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Study of an Axial Fan Combined with a Microperforated Duct

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Study of an axial fan combined with a microperforated duct

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INTER-NOISE 15, SAN FRANCISCO, USA
8/11/2015 TUESDAY

Acknowledgement



□ 3M Company, USA

- The authors acknowledge the support of 3M Corporation through the provision of materials for the fan noise experiments and for the financial support of this work.

Objective

- ❑ Two main fan types of HVAC

	Noise Level	Air Volume	Static Pressure
Axial Fans	Low	High	Low
Centrifugal Fans	High	Low	High

- ❑ By adopting the microperforated duct for the HVAC system using an axial fan, it is expected to have benefits in the reduction of noise level while maintaining similar volume flow rate performance and static pressure capabilities of the impermeable duct.

- ❑ Noise reduction performance of the microperforated duct will be **studied experimentally by measuring the sound power radiated from the ducted fan.**

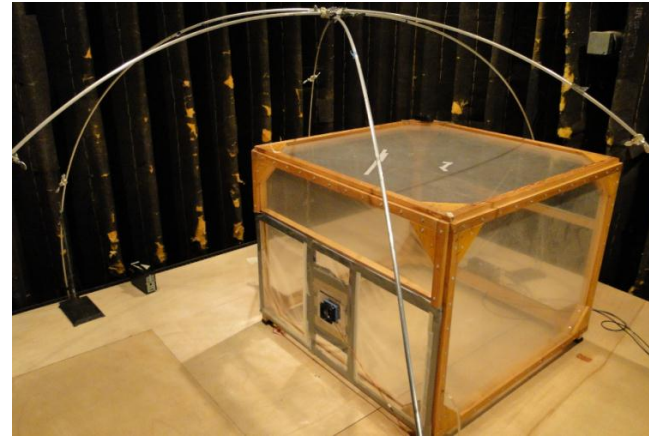
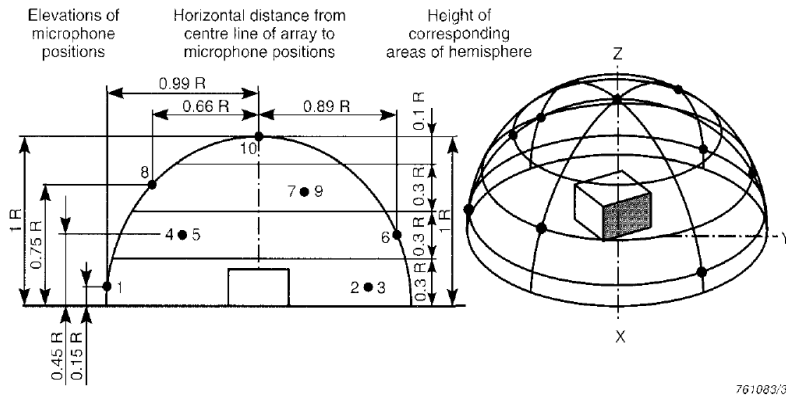


- ❑ Sound field around the microperforated ducted fan will be **visualized by using the nearfield Acoustic Holography method.**



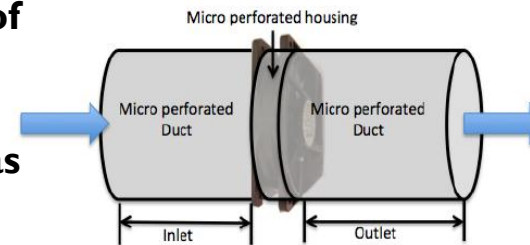
Experimental setup

Hemispherical Frame Configuration for Sound Power Level measurement.

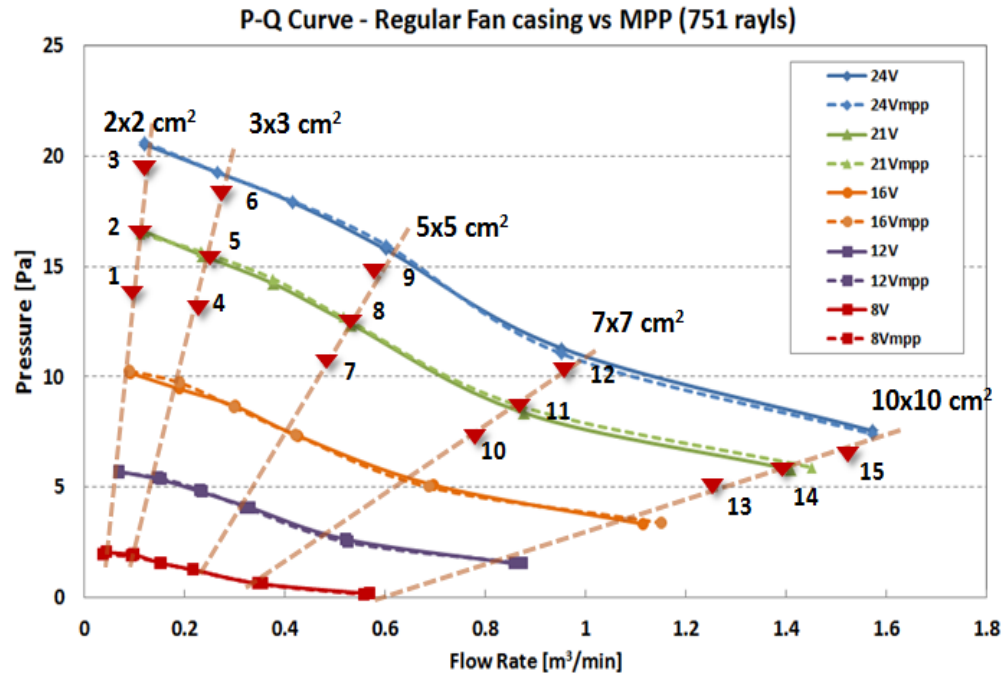


Controllable opening

- Plenum designed based on ISO 10302.
- The test plenum is intended for measuring the flow rate and the fan static pressure.
- 10 Microphone positions on equal areas on the surface of a hemisphere to measure sound power. [ISO 3744]
- Radius of hemispherical frame is **5.5 ft.**
- Test equipment including the hemispherical frame was set up in the anechoic chamber at Herrick Laboratories.



P-Q curve and operating points



▼ Fan operation condition for comparison

- ✓ Rotation speed was controlled by giving different input voltage 19V, 21V and 23V of input voltage
- ✓ Flow exit area was varied from 2 x 2 to 10 x 10 cm²

Pt.	Pressure [Pa]	Opening Area [cm ²]	Flow Rate [m ³ /min]	Flow Vel. [m/s]	Rotation Speed [RPM]
1	12.0	2x2	0.1	3.8	1474.7
2	15.2	2x2	0.1	4.6	1599.3
3	17.8	2x2	0.1	5.4	1716.7
4	11.9	3x3	0.2	3.7	1492.7
5	14.1	3x3	0.2	4.1	1618.7
6	16.4	3x3	0.2	4.4	1736.7
7	9.5	5x5	0.4	2.8	1542.7
8	11.6	5x5	0.5	3.4	1676.0
9	13.4	5x5	0.6	3.9	1806.0
10	6.7	7x7	0.8	2.7	1606.0
11	8.2	7x7	0.9	2.9	1748.0
12	9.2	7x7	1.0	3.3	1882.0
13	4.5	10x10	1.3	2.2	1580.7
14	5.4	10x10	1.4	2.4	1712.0
15	6.3	10x10	1.6	2.6	1850.0

Testing procedures

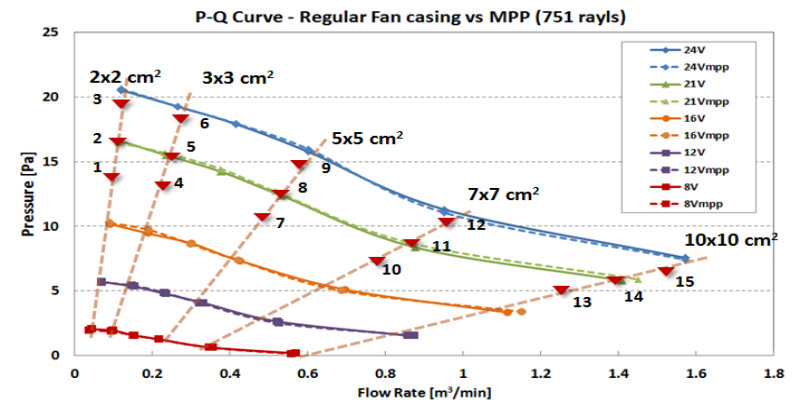
1. Operate a fan at different operating conditions selected from the fan's performance curve.

2. Measure the signals at the surface of hemispherical array.

3. Calculate sound power level according to ISO 3744

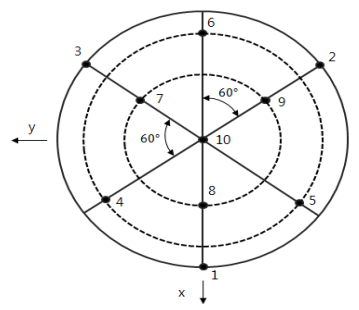


9-12 AUGUST 2015
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Position #	z-dir.	Position #	z-dir.
1	0.15 R	6	0.45 R
2	0.15 R	7	0.75 R
3	0.15 R	8	0.75 R
4	0.45 R	9	0.75 R
5	0.45 R	10	1 R

R: Radius of Hemispherical frame



$$L_w = L_p + 10 \log_{10} \frac{S}{S_{ref}}$$

L_p : Space – averaged sound pressure level

S_{ref} : Reference area, 1 m²

S : Surface area of the hemisphere

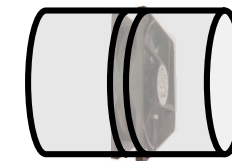
Duct dimensions and material properties

□ Duct Lengths

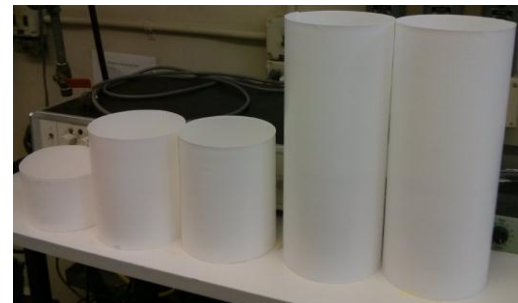
	Inlet Length [cm]	Outlet Length [cm]	Total Length [cm]
Duct Short	6.00	6.00	12.0
Duct Long	27.8	27.8	55.6

□ MPP properties

	Hole Diameter [μm]	Thickness [m]	Flow Resistance [Rayls]
MPP 75I	150.50	0.00035	75I



Duct Short MPP 75I

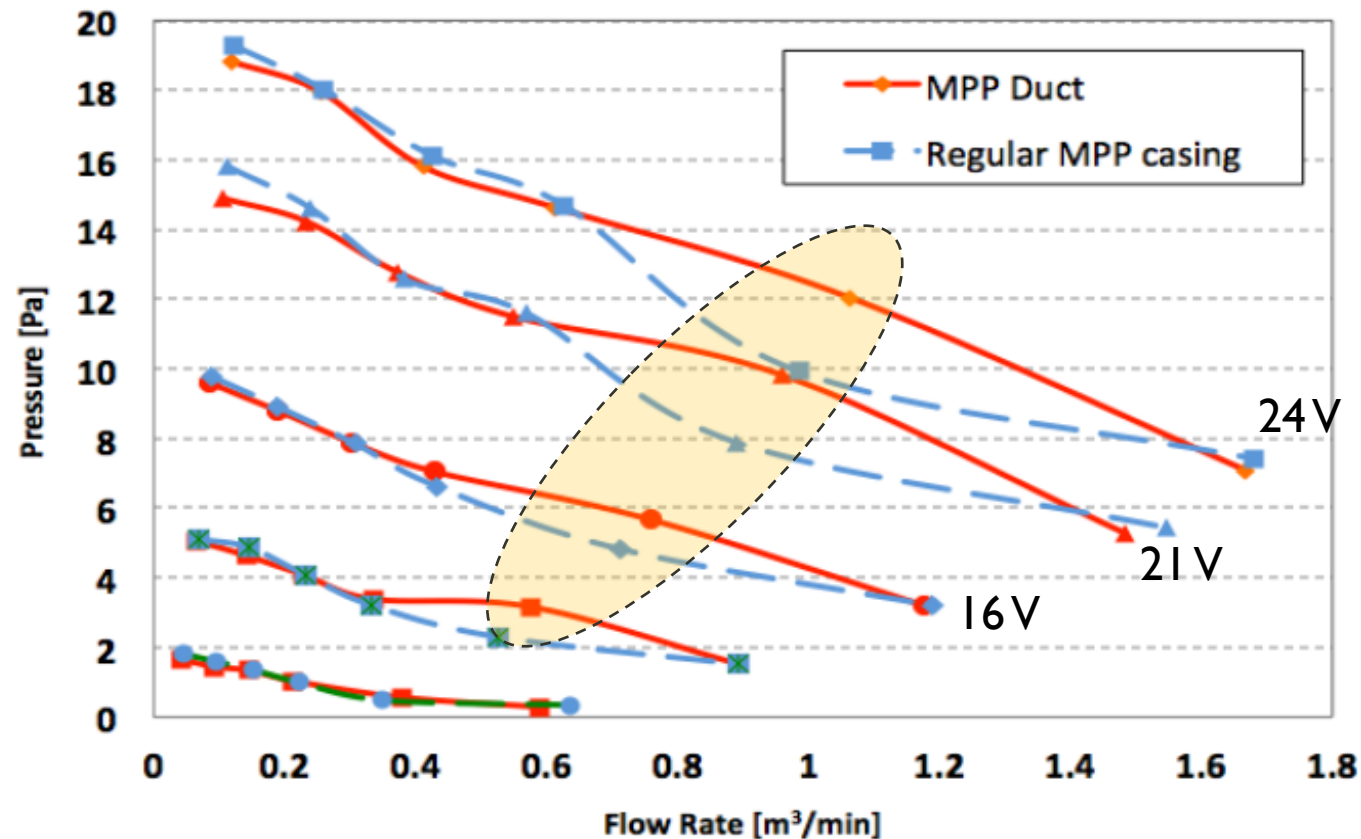


Duct Long MPP 75I



Performance of extended housing

P-Q Curve – MPP (75l Rays) Duct Casing vs MPP (75l Rays) Regular Fan



- ❑ MPP duct casing generates more static pressure and flow rate at less operating voltage!!
- ❑ Regular MPP casing results were from Noise-con 13, Denver, CO, USA

Short ducts test results

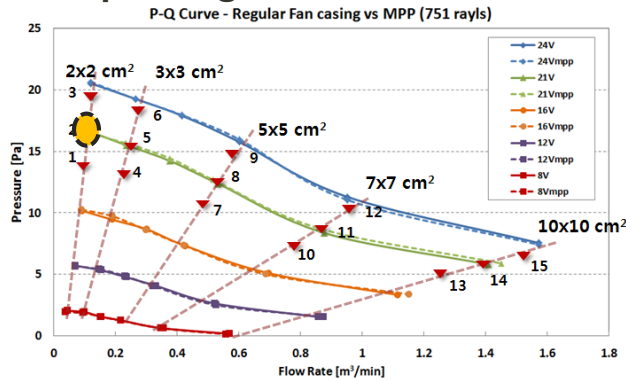
Comparison



**Duct short
Not-Perf.**

**Duct short
MPP 751**

Operating Point



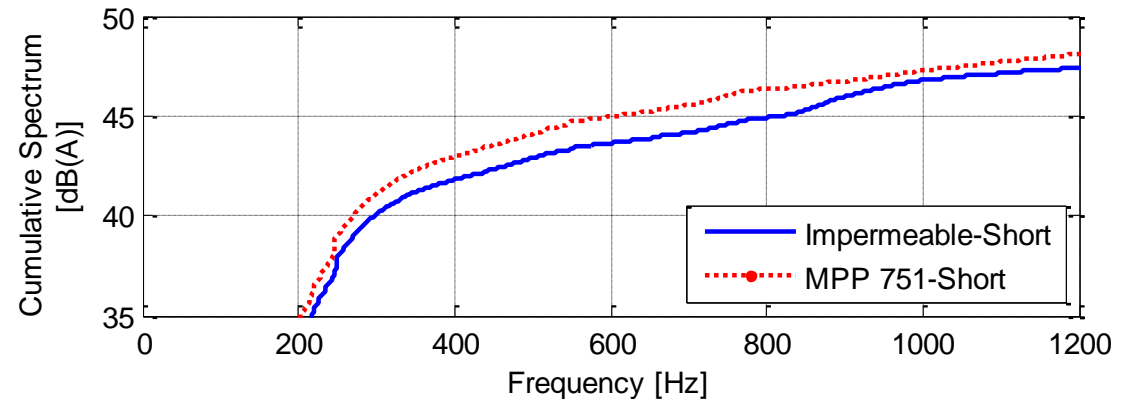
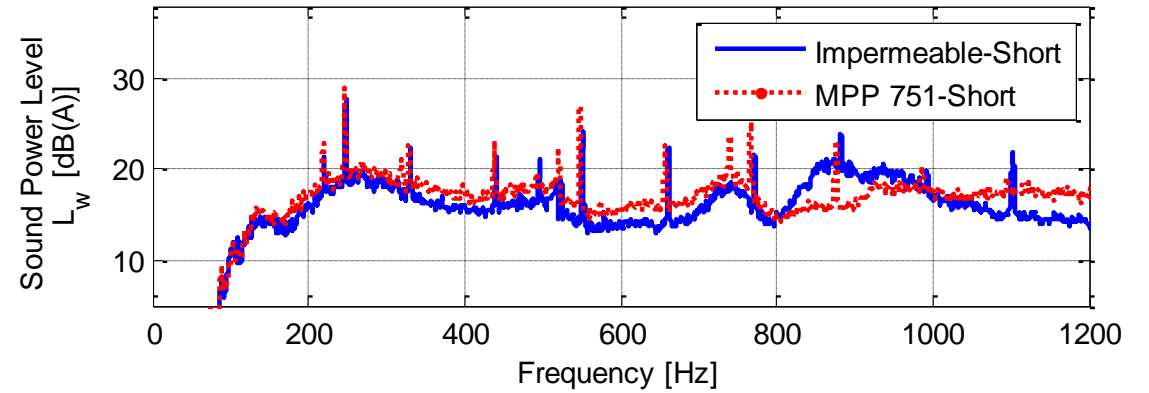
Blade Passage Tone [dB(A)]

DUCT REG.	DUCT 751
27.7	29.0

Overall Sound Power Level [dB(A)]

DUCT REG.	DUCT 751
50.4	51.1

Measurement at operating condition #2



Short ducts test results

❑ Blade passage tone levels comparisons at all operating points.

OP Blade Passage Tone Level [dBA]			OP Blade Passage Tone Level [dBA]			OP Blade Passage Tone Level [dBA]		
OP #	Impermeable	MPP 75 I	OP #	Impermeable	MPP75 I	OP #	Impermeable	MPP75 I
1	23.5	24.9	6	30.6	30.8	11	32.3	32.6
2	27.7	29.0	7	25.7	23.0	12	34.4	33.5
3	29.2	31.6	8	28.8	26.4	13	33.0	33.5
4	25.6	24.6	9	30.7	29.1	14	37.6	37.5
5	27.8	28.7	10	28.5	29.2	15	38.4	39.4

❑ Overall sound power levels comparisons at all operating points.

OP Overall Sound Power Level [dBA]			OP Overall Sound Power Level [dBA]			OP Overall Sound Power Level [dBA]		
OP #	Impermeable	MPP 75 I	OP #	Impermeable	MPP75 I	OP #	Impermeable	MPP75 I
1	48.5	49.1	6	51.7	52.3	11	51.0	51.4
2	50.4	51.1	7	49.0	49.3	12	52.4	52.8
3	51.7	52.4	8	50.3	50.9	13	49.7	49.9
4	48.6	49.0	9	51.7	52.4	14	52.0	52.1
5	50.3	50.9	10	49.0	49.4	15	53.4	53.6

✓ Short microperforated duct does not have beneficial effects compare to impermeable duct.

Long ducts test results

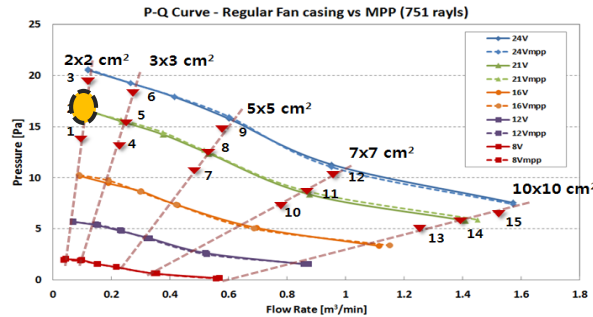
Comparison



**Duct Long
Not-Perf.**

**Duct Long
MPP 751**

Operating Point



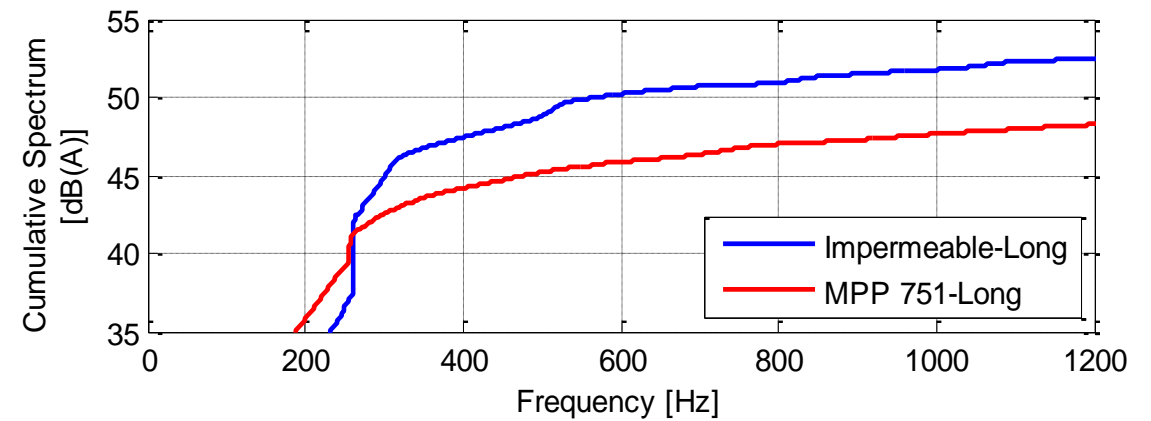
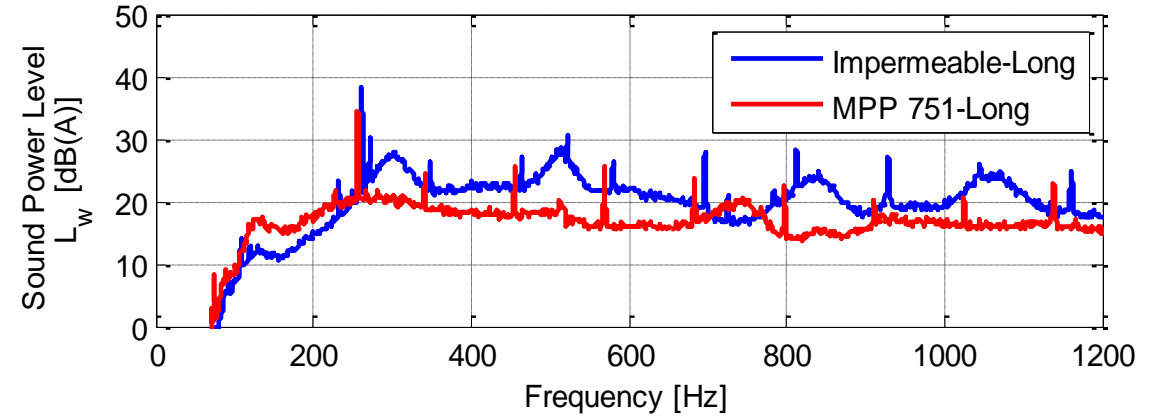
Blade Passage Tone [dB(A)]

DUCT REG.	DUCT 751
38.3	34.4

Overall Sound Power Level [dB(A)]

DUCT REG.	DUCT 751
53.8	50.7

Measurement at operating condition #2



Long ducts test results

❑ Blade passage tone levels comparisons at all operating points.

OP Blade Passage Tone Level [dBA]			OP Blade Passage Tone Level [dBA]			OP Blade Passage Tone Level [dBA]		
OP #	Impermeable	MPP 75 I	OP #	Impermeable	MPP75 I	OP #	Impermeable	MPP75 I
1	30.4	29.7	6	45.6	36.3	11	33.1	30.4
2	38.3	34.3	7	29.9	26.4	12	39.7	35.2
3	43.6	37.2	8	37.8	32.0	13	27.7	25.7
4	30.4	28.3	9	43.6	35.8	14	32.3	29.6
5	39.8	33.0	10	25.3	25.3	15	36.1	31.6

❑ Overall sound power levels comparisons at all operating points.

OP Overall Sound Power Level [dBA]			OP Overall Sound Power Level [dBA]			OP Overall Sound Power Level [dBA]		
OP #	Impermeable	MPP 75 I	OP #	Impermeable	MPP75 I	OP #	Impermeable	MPP75 I
1	54.9	48.9	6	56.1	52.1	11	54.3	52.8
2	53.8	50.7	7	53.4	49.6	12	56.6	54.5
3	55.9	52.1	8	52.8	50.9	13	51.0	48.3
4	57.3	48.9	9	55.0	52.8	14	52.9	52.5
5	53.5	50.6	10	59.8	54.1	15	54.1	53.9

✓ Long microperforated duct has beneficial effects compare to impermeable duct.

Pressure generated by the long ducts

- ❑ Pressures generated by the long ducted fan was measured with the micromanometer (Dwyer Model 1430) repeatedly and then the results were averaged.
- ❑ The accuracy of micromanometer : ± 0.06 Pa



Short ducts comparison

	REG [Pa]	Duct 75 l [Pa]		REG [Pa]	Duct 75 l [Pa]		REG [Pa]	Duct 75 l [Pa]
1	11.3	11.8	6	15.8	16.4	11	9.7	9.8
2	14.8	15.8	7	7.9	8.9	12	10.8	10.8
3	17.3	17.5	8	10.8	11.8	13	4.1	4.1
4	10.8	10.8	9	12.8	13.5	14	5.1	5.1
5	13.8	13.8	10	6.9	6.9	15	6.0	6.0

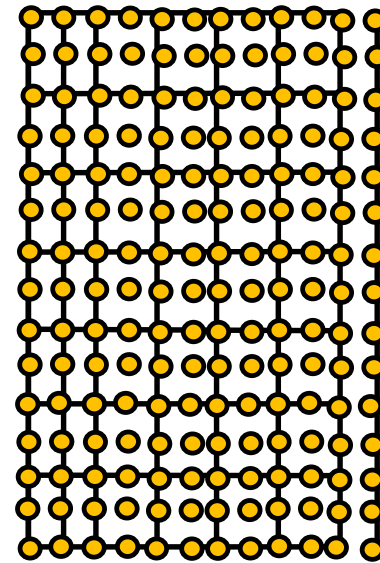
Long ducts comparison

	REG [Pa]	Duct 75 l [Pa]		REG [Pa]	Duct 75 l [Pa]		REG [Pa]	Duct 75 l [Pa]
1	9.8	10.3	6	14.4	14.9	11	8.8	9.0
2	12.8	13.2	7	8.2	8.5	12	10.6	10.8
3	15.1	15.8	8	10.9	11.3	13	4.1	4.1
4	9.2	9.8	9	12.8	13.3	14	5.5	5.7
5	12.1	12.8	10	6.5	6.8	15	6.8	7.0

Noise Field Studies – Nearfield Acoustic Holography

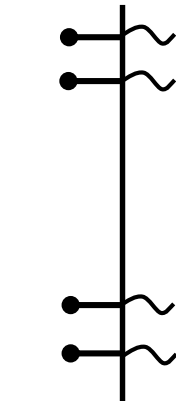
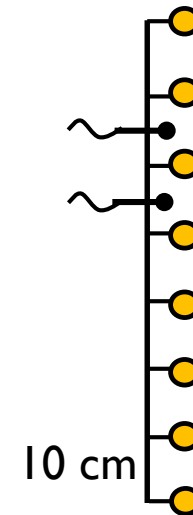


Side-View



16 x 12
Microphone
Array

Top-View



Reference
Microphones

- Distance between the array microphones were filled by physical interpolation of the array.

Multi-reference Nearfield Acoustic Holography procedure

1. Measure the pressure field with array Microphones.

$$\mathbf{p} = \mathbf{H}_{pr} \mathbf{r}$$

$$\begin{bmatrix} p_1 \\ p_2 \\ \vdots \\ p_N \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} & \dots & h_{1M} \\ h_{21} & h_{22} & \dots & h_{2M} \\ \vdots & \vdots & \ddots & \vdots \\ h_{N1} & h_{N2} & \dots & h_{NM} \end{bmatrix} \begin{bmatrix} r_1 \\ r_2 \\ \vdots \\ r_M \end{bmatrix}$$

$\mathbf{p} \qquad \mathbf{H}_{pr} \qquad \mathbf{r}$

N: Number of signals on the measurement surface
M: Number of reference signals

2. Cross-spectra between measurement surface and reference signals

$$\mathbf{S}_{pr} = \mathbf{p} \mathbf{r}^H = \mathbf{H}_{pr} \mathbf{S}_{rr}$$

3. Decompose reference cross-spectra \mathbf{S}_{rr} using Singular Value Decomposition method

$$\mathbf{S}_{rr} = \mathbf{V} \mathbf{\Sigma} \mathbf{V}^H \quad \mathbf{V} : \text{Unitary matrix}$$

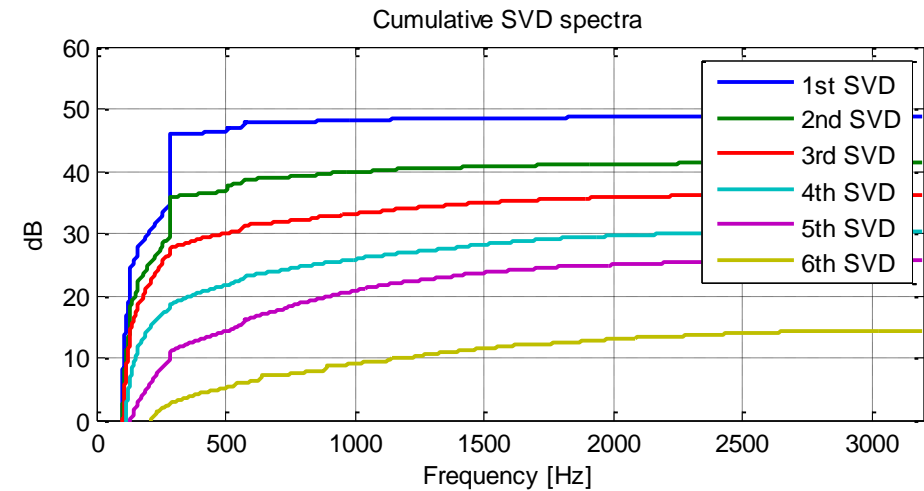
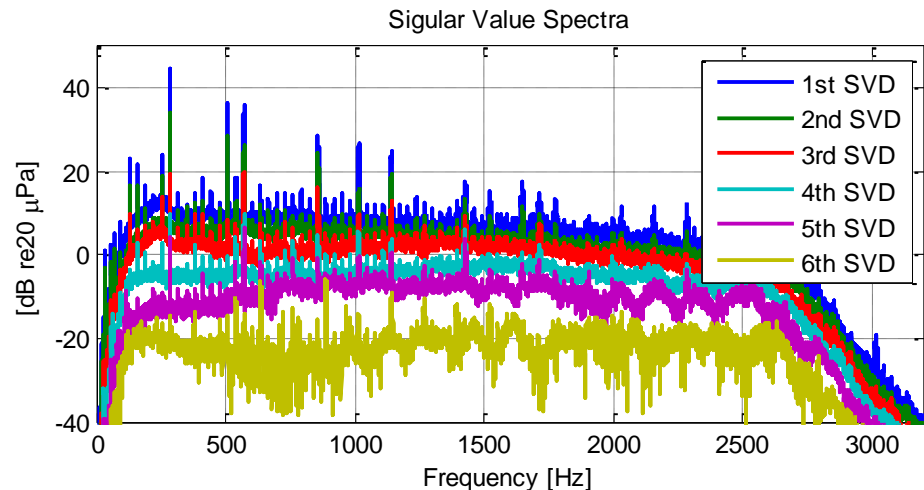
$$\mathbf{H}_{pr} = \mathbf{S}_{rp}^H \mathbf{V} \mathbf{\Sigma}^{-1} \mathbf{V}^H \quad \rightarrow \quad \mathbf{S}_{pp} = \mathbf{H}_{pr} \mathbf{S}_{rp} = \mathbf{H}_{pr} \mathbf{S}_{rr} \mathbf{H}_{pr}^H$$

4. Partial field

$$\mathbf{p} = \mathbf{H}_{pr} \mathbf{V} \mathbf{\Sigma}^{1/2} = \mathbf{S}_{rp}^H \mathbf{V} \mathbf{\Sigma}^{-1/2}$$

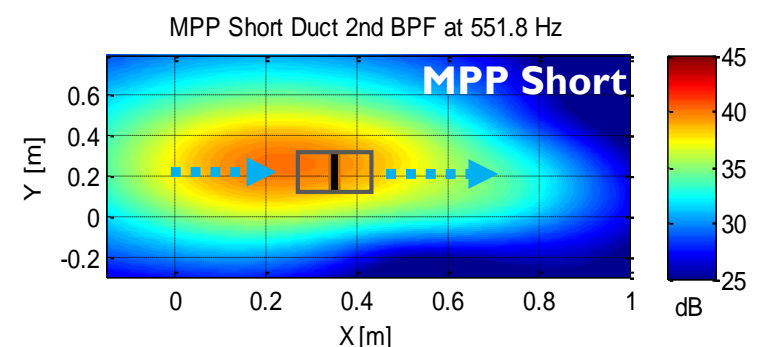
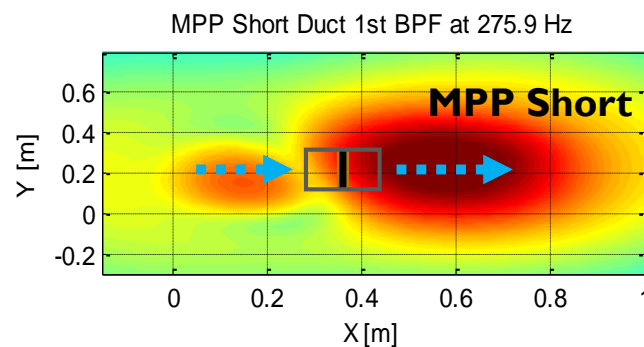
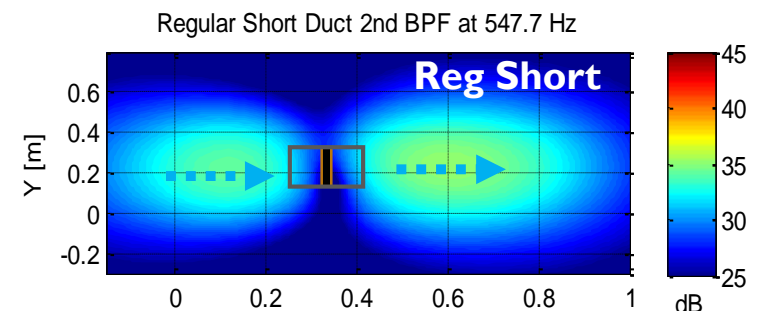
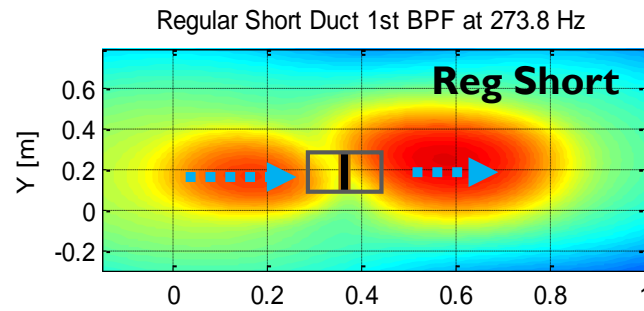
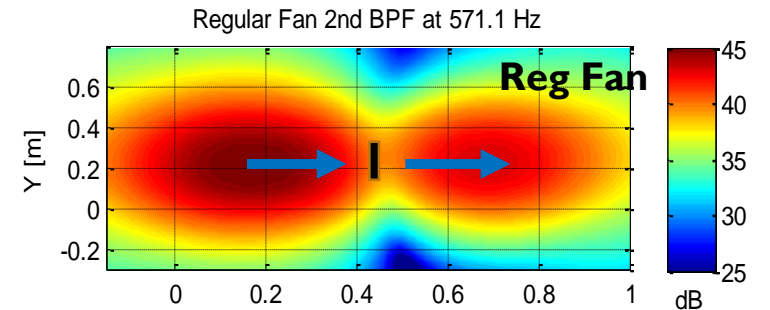
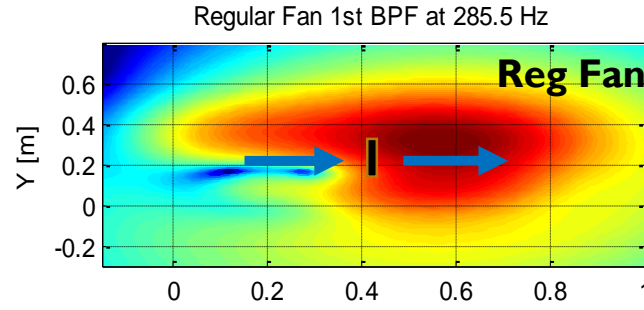
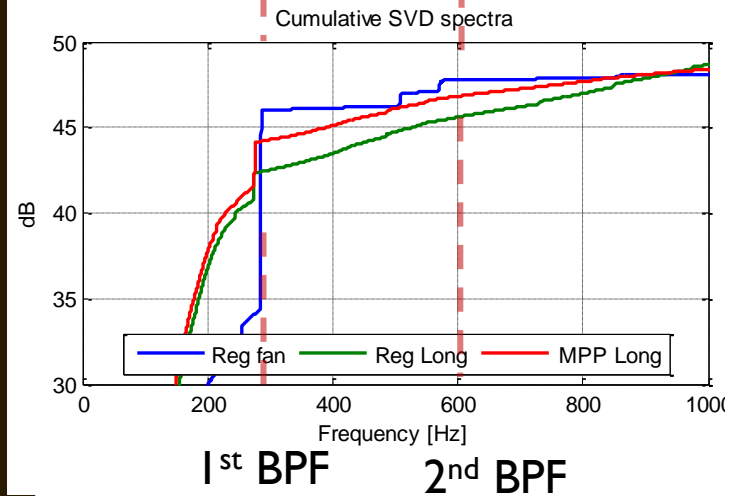
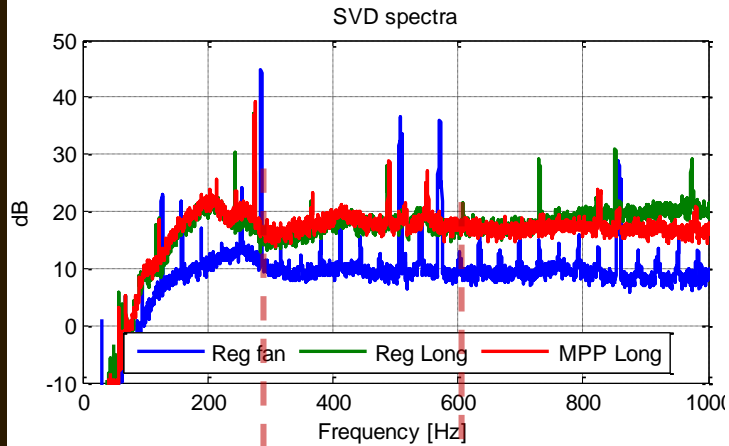
5. Planar Nearfield Acoustic Holography method & Wavenumber filtering applied

Singular Value Spectra

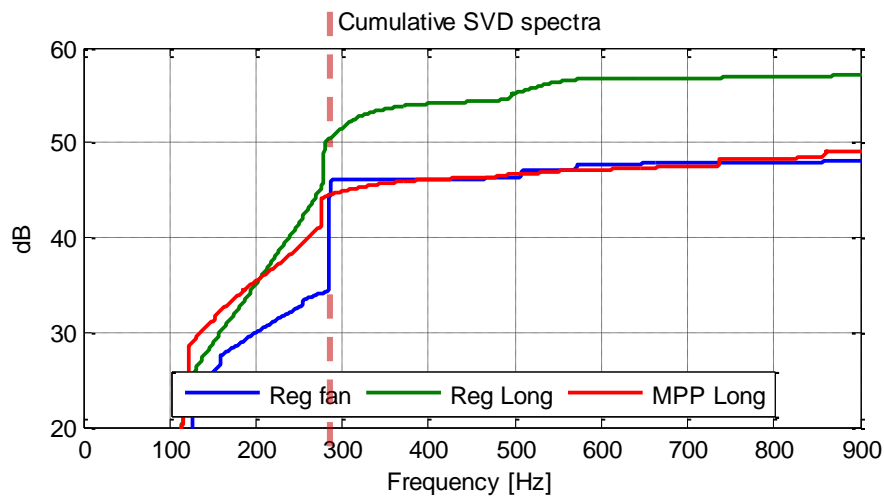
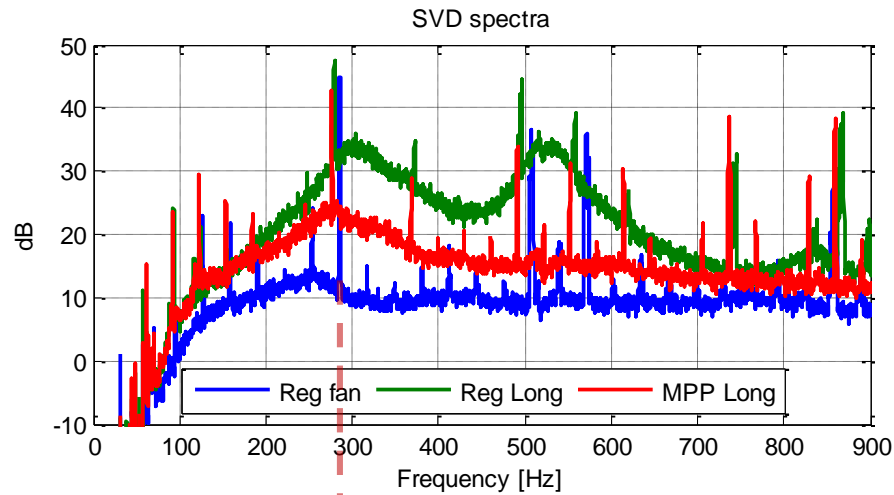


- Singular Value Spectra of Regular Fan.
- Dominant 1st SVD spectrum.
- Partial Noise Field will be provided using 1st SVD Spectra for each duct casing.

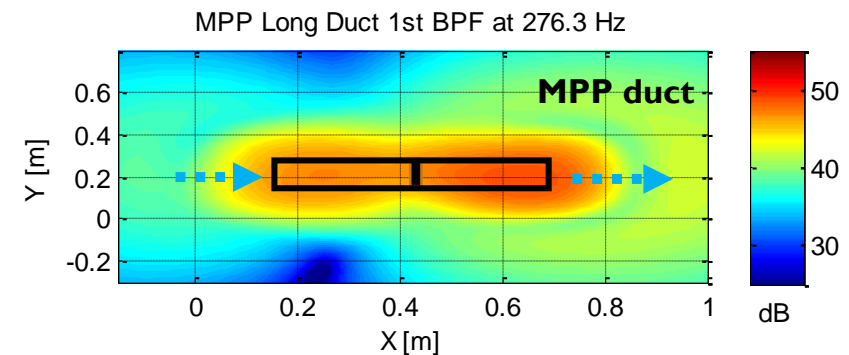
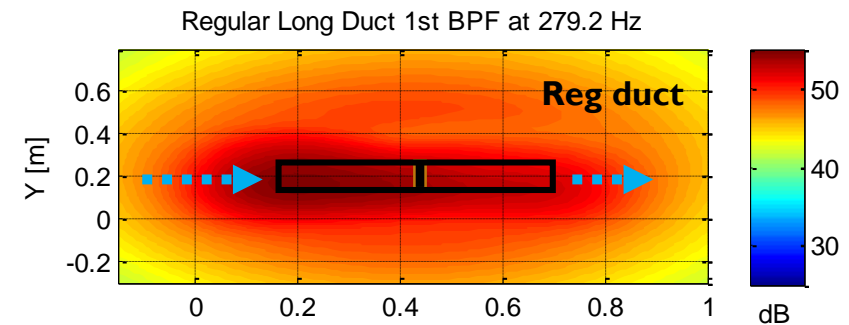
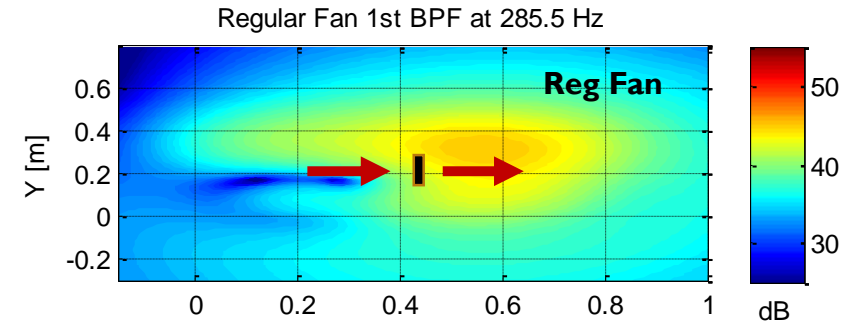
Short ducts at Blade Passage Frequencies



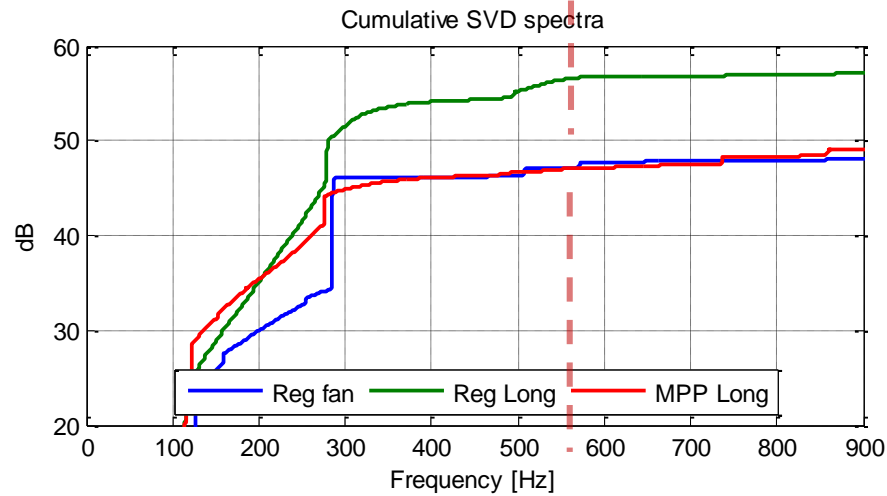
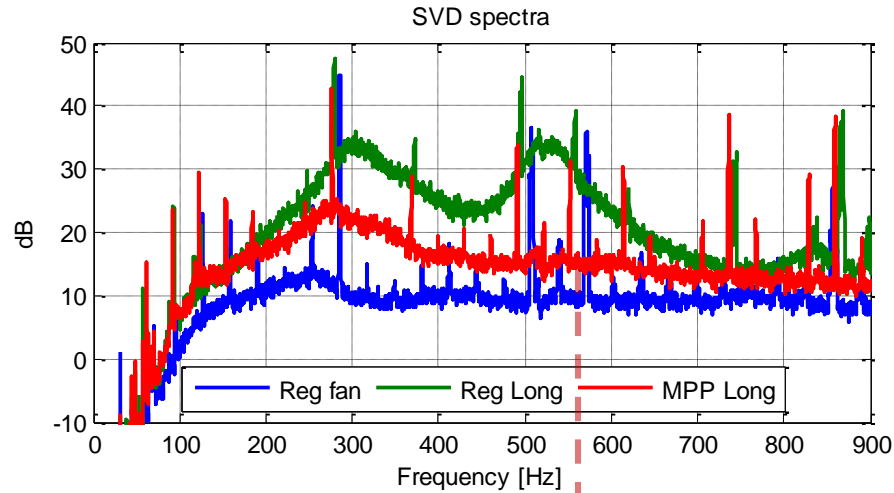
Sound fields of Long ducts at 1st BPF



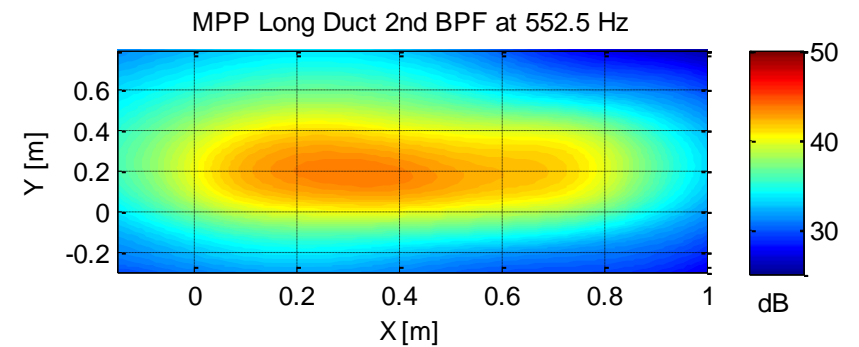
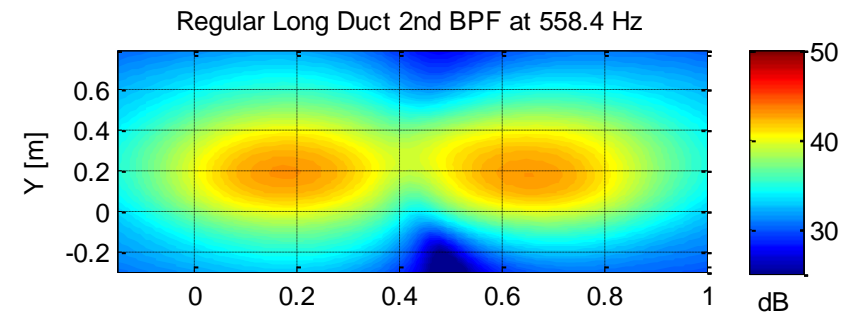
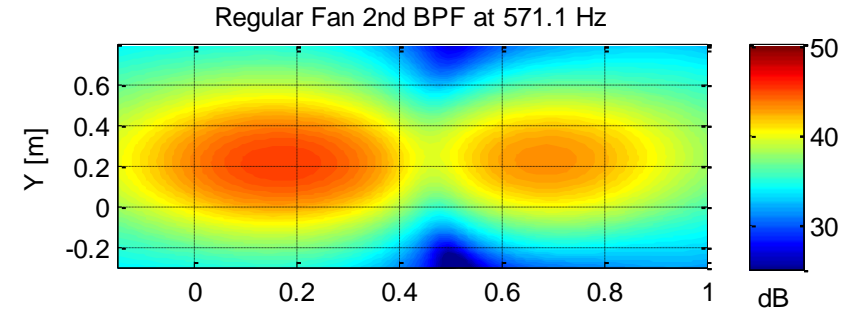
1st BPF



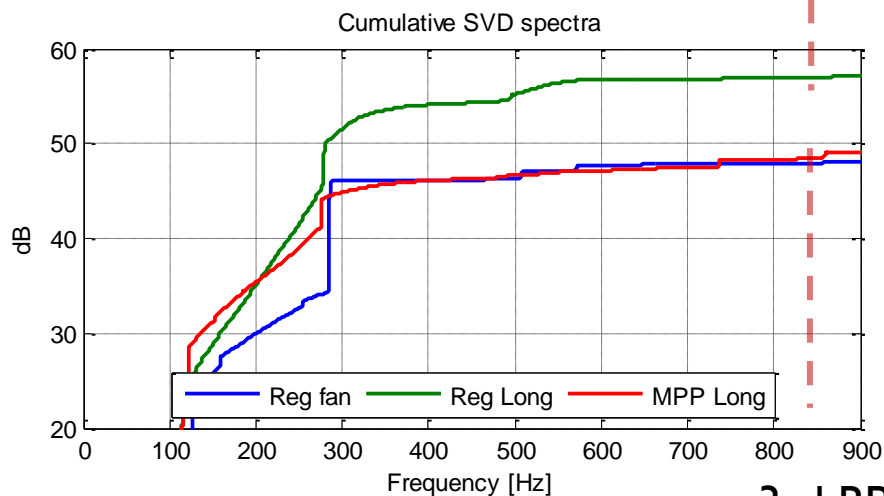
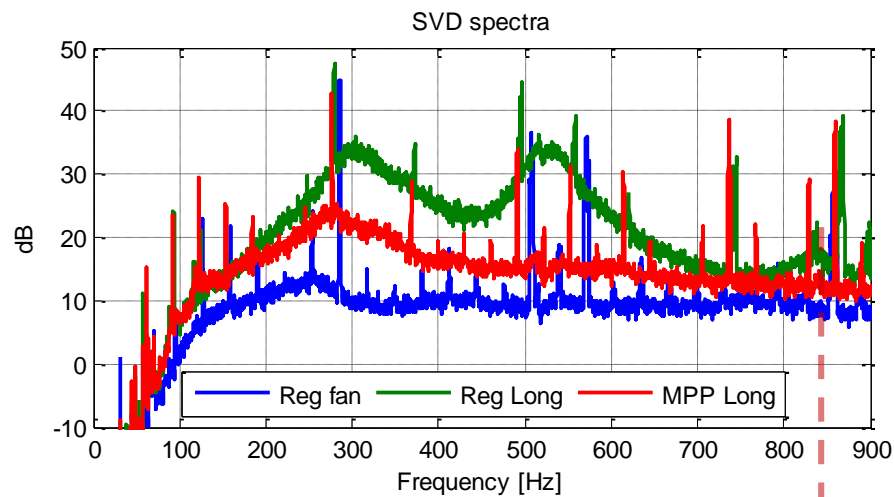
Sound fields of Long ducts at 2nd BPF



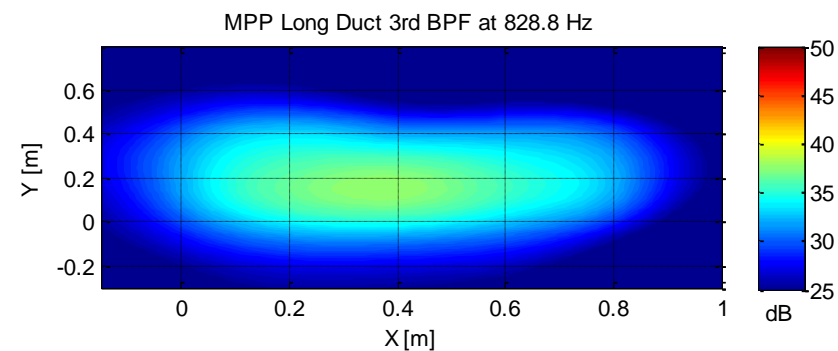
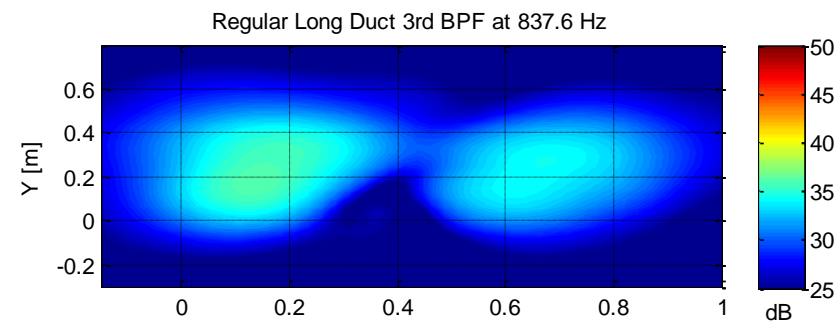
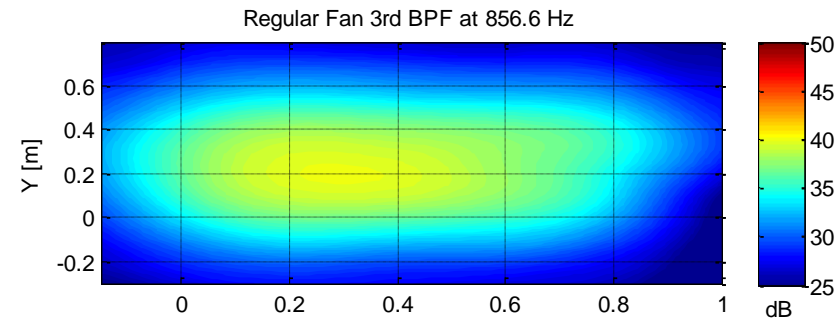
2nd BPF



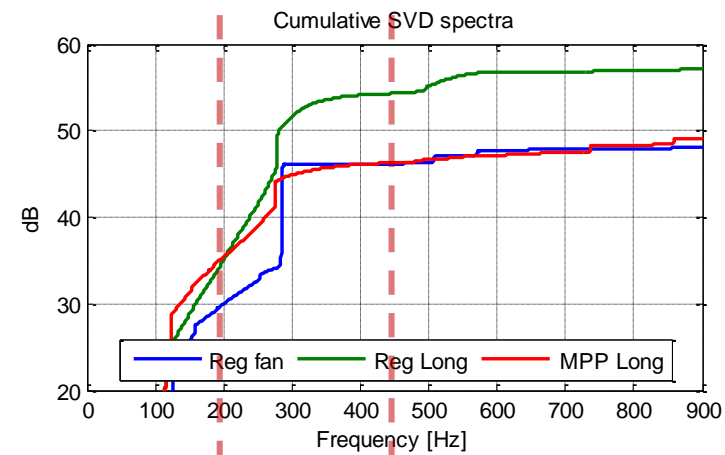
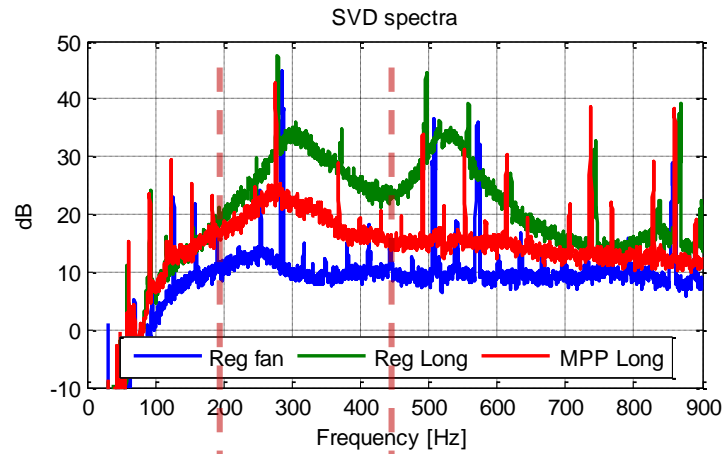
Sound fields of Long ducts at 3rd BPF



3rd BPF

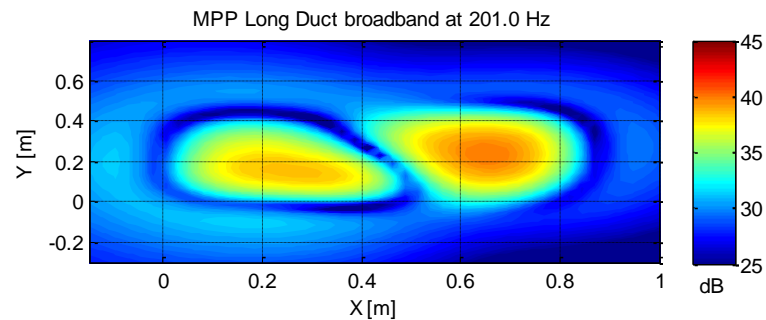
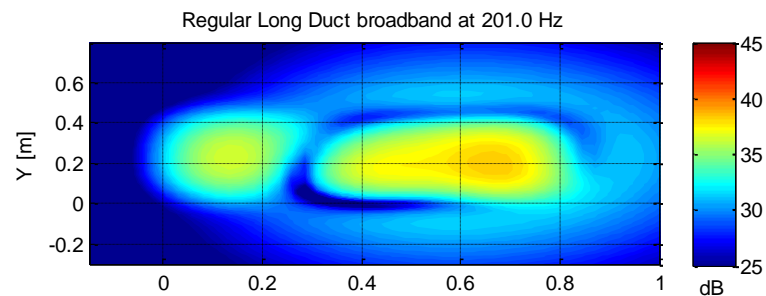
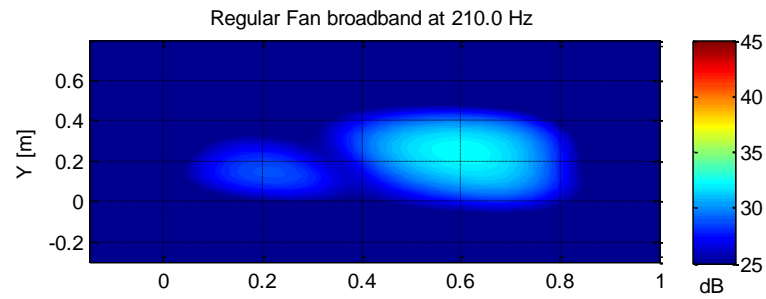


Broadband regions of Long ducts

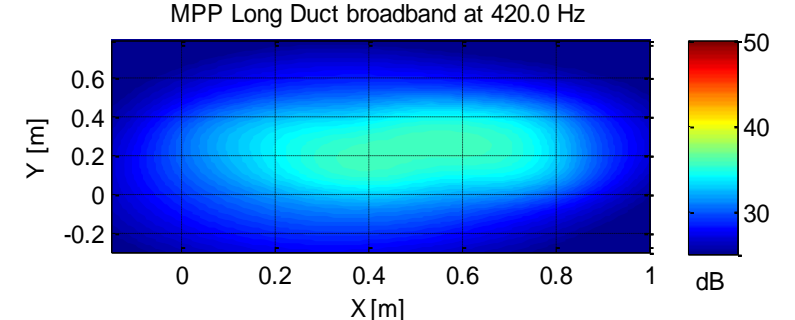
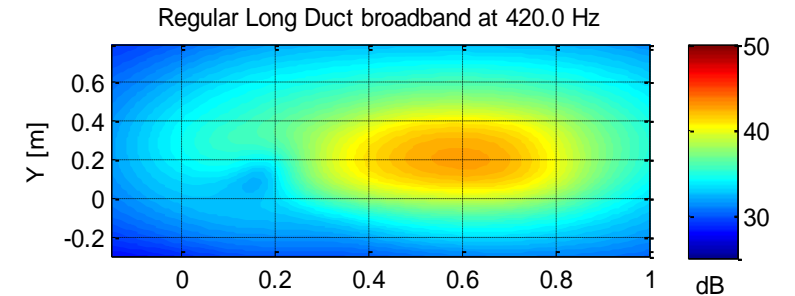
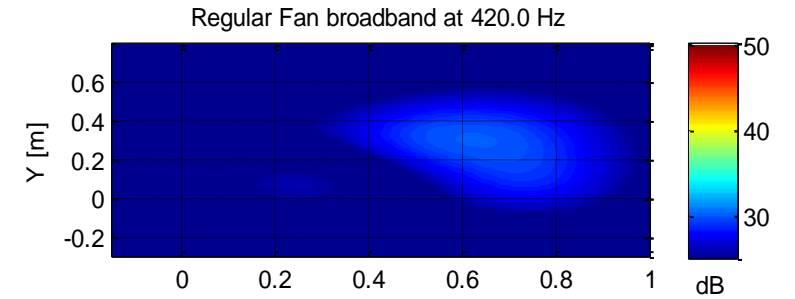


200 Hz 420 Hz

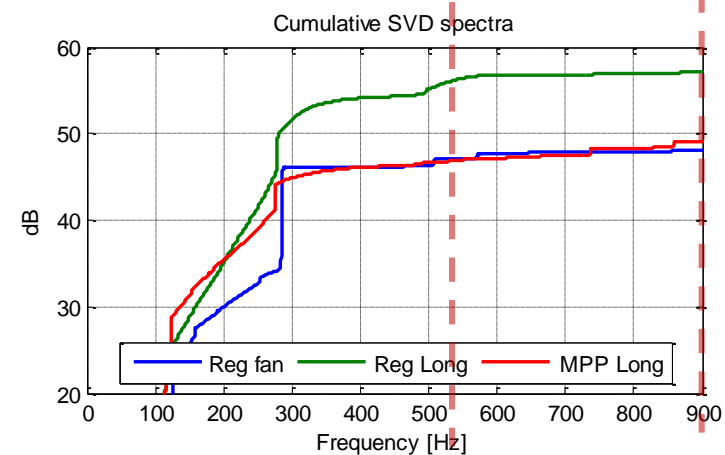
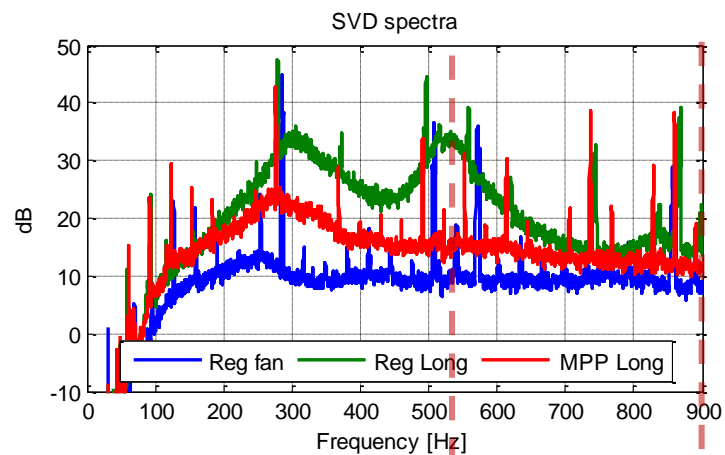
200 Hz



420 Hz

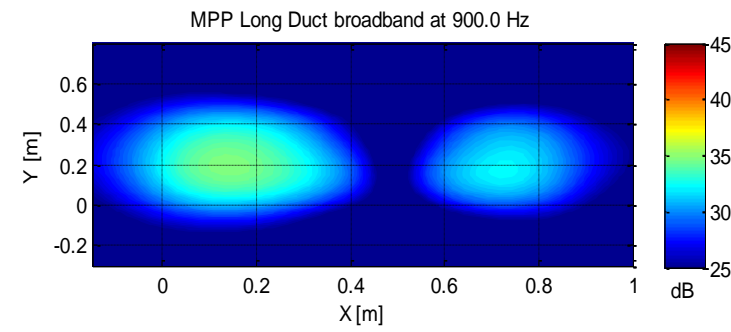
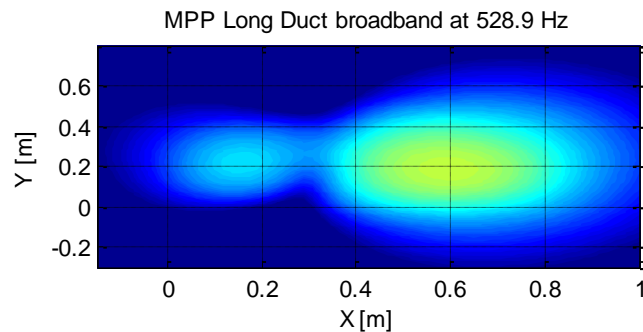
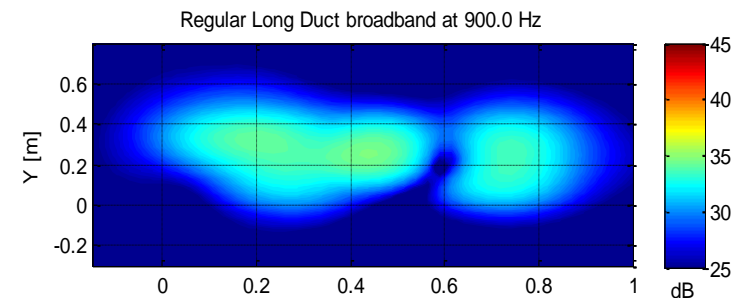
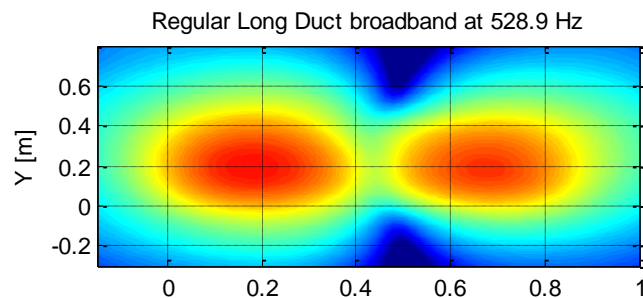
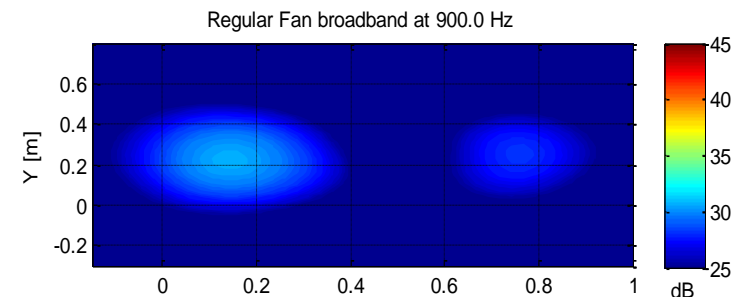
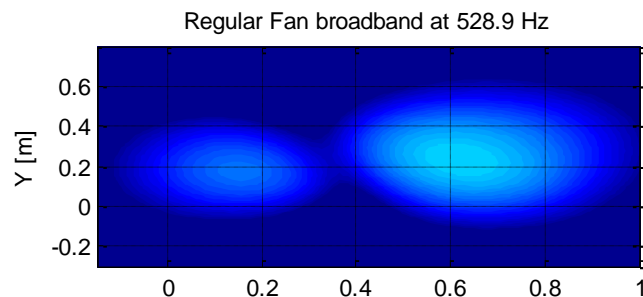


Broadband regions of Long ducts



528.9Hz

900 Hz



Conclusion & Future Plan

- Sound power radiation from the fans with impermeable duct and microperforated duct were measured and compared. Moreover, the sound field around the ducted fans with different materials were visualized using the nearfield acoustic holography method.
- Proper length should be selected when using microperforated material as a duct material because there should have enough distance to dissipate sound wave as the wave travel through the duct.
 - Long impermeable duct increased the noise level of the regular fan but this noise level can be reduced by replacing the duct with the same length of long MPP duct.
- The microperforated duct could provide better performance in flow transfer and static pressure generation compared to the impermeable duct.
- Different inlet and outlet length combinations of the ducted fan will be considered.
- Resonant fan scroll housing will be considered.