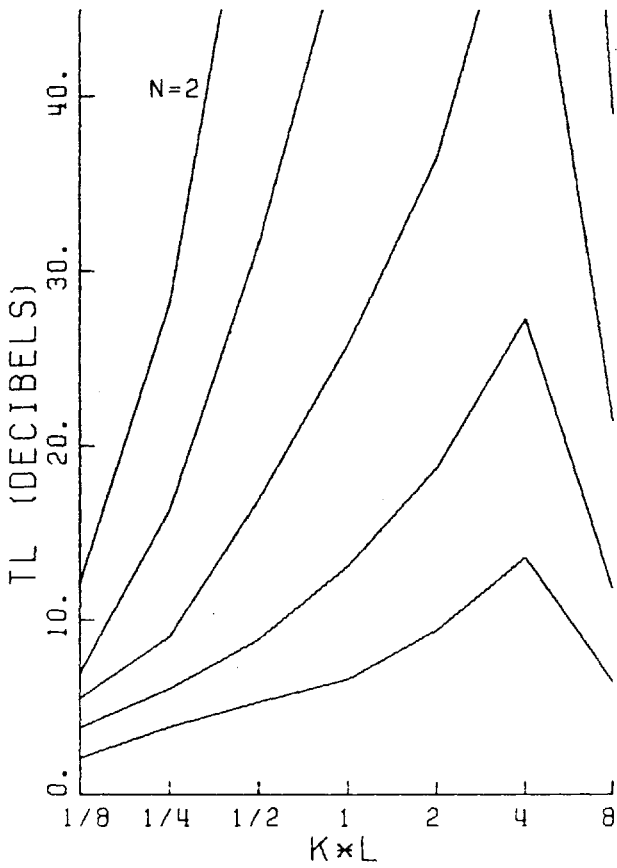
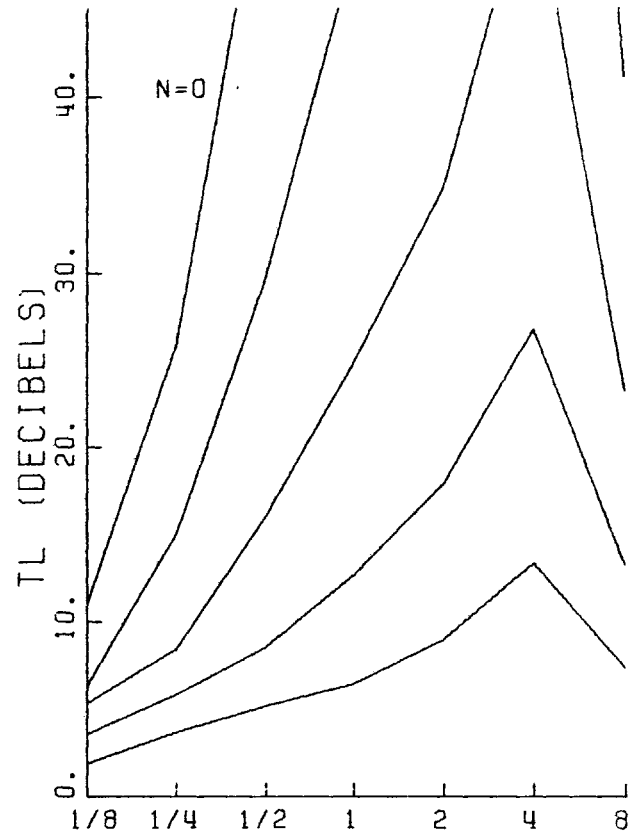


Figure A3.79

THETA=4.  
 D/L=2.000  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

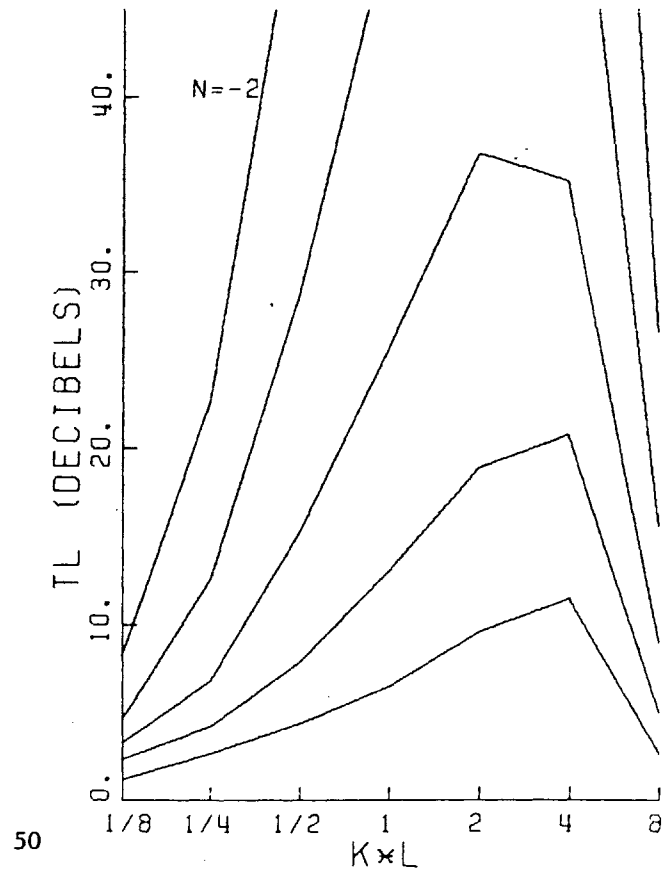
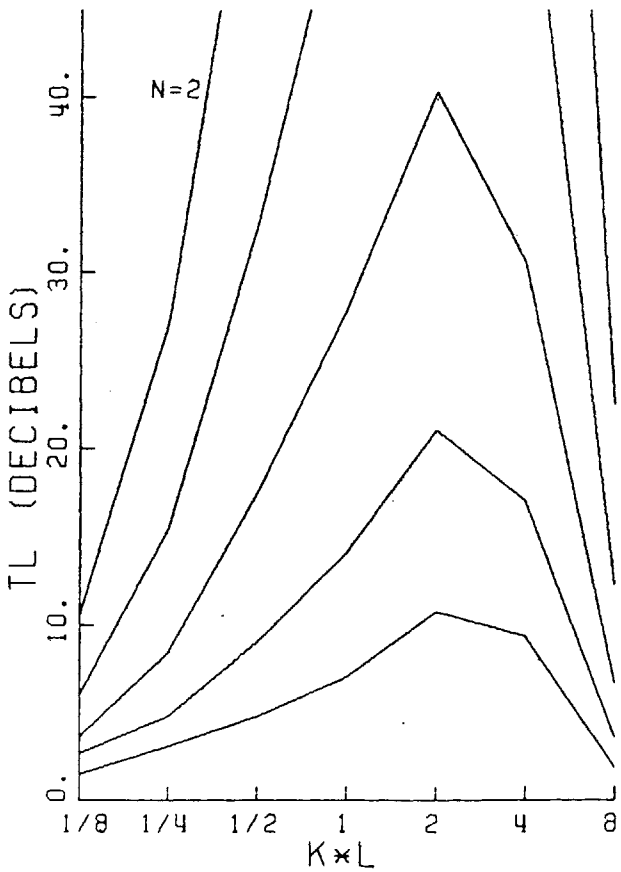
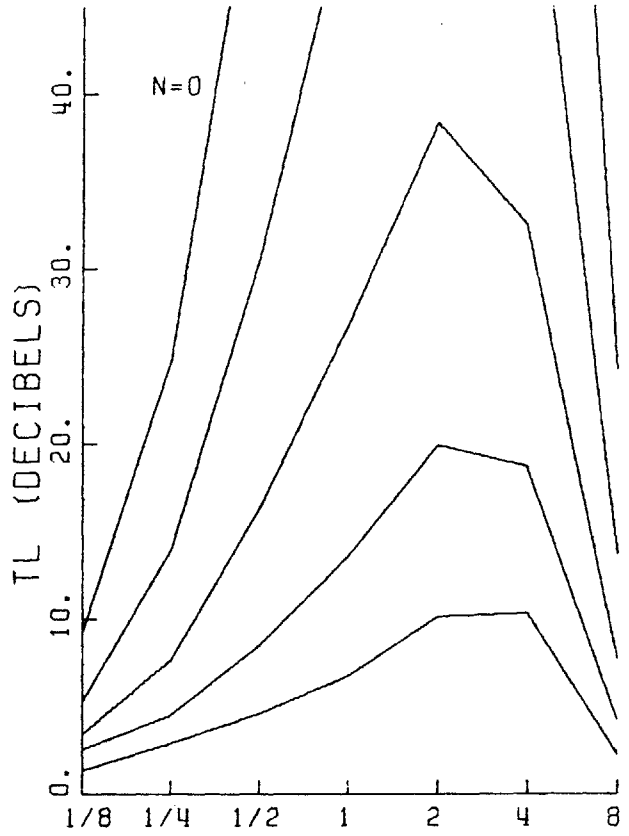


Figure A3.80

THETA=4.  
 D/L=4.828  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

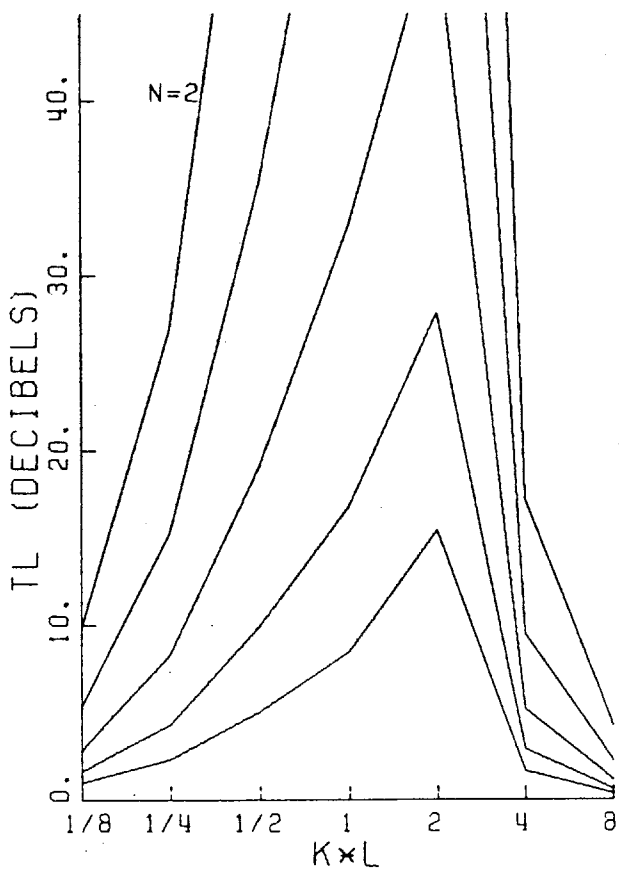
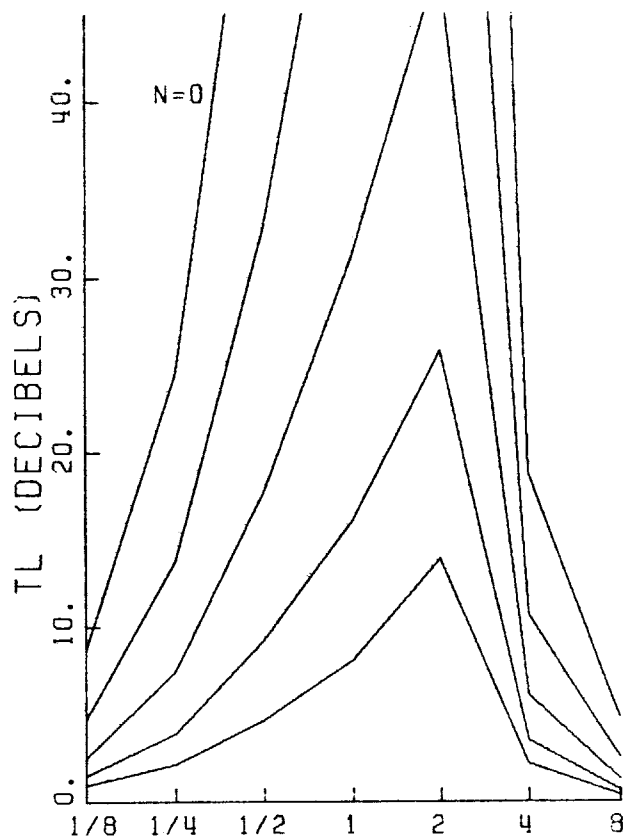




Figure A3.81

THETA=4.  
 D/L=12.928  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

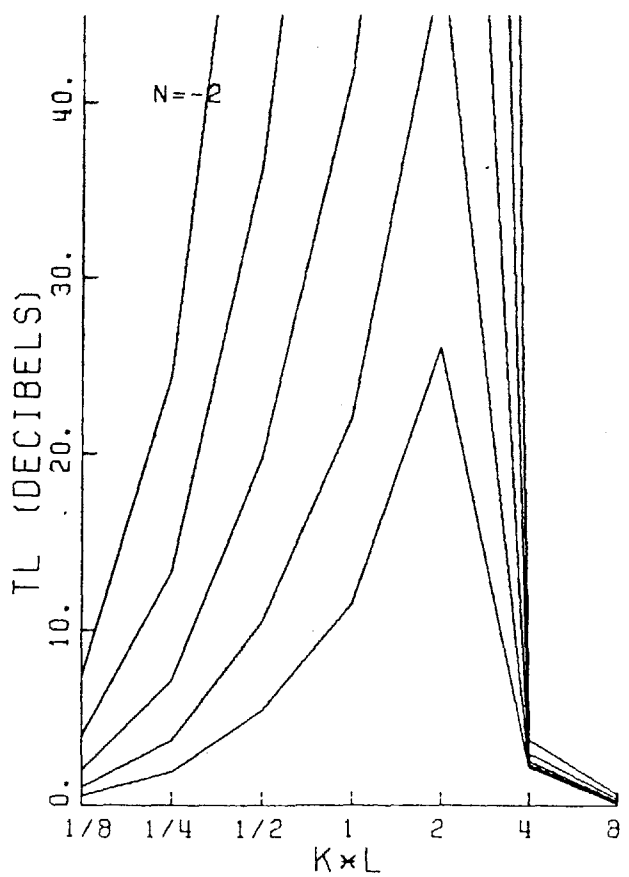
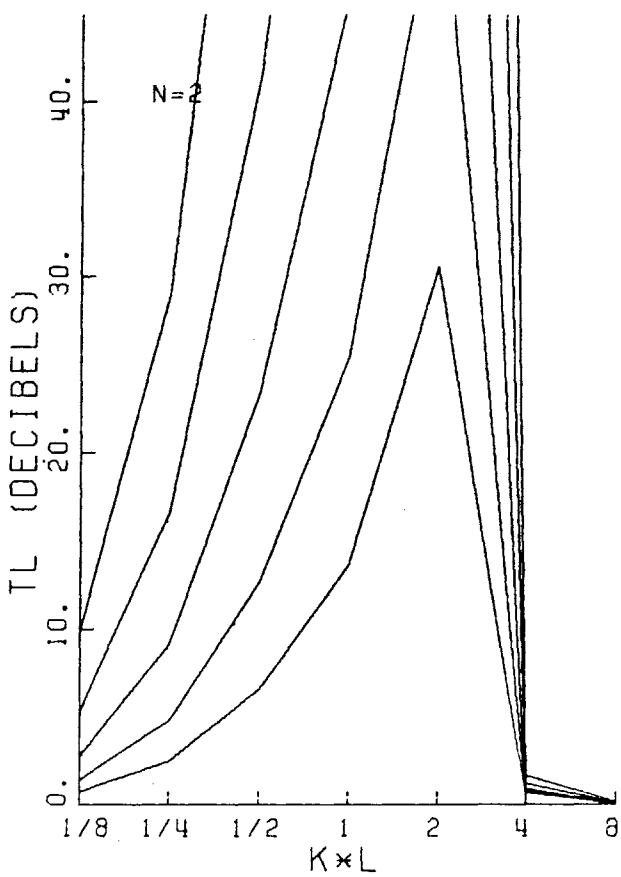
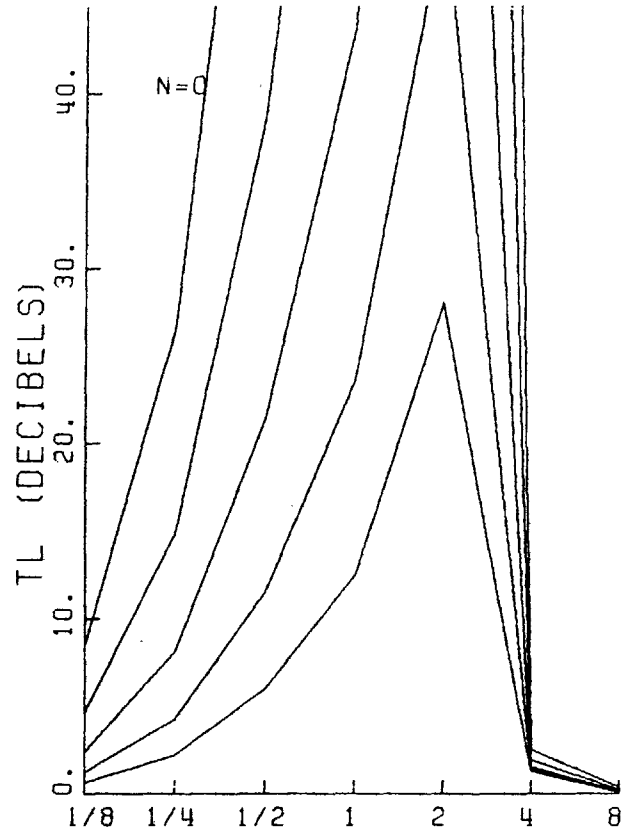


Figure A3.82

THETA=8.  
 D/L=1.094  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

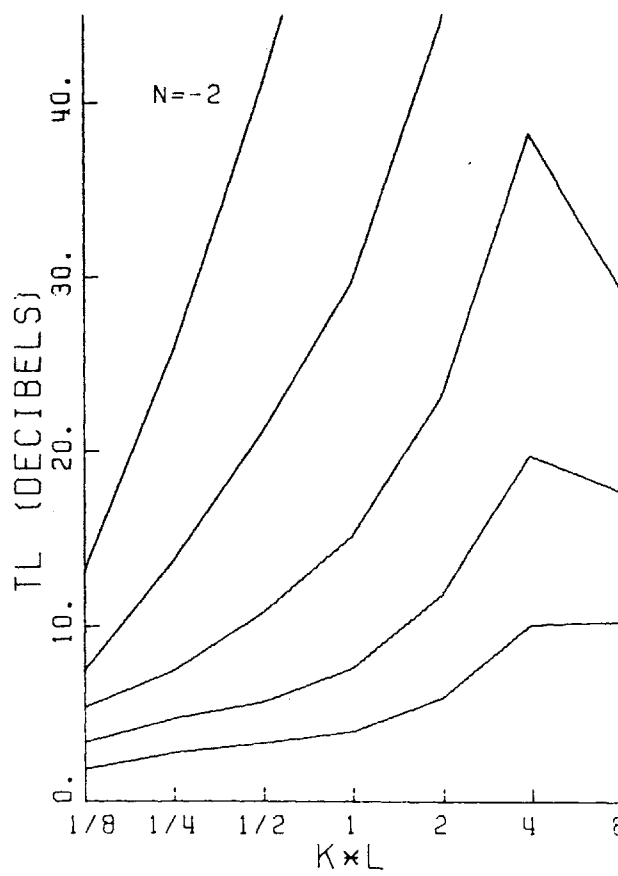
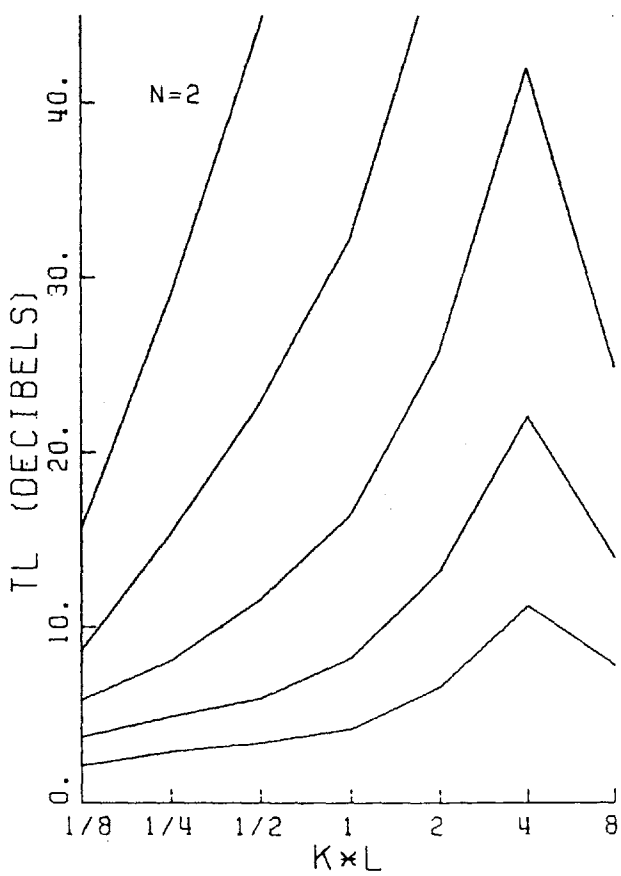
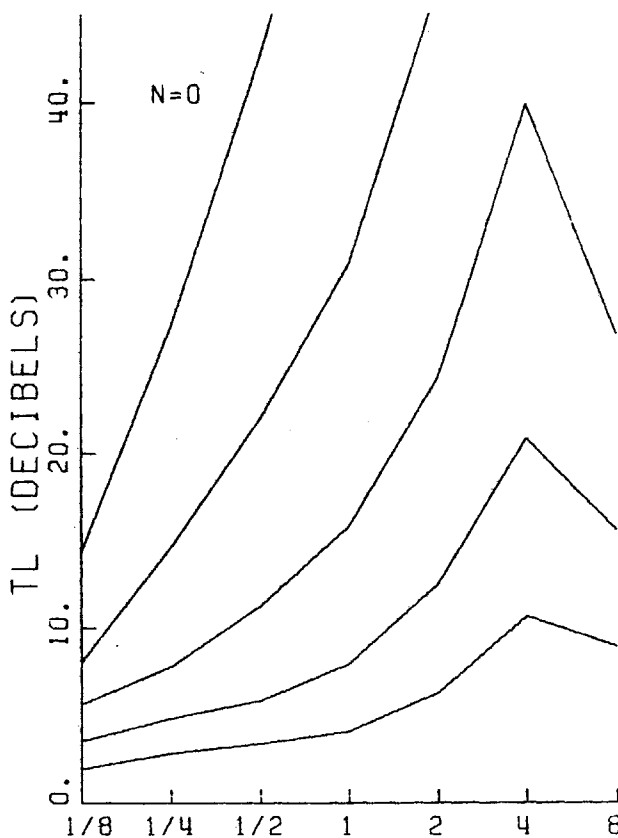


Figure A3.83

THETA=8.  
 D/L=2.000  
 AREA RATIO=1

S/D=16  
 8  
 4  
 2  
 1

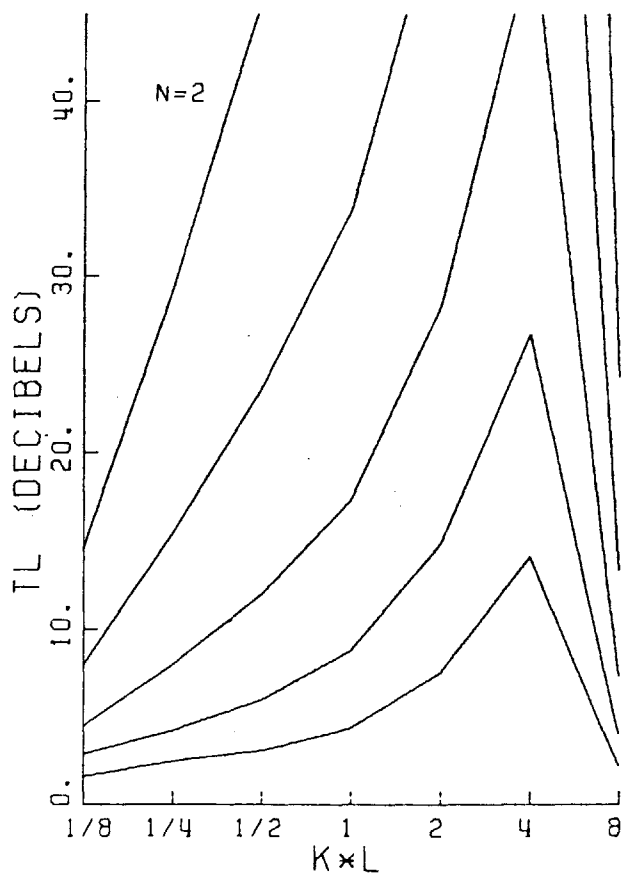
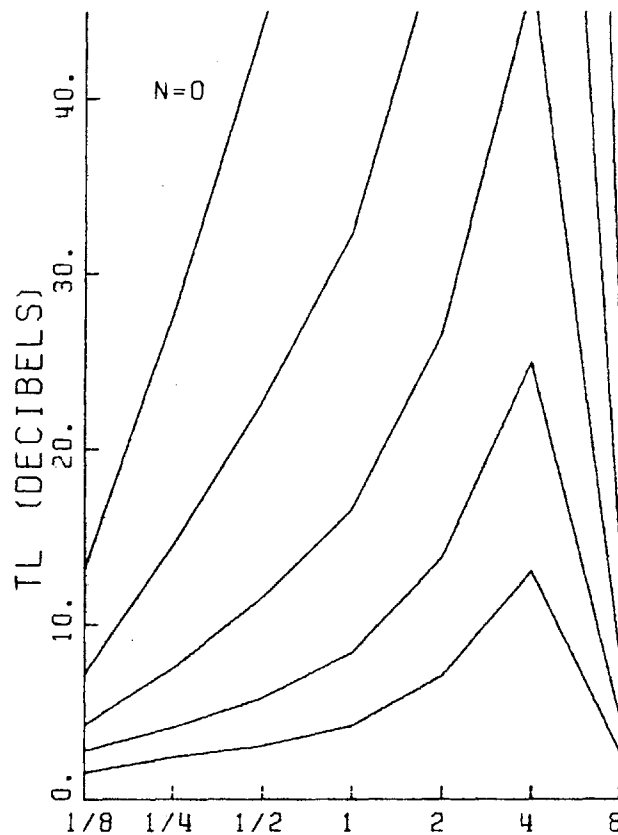


Figure A3.84

THETA=8.  
 D/L=4.828  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

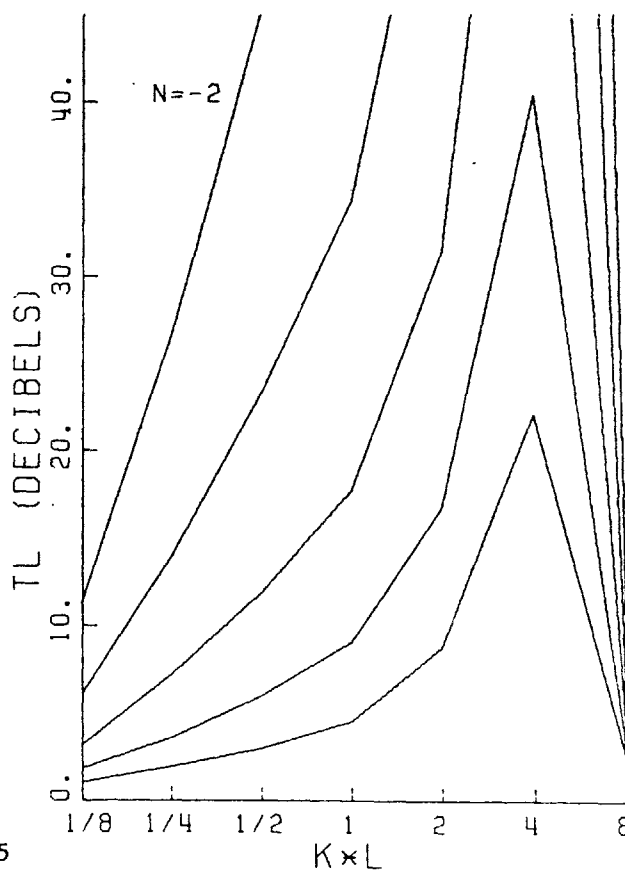
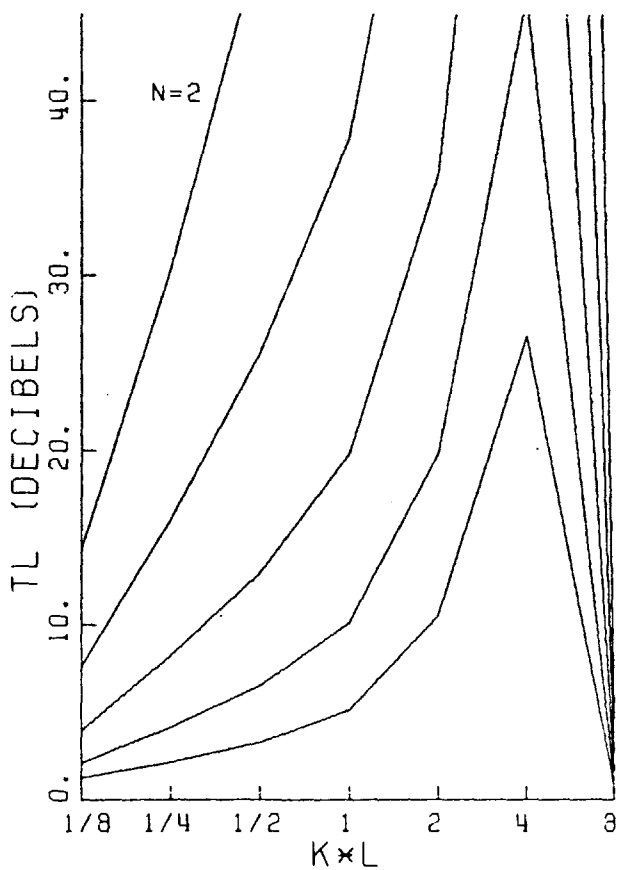
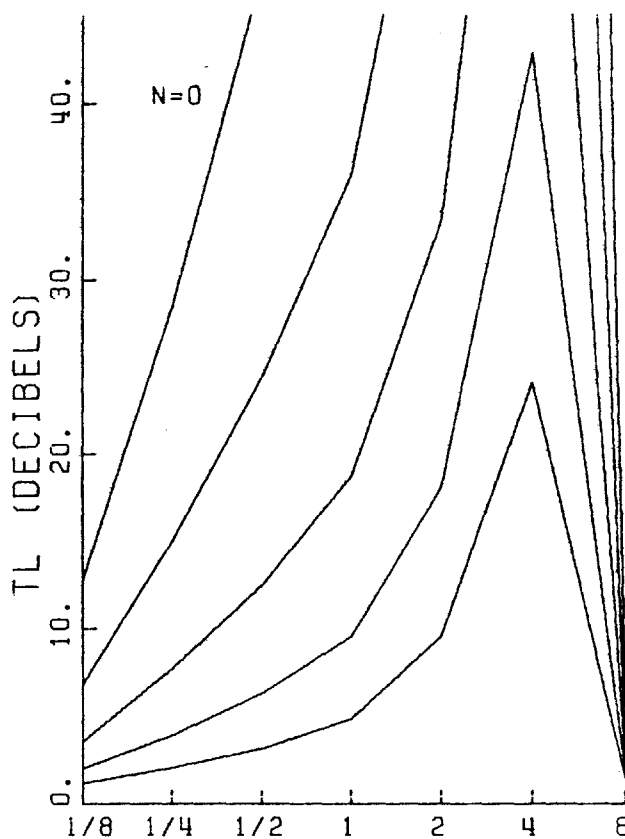


Figure A3.85

THETA=8.  
D/L=12.928  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

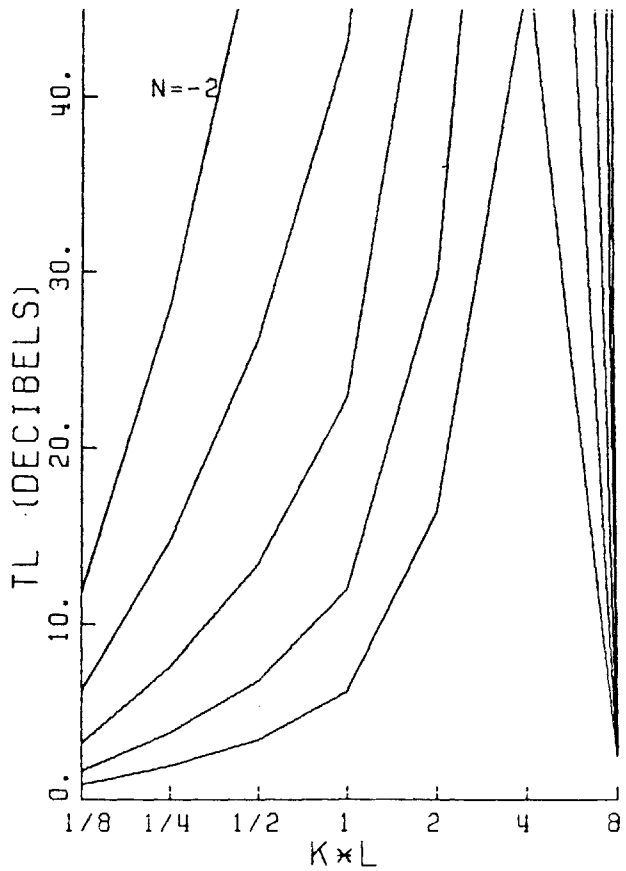
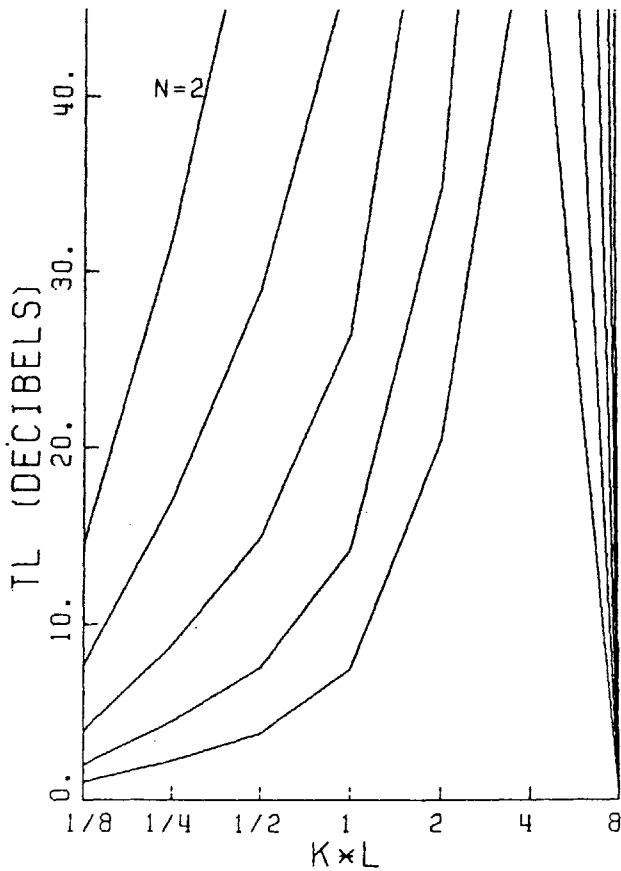
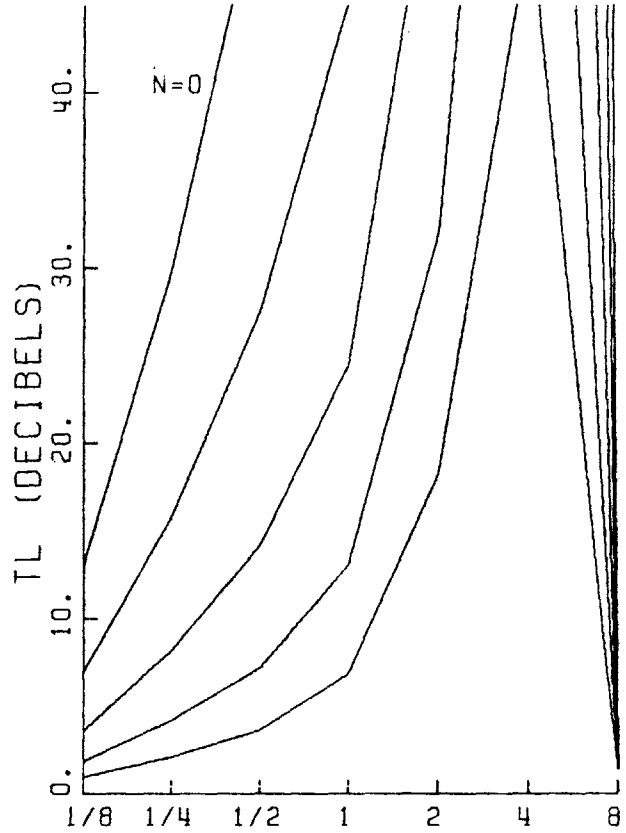


Figure A3.86

THETA=12.  
 D/L=1.094  
 AREA RATIO=1

S/D=16  
     8  
     4  
     2  
     1

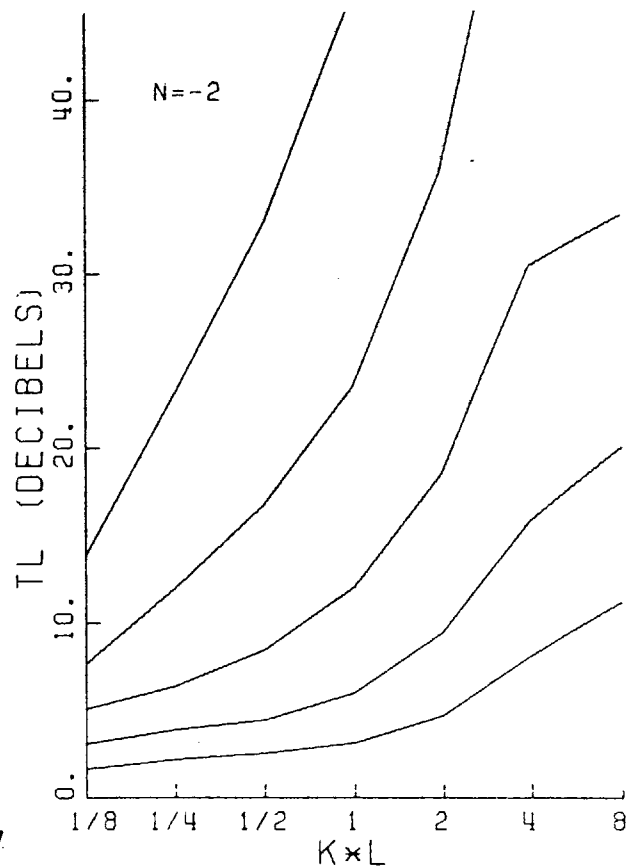
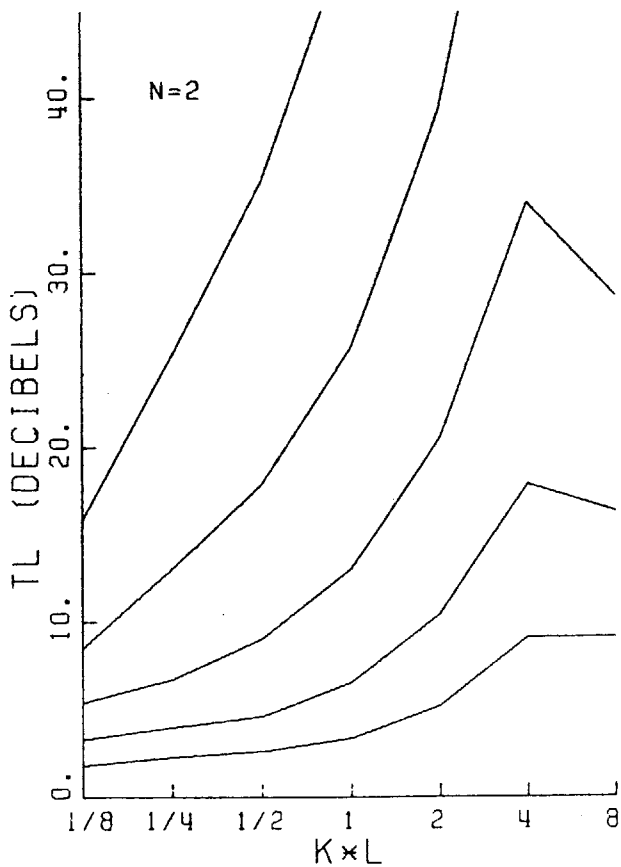
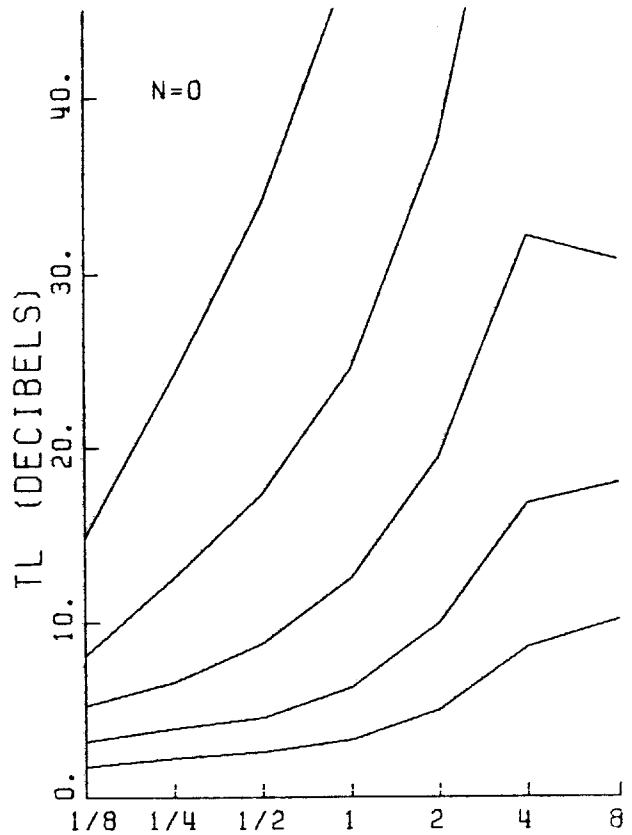
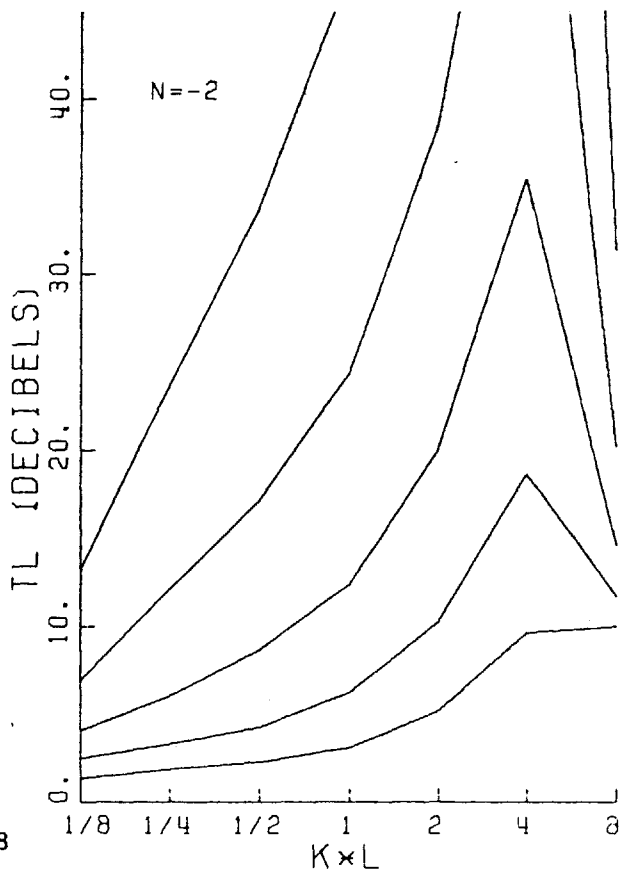
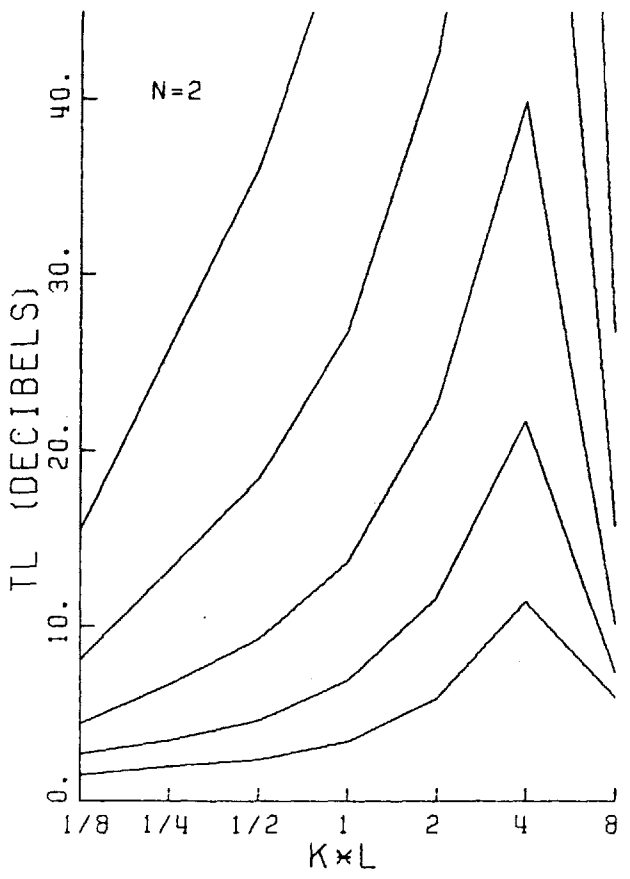
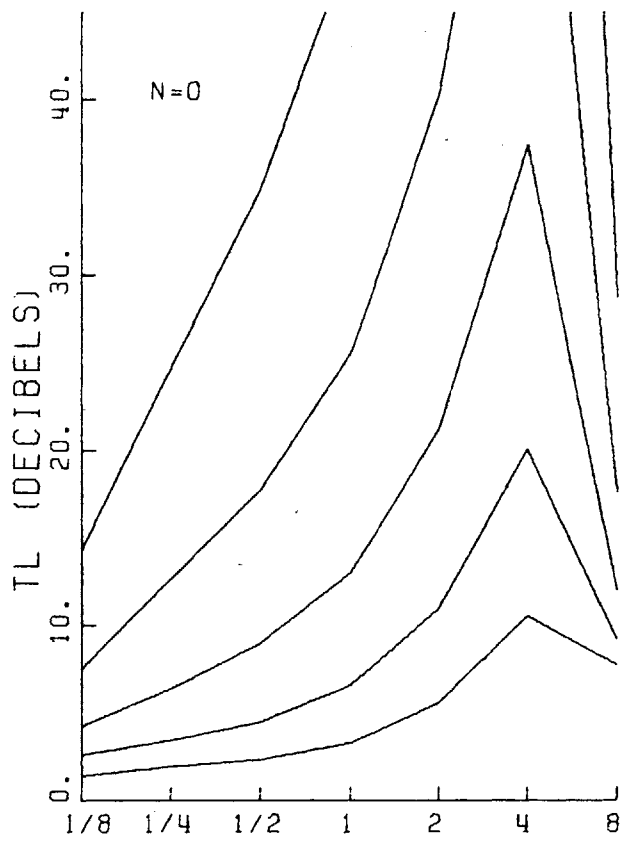


Figure A3.87

THETA=12.  
D/L=2.000  
AREA RATIO=1

S/D=16  
8  
4  
2  
1



**Figure A3.88**

THETA=12.  
 D/L=4.828  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

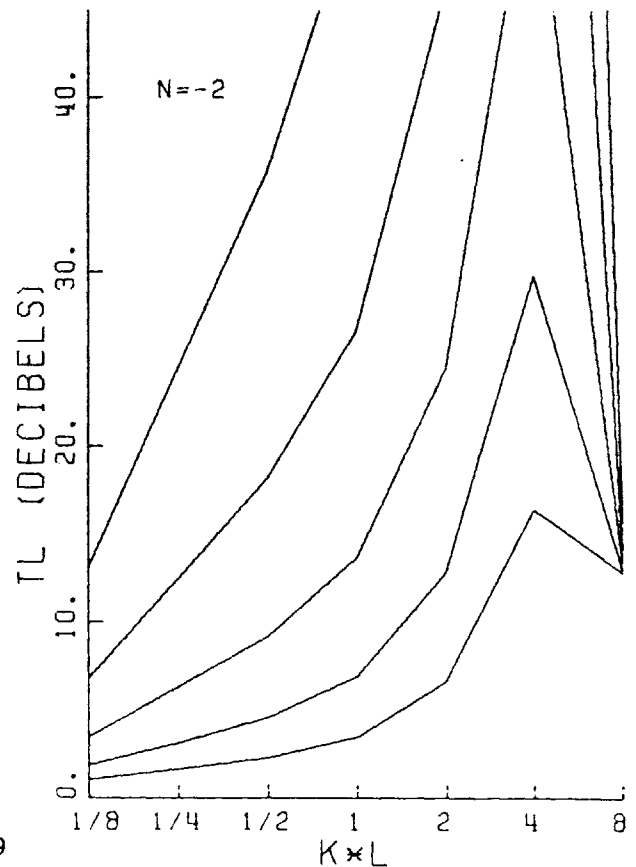
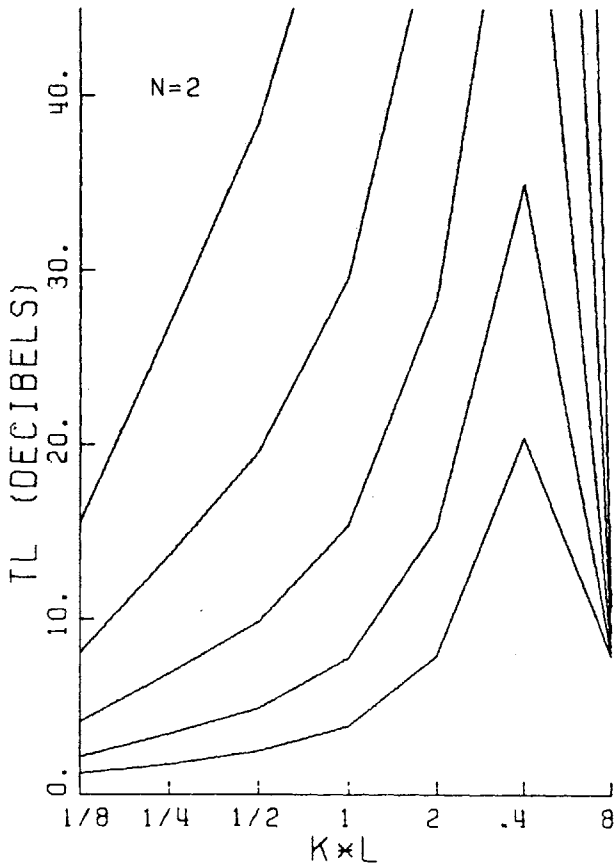
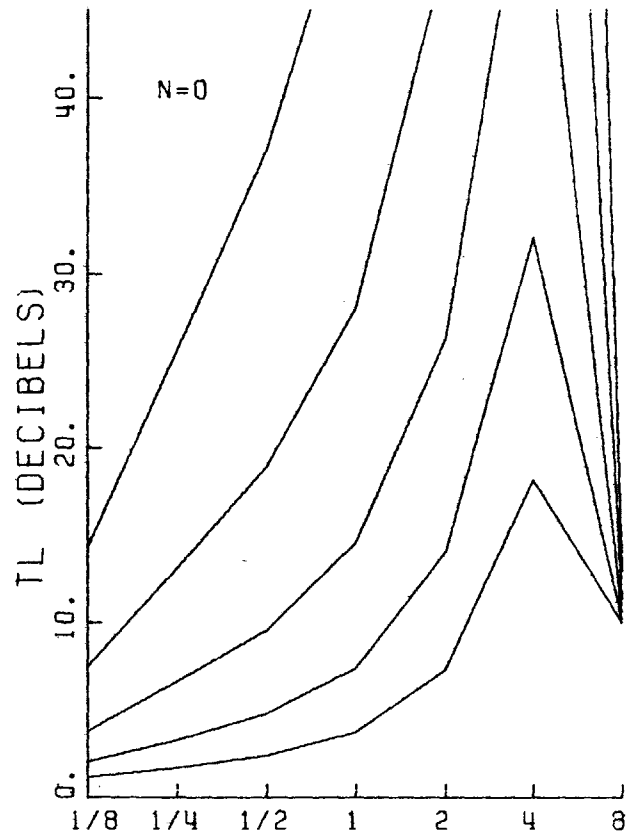




Figure A3.89

THETA=12.  
D/L=12.928  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

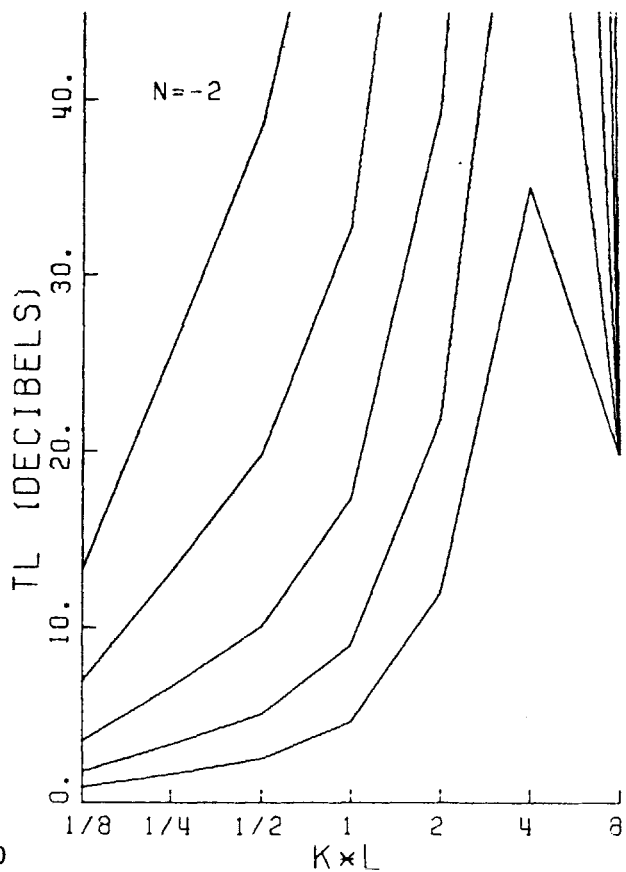
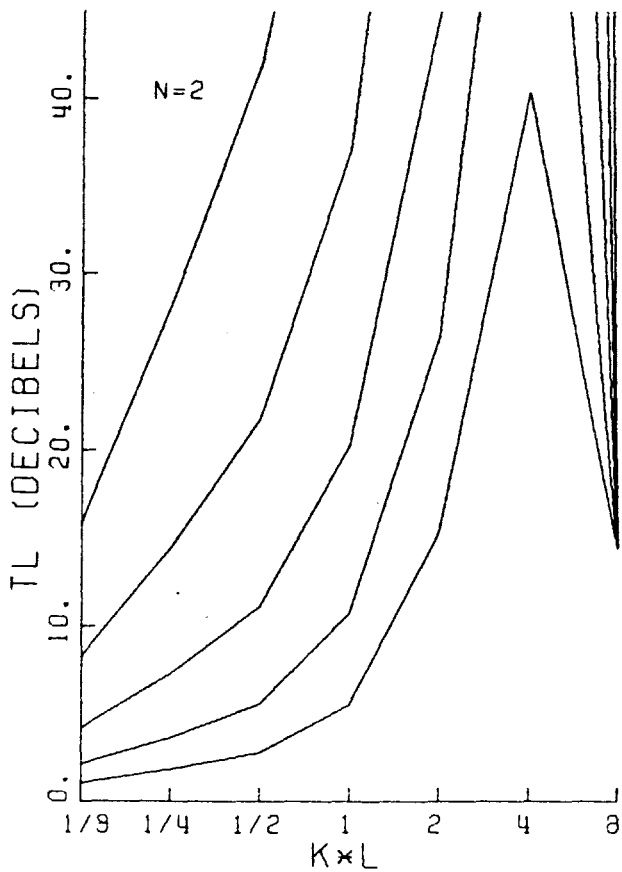
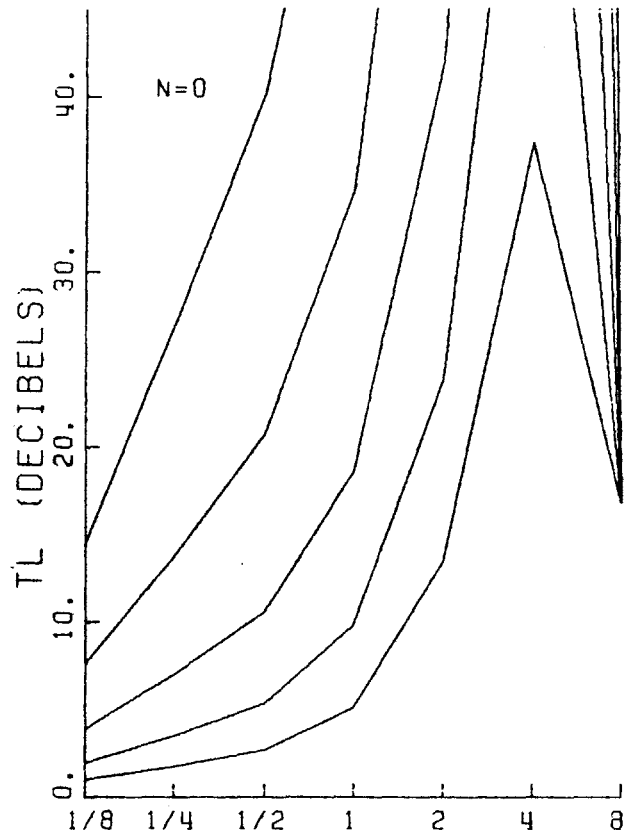


Figure A3.90

THETA=16.  
D/L=1.094  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

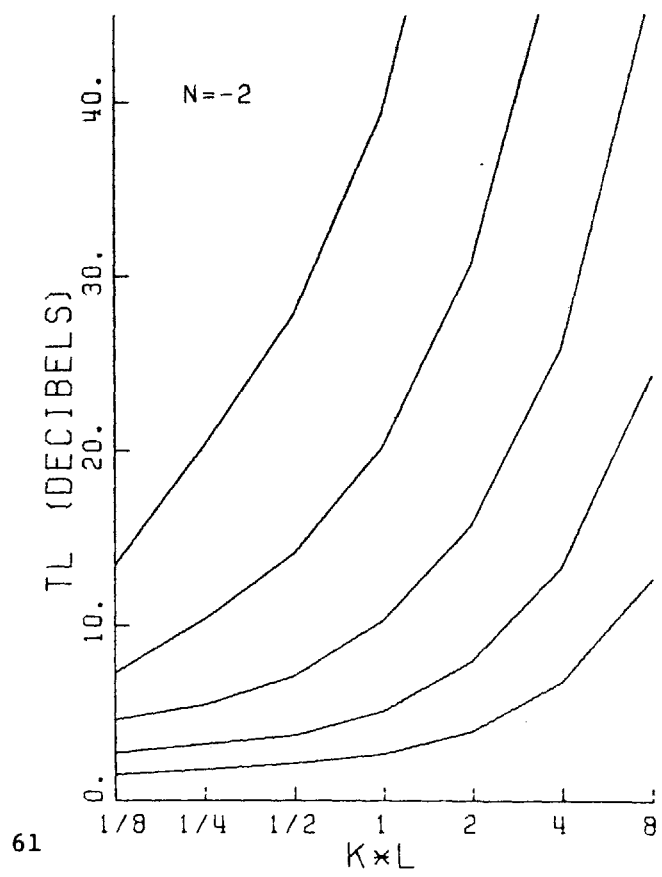
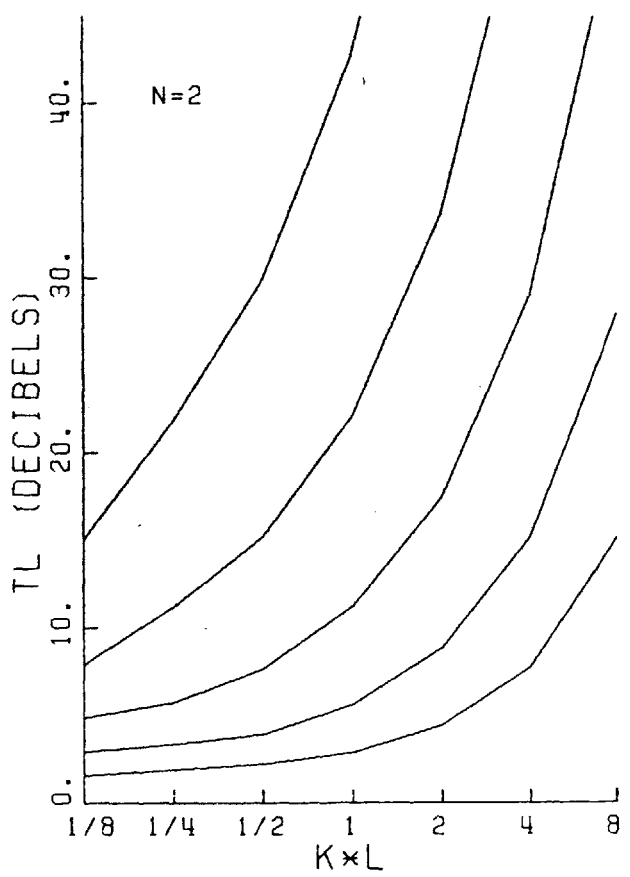
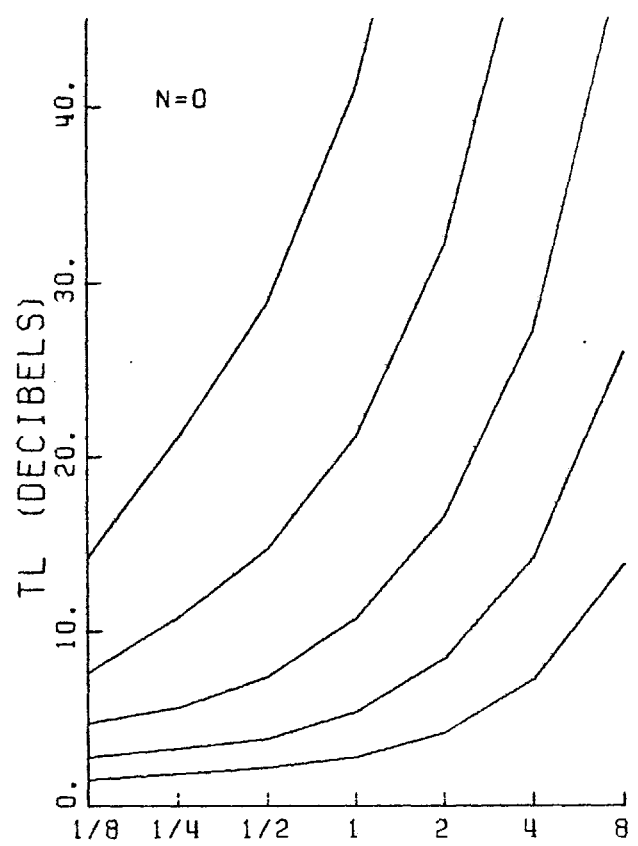


Figure A3.91

THETA=16.  
D/L=2.000  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

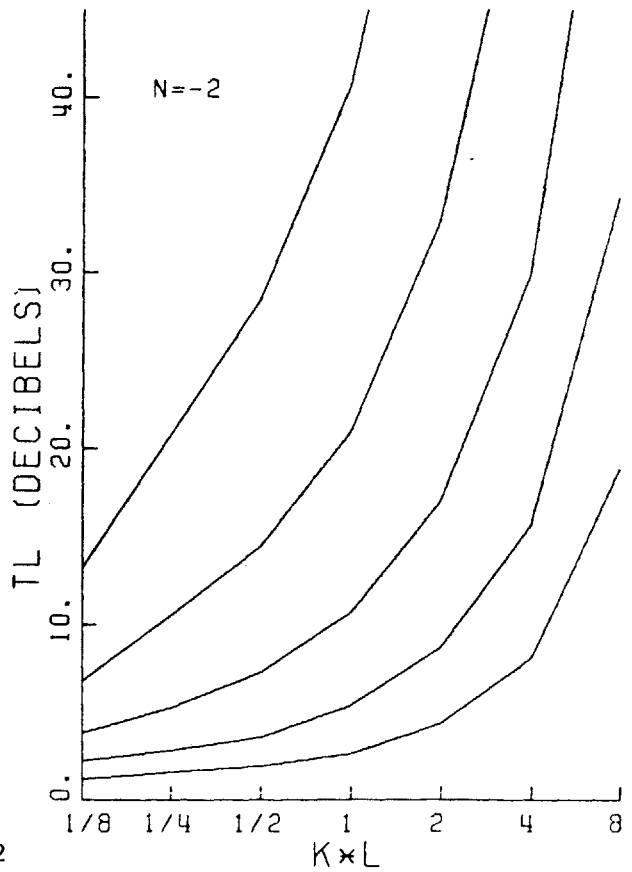
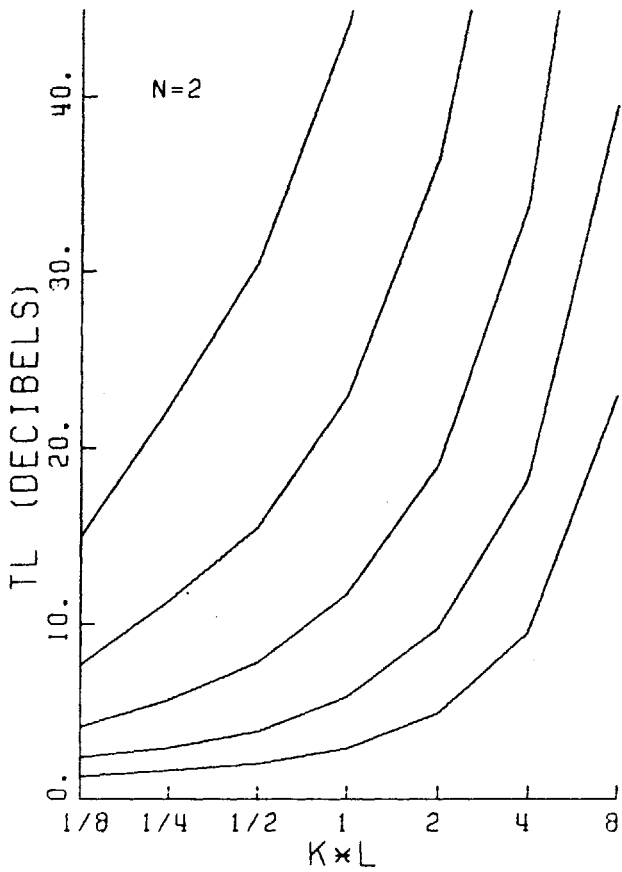
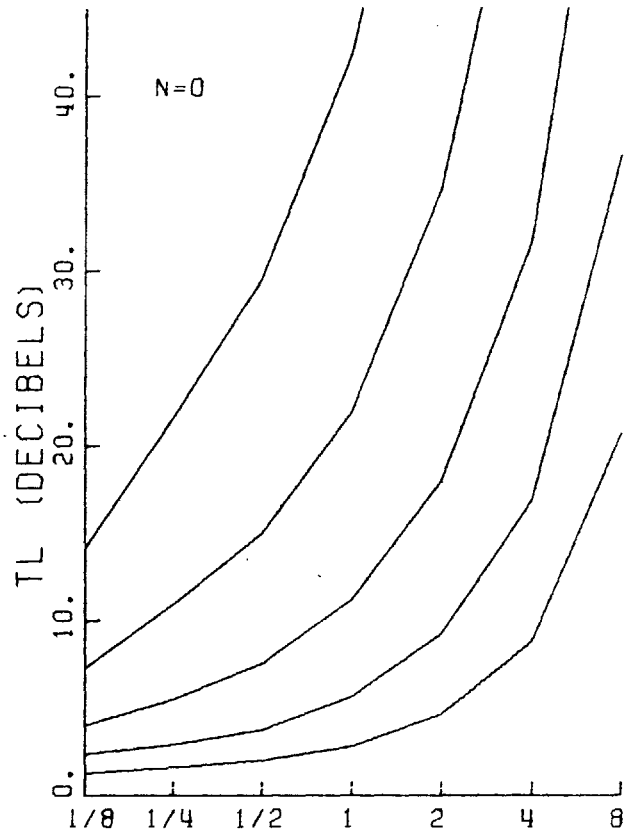


Figure A3.92

THETA=16.  
D/L=4.828  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

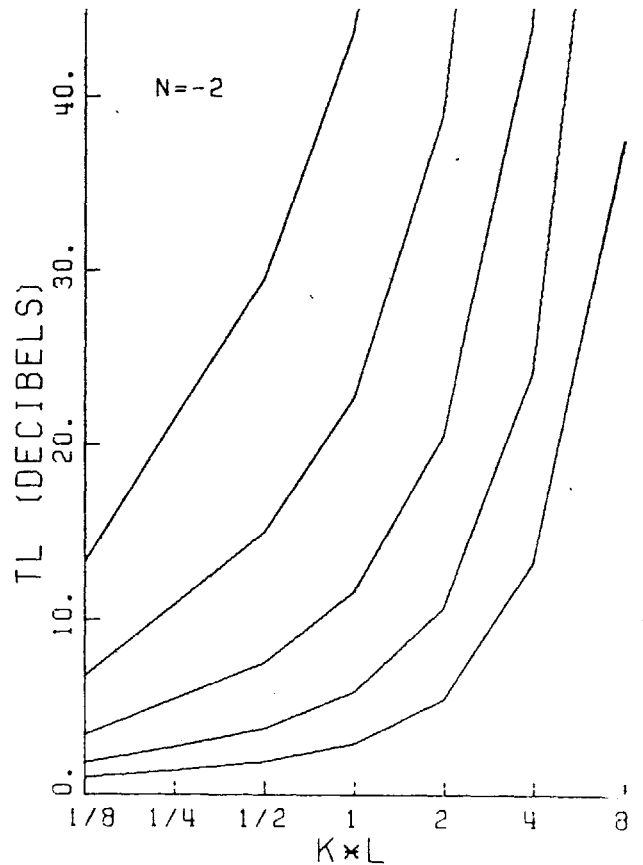
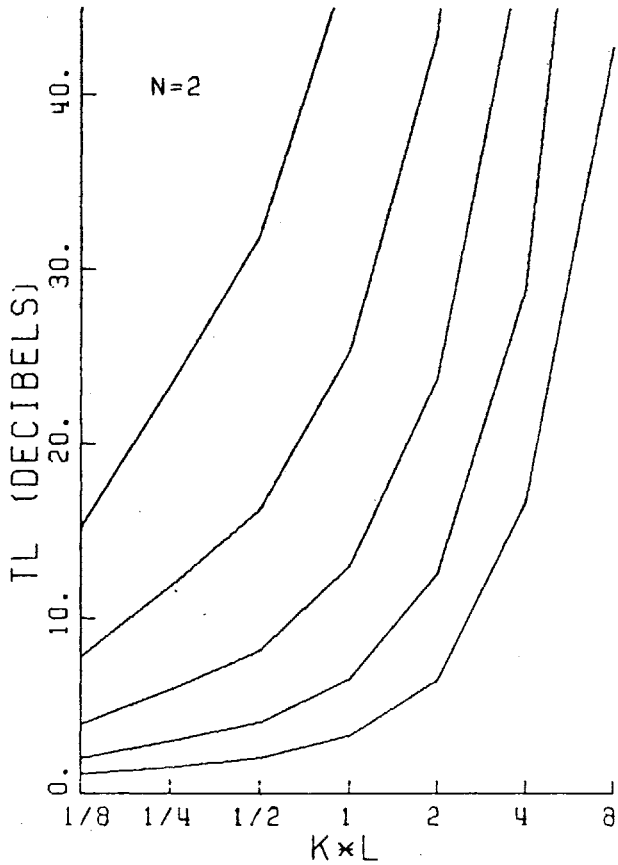
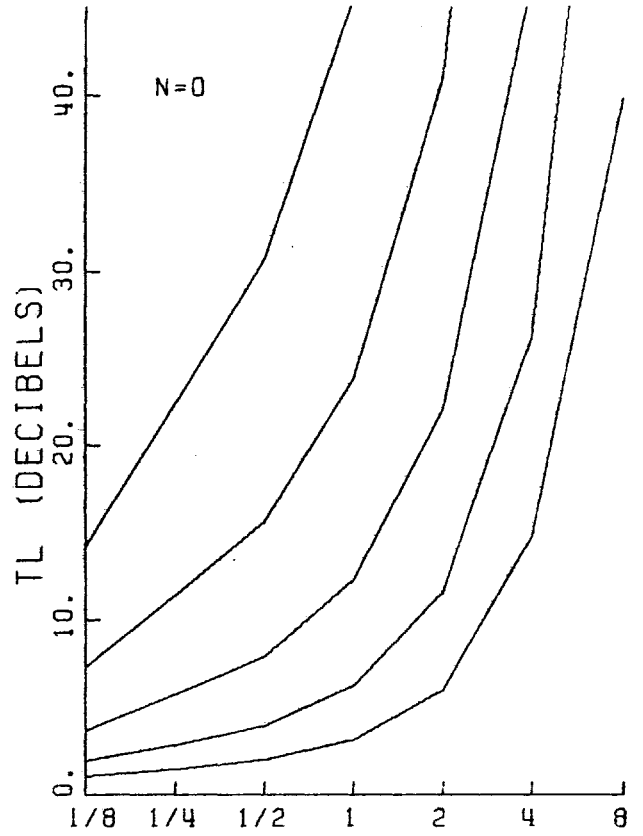


Figure A3.93

THETA=16.  
 D/L=12.928  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

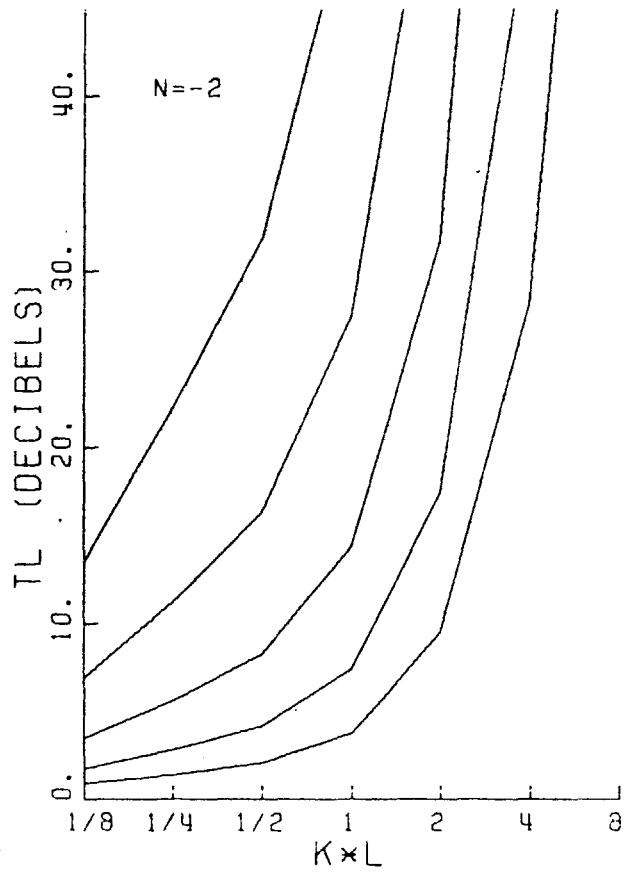
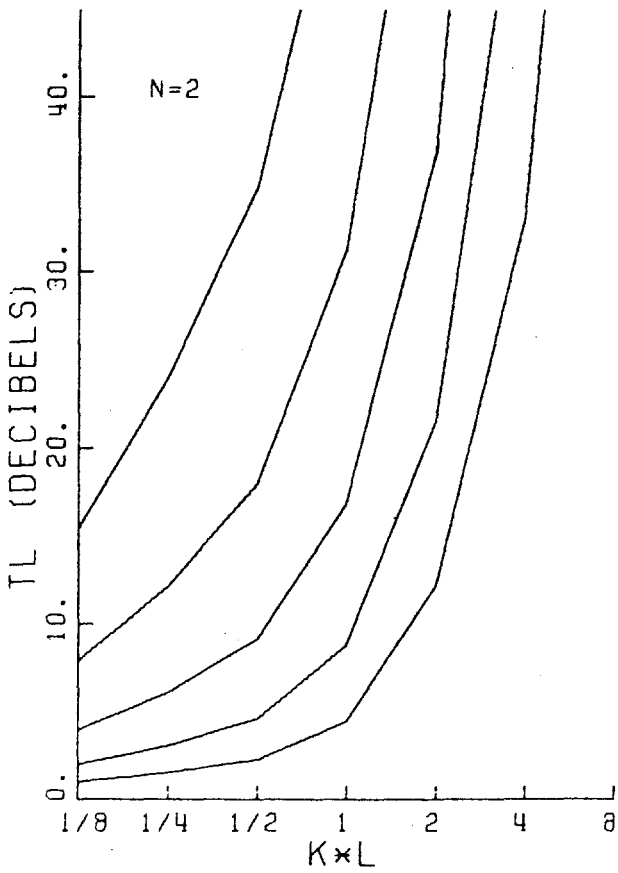
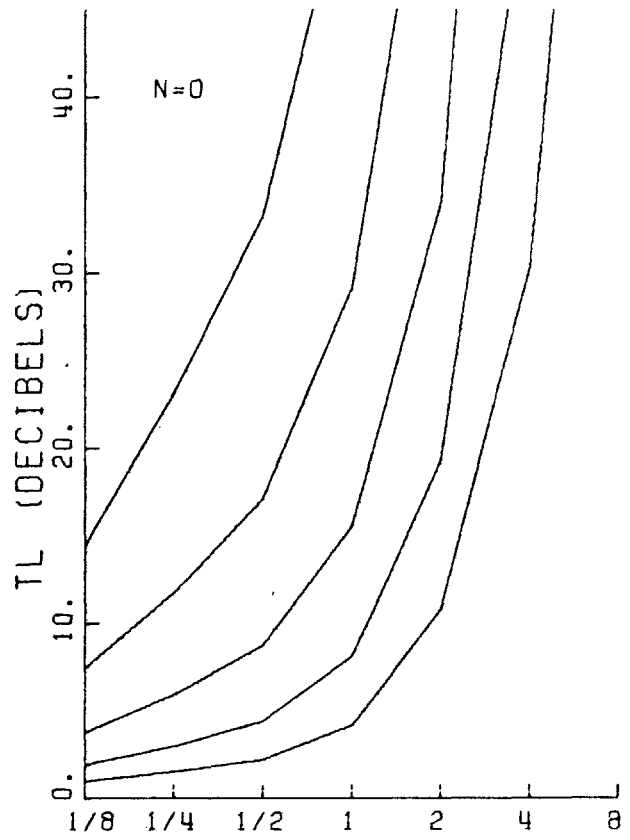


Figure A3.94

THETA=20.  
 D/L=1.094  
 AREA RATIO=1

S/D=16  
       8  
       4  
       2  
       1

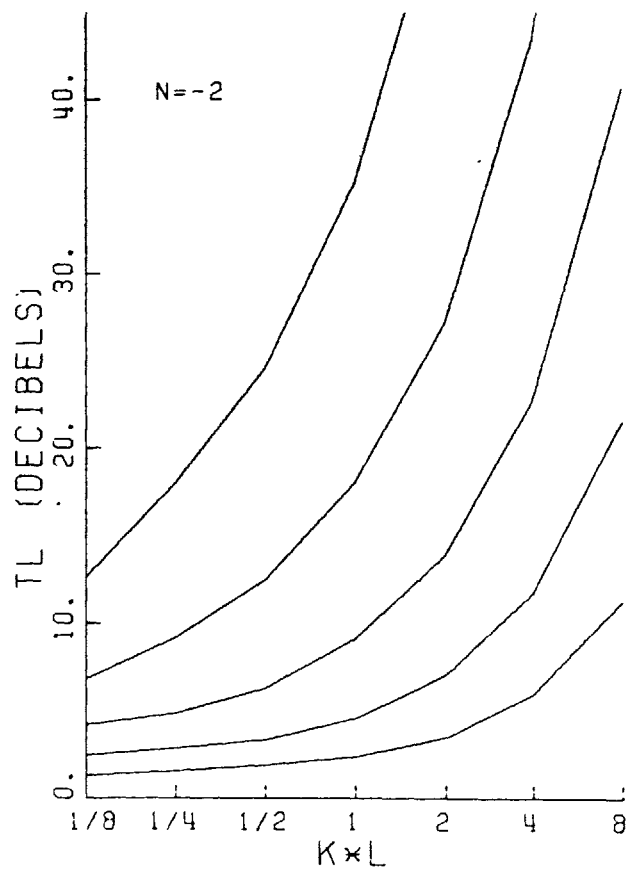
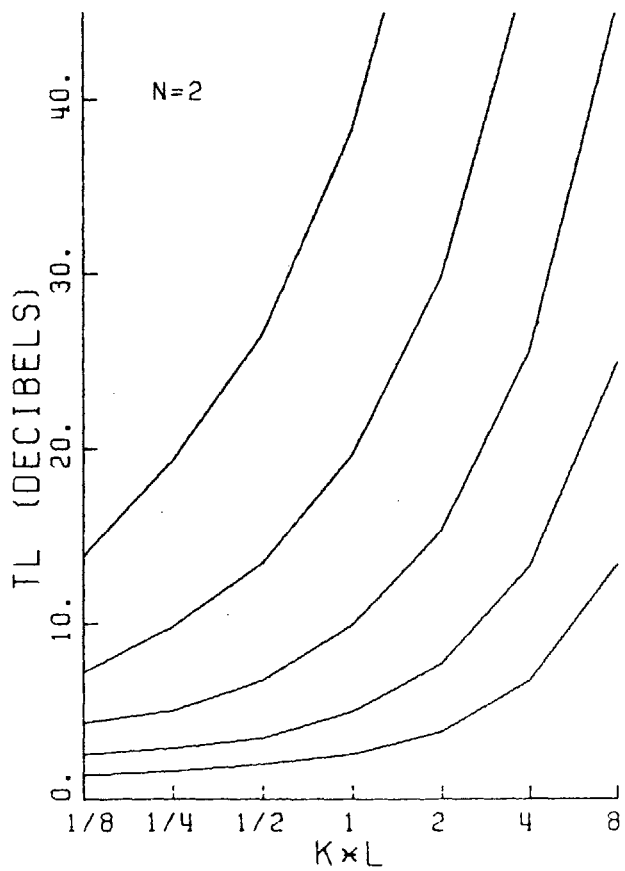
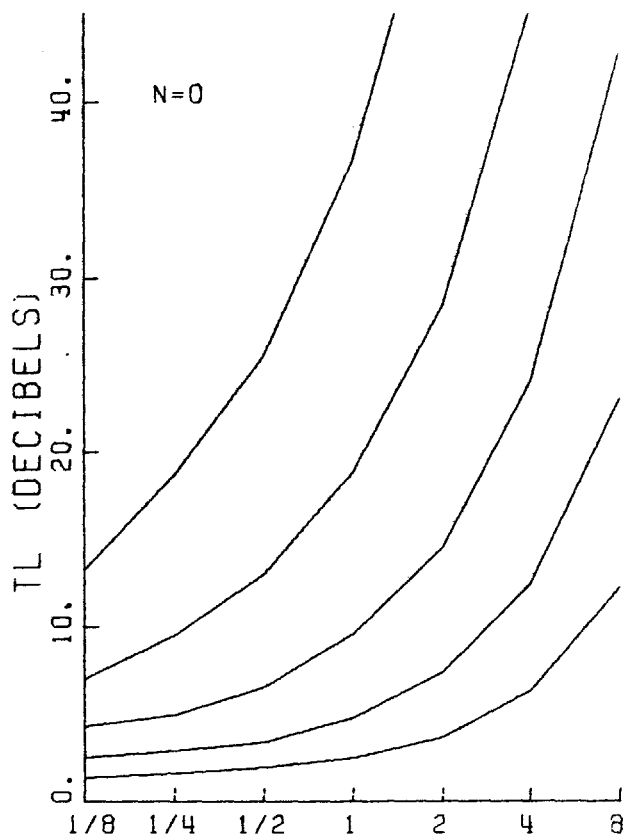


Figure A3.95

THETA=20.  
D/L=2.000  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

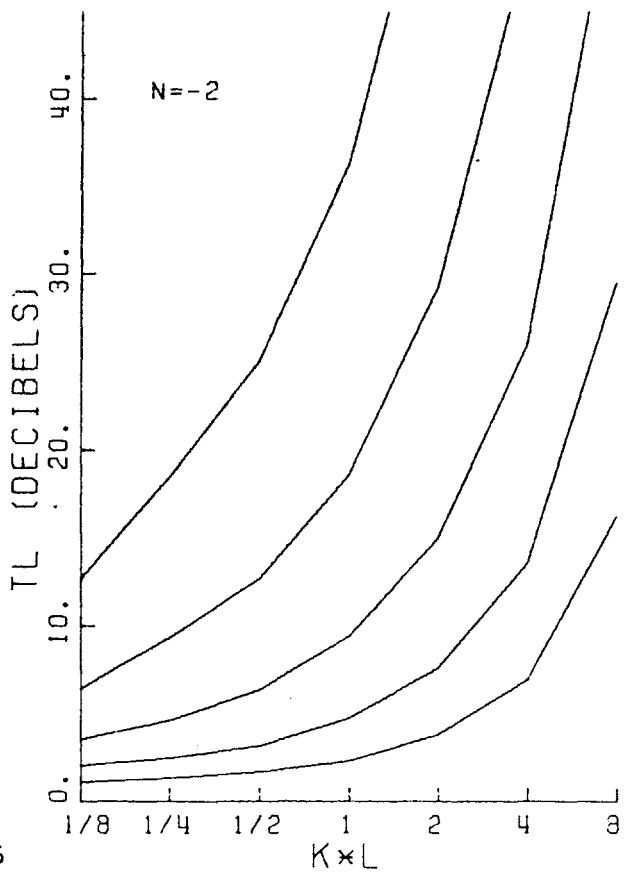
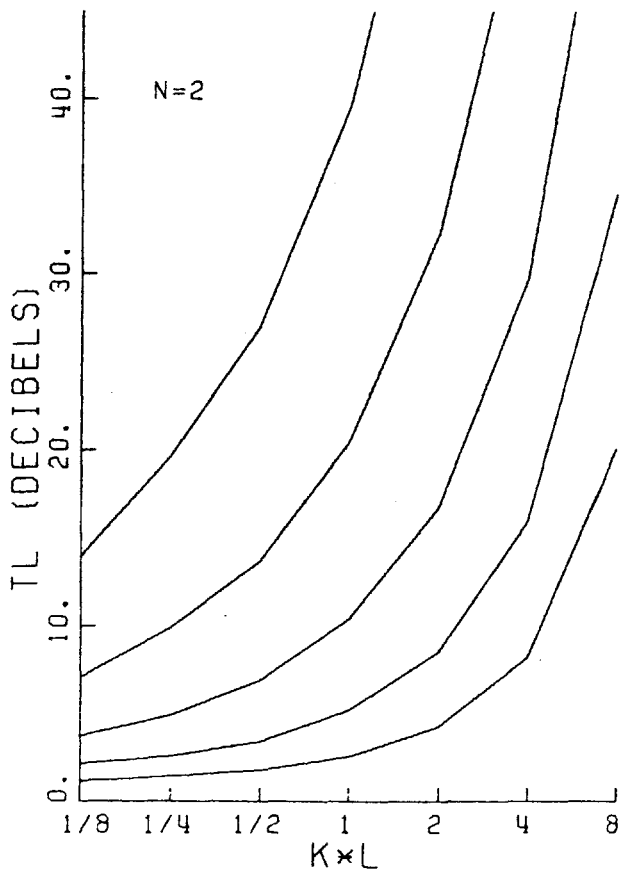
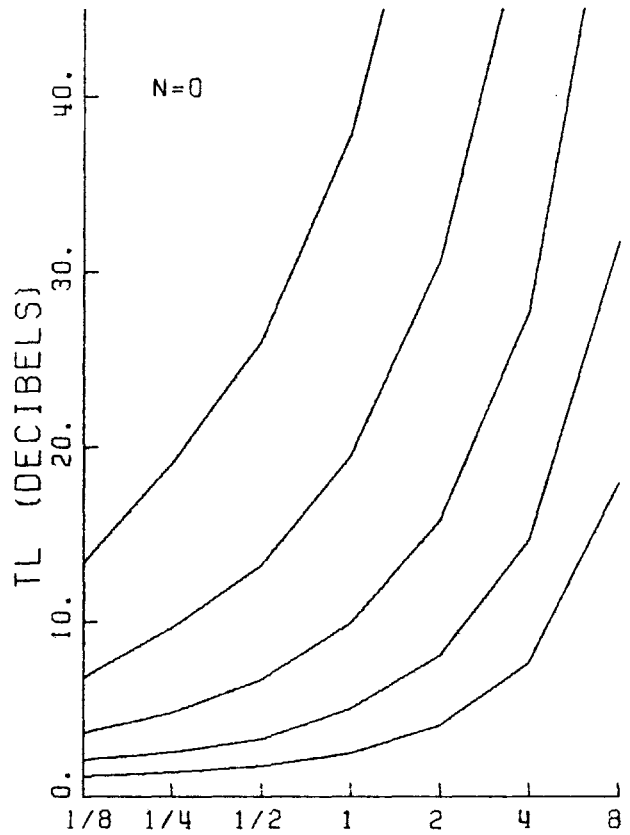


Figure A3.96

THETA=20.  
D/L=4.828  
AREA RATIO=1

S/D=16  
8  
4  
2  
1

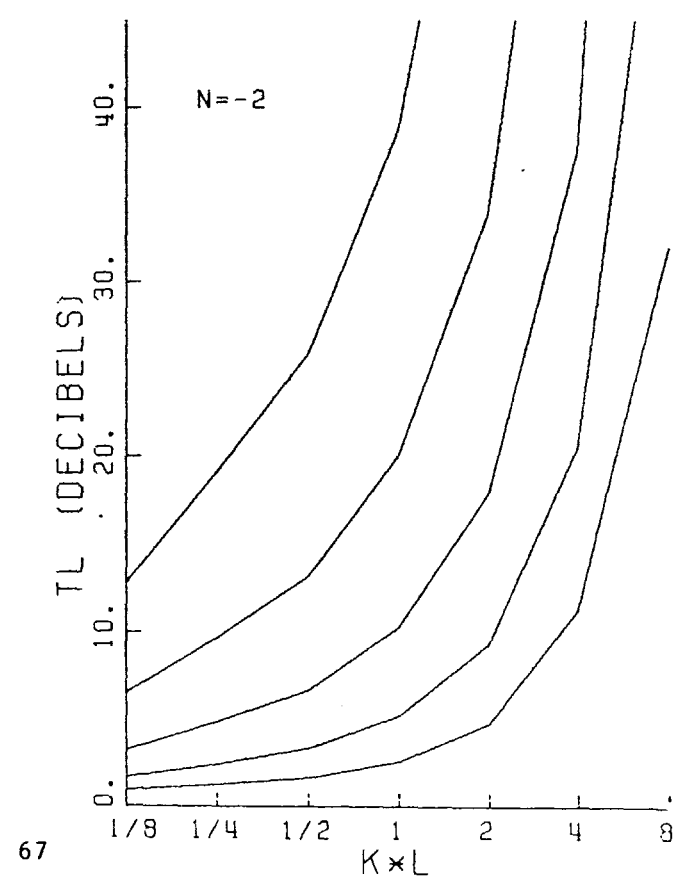
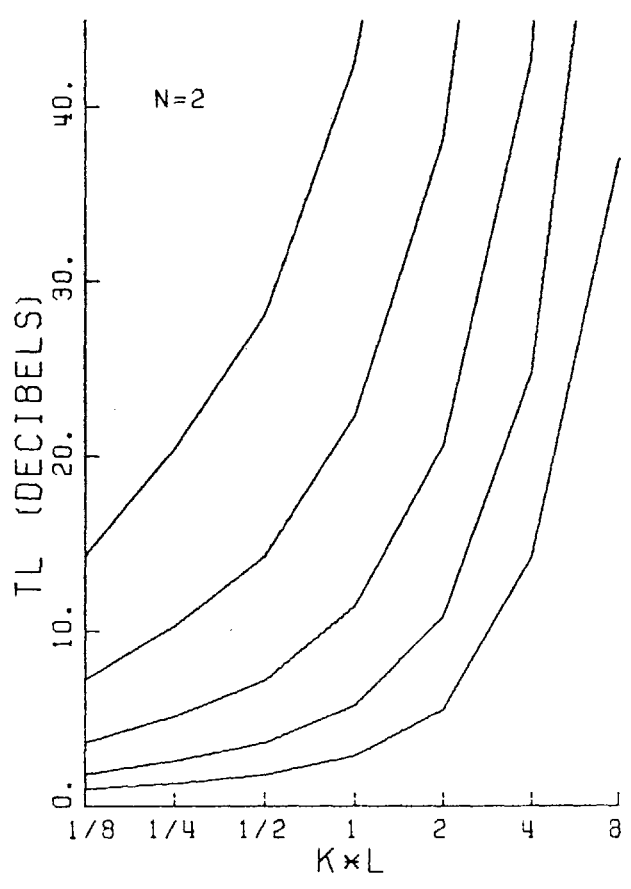
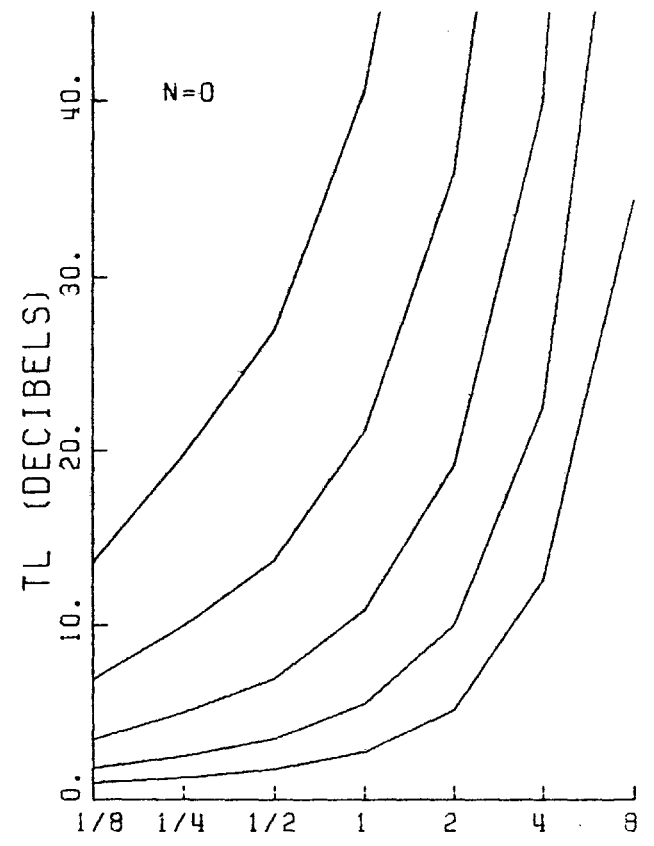
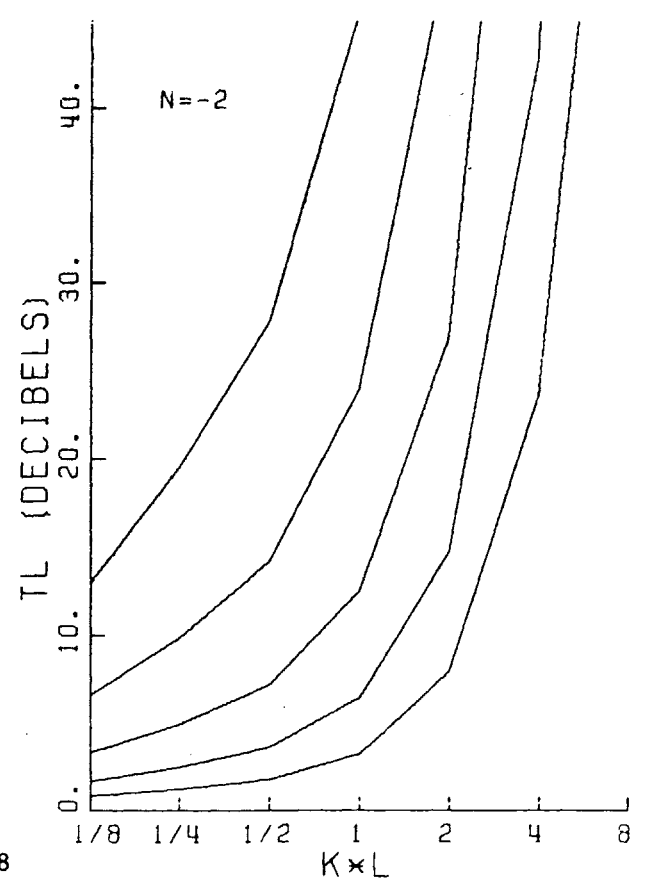
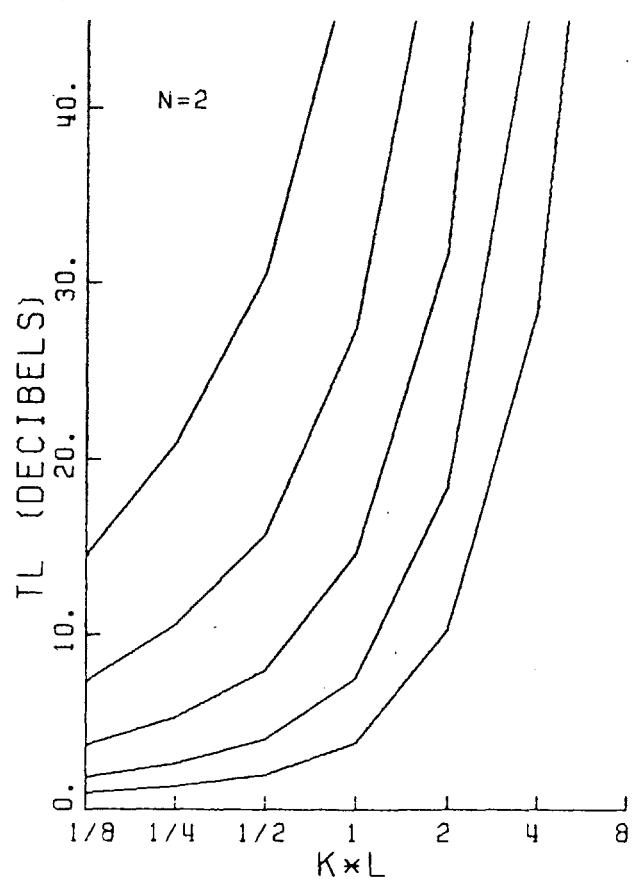
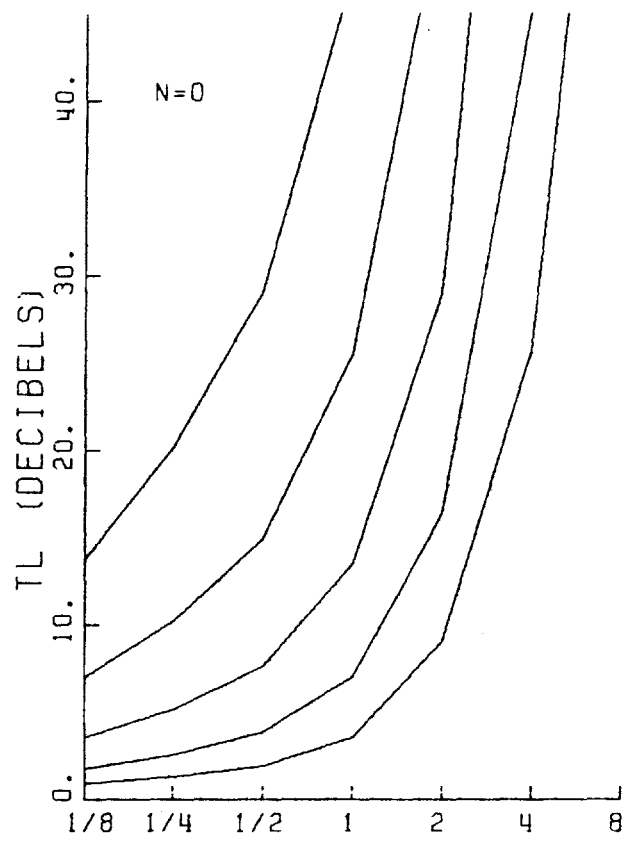




Figure A3.97

THETA=20.  
D/L=12.928  
AREA RATIO=1

S/D=16  
8  
4  
2  
1



Figures A3.110 - A3.113: Octave band TL vs S/D for a circular duct lined with a resistive screen type resonator liner. Each figure corresponds to a different value of D/L. In each figure four frames are shown, corresponding to  $\theta = 0.5, 1, 2,$  and  $4$ . In each frame four curves are plotted, corresponding to four different values of kL as indicated by symbols.

Figure A3.110  
 AREA RATIO=1.0     $D/L=1.054$

C-R

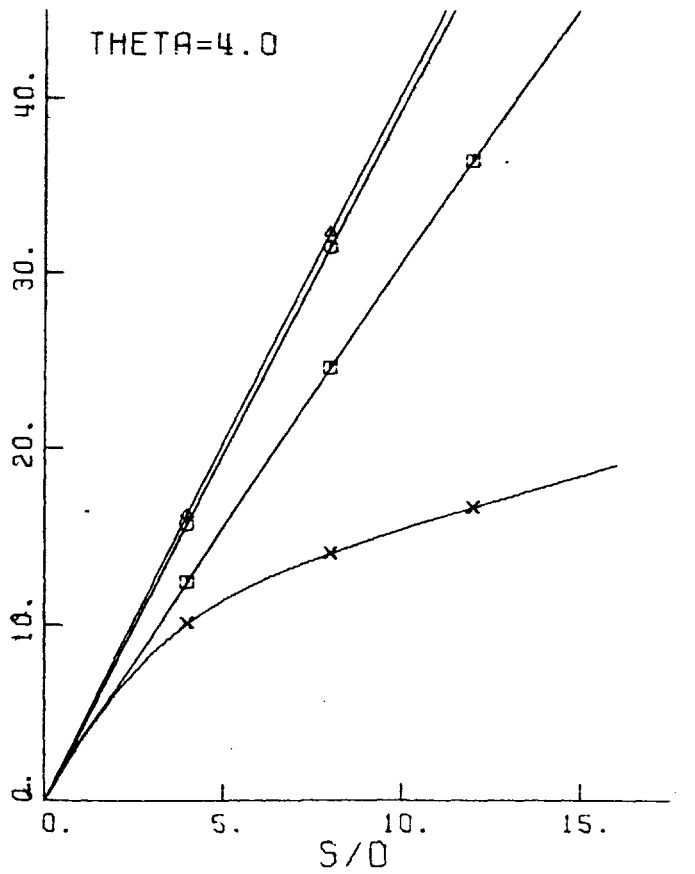
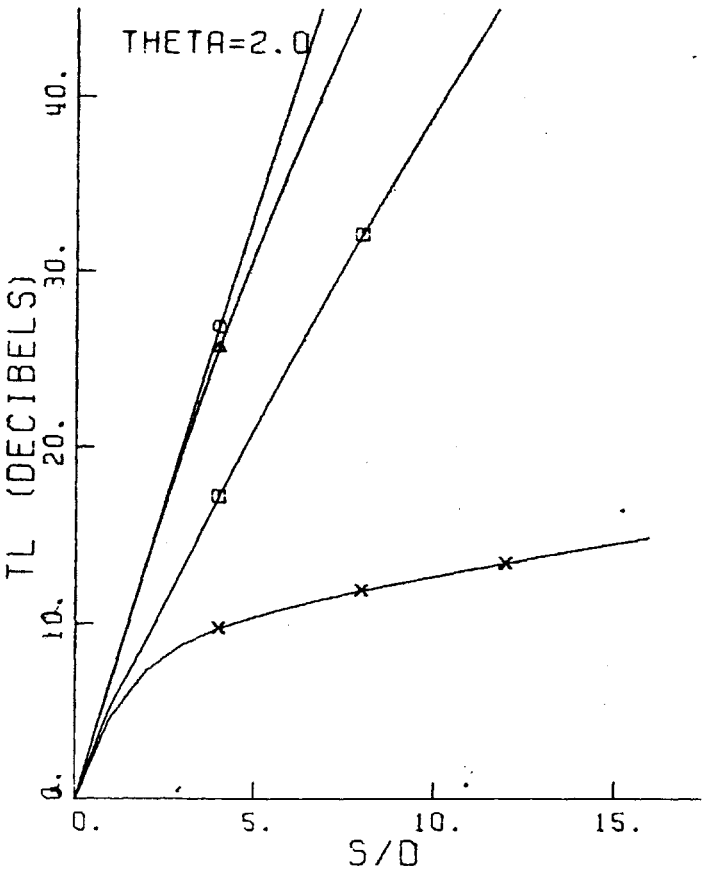
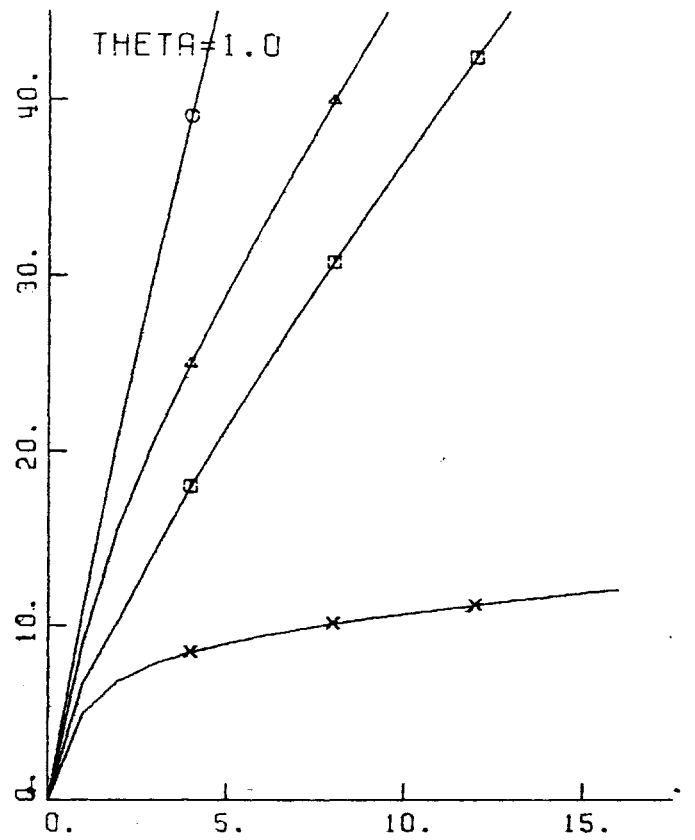
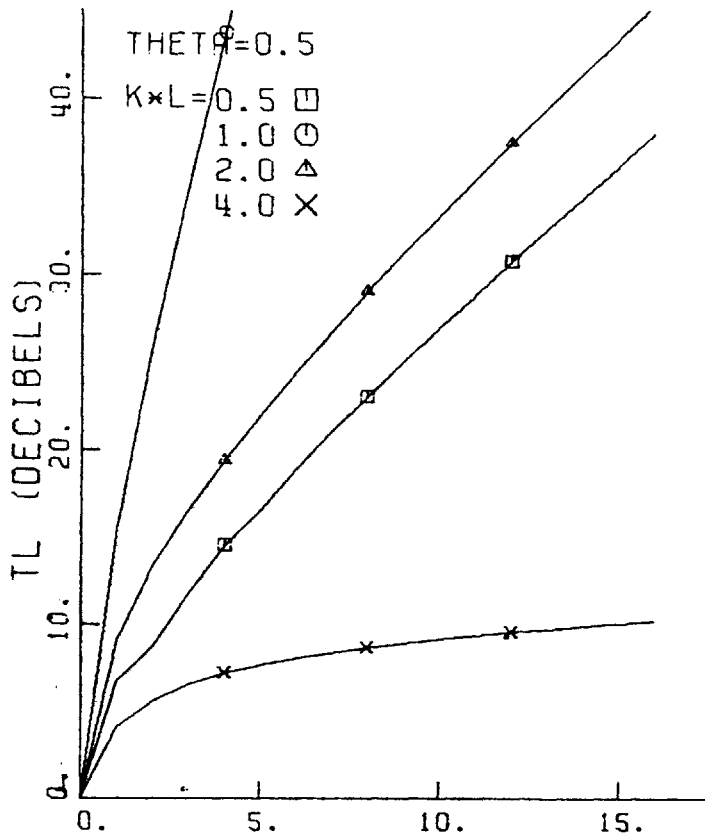


Figure A3.111

C-R

AREA RATIO=1.0 D/L=2.000

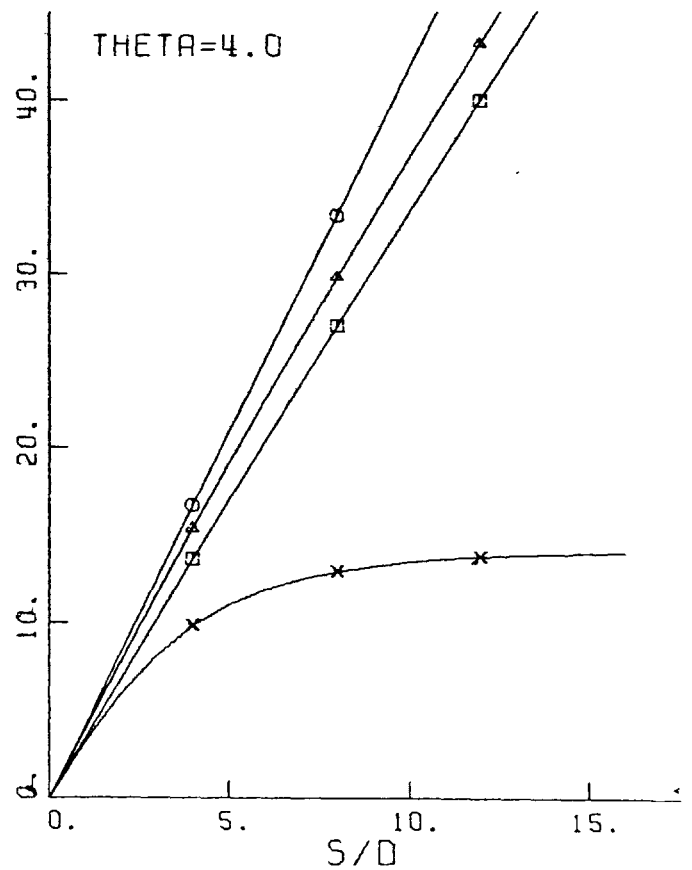
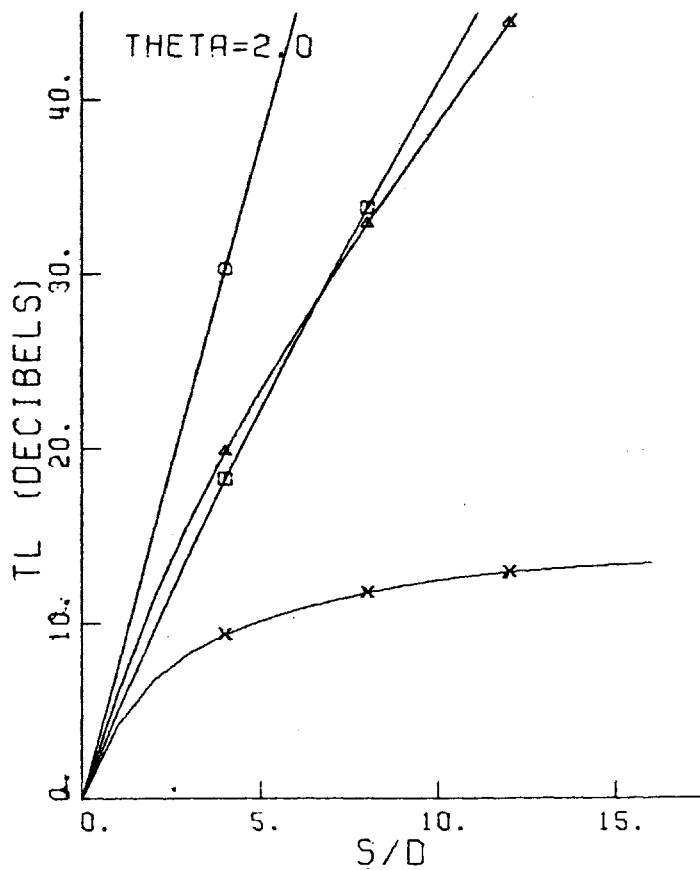
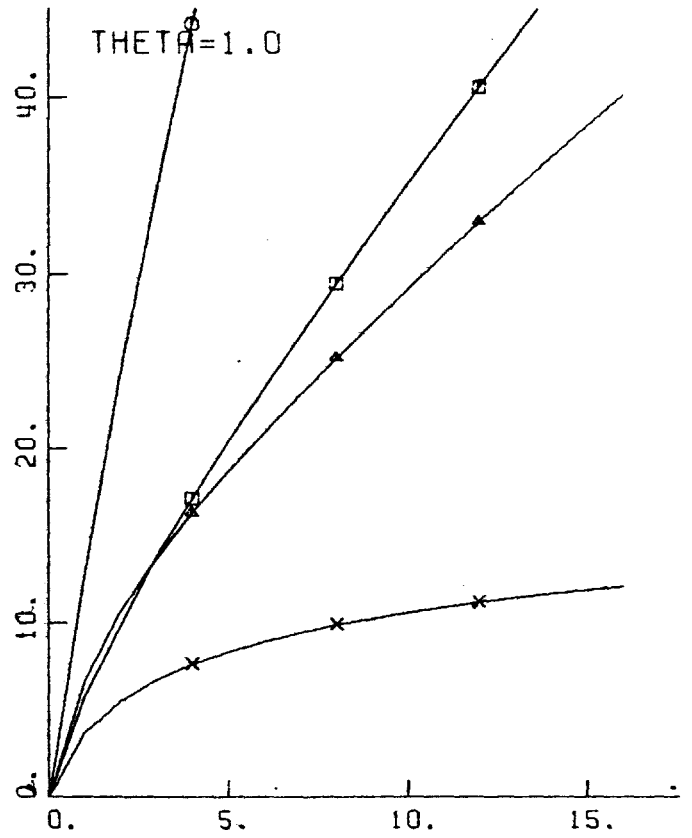
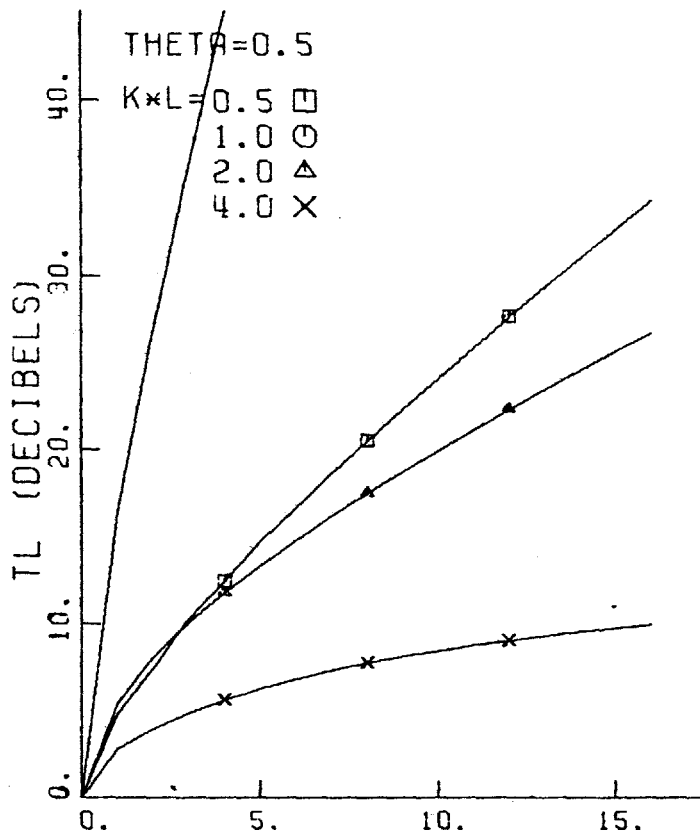


Figure A3.112

C-R

AREA RATIO=1.0 D/L=4.828

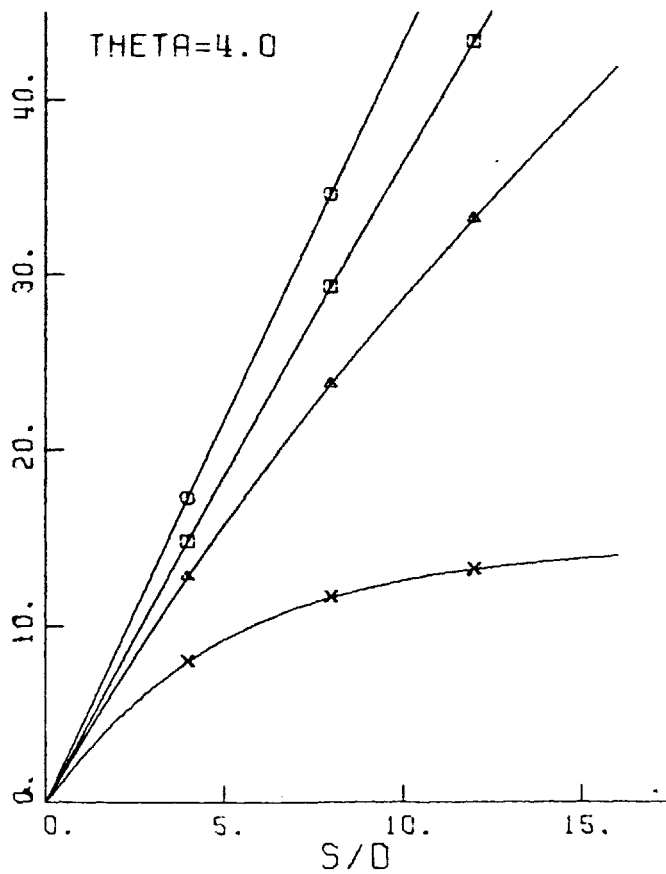
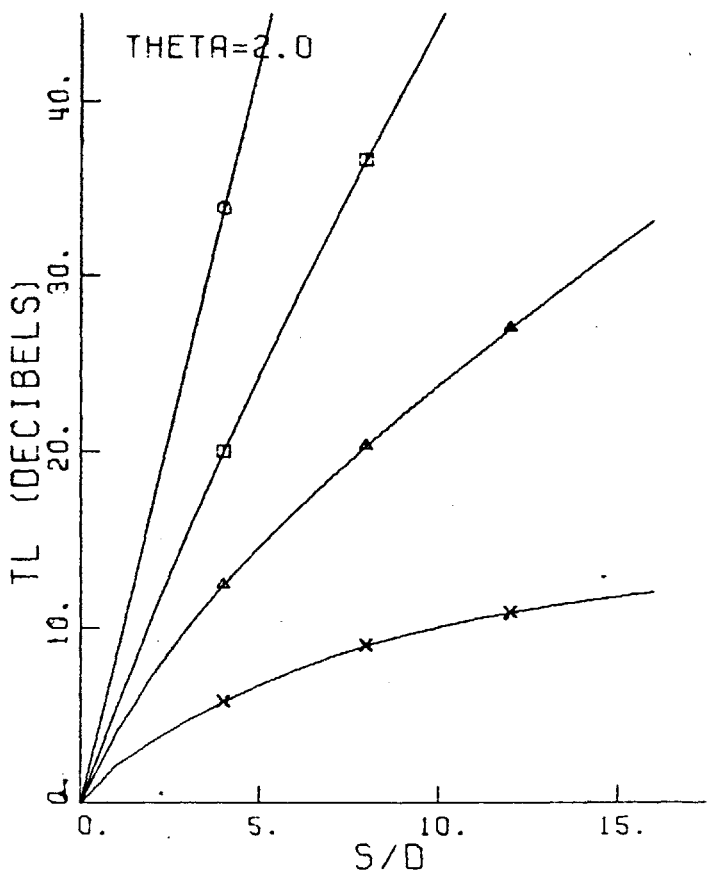
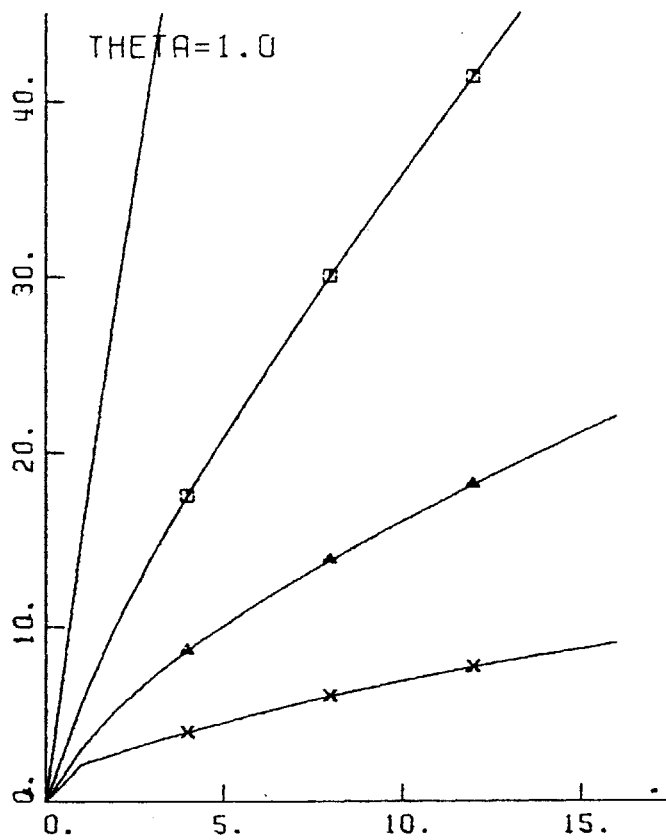
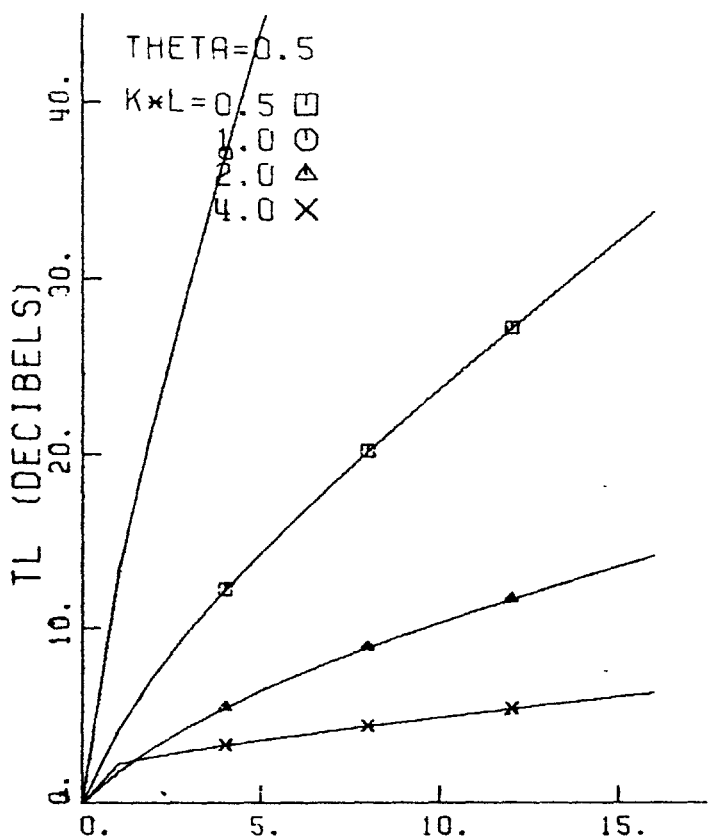
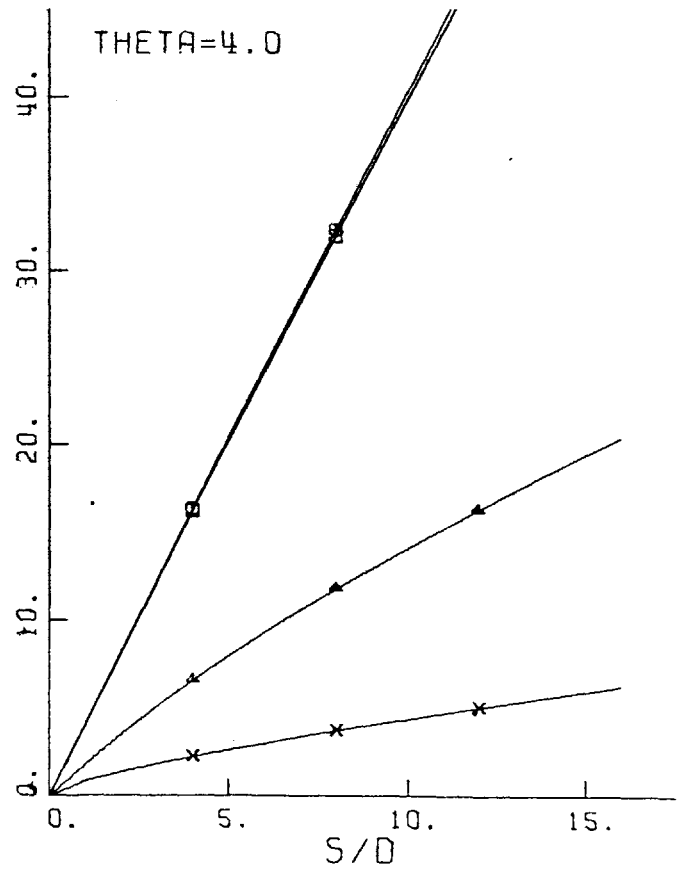
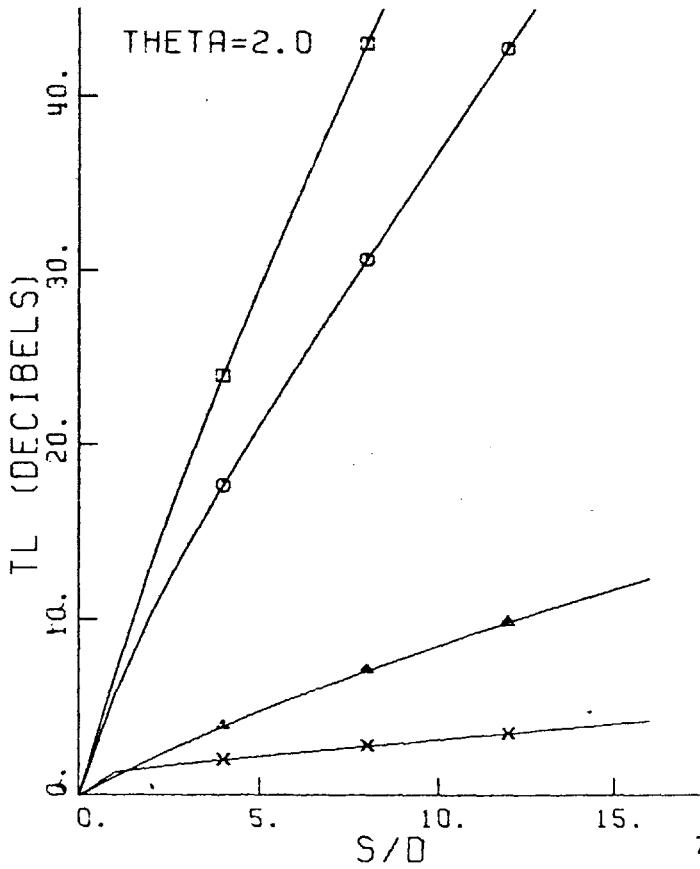
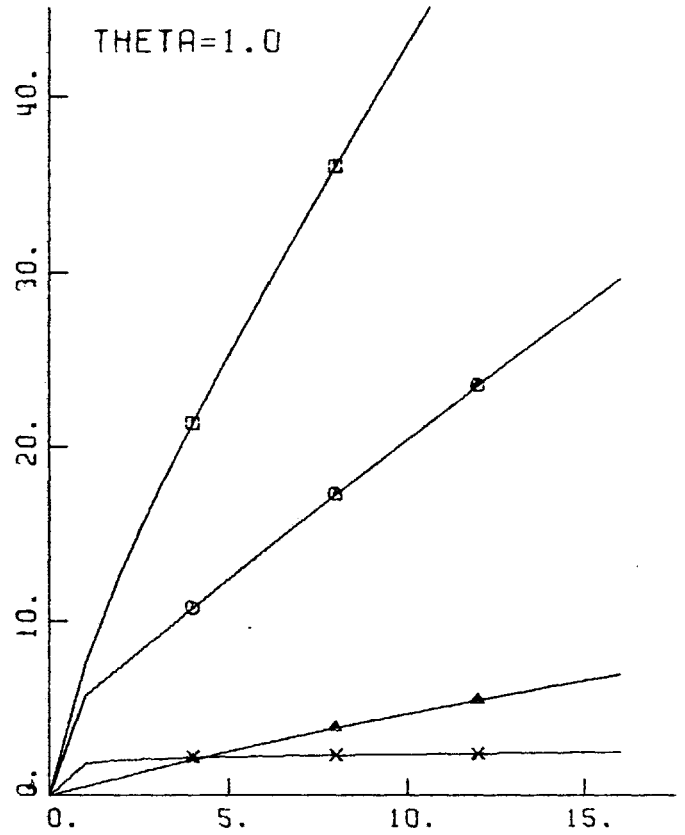
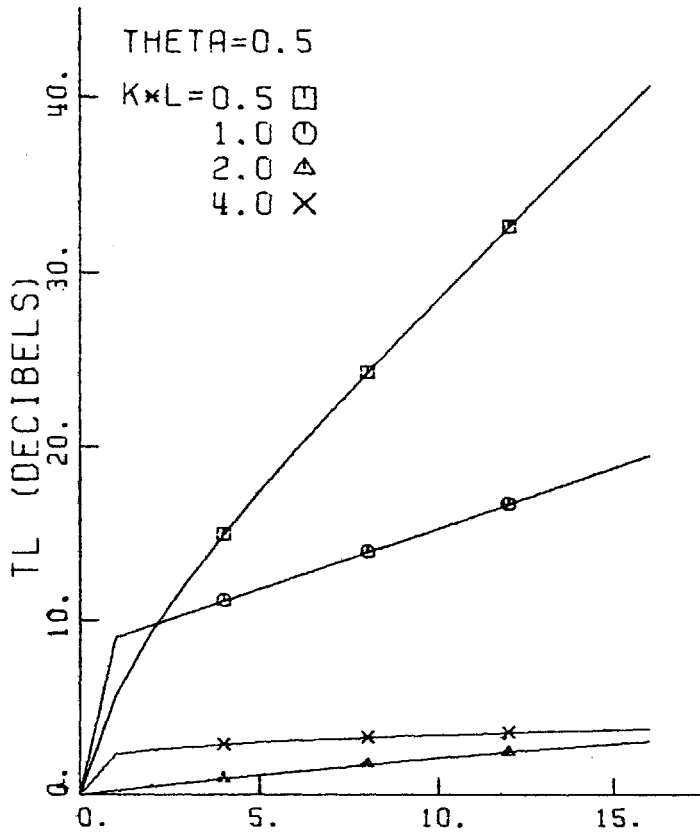


Figure A3.113

C-R

AREA RATIO=1.0 D/L=12.928



Figures A3.114 - A3.121: Octave band TL vs S/D for a circular duct lined with a resistive screen type resonator liner.

The format is the same as in Figs. A3.110 - A3.113.

Figure A3.114

AREA RATIO=1.0 D/L=1.054

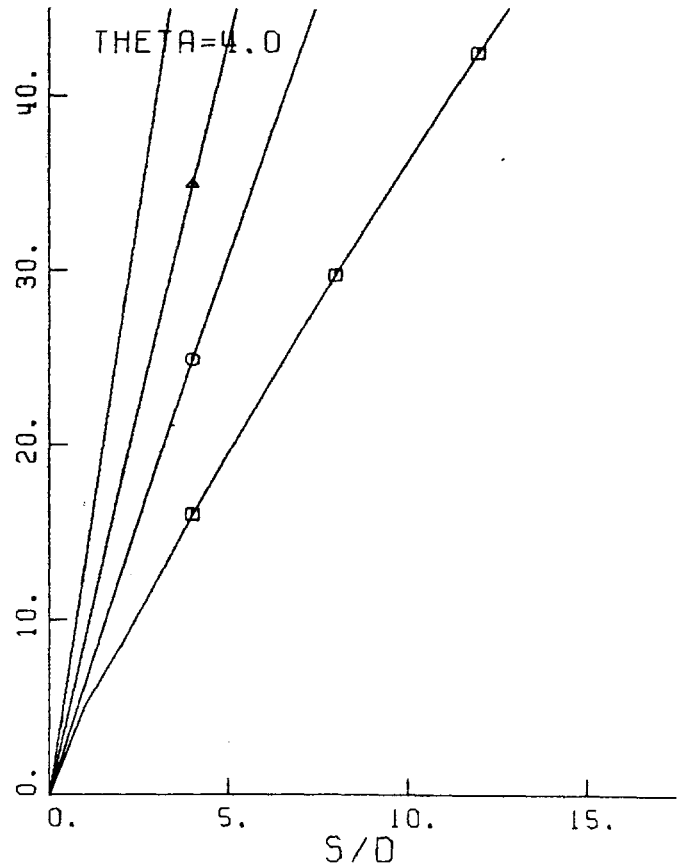
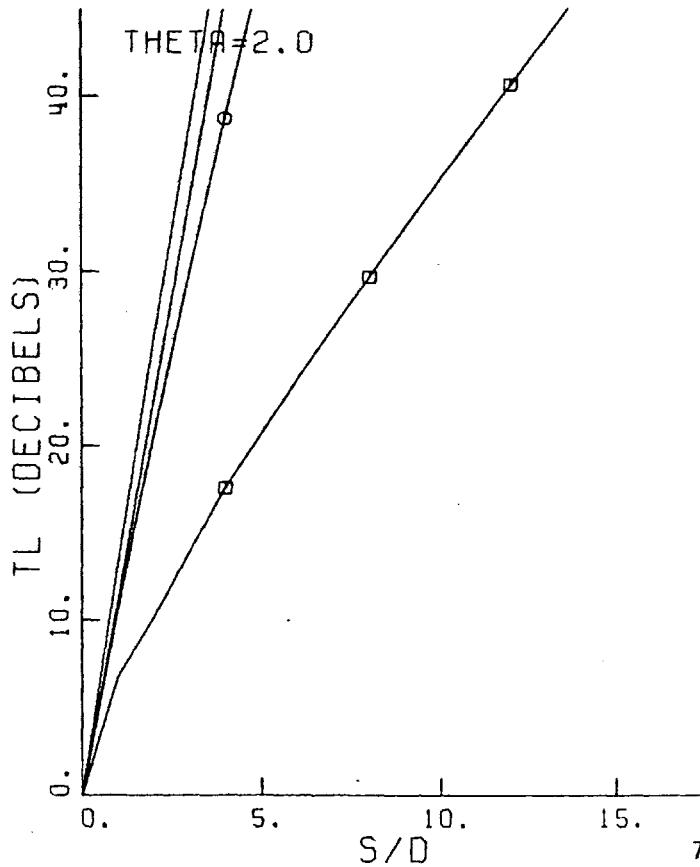
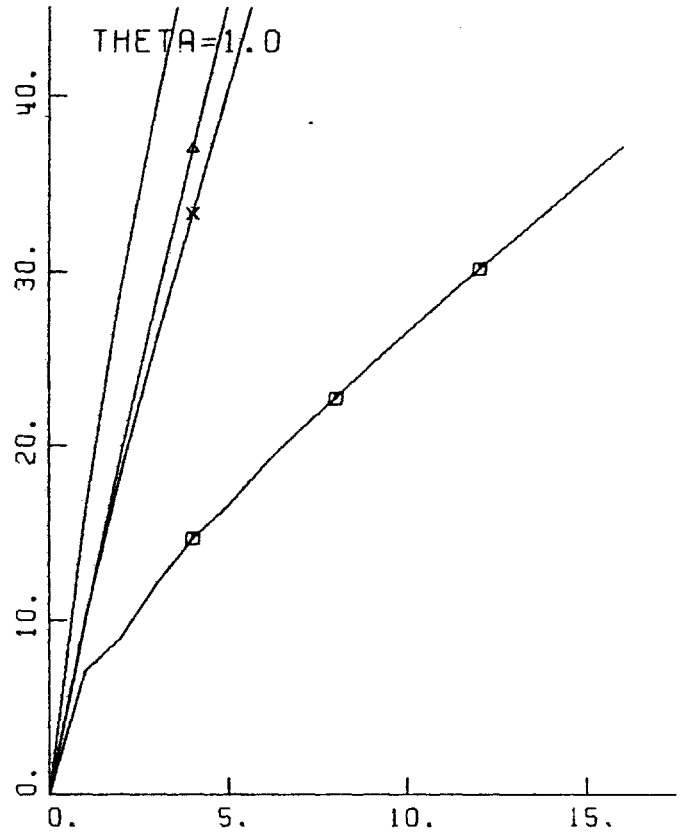
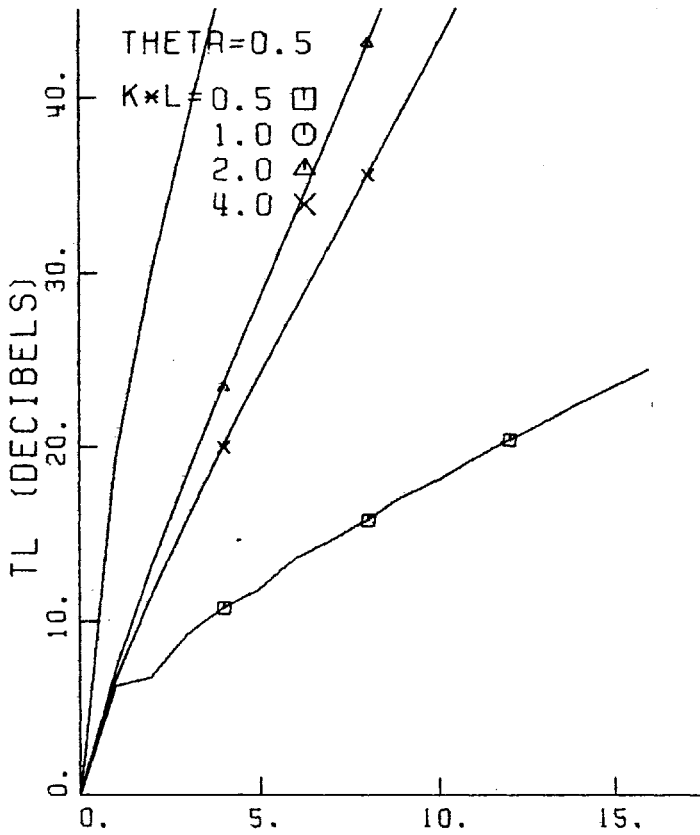




Figure A3.115

C-P

AREA RATIO=1.0 D/L=1.054

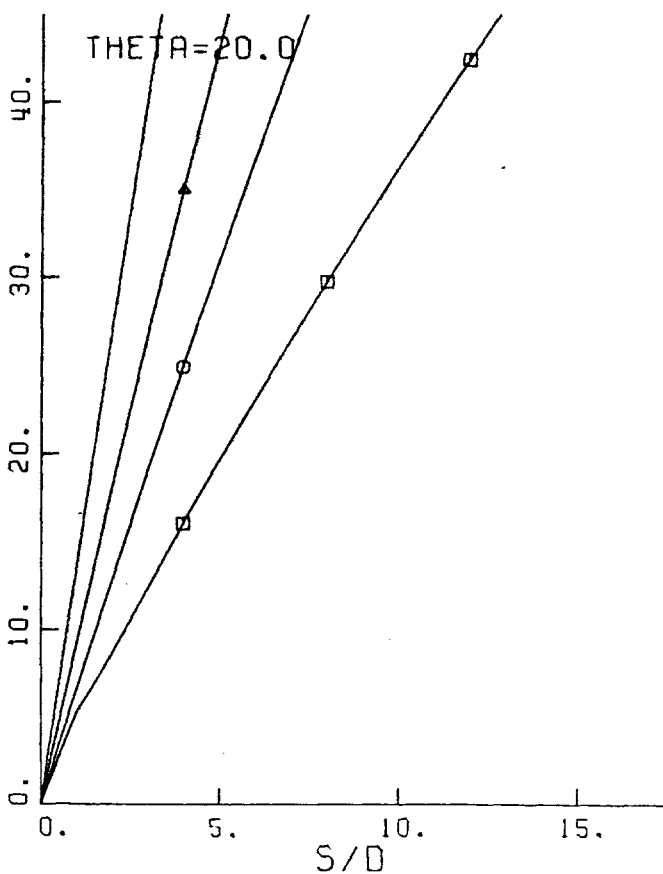
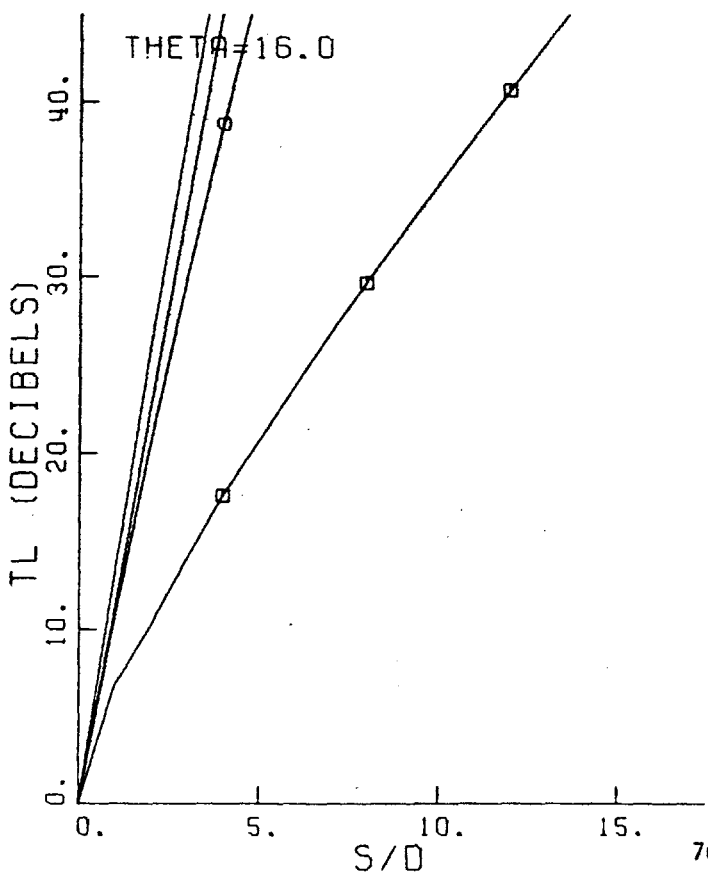
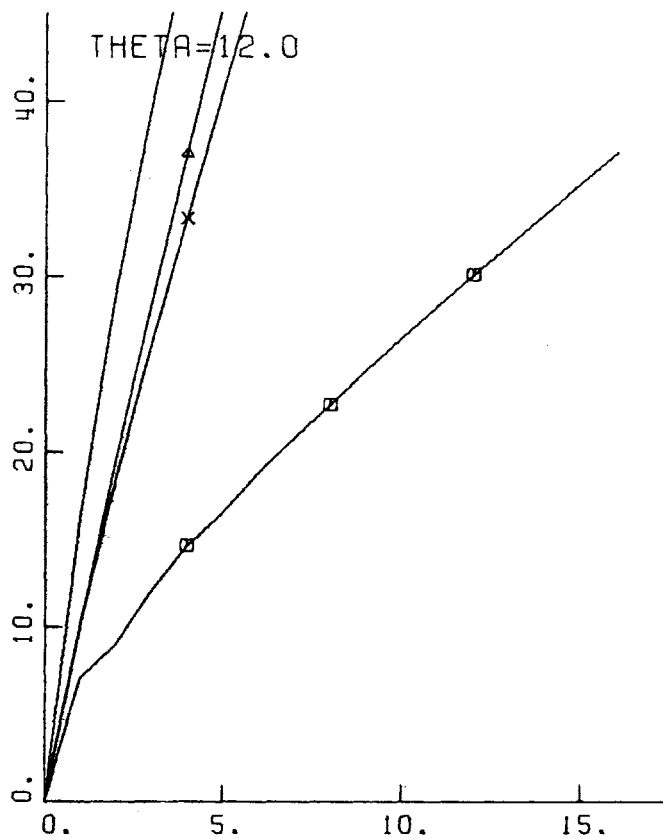
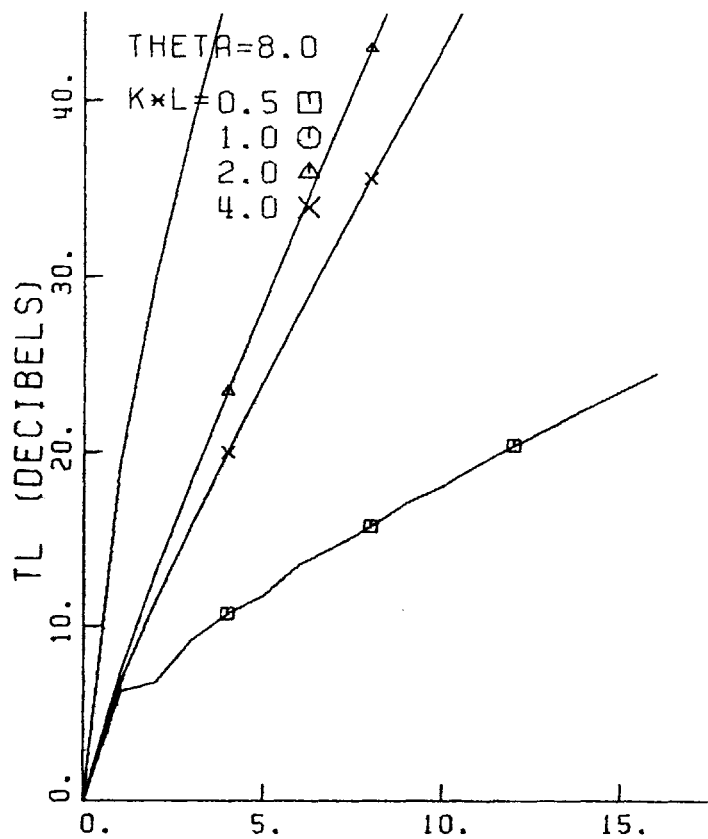


Figure A3.116

AREA RATIO=1.0 D/L=2.000

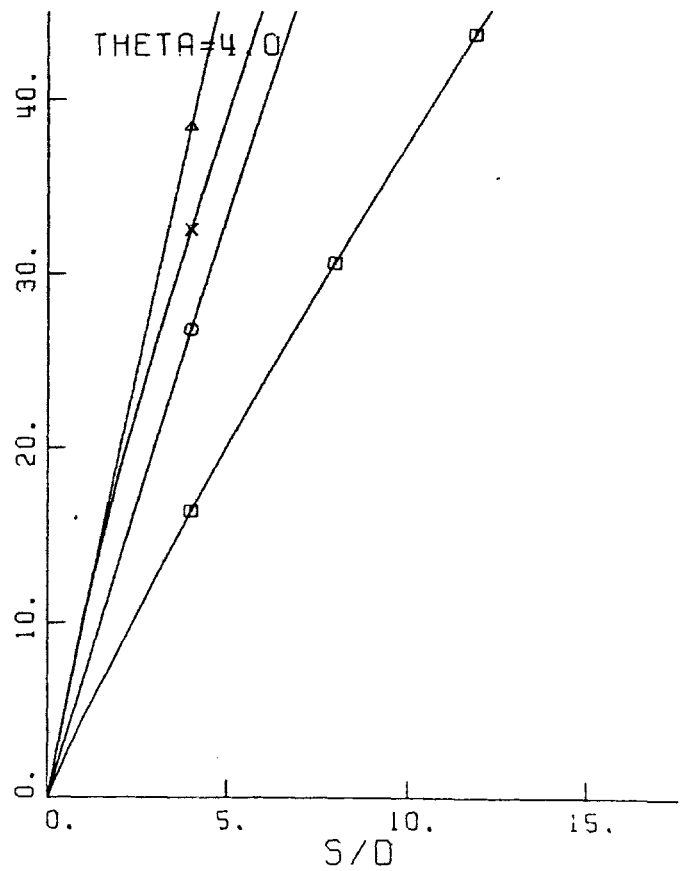
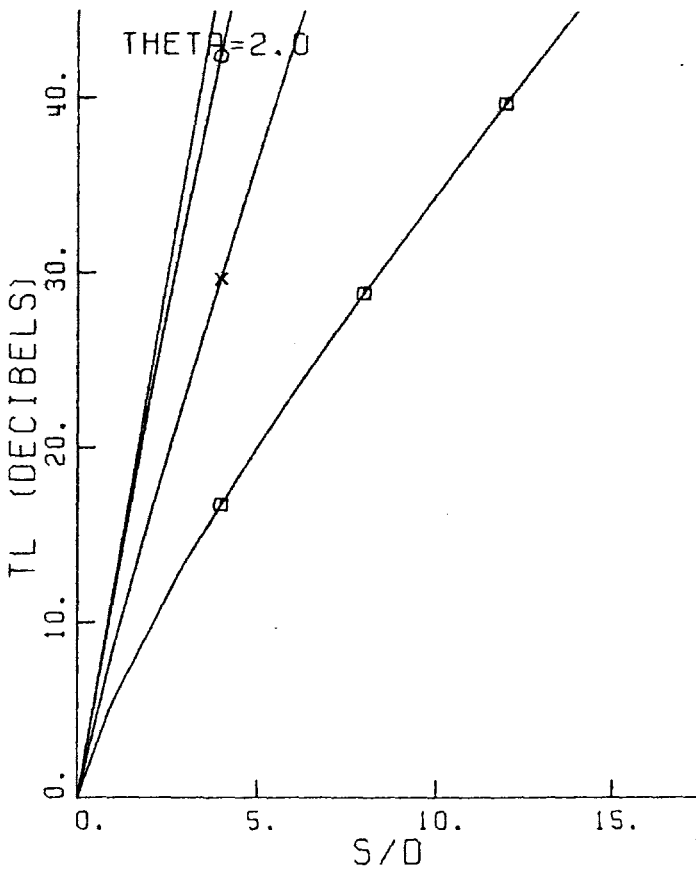
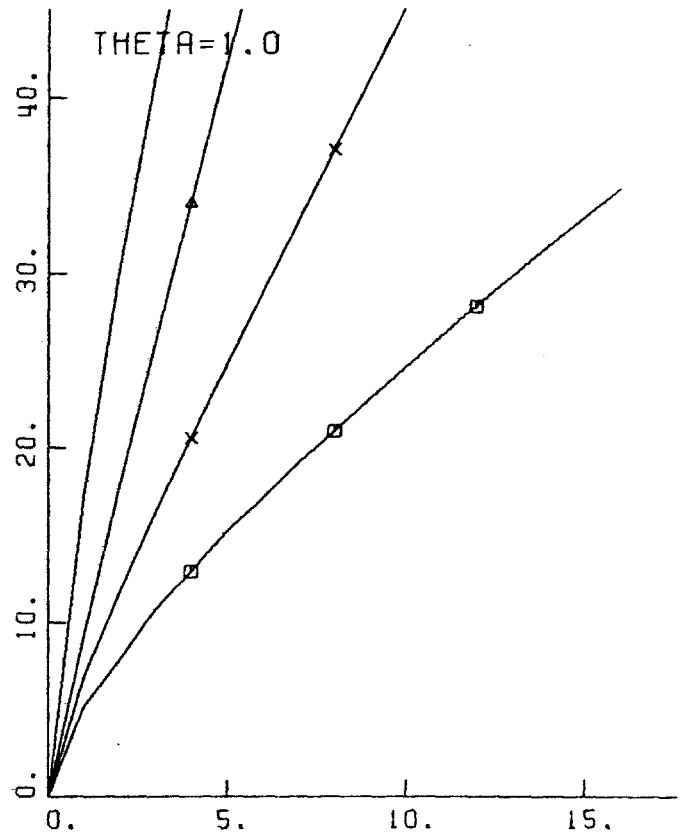
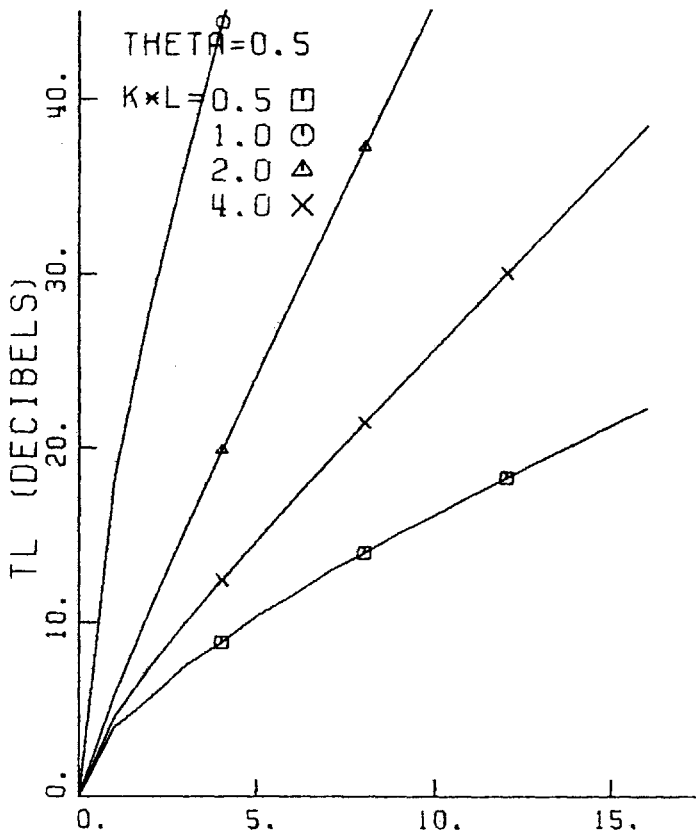


Figure A3.117

C-P

AREA RATIO=1.0 D/L=2.000

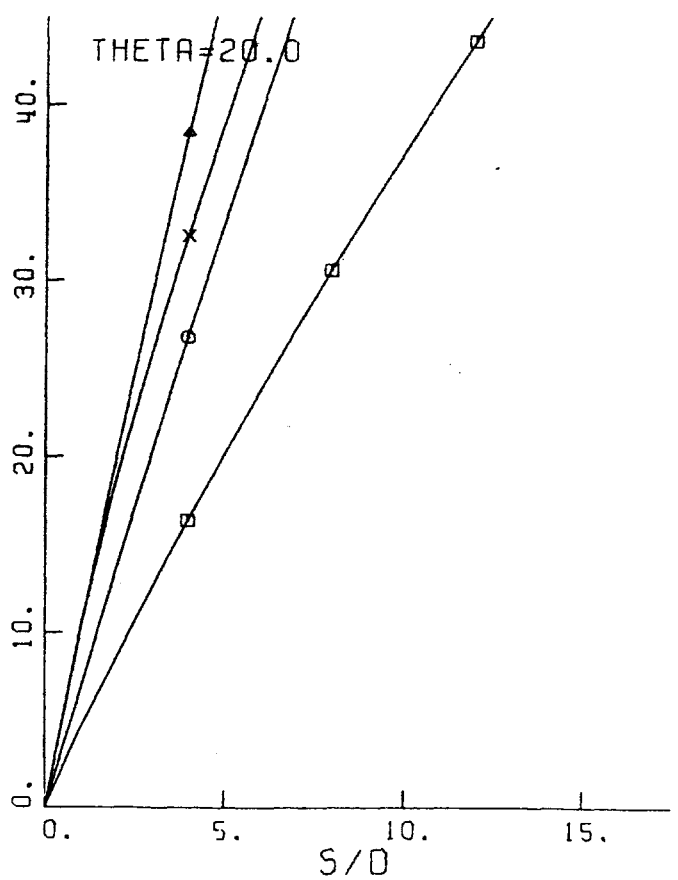
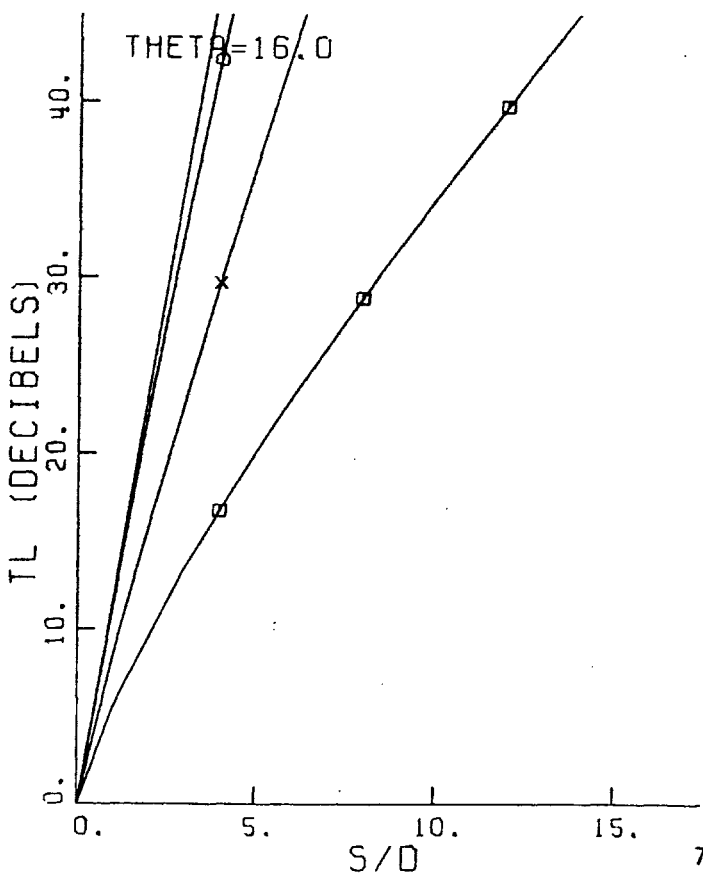
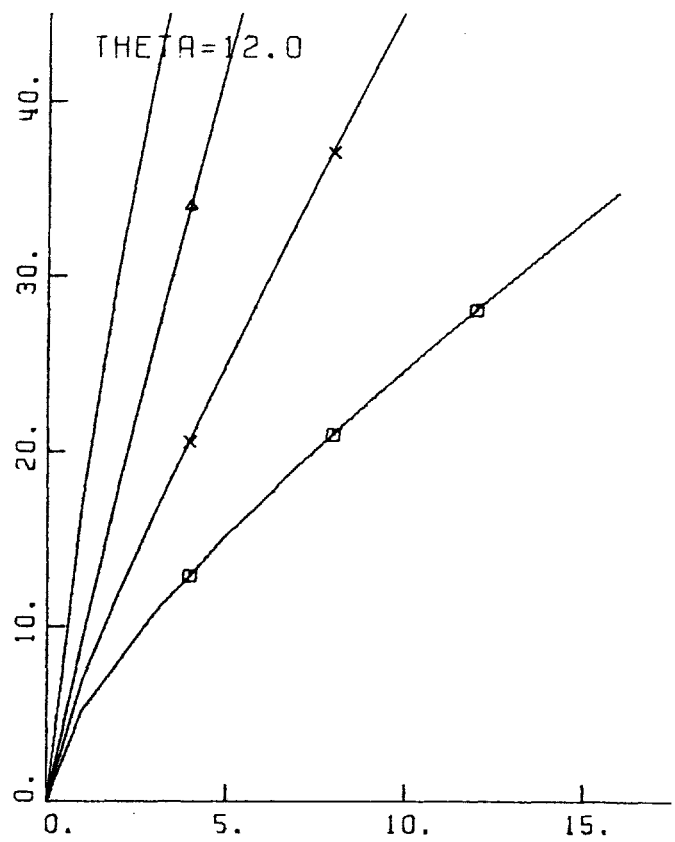
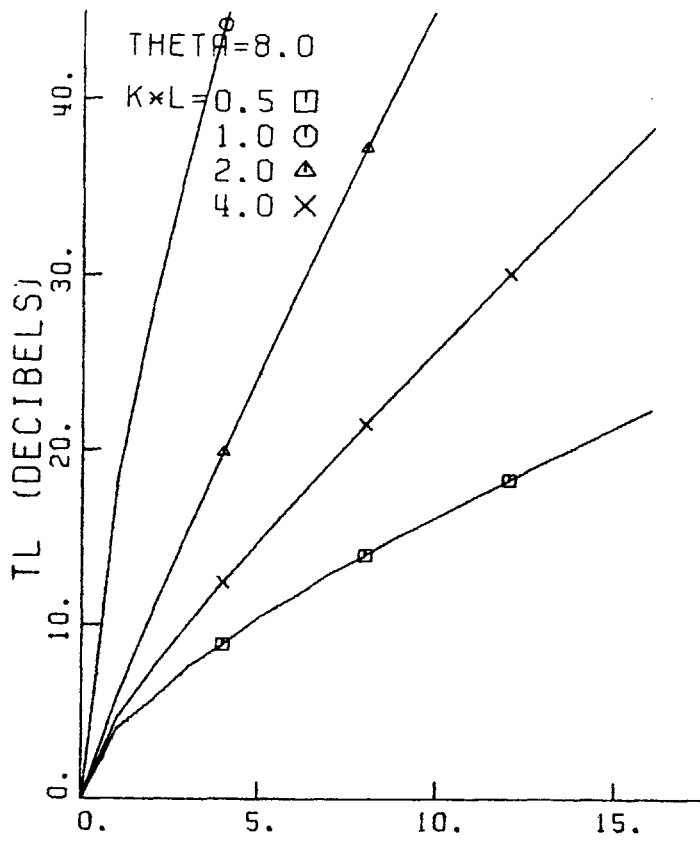


Figure A3.118

C-P

AREA RATIO=1.0     $D/L=4.828$

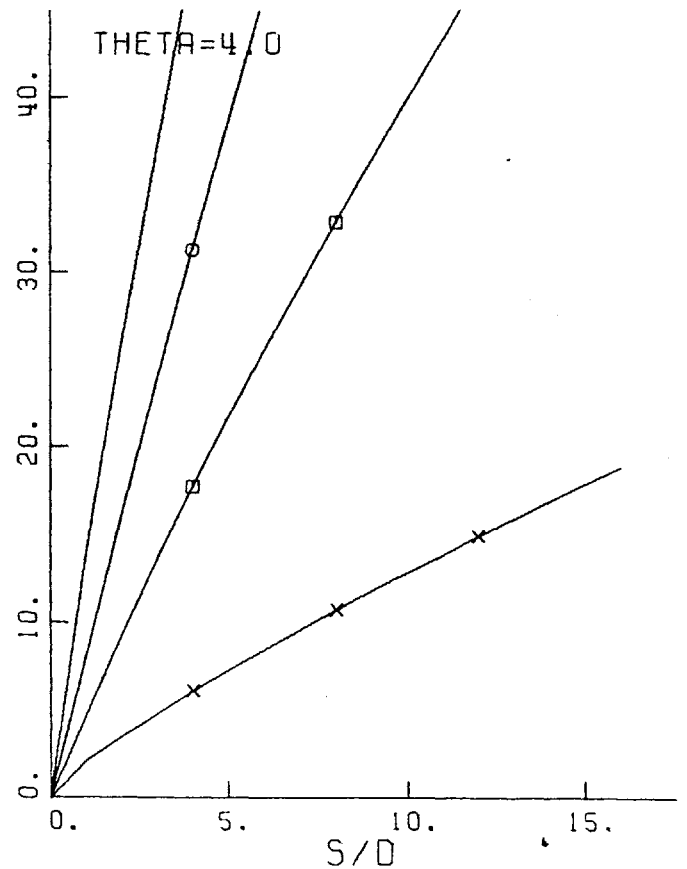
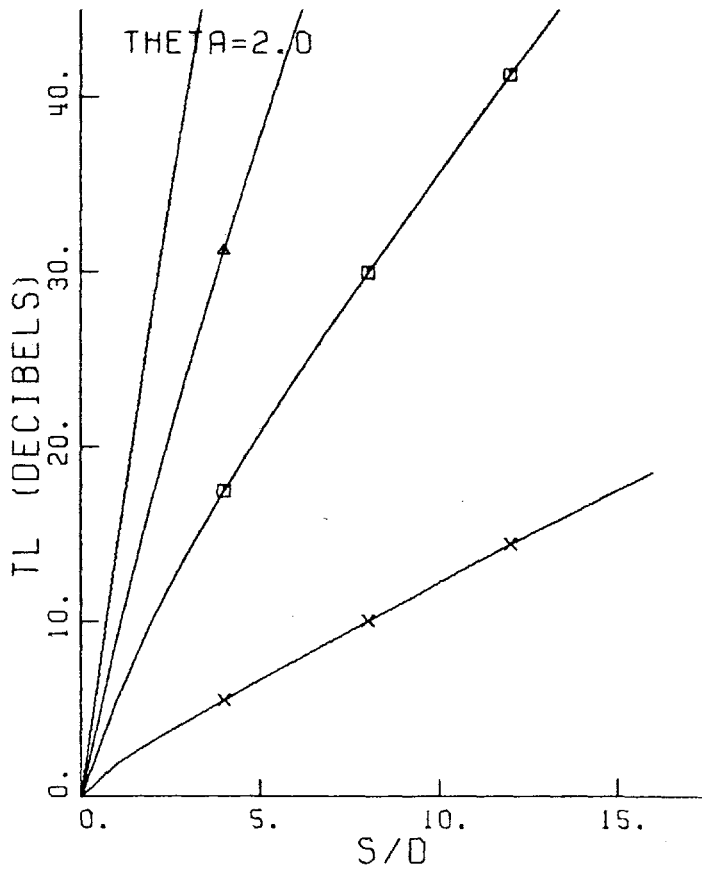
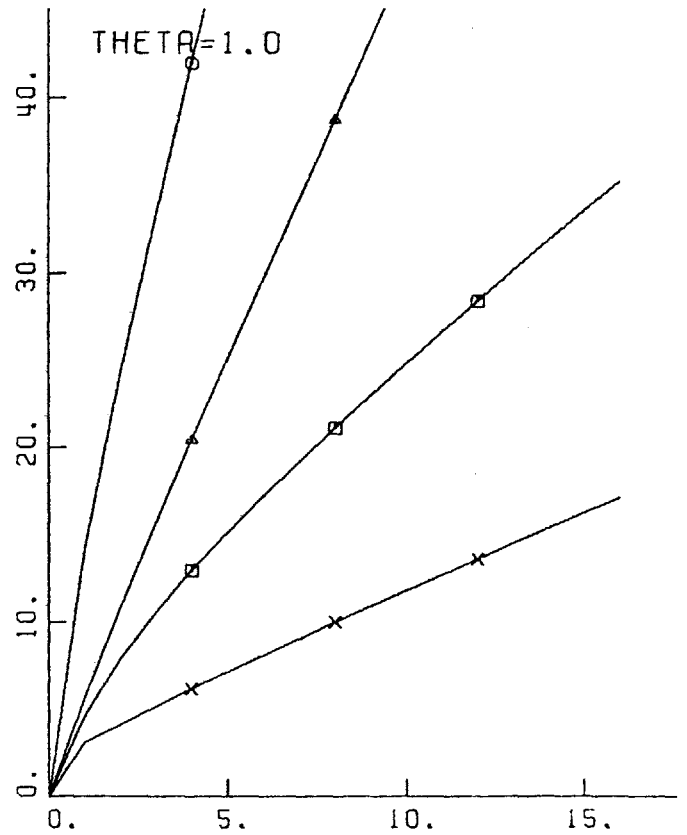
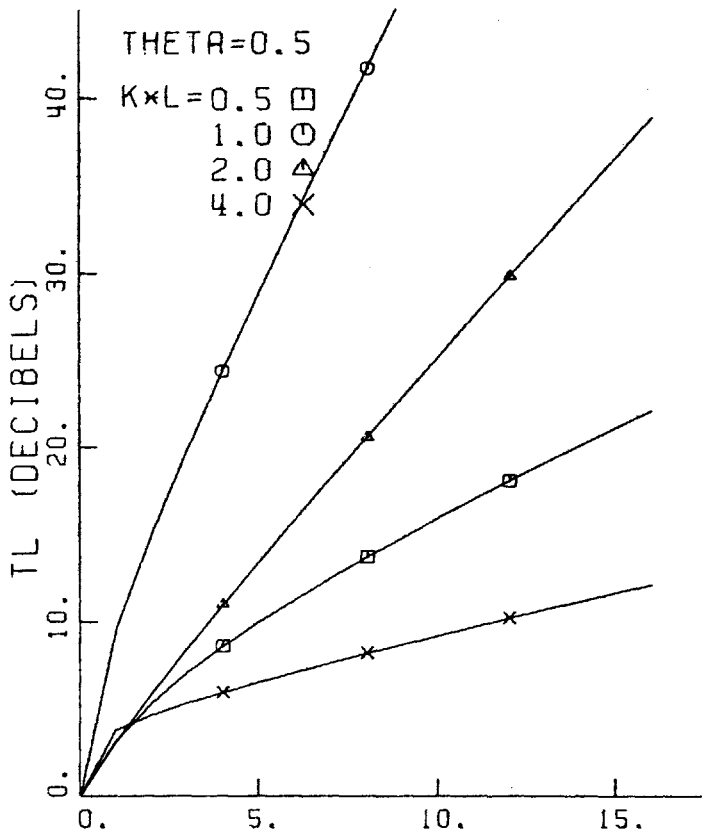


Figure A3.119

C-P

AREA RATIO=1.0 D/L=4.828

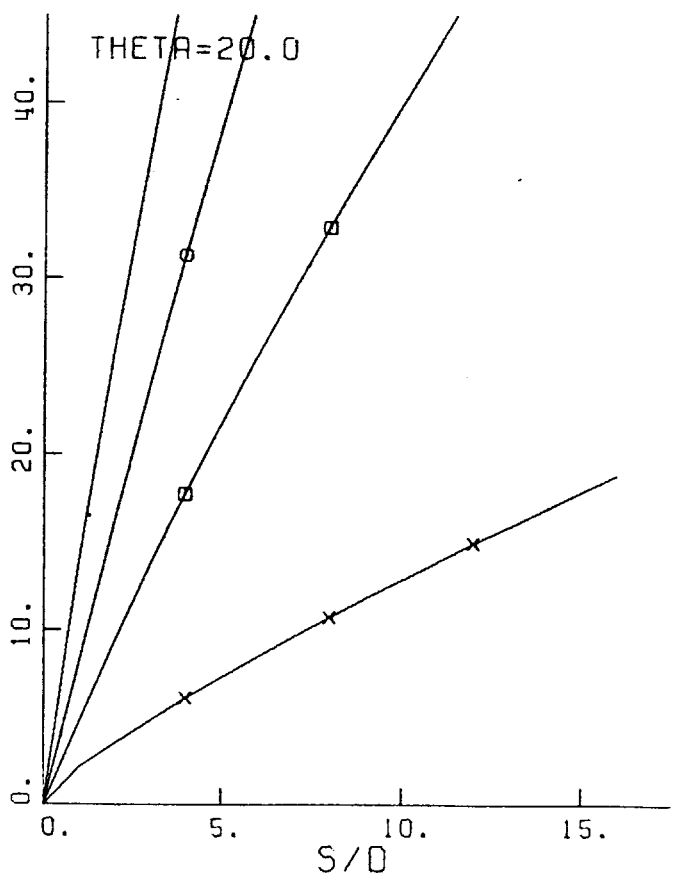
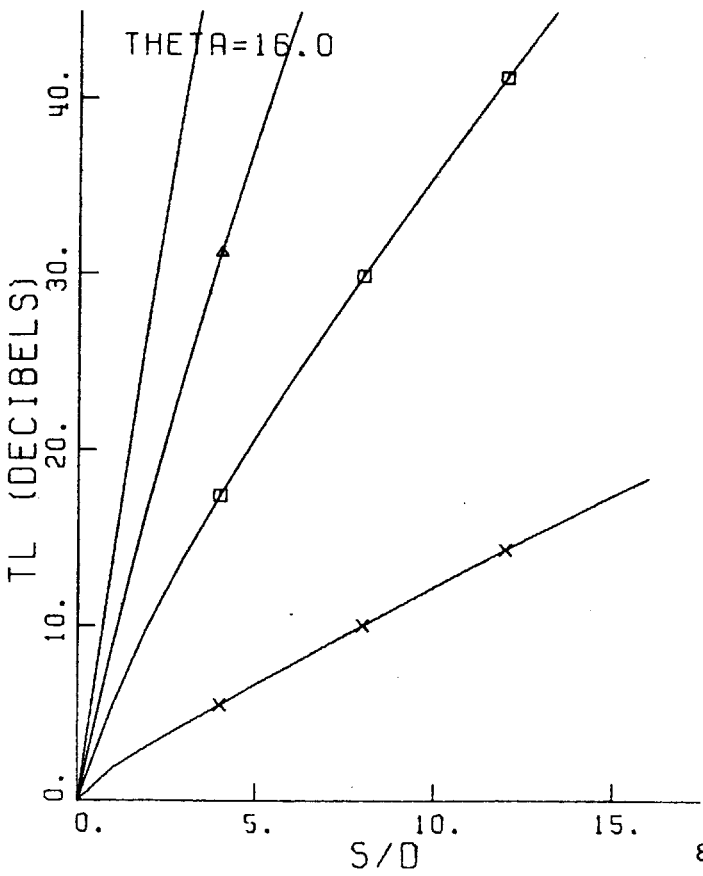
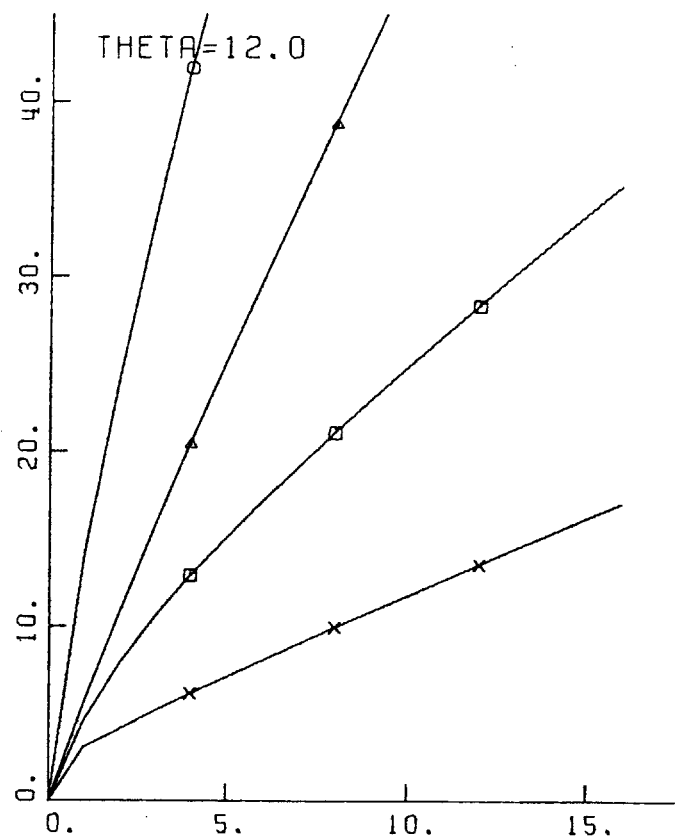
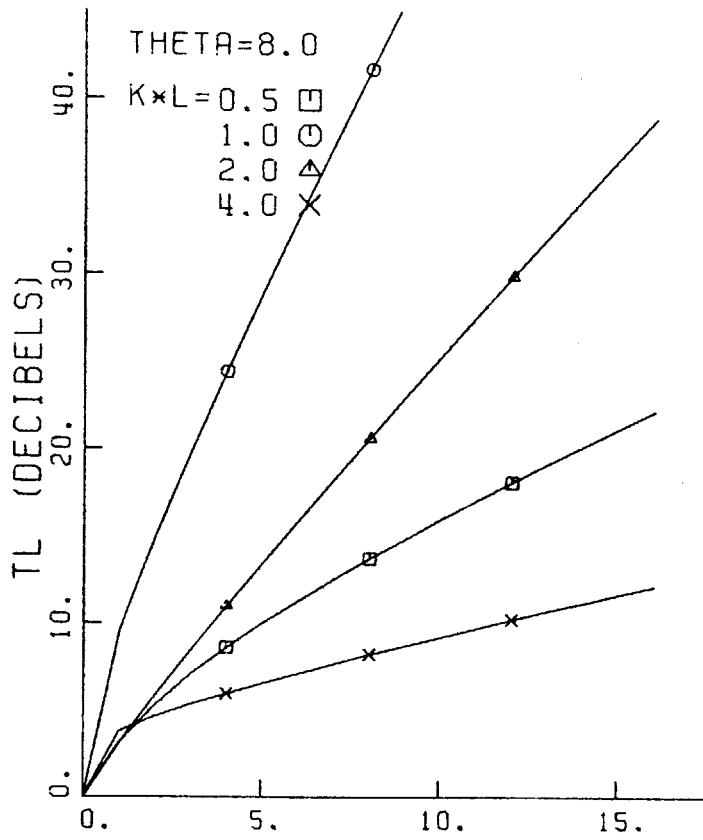


Figure A3.120

AREA RATIO=1.0 D/L=12.928

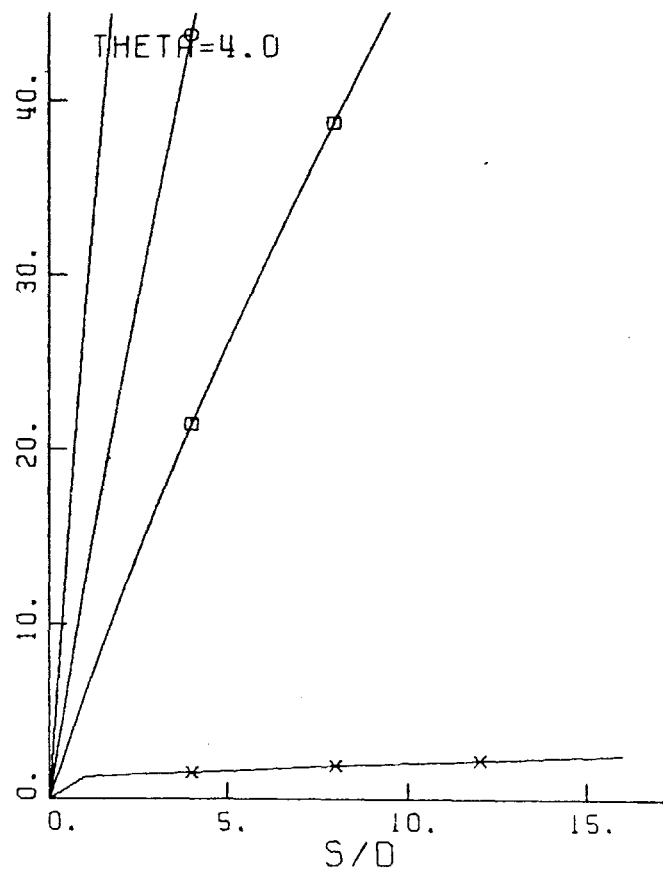
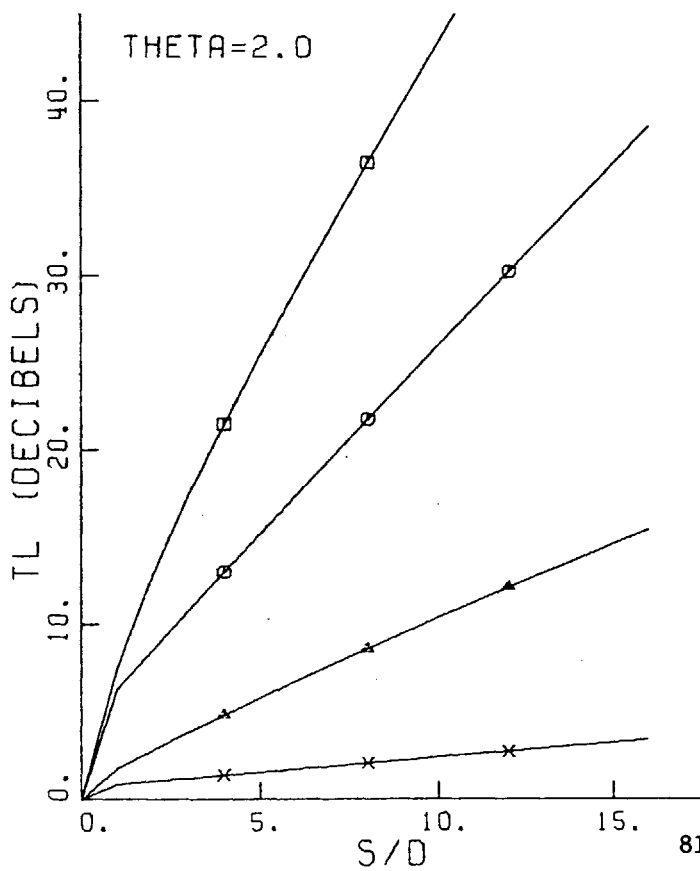
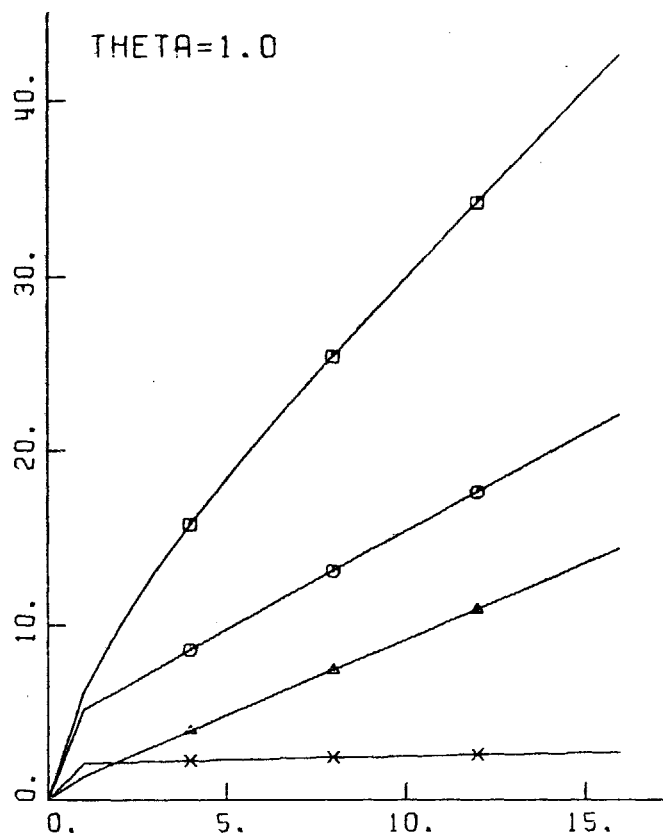
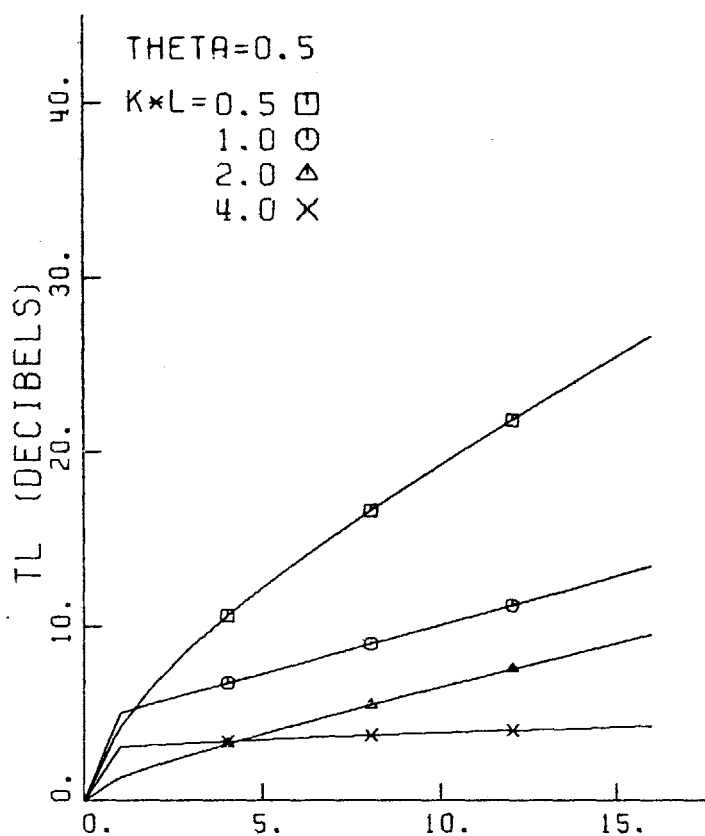
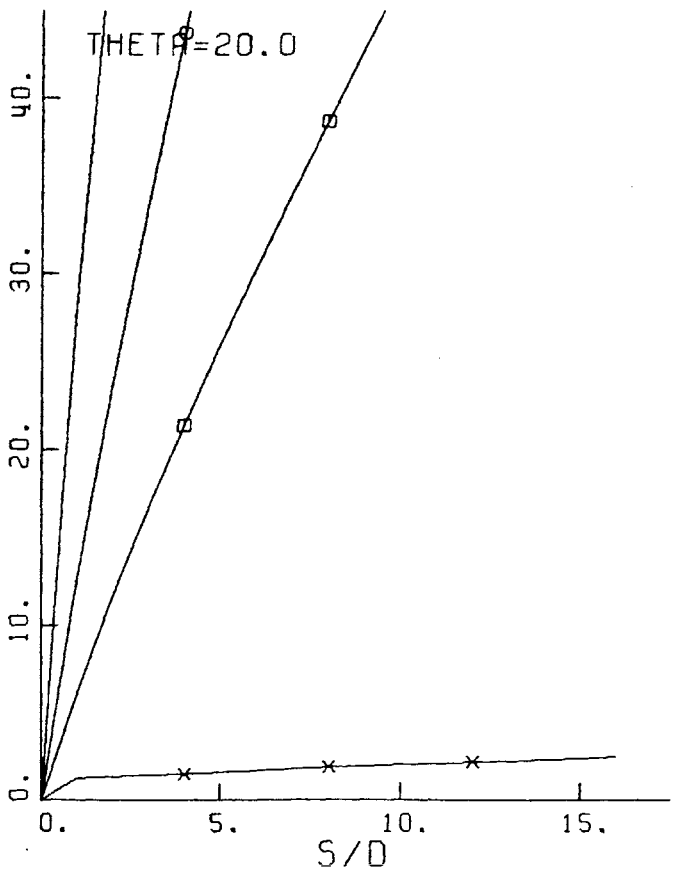
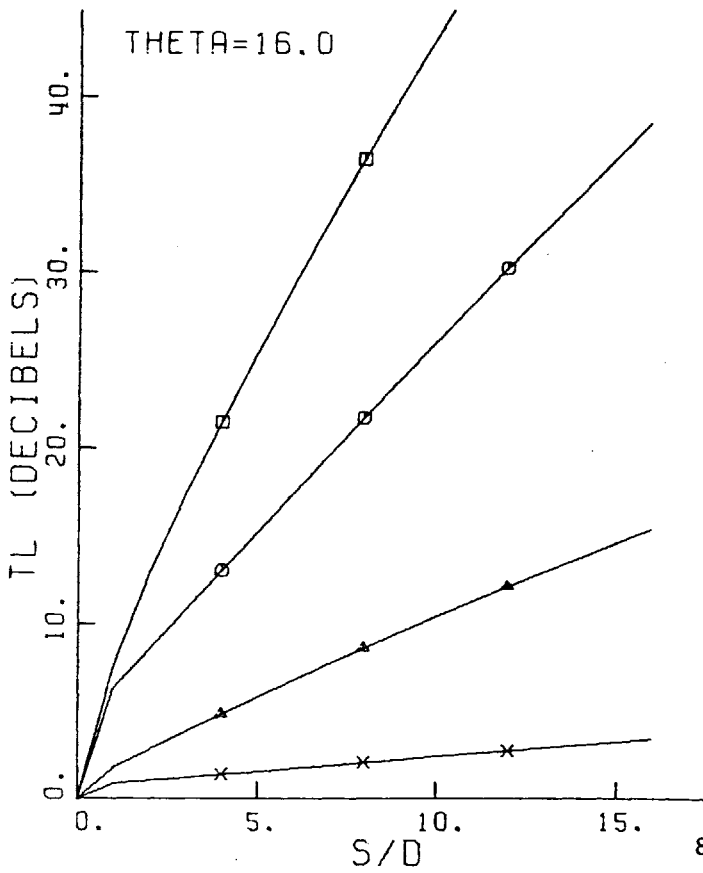
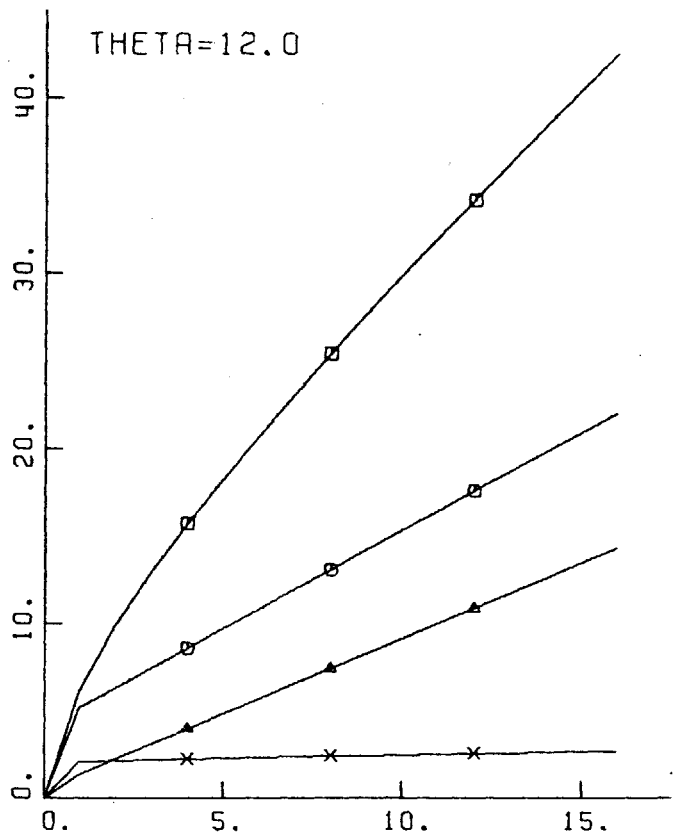
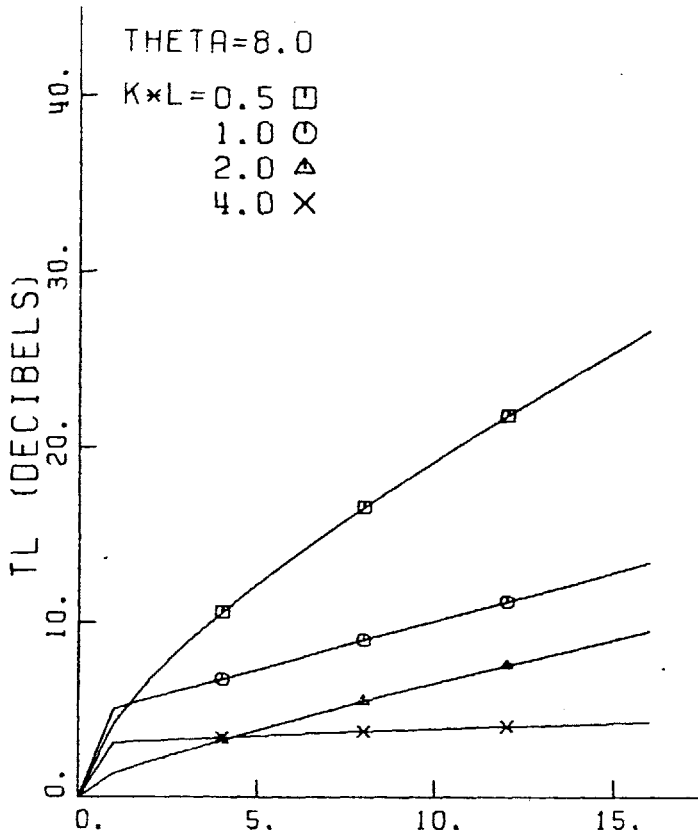


Figure A3.121

C-P

AREA RATIO=1.0 D/L=12.928



## A2. COMPUTER PROGRAMS

The computer program CCHOC, which obtains complex wave numbers in lined circular ducts, has been revised. In the new program (YCHO) the Hankel functions with complex arguments are used to obtain the exact boundary impedances.

During the preparation of this addendum we have developed a new subroutine (CMJYB) to compute the complex J- and Y-Bessel functions. This subroutine is superior to the M.I.T. Math. Library subroutines for the complex Bessel functions in accuracy and speed.

To accommodate CMJYB the subroutines RTCHO, BECHO\* and complex function FUN(Z)\* have been revised. The other subroutines remain unchanged.

\* These two subroutines were previously included in the listing of RTCHO.



C THIS PROGRAM COMPUTES COMPLEX WAVE VECTORS IN A LINED CIRCULAR  
 C DUCT USING COMPLEX EIGENVALUES OBTAINED BY THE SUBROUTINE RTCHO,  
 C THEN PERFORMS INTEGRATION TO OBTAIN OCTAVE BAND TRANSMISSION  
 C LOSS OF SOUND POWEPS.  
 C TO FIND EXACT WALL IMPEDANCE, COMPLEX HANKEL FUNCTIONS HAVE BEEN  
 C USED.  
 C THIS PROGRAM HAS BEEN CREATED BY Y.C.CHO AT M.I.T. GAS TURBINE  
 C LABORATORY IN 1974.

```

  IMPLICIT COMPLEX*8 (C)
  COMMON /RIMIT/ZIN(64,4)
  COMMON /QFNT/AAA, BBB
  COMMON /BYCF/DDY0, DDY1
  COMPLEX ANSW(4), W(4), ZIN, CKIA(2, 8, 4, 114)
  REAL TT(8) / .5, 1., 2., 4., 8., 12., 16., 20. /
  REAL ARATIO(4) / .125, .25, .5, .75 /
  REAL XRS(5) / 1., 2., 4., 8., 16. /, CABS, COS, COUNT(7)
  REAL V(7) / .0625, .125, .25, .5, 1., 2., 4. /
  REAL GN(113), GE(4), YO(17), YP(17), YN(17), ZO(17), ZP(17), ZN(17)
  REAL ATTO(7), ATTP(7), ATIN(7)
  REAL ATTD(2, 2, 8, 4, 5, 3, 7), YCOM(113), COTAN
  REAL RCTNC(4, 113)
  REAL*4 DDY0(30), DDY1(30)
  REAL*8 DYC(30), DY1(30), DK, DKN
  COMPLEX*16 ZV1, ZV2, ZZ01, ZZ11, ZY01, ZY11, ZZA, ZYA
  DIMENSION CJE(2), CYB(2)

```

```

100 FORMAT(8F10.5)
120 FORMAT(8F10.5)
110 FORMAT(8I10)
202 FORMAT(1X, 3I1, 1X, 7E17.7/)
300 FORMAT('1 SOUND ATTENUATION IN CIRCULAR SILENCER LINED WITH
1RESONATOR.'/)
301 FORMAT('1 SOUND ATTENUATION IN CIRCULAR SILENCER LINED WITH
1POROUS MATERIAL.'/)
601 FORMAT('1 SOUND ATTENUATION IN CIRCULAR DUCT LINED WITH
1RESONATOR.'/)
602 FORMAT('1 SOUND ATTENUATION IN CIRCULAR DUCT LINED WITH

```

YCH00001  
 YCH00002  
 YCH00003  
 YCH00004  
 YCH00005  
 YCH00006  
 YCH00007  
 YCH00008  
 YCH00009  
 YCH00010  
 YCH00011  
 YCH00012  
 YCH00013  
 YCH00014  
 YCH00015  
 YCH00016  
 YCH00017  
 YCH00018  
 YCH00019  
 YCH00020  
 YCH00021  
 YCH00022  
 YCH00023  
 YCH00024  
 YCH00025  
 YCH00026  
 YCH00027  
 YCH00028  
 YCH00029  
 YCH00030  
 YCH00031  
 YCH00032  
 YCH00033  
 YCH00034  
 YCH00035  
 YCH00036

1	POROUS MATERIAL.'/)	YCH00037
410	FORMAT(1X,4I2,I4,2F12.4,' NO ROOT...'/)	YCH00038
401	FORMAT(1X,2I2,I4,3F10.5,4E15.7//)	YCH00039
404	FORMAT(3X,3I3,I4,5E15.4/)	YCH00040
407	FORMAT(6X,7F17.8/)	YCH00041
408	FORMAT(1X,' TRANSMISSION COEFFICIENT COMPUTED ON OCTAVE BANDS'/	YCH00042
	11X,' CENTER FREQUENCIES ARE EQUAL TO'/)	YCH00043
C 409	FORMAT(2X,' GAMMA=',F4.2/)	YCH00044
415	FORMAT(10X,' T=',F5.2/)	YCH00045
411	FORMAT(20X,' AREA RATIO=',F5.3,' OR D/L=',F6.3/)	YCH00046
412	FORMAT(30X,' LENGTH OF LINING/D=',F5.2/)	YCH00047
501	FORMAT(3I1,I3,2X,6E12.5)	YCH00048
505	FORMAT(6I1,4X,7F10.4)	YCH00049
3031	FORMAT(1X,' NUMBER OF INCORRECT ROOTS =',I5/)	YCH00050
	READ(5,100) ((ZIN(L,I),I=1,4),L=1,64)	YCH00051
	READ(5,120) (GN(L),L=1,113)	YCH00052
	READ(5,110) NK,NGK,NI,NGI,NM,NGM,IJK1,IJK2	YCH00053
	GB(1)=1./(SQRT(8.)-1.)	YCH00054
	GB(2)=1.	YCH00055
	GB(3)=1./(SQRT(2.)-1.)	YCH00056
	GE(4)=1./(2./SQRT(3.)-1.)	YCH00057
	CEI=(0.,1.)	YCH00058
	ATMX=EXP(160.)	YCH00059
	PI=3.14159	YCH00060
	PV=2./PI	YCH00061
	ATMIV=1./ATMX	YCH00062
	ATDMX=10.*ALOG10(ATMX)	YCH00063
	DDY0(1)=1.D0	YCH00064
	DDY1(1)=1.25D0	YCH00065
	DY0(1)=1.D0	YCH00066
	DY1(1)=1.25D0	YCH00067
	DO 1010 K=2,30	YCH00068
	DK=K+1	YCH00069
	DKN=K	YCH00070
	DY0(K)=DY0(K-1)+1.D0/DKN	YCH00071
	DY1(K)=DY1(K-1)+5.D-1/DK	YCH00072

	DDY0(K)=DY0(K)/DY0(K-1)	YCH00073
	DDY1(K)=DY1(K)/DY1(K-1)	YCH00074
1010	CONTINUE	YCH00075
	DO 40 IJK=IJK1,IJK2	YCH00076
	NQQ=0	YCH00077
	IF(IJK.EQ.2) NGK=NGK+4	YCH00078
	DO 40 IJL=2,2	YCH00079
	IF(IJK.EQ.1.AND.IJL.EQ.1) WRITE(6,300)	YCH00080
	IF(IJK.EQ.1.AND.IJL.EQ.2) WRITE(6,601)	YCH00081
	IF(IJK.EQ.2.AND.IJL.EQ.1) WRITE(6,301)	YCH00082
	IF(IJK.EQ.2.AND.IJL.EQ.2) WRITE(6,602)	YCH00083
C	IF(IJK.EQ.1) NJ=1	YCH00084
C	IF(IJK.EQ.2) NJ=2	YCH00085
C	IF(IJK.EQ.1) NGJ=1	YCH00086
C	IF(IJK.EQ.2) NGJ=3	YCH00087
C	DO 50 J=NJ,NGJ	YCH00088
C	GAMJ=GAM(J)	YCH00089
	GAMJ=1.5	YCH00090
	DO 50 K=NK,NGK	YCH00091
	TTK=TT(K)	YCH00092
	DO 50 I=NI,NGI	YCH00093
	GBI=GB(I)	YCH00094
	DO 50 M=NM,NGM	YCH00095
	XRSM=XRS(M)	YCH00096
	DO 55 LS=1,113	YCH00097
	GNL=GN(LS)	YCH00098
	GNB=GNL*GPI	YCH00099
	GLB=GNL+GNB	YCH00100
	IF(M.NE.1) GO TO 33	YCH00101
	IF(IJK.EQ.2) GO TO 15	YCH00102
	IF(K.NE.NK) GO TO 666	YCH00103
	ERB=.0001	YCH00104
	CALL BFSJ(GNB,0,BJ01,ERB,IER)	YCH00105
	CALL PESJ(GNB,1,FJ11,ERB,IER)	YCH00106
	CALL BFSJ(GLB,1,BJ12,ERB,IER)	YCH00107
	CALL PESY(GNB,0,BYC1,IER)	YCH00108

```

CALL BESY (GNB, 1, BY11, IER)
CALL BESY (GLE, 1, BY12, IER)
RJNOR=BJ01*BY12-BY01*BJ12
RJDOM=PJ11*BY12-EY11*BJ12
RCTNC (I, LS) =RJNOR/RJDOM
666 CTTK=RCTNC (I, LS) + (0., 1.) *TTK
CAB=GNB/CTTK
GO TO 16
15 RTG=SQRT (.5*GAMJ)
SQRTN=SQRT (1. + (TTK/GNL) **2)
QPKR=RTG*SQRT (SQRTN+1.)
QPKI=RTG*SQRT (SQRTN-1.)
CQHR=CMPLX (QPKR, QPKI)
X1=GNB*QPKR
Y1=GNB*QPKI
X2=X1+QPKR*GNL
Y2=Y1+QPKI*GNL
RXY1=SQRT (X1*X1+Y1*Y1)
RXY2=SQRT (X2*X2+Y2*Y2)
CZ1=CMPLX (X1, Y1)
CZ2=CMPLX (X2, Y2)
CPL1=(1., 0.)
IF (RXY1.GE.7.) GO TO 7301
CALL CMJYES (CZ1, RXY1, CJB, CYB)
CHK011=CJB (1) +CEI*CYB (1)
CHK021=CJB (1) -CEI*CYB (1)
CHK111=CJB (2) +CEI*CYB (2)
CHK121=CJB (2) -CEI*CYB (2)
IF (CABS (CHK011) .LT. 1.E-50) GO TO 7201
CPU1=CHK111/CHK011
CPU2=CHK121/CHK011
CPL2=CHK021/CHK011
GO TO 7202
7201 CPU1=CHK111
CPU2=CHK121
CPL1=(0., 0.)

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YCH00109
YCH00110
YCH00111
YCH00112
YCH00113
YCH00114
YCH00115
YCH00116
YCH00117
YCH00118
YCH00119
YCH00120
YCH00121
YCH00122
YCH00123
YCH00124
YCH00125
YCH00126
YCH00127
YCH00128
YCH00129
YCH00130
YCH00131
YCH00132
YCH00133
YCH00134
YCH00135
YCH00136
YCH00137
YCH00138
YCH00139
YCH00140
YCH00141
YCH00142
YCH00143
YCH00144

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CPL2=CHK021
7202 IF(RXY2.GE.7.) GO TO 7401
CALL CMJYFS(CZ2,RXY2,CJB,CYB)
CPUL=(CJB(2)+CEI*CYB(2))/(CJB(2)-CEI*CYB(2))
GO TO 7501
7401 IF(Y2.GT.80.) GO TO 7402
KP2=RXY2+1.
IF(KP2.GE.11) KP2=11
ZV2=CZ2
CALL JYHSL(1,KP2,ZV2,ZZA,ZYA)
CFTAI=EXP(-2.*Y2)
CFTAR=CEI*COS(2.*X2)-SIN(2.*X2)
CZTA=ZZA
CYTA=ZYA
CPUL=CFTAI*CFTAR*(CZTA+CEI*CYTA)/(CZTA-CEI*CYTA)
GO TO 7501
7402 CPUL=(0.,0.)
GO TO 7501
7301 ZV2=CZ2
ZV1=CZ1
KP1=RXY1+1
KP2=RXY2+1
IF(KP1.GE.11) KP1=11
IF(KP2.GE.11) KP2=11
CALL JYHSL(0,KP1,ZV1,ZZ01,ZY01)
CALL JYHSL(1,KP1,ZV1,ZZ11,ZY11)
CZZ01=ZZ01
CZY01=ZY01
CZZ11=ZZ11
CZY11=ZY11
CPPF=CZZ01+CEI*CZY01
CPU1=-CEI*(CZZ11+CEI*CZY11)/CPPF
CPU2=-CEI*(CZZ11-CEI*CZY11)/CPPF
CPL2=-(CZZ01-CEI*CZY01)/CPPF
Y21=Y2-Y1
IF(Y21.GT.80.) GO TO 7302

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YCH00145
YCH00146
YCH00147
YCH00148
YCH00149
YCH00150
YCH00151
YCH00152
YCH00153
YCH00154
YCH00155
YCH00156
YCH00157
YCH00158
YCH00159
YCH00160
YCH00161
YCH00162
YCH00163
YCH00164
YCH00165
YCH00166
YCH00167
YCH00168
YCH00169
YCH00170
YCH00171
YCH00172
YCH00173
YCH00174
YCH00175
YCH00176
YCH00177
YCH00178
YCH00179
YCH00180

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X21=X2-X1
CALL JYHSL(1,KP2,ZV2,ZZA,ZYA)
CZZ2=ZZA
CZY2=ZYA
CFTAI=EXP(-2.*Y21)
CFTAR=COS(2.*X21)+CEI*SIN(2.*X21)
CPUL=CFTAI*CFTAR*(CZZ2+CEI*CZY2)/(CZZ2-CEI*CZY2)
GO TO 7501
7302 CPUL=(0.,0.)
7501 CTANM=CPU1-CPUL*CPU2
CTAND=CPL1-CPUL*CPL2
IF(CABS(CTAND).LT.1.E-50) GO TO 7502
CTAN=CTANM/CTAND
CAB=GNB*CTAN/CQHR
GO TO 16
7502 IF(CABS(CTANM).GT.1.E-30) GO TO 7503
CAB=1.E+20
GO TO 16
7503 WRITE(6,401) K,I,LS,TTK,GBI,GNL,CZ1,CZ2
CAB=1.1111
16 AAA=REAL(CAB)
BBB=AIMAG(CAB)
IF(BBB.EQ.0..AND.AAA.GT.1.E+4) GO TO 303
GO TO 351
303 AAA=10000.
ANSW(1)=CMPLX(2.40483,0.)
W(1)=CMPLX(0.,0.)
NQ7=1
TERMQ=GNB**2-2.40483**2
IF(TERMQ) 304,305,305
304 RFALK=0.
AIMAK=SQRT(-TERMQ)
GO TO 22
305 REALK=SQRT(TERMQ)
AIMAK=0.
GO TO 22

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YCH00181
YCH00182
YCH00183
YCH00184
YCH00185
YCH00186
YCH00187
YCH00188
YCH00189
YCH00190
YCH00191
YCH00192
YCH00193
YCH00194
YCH00195
YCH00196
YCH00197
YCH00198
YCH00199
YCH00200
YCH00201
YCH00202
YCH00203
YCH00204
YCH00205
YCH00206
YCH00207
YCH00208
YCH00209
YCH00210
YCH00211
YCH00212
YCH00213
YCH00214
YCH00215
YCH00216

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351	IF (ABS (AAA) .LE. 1.E-5) AAA=0.	YCH00217
	IF (ABS (BBB) .LE. 1.E-5) BBB=0.	YCH00218
	CALL RTCHO (NQ7, ANSW, W)	YCH00219
	IF (NQ7.EQ.0) GO TO 60	YCH00220
	XIRE=REAL (ANSW (1))	YCH00221
	XIIM=AIMAG (ANSW (1))	YCH00222
	CALL WAVEK (GNB, XIRE, XIIM, REALK, AIMAK)	YCH00223
22	CKIA (IJK, K, I, LS) =CMPLX (REALK, AIMAK)	YCH00224
	AW=CABS (W (1))	YCH00225
	IF (AW.LT..01) GO TO 33	YCH00226
	WRITE (6, 404) IJK, K, I, LS, AW, AAA, BBB, ANSW (1)	YCH00227
33	CYKE=CKIA (IJK, K, I, LS) *XRSM*2.	YCH00228
	IF (IJL.EQ.1) CKR=GBI*CKIA (IJK, K, I, LS) /GNL / (1.+GBI) **2	YCH00229
	IF (IJL.EQ.2) CKR=CKIA (IJK, K, I, LS) /GNB	YCH00230
	CKRV= (0., .5) * (CKR+1./CKR)	YCH00231
	AMCK=AIMAG (CYKE)	YCH00232
	IF (AMCK.GT.80.) GO TO 5	YCH00233
	CSUM=CCOS (CYKE) -CKRV*CSIN (CYKE)	YCH00234
	ASUM=CABS (CSUM)	YCH00235
	YCOM (LS) =1./ASUM**2*ATMX	YCH00236
	GO TO 55	YCH00237
5	IF (AMCK.GT.160.) GO TO 6	YCH00238
	YCOM (LS) =4.*EXP (-2.* (AMCK-80.)) /CABS (1.+CKRV) **2	YCH00239
	GO TO 55	YCH00240
6	YCOM (LS) =0.	YCH00241
	GO TO 55	YCH00242
60	WRITE (6, 410) NQ7, IJK, K, I, LS, AAA, BBB	YCH00243
	LSSS=LS-1	YCH00244
	CKIA (IJK, K, I, LS) =CKIA (IJK, K, I, LSSS)	YCH00245
	YCOM (LS) =YCOM (LSSS)	YCH00246
	NQQ=NQQ+1	YCH00247
	IF (NQQ.GT.20) GO TO 3030	YCH00248
55	CONTINUE	YCH00249
	CKIA (IJK, K, I, 114) = (0., 0.)	YCH00250
	DO 20 L=1, 7	YCH00251
	HI=SQRT (2.) *V (L)	YCH00252

H=.0625*HI	YCH00253
LM=16*(L-1)	YCH00254
DO 30 KL=1,17	YCH00255
KLM=KL+LM	YCH00256
YO(KL)=YCOM(KLM)/HI	YCH00257
AKL=FLOAT(KL-1)	YCH00258
YP(KL)=(HI+H*AKL)**2*YO(KL)	YCH00259
YN(KL)=YO(KL)/(HI+H*AKL)**2	YCH00260
30 CONTINUE	YCH00261
CALL QSF(H,YO,ZO,17)	YCH00262
IF(ZO(17).LT.ATMIV) GO TO 21	YCH00263
ATTD(IJK,IJL,K,I,M,1,L)=-10.*ALOG10(ZO(17))+ATDMX	YCH00264
GO TO 26	YCH00265
21 ATTD(IJK,IJL,K,I,M,1,L)=2.*ATDMX	YCH00266
26 CALL QSF(H,YP,ZP,17)	YCH00267
ATTP(L)=3.*ZP(17)/HI**2/7.	YCH00268
IF(ATTP(L).LT.ATMIV) GO TO 23	YCH00269
ATTD(IJK,IJL,K,I,M,2,L)=-10.*ALOG10(ATTP(L))+ATDMX	YCH00270
GO TO 24	YCH00271
23 ATTD(IJK,IJL,K,I,M,2,L)=2.*ATDMX	YCH00272
24 CALL QSF(H,YN,ZN,17)	YCH00273
ATTN(L)=2.*ZN(17)*HI**2	YCH00274
IF(ATTN(L).LT.ATMIV) GO TO 25	YCH00275
ATTD(IJK,IJL,K,I,M,3,L)=-10.*ALOG10(ATTN(L))+ATDMX	YCH00276
GO TO 20	YCH00277
25 ATTD(IJK,IJL,K,I,M,3,L)=2.*ATDMX	YCH00278
20 CONTINUE	YCH00279
50 CONTINUE	YCH00280
DO 54 LX=1,7	YCH00281
COUNT(LX)=2.*V(LX)	YCH00282
54 CONTINUE	YCH00283
WRITE(6,408)	YCH00284
WRITE(6,407) (COUNT(LX),LX=1,7)	YCH00285
C DO 56 JX=NJ,NGJ	YCH00286
C WRITE(6,409) GAM(JX)	YCH00287
DO 56 KX=NK,NGK	YCH00288



	KP=KX	YCH00289
	WRITE(6,415) TT(KX)	YCH00290
	DO 56 IX=NI,NGI	YCH00291
	TGB=2.*GE(IX)	YCH00292
	WRITE(6,411) ARATIO(IX),TGB	YCH00293
	DO 56 MX=NM,NGM	YCH00294
	WRITE(6,412) XRS(MX)	YCH00295
C	IF(IJK.EQ.1) JY=JX	YCH00296
C	IF(IJK.EQ.2) JY=JX-1	YCH00297
	WRITE(6,202) KP,IX,MX,(ATTD(IJK,IJL,KX,IX,MX,1,LX),LX=1,7)	YCH00298
	WRITE(6,202) KP,IX,MX,(ATTD(IJK,IJL,KX,IX,MX,2,LX),LX=1,7)	YCH00299
	WRITE(6,202) KP,IX,MX,(ATTD(IJK,IJL,KX,IX,MX,3,LX),LX=1,7)	YCH00300
56	CONTINUE	YCH00301
40	CONTINUE	YCH00302
	NGK=4	YCH00303
	DO 1001 IJKB=IJK1,IJK2	YCH00304
	IF(IJKB.EQ.2) NGK=NGK+4	YCH00305
	DO 1001 KB=NK,NGK	YCH00306
	KN=KB	YCH00307
	DO 1001 IB=1,4	YCH00308
	DO 1002 LAB=1,38	YCH00309
	LABI=3*(LAB-1)+1	YCH00310
	LABT=LABI+2	YCH00311
	WRITE(7,501) IJKB,KN,IB,LABI,(CKIA(IJKB,KB,IB,LSB),LSB=LABI,LAPT)	YCH00312
1002	CONTINUE	YCH00313
1001	CONTINUE	YCH00314
	NGK=4	YCH00315
	DO 2001 IJKD=IJK1,IJK2	YCH00316
	IF(IJKD.EQ.2) NGK=NGK+4	YCH00317
	DO 2001 IJLD=2,2	YCH00318
	DO 2001 NB=1,3	YCH00319
	DO 2001 KD=NK,NGK	YCH00320
	KM=KD	YCH00321
	DO 2001 ID=1,4	YCH00322
	DO 2001 MD=1,5	YCH00323
	WRITE(7,505) IJKD,IJLD,NB,KM,ID,MD,(ATTD(IJKD,IJLD,KD,ID,MD,NB,	YCH00324

```
1LXD),LXD=1,7)
2001 CONTINUE
3030 WRITE(6,3031) NQQ
STOP
END
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YCH00325
YCH00326
YCH00327
YCH00328
YCH00329
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```
      SUBROUTINE CMJYB(CZ,CJB,CYB)
C   CMJYB COMPUTES THE FIRST AND SECOND COMPLEX J- AND Y-BESSEL.
C   THIS PROGRAM HAS BEEN CREATED BY Y.C.CHO AT M.I.T. GAS TURBINE
C   LABORATORY IN 1974.
      COMPLEX*8 CZ,CJB(2),CYB(2)
      RXY=CABS(CZ)
      IF(RXY.GE.7.) GO TO 200
      CALL CMJYBS(CZ,RXY,CJB,CYB)
      GO TO 201
200 CALL CMJYBG(CZ,CJB,CYB)
201 RETURN
      END
```

```
CMJY0001
CMJY0002
CMJY0003
CMJY0004
CMJY0005
CMJY0006
CMJY0007
CMJY0008
CMJY0009
CMJY0010
CMJY0011
CMJY0012
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SUBROUTINE CMJYBS (CZ, RXY, CJB, CYB)
IMPLICIT COMPLEX*8 (C, Z)
COMMON/BYCF/DDY0, DDY1
DIMENSION ZX0 (30), CJB (2), CYB (2), DDY0 (30), DDY1 (30)
DPI=3.14159
DPV=2./DPI
DGM=.577216
ZHF=CZ/2.
ZLG=CLOG (ZHF) +DGM
NL=30
IF (RXY.LT.2.) NL=10
IF (RXY.LT..2) NL=5
IF (RXY.LT..01) NL=3
IF (RXY.LT.1.E-5) NL=2
IF (RXY.LT.1.E-20) GO TO 100
ZZ0=1.
ZZ1=1.
ZY1=1.
ZY0=1.
NLS=NL+1
ZT=-.25*CZ*CZ
DO 50 K=1, NL
NS=NLS-K
DK0=NS*NS
DK1=NS*(NS+1)
ZTD0=ZI/DK0
ZZ0=1.00+ZZ0*ZTD0
ZTD1=ZT/DK1
ZZ1=1.00+ZZ1*ZTD1
ZY0=1.00+ZY0*ZTD0*DDY0 (NS)
ZY1=1.00+ZY1*ZTD1*DDY1 (NS)
50 CONTINUE
CJB (1) =ZZ0
ZJB1=ZZ1*ZHF
CJB (2) =ZJB1
CYB (1) =DPV*(ZLG*ZZ0-ZY0+1.00)

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```

CJYS0001
CJYS0002
CJYS0003
CJYS0004
CJYS0005
CJYS0006
CJYS0007
CJYS0008
CJYS0009
CJYS0010
CJYS0011
CJYS0012
CJYS0013
CJYS0014
CJYS0015
CJYS0016
CJYS0017
CJYS0018
CJYS0019
CJYS0020
CJYS0021
CJYS0022
CJYS0023
CJYS0024
CJYS0025
CJYS0026
CJYS0027
CJYS0028
CJYS0029
CJYS0030
CJYS0031
CJYS0032
CJYS0033
CJYS0034
CJYS0035
CJYS0036

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```
CYB(2) = DPV * (ZLG * ZJB1 - ZHF * (ZY1 - .5) - 1. / CZ)
GO TO 2
100 CJB(1) = (1., 0.)
    CJB(2) = .5 * CZ
    CYB(1) = DPV * ZLG
    CYB(2) = -DPV / CZ
2 RETURN
END
```

```
CJYS0037
CJYS0038
CJYS0039
CJYS0040
CJYS0041
CJYS0042
CJYS0043
CJYS0044
```

	SUBROUTINE CMJYBG(CZ,CJB,CYB)	CJYG0001
C	IF ABS(DY) IS GREATER THAN 50.,EXP(-ABS(DY))*CJB AND CYB ARE RETURNED	CJYG0002
	IMPLICIT REAL*8 (D),COMPLEX*8 (C),COMPLEX*16 (Z)	CJYG0003
	REAL*8 DPHR(2),DCSR(2),DSNR(2),DOSR(2),DOSI(2),DINR(2),DINI(2)	CJYG0004
	REAL*8 DRZA(2),DRYA(2),DIZA(2),DIYA(2),DRW(2),DIW(2)	CJYG0005
	REAL*8 DJR(2),DJI(2)	CJYG0006
	REAL*8 DRV(2),DIV(2),DVR(2),DYI(2)	CJYG0007
	COMPLEX*16 DCMLX	CJYG0008
	DIMENSION CJB(2),CYB(2)	CJYG0009
	DPI=3.14159265359D0	CJYG0010
	DX=REAL(CZ)	CJYG0011
	DY=AIMAG(CZ)	CJYG0012
	DXY=DSQRT(DX*DX+DY*DY)	CJYG0013
	ZV=DCMLX(DX,DY)	CJYG0014
	DXS=DX/DXY	CJYG0015
	DQR=DSQRT(1.D0+DXS)	CJYG0016
	DQI=-DSQRT(1.D0-DXS)	CJYG0017
	DAPT=DSQRT(1.D0/DPI)/DSQRT(DXY)	CJYG0018
	IF(DY.GT.5.D+1) GO TO 20	CJYG0019
	IF(DY.LT.-5.D+1) GO TO 21	CJYG0020
	DXPP=DEXP(DY)	CJYG0021
	DXPN=1./DXPP	CJYG0022
	GO TO 30	CJYG0023
20	DXPP=1.D0	CJYG0024
	DXPN=0.D0	CJYG0025
	GO TO 30	CJYG0026
21	DXPP=0.D0	CJYG0027
	DXPN=1.D0	CJYG0028
30	DCSH=5.D-1*(DXPP+DXPN)	CJYG0029
	DSNH=5.D-1*(DXPP-DXPN)	CJYG0030
	KP=DXY+1.	CJYG0031
	IF(KP.GE.11) KP=11	CJYG0032
	DO 10 II=1,2	CJYG0033
	DII=2.5D-1	CJYG0034
	IF(II.EQ.2) DII=7.5D-1	CJYG0035
	DPHR(II)=DX-DII*DPI	CJYG0036

DCSR (II) =DCOS (DPHR (II) )	CJYG0037
DSNR (II) =DSIN (DPHR (II) )	CJYG0038
DOSR (II) =DCSR (II) *DCSH	CJYG0039
DOSI (II) =-DSNR (II) *DSNH	CJYG0040
DINR (II) =DSNR (II) *DCSH	CJYG0041
DINI (II) =DCSR (II) *DSNH	CJYG0042
NKU=II- 1	CJYG0043
CALL JYHSL (NKU,KP,ZV,ZZA,ZYA)	CJYG0044
DRZA (II) =DREAL (ZZA)	CJYG0045
DIZA (II) =DIMAG (ZZA)	CJYG0046
DRYA (II) =DREAL (ZYA)	CJYG0047
DIYA (II) =DIMAG (ZYA)	CJYG0048
DRW (II) =DRZA (II) *DOSR (II) -DIZA (II) *DOSI (II) -DRYA (II) *DINR (II) +	CJYG0049
1 DIYA (II) *DINI (II)	CJYG0050
DIW (II) =DRZA (II) *DOSI (II) +DIZA (II) *DOSR (II) -DRYA (II) *DINI (II) -	CJYG0051
1 DIYA (II) *DINR (II)	CJYG0052
DJR (II) =DAPT* (DQR*DRW (II) -DQI*DIW (II) )	CJYG0053
DJI (II) =DAPT* (DQR*DIW (II) +DQI*DRW (II) )	CJYG0054
DRV (II) =DRZA (II) *DINR (II) -DIZA (II) *DINI (II) +DRYA (II) *DOSR (II) -	CJYG0055
1 DIYA (II) *DOSI (II)	CJYG0056
DIV (II) =DRZA (II) *DINI (II) +DIZA (II) *DINR (II) +DRYA (II) *DOSI (II) +	CJYG0057
1 DIYA (II) *DOSR (II)	CJYG0058
DYR (II) =DAPT* (DQR*DRV (II) -DQI*DIV (II) )	CJYG0059
DYI (II) =DAPT* (DQR*DIV (II) +DQI*DRV (II) )	CJYG0060
CJB (II) =DCMPLX (DJR (II) ,DJI (II) )	CJYG0061
CYB (II) =DCMPLX (DYR (II) ,DYI (II) )	CJYG0062
10 CONTINUE	CJYG0063
RETURN	CJYG0064
END	CJYG0065

```

SUBROUTINE JYHSL(N,KP,ZX,ZZTA,ZYTA)
C  JYHSL OBTAINS FACTOR OF A COMPLEX BESSEL FUNCTION FOR A LARGE ARG.
  IMPLICIT REAL*8 (D),COMPLEX*16 (Z)
  ZT=1.5625D-2/ZX/ZX
  DN4=4*N*N
  ZZTM=1.D0
  ZYTM=1.D0
  IF(N.EQ.1) KP=KP+1
  IF(KP.LE.2) KP=2
  KPS=KP-1
  DO 10 J=1,KPS
  DJ4=4*(KP-J)
  DJ2=2*(KP-J)
  DNJ41=DN4-(DJ4-1.D0)*(DJ4-1.D0)
  DNJ43=DN4-(DJ4-3.D0)*(DJ4-3.D0)
  DJ21=DJ2*(DJ2-1.D0)
  ZFTZ=DNJ41*DNJ43/DJ21
  ZZTM=1.D0-ZZTM*ZFTZ*ZT
  DNJ45=DN4-(DJ4+1.D0)*(DJ4+1.D0)
  DJ22=DJ2*(DJ2+1.D0)
  ZFTY=DNJ41*DNJ45/DJ22
  ZYTM=1.D0-ZYTM*ZFTY*ZT
10 CONTINUE
  ZZTA=ZZTM
  ZYTA=(DN4-1.D0)*1.25D-1/ZX*ZYTM
  RETURN
  END

```

```

JYSL0001
JYSL0002
JYSL0003
JYSL0004
JYSL0005
JYSL0006
JYSL0007
JYSL0008
JYSL0009
JYSL0010
JYSL0011
JYSL0012
JYSL0013
JYSL0014
JYSL0015
JYSL0016
JYSL0017
JYSL0018
JYSL0019
JYSL0020
JYSL0021
JYSL0022
JYSL0023
JYSL0024
JYSL0025
JYSL0026
JYSL0027

```



```

SUBROUTINE RTCHO(NQ7,ANSW,W)
C SUBROUTINE RCHO OBTAINS FUNDAMENTAL EIGENVALUES FOR WAVES IN A
C LINED CIRCULAR DUCT. IN OTHER WORD, IT OBTAINS FIRST ROOTS
C OF THE EQUATION,  $X*J_1(X)/J_0(X)=\text{CMPLX}(AAA,BBB)$ , WHERE  $J_0(X)$ 
C AND  $J_1(X)$  ARE BESSEL FUNCTIONS OF THE ORDERS OF ZERO AND ONE
C WITH COMPLEX ARGUMENTS.
C RTCHO CALLS BECHO AND YSQNK9. BECHO CALLS CMJYB AND SSP
C SUBROUTINES FOR REAL BESSEL FUCTIONS. YSQNK9 IS THE
C SUBROUTINE REVISED FORM M.I.T. MATH. LIBRARY SUBROUTINE.
C IN CALLING PROGRAM, COMMON STATEMENT SHOULD BE MADE TO SUPLY VALUES
C OF AAA AND BBB, AND ZIN(64,4).
      IMPLICIT COMPLEX*8 (C)
      COMPLEX*8 Z(4),ERROR,ANSW(4),RETErr,FUN,W(4),CMPLX
      COMPLEX*8 CJB(2),CYB(2)
      COMPLEX*8 ZIN,ZAB
      COMMON /RIMIT/ZIN(64,4)
      COMMON /QFNT/AAA,BBB
      REAL*4 JR0,J10,JR1,J11,CABS,COS
      EXTERNAL FUN,FCT,FCTI
91 FORMAT(1X,' ROOT IS NOT ACCURATE')
      AAQ=AAA**2
      BEQ=BBB**2
      ABQ=AAQ+BEQ
      IF(ABQ.GT.4.) GO TO 44
      CAB=CMPLX(AAA,BBB)
      CAFDP=CAB+(2.,0.)
      CABFR=CAB+(4.,0.)
      CRDF=CSQRT(CABDP**2-CABFR*CAF)
      CX=(2.,0.)*(CABDP-CRDF)/CABFR
      IF(CABS(CX).GE.1.) GO TO 44
      CZT=(2.,0.)*CSQRT(CX)
      IF(AIMAG(CZT).GT.0.) CZT=-CZT
      DO 8601 LSD=1,20
      XPT=REAL(CZT)
      YPT=AIMAG(CZT)
      CALL BECHO(XPT,YPT,ART,BIT,GJR0,GJ10,GJR1,GJ11)

```

```

RTCH0001
RTCH0002
RTCH0003
RTCH0004
RTCH0005
RTCH0006
RTCH0007
RTCH0008
RTCH0009
RTCH0010
RTCH0011
RCHO0020 RTCH0012
RCHO0030 RTCH0013
RTCH0014
RCHO0040 RTCH0015
RTCH0016
RTCH0017
RTCH0018
RCHO0070 RTCH0019
RCHO0080 RTCH0020
RCHO0090 RTCH0021
RCHO0100 RTCH0022
RCHO0110 RTCH0023
RCHO0120 RTCH0024
RCHO0130 RTCH0025
RCHO0140 RTCH0026
RCHO0150 RTCH0027
RCHO0160 RTCH0028
RCHO0170 RTCH0029
RCHO0180 RTCH0030
RCHO0190 RTCH0031
RCHO0200 RTCH0032
RCHO0210 RTCH0033
RCHO0220 RTCH0034
RCHO0230 RTCH0035
RCHO0240 RTCH0036

```

```

WT1=ART-AAA
WT2=BIT-BBB
W(1)=CMPLX(WT1,WT2)
CANSP=CZT
IF(CABS(W(1)).LT..0005) GO TO 8511
CJ1=CMPLX(GJR1,GJI1)
CJ0=CMPLX(GJR0,GJI0)
CZJ0=CZT*CJ0
CZJ1=CZT*CJ1
CAJ0=CAF*CJ0
CAJ1=CAB*CJ1
CAZJ=CAB*CJ1/CZT
C1=CZJ0+CAJ1
C2=(2.,0.)*(CZJ1-CAJ0)
CJDB=CJ0-CZJ1+CAJ0-CAZJ
CROT=CSQRT(C1**2-C2*CJDB)
CZDLT=(CROT-C1)/CJDB
8601 CZT=CZT+CZDLT
      CCNTINUE
      CANSP=CZT
      IF(CABS(W(1)).LT..0005) GO TO 8511
44  AOS=.666667+.333333*AAA
      IF(ABO.GT.AOS) GO TO 31
      IF(BBB.NE.0.) GO TO 80
      IF(AAA.LT.0.) GO TO 45
      XAB=SQRT(8.*AAA/(4.+AAA))
      YAB=0.
      D=1.E-5
      NCN=0
      CALL BESJ(XAF,NON,BJ,D,IER)
      BJO=BJ
      NON=1
      CALL BESJ(XAB,NON,BJ,D,IER)
      BJ1=BJ
      PRE=XAF*BJ1-AAA*BJ0
      ANSW(1)=CMPLX(XAB,0.)

```

```

RCH00250 RTCH0037
RCH00260 RTCH0038
RCH00270 RTCH0039
RCH00280 RTCH0040
RCH00290 RTCH0041
RCH00300 RTCH0042
RCH00310 RTCH0043
RCH00320 RTCH0044
RCH00330 RTCH0045
RCH00340 RTCH0046
RCH00350 RTCH0047
RCH00360 RTCH0048
RCH00370 RTCH0049
RCH00380 RTCH0050
RCH00390 RTCH0051
RCH00400 RTCH0052
RCH00410 RTCH0053
RCH00420 RTCH0054
RCH00430 RTCH0055
RCH00440 RTCH0056
RCH00450 RTCH0057
RCH00460 RTCH0058
RCH00470 RTCH0059
RCH00480 RTCH0060
RCH00490 RTCH0061
RCH00500 RTCH0062
RCH00510 RTCH0063
RCH00520 RTCH0064
RCH00530 RTCH0065
RCH00540 RTCH0066
RCH00550 RTCH0067
RCH00560 RTCH0068
RCH00570 RTCH0069
RCH00580 RTCH0070
RCH00590 RTCH0071
RCH00600 RTCH0072

```

```

W(1)=CMPLX(FRE,0.)
NQ7=1
GO TO 21
45 XAB=0.
YAB=SQRT(-8.*AAA/(4.+AAA))
CALL IO(YAB,RI0)
CALL IPI(YAB,RI)
FRE=AAA*RI0+YAB*RI
ANSW(1)=CMPLX(0.,-YAB)
W(1)=CMPLX(FRE,0.)
NQ7=1
GO TO 21
80 SQSD=4.*AAA+ABQ
SQSF=SQRT(SQSD**2+16.*BBQ)
SQDN=4.+2.*AAA+.25*ABQ
XAP=SQRT((SQSF+SQSD)/SQDN)
YAB=-SQRT((SQSF-SQSD)/SQDN)
ANSW(1)=CMPLX(XAP,YAB)
W(1)=FUN(ANSW(1))
NQ7=1
GO TO 21
31 IF(BBB.NE.0.) GO TO 81
IF(AAA) 82,83,83
82 IF(AAA.LT.-.7055) GO TO 251
XLI=-AAA+.57
XRI=-AAA+.6
GO TO 90
251 IF(AAA.LI.-1.705) GO TO 252
XLI=-AAA+.59
XRI=-AAA+.61
GO TO 90
252 IF(AAA.LE.-2.) GO TO 8500
XLI=-AAA+.5
XRI=-AAA+.6
GO TO 90
90 EPS=1.E-4

```

```

RCH00610 RTCH0073
RCH00620 RTCH0074
RCH00630 RTCH0075
RCH00640 RTCH0076
RCH00650 RTCH0077
RCH00660 RTCH0078
RCH00670 RTCH0079
RCH00680 RTCH0080
RCH00690 RTCH0081
RCH00700 RTCH0082
RCH00710 RTCH0083
RCH00720 RTCH0084
RCH00730 RTCH0085
RCH00740 RTCH0086
RCH00750 RTCH0087
RCH00760 RTCH0088
RCH00770 RTCH0089
RCH00780 RTCH0090
RCH00790 RTCH0091
RCH00800 RTCH0092
RCH00810 RTCH0093
RCH00820 RTCH0094
RCH00830 RTCH0095
RCH00840 RTCH0096
RCH00850 RTCH0097
RCH00860 RTCH0098
RCH00870 RTCH0099
RCH00880 RTCH0100
RCH00890 RTCH0101
RCH00900 RTCH0102
RCH00910 RTCH0103
RCH00920 RTCH0104
RCH00930 RTCH0105
RCH00940 RTCH0106
RCH00950 RTCH0107
RCH00960 RTCH0108

```

```

IEND=300
CALL RTMI (YN,FI,FCTI,XLI,XRI,EPS,IEND,IER)
ANSW(1)=CMPLX(0.,-YN)
W(1)=CMPLX(FI,0.)
NQ7=1
IF(IER.NE.0) WRITE(6,91)
GO TO 21
83 IF(AAA.GT.1.0944) GO TO 161
XLI=1.25
XRI=1.31
GO TO 69
161 IF(AAA.GT.1.3385) GO TO 162
XLI=1.29
XRI=1.41
GO TO 69
162 IF(AAA.GT.1.6351) GO TO 163
XLI=1.39
XRI=1.51
GO TO 69
163 IF(AAA.GT.2.0023) GO TO 164
XLI=1.49
XRI=1.61
GO TO 69
164 IF(AAA.GT.2.4679) GO TO 131
XLI=1.59
XRI=1.71
GO TO 69
131 IF(AAA.GT.3.0788) GO TO 169
XLI=1.69
XRI=1.81
GO TO 69
169 IF(AAA.GT.3.9181) GO TO 132
XLI=1.79
XRI=1.91
GO TO 69
132 IF(AAA.GT.5.1519) GO TO 133

```

```

RCHO0970 RTCH0109
RCHO0980 RTCH0110
RCHO0990 RTCH0111
RCHO1000 RTCH0112
RCHO1010 RTCH0113
RCHO1020 RTCH0114
RCHO1030 RTCH0115
RCHO1040 RTCH0116
RCHO1050 RTCH0117
RCHO1060 RTCH0118
RCHO1070 RTCH0119
RCHO1080 RTCH0120
RCHO1090 RTCH0121
RCHO1100 RTCH0122
RCHO1110 RTCH0123
RCHO1120 RTCH0124
RCHO1130 RTCH0125
RCHO1140 RTCH0126
RCHO1150 RTCH0127
RCHO1160 RTCH0128
RCHO1170 RTCH0129
RCHO1180 RTCH0130
RCHO1190 RTCH0131
RCHO1200 RTCH0132
RCHO1210 RTCH0133
RCHO1220 RTCH0134
RCHO1230 RTCH0135
RCHO1240 RTCH0136
RCHO1250 RTCH0137
RCHO1260 RTCH0138
RCHO1270 RTCH0139
RCHO1280 RTCH0140
RCHO1290 RTCH0141
RCHO1300 RTCH0142
RCHO1310 RTCH0143
RCHO1320 RTCH0144

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```

XLI=1.89
XRI=2.01
GO TO 69
133 IF(AAA.GT.7.1631) GO TO 134
XLI=1.99
XRI=2.11
GO TO 69
134 IF(AAA.GT.10.) GO TO 8100
XLI=2.09
XRI=2.21
69 IEND=300
EPS=1.E-4
CALL RTMI(X,F,PCT,XLI,XRI,EPS,IEND,IER)
ANSW(1)=CMPLX(X,0.)
W(1)=CMPLX(F,0.)
NQ7=1
IF(IER.NE.0) WRITE(6,91)
GO TO 21
81 IF(AAA.LT.0.) GO TO 2001
IF(ABQ.GE.99.) GO TO 8100
IF(AAA.GT.0.66) GO TO 1001
IF(BBB.LT.-1.) GO TO 1101
L=1
GO TO 1000
1101 IF(BBB.LT.-1.475) GO TO 1102
L=2
GO TO 1000
1102 IF(BBB.LT.-2.1) GO TO 1103
L=3
GO TO 1000
1103 IF(BBB.LT.-3.5) GO TO 1104
L=4
GO TO 1000
1104 IF(BBB.LT.-5.) GO TO 1121
L=5
GO TO 1000

```

```

RCHO1330 RTCHO145
RCHO1340 RTCHO146
RCHO1350 RTCHO147
RCHO1360 RTCHO148
RCHO1370 RTCHO149
RCHO1380 RTCHO150
RCHO1390 RTCHO151
RCHO1400 RTCHO152
RCHO1410 RTCHO153
RCHO1420 RTCHO154
RCHO1430 RTCHO155
RCHO1440 RTCHO156
RCHO1450 RTCHO157
RCHO1460 RTCHO158
RCHO1470 RTCHO159
RCHO1480 RTCHO160
RCHO1490 RTCHO161
RCHO1500 RTCHO162
RCHO1510 RTCHO163
RCHO1520 RTCHO164
RCHO1530 RTCHO165
RCHO1540 RTCHO166
RCHO1550 RTCHO167
RCHO1560 RTCHO168
RCHO1570 RTCHO169
RCHO1580 RTCHO170
RCHO1590 RTCHO171
RCHO1600 RTCHO172
RCHO1610 RTCHO173
RCHO1620 RTCHO174
RCHO1630 RTCHO175
RCHO1640 RTCHO176
RCHO1650 RTCHO177
RCHO1660 RTCHO178
RCHO1670 RTCHO179
RCHO1680 RTCHO180

```

1121 L=6  
GO TO 1000  
1001 IF(AAA.GT.1.) GO TO 1002  
IF(BBB.LT.-1.5) GO TO 1201  
IF(BBB.LT.-.4) GO TO 1211  
L=7  
GO TO 1000  
1211 IF(BBB.LT.-.7) GO TO 1213  
L=8  
GO TO 1000  
1213 IF(BBB.LT.-1.) GO TO 1212  
L=60  
GO TO 1000  
1212 L=9  
GO TO 1000  
1201 IF(BBB.LT.-2.4) GO TO 1202  
L=10  
GO TO 1000  
1202 IF(BBB.LT.-4.) GO TO 1203  
L=11  
GO TO 1000  
1203 IF(BBB.LT.-5.) GO TO 1204  
L=12  
GO TO 1000  
1204 IF(BBB.LT.-7.) GO TO 1205  
L=62  
GO TO 1000  
1205 L=63  
GO TO 1000  
1002 IF(AAA.GT.1.7) GO TO 1003  
IF(BBB.LT.-.85) GO TO 1301  
L=13  
GO TO 1000  
1301 IF(BBB.LT.-1.9) GO TO 1302  
L=14  
GO TO 1000

RCHO1690 RTCHO181  
RCHO1700 RTCHO182  
RCHO1710 RTCHO183  
RCHO1720 RTCHO184  
RCHO1730 RTCHO185  
RCHO1740 RTCHO186  
RCHO1750 RTCHO187  
RCHO1760 RTCHO188  
RCHO1770 RTCHO189  
RCHO1780 RTCHO190  
RCHO1790 RTCHO191  
RCHO1800 RTCHO192  
RCHO1810 RTCHO193  
RCHO1820 RTCHO194  
RCHO1830 RTCHO195  
RCHO1840 RTCHO196  
RCHO1850 RTCHO197  
RCHO1860 RTCHO198  
RCHO1870 RTCHO199  
RCHO1880 RTCHO200  
RCHO1890 RTCHO201  
RCHO1900 RTCHO202  
RCHO1910 RTCHO203  
RCHO1920 RTCHO204  
RCHO1930 RTCHO205  
RCHO1940 RTCHO206  
RCHO1950 RTCHO207  
RCHO1960 RTCHO208  
RCHO1970 RTCHO209  
RCHO1980 RTCHO210  
RCHO1990 RTCHO211  
RCHO2000 RTCHO212  
RCHO2010 RTCHO213  
RCHO2020 RTCHO214  
RCHO2030 RTCHO215  
RCHO2040 RTCHO216

```

1302 IF(BBB.LT.-3.4) GO TO 1303
      L=15
      GO TO 1000
1303 IF(BBB.LT.-6.) GO TO 1304
      L=16
      GO TO 1000
1304 L=17
      GO TO 1000
1003 IF(AAA.GT.3.5) GO TO 1004
      IF(BBB.LT.-1.) GO TO 1401
      L=18
      GO TO 1000
1401 IF(BBB.LT.-2.7) GO TO 1402
      L=19
      GO TO 1000
1402 IF(BBB.LT.-6.) GO TO 1403
      L=20
      GO TO 1000
1403 L=21
      GO TO 1000
1004 IF(AAA.GT.8.) GO TO 1005
      IF(BBB.LT.-3.5) GO TO 1501
      L=22
      GO TO 1000
1501 L=23
      GO TO 1000
1005 L=24
      GO TO 1000
2001 PHI=ATAN(-AAA/BBB)*180./3.14159
      IF(PHI.LT.-23.3) GO TO 3001
      IF(ABQ.GE.99.) GO TO 8100
      IF(BBB.LT.-.72) GO TO 2101
      L=25
      GO TO 1000
2101 IF(BBB.LT.-1.005) GO TO 2201
      L=26

```

```

RCHO2050 RTCH0217
RCHO2060 RTCH0218
RCHO2070 RTCH0219
RCHO2080 RTCH0220
RCHO2090 RTCH0221
RCHO2100 RTCH0222
RCHO2110 RTCH0223
RCHO2120 RTCH0224
RCHO2130 RTCH0225
RCHO2140 RTCH0226
RCHO2150 RTCH0227
RCHO2160 RTCH0228
RCHO2170 RTCH0229
RCHO2180 RTCH0230
RCHO2190 RTCH0231
RCHO2200 RTCH0232
RCHO2210 RTCH0233
RCHO2220 RTCH0234
RCHO2230 RTCH0235
RCHO2240 RTCH0236
RCHO2250 RTCH0237
RCHO2260 RTCH0238
RCHO2270 RTCH0239
RCHO2280 RTCH0240
RCHO2290 RTCH0241
RCHO2300 RTCH0242
RCHO2310 RTCH0243
RCHO2320 RTCH0244
RCHO2330 RTCH0245
RCHO2340 RTCH0246
RCHO2350 RTCH0247
RCHO2360 RTCH0248
RCHO2370 RTCH0249
RCHO2380 RTCH0250
RCHO2390 RTCH0251
RCHO2400 RTCH0252

```

GO TO 1000  
2201 IF(BBB.LT.-1.486) GO TO 2301  
L=27  
GO TO 1000  
2301 IF(BBB.LT.-1.9) GO TO 2401  
L=28  
GO TO 1000  
2401 IF(BBB.LT.-2.4) GO TO 2501  
IF(AAA.LT.-.6) GO TO 2402  
L=29  
GO TO 1000  
2402 L=30  
GO TO 1000  
2501 IF(BBB.LT.-3.) GO TO 2601  
IF(AAA.LT.-.6) GO TO 2502  
L=31  
GO TO 1000  
2502 IF(AAA.LT.-1.) GO TO 2503  
L=32  
GO TO 1000  
2503 IF(AAA.LT.-1.2) GO TO 2504  
L=33  
GO TO 1000  
2504 L=34  
GO TO 1000  
2601 IF(BBB.LT.-3.5) GO TO 2701  
IF(AAA.LT.-.5) GO TO 2602  
L=35  
GO TO 1000  
2602 IF(AAA.LT.-.8) GO TO 2603  
L=36  
GO TO 1000  
2603 IF(AAA.LT.-1.) GO TO 2604  
L=37  
GO TO 1000  
2604 L=38

RCHO2410 RTCH0253  
RCHO2420 RTCH0254  
RCHO2430 RTCH0255  
RCHO2440 RTCH0256  
RCHO2450 RTCH0257  
RCHO2460 RTCH0258  
RCHO2470 RTCH0259  
RCHO2480 RTCH0260  
RCHO2490 RTCH0261  
RCHO2500 RTCH0262  
RCHO2510 RTCH0263  
RCHO2520 RTCH0264  
RCHO2530 RTCH0265  
RCHO2540 RTCH0266  
RCHO2550 RTCH0267  
RCHO2560 RTCH0268  
RCHO2570 RTCH0269  
RCHO2580 RTCH0270  
RCHO2590 RTCH0271  
RCHO2600 RTCH0272  
RCHO2610 RTCH0273  
RCHO2620 RTCH0274  
RCHO2630 RTCH0275  
RCHO2640 RTCH0276  
RCHO2650 RTCH0277  
RCHO2660 RTCH0278  
RCHO2670 RTCH0279  
RCHO2680 RTCH0280  
RCHO2690 RTCH0281  
RCHO2700 RTCH0282  
RCHO2710 RTCH0283  
RCHO2720 RTCH0284  
RCHO2730 RTCH0285  
RCHO2740 RTCH0286  
RCHO2750 RTCH0287  
RCHO2760 RTCH0288



GO TO 1000  
2701 IF (BBB.LT.-5.) GO TO 2801  
IF (AAA.LT.-.8) GO TO 2702  
L=39  
GO TO 1000  
2702 IF (BBE.LE.-4.) GO TO 2703  
L=40  
GO TO 1000  
2703 L=61  
GO TO 1000  
2801 L=41  
GO TO 1000  
3001 IF (AAA.LE.-1.5) GO TO 8500  
IF (AAA.GT.-1.5) GO TO 7001  
IF (BBE.LT.-1.5) GO TO 6002  
L=42  
GO TO 2000  
6002 IF (BBB.LT.-2.5) GO TO 6003  
L=43  
GO TO 2000  
6003 IF (BBB.LT.-3.5) GO TO 6004  
L=44  
GO TO 2000  
6004 L=45  
GO TO 2000  
7001 IF (BBB.LT.-.5) GO TO 7101  
IF (AAA.GT.-1.1) GO TO 7002  
L=46  
GO TO 2000  
7002 IF (AAA.GT.-.5) GO TO 7003  
L=47  
GO TO 2000  
7003 L=48  
GO TO 2000  
7101 IF (BBB.LE.-1.) GO TO 7201  
IF (AAA.GT.-1.1) GO TO 7102

RCHO2770 RTCH0289  
RCHO2780 RTCH0290  
RCHO2790 RTCH0291  
RCHO2800 RTCH0292  
RCHO2810 RTCH0293  
RCHO2820 RTCH0294  
RCHO2830 RTCH0295  
RCHO2840 RTCH0296  
RCHO2850 RTCH0297  
RCHO2860 RTCH0298  
RCHO2870 RTCH0299  
RCHO2880 RTCH0300  
RCHO2890 RTCH0301  
RCHO2900 RTCH0302  
RCHO2910 RTCH0303  
RCHO2920 RTCH0304  
RCHO2930 RTCH0305  
RCHO2940 RTCH0306  
RCHO2950 RTCH0307  
RCHO3980 RTCH0308  
RCHO3990 RTCH0309  
RCHO4000 RTCH0310  
RCHO4010 RTCH0311  
RCHO4020 RTCH0312  
RCHO4030 RTCH0313  
RCHO4040 RTCH0314  
RCHO4050 RTCH0315  
RCHO4060 RTCH0316  
RCHO4070 RTCH0317  
RCHO4080 RTCH0318  
RCHO4090 RTCH0319  
RCHO4100 RTCH0320  
RCHO4110 RTCH0321  
RCHO4120 RTCH0322  
RCHO4130 RTCH0323  
RCHO4140 RTCH0324

```

L=49
GO TO 2000
7102 IF(AAA.GT.-.5) GO TO 7103
L=50
GO TO 2000
7103 L=51
GO TO 2000
7201 IF(PRE.LT.-1.5) GO TO 7301
IF(AAA.GT.-1.1) GO TO 7202
L=52
GO TO 2000
7202 L=53
GO TO 2000
7301 IF(BBB.LT.-2.) GO TO 7401
L=54
GO TO 2000
7401 IF(PRE.LT.-2.5) GO TO 7501
L=55
GO TO 2000
7501 IF(BBB.LT.-2.7) GO TO 7601
IF(AAA.GT.-1.3) GO TO 7502
L=56
GO TO 2000
7502 L=57
GO TO 3000
7601 IF(AAA.GT.-1.4) GO TO 7602
IF(BBB.LT.-2.94) GO TO 7611
L=58
GO TO 2000
7611 L=64
GO TO 2000
7602 L=59
GO TO 2000
1000 Z(1)=ZIN(L,1)
Z(2)=ZIN(L,2)
Z(3)=ZIN(L,3)

```

```

RCH04150 RTCH0325
RCH04160 RTCH0326
RCH04170 RTCH0327
RCH04180 RTCH0328
RCH04190 RTCH0329
RCH04200 RTCH0330
RCH04210 RTCH0331
RCH04220 RTCH0332
RCH04230 RTCH0333
RCH04240 RTCH0334
RCH04250 RTCH0335
RCH04260 RTCH0336
RCH04270 RTCH0337
RCH04280 RTCH0338
RCH04290 RTCH0339
RCH04300 RTCH0340
RCH04310 RTCH0341
RCH04320 RTCH0342
RCH04330 RTCH0343
RCH04340 RTCH0344
RCH04350 RTCH0345
RCH04360 RTCH0346
RCH04370 RTCH0347
RCH04380 RTCH0348
RCH04390 RTCH0349
RCH04400 RTCH0350
RCH04410 RTCH0351
RCH04420 RTCH0352
RCH04430 RTCH0353
RCH04440 RTCH0354
RCH04450 RTCH0355
RCH04460 RTCH0356
RCH04470 RTCH0357
RCH04480 RTCH0358
RCH04490 RTCH0359
RCH04500 RTCH0360

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```

      Z(4)=ZIN(L,4)
      GO TO 9000
2000 ZAB=CMPLX(-BBB,AAA)
      Z(1)=ZAB-ZIN(L,1)
      Z(2)=ZAB-ZIN(L,2)
      Z(3)=ZAB-ZIN(L,3)
      Z(4)=ZAB-ZIN(L,4)
      GO TO 9000
3000 ZAB=CMPLX(-BBB,0.)
      Z(1)=ZAB-ZIN(L,1)
      Z(2)=ZAB-ZIN(L,2)
      Z(3)=ZAB-ZIN(L,3)
      Z(4)=ZAB-ZIN(L,4)
9000 M=2
      N=4
      NPRINT=0
      ERROR=(1.E-2,1.E-2)
      CALL YSQNK9(Z,N,ERROR,M,NPRINT,ANSW,W,RETErr,NO,FUN,NQ7)
      GO TO 21
8100 XO=2.40483
      CAB=CMPLX(AAA,BBB)
      CAHF=CAB+(.5,0.)
      DQN=XO**2+.25
      CQRT=CSQRT((1.,0.)+1.33333*DQN/CAHF**2)
      CANSP=XO*((1.,0.)-1.5*CAHF*(CQRT-(1.,0.)))/DQN
      DO 8505 LPS=1,20
      XP=REAL(CANSP)
      YP=AIMAG(CANSP)
      CALL BECHO(XP,YP,ARE,BIM,JR0,J10,JR1,J11)
      W1=ARE-AAA
      W2=BIM-BBB
      W(1)=CMPLX(W1,W2)
      IF(CABS(W(1)).LT..0005) GO TO 8511
      CIAP=CMPLX(JR0,J10)/CMPLX(JR1,J11)
      CZAJ=CANSP/CAB
      CMAPJ=CIAP*CZAJ

```

```

RCHO4510 RTCH0361
RCHO4520 RTCH0362
RCHO4530 RTCH0363
RCHO4540 RTCH0364
RCHO4550 RTCH0365
RCHO4560 RTCH0366
RCHO4570 RTCH0367
RCHO4580 RTCH0368
RCHO4590 RTCH0369
RCHO4600 RTCH0370
RCHO4610 RTCH0371
RCHO4620 RTCH0372
RCHO4630 RTCH0373
RCHO4640 RTCH0374
RCHO4650 RTCH0375
RCHO4660 RTCH0376
RCHO4670 RTCH0377
RCHO4680 RTCH0378
RCHO4690 RTCH0379
RCHO4700 RTCH0380
RCHO4710 RTCH0381
RCHO4720 RTCH0382
RCHO4730 RTCH0383
RCHO4740 RTCH0384
RCHO4750 RTCH0385
RCHO4760 RTCH0386
RCHO4770 RTCH0387
RCHO4780 RTCH0388
RCHO4790 RTCH0389
RCHO4800 RTCH0390
RCHO4810 RTCH0391
RCHO4820 RTCH0392
RCHO4830 RTCH0393
RCHO4840 RTCH0394
RCHO4850 RTCH0395
RCHO4860 RTCH0396

```

```

      CADM=1./CANSP+CZAJ
      CZMAP=1.+CMAPJ
      CQI=2.*CADM*(CTAP-CZAJ)/CZMAP**2
      CDELZ=CZMAP*((1.,0.)-CSQRT((1.,0.)-CQI))/CADM
8505  CONTINUE
      GO TO 8511
8500  CDAB=(.5,0.)
      CAB=CMPLX(AAA,BBB)
      CEI=(0.,1.)
      DO 8501 KPS=1,20
      CZ=CEI*(CAB-CDAB)
      XP=REAL(CZ)
      YP=AIMAG(CZ)
      IF(XP.NE.0..AND.YP.NE.0.) GO TO 8503
      CALL BECHO(XP,YP,ARE,BIM,JRO,JIO,JP1,JI1)
      CALP=CMPLX(JP1,JI1)/CMPLX(JRO,JIO)
      GO TO 8504
8503  CALL CMJYB(CZ,CJB,CYB)
      CALP=CJB(2)/CJB(1)
8504  CALP2=CALP**2
      CPLP=CALP2+(1.,0.)
      CPLM=(1.,0.)-CALP2
      CALPP=CPLP/CALP
      CZAP=CZ*CALP
      CPLZ=CPLM/CZAP
      CQ=(CPLP+(.5,0.)*CPLZ)*((1.,0.)-CAB/CZAP)/CALPP**2
      CORP=(1.,0.)-CSQRT((1.,0.)-(4.,0.)*CQ)
      CDNM=(2.,0.)*CPLP+CPLZ
      CANSP=CZ-CALPP*CORP/CDNM
      XP=REAL(CANSP)
      YP=AIMAG(CANSP)
      CALL BECHO(XP,YP,ARE,BIM,JRO,JIO,JP1,JI1)
      W1=ARE-AAA
      W2=BIM-BBB
      W(1)=CMPLX(W1,W2)

```

```

RCHO4870 RTCH0397
RCHO4880 RTCH0398
RCHO4890 RTCH0399
RCHO4900 RTCH0400
RCHO4910 RTCH0401
RCHO4920 RTCH0402
RCHO4930 RTCH0403
RCHO4940 RTCH0404
RCHO4950 RTCH0405
RCHO4960 RTCH0406
RCHO4970 RTCH0407
RCHO4980 RTCH0408
RCHO4990 RTCH0409
RCHO5000 RTCH0410
RCHO5010 RTCH0411
RCHO5020 RTCH0412
RCHO5030 RTCH0413
RCHO5040 RTCH0414
          RTCH0415
          RTCH0416
RCHO5100 RTCH0417
RCHO5110 RTCH0418
RCHO5120 RTCH0419
RCHO5130 RTCH0420
RCHO5140 RTCH0421
RCHO5150 RTCH0422
RCHO5160 RTCH0423
RCHO5170 RTCH0424
RCHO5180 RTCH0425
RCHO5190 RTCH0426
RCHO5200 RTCH0427
RCHO5210 RTCH0428
RCHO5220 RTCH0429
RCHO5230 RTCH0430
RCHO5240 RTCH0431
RCHO5250 RTCH0432

```

```
IF(CABS(W(1)).LT..0005) GO TO 8511
DA=ARE-YP
DE=RI4+XP
CDAB=CMPLX(DA,DB)
8501 CONTINUE
8511 ANSW(1)=CANSP
NQ7=1
21 RETURN
END
```

```
RCH05260 RTCH0433
RCH05270 RTCH0434
RCH05280 RTCH0435
RCH05290 RTCH0436
RCH05300 RTCH0437
RCH05310 RTCH0438
RCH05320 RTCH0439
RCH05330 RTCH0440
RCH05340 RTCH0441
```

```

SUBROUTINE BECHO (XP,YP,ARE,BIM,JR0,JIO,JR1,JI1)
REAL*4 JR0,JIO,JR1,JI1
COMPLEX*8 CJB(2),CYB(2),CZ,CMPLX
IF (ABS(XP).LT.1.E-30) XP=0.
IF (ABS(YP).LT.1.E-30) YP=0.
IF (YP.NE.0.) GO TO 21
D=1.E-6
NJ=0
CALL BESJ (XP,NJ,JR0,D,IER)
IF (JR0.LT.1.E-10.AND.JR0.GE.0.) JR0=1.E-10
IF (JR0.LT.0..AND.JR0.GT.-1.E-10) JR0=-1.E-10
NJ=1
CALL BESJ (XP,NJ,JR1,D,IER)
ARE=XP*JR1/JR0
BIM=0.
JIO=0.
JI1=0.
GO TO 50
21 IF (XP.NE.0.) GO TO 31
YN=-YP
CALL IO (YN,JR0)
IF (JR0.LT.1.E-10.AND.JR0.GE.0.) JR0=1.E-10
IF (JR0.LT.0..AND.JR0.GT.-1.E-10) JR0=-1.E-10
CALL IRI (YN,JI1)
ARE=YP*JI1/JR0
JIO=0.
JR1=0.
BIM=0.
GO TO 50
31 CZ=CMPLX (XP,YP)
CALL CMJYB (CZ,CJB,CYB)
JR0=REAL (CJB (1))
JR1=REAL (CJB (2))
JIO=AIMAG (CJB (1))
JI1=AIMAG (CJB (2))
IF (JR0.LT.1.E-20.AND.JR0.GE.0.) JR0=1.E-20

```

```

BECH0001
BECH0002
BECH0003
BECH0004
BECH0005
BECH0006
BECH0007
BECH0008
BECH0009
BECH0010
BECH0011
BECH0012
BECH0013
BECH0014
BECH0015
BECH0016
BECH0017
BECH0018
BECH0019
BECH0020
BECH0021
BECH0022
BECH0023
BECH0024
BECH0025
BECH0026
BECH0027
BECH0028
BECH0029
BECH0030
BECH0031
BECH0032
BECH0033
BECH0034
BECH0035
BECH0036

```

IF (JIO.LT.1.E-20.AND.JIO.GE.0.) JIO=1.E-20	BECH0037
IF (JR1.LT.1.E-20.AND.JR1.GE.0.) JR1=1.E-20	BECH0038
IF (JI1.LT.1.E-20.AND.JI1.GE.0.) JI1=1.E-20	BECH0039
IF (JRO.LT.0..AND.JRO.GT.-1.E-20) JRO=-1.E-20	BECH0040
IF (JIO.LT.0..AND.JIO.GT.-1.E-20) JIO=-1.E-20	BECH0041
IF (JR1.LT.0..AND.JR1.GT.-1.E-20) JR1=-1.E-20	BECH0042
IF (JI1.LT.0..AND.JI1.GT.-1.E-20) JI1=-1.E-20	BECH0043
RD=JRO*JRC+JIO*JIO	BECH0044
IF (RD.LT.1.E-30) RD=1.E-30	BECH0045
RA=JRO*JR1+JIO*JI1	BECH0046
RB=JRO*JI1-JR1*JIO	BECH0047
ARE=(XP*RA-YP*RB)/RD	BECH0048
BIM=(XP*RB+YP*RA)/RD	BECH0049
50 RETURN	BECH0050
END	BECH0051

```
COMPLEX FUNCTION FUN(Z)
COMPLEX*8 Z, CMPLX, ACM, CJB(2), CYB(2)
DIMENSION BJRE(2), BJIM(2)
COMMON /QFNT/AAA, BBB
AC=AAA
BC=BBB
ACM=CMPLX(AC, BC)
CALL CMJYB(Z, CJB, CYB)
FUN=Z*CJB(2) - ACM*CJB(1)
RETURN
END
```

```
FUNZ0001
FUNZ0002
FUNZ0003
FUNZ0004
FUNZ0005
FUNZ0006
FUNZ0007
FUNZ0008
FUNZ0009
FUNZ0010
FUNZ0011
```