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Midwest Guardrail System With Southern Yellow Pine Posts

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MIDWEST GUARDRAIL SYSTEM (MGS)

WITH SOUTHERN YELLOW PINE

POSTS

Submitted by

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wood posts. However, Southern Ye The goal of this research was to ev long (152-mm x 203-mm x 1,829-n in. x 8-in. x 72-in. long (152-mm x with SYP posts would likely be s	How Pine (SYP) is the most com aluate the MGS with rectangular mm) rectangular White Pine post v & 203-mm x 1,829-mm) Southern uccessful, but full-scale crash te	n approved for use with various alternative species of mon wood guardrail post material in the United States. SYP posts. In a previous test, the 6-in. x 8-in. x 72-in. was found to have 39 percent lower capacity than the 6- Yellow Pine post. This result indicated that the MGS esting was deemed useful to verify satisfactory safety under Manual for Assessing Safety Hardware (MASH)

TL-3 test conditions.

The MGS was crash tested with 6-in. x 8-in. x 72-in. long (152-mm x 203-mm x 1,829-mm) Southern Yellow Pine posts. This system also used a 6-in. x 12-in. x 14¹/4-in. long (152-mm x 305-mm x 362-mm) blockout as well as 12-gauge (2.66-mm) guardrail sections. The design was evaluated using a small car (test no. 3-10) and a pickup truck (test no. 3-11) according to the testing standards established in the MASH. The MGS with Southern Yellow Pine posts met the MASH safety requirements for both full-scale crash tests. Following the full-scale crash testing, recommendations were given regarding the use of SYP posts in special MGS applications.

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This report was completed with funding from the Federal Highway Administration, U.S. Department of Transportation. The contents of this report reflect the views and opinions of the authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the state highway departments participating in the Midwest States Regional Pooled Fund Program nor the Federal Highway Administration, U.S. Department of Transportation. This report does not constitute a standard, specification, regulation, product endorsement, or an endorsement of manufacturers.

UNCERTAINTY OF MEASUREMENT STATEMENT

The Midwest Roadside Safety Facility (MwRSF) has determined the uncertainty of measurements for several parameters involved in standard full-scale crash testing and non-standard testing of roadside safety features. Information regarding the uncertainty of measurements for critical parameters is available upon request by the sponsor and the Federal Highway Administration.

INDEPENDENT APPROVING AUTHORITY

The Independent Approving Authority (IAA) for the data contained herein was Scott Rosenbaugh, Research Associate Engineer.

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1 INTRODUCTION

1.1 Problem Statement

The Midwest Guardrail System (MGS) is a non-proprietary, strong post, W-beam barrier composed of W6x9 or W6x8.5 steel posts or wood guardrail posts, 12-gauge (2.66-mm) W-beam rail, and a 12-in. (305-mm) deep blockout. The MGS has been evaluated under the safety criteria of both the National Cooperative Highway Research Program (NCHRP) Report No. 350 [1] and the *Manual for Assessing Safety Hardware (MASH)* [2] under Test Level 3 (TL-3) impact conditions. Subsequently, the Federal Highway Administration (FHWA) deemed the MGS eligible for reimbursement under the Federal-Aid Highway Program. However, the MGS had never been tested with rectangular Southern Yellow Pine (SYP) wood posts to evaluate the working width and dynamic deflection of the system. Being that rectangular SYP posts are the most commonly used wood guardrail posts in the United States, it was proposed that an evaluation of the MGS with SYP posts would prove beneficial for many State Departments of Transportation (DOTs).

The MGS was previously tested and approved for use with several wood post variations. The MGS has been successfully tested with both alternative wood species round posts [3] and 6in. x 8-in. x 72-in. long (152-mm x 203-mm x 1829-mm) rectangular White Pine (WP) posts [4]. WP posts have approximately 39 percent lower capacity than standard SYP wood posts [5]. The Midwest Roadside Safety Facility (MwRSF) performed a crash test under MASH test designation no. 3-11 on the MGS with WP posts. The 2270P vehicle was smoothly redirected in test no. MGSWP-1, and six posts fractured or split [5]. Although test no. MGSWP-1 was a good indicator that the MGS would perform well with SYP posts, the Midwest Pooled Fund Program members desired to obtain the actual system behavior (e.g., dynamic deflection and working width) for a SYP wood post MGS.

1.2 Objective

The objective of this research effort was to evaluate the safety performance of the MGS with 6-in. x 8-in. x 72-in. long (152-mm x 203-mm x 1829-mm) SYP posts according to the TL-3 full-scale crash testing criteria set forth in MASH.

1.3 Scope

The research objective was achieved through the completion of several tasks. First, two full-scale crash tests were conducted on the MGS with SYP wood posts. The crash tests utilized a pickup truck and a small car, weighing approximately 5,000 lb (2,268 kg) and 2,425 lb (1,100 kg), respectively. The target impact conditions for both tests were an impact speed of 62 mph (100 km/hr) and an impact angle of 25 degrees. Next, the test results were analyzed, evaluated, and documented. Finally, conclusions and recommendations were made that pertain to the safety performance of the MGS with SYP posts.

2 DESIGN DETAILS

The test installation consisted of 181 ft - 3 in. (55.3 m) of standard 12-gauge (2.66-mm) W-beam supported by SYP wood posts, as shown in Figure 1. Anchorage systems similar to those used on tangent guardrail terminals were utilized on both the upstream and downstream ends of the guardrail system. Design details are shown in Figures 1 through 10. Photographs of the test installations are shown in Figures 11 and 12. Material specifications, mill certifications, and certificates of conformity for the component materials are shown in Appendix A.

The system was constructed with twenty-nine wood posts spaced at 75 in. (1,905 mm) on center, as shown in Figures 1 and 2. Post nos. 3 through 27 were 6-in. x 8-in. x 72-in. long (152mm x 203-mm x 1,829-mm) Grade 1 SYP wood posts with a soil embedment depth of 40 in. (1,016 mm). A 6-in. wide x 12-in. deep x 14¹/₄-in. long (152-mm x 305-mm x 362-mm) wood spacer blockout was used to block the rail away from the front face of each steel post. A 16D double head nail was also driven through a hole in the front flange of the post into the top of the blockout assembly to prevent rotation of the blockout. Post nos. 1, 2, 28, and 29 were breakaway cable terminal (BCT) timber posts measuring $5\frac{1}{2}$ in. wide x $7\frac{1}{2}$ in. deep x 46 in. long (140 mm x 191 mm x 1,168 mm) and were placed in 6-ft (1.8-m) long foundation tubes, as shown in Figure 6. A tangent anchorage system was utilized on the upstream and downstream ends of the guardrail system in order to develop the barrier's tensile capacity. The anchorage system consisted of timber posts, foundation tubes, anchor cables, bearing plates, rail brackets, and channel struts, which closely resembled the hardware used in the Modified BCT system. As such, this system is believed to be representative of existing guardrail terminal end anchorages. All posts were placed in a compacted coarse, crushed limestone material.

Standard 12-ft 6-in. (3.81-m) long 12-gauge (2.66-mm) W-beam rails with additional post bolt slots at half-post spacings were placed between post nos. 1 and 29, as shown in Figures

1, 2, and 9. Standard splice bolts, $\frac{5}{8}$ x 22 in. (M16x559) long guardrail bolt and nuts, were used to attach the rail to the posts. The W-beam's top rail height for MGSSYP-1 was 31 in. (787 mm) with a 24%-in. (632-mm) center mounting height. The rail splices were placed at midspan locations, as shown in Figures 1 and 2. All lap-splice connections between the rail sections were configured with the upstream segment in front to minimize vehicle snag at the splice during the crash test.

The installation for test no. MGSSYP-2 was raised 1 in. (25 mm) such that the height to the top of the guardrail was 32 in. (813 mm), as shown in Figures 13 through 22. Photographs of the test installation for test no. MGSSYP-2 are shown in Figure 23.

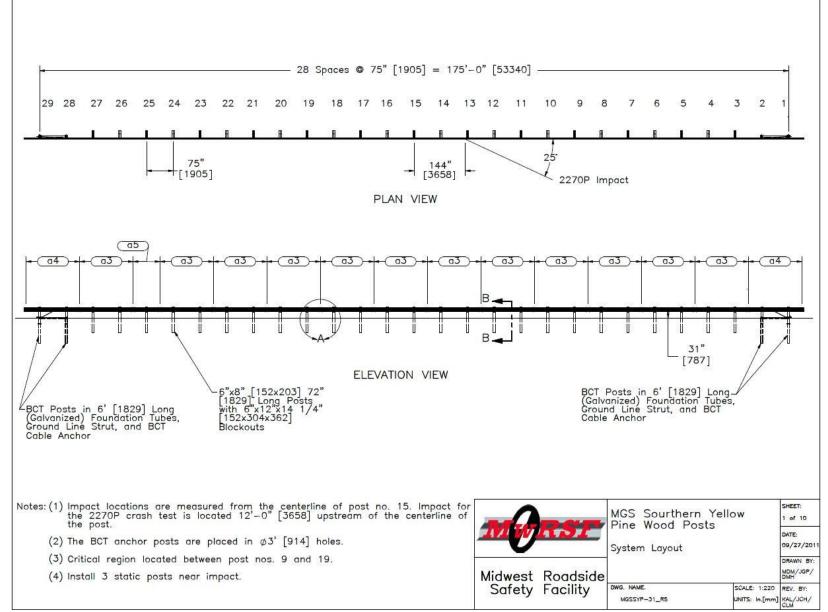


Figure 1. Test Installation Layout, Test No. MGSSYP-1

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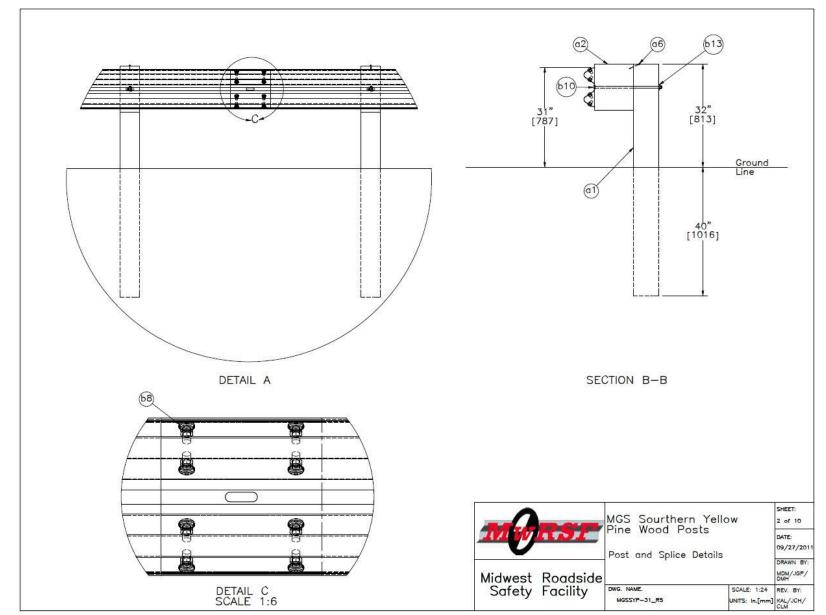


Figure 2. Post and Splice Details, Test No. MGSSYP-1

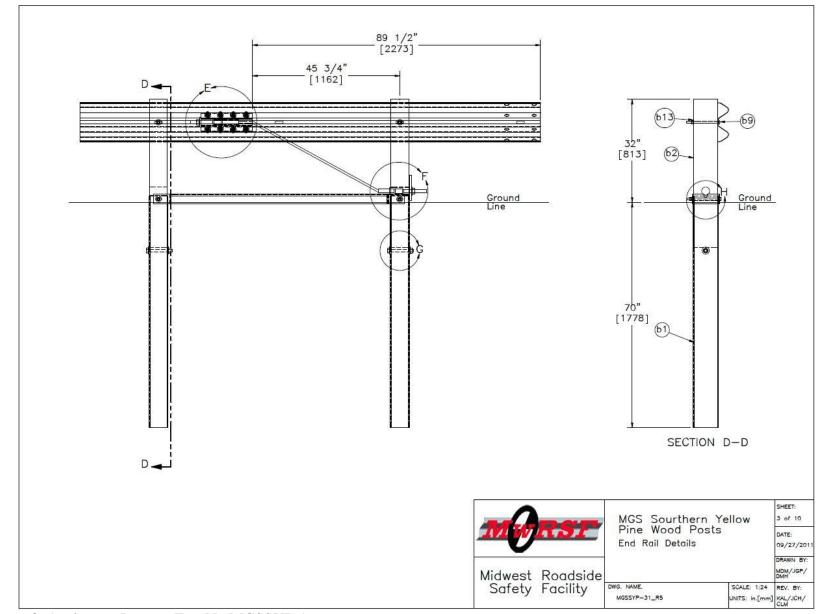


Figure 3. Anchorage Layout, Test No.MGSSYP-1

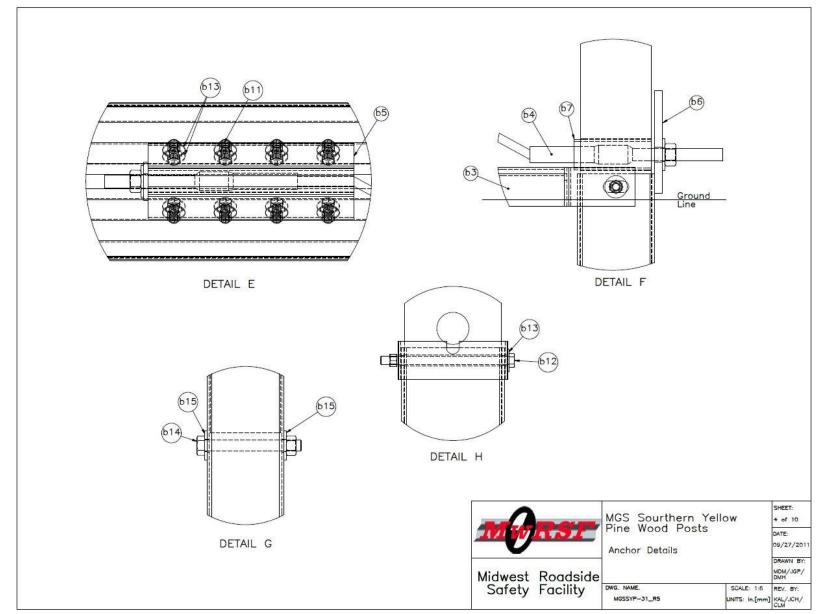


Figure 4. Anchorage Component Details, Test No. MGSSYP-1

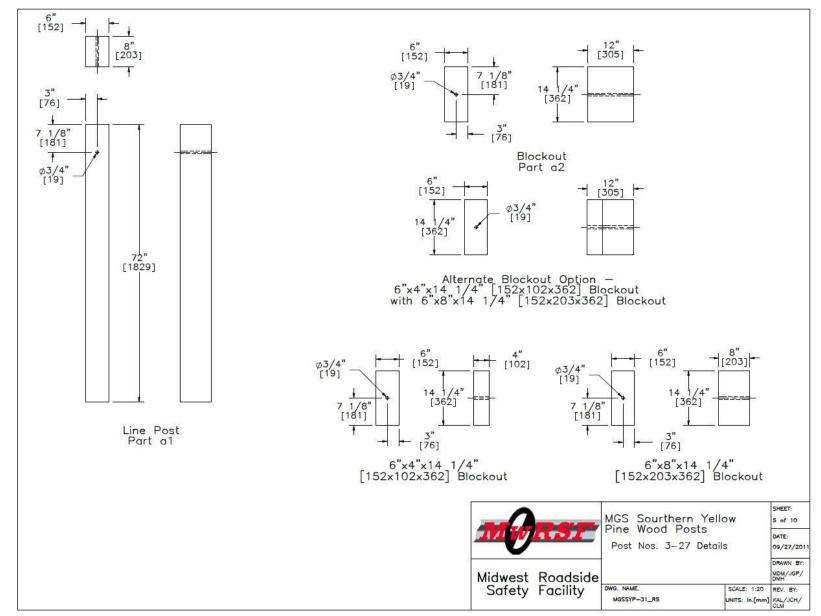


Figure 5. Post nos. 3 through 27 and Blockout Details, Test No. MGSSYP-1

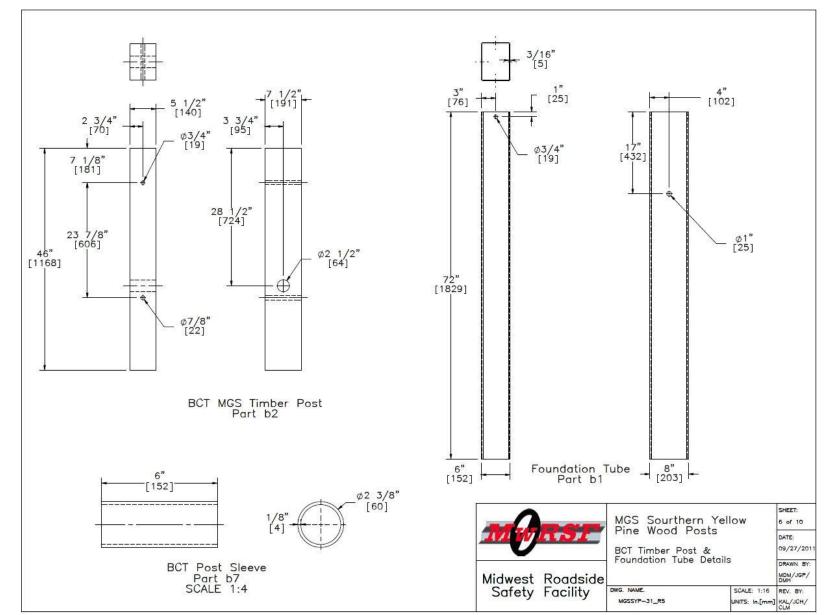


Figure 6. BCT Timber Post and Foundation Tube Details, Test No. MGSSYP-1

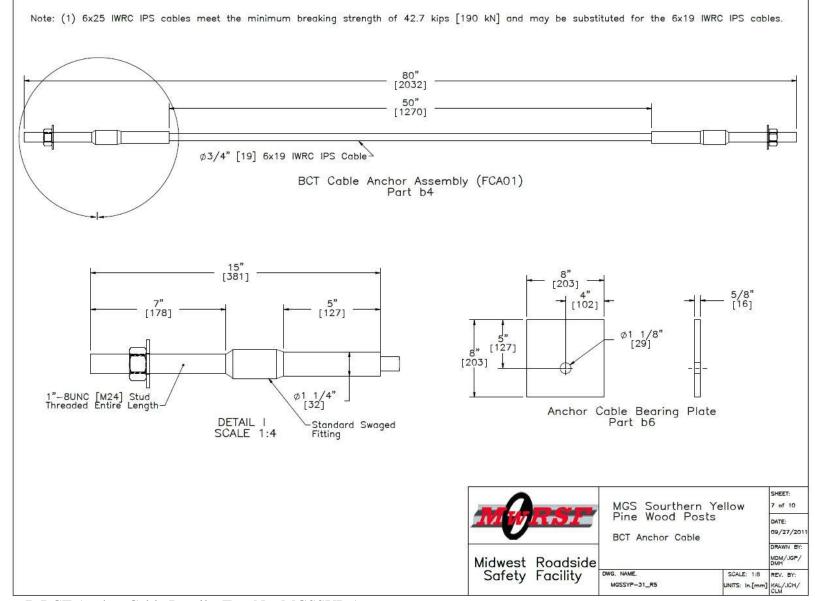


Figure 7. BCT Anchor Cable Details, Test No. MGSSYP-1

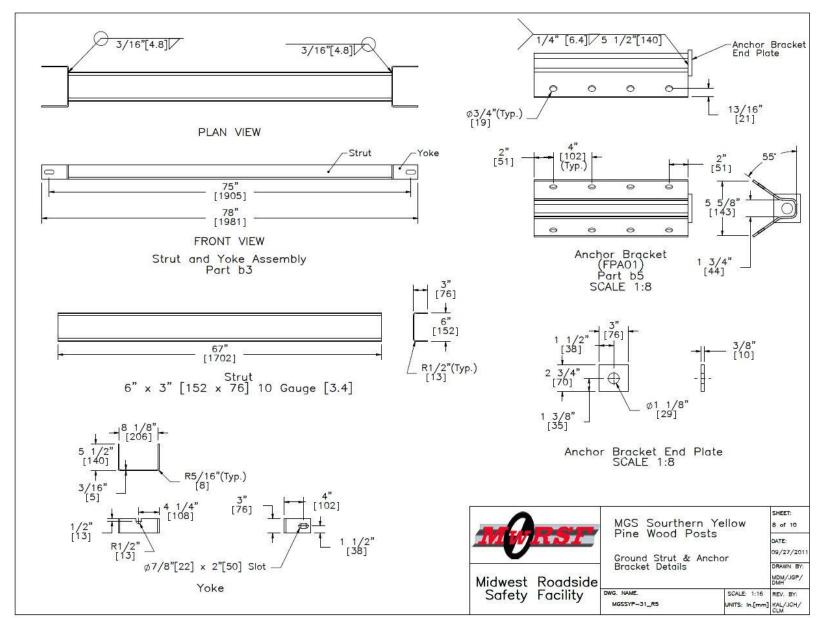


Figure 8. Ground Strut and Anchor Bracket Details, Test No. MGSSYP-1

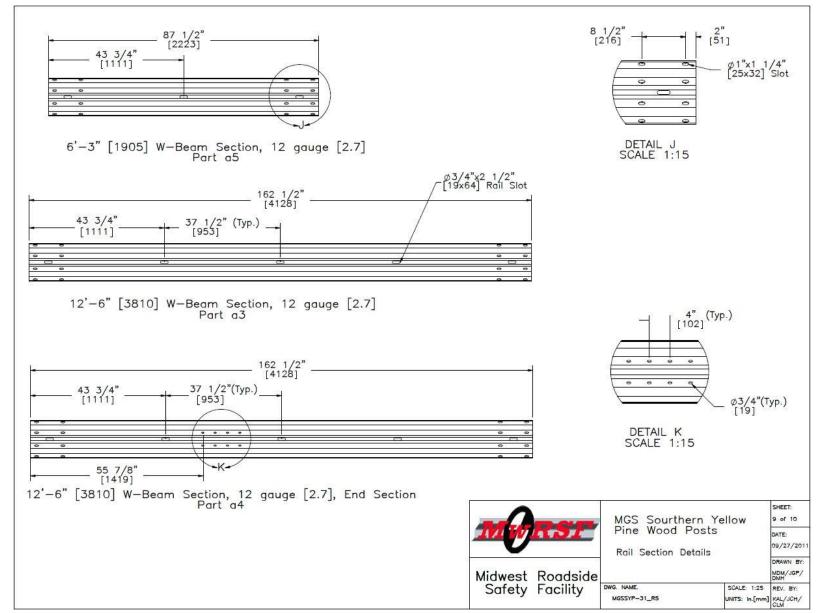


Figure 9. Rail Section Details, Test No. MGSSYP-1

Item No.	QTY.	Description	Material Specification	Hardware Guide
a1	25	6"x8"x72" [152x203x1829] Southern Yellow Pine Wood Post	SYP Grade No.1 or better	PDE02
α2	25	6"x12"x14 1/4" [152x305x362] MGS Timber Blockout	SYP Grade No.1 or better	PDB11a
a3	12	12'-6" [3810] 4-Space W-Beam Guardrail	12 gauge [2.7] AASHTO M180	RWM04a
a4	2	12'-6" [3810] BCT Terminal Rail Section	12 gauge [2.7] AASHTO M180	822
a5	1	6'-3" [1905] W-Beam Spacer Guardrail	12 gauge [2.7] AASHTO M180	RWM01a
a6	25	16D Double Head Nail	<u></u>	822
b1	4	72" [1829] Long Foundation Tube	ASTM A500 Gr. B	PTE06
b2	4	BCT Timber Post-MGS Height	SYP Grade No.1 or better	PDF01
b3	2	Strut and Yoke Assembly	ASTM A36 Steel Galvanized	
b4	2	BCT Cable Anchor Assembly	Ø3/4" 6x19 IWRC IPS Galvanized Wire Rope	FCA01-0
b5	2	Guardrail Anchor Bracket	ASTM A36 Steel	
b6	2	8"x8"x5/8" [203x203x16] BCT Bearing Plate	ASTM A36 Steel	FPB01
b7	2	2 3/8" [60] O.D.x 6" [152] Long BCT Post Sleeve	ASTM A53 Grade B Schedule 40	FMM02
b8	112	5/8" Dia. x 1 1/4" [M16x32] Long Guardrail Bolt and Double Recessed Nul	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBB01
b9	4	5/8" Dia. x 10" [M16x254] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBB03
b10	25	5/8" Dia. x 22" [M16x559] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBB07
b11	16	5/8" Dia. x 1 1/2" [M16x38] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX16a
b12	4	5/8" Dia. x 9 1/2" [M16x241] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX16a
b13	69	5/8" [16] Dia. Plain Round Washer	ASTM F844 or Grade 2 Steel	FWC16a
b14	4	7/8" Dia. x 7 1/2" [M22x191] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 A	FBX22a
b15	8	7/8" [22] Dia. Plain Round Washer	ASTM F844 or Grade 2 Steel	FWC22a
			MGS Sourthern Yellow Pine Wood Posts Bill of Materials Midwest Roadside Safety Facility	

Figure 10. Bill of Materials, Test No. MGSSYP-1







Figure 11. Test Installation Photographs, Test No. MGSSYP-1





Figure 12. Test Installation Photographs, Test No. MGSSYP-1

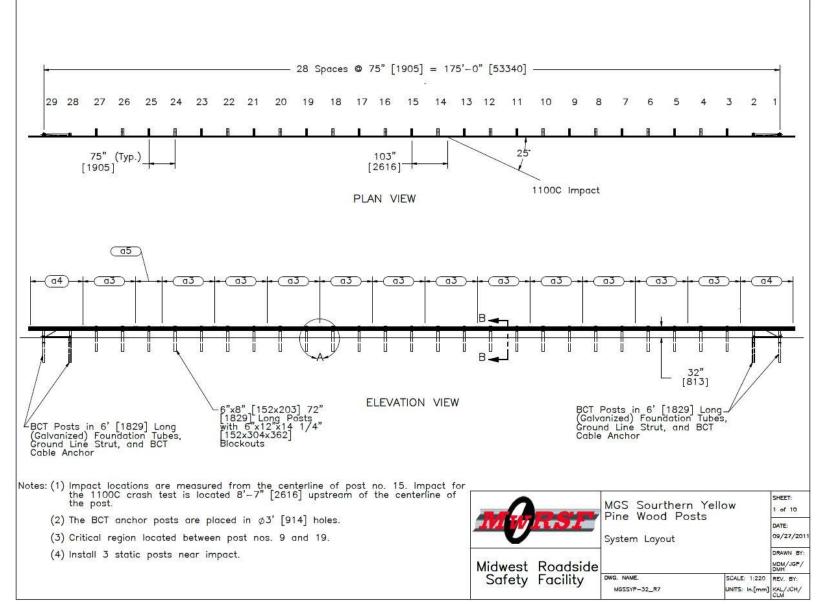


Figure 13. Test Installation Layout, Test No. MGSSYP-2

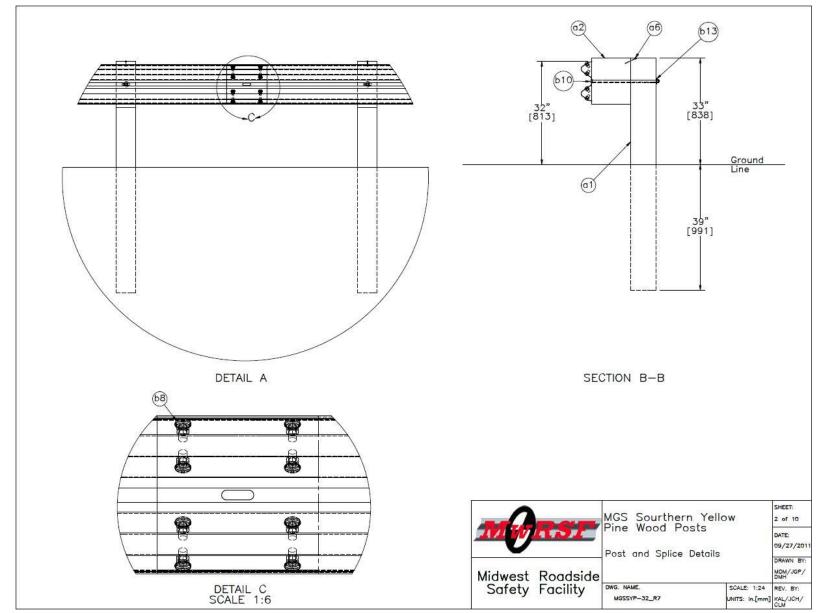


Figure 14. Post and Splice Details, Test No. MGSSYP-2

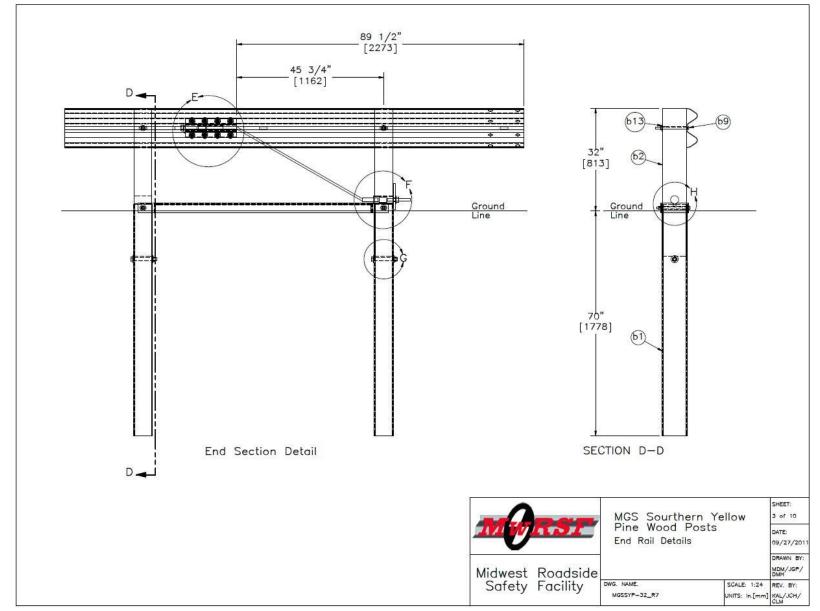


Figure 15. Anchorage Layout, Test No. MGSSYP-2

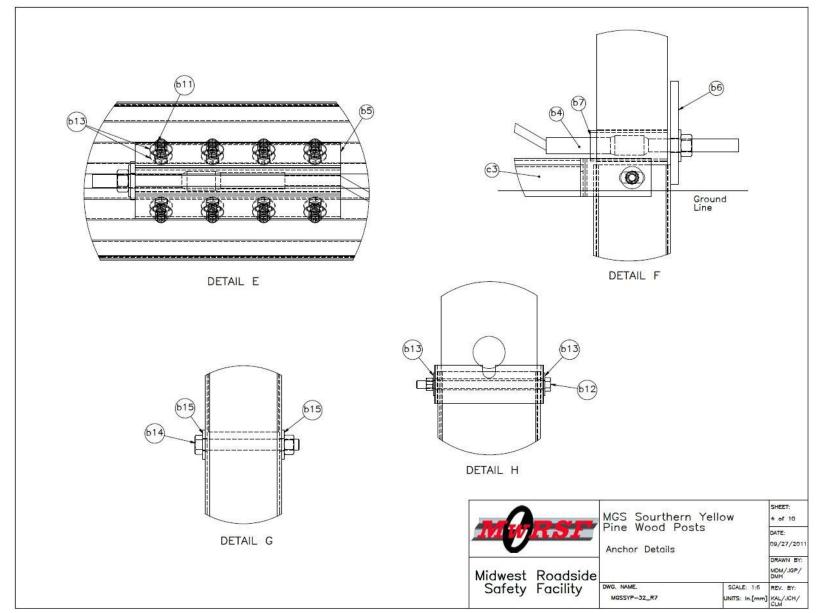


Figure 16. Anchorage Component Details, Test No. MGSSYP-2

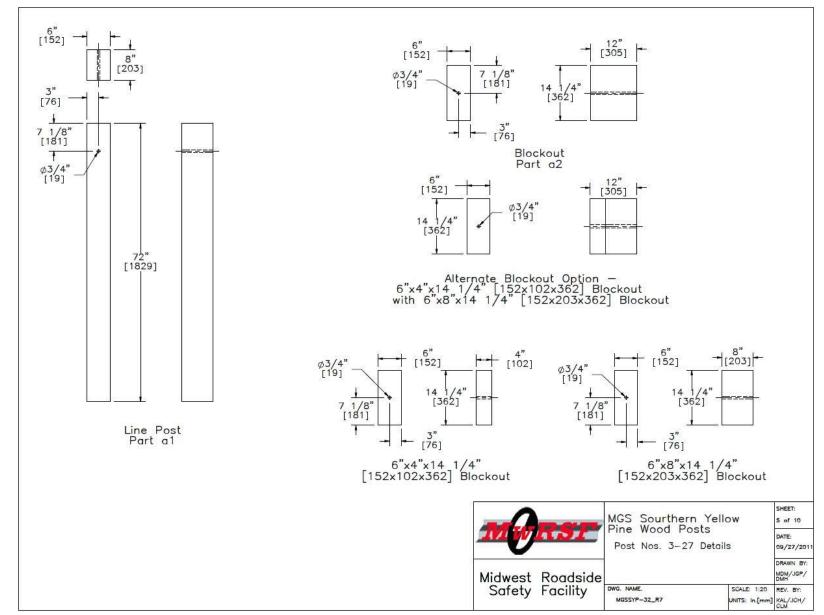


Figure 17. Post nos. 3 through 27 and Blockout Details, Test No. MGSSYP-2

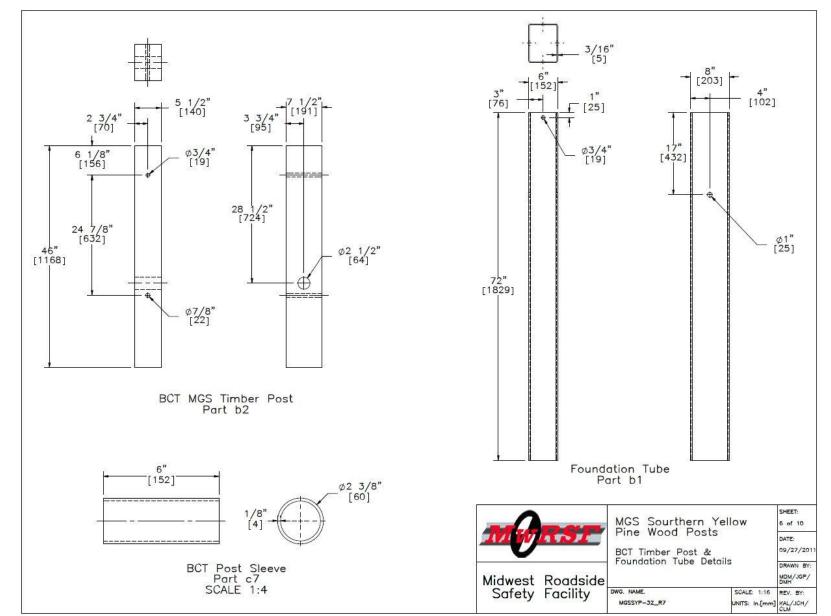


Figure 18. BCT Timber Post and Foundation Tube Details, Test No. MGSSYP-2

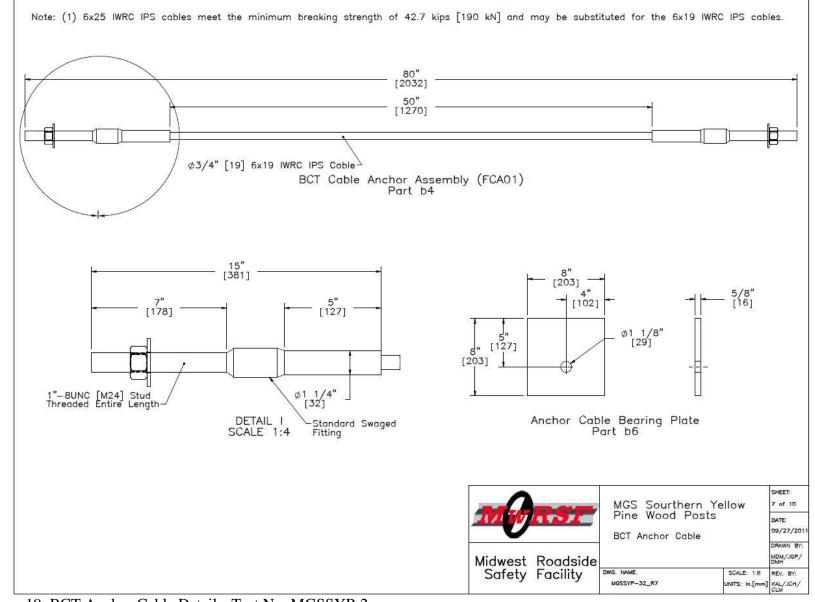


Figure 19. BCT Anchor Cable Details, Test No. MGSSYP-2

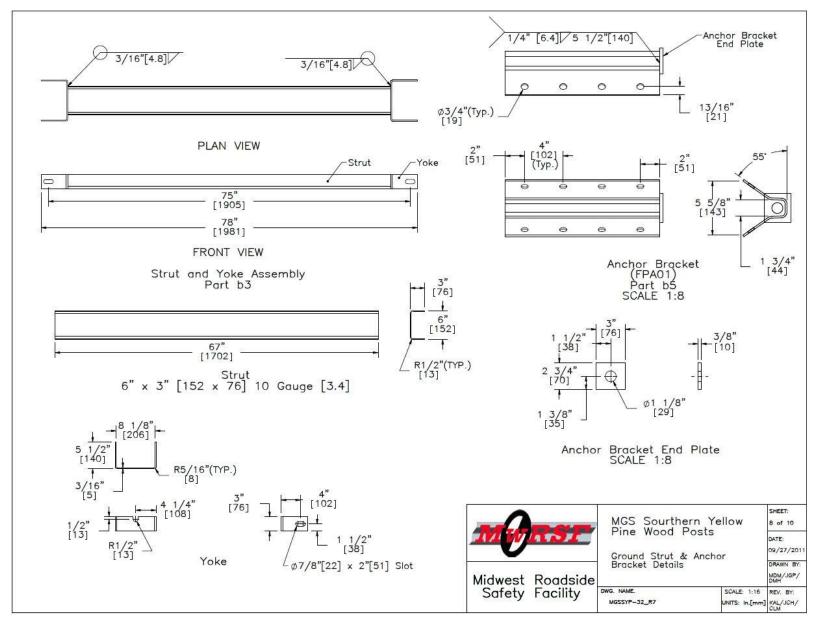


Figure 20. Ground Strut and Anchor Bracket Details, Test No. MGSSYP-2

24

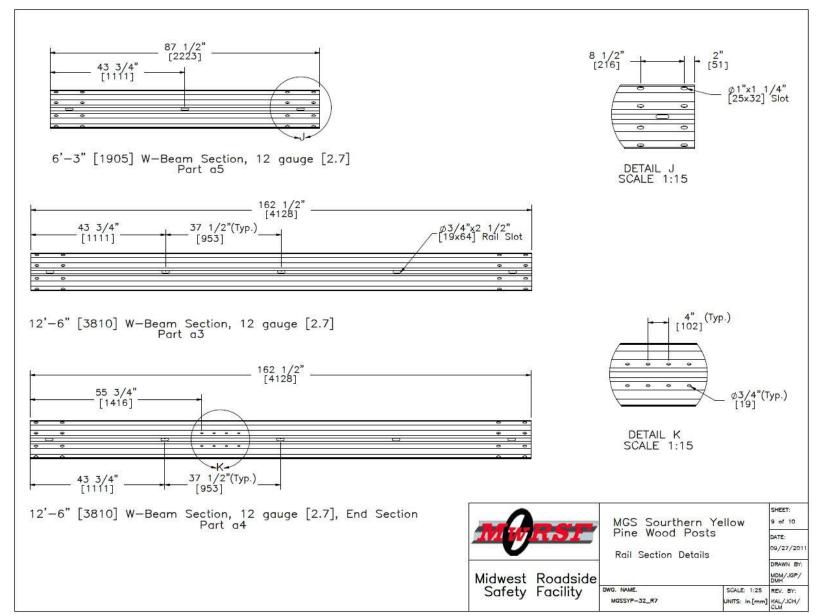


Figure 21. Rail Section Details, Test No. MGSSYP-2

25

Item No.	QTY.	Description	Material Specification	Hardware Guide		
a1	25	6"x8"x72" [152x203x1829] Southern Yellow Pine Wood Post	SYP Grade No.1 or better	PDE02		
۵2	25	6"x12"x14 1/4" [152x305x362] MGS Timber Blockout	SYP Grade No.1 or better	PDB11a		
۵3	12	12'-6" [3810] 4-Space W-Beam Guardrail	12 gauge [2.7] AASHTO M180	RWM04a		
۵4	2	12'-6" [3810] BCT Terminal Rail Section	12 gauge [2.7] AASHTO M180			
۵5	1	6'-3" [1905] W-Beam Spacer Guardrail	12 gauge [2.7] AASHTO M180	RWM01a		
a6	25	16D Double Head Nail		-		
b1	4	72" [1829] Long Foundation Tube	ASTM A500 Gr. B	PTE06		
b2	4	BCT Timber Post-MGS Height	SYP Grade No.1 or better	PDF01		
b3	2	Strut and Yoke Assembly	ASTM A36 Steel Galvanized	-		
b4	2	BCT Cable Anchor Assembly	ϕ 3/4" 6x19 IWRC IPS Galvanized Wire Rope	FCA01-0		
b5	2	Guardrail Anchor Bracket	ASTM A36 Steel	FPA01		
b6	2 8"x8"x5/8" [203x203x16] BCT Bearing Plate ASTM A36 Steel					
b7	2	2 3/8" [60] 0.D.x 6" [152] Long BCT Post Sleeve	ASTM A53 Grade B Schedule 40	FMM02		
b8	112	5/8" Dia. x 1 1/4" [M16x32] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 /	FBB01		
b9	4	5/8" Dia. x 10" [M16x254] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 /	FBB03		
b10	25	5/8" Dia. x 22" [M16x559] Long Guardrail Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 /	FBB07		
b11	16	5/8" Dia. x 1 1/2" [M16x38] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 /	FBX16a		
b12	4	5/8" Dia. x 9 1/2" [M16x241] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 /	FBX16a		
b13	69	5/8" [16] Dia. Plain Round Washer	ASTM F844 or Grade 2 Steel	FWC16a		
b14	4	7/8" Dia. x 7 1/2" [M22x191] Long Hex Bolt and Double Recessed Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 /	FBX22a		
b15	8	7/8" [22] Dia. Plain Round Washer	ASTM F844 or Grade 2 Steel	FWC22a		
			MGS Sourthern Yellow Pine Wood Posts Bill of Materials Vidwest Roadside Safety Facility	SHEET: 10 of 10 DATE: 09/27/21 DRAWN B MDM/JGP DMH Ione REV. BY: [mm] KAL/JOH/		

Figure 22. Bill of Materials, Test No. MGSSYP-2



Figure 23. Test Installation Photographs, Test No. MGSSYP-2

3 TEST REQUIREMENTS AND EVALUATION CRITERIA

3.1 Test Requirements

Longitudinal barriers, such as W-beam guardrails, must satisfy impact safety standards in order to be accepted by the Federal Highway Administration (FHWA) for use on the National Highway System (NHS). For new hardware, these safety standards consist of the guidelines and procedures published in MASH [2]. According to TL-3 of MASH, longitudinal barrier systems must be subjected to two full-scale vehicle crash tests. The two full-scale crash tests are noted below:

- 1. Test Designation No. 3-10 consists of a 2,425-lb (1,100-kg) passenger car impacting the system at a nominal speed and angle of 62 mph (100 km/h) and 25 degrees, respectively.
- 2. Test Designation No. 3-11 consists of a 5,000-lb (2,268-kg) pickup truck impacting the system at a nominal speed and angle of 62 mph (100 km/h) and 25 degrees, respectively.

The test conditions of TL-3 longitudinal barriers are summarized in Table 1.

_	Test	_	Imp	act Condit	ions		
Test Article	Designation	Test Vehicle	Speed		Angle	Evaluation Criteria ¹	
Anticle	No.	venicie	mph	km/h	(deg)	Cincina	
Longitudinal	3-10	1100C	62	100	25	A,D,F,H,I	
Barrier	3-11	2270P	62	100	25	A,D,F,H,I	

Table 1. MASH TL-3 Crash Test Conditions

¹ Evaluation criteria explained in Table 2.

3.2 Evaluation Criteria

Evaluation criteria for full-scale vehicle crash testing are based on three appraisal areas: (1) structural adequacy; (2) occupant risk; and (3) vehicle trajectory after collision. Criteria for structural adequacy are intended to evaluate the ability of the longitudinal barrier to contain and redirect impacting vehicles. In addition, controlled lateral deflection of the test article is acceptable. Occupant risk evaluates the degree of hazard to occupants in the impacting vehicle. Post-impact vehicle trajectory is a measure of the potential of the vehicle to result in a secondary collision with other vehicles and/or fixed objects, thereby increasing the risk of injury to the occupants of the impacting vehicle and/or other vehicles. These evaluation criteria are summarized in Table 2 and defined in greater detail in MASH. The full-scale vehicle crash test was conducted and reported in accordance with the procedures provided in MASH.

In addition to the standard occupant risk measures, the Post-Impact Head Deceleration (PHD), the Theoretical Head Impact Velocity (THIV), and the Acceleration Severity Index (ASI) were determined and reported on the test summary sheet. Additional discussion on PHD, THIV and ASI is provided in MASH. Note that ASI values were calculated according to MASH as developed by TTI.

3.3 Soil Strength Requirements

In order to limit the variation of soil strength among testing agencies, foundation soil must satisfy the recommended performance characteristics set forth in Chapter 3 and Appendix B of MASH. Testing facilities must first subject the designated soil to a dynamic post test to demonstrate a minimum dynamic load of 7.5 kips (33.4 kN) at deflections between 5 and 20 in. (127 and 508 mm). If satisfactory results are observed, a static test is conducted using an identical test installation. The results from this static test become the baseline requirement for soil strength in future full-scale crash testing in which the designated soil is used. An additional post installed near the impact point is statically tested on the day of full-scale crash test in the same manner as used in the baseline static test. The full-scale crash test can be conducted only if the static test results show a soil resistance equal to or greater than 90 percent of the baseline static test at deflections of 5, 10, and 15 in. (127, 254, and 381 mm) or if a dynamic test shows a

soil resistance of at least 7.5 kips (33.4 kN) at deflections between 5 and 20 in. (127 and 508

mm). Otherwise, the crash test must be postponed until the soil demonstrates adequate post-soil strength.

Table 2. MASH E	Evaluation	Criteria fo	r Longitudinal	Barrier
	2 varaation	Cincina 10	n Longituamai	Duillei

Г	-							
Structural Adequacy	А.	Test article should contain and redirect the vehicle or bring the vehicle to a controlled stop; the vehicle should not penetrate, underride, or override the installation although controlled lateral deflection of the test article is acceptable.						
	D.	Detached elements, fragment should not penetrate or show compartment, or present a pedestrians, or personnel in intrusions into, the occupant set forth in Section 5.3 and Ap	potential for penetra an undue hazard a work zone. De compartment should	ating the occupant to other traffic, formations of, or not exceed limits				
	F.	The vehicle should remain upright during and after collision. The maximum roll and pitch angles are not to exceed 75 degrees.						
Occupant	H.	Occupant Impact Velocity (OIV) (see Appendix A, Section A5.3 MASH for calculation procedure) should satisfy the following limits:						
Risk		Occupant Impact Velocity Limits						
		Component	Preferred	Maximum				
		Longitudinal and Lateral	30 ft/s (9.1 m/s)	40 ft/s (12.2 m/s)				
	I.	The Occupant Ridedown Ad Section A5.3 of MASH for ca following limits:						
		Occupant Ridedown Acceleration Limits						
		Component	Preferred	Maximum				
		Longitudinal and Lateral	15.0 g's	20.49 g's				

4 TEST CONDITIONS

4.1 Test Facility

The testing facility is located at the Lincoln Air Park on the northwest side of the Lincoln Municipal Airport and is approximately 5 miles (8.0 km) northwest of the University of Nebraska-Lincoln.

4.2 Vehicle Tow and Guidance System

A reverse cable tow system with a 1:2 mechanical advantage was used to propel the test vehicle. The distance traveled and the speed of the tow vehicle were one-half that of the test vehicle. The test vehicle was released from the tow cable before impact with the barrier system. A digital speedometer on the tow vehicle increased the accuracy of the test vehicle impact speed.

A vehicle guidance system developed by Hinch [6] was used to steer the test vehicle. A guide flag, attached to the left-front wheel and the guide cable, was sheared off before impact with the barrier system. The ³/₈-in. (9.5-mm) diameter guide cable was tensioned to approximately 3,500 lb (15.6 kN) and supported both laterally and vertically every 100 ft (30.5 m) by hinged stanchions. The hinged stanchions stood upright while holding up the guide cable, but as the vehicle was towed down the line, the guide flag struck and knocked each stanchion to the ground.

4.3 Test Vehicles

For test no. MGSSYP-1, a 2004 Dodge Ram Quad Cab 1500 pickup truck was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 5,130 lb (2,327 kg), 5,029 lb (2,281 kg), and 5,199 lb (2,358 kg), respectively. The test vehicle is shown in Figure 24, and vehicle dimensions are shown in Figure 25.

For test no. MGSSYP-2, a 2004 Kia Rio sedan was used as the test vehicle. The curb, test inertial, and gross static vehicle weights were 2,402 lb (1,090 kg), 2,442 lb (1,108 kg), 2,612







Figure 24. Test Vehicle, Test No. MGSSYP-1

Date:	8/3/20	11		Т	est Numb	er: MGS	SYP-1		Model:	2270P/Ran	n 1500
Make:	Dodg	ge		V	ehicle I.D	.#: <u>1D7</u> I	HA18DX4	J254351	_		
Tire Size:	LT245/70) R17			Ye	ar: 2004			Odometer:	22376	3
, *(All Measureme	Fire Inflation		do)		35 Psi						
					[]		Ť	Vel	hicle Geom	etry in. (mm)
 n t Wheel			S			 m Wheel	 ۵	a 78	(1981)	b 74	(1880)
Track						Track	Ī	c 227 3/4	(5785)	d 47	(1194)
<u> </u>			<u> </u>					e <u>140 1/2</u>	(3569)	f <u>40 1/4</u>	(1022)
	Test Inert	ial C.M.—						g28_1/8	(716)	h <u>62 1/2</u>	(1588)
		\			← q →	TIRE DIA		i <u>1</u> 4	(356)	j_26	(660)
t				M	+ r +			k 20	(508)	l 28 1/2	(724)
 b	6					\rightarrow		m <u>67 7/8</u>	(1724)	n <u>67 1/2</u>	(1715)
1-				9				o <u>44</u>	(1118)	p3	(76)
_					Ý			q <u>30</u>	(762)	r <u>181/2</u>	(470)
			-	— h —		1		s <u>14</u>	(356)	t 75 1/2	(1918)
	d		—— e —			f			_	ront <u>14 1/4</u>	(362)
		Wrear	— c —	W _f ,	ront				-	Rear <u>14 1/2</u> e (F) <u>33 3/4</u>	(368) (857)
Mass Distribu	tion lb (kg)									$e(\mathbf{R}) = \frac{35 \ 3/4}{36 \ 1/2}$	(927)
Gross Static	LF 1437	(652)	RF	1466	(665)					t (F) 16 1/4	(413)
	LR 1113	(505)	RR	1183	(537)			Fi	rame Heigh	t (R) 24	(610)
			_						Engine 1	Гуре <u>8Cyl</u>	. GAS
Weights lb (kg)	Curb		Te	st Inertial		Gross Static			Engine	Size <u>5.7L</u>	345CI
W-front	2856	(1295)	_	2798	(1269)	2903 (1	317)		Transmitio	on Type:	
W-rear	2274	(1031)	_	2231	(1012)	2296 (1	041)		(Automatic	Manua
W-total	5130	(2327)	_	5029	(2281)	5199 (2	358)		1	WD RWD	4WD
GVWR Ra	tings					Du	mmy Data	a			
	Front		3650					ype: Hybrid II			
	Rear		3900					ass: 170 lbs			
	Total		6650			1	Seat Posit	tion: Passenge	r		

Figure 25. Vehicle Dimensions, Test No. MGSSYP-1

lb (1,185 kg) respectively. The test vehicle is shown in Figure 26, and the vehicle dimensions are shown in Figure 27.

The longitudinal component of the center of gravity (c.g.) was determined using the measured axle weights. The Suspension Method [7] was used to determine the vertical component of the c.g. for the pickup truck. This method is based on the principle that the c.g. of any freely suspended body is in the vertical plane through the point of suspension. The vehicle was suspended successively in three positions, and the respective planes containing the c.g. were established. The intersection of these planes pinpointed the final c.g. location for the test inertial condition. The vertical component of the c.g. for the 1100C vehicle was based on historical c.g. height measurements. The location of the final c.g. is shown in Figures 25 through 29. Data used to calculate the location of the c.g. and ballast information are shown in Appendix B.

Square, black- and white-checkered targets were placed on the vehicles for reference to be viewed from the high-speed digital video cameras and aid in the video analysis, as shown in Figures 28 and 29. Round, checkered targets were placed on the center of gravity on the left-side door, the right-side door, and the roof of the vehicle.

The front wheels of the test vehicles were aligned to vehicle standards except the toe-in value was adjusted to zero so that the vehicles would track properly along the guide cable. A 5B flash bulb was mounted on the right side of the vehicle's dash for both tests and was fired by a pressure tape switch mounted at the impact corner of the bumper. The flash bulb was fired upon initial impact with the test article to create a visual indicator of the precise time of impact on the high-speed videos. A remote controlled brake system was installed in the test vehicles so the vehicles could be brought safely to a stop after the test.







Figure 26. Test Vehicle, Test No. MGSSYP-2

Date:	:	9/13/2	011			Test Num	ıber:	М	IGSSYP-2	2 Model:1100C
Make:		Kia	L			Vehicle I.	D.#:	K	NADC125	5046350879
Tire Size:							ear:	20	04	Odometer: 85056
*(All Measure)			Pressure: Impacting	Side)		30psi				
-	$\overline{\mathcal{O}}$					、 、	$\overline{\mathbb{N}}$			Vehicle Geometry in. (mm)
		[Ĭ				╎╂		1	a 65 1/4 (1657) b 55 (1397)
a m —	- -					+ +	- +	<u>ل</u> vehicle	- n t	c <u>167 (4242)</u> d <u>38 1/2 (978)</u>
		r			<i>H</i>					e <u>95 3/4 (2432)</u> f <u>32 3/4 (832)</u>
		<u> </u>					IJ			g <u>17 (432)</u> h <u>37 (942)</u>
										i <u>81/2 (216)</u> j <u>21 (533)</u>
		a								k <u>11 1/2 (292)</u> l <u>22 (559)</u>
_	┥┝				J	<i>N</i>			f	m <u>56 1/8 (1426)</u> n <u>56 3/4 (1441)</u>
						0	7		 b	o <u>27 3/8 (695)</u> p <u>3 (76)</u>
	B	1000				100	Щ <u> </u>	•		q 22 1/2 (572) r 15 1/4 (387)
Ji		0000		s				k		s <u>11</u> (279) t <u>60 1/4</u> (1530)
	-	f	h T	e		0		Ţ.		Wheel Center Height Front 10 3/4 (273) Will 10 4 Will 14 D 10 7/9 (276)
	-	\checkmark	Wfront	С		₩re	ar			Wheel Center Height Rear10 7/8(276)Wheel Well Clearance (F)23 7/8(606)
Mass Distrib	oution	ı lb (kg)							Wheel Well Clearance (R) 24 (610)
Gross Static	LF	783	(355)	RF	797	(362)				Frame Height (F) 6 3/4 (171)
	LR		(219)	-		(249)				Frame Height (R) 16 1/2 (419)
				-		<u>, , , , , , , , , , , , , , , , , , , </u>				Engine Type 4cyl gas
Weights lb (kg)		Curb		To	st Inerti	ial	C	ross Stat	ic	Engine Size 1.4L
W-front		•	(688)			(679)	01	*	(717)	Transmition Type:
W-rear		885	(401)	•		(429)	-	·	(468)	Automatic Manual
W-total		2402	(1090)	•		(1108)	1		(1185)	FWD RWD 4WD
				-						
GVWR F	Rating	gs							Dummy D	Data
		Front		1808						Type: Hybrid 1
										Mass: 170 lbs.
							Seat Position: Passenger			
Note	any d	amage p	rior to test:	:	Minor 1	Hail Dam	age			

Figure 27. Vehicle Dimensions, Test No. MGSSYP-2

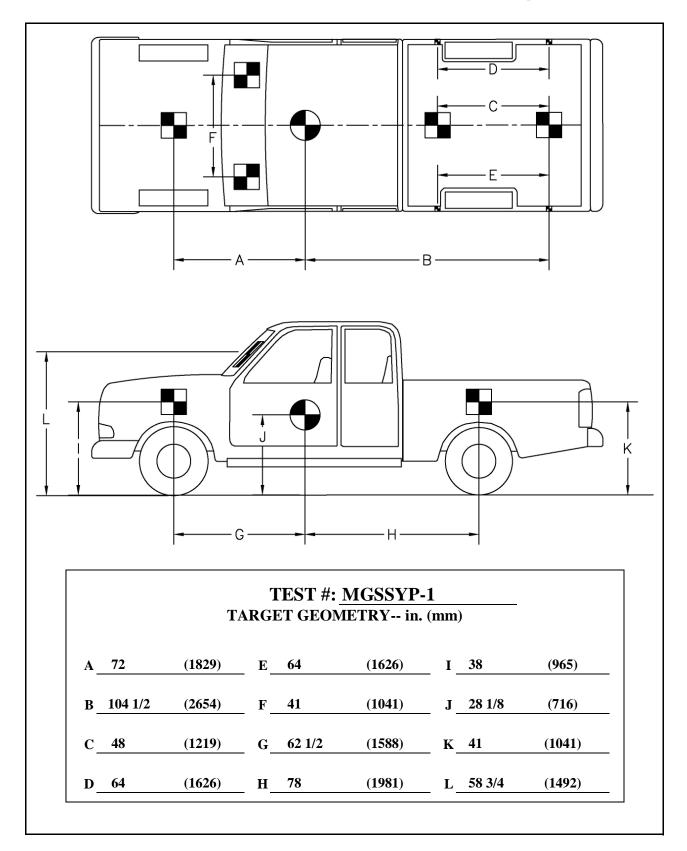


Figure 28. Target Geometry, Test No. MGSSYP-1

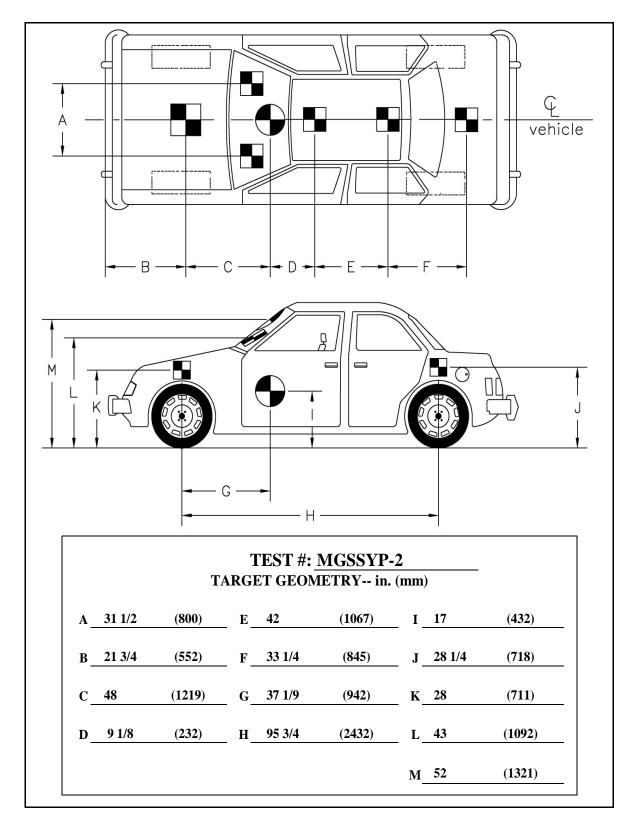


Figure 29. Target Geometry, Test No. MGSSYP-2

4.4 Simulated Occupant

For test nos. MGSSYP-1 and MGSSYP-2, a Hybrid II 50th-Percentile, Adult Male Dummy, equipped with clothing and footwear, was placed in the right-front seat of the test vehicle with the seat belt fastened. The dummy, which had a final weight of 170 lb (77 kg), was represented by model no. 572, serial no. 451, and was manufactured by Android Systems of Carson, California. As recommended by MASH, the dummy was not included in calculating the c.g. location.

4.5 Data Acquisition Systems

4.5.1 Accelerometers

Two environmental shock and vibration sensor/recorder systems were used to measure the accelerations in the longitudinal, lateral, and vertical directions. All of the accelerometers were mounted near the center of gravity of the test vehicles. The electronic accelerometer data obtained in dynamic testing was filtered using the SAE Class 60 and the SAE Class 180 Butterworth filter conforming to SAE J211/1 specifications [8].

The first accelerometer system was a two-arm piezoresistive accelerometer system manufactured by Endevco of San Juan Capistrano, California. Three accelerometers were used to measure each of the longitudinal, lateral, and vertical accelerations independently at a sample rate of 10,000 Hz. Two additional accelerometers were used to measure longitudinal and lateral accelerations independently at the same rate. The accelerometers were configured and controlled using a system developed and manufactured by Diversified Technical Systems, Inc. (DTS) of Seal Beach, California. More specifically, data was collected using a DTS Sensor Input Module (SIM), Model TDAS3-SIM-16M. The SIM was configured with 16 MB SRAM and 8 sensor input channels with 250 kB SRAM/channel. The SIM was mounted on a TDAS3-R4 module rack. The module rack was configured with isolated power/event/communications, 10BaseT

Ethernet and RS232 communication, and an internal backup battery. Both the SIM and module rack were crashworthy. The "DTS TDAS Control" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

The second system, Model EDR-3, was a triaxial piezoresistive accelerometer system manufactured by IST of Okemos, Michigan. The EDR-3 was configured with 256 kB of RAM, a range of ± 200 g's, a sample rate of 3,200 Hz, and a 1,120 Hz low-pass filter. The "DynaMax 1 (DM-1)" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the accelerometer data.

4.5.2 Rate Transducers

An angular rate sensor, the ARS-1500, with a range of 1,500 degrees/sec in each of the three directions (roll, pitch, and yaw) was used to measure the rates of rotation of the test vehicles. The angular rate sensor was mounted on an aluminum block inside the test vehicle near the center of gravity and recorded data at 10,000 Hz to the SIM. The raw data measurements were then downloaded, converted to the proper Euler angles for analysis, and plotted. The "DTS TDAS Control" computer software program and a customized Microsoft Excel worksheet were used to analyze and plot the angular rate sensor data.

4.5.3 Pressure Tape Switches

For test nos. MGSSYP-1 and MGSSYP-2, five pressure-activated tape switches, spaced at approximately 6.56-ft (2-m) intervals, were used to determine the speed of the vehicle before impact. Each tape switch fired a strobe light which sent an electronic timing signal to the data acquisition system as the right-front tire of the test vehicle passed over it. Test vehicle speeds were determined from electronic timing mark data recorded using TestPoint and LabVIEW computer software programs. Strobe lights and high-speed video analysis are used only as a backup in the event that vehicle speed cannot be determined from the electronic data.

4.5.4 Digital Photography

Two AOS VITcam high-speed digital video cameras, three AOS X-PRI high-speed digital video cameras, four JVC digital video cameras, and two Canon digital video cameras were utilized to film test no. MGSSYP-1. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 30.

Three AOS VITcam high-speed digital video cameras, three AOS X-PRI high-speed digital video cameras, four JVC digital video cameras, and two Canon digital video cameras were utilized to film test no. MGSSYP-2. Camera details, camera operating speeds, lens information, and a schematic of the camera locations relative to the system are shown in Figure 31.

The high-speed videos were analyzed using ImageExpress, MotionPlus, and RedLake MotionScope software programs. Actual camera speed and camera divergence factors were considered in the analysis of the high-speed videos. A Nikon D50 digital still camera was also used to document pre- and post-test conditions for all tests.

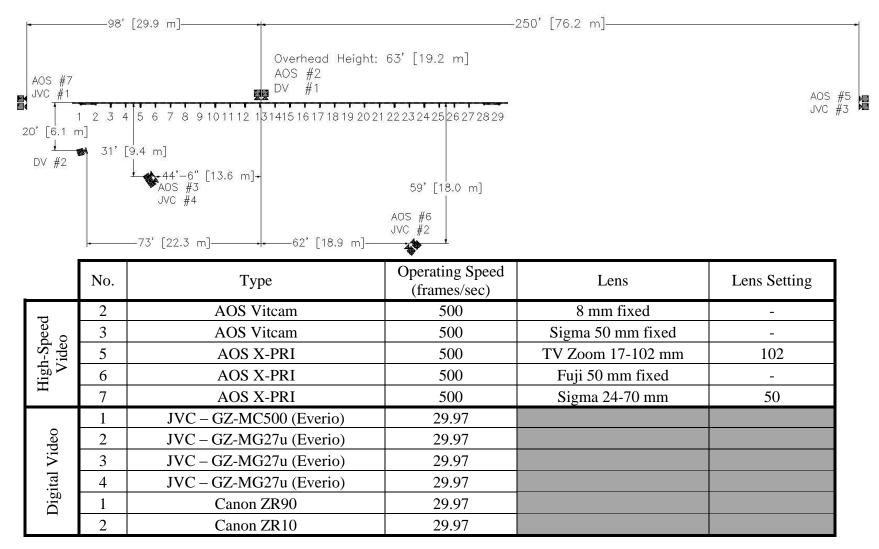


Figure 30. Camera Locations, Speeds, and Lens Settings, Test No. MGSSYP-1

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AOS JVC	#6 #1	1 2	AOS #3	0 21 22 23 24 25 26 27 28 29 ' [9.4 m] AOS #7	241' [73.5 m]	
		No.	JVC #2 Type	JVC #4 Operating Speed (frames/sec)	Lens	Lens Setting
ľ	eo	1	AOS Vitcam CTM	500	Cosmicar 12.5 mm fixed	_
	High-Speed Video	3	AOS Vitcam	500	Sigma 24-70 mm	35
	ed	4	AOS Vitcam	500	-	-
	Spe	5	AOS X-PRI	500	Canon 17-102 mm	102
	gh-,	6	AOS X-PRI	500	Fujinon 50 mm fixed	-
	Hi	7	AOS X-PRI	500	Sigma 50 mm fixed	-
ſ		1	JVC – GZ-MC500 (Everio)	29.97		
	deo	2	JVC – GZ-MG27u (Everio)	29.97		
	Vi	3	JVC – GZ-MG27u (Everio)	29.97	· · · · · · · · · · · · · · · · · · ·	
	jital	4	JVC – GZ-MG27u (Everio)	29.97		
	Digital Video	1	Canon ZR90	29.97		
		2	Canon ZR10	29.97		

Figure 31. Camera Locations, Speeds, and Lens Settings, Test No. MGSSYP-2

AOS #5 JVC #3

5 FULL-SCALE CRASH TEST NO. MGSSYP-1

5.1 Dynamic Soil Test

Before full-scale crash test no. MGSSYP-1 was conducted, the strength of the foundation soil was evaluated with a dynamic test, as described in MASH [2]. The dynamic test results are shown in Appendix C. The force vs. deflection curve for the dynamic soil test was determined using the acceleration data from the bogie vehicle to determine both the load and deflection of the post in the soil. While Appendix B of MASH requires the use of load cells for determination of post-soil forces, MwRSF has demonstrated through previous bogie tests of posts in soil that the load versus deflection as determined by accelerometers on the bogie vehicle compares well with data obtained from load cells mounted on an impacted post. There are minor differences in the load and deflection as measured by the accelerometer versus a dedicated transducer. First, loads measured by the load cell are expected to be slightly higher than those measured by the accelerometer due to the accelerometer only capturing the longitudinal component of the impact force as the post rotates backward. The vertical component of the impact load, which increases in magnitude as the rotation angle increases, is not reflected in the accelerometer data. Thus, utilizing accelerometers to obtain force data would be a conservative estimate of soil strength.

The soil strength test conducted prior to test no. MGSSYP-1 demonstrated that the soil for the test generated relatively high initial force levels, but the force level between 19 and 20 in. (483 and 508 mm) was slightly lower than the MASH requirement of 7,500 lb (33.4 kN). It was reasoned that the soil strength was sufficient even though the end of the post-soil force vs. deflection curve dipped slightly below the required threshold. First, the initial loading of the soil was significantly higher than the 7,500 lb (33.4 kN) force limit for the initial 10 in. (254 mm) of deflection. This indicated that the soil stiffness was high and that the soil was absorbing a significant amount of energy. Second, as noted above, the force data measured by the

accelerometer is conservative and was likely underestimating the soil resistance near the end of the post deflection. Third, the post-soil forces were only below the threshold for a limited deflection near the end of the 20 in. (508 mm) deflection limit. As such, the effect on overall post behavior was determined to be negligible.

5.2 Test No. MGSSYP-1

The 5,199-lb (2,358-kg) pickup truck impacted the MGS with SYP wood posts at a speed of 62.2 mph (100.1 km/h) and at an angle of 24.9 degrees. A summary of the test results and sequential photographs are shown in Figure 32. Additional sequential photographs are shown in Figures 33 and 34.

5.3 Weather Conditions

Test no. MGSSYP-1 was conducted on August 3, 2011 at approximately 4:45 pm. The weather conditions as per the National Oceanic and Atmospheric Administration (station 14939/LNK) were reported and are shown in Table 3 [9].

her Conditions, Test No. MGSS IP-1						
Temperature	85° F					
Humidity	55 %					
Wind Speed	11 mph					
Wind Direction	30° from True North					
Sky Conditions	Sunny					
Visibility	10 Statute Miles					
Pavement Surface	Dry					
Previous 3-Day Precipitat	ion 0.00 in.					
Previous 7-Day Precipitat	ion 0.14 in.					

Table 3. Weather Conditions, Test No. MGSSYP-1

5.4 Test Description

Initial vehicle impact was to occur 12 ft (3.7 m) upstream of the center line of post no. 15, as shown in Figure 35, which was selected using the CIP plots found in Section 2.3 of MASH to maximize pocketing and the propensity of wheel snag. The actual point of impact was 12 ft – 6 in. (3.8 m) upstream of post no. 15. A sequential description of the impact event is contained in Table 4. The vehicle came to rest 209 ft (63.7 m) downstream of the impact point and 56 ft - 10 in. (17.3 m) laterally behind the barrier system, and its trajectory did not violate the bounds of the exit box. The vehicle trajectory and final position are shown in Figures 32 and 36.

TIME	EVENT
(sec)	
0.000	The right-front corner of vehicle impacted rail $12 \text{ ft} - 6 \text{ in.} (3.8 \text{ m})$ upstream from post no. 15.
0.004	Post no. 13 deflected backward.
0.022	The right-front fender of vehicle deformed, post no. 14 deflected backward, and rail kinked downstream of post no. 14.
0.030	The upstream terminal deflected downstream, post no. 1 was moved upward, and post no. 12 deflected backward.
0.038	The right-front headlight shattered, downstream terminal rail deflected upstream, post no. 15 deflected backward, and rail kinked upstream of post no. 15.
0.060	The rail kinked downstream of post no. 15, and vehicle began to yaw counterclockwise.
0.066	The rail released from post no. 14.
0.074	Post no. 16 deflected backward.
0.080	Post no. 14 began to fracture.
0.095	The posts upstream of impact rotated toward impact point, and right-front wheel snagged on post no. 14 and disengaged from vehicle.
0.100	Post no. 15 fractured.
0.112	The rail released from post no. 15.
0.118	A kink formed in rail downstream of post no. 16, post no. 16 fractured approximately 1 ft (305 mm) above ground level, and right-front door of vehicle became slightly ajar.
0.136	Post nos. 17 and 18 deflected backward, and the vehicle rolled away from system.
0.144	The rail released from post no. 16.
0.154	The rail kinked at post no. 18.
0.228	The vehicle rolled slightly toward system.
0.238	The undercarriage of vehicle impacted remaining 1 ft (305 mm) of post no. 16.
0.290	The vehicle was parallel to system with a speed of 46.8 mph (75.3 km/h).
0.300	The upstream terminal was at maximum deflection, post no. 19 deflected backward, and post no. 17 fractured.

 Table 4. Sequential Description of Impact Events, Test No. MGSSYP-1

0.308	The rail released from post no. 17.
0.652	The vehicle exited system with a speed of 37.8 mph (60.8 km/h) and at an angle of 15.7 degrees.
0.892	The right-front brake disk contacted ground.
0.966	The right-front bumper contacted ground.

5.5 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 37 through 38. Barrier damage consisted of deformed guardrail, fractured posts, and contact marks on the front face of the W-beam guardrail. The length of vehicle contact along the barrier was approximately 34 ft - 4 in. (10.5 m) which spanned from 4 in. (102 mm) upstream of the centerline of post no. 13 and extended to 33 in. (838 mm) downstream of post no. 18.

The rail disengaged from several posts both upstream and downstream of impact. The guardrail bolt pulled through the rail at post nos. 3 through 5, 7 through 9, and 14 through 17. A ¹/₄-in. (6-mm) tear was found in the rail on the upstream end of the slot at post no 3. A ¹/₄-in. (6-mm) tear also occurred at the bottom center of the slot at post no. 7. A ¹/₂-in. (13-mm) tear occurred on the bottom downstream edge of the slot at post no. 14.

Deformations in the rail occurred from post no. 12 to post no. 18. The top of the rail kinked at post no. 12. The rail buckled 2¹/₂ in. (64 mm) downstream of the downstream side of the slot at post no. 13. The bottom corrugation began to fold at post no. 13. Folding of the bottom corrugation also occurred from 52 in. (1,321 mm) downstream of post no. 13 and extended to 33 in. (838 mm) downstream of post no. 14. The rail kinked 4 in. (102 mm) upstream of post no. 13. Flattening of the rail began 1 in. (25 mm) downstream of post no. 13 and extended to 52 in. (1,321 mm) downstream of post no. 13. Flattening occurred again from 33 in. (838 mm) downstream of post no. 13. Flattening occurred again from 33 in. (838 mm) downstream of post no. 14 and extended to 5 in. (127 mm) upstream of post no. 17. Flattening also occurred from 23 in. (584 mm) upstream of post no. 18 and extended to 10 in. (254 mm)

downstream of post no. 18. The bottom corrugation of the rail kinked at 31 in. (787 mm) downstream of post no. 18. The rail also buckled at post no. 18.

The top of the blockouts of post nos. 3 through 5 were twisted upstream. The top of the blockouts of post nos. 6 and 7 were twisted downstream. The front of the blockouts for post nos. 6 and 10 were rotated downstream. The top of the blockouts for post nos. 9 and 11 were twisted downstream.

Damage to the posts began at post no. 6, which split on the front face downstream corner. Post no. 10 split at the center of the top of the post from the front to the back. This split started at the top of the post and extended 8½ in. (216 mm) down the post. Post no. 11 split at the center of the post from the front to the back. The split started at the top of the post and extended to the groundline. Post nos. 12 and 13 rotated backwards and split at the center of the post from the front of the post to the back of the post. The splits on both posts started at the top of the post and continued to the groundline. Post nos. 14 through 17 were fractured at the groundline. Post no. 14 came to rest 9 ft – 6 in. (2,896 mm) behind the barrier. Post no. 15 came to rest 9 ft – 3 in. (2,819 mm) behind the barrier. Post no. 16 came to rest 14 ft – 6 in. (4,420 mm) behind the barrier. Post no. 17 came to rest 1 ft – 1 in. (330 mm) behind the barrier. Tire contact marks were found 21 in. (533 mm) down from the top of the front face of post no. 14. Post no. 16 was split into 3 pieces due to contact with the vehicle, and contact marks were also found on the front face of the post. Soil gaps, heaves, and craters can be found in Table 5.

The maximum permanent set of the barrier system was 30¹/₄ in. (768 mm) at the midspan between post nos. 15 and 16, as measured in the field. The maximum lateral dynamic rail and post deflections were 40.0 in. (1,016 mm) at post no. 15 and 28.1 in. (714 mm) at post no. 17, respectively, as determined from high-speed digital video analysis. The working width of the

system was found to be 53.8 in. (1,367 mm), also determined from high-speed digital video analysis.

	S	oil Gap Locatio in. (mm)	Soil He in. (n		Soil Crater, in. (mm)			
Post No.	Upstream	Downstream	Front	Back	Diameter	Height	Diameter	Depth
1	11/2 (38)	0	0	0	28 (711)	3 (76)	0	0
2	¹ ⁄4 (6)	¹ ⁄4 (6)	0	0	0	0	0	0
12	¹ / ₂ (13)	0	1/2 (13)	0	0	0	0	0
13	³ ⁄ ₄ (19)	0	21/4 (57)	3⁄4 (19)	27 (686)	3 (76)	0	0
14	0	0	1¾ (44)	2 (51)	17 (432)	2 (51)	13 (330)	4 (102)
15	0	0	0	0	0	0	42 (1,067)	3 (76)
16	0	0	0	0	24 (610)	3 (76)	0	0
17	0	0	4 (102)	0	20 (508)	4 (102)	0	0
18	0	0	11/4 (32)	21/2 (64)	18 (457)	4 (102)	0	0
19	0	0	1/4 (6)	1/4 (6)	0	0	0	0
29	0	¹ ⁄4 (6)	0	0	0	0	0	0

Table 5. Soil Gap, Soil Heave, and Soil Crater Measurements, Test No. MGSSYP-1

¹ If a post is omitted in the table, there were no soil disturbances at that post location

5.6 Vehicle Damage

The damage to the vehicle was minimal, as shown in Figures 47 and 48. The maximum occupant compartment deformations are listed in Table 6 along with the deformation limits established in MASH for various areas of the occupant compartment. Note that none of the MASH established deformation limits were violated. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix D.

LOCATION	MAXIMUM DEFORMATION in. (mm)	MASH ALLOWABLE DEFORMATION in. (mm)
Wheel Well & Toe Pan	¹ / ₂ (13)	≤9 (229)
Floor Pan & Transmission Tunnel	¹ / ₂ (13)	≤ 12 (305)
Side Front Panel (in Front of A-Pillar)	³ ⁄ ₄ (19)	≤ 12 (305)
Side Door (Above Seat)	³ ⁄ ₄ (19)	≤9 (229)
Side Door (Below Seat)	1 (25)	≤ 12 (305)
Roof	0	≤4 (102)
Windshield	0	≤3 (76)

Table 6. Maximum Occupant Compartment Deformations by Location

The majority of the damage was concentrated on the right-front corner and right side of the vehicle where the impact occurred. The front bumper was bent on the right lower side approximately 8 in. (203 mm) from the centerline of the vehicle. There was also a kink on the top of the front bumper approximately 19 in. (483 mm) from the centerline of the vehicle. There were contact marks on the right side of the front bumper cover. The front bumper cover also had a 5-in. (127-mm) tear along the right quarter panel. The grill of the vehicle was deformed backward 21/2 in. (64 mm) on the bottom right side. The right quarter panel was folded inward 7 in. (178 mm). The right headlight fractured, and the right-front tire detached from the vehicle at the wheel bearing. The right-front upper control arm and disc brake assembly detached. Contact marks extended the entire length of the right side of the vehicle. Both of the doors on the right side were slightly ajar. The top of the right-front door separated 1 in. (25 mm) from the cab of the vehicle, while the bottom of the right rear door separated ³/₄ in. (19 mm) from the cab. The right-front door also had flattening that extended the entire length of the door 17 in. (432 mm) up from the bottom of the door. The right-rear door had contact marks that extended the length of the door. Flattening occurred at the bottom of the door and at the rear corner of the cab. The right

side of the rear bumper was flattened and had a kink 12 in. (305 mm) from the right fender. The right-rear taillight separated approximately 2½ in. (64) mm from the fender. A 35 in. (889 mm) long crack was found down the center of the windshield.

5.7 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec average occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 7. Note that the OIVs and ORAs were within the suggested limits provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 7.

The results of the occupant risk analysis, as determined from the accelerometer data, are summarized in Figure 32. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix E.

Evaluation Criteria		Tran	sducer	MASH Limits	
		EDR-3	DTS		
OIV ft/s (m/s)	Longitudinal	-14.20 (-4.33)	-13.25 (-4.04)	≤ 40 (12.2)	
	Lateral	-14.77 (-4.50)	-14.74 (-4.50)	≤40 (12.2)	
ORA g's	Longitudinal	8.39 -7.56	-8.14	≤ 20.49	
	Lateral	-7.65	-8.51	\leq 20.49	
THIV ft/s (m/s)		NA	19.82 (6.04)	not required	
PHD g's		NA	11.36	not required	
ASI ¹		0.70	0.70	not required	

Table 7. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. MGSSYP-1

¹ASI procedures based on MASH Appendix F

5.8 Discussion

The analysis of the test results for test no. MGSSYP-1 showed that the system adequately contained and redirected the 2270P vehicle with controlled lateral displacements of the barrier. There were no detached elements nor fragments which showed potential for penetrating the occupant compartment nor presented undue hazard to other traffic. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle did not penetrate nor ride over the barrier and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix E, were deemed acceptable because they did not adversely influence occupant risk safety criteria nor cause rollover. After impact, the vehicle exited the barrier at an angle of 15.7 degrees. Therefore, test no. MGSSYP-1 was determined to be acceptable according to the MASH safety performance criteria for test designation no. 3-11.

						P ++			
0.000 sec	0.096 sec	0.290 sec		0.402 sec		502 sec			
24.5 1 2 3 4 5 6 7 8 9 10 11 12 56'-10" [17.3 m]	16'-8' [5.1 m] 23242526272829 32'-10" [10.0 m]			31, [281]					
		- in the							
• •	MwRSF MGSSYP-1	• Vehic	le Damage			Minimal			
• Date			VDS ^[11] 01-RFQ-4						
MASH Test Designation No	 MASH Test Designation No		CDC ^[12] 01-RYEW-3						
			Maximum Interior Deformation1 in. (25 mm)						
	• Total Length			Test Article Damage					
 Key Component – Steel W-Beam Guardrail Maximum Test Article Deflections 									
Thickness		Permanent Set							
Top Mounting Height		Dynamic							
• Key Component – Southern Yellow			Working Width			in. (1,367 mm)			
	6 x 8 x 72 in. (152 x 203 x 1,829 mm)	 Maxir 	Maximum Angular Displacements						
	Post Spacing		Roll						
Embedment Depth			Pitch						
Key Component – Wood Blockout			Yaw			44.1°			
	6 x 12 x 14¼ in. (152 x 305 x 362 mm)	 Transe 	lucer Data						
Vehicle Make /Model		Evaluation Criteria		Transducer		MASH			
Curb		Evalua	uon Criteria	EDR-3	DTS	Limit			
		OIV	Longitudinal	-14.20 (-4.33)	-13.25 (-4.04)	$\leq 40(12.2)$			
	5,199 lb (2,358 kg)	ft/s		· · · ·	、 <i>'</i>	- 、 ,			
Impact Conditions		(m/s)	Lateral	-14.77(-4.50)	-14.74 (-4.50)	\leq 40 (12.2)			
		ORA	Longitudinal	8.39	-8.14	≤ 20.49			
	ft fin (2.8 m) Unstroom of Post No. 15	g's	U	-7.56					
1	ft $- 6$ in. (3.8 m) Upstream of Post No. 15	53	Lateral	-7.65	-8.51	≤ 20.49			
 Impact Severity		THIV	- ft/s (m/s)	NA	19.82 (6.04)	not			
					17:02 (0:01)	required			
1		זת	ID – g's	NA	11.26	not			
		PI	ID - g s	INA	11.36	required			
Exit Box Criterion				0.70		not			
			ASI	0.70	0.70	required			
•		L			1	1			
11 C	56 ft - 10 in. (17.3) laterally behind								

56 ft - 10 in. (17.3) laterally behindFigure 32. Summary of Test Results and Sequential Photographs, Test No. MGSSYP-1

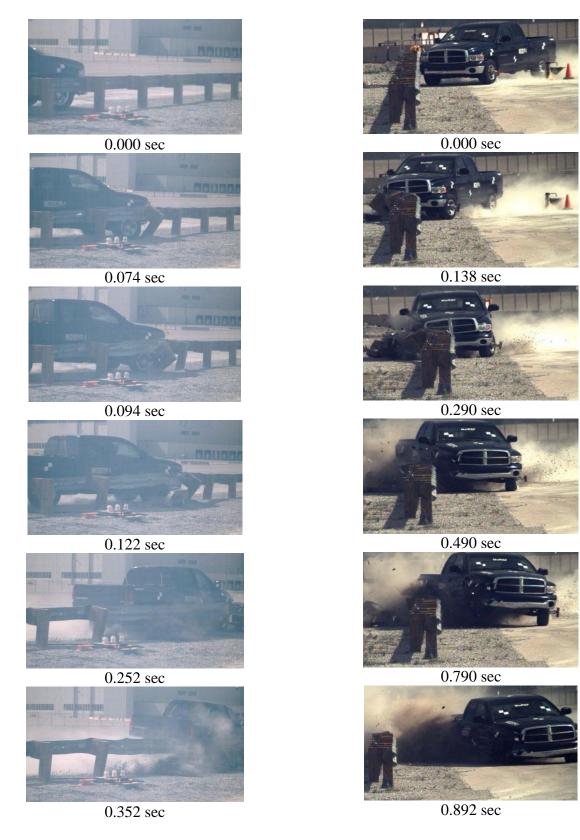


Figure 33. Additional Sequential Photographs, Test No. MGSSYP-1

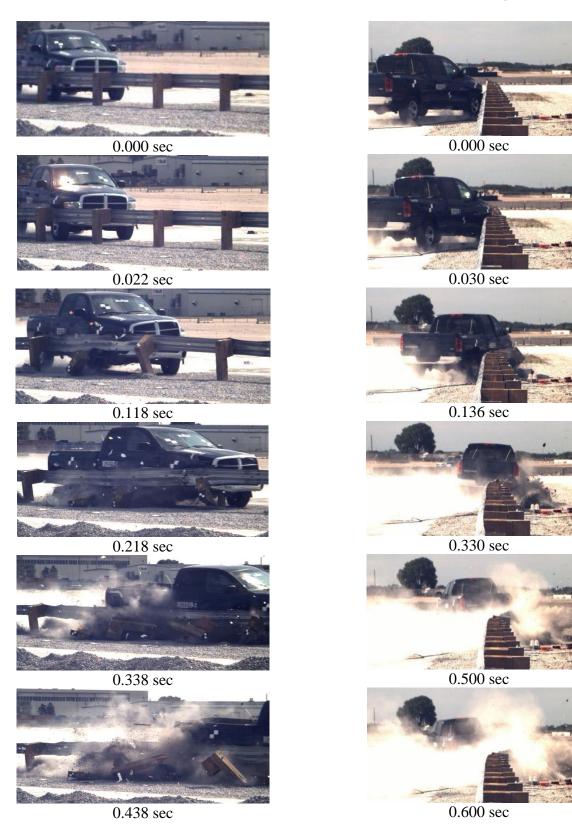


Figure 34. Additional Sequential Photographs, Test No. MGSSYP-1







Figure 35. Impact Location, Test No. MGSSYP-1





Figure 36. Vehicle Final Position and Trajectory Marks, Test No. MGSSYP-1







Figure 37. System Damage, Test No. MGSSYP-1

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Figure 38. Rail Damage Between Post Nos. 13 and 18, Test No. MGSSYP-1









Figure 39. Post Nos. 6 and 10 Damage, Test No. MGSSYP-1

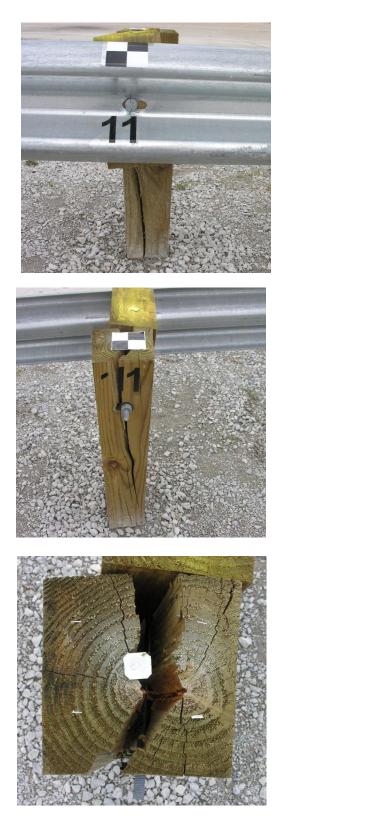




Figure 40. Post Nos. 11 and 12 Damage, Test No. MGSSYP-1.





Figure 41. Post Nos. 13 and 14 Damage, Test No. MGSSYP-1



Figure 42. Post Nos. 15 and 16 Damage, Test No. MGSSYP-1

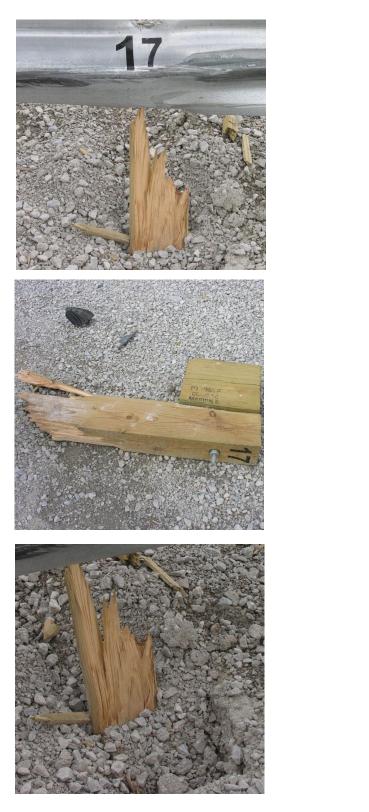




Figure 43. Post Nos. 17 and 18 Damage, Test No. MGSSYP-1

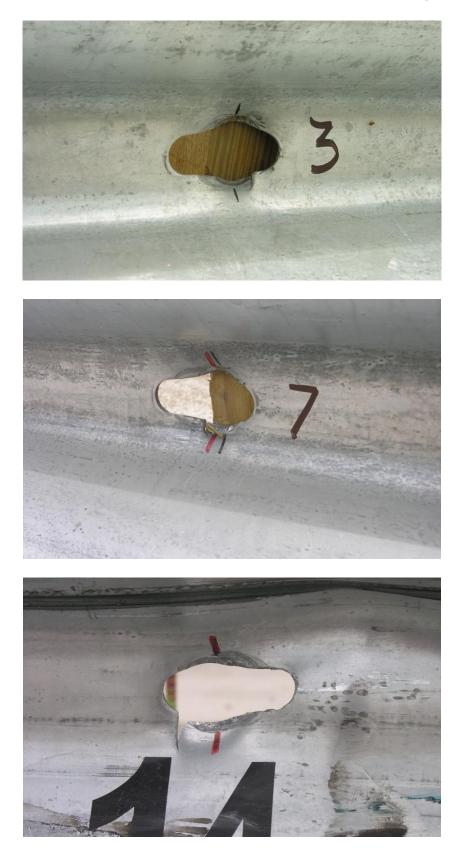


Figure 44. Local Rail Tearing at Post Nos. 3, 7, and 14, Test No. MGSSYP-1

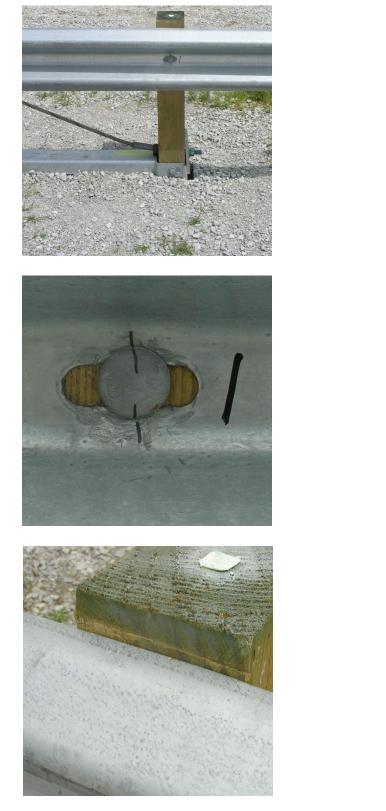




Figure 45. Upstream Anchor Damage, Test No. MGSSYP-1

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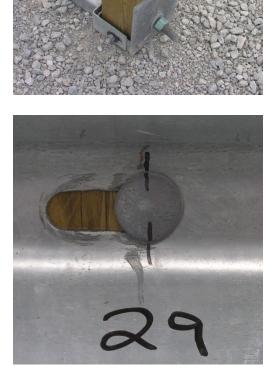


Figure 46. Downstream Anchor Damage, Test No. MGSSYP-1



Figure 47. Vehicle Damage, Test No. MGSSYP-1

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Figure 48. Vehicle Damage, Test No. MGSSYP-1

6 FULL-SCALE CRASH TEST NO. MGSSYP-2

6.1 Static Soil Test

Before full-scale crash test no. MGSSYP-2 was conducted, the strength of the foundation soil was evaluated with a static test, as described in MASH. The post-soil resistance was measured at deflections of 5 in., 10 in., and 15 in. (127 mm, 254 mm, and 381 mm) using load cells during a static test, as shown in Table 8. The complete force versus deflection curves for the static post test are shown in Appendix C.

Table 8. Soil Resistance

Displacement		ay Load [kN]	Minimum Load (90% Baseline)		
in. [mm]	in. [mm] Load Cell #1		lb [kg]		
5 [127]	7,814 [34.8]	7,899 [35.1]	5,547 [24.7]		
10 [254]	7,899 [35.1]	8,013 [35.6]	6,650 [29.6]		
15 [381]	6,852 [30.5]	6,845 [30.4]	6,973 [31.0]		

At 5 in. (127 mm) of deflection, the static post-soil resistance was approximately 41 percent higher than the baseline minimum. As the post rotated through the 10 in. (254 mm) was approximately 19 percent greater than the baseline minimum. At 15 in. (381 mm) of deflection, the post-soil resistance was less than 2 percent lower than the baseline minimum value. However, it should be noted that the static baseline capacity was excessively high, as shown in Figure C-2, and it corresponded to a soil strength with significant dynamic post-soil resistance, ranging between 10,000 lb (44.5 kN) and 11,000 lb (48.9 kN). As such, the test day dynamic soil strength would have easily surpassed the 7,500-lb (33.4-kN) limit. Therefore, the soil was determined to provide adequate strength for embedded wood guardrail posts, and full-scale crash testing was then conducted on the barrier system.

6.2 Test No. MGSSYP-2

The 2,612-lb (1,185-kg) small car impacted the MGS with SYP wood posts at a speed of 61.5 mph (99.0 km/h) and at an angle of 25.3 degrees. A summary of the test results and sequential photographs are shown in Figure 49. Additional sequential photographs are shown in Figures 50 and 51.

6.3 Weather Conditions

Test no. MGSSYP-2 was conducted on September 13, 2011 at approximately 4:30 pm. The weather conditions as per the National Oceanic and Atmospheric Administration (station 14939/LNK) were reported and are shown in Table 9 [9].

Table 9. Weather Conditions,	Test No. MGSSYP-2
------------------------------	-------------------

Temperature	70° F
Humidity	53 %
Wind Speed	10 mph
Wind Direction	10° from True North
Sky Conditions	Sunny
Visibility	10 Statute Miles
Pavement Surface	Dry
Previous 3-Day Precipitation	0.00 in.
Previous 7-Day Precipitation	0.00 in.

6.4 Test Description

Initial vehicle impact was to occur 8 ft – 7 in. (2.6 m) upstream of the center line of post no. 15, as shown in Figure 52, which was selected using the CIP plots found in Section 2.3 of MASH to maximize pocketing and the propensity of wheel snag. The actual point of impact was 8 ft – 4 in. (2.5 m) upstream of post no. 15. A sequential description of the impact events is contained in Table 10. The vehicle came to a rest 168 ft – 2 in. (51.3 m) downstream of the impact location and 17 ft – 11 in. (5.5 m) laterally in front of the barrier system, and its trajectory did not violate the bounds of the exit box. The vehicle trajectory and final position are shown in

Figure 53.

TIME (sec)	EVENT
0.000	The right-front corner of vehicle impacted rail 8 ft $-$ 4 in. (2.5 m) upstream of post no. 15.
0.008	The hood of vehicle separated and began to override rail.
0.030	Post nos. 14 and 15 rotated backward.
0.062	The rail penetrated front of vehicle to center point.
0.082	The blockout of post no. 15 twisted.
0.084	The vehicle impacted post no. 15.
0.088	The front bumper of vehicle started detaching.
0.090	Post no. 16 rotated backward.
0.096	The right-front door became ajar.
0.112	The rail detached from post no. 15.
0.120	The surrogate occupant's head impacted right-front window and shattered it.
0.136	Post no. 15 fractured near groundline.
0.150	The right side of front bumper detached from vehicle.
0.164	Post no. 15 became airborne, and vehicle impacted blockout of post no. 16, causing it to twist.
0.166	The vehicle impacted post no. 16.
0.186	The maximum deflection of system occurred.
0.194	The right-front tire impacted post no. 16, causing it to split vertically and fracture near groundline.
0.222	The blockout of post no. 16 detached from post no. 16
0.258	The detached portion of front bumper impacted ground.
0.260	The vehicle was parallel with system at a speed of 41.2 mph (66.3 km/h).
0.262	The vehicle impacted blockout of post no. 17.
0.280	The vehicle redirected away from system.
0.290	The right-front tire impacted post no. 17.
0.320	Post no. 17 rotated slightly back toward traffic.
0.370	The front of vehicle lost contact with rail.
0.484	The vehicle exited system at a speed of 35.7 mph (57.4 km/h) and at an angle of 13.6 degrees.

 Table 10. Sequential Description of Impact Events, Test No. MGSSYP-2

6.5 Barrier Damage

Damage to the barrier was moderate, as shown in Figures 54 through 56. Barrier damage consisted of deformed guardrail, rotated and fractured posts, and contact marks on the guardrail and posts. The length of vehicle contact along the barrier was approximately 23 ft – 1 in. (7.0 m) which spanned from 2 ft – $6\frac{1}{2}$ in. (775 mm) upstream of post no. 14 to 1 ft – $9\frac{1}{2}$ in. (546 mm) downstream of post no. 17.

The guardrail bolt pulled through the rail at post nos. 15 through 17. A 1-in. (25-mm) tear was found in the bolt slot of the rail at post no. 15. The rail kinked at the downstream edge of post no. 13. The rail kinked at the top of the rail at the midspan between post nos. 13 and 14. The rail buckled at the downstream edge of the blockout at post no. 14. Flattening occurred from post no. 14 and extended to the splice downstream from post no. 16. The rail buckled at post no. 17 and kinked at post no. 18.

Post no. 15 fractured at the groundline and splintered on the upstream corner of the front face. Contact marks were found on the front of post no. 15. Post no. 16 fractured at the groundline, and tire gouging was found on the front face of the post. Post no. 17 deflected backwards. The top of post no. 17 split at the nail location, and a 6½-in. (165-mm) gouge was found on the upstream side of the front face. Soil gaps, heaves, and craters can be found in Table 11.

The maximum permanent set of the barrier system measured from the back of the posts was 11 in. (279 mm) at post no. 17, as measured in the field. The maximum permanent set of the rail was 16¹/₄ in. (413 mm) at the midspan between post nos. 15 and 16, as measured in the field. The maximum lateral dynamic barrier deflection was 22.2 in. (564 mm) at the midspan between post nos. 15 and 16, as determined from high-speed digital video analysis. The working width of

the system was found to be 39.7 in. (1,008 mm), also determined from high-speed digital video analysis.

	S	oil Gap Locatio in. (mm)	on ¹ ,	Soil H in. (n		Soil Crater, in. (mm)		
Post No.	Upstream	Downstream	Front	Back	Diameter	Height	Diameter	Depth
13	0	0	¹ / ₂ (13)	0	0	0	0	0
14	0	0	2½ (64)	1 (25)	13 (330)	3 (76)	0	0
15	0	0	2 (51)	0	0	0	20 (508)	31/2 (89)
16	0	0	0	0	22 (559)	2 (51)	19 (483)	3 (76)
17	11/2 (38)	0	4 (102)	0	22 (559)	4 (102)	0	0
18	0	0	3⁄4 (19)	0	0	0	0	0
29	0	¹ / ₂ (13)	0	0	0	0	0	0

Table 11. Soil Gap, Soil Heave, Soil Crater Measurements, Test No. MGSSYP-2

¹ If a post is omitted in the table, there were no soil disturbances at that post location

6.6 Vehicle Damage

The damage to the vehicle was moderate, as shown in Figures 61 and 62. The maximum occupant compartment deformations are listed in Table 12 along with the deformation limits established in MASH for various areas of the occupant compartment. Note that none of the MASH established deformation limits were violated. Complete occupant compartment and vehicle deformations and the corresponding locations are provided in Appendix D.

Table 12. Maximum Occupant Compartment Deformations by Location

LOCATION	MAXIMUM DEFORMATION	MASH ALLOWABLE DEFORMATION
	in. (mm)	in. (mm)
Wheel Well & Toe Pan	¹ / ₂ (13)	≤ 9 (229)
Floor Pan & Transmission Tunnel	¹ ⁄4 (6)	≤ 12 (305)
Side Front Panel (in Front of A-Pillar)	³ ⁄ ₄ (19)	≤12 (305)
Side Door (Above Seat)	1 ¼ (32)	≤ 9 (229)
Side Door (Below Seat)	¹ ⁄4 (6)	≤ 12 (305)
Roof	0	≤ 4 (102)
Windshield	0	≤ 3 (76)

The majority of the damage was concentrated on the right-front corner and right side of the vehicle where the impact occurred. The right-front of the vehicle was folded under. The right-front quarter panel crushed inward 13 in. (330 mm) and into the shock absorber. Contact marks and gouging were found on the right-front fender. The right-front wheel dented and crushed severely. The right-front tire was punctured and deflated. The tie-rod on the right-front side fractured. The right-front control arm bent and disengaged from the vehicle. The door on the right-front of the vehicle was dented, ajar from the vehicle, and crushed inward. The mirror on the right side disengaged from the vehicle. The windshield cracked on the right side from the vehicle 11 in. (533 mm) toward the center and the entire height of the windshield. Tears were found along the bottom of the right-front fender behind the wheel well. The bottom of the door frame crushed inward for 1 ft (305 mm) behind the right-front wheel well. The radiator fan disengaged from the vehicle, and brake fluid leaked from the right side. The radiator fan disengaged from the vehicle, and brake fluid leaked from the right side. Contact marks extended the entire length of the right side of the vehicle.

6.7 Occupant Risk

The calculated occupant impact velocities (OIVs) and maximum 0.010-sec occupant ridedown accelerations (ORAs) in both the longitudinal and lateral directions are shown in Table 13. Note that the OIVs and ORAs were within the suggested limits provided in MASH. The calculated THIV, PHD, and ASI values are also shown in Table 13.

The results of the occupant risk analysis, as determined from the accelerometer data, are summarized in Figure 49. The recorded data from the accelerometers and the rate transducers are shown graphically in Appendix F.

Evaluation Criteria		Transo	MASH		
		EDR-3	DTS	Limits	
OIV	Longitudinal	-17.13 (-5.22)	-15.70 (-4.79)	≤ 40 (12.2)	
ft/s (m/s)	Lateral	-19.52 (-5.95) -20.92 (-6.38)		≤40 (12.2)	
ORA Longitudinal		-13.05	-13.34	≤ 20.49	
g's	Lateral	-7.42	-9.30	≤ 20.49	
	HIV s (m/s)	NA	27.92 (8.51)	not required	
PHD g's		NA	14.38	not required	
ASI ¹		0.91	0.99	not required	

Table 13. Summary of OIV, ORA, THIV, PHD, and ASI Values, Test No. MGSSYP-2

¹ASI procedures based on MASH Appendix F

6.8 Discussion

The analysis of the test results for test no. MGSSYP-2 showed that the system adequately contained and redirected the 1100C vehicle with controlled lateral displacements of the barrier. There were no detached elements or fragments which showed potential for penetrating the occupant compartment nor presented undue hazard to other traffic. Deformations of, or intrusions into, the occupant compartment that could have caused serious injury did not occur. The test vehicle did not penetrate nor ride over the barrier and remained upright during and after the collision. Vehicle roll, pitch, and yaw angular displacements, as shown in Appendix F, were deemed acceptable because they did not adversely influence occupant risk safety criteria nor cause rollover. After impact, the vehicle exited the barrier at an angle of 13.6 degrees. Therefore, test no. MGSSYP-2 was determined to be acceptable according to the MASH safety performance criteria for test designation no. 3-10.

					Y	
0.000 sec	0.128 sec	0.268 sec	0	378 sec	0.492 \$	sec
25.3	-168'-2" [51.3 m] ЕХІТ ВОХ		-		33* [838] Cround	
1 2 3 4 5 6 7 8 9 10 11 12 13 14	LF TIRE KF TIRE 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29		ł		39" [991]	
Test Agency		Vehic	le Stopping Distance	e16	$\frac{1}{1}$ $\frac{1}{2}$ $\frac{1}$	wnstream
	MGSSYP-2	· · · · · · · · · · · · · · · · · · ·	te Stopping Distance		-11 in. (5.5 m) laterall	
		Vehic	le Damage			
6			CDC ^[12]			RYEW-5
				Deformation		
 Key Component – Steel W-Beam C 		Test A	article Damage		Ì	Moderate
			num Test Article De			
						(413 mm)
Key Component – Southern Yellow						· /
		 Maxir 	num Angular Displa		()	,,
1 0					-10	.7 ° < 75°
Key Component – Wood Blockout						
	6 x 12 x 14¼ in. (152 x 305 x 362 mm)					
		Transe	lucer Data			
				Transo	lucer	MASH
	2,442 lb (1,108 kg)	Evalu	ation Criteria	EDR-3	DTS	Limit
						≤ 40
Impact Conditions		OIV	Longitudinal	-17.13 (-5.22)	-15.72 (-4.79)	(12.2)
1	61.5 mph (98.9 km/h)	ft/s				≤ 40
		(m/s)	Lateral	-19.52(-5.95)	-20.93 (-6.38)	(12.2)
Angle (Orientation)			Longitudin-1	12.05	12.04	× /
Impact Location	8 ft – 4 in. (2.5 m) Upstream of Post No. 15	ORA	Longitudinal	-13.05	-13.04	≤ 20.49
Impact Severity (IS)	56.4 kip-ft (76.4 kJ) > 51 kip-ft (69.7 kJ)	g's	Lateral	-7.42	-9.30	≤ 20.49
Exit Conditions						not
1		THIV	7 – ft/s (m/s)	NA	27.92 (8.51)	required
Angle (Trajectory)						not
		P	HD – g's	NA	14.38	required
Exit Box Criterion	Pass	<u> </u>				not
Vehicle Stability	Satisfactory		ASI	0.91	0.99	required
		L			1	icquireu

Figure 49. Summary of Test Results and Sequential Photographs, Test No. MGSSYP-2

ΓT



0.000 sec



0.080 sec



0.136 sec



0.222 sec



0.474 sec



0.570 sec



0.000 sec



0.088 sec



0.142 sec



0.260 sec



0.444 sec



0.764 sec

Figure 50. Additional Sequential Photographs, Test No. MGSSYP-2

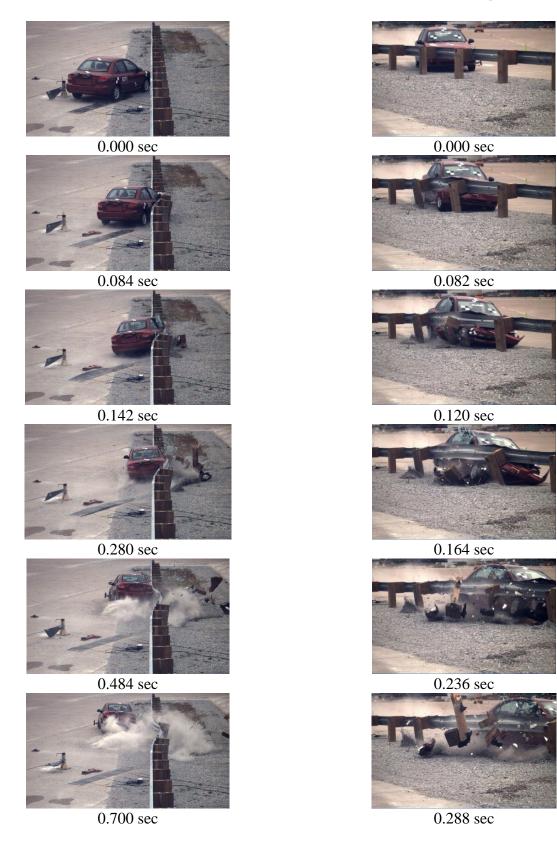


Figure 51. Additional Sequential Photographs, Test No. MGSSYP-2



Figure 52. Impact Location, Test No. MGSSYP-2

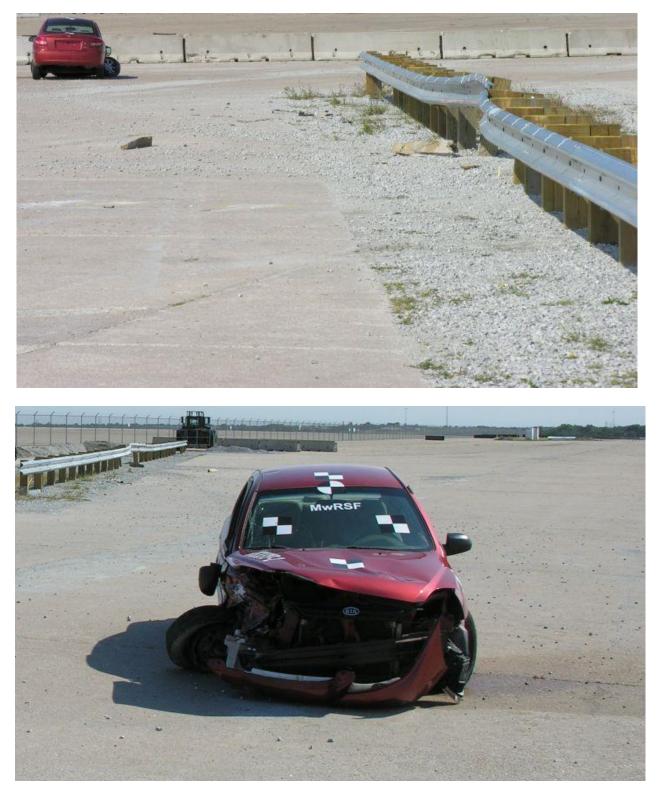


Figure 53. Vehicle Final Position and Trajectory Marks, Test No. MGSSYP-2



Figure 54. System Damage, Test No. MGSSYP-2



Figure 55. Rail Damage Between Post Nos. 13 and 15, Test No. MGSSYP-2



Figure 56. Rail Damage Between Post Nos. 16 and 18, Test No. MGSSYP-2





Figure 57. Post Nos. 13 and 14 Damage, Test No. MGSSYP-2



Figure 58. Post Nos. 15 and 16 Damage, Test No. MGSSYP-2



Figure 59. Post Nos. 17 and 18 Damage, Test No. MGSSYP-2

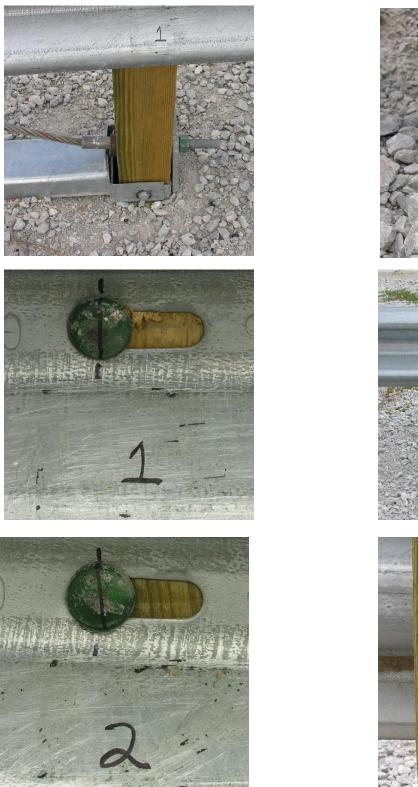




Figure 60. Upstream Anchor Damage, Test No. MGSSYP-2



Figure 61. Vehicle Damage, Test No. MGSSYP-2

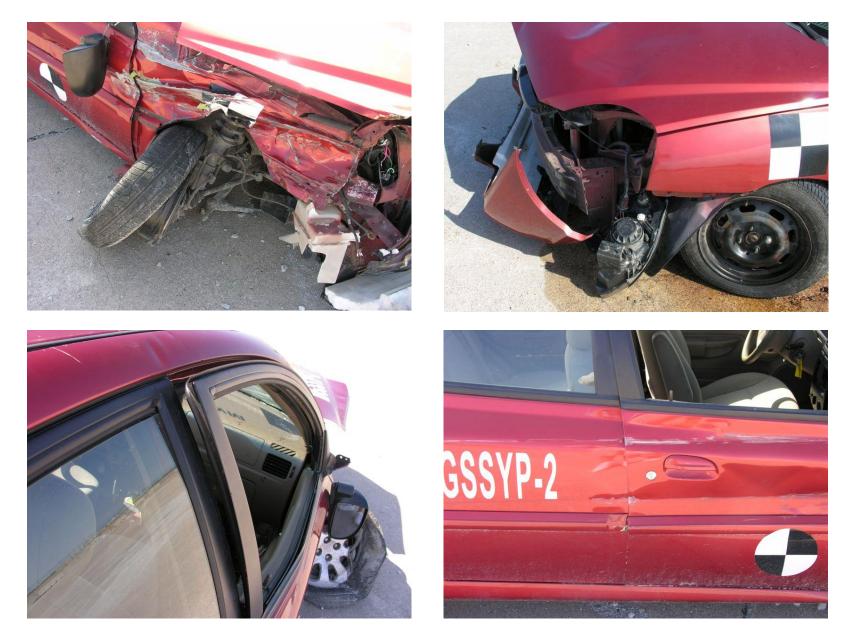


Figure 62. Vehicle Damage, Test No. MGSSYP-2

7 SUMMARY AND CONCLUSIONS

A non-proprietary, Southern Yellow Pine wood post, W-beam guardrail system was developed and crash tested according to MASH. The wood post MGS utilized 6-in. x 8-in. x 72in. (152-mm x 203-mm x 1,829-mm) Southern Yellow Pine posts instead of the standard W6x8.5x72 in. (W152x216x1,829 mm) steel posts. Two full-scale crash tests were performed according to the TL-3 safety performance criteria, as defined in MASH. Test no. MGSSYP-1 (test designation no. 3-11) consisted of a 5,199-lb (2,358-kg) pickup truck impacting the MGS with Southern Yellow Pine posts at a speed of 62.2 mph (100.1 km/h) and at an angle of 24.9 degrees. The vehicle was contained and smoothly redirected. Test no. MGSSYP-2 (test designation no. 3-10) consisted of a 2,612-lb (1,185-kg) small car impacting the wood post MGS at a speed of 61.5 mph (99.0 km/h) and at an angle of 25.3 degrees. The vehicle was contained and smoothly redirected. Thus, the MGS with Southern Yellow Pine posts was judged to be acceptable according to the safety performance criteria presented in MASH. A summary of the safety performance evaluation is provided in Table 14. The successful evaluation of the MGS with Southern Yellow Pine posts as a non-proprietary system may prevent State DOTs that already have an inventory of Southern Yellow Pine posts from having to invest in an inventory of specialized components for use in other systems.

The standard MGS has demonstrated acceptable safety performance when configured with either standard W6x9 (W152x13.4) or W6x8.5 (W152x12.6) steel posts [13-15], round wood posts [3], 6-in. x 8-in. (152-mm x 203-mm) White Pine wood posts [4], and now 6-in. x 8-in. (152-mm x 203-mm) Southern Yellow Pine wood posts. The different configurations have exhibited similar performance, as shown in Table 15. Therefore, the MGS configured with standard-sized, Southern Yellow Pine wood posts is an acceptable alternative to the previously-

recommended, steel post, round wood post, and rectangular White Pine wood post configurations.

Evaluation Factors		Eva	luation Criteria		Test No. MGSSYP-1	Test No. MGSSYP-2
Structural Adequacy	А.	Test article should contain and controlled stop; the vehicle sh installation although controlled la	nould not penetrate, und	S	S	
Occupant Risk	D.	Detached elements, fragments of penetrate or show potential for p an undue hazard to other traf Deformations of, or intrusions in limits set forth in Section 5.3 and	compartment, or present onnel in a work zone.	S	S	
	F.	The vehicle should remain uprig and pitch angles are not to exceed	ion. The maximum roll	S	S	
	H.	Occupant Impact Velocity (OIV calculation procedure) should sat				
		Occupa	S	S		
		Component	Preferred	Maximum		
		Longitudinal and Lateral	30 ft/s (9.1 m/s)	40 ft/s (12.2 m/s)		
	I.	The Occupant Ridedown Accele MASH for calculation procedure				
		Occupant F	Ridedown Acceleration Lir	nits	S	S
		Component	Preferred	Maximum		
		Longitudinal and Lateral	15.0 g's	20.49 g's		
		MASH Test Desig	gnation Number		3-11	3-10
		Pass/H	Fail		Pass	Pass

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Table 15.	Comparison	of MGS wi	th Steel and	Wood Post

		MGS								ĴŚ			
Perfor	mance Criteria	7¼-in. D Dougl Pos	as Fir	8-in. Dia Ponderos Pos	sa Pine	W6x9 St	eel Posts	W6x9 St	eel Posts		-in. White Posts	6-in. x Southern Pine l	Yellow
Te	est Criteria	NCHR	P 350	NCHR	P 350	NCHF	RP 350	MA	SH	MA	ASH	MA	SH
Test D	esignation No.	3-11	3-10	3-11	3-10	3-11	3-10	3-11	3-10	3-11	3-10	3-11	3-10
Test Vehicle		2000P [3]	820C ¹	2000P [3]	820C ¹	2000P [13]	820C [13]	2270P [14]	1100C [15]	2270P [4]	1100C ¹	2270P	1100C
Impact Severity kip-ft (kJ)		106.4 (144.3)	-	107.2 (145.3)	-	101.5 (137.7)	31.2 (42.3)	122.3 (165.8)	58.8 (79.7)	131.5 (178.3)	-	115.5 (156.6)	56.4 (76.4)
D	rmanent Set Deflections in. (mm)	35.5 (902)	-	27.8 (705)	-	26.0 (652)	9.4 (238)	31 ⁵ / ₈ (803)	19.9 (505)	33¾ (857)	-	30¼ (768)	16¼ (413)
2	nic Deflections in. (mm)	60.2 (1,529)	-	37.6 (956)	-	43.1 (1,094)	17.4 (443)	43.9 (1,115)	35.9 (913)	46.3 (1,176)	-	40.0 (1,016)	22.2 (564)
	rking Width in. (mm)	60.3 (1,531)	-	48.6 (1,234)	-	49.6 (1,260)	40.3 (1,023)	48.6 (1,234)	48.3 (1,227)	58.4 (1,483)	-	53.8 (1,367)	39.7 (1,008)
OIV ft/s	Longitudinal	13.22 (4.03)	-	22.47 (6.85)	-	18.32 (5.58)	11.55 (3.52)	15.32 (4.67)	14.83 (4.52)	-15.27 (-4.65)	-	-13.25 (-4.04)	-15.72 (-4.79)
(m/s)	Lateral	13.22 (4.03)	-	23.56 (7.18)	-	12.87 (3.89)	18.64 (5.68)	15.62 (4.76)	17.13 (5.22)	-16.14 (-4.92)	-	-14.74 (-4.50)	-20.93 (-6.38)
ORA	Longitudinal	8.76	-	5.90	-	9.50	6.13	8.23	16.14	-8.25	-	-8.14	-13.04
g's	Lateral	5.69	-	4.09	-	6.94	7.97	6.93	8.37	-10.13	-	-8.51	-9.30

¹This test was not conducted.

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8 IMPLEMENTATION GUIDANCE

8.1 Background

As previously noted, the research detailed herein demonstrated that the MGS utilizing 6in. x 8-in. x 72-in. (152-mm x 203-mm x 1,829-mm) Southern Yellow Pine posts, performed in an acceptable manner according to test designation nos. 3-10 and 3-11 of the MASH impact safety standards. However, several variations of the MGS system have been developed for special applications, which may be more sensitive to the use of wood posts. These special applications would include the MGS long-span system, MGS adjacent to 2:1 fill slopes, MGS on 8:1 approach slopes, MGS adjacent to a curb, MGS stiffness transition to approach guardrail transitions, MGS with reduced post spacing, and MGS without blockouts. Since several MGS variations are available, recommendations regarding the use SYP wood posts will likely vary depending on the nature and behavior of the special applications listed above. Implementation guidance and/or recommendations regarding the use SYP wood posts in these special applications are discussed below.

8.2 MGS Long-Span Guardrail

The MGS long-span guardrail system was successfully full-scale crash tested using an unsupported length of 25 ft (7.62 m) and three CRT posts with 12-in. (305-mm) deep blockouts adjacent to each end of the unsupported span [16]. These CRT posts were incorporated into the system in order to mitigate concerns for wheel snag on posts adjacent to the unsupported span when traversing from the unsupported span to the downstream standard guardrail. Adjacent to the CRT posts, the standard MGS utilized 12-in. (305-mm) deep blockouts. The MGS long-span guardrail system was installed with the back of the CRT posts positioned flush with the front face of the culvert headwall. The posts upstream and downstream from the culvert were installed 2 ft (610 mm) away from the slope break point of a 3:1 fill slope.

Occasionally, it may be desirable to attach a SYP wood post version of the MGS to the MGS long-span guardrail system. There are no concerns regarding the use of SYP wood posts in the MGS long-span guardrail system. The SYP wood-post version of the MGS performed in an acceptable manner when using the standard post spacing on level terrain and full-scale crash tested under the MASH TL-3 safety performance criteria using both the 1100C and 2270P vehicles. The maximum dynamic deflections of the MGS with W6x8.5 (W152x12.6) steel posts and SYP wood posts under MASH designation no. 3-11 were found to be 43.9 in. (1,115 mm) and 40.0 in. (1,016 mm), respectively. These results indicate that the relative deflection and stiffness of the wood and steel post versions of the MGS are very similar. As such, the SYP wood post version of the MGS long-span guardrail system when attached to guardrail beyond the upstream and downstream CRT wood posts. Therefore, it would seem reasonable to allow for the SYP wood post MGS to be attached to the MGS long-span guardrail system, as shown in Figure 63.

8.3 MGS Adjacent to 2:1 Fill Slopes

Previously, the 31-in. (787-mm) tall Midwest Guardrail System with 9-ft (2.74-m) long W6x8.5 (W152x12.6) steel posts was successfully crash tested under the MASH TL-3 criteria when installed at the slope break point of a 2:1 fill slope using standard post spacing and blockouts [17]. However, similar crash testing was not successful for the minimum recommended MGS mounting height of 27¾ in. (705 mm). As such, the minimum recommended top mounting height is unknown for the MGS adjacent to 2:1 fill slopes. Later and based on dynamic component testing, a wood post version of the MGS system was configured with 7.5-ft (2,286-mm) long, SYP posts and for use in shielding a 2:1 fill slope, as shown in Figure 64. For the SYP wood post variation, the embedment depth was 58 in. (1,473 mm). Based on this

previous research, it is highly recommended that the MGS with 7.5-ft (2,286-mm) long SYP wood posts adjacent to 2:1 fill slopes utilize a minimum top mounting height of 31 in. (787 mm).

8.4 MGS on 8:1 Approach Slopes

Previously, full-scale crash testing was successfully performed on the steel-post version of the MGS installed on an 8:1 approach slope with the W-beam positioned 5 ft (1.52 m) laterally behind the slope break point [18]. This testing program was conducted according to the NCHRP Report No. 350 impact safety standards using both an 820C small car and a 2000P pickup truck. From the crash testing program, the mounting height of the blocked MGS relative to the airborne trajectory of the front bumper and impact-side wheels was deemed critical for satisfactorily containing the 2000P pickup truck. Arguably, the test results may have also demonstrated that the 31-in. (787-mm) top railing height greatly contributed to adequate vehicle containment and stable redirection.

Based on the similar performance of the steel and wood post versions of the MGS system when tested on level terrain, there is little concern that the use of SYP wood posts would adversely affect the performance of the MGS on 8:1 approach slopes. Therefore, it is believed to be acceptable to install SYP wood posts with the MGS on an 8:1 approach slope using the previously-evaluated offset values, as shown in Figure 65.

8.5 MGS Adjacent to Curb

The steel post MGS was successfully crash tested and evaluated with the front face of the W-beam rail placed 6 in. (152 mm) behind the front face of a 6-in. (152-mm) tall concrete curb according to the NCHRP Report No. 350 TL-3 criteria using a 2000P pickup truck [19]. Based on the similar performance of the steel and wood post versions of the MGS system when tested on level terrain, there is little concern that the use of SYP wood posts would adversely affect the performance of the MGS installed adjacent to a curb. Therefore, it is believed to be acceptable to

install a SYP wood post MGS with the front face of the W-beam rail placed 6 in. (152 mm) behind the front face of a 6-in. (152-mm) tall concrete curb, as shown in Figure 66.

8.6 MGS Stiffness Transition to Approach Guardrail Transitions

Several options for approach guardrail transitions for the MGS system have been developed. As part of those efforts, a research project was conducted with the objective of identifying a wood-post MGS approach transition system that was equivalent to a previouslydesigned and full-scale crash tested steel-post MGS stiffness transition that utilized W6x9 and W6x15 steel posts [10]. A literature study on previous bogie testing and comparisons between wood and steel guardrail posts suggested that 6-ft (1.8-m) long, 6-in. x 8-in. (152-mm x 203mm) wood posts and W6x9 (W152x13.4) steel posts have similar force versus displacement characteristics. However, very little component testing had been previously conducted on larger transition posts. Thus, a bogie testing program was undertaken to determine the behavior of W6x15 (W152x22.3) steel posts and wood posts of various cross sections and embedment depths. Early in this bogie-testing program, the propensity for wood-post fracture in stiff soil was observed. As a result, the wood-post replacements were conservatively selected such that the cross section had excess strength capacity to minimize the risk of post fracture. Ultimately, 6.5 ft (2.0 m) long 8-in. x 10-in. (203-mm x 254-mm) wood posts provided similar resistance to rotation and were selected as the replacement for the 7-ft (2.1-m) long W6x15 (W152x22.3) steel transition posts.

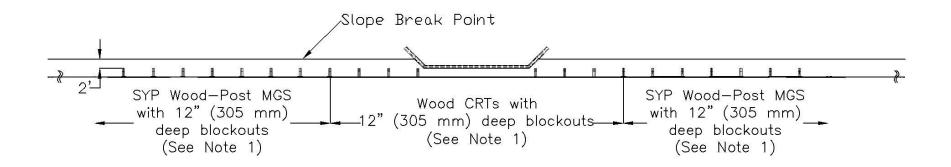
The steel-post MGS stiffness transition was found to satisfy all of the TL-3 safety performance criteria of MASH through a full-scale crash testing program. Since BARRIER VII analysis showed the proposed wood-post transition system behaved similarly and without increases in deflections, pocketing, or snag, it was believed that the wood-post transition system would also satisfy the TL-3 performance criteria of MASH. Therefore, the wood-post MGS stiffness transition was recommended for use as a TL-3 safety barrier. Full details on the wood post approach transition and recommendations for its use can be found in MwRSF research report no. TRP-03-243-11. In addition, it is believed that the use of the MGS with SYP wood posts in standard MGS guardrail upstream of the approach guardrail transition would be acceptable as well.

8.7 MGS with Reduced Post Spacing

A steel-post version of the MGS with quarter-post spacing was successfully full-scale crash tested and evaluated using a 2000P pickup truck according to the TL-3 criteria found in NCHRP Report No. 350 [19]. Subsequent analysis of the barrier system with BARRIER VII was used to develop details for a half-post spacing version of the MGS as well. As noted previously, the performance of the steel and wood post versions of the MGS system were found to be very similar in terms of stiffness and dynamic deflection. Thus, it is reasonable to assume that a SYP wood post MGS with reduced post spacing would provide similar performance to the previously evaluated steel post system.

8.8 MGS without Blockouts

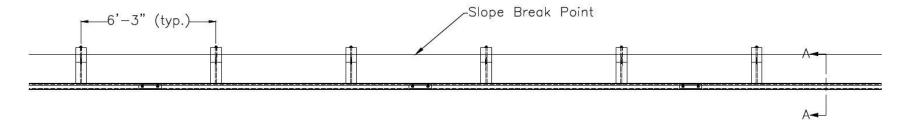
Over the years, MwRSF has crash tested several wood-post MGS systems with blockouts, including the rectangular, SYP wood posts evaluation detailed herein. These woodpost MGS systems provided acceptable safety performance without concerns for vehicular instabilities, excessive occupant ridedown decelerations, or critical occupant impact velocities. Based on the similar performance observed for the wood- and steel-post MGS systems with blockouts, there may be a desire for end users to install a non-blocked, wood post MGS. Unfortunately, no crash tests have been performed on non-blocked versions of the wood-post MGS. Wood and steel guardrail posts can provide slightly different behaviors when loaded through the W-beam rail and about the strong and weak axis of bending. Typical steel guardrail posts may rotate in soil, bend about one of the strong and weak axes near the ground line, or plastically deform from a combination of eccentric loading and/or lateral torsional buckling. Typical wood posts may also rotate in soil or fracture near the ground line. Based on these slight differences in post-soil behavior, there are some concerns that the removal of the blockout from the wood-post MGS may potentially lead to: (1) increased propensity for wheel snag on wood posts; (2) increased vehicle decelerations; and/or (3) greater risk of vehicular instabilities upon redirection. Thus, these outcomes could potentially result in degraded barrier performance. As such, it is not recommended to remove the blockouts from the wood-post MGS without further analysis and crash testing.



Note: (1) Back of post must be installed on level or mostly level soil grading 2 ft (0.6 m) away from the slope break point of a 3:1 or steeper fill slope. The back of the CRT posts can be flush with the headwall. The headwall cannot extend higher than 2 in. (51mm) above the ground line. The wingwall must match the fill slope.

Figure 63. MGS Long-Span System with SYP Wood Post MGS

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PLAN VIEW

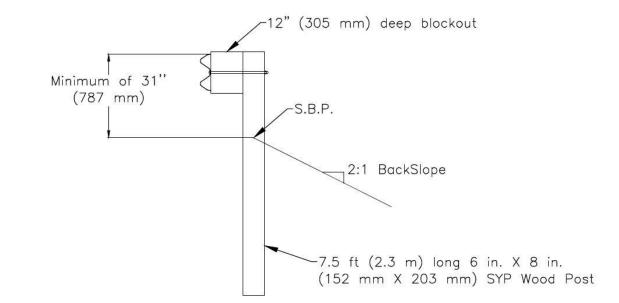


Figure 64. SYP Wood Post MGS Adjacent to 2:1 Fill-Slope

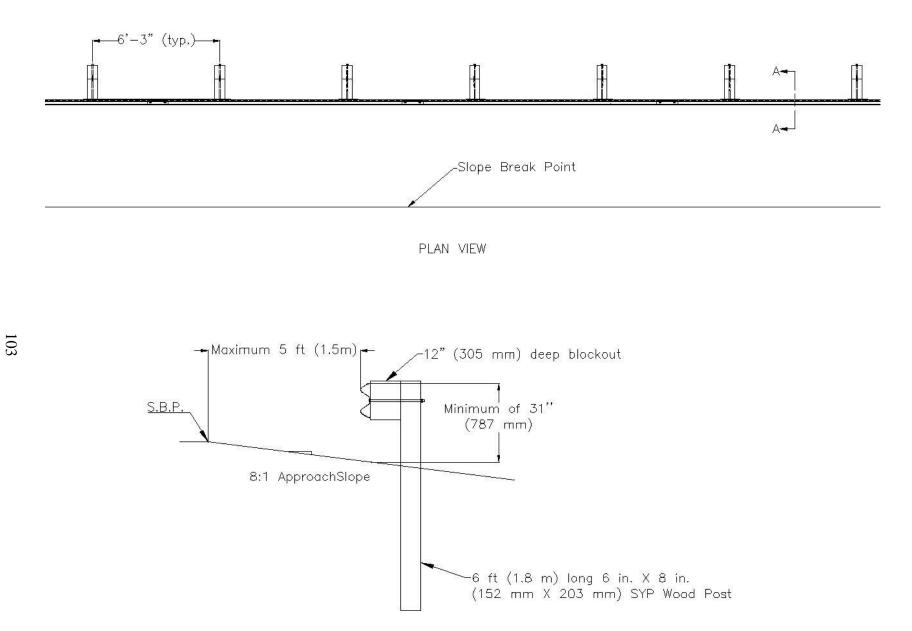


Figure 65. Use of SYP Wood Post MGS on 8:1 Approach Slope

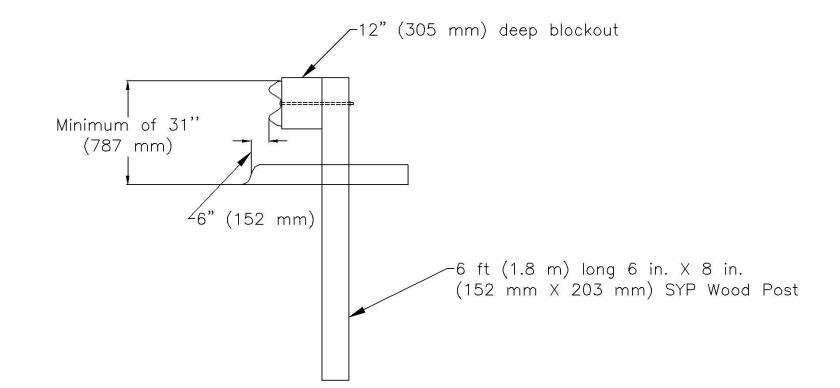


Figure 66. SYP Wood Post MGS Adjacent to Curb Cross-Section

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10 APPENDICES

Appendix A. Material Specifications

MGSSYP-1		
Description	Material Specification	Reference
6"x8"x72" [152x203x1829] Southern Yellow Pine Wood Post	SYP Grade No.1 or better	White Tag
6"x12"x14 1/4" [152x305x362] Blockout	SYP Grade No.1 or better	Yellow Tag
12'-6" [3810] W-Beam MGS Section	12 gauge [2.7] AASHTO M180	4614
12'-6" [3810] W-Beam MGS End Section	12 gauge [2.7] AASHTO M180	4614
6'-3" [1905] W-Beam MGS Section	12 gauge [2.7] AASHTO M180	10-0142-5
16D Double Head Nail	-	N/A
72" [1829] Long Foundation Tube	ASTM A500 Gr. B	090458-7
BCT Timber Post-MGS Height	SYP Grade No.1 or better	10-0282
Strut and Yoke Assembly	ASTM A36 Steel Galvanized	090453-8
BCT Cable Anchor Assembly	ø 3/4" 6x19 IWRC IPS Galvanized Wire Rope	Black Paint "A1
Anchor Bracket Assembly	ASTM A36 Steel	090453-10
8"x8"x5/8" [203x203x16] Anchor Cable Bearing Plate	ASTM A36 Steel	090453-9
2 3/8" [60] O.D.x 6" [152] Long BCT Post Sleeve	ASTM A53 Grade B Schedule 40	90458
5/8" Dia. x 1 1/4" [M16x32] Long Guardrail Bolt and Nut	ASTM A307 Steel/ Nut ASTM A563 DH	100144-1,3
5/8" Dia. x 10" [M16x254] Long Guardrail Bolt and Nut	ASTM A307 Steel/ Nut ASTM A563 DH	Black Paint
5/8" Dia. x 22" [M16x559] Long Guardrail Bolt and Nut	ASTM A307 Steel/ Nut ASTM A563 DH	Black Paint
5/8" Dia. x 1 1/2" [M16x38] Long Hex Head Bolt	ASTM A307 Steel/ Nut ASTM A563 DH	11-0006-3
5/8"Dia. x 9 1/2"[M16x241] Long Hex Head Bolt and Nut	ASTM A307 Steel/ Nut ASTM A563 DH	090453-11
5/8" [16] Dia. Flat Washer	ASTM A307 Steel	N/A
7/8" Dia. x 7 1/2" [M22x191] Long Hex Head Bolt and Nut	ASTM A307 Steel / Nut ASTM A563 DH	N/A
7/8" [22] Dia. Flat Washer	ASTM A307 Steel	N/A

Figure A-1. Bill of Materials, Test No. MGSSYP-1

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MGSSYP-2		
Description	Material Specification	Reference
6"x8"x72" [152x203x1829] Southern Yellow Pine Wood Post	SYP Grade No.1 or better	(TAGGED SPA BLUE PAINT) / (TAGGED WHITE PAINT)
6"x12"x14 1/4" [152x305x362] MGS Timber Blockout	SYP Grade No.1 or better	TAGGED GLOSS SUN YELLOW PAINT
12'-6" [3810] 4-Space W-Beam Guardrail	12 gauge [2.7] AASHTO M180	4614
12'-6" [3810] BCT Terminal Rail Section	12 gauge [2.7] AASHTO M180	4614 AND 3390
6'—3" [1905] W—Beam Spacer Guardrail	12 gauge [2.7] AASHTO M180	10-0142-5
16D Double Head Nail	_	SCAN 16d-1
72" [1829] Long Foundation Tube	ASTM A500 Gr. B	090453-7 AND 09-0458
BCT Timber Post-MGS Height	SYP Grade No.1 or better	TAGGED WHITE PAINT
Strut and Yoke Assembly	ASTM A36 Steel Galvanized	09-0453-8
BCT Cable Anchor Assembly	Ø 3/4" 6x19 IWRC IPS Galvanized Wire Rope	STAMPED "A1" AND BLACK PAINT
Guardrail Anchor Bracket	ASTM A36 Steel	090453-10
8"x8"x5/8" [203x203x16] BCT Bearing Plate	ASTM A36 Steel	090453-9
2 3/8" [60] O.D.x 6" [152] Long BCT Post Sleeve	ASTM A53 Grade B Schedule 40	09-0458
5/8" Dia. x 1 1/4" [M16x32] Long Guardrail Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	100144-1 (BOLTS)/ 10-0144-3 (NUTS) AND 12-0033 (NUTS)
5/8" Dia. x 10" [M16x254] Long Guardrail Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	09-0453-2 (Green Paint) / 12-0033 (NUTS)
5/8" Dia. x 22" [M16x559] Long Guardrail Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	10-0143(GLOSS NAVY BLUE PAINT) and 11 0490 (BLACK PAINT)/12-0033 (NUTS)
5/8" Dia. x 1 1/2" [M16x38] Long Hex Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	11-0006-3 (HEX BOLTS)/ 12-0030 (nuts)
5/8" Dia. x 9 1/2" [M16x241] Long Hex Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	BLACK PAINT (bolt)/12-0030 (nut)
5/8" [16] Dia. Plain Round Washer	ASTM A307 or Grade 2 Steel	09-0453-15/ N/A
7/8" Dia. x 7 1/2" [M22x191] Long Hex Bolt and Nut	Bolt ASTM A307 or Grade 2 Steel/ Nut ASTM A563 DH	110492 (bolts and nuts)/12- 0037(BOLT) and (NUT)12-0030
7/8" [22] Dia. Plain Round Washer	ASTM A307 or Grade 2 Steel	1JY82/12-0037
SOIL	350 SOIL	6222011

Figure A-2. Bill of Materials, Test No. MGSSYP-2



JULY 20, 2010

MIDWEST MACHINERY & SUPPLY MILFORD, NE

The following material delivered on 7/20/10 on bill of lading number 20254 has been inspected before and after treatment and is in full compliance with applicable Nebraska Department of Roads requirements for southern yellow pine Timber Guardrail Components, preservative treated with Chromated-Copper-Arsenate (CCA-C) to a minimum retention of .60 lbs/cu.ft. The acceptance of each piece by company quality control is indicated by a hammer brand on the end of each piece.

МАТ	ERIAL	CHARGE #	DATE	RETENTION	QUANTITY
6x8x6'	Line Post	10-342	7/1/10	0.62	105

THIS CERTIFICATE APPLIES TO MATERIAL ORDERED FOR your order no.: 2333 FOR ANY INQUIRIES, PLEASE RETAIN THIS DOCUMENT FOR FUTURE REFERENCE. THANK YOU FOR YOUR ORDER.

SINCERELY,

Korn & Sh Karen Storey

SIGNED BEFORE ME THIS 20 DAY OF JULY 2010.

Notary: Willie Floyd Johny Georgia My Commission Expires Oct. 19, 2010	NOTA AL NOTA AL VIBLIC COLUMITION
Phone: 706-234-1605	P.O. Box 99, Armuchee, GA 30105

Fax: 706-235-8132

Figure A-3. Southern Yellow Pine Posts, Test Nos. MGSSYP-1 and MGSSYP-2



SEP 17 2010

CERTIFICATE OF COMPLIANCE

SEPTEMBER 10, 2010

MIDWEST MACHINERY & SUPPLY MILFORD, NE

The following material delivered on 9/10/10 on bill of lading number 20374 has been inspected before and after treatment and is in full compliance with applicable Nebraska Department of Roads requirements for southern yellow pine Timber Guardrail Components, preservative treated with Chromated-Copper-Arsenate (CCA-C) to a minimum retention of .60 lbs/cu.ft. The acceptance of each piece by company quality control is indicated by a hammer brand on the end of each piece.

MAT	ERIAL	CHARGE #	DATE	RETENTION	QUANTITY
6x8x14"	OCD Blockout	10-456	8/31/10	0.75	280
51/2X71/2X421/2"	BCT Post	10-192	4/15/10	0.64	48
6x8x18"	Blockout	10-456	8/31/10	0.75	70
6x8x22"	Blockout	10-456	8/31/10	0.75	140

This certificate applies to material ordered for your order no.: 2355 For any inquiries, please retain this document for future reference. Thank you for your order.

SINCERELY,

Kom & Shy Karen Storey

SIGNED BEFORE ME THIS 10 DAY OF SEPTEMBER 2010.

Notary:	Willing SE	ali	NAM S. HOUS	NON	
	L) Hand Solar Notary Public Floyd Colar My Commission Expires (ty Georgia Oct. 19, 2010	AUBLIC		
			LO COUNTY.		

Phone: 706-234-1605

P.O. Box 99, Armuchee, GA 30105

Fax: 706-235-8132

Figure A-4. Southern Yellow Pine Posts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

PERMA-TREAT OF ILLINOIS, INC.

1800 PERMA-TREAT DRIVE, PO BOX 99 MARION, IL 62959 PH# 800.572.7384 FAX# 618.993.8680

This is to certify that the guardrail material has been treated and inspected according to the Iowa Department of Transportation Specification requirements and IM 462. Also, conforms to State of Illinois specification.

This material has been processed from Rough Sawn #1 Southern Yellow Pine.

Company:

Bill of Lading:

Title: Resident

Date: 5/10/11

Quantity	Description	Charge #	Date of Treatment	Treatment	MC prior to Treatment
30	6XBX7 aH	4835	4.4.11	.60 CCA-C	20%
30	6X8X7 2H	4800	12-6-10	.60 CCA-C	20%
30	GX8X7' 2H	4843	4-8-11	.60 CCA-C	20%
(OD)	6X8X6 CRT	4850	4-19-11	.60 CCA-C	20%
90	10×8×6 CRT	4845	4-15-11	.60 CCA-C	20%
252	6XIAXI4 IH	4844	4-12-11	.60 CCA-C	20%
288	6X8X18 SHTERE	4851	4-19-11	.60 CCA-C	20%
144	6×8×18 attime		4-12-11	.60 CCA-C	20%
				.60 CCA-C	20%
				.60 CCA-C	20%
				.60 CCA-C	20%
				.60 CCA-C	20%
\mathcal{A}	at of Minois, Inc	5		ARIZED	2
By: M				to and describe me this $\sqrt{0}$ d	

Before me this /D day of () day 2011 By Dava By OFFICIAL SEAL SARA BOND Official Seal My Commission Expires 01-31-2015

Figure A-5. Wood Blockouts, Test Nos. MGSSYP-1 and MGSSYP-2

2009 **GREGORY HIGHWAY PRODUCTS, INC.** 4100 13th St. P.O. Box 80508 1 Canton, Ohio 44708 X Test Report DATE SHIPPED: 05/07/09 B.O.L. # 39963 * UNIVERSITY OF NEBRASKA-LINCOLN Customer: Customer P.O. 4500204081/ 04/06/2009 401 CANFIELD ADMIN BLDG P O BOX 880439 Shipped to: UNIVERSITY OF NEBRASKA-LINCOLN TEST PANELS LINCOLN, NE. 68588-0439 Project : GHP Order No 105271 Yield Elong. Quantity Class Туре Description Tensile HT # code C. Mn. P. S. Si. 12GA 12FT6IN/3FT1 1/2IN WB T2 0.011 0.003 0.03 89432 67993 19.8 160 A 2 4614 0.21 0.84 Bolts comply with ASTM A-307 specifications and are galvanized in accordance with ASTM A-153, unless otherwise stated. Nuts comply with ASTM A-563 specifications and are galvanized in accordance with ASTM A-153, unless otherwise stated. All other galvanized material conforms with ASTM-123 & ASTM-525 All steel used in the manufacture is of Domestic Origin, "Made and Melled in the United States" All. Guardrail: and Terminal Sections meets AASHTO M-180, All structural steel meets AASHTO M-183 & M270 All Bolts and Nuts are of Domestic Origin All material fabricated in accordance with Nebraska Department of Transportation STATE OF OHIO: COUNTY OF STARK sion resistant Guardrail and terminal sections meet ASTM A606, Type 4. All controlled oxidized/get Sworn to and subscribed before me, a Notary Public, by Andrew Artar this 8th day of May, 2009. By: Andrew Artar Vice President of Sales & Marketing Gregory Highway Products, Inc. CYNTHIA K. CRAWFORD Notary Public, State of Ohio My Commission Expires 09-16-2012

Figure A-6. 12-ft 6-in. Long W-Beam, Test Nos. MGSSYP-1 and MGSSYP-2

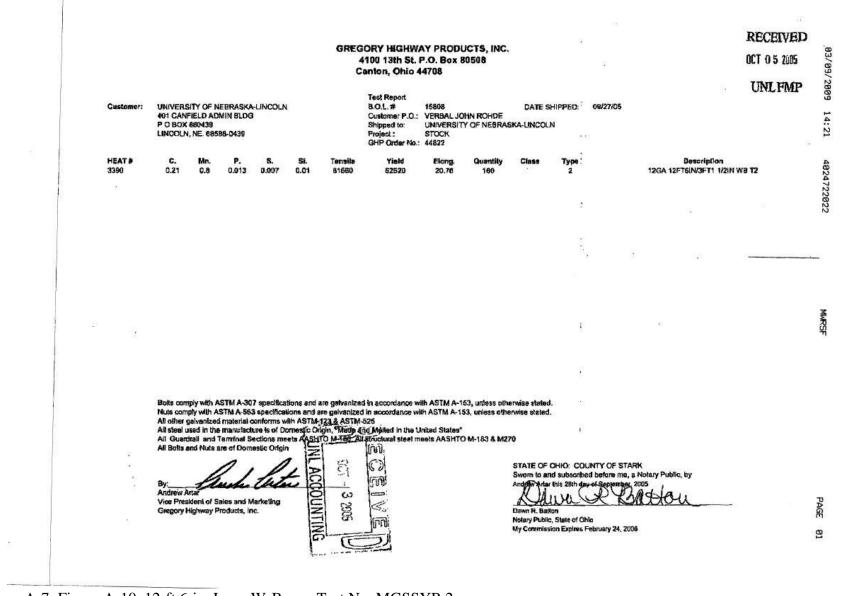


Figure A-7. Figure A-10. 12-ft 6-in. Long W-Beam, Test No. MGSSYP-2

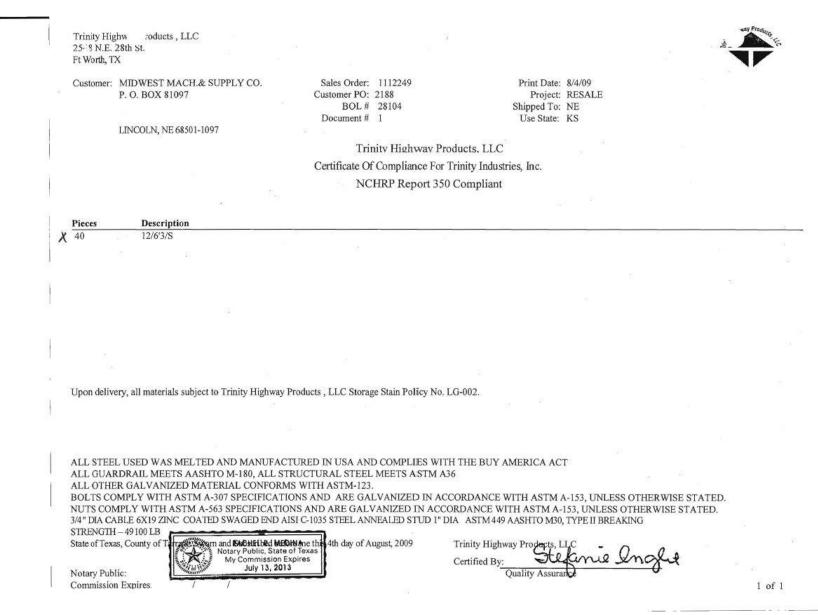
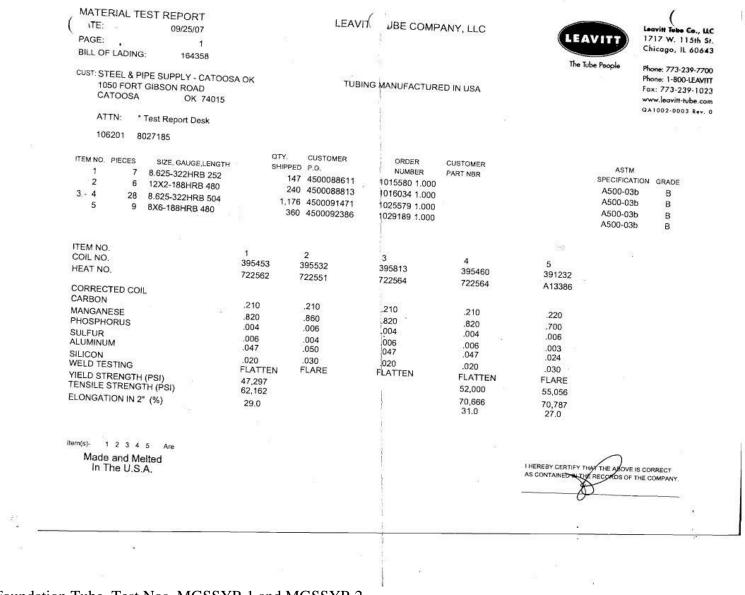


Figure A-8. 6-ft 3-in. Long W-Beam, Test Nos. MGSSYP-1 and MGSSYP-2



117

September 4, 2013 MwRSF Test No. TRP-03-272-13 Certified Analysis



As of: 5/22/09

 Mail
 Trioity Highway Products, LLC

 425 E. O'Connor
 Order Number: 1108107

 Lins, OH
 Customer PO: 2132

 Customer: MIDWEST MACH.& SUPPLY CO.
 BOL Number: 48341

 P. O. BOX 81097
 Document #: 1

 Shipped To: NE
 LINCOLN, NE 68501-1097

Project: STOCK

	Qty	Part#	Description	Spec	CL	TY	Heat Code/ Beat #	Vield	TS	Elg	С	Min	₽	S	Sł	Cu	Cb	Cr	Va .	ACW
-		1000 Aug 1000 Aug 100		M-	180 A	2.	C49037	64,600	88,600	21.2	0.210	0.880	0.010	0.000	0.030	0.080	0.000	0.060	0.010	4
8	25	736G	57TUBE \$1/.188"X6"X8"FLA	A-500	, ,		¥85912	56,500	72,980	37.0	0.210	0.778	0.009	0.006	0.016	0.010	0.00	0.020	0.001	4
	6	742G	60 TUBE SL/.188X8X6	A-508	1		¥85912	56,580	72,980	37.0	0.210	0.770	0.009	0.006	0.016	0.010	0.00	0.020	0.001	¢
	26	764G	1/4"X24"X24"SOIL PLATE	A-36			120039	46,660	73,630	26.9	0.190	0.520	0.012	0.003	0.020	0.090	0.00	0.040	0.000	4
	32	923G	BRONSTAD 98" W/O	M-180	A	2	122209	63,590	82,010	26.6	0.190	0.730	0.015	0.004	0.020	0.110	0.00	0.040	0.000	4
	4	927G	10/END SHOE/EXT	M-180	B	2	A\$14375	59,770	78,641	27.4	0.210	0.750	0.017	6.005	0.030	6.090	0.00	0.036	0.002	4

-3288	Upon delivery, all materials subject to Trinity Highway Products, LLC Storage Stain Policy No. LG-002.	
402-761	ALL STEEL USED WAS MELTED AND MANUFACTURED IN USA AND COMPLIES WITH THE BUY AMERICA ACT. ALL GUARDRAIL MEETS AASHTO M-180, ALL STRUCTURAL STEEL MEETS ASTM A36 ALL GALVANIZED MATERIAL CONFORMS WITH ASTM-123, UNLESS OTHER WISE STATED.	
36.1	BOLTS COMPLY WITH ASTM A-307 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED. NUTS COMPLY WITH ASTM A-563 SPECIFICATIONS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATED.	
16	3/4" DIA CABLE 6X19 ZINC COATED SWAGED END AISI C-1035 STEEL ANNEALED STUD I" DIA ASTM 449 AASHTO M30, TYPE II BREAKING STRENOTH 49100 LB	
06/04/2009	State of Ohio, County of Allen. Swom and subscribed before me this 22nd day of May, 2009 Trinity Highnest Products, LL Notary Public: June Hearling Commission Expires 11 28 17612	4 of 7

Figure A-10. Foundation Tube, Test No. MGSSYP-2

MIDNEST MACHINERY

TINNEN			
HMPEN	ND.	STI	EEL
FORMERLY M	STERM	V SALER	S. INC

This is to certify	that the materials shipped, a	s indicated, conform to t	he State of Nebrasl	a specifications.
Order Number:	89198			
Project Number				
OUANTITY	DESCRIPTION	CILADOD	TDEATMENT	TDEATED

QUANTITY	DESCRIPTION	CHARGE NO.	TREATMENT	TREATER
50	6x8-46" DSS SYP S4S BCT Post	38040	CCA	MWT
2. 81	21			
		£.		
5. 5.	an <u>u</u> ra a ^{na} t			
				6
0.0				
52				

MWT - MIDWEST WOOD TREATING, INC., NORWALK, OH MWT-OK - MIDWEST WOOD TREATING, INC., CHICKASHA, OK

Made & Treated in the USA. Meets AASHTO Spees M	133 & M168.
AMERICAN TIMBER AND STEEK	NOTARIZED
By Heather L. Seward falling Levace	Sworn to and subscribed before me
Title_Sales Assistant	this <u>13th</u> day of <u>April</u> 2010.
DateApril 13, 2010	by Lope Wilhelm
American Timber And Steel Corp 4832 Plank Rd / PO Box 767 Norwalk	A OH 44857 Ph. 4 Baces (10) Fax: 419 663 (10) 2014
"THE TIMBER	SPECIALISTS"

Figure A-11. BCT Timber Post, Test Nos. MGSSYP-1 and MGSSYP-2

	MIDWEST MACH & SUPPLY CO. P. O. BOX 81097 LINCOLN, NE 68501-1097	Sales Order: 1093497 Customer PO: 2030 BOL # 43073 Document # 1	Print Date: 6/30/08 Project: RESALE Shipped To: NE Use State: KS	
	Directar, 112 08301-1037	Trinity Highway P	mahuta IIC	
1 22	Cartificate		Inc. ** SLOTTED RAIL TERMINAL **	
	Certificate O	NCHRP Report 35	and the second sec	
		NCHRP Report 55	to Compliant	
ces	Description			
	5/8"X10" GR BOLT A307	an na Albana na Albana an Albana an Albana ga ang a Bana na Pangalan Albana an Albana.		
2	5/8"X18" GR BOLT A307			
	1" ROUND WASHER F844			
	1º HEX NUT A563		MPCAI	2
2	WD 60 POST 6X8 CRT	31	MGSBI	1
24	WD BLK 6X8X14 DR			
	NAIL 16d SRT			
	WD 3'9 POST 5.5X7.5 BAND			
	STRUT & YOKE ASSY			
8	SLOT GUARD '98		Ground Stru	+
1 11	3/8 X 3 X 4 PL WASHER		Created Serve	<i>c</i>
			. 090	453-8
dolian				
HE COLOC	ery, all materials subject to Trinity Highway	Products, LLC Storage State Poncy Ro	3. 123-002.	
STEEL	LUSED WAS MELTED AND MANUFAC	TURRO IN USA AND COMPLIES W	TTY THE BUY AMERICA ACT	
GUAR	RDRAIL MEETS AASHTO M-180, ALL ST	TRUCTURAL STEEL MEETS ASTM	A36	
	R GALVANIZED MATERIAL CONFORM		100	
			CORDANCE WITH ASTM A-153, UNLESS OTHERWISE STAT	TED.
			CORDANCE WITH ASTM A-153, UNLESS OTHERWISE STATE	
			" DIA. ASTM 449 AASHTO M30, TYPE II BREAKING	
TS COM		an crussosan Anna and a lub l	DIA ADDRESS ADDA I LEDI DROMANO	
TS COM	-4910018			
TS COM DIA CA ENOTH	- 49100 LB	a statistic day of two 2000		10
TS COM DIA CA ENOTH	- 49100 LB o, County of Allen. Swom and Subscribed befor	entethis 30th day of June, 2008	- Illa	R
IS COM DIA CA ENOTH	- 49100 LB	smethis 30th day of June, 2008	Trinity Highway Products, LLC HARLOW	K

Figure A-12. Strut and Yoke Assembly, Test Nos. MGSSYP-1 and MGSSYP-2

	Carlora V a V	within the
	Certified Analysis	AND THE
Trinity Highway Products, LLC		
.550 East Robb Ave.	Order Number: 1145215	
Lima, OH 45801	Customer PO: 2441	Asof: 4/15/11
Customer: MIDWEST MACH.& SUPPLY CO.	BOL Number: 61905	AS01;4/15/11
P. O. BOX 703	Document #: 1	
	Shipped To: NE	
MILFORD, NE 68405	Use State: KS	
Project: RESALE		
		#5
Qty Part# Description Spec 25 980G T10/END SHOE/SLANT A-1011-SS	CL TY Heat Code/ Heat # Yield TS Elg C Mn A57723 49 000 64 500 348 0000 0 326 0	P S Si Cu Cb Cr Vn ACW
55 WEG TREED BLOSDENNT MILITISS	A57723 49,000 64,500 34.8 0,080 0.350 0	018 0.005 0.020 0.090 0.00 0.060 0.001 4
¥		
Upon delivery, all materials subject to Trinity Highway P	Products , LLC Storage Stain Policy No. LG-002.	
ALL STEEL USED WAS MELTED AND MANUFACTURE	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT	
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL STI ALL COATINGS PROCESSES OF THE STEEL OR IRON A	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 ARE PERFORMED IN USA AND COMPLIES WITH THE "BLIV AMERICA ACT"	
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL STI ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 ARE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED.	
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATIO	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 .RE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNL	ESS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION NUTS COMPLY WITH ASTM A-563 SPECIFICATION	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNL NS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-152, 100 D	COTURNUM COLUMNS
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL STI ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-563 SPECIFICATION WASHERS COMPLY WITH ASTM F-436 SPECIFICATION 3/4" DIA CABLE 6X19 ZINC COATED SWAGED BND AI	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE INS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL STI ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION NUTS COMPLY WITH ASTM A-563 SPECIFICATION WASHERS COMPLY WITH ASTM A-563 SPECIFICATION	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNL NS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-152, 100 D	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM A-366 SPECIFICATION WASHERS COMPLY WITH ASTM F-366 SPECIFICATION 3/4" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 RE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE NS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE NAND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM A-366 SPECIFICATION 34" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB State of Onio, County of Allen Swonhand subscribed before Notary Public:	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE INS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR THE STATE ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM F-436 SPECIFICATION 34" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 RE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE NS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE NAND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM A-366 SPECIFICATION 34" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB State of Onio, County of Allen Sworthand subscribed before Notary Public:	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE INS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR THE STATE ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM A-366 SPECIFICATION 34" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB State of Onio, County of Allen Sworthand subscribed before Notary Public:	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE INS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR THE STATE ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM A-366 SPECIFICATION 34" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB State of Onio, County of Allen Sworthand subscribed before Notary Public:	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE INS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR THE STATE ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM A-366 SPECIFICATION 34" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB State of Onio, County of Allen Sworthand subscribed before Notary Public:	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE INS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR THE STATE ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM A-366 SPECIFICATION 34" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB State of Onio, County of Allen Sworthand subscribed before Notary Public:	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE INS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR THE STATE ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.
ALL STEEL USED WAS MELTED AND MANUFACTURE ALL GUARDRAIL MEETS AASHTO M-180, ALL ST ALL COATINGS PROCESSES OF THE STEEL OR IRON A ALL GALVANIZED MATERIAL CONFORMS WITH BOLTS COMPLY WITH ASTM A-307 SPECIFICATION WASHERS COMPLY WITH ASTM A-363 SPECIFICATION WASHERS COMPLY WITH ASTM A-366 SPECIFICATION 34" DIA CABLE 6X19 ZINC COATED SWAGED END AI STRENGTH - 49100 LB State of Onio, County of Allen Sworthand subscribed before Notary Public:	D IN USA AND COMPLIES WITH THE BUY AMERICA ACT. RUCTURAL STEEL MEETS ASTM A36 IRE PERFORMED IN USA AND COMPLIES WITH THE "BUY AMERICA ACT" ASTM-123, UNLESS OTHERWISE STATED. DNS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE INS AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM A-153, UNLE I AND/OR F-844 AND ARE GALVANIZED IN ACCORDANCE WITH ASTM F-2329 SI C-1035 STEEL ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR THE STATE ANNEALED STUD 1" DIA ASTM 449 AASHTO M30, TYPE II BR	SS OTHERWISE STATED.

Figure A-13. BCT Cable Anchor Assembly, Test Nos. MGSSYP-1 and MGSSYP-2

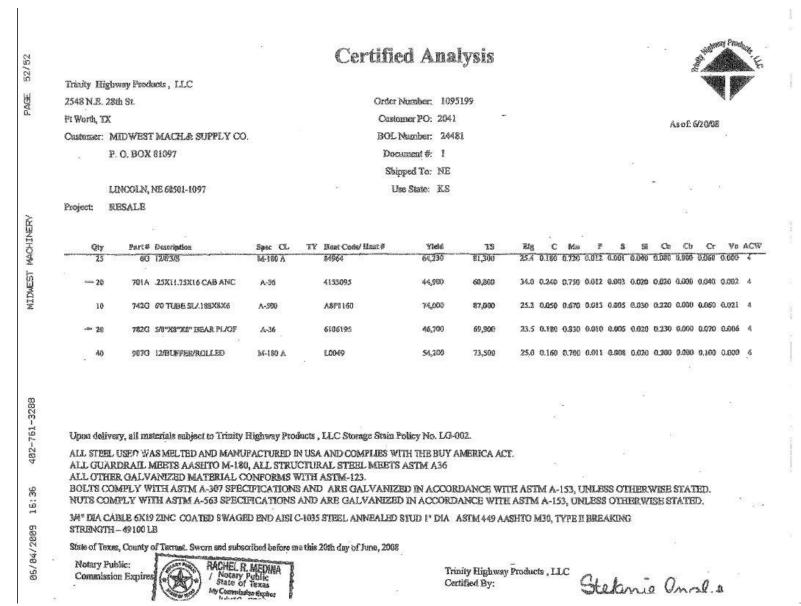


Figure A-14. Anchor Bracket Assembly, Test Nos. MGSSYP-1 and MGSSYP-2

122

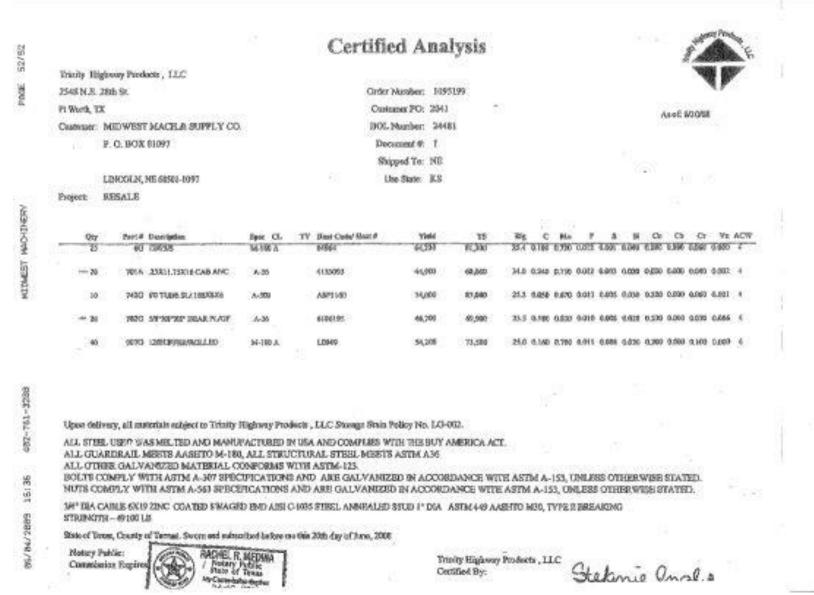


Figure A-15. Anchor Cable Bearing Plate, Test Nos. MGSSYP-1 and MGSSYP-2

123

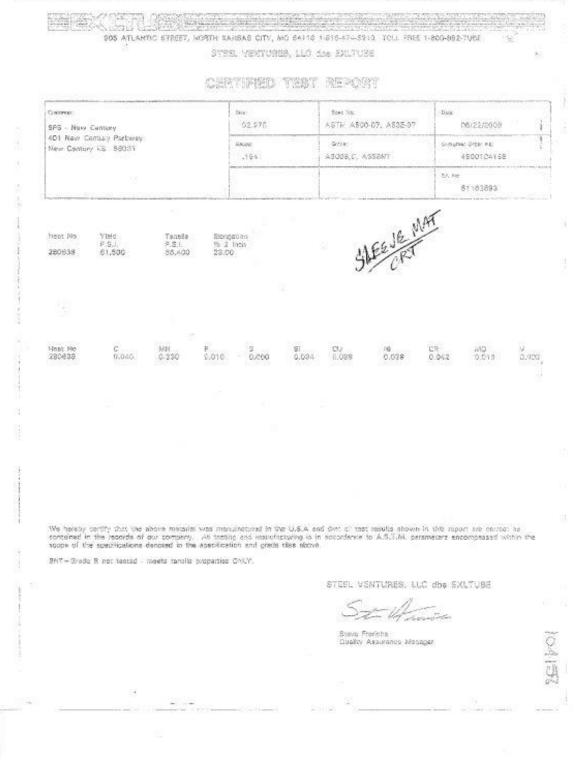


Figure A-16. BCT Post Sleeve, Test Nos. MGSSYP-1 and MGSSYP-2

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Figure A-17. 5/8-in. x 11/4-in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2

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Figure A-19. 5% in. Nut, Test Nos. MGSSYP-1 and MGSSYP-2

11/04/2009 06:18 402-761-3288 MIDWEST MACHINERY PAGE 07/10 A CHELLER Trinity Metals Laboratory A DIVISION OF TRINITY INDUSTRIES 4001 IRVING BLVD. 75247 - P.O. BOX 568687 DALLAS, TX 75358-8887 Phone: 214.589.7501 FAX: 214.589.7584 Lab No: 9080059F Completion Date: 08/10/2009 Weld Spec: Material Type: A 553 A Material Size: 5/5" GR Nuta 3340B Received Date: 08/07/2009 Head Code: Head Number: 5072060 PO or Work Order: 55:50053 Teet Spac: F806 ASTM METHODS Other Information: Lot # 090717N2 SUE HENLINE TRENTLY HWY PRODUCTS, LLC #55 ROLLFORM LIMA, OH 45801 HARDNESS TEST: 1 1 PASSED Measured Value Measured Amt Hardness Type: HARDNESS ROCKWELL BW Measured Value 89 Hardness Location: SURFACE of WRENCH FLAT - A Hardness Average: 88.5 Mossured Volue 88 PASSED **Measured Value** Hardness Type: HARDNESS ROCKWELL BW Measured Amt Hardnots Location: SURFACE of WRENCH FLAT - B Measured Value 92 Herdness Average: 92 Measured Value 92 PASSED Measured Value Measured Amt Hardness Type: HARONESS ROCKWELL BW Herdness Losetion: SURFACE of WRENCH FLAT - C Measured Value 85 Hardness Average: 87.5 Messured Value 87 PASSED Measured Value **Measured Amt** Hardness Type: HARDNESS-ROCKWELL BW ans Location: SURFACE of WRENCH FLAT - D Measured Value 90 Hardnees Average: 88.5 Measured Value 89 We cortly the above results to be a true and accurate representation of the sample(s) submitted. Alteration or partial reproduction of this report will void cortification. NVLAP Cortificate of Accorditation offsettive through 12-31-09. This report may not be used to claim product cortification, approval, or and swement by NVLAP, NIST, or any agency of the federal government. This LOD Page 1 of 2

Figure A-20. 5% in. Nut, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

Frinity Metals Laboratory . DIVISION OF TRINITY INDUSTRIES 001 IRVING BLVD. 75247 - P.O. BOX 568887 ALLAS, TX 75359-8887 homx 214.689.7591 FAX: 214.689.7564	Armady.	2		•
LAD NO: 9080039F SUE HENLINE RINTY MAY PRODUCTS, LLC #85 OLLFORM MA, OH 45801	Received Dele: 08/07/2009 Heat Code: Heat Number: 5072080 PC or Work Order: 55-50083 Text Spor: F606 ASTM M Other Information: Let # 09071	ETHODS		9 g
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Figure A-21. 5% in. Nut, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

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Figure A-22. 5% in. Nut, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

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Figure A-23. ⁵/₈ in. Nut, Test No. MGSSYP-2

I rinity Metals Laboratory A GWISION OF TRINITY INSUSTRIES 1001 IFWING BLVD. 7547 - P.O. BOX 56867 DULAS, TX 7538-8487 Prome: 214 548 7591 FAX: 214 549,7594	Alara A		VIA0
Lab No: 11040021F KEITH HAMBURG IRINTY HWY PRODUCTS, LLC #55 YOLLFORM WALFORM HISO1	Reserved Oate: 04/04/2011 Heat Code: Heat Number: 20131460 8 J PC or Work Oxten: 10318N2 Test Spec: F606 ASTM 3 Other Information: 05-61587	Material Size	2
HARDNESS TEST:			
	No. of Market	Manage of Aust	PASSED
Hardness Type: HARDNESS ROCKWELL BW	Measured Value	Measured Amt	
Hardness Location: Surface of Wrench Flat A Hardness Average: 88.5	Measured Value	87	
16.02		-	
Hardnass Type: HARDNESS ROCKWELL BW	Measured Value	Measured Amt	PASSED
Hardness Location: Surface of Wrench Flat B	Measured Value	14	
Hardness Average: 84	Measured Value	84	
Hardness Type: RARDNESS ROCKWELL BW	Measured Value	Measured Amt	PASSED
Hardness Location: Surface of Wrends Flat C	Measured Value	87	
Hardness Average: 87	Measured Value	87	
Hardness Type: HARDNESS ROCKWELL BW	Measured Value	Measured Amt	PASSED
Hardness Location: Gurlace of Wiench Flat D	Measured Value	47	
Hardness Average: 87.5	Measured Value	85	
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	d.Du.J	20	
e certify the above results to be a true and accurate report port will void certification. WHAP Certificate of Accessitat riffication, approval, or endorsement by WHAP, NIST, or	servation of the sample(s) submitted ion effective through 12-31-11. This re any agency of the federal governme	Alteration or partial reprodu- port may not be used to char it Which like IS Let Director, Horae 5, Serier, FE	ction of this n product
	Page 1 of 2		
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Figure A-24. 5% in. Nut, Test No. MGSSYP-2 (cont.)

rinity Metals Laboratory Downen of Tenny Houstres Col RVING BLVD, 75947 - P.O. BOX 56887 MLAS, TX 7556-6857 Tene: 214.589.7591 FAX: 214.569.7594	Kinig. B NSB A NSB A		ylaqi
AD NO: 11040021F EITH HAMBURG RINTY HWY PRODUCTS, LLC #55 DLL-ORM MA, CH 45801	Received Date: 04/04/2011 Heat Code: Heat Norther: 20131460 8.2 PO or Work Order: 10/031802 Test Spec: 7606 ASTM & Other Information: 55-61507	Material Size	1
			PASSED
Haleneys Type: HARDNESS ROCKWELL RM	Measured Value	Measured Amt	
Hardness Location: Surface of Wrench Flat E	Measured Volue	87	
Hardness Average: 86.5	Measured Value	80	
OTHER TEST:			
Type: NUT PROOF LOAD (to 30K)		Quant	ty amount: 5
Samples PASSED proof loads of 16,950 l	lbs.		
Type: HEAD MARKINGS		Quant	ty amount: 1
TRN N		- 4	
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Figure A-25. 5% in. Nut, Test No. MGSSYP-2 (cont.)

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Figure A-26. ⁵/₈ in. x 10 in. Bolt, Test Nos. MGSSYP-1 and MGSSYP-2

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	Mid West Fabricating C	ompany		
$() _{\mathcal{M}}$	Rockmill Division 115 West Fair Avenue ancaster, OH 43130 740) 681-4411	Lab Test Re	port	
		Data Re	asa1946	
	ite: 24-Sep-08	Semple I: Sample I:	2.65	
Part Numb	ler; 10-5	Sample 3:	2.63	
Descripti	on: 10" POST BOLT W/6" THRD	Sample 4:	2.95	
Lot Mumb	her: \$5217	Sample St	3.26	3
Custom	eer Trinity	Szunpla 5:	2.13	
Tast 1)	pe: Permiscope	Sumple 7:	3.12	
Heat Numb	ver: 7261611	Semple 8:	2.64	
Process	wr: Columbus	Sample S:	3.50	
	W2: ASTM=A153-A153/98	Sample 101	3.71	
100		Semple 3.1;	2.15	
	90C 1.77 Mil	Sample 1.2:	2.73	
Sample (Sample 131	3.01	
Dispositi	ion: Ship	Semple 14:	2.70	
Ship.	ID: XB9	Sample 15: Sample 16:	3,28	
		Sample 171	3.12	
		Semple 18:	2,39	
		Sampia 29:	2.44	
123		Sampla 20:	2.58	
		Average:	2.64	
Conform	nance ·		14	
Non-Co	nformance	Parformed By: D.Smith		
				3
This report sh	all not be reproduced, except in full	, without the writins approval	i of	
	Mid West Fabricating Company's Q	uality Dopartnessvi.		8
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				3 <i>8</i> :

Figure A-27. 5/8 in. x 10 in. Bolt, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

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MIDWEST MACHINERY

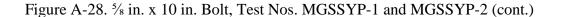
Mid West Fabricating Company **Rockmlil Division** 3115 West Fair Avenue Lancester, OH 43130 (740) 581-4411

Lab Test Report

			Data R	esults
Daber	24-Sep-08		Sample 1:	\$5.20
Part Number:	10-6		Sample 2:	86.80
	W.S		Sample 3:	65.40
	10" POST BOLT W/6" THRO		Sample 41	85.90
Lot Aumber:	85217		Sample St	85,66
Castomer	Trinity		Sample &	00,00
Test Type:	Rociewell		Sample 7:	0.00
Heat Mumber:	7261611		Sumple 8:	0.06
Processor	Columbus		Sample 91	0.00
			Sample 10:	0.00
Testing Standard:	ASTM=E18-98		Sample 11:	0.00
Aequirement:	69-100 "S"		Sample 12:	0.00
Sample Qty:	5	8	Sumple 13:	0.00
Disposition:	Screp	625	Sample 14:	0.00
Stein 7D:			Sumple 18:	0.00
			Security 16:	0.90
			Sample 17:	6.00 .
XII			Sample 28:	00.0
			Sampla 19:	0,00
			Sampia 20;	0.00
			Avarages	85.80
 Conforman 	ice			
Non-Confo	mance	Burlan	od For D.Solt	ħ

Performed By: 0.Smith

1.14 S 6. This report shall not be repreduced, accept in full, without the writkes opproval of Bild Wast Pabricating Company's Quality Department.



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Mid Rock 3115 Lanca (740)

Mid West Fabricating Company Rockmill Division 3115 West Pair Avenue Lancester, OH 45130 (740) 681-4412

2

ab Test Repor	
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		Data I	lesuits
Date:	24-Sep-08	Sumple 1:	16,850.00
Part Number:	16-6	Sample 2r	17,378.00
		Sample 3;	17,190.00
	10" POST BOLT W/6" THRD	Semple 4:	17,900.00
Lot Number:	85217	Sample 5:	17,300.00
Customer:	Trinity	Semple 6:	0.00
Test Type:	Rockwell	Sample 71	0.00
Heat Number:	7251611	Sample 8:	0.00
Processart		Sample 9:	0.00
		Sample 10:	0,90
Testing Standard:	ASTM#:F606-958	Sample 11:	0,00
Requirements		Santpha 12:	0.00
Sample Qty:	5	Sample 33:	0.00
Disposition:	Screp	Sample 14:	00,00
Ship 1D:		Semple 15t	0.00
		Sumple 15:	0.00
		Sample 17:	0.60 ,
	15	Sample 18:	0.00
		Sample 19:	0,60
	83	Sample 201	0.00

Conformance

Non-Conformance

Performed By: 0.9mith

Average: 17,242.00

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Figure A-29. ⁵/₈ in. x 10 in. Bolt, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

-	+							
			INSPECTIC	N CERTIFICATE				
			126 N ROCKF	BOLT & STEEL CO. NLL STREET ORD, IL 61101 - FAX# 815-958-3111				
	CUSTOMER NA	ME:	BENNETT BOLT WORKS	ß				
	CUSTOMER P.O	D.:	6008015					
	INVOICE #:	945308	3	DATE SHIPPED:	2/3/11			
	LOT #:	21306	3					
	SPECIFICATION	N:	ASTM A307, GRADE A M	ILD CARBON STEEL B	OLTS			
			TENSILE RESULTS:	SPECIFICATION 60,000 min.	ACTUAL 77,730 77,787	75,314		
2			HARDNESS RESULTS:	SPECIFICATION 100 MAX	88.80 90.83	85,46 86,83		
	COATING: AS	STM SPE	CIFICATION F2329 HOT D	P GALVANIZE				
	STEEL SUPPLI	ER:	NUCOR, NUCOR				2	<i>%</i>
	HEAT NO. NF	1010253	801, NF1020257001			<u>案</u>):		
	QUANTITY AND	DESCR	IPTION:					
	500 PC	S 5/8" X	22" GUARD RAIL BOLT					
	AND MANUFACTURED BY THE MATERIALS SU	IN THE U.S. A PPLIER, AND ROER MEET	BOLTS HAVE BEEN MANUFACTURE WE FURTHER CERTIFY THAT TH 5 THAT OUR PROCEDURES FOR TH OR EXCEED ALL APPLICABLE TES	IS DATA IS A TRUE REPRESENT E CONTROL OF PRODUCT QU	TATION OF INFO ALITY ASSURE T IN-REQUIREMEN	DRMATION PROV PHAT ALL ITEMS ITS PER ABOVE	IDED	
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Figure A-30. ⁵/₈ in. x 22 in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2

06/14/11 03:40 PM 315-689-3999 V1a VSI-FAX Page 3 of 7 #2120 | Mill Certification Details NUCOR NUCOR CORPORATION NUCOR STEEL NEBRASKA Mill Certification Details - 8/19/2010 8:47 AM Customer: KING STEEL CORP - GRAND BLANC Bill of Lading #: 178801 Chief Metallurgist : Jim Hill Date: 7/13/2010 Heat # : NF1010253801 Tag # : NF1011097050 Product WIRE Size : 304-147 Product : WIRE Division : Norfolk, NE Size : .594-19/32 Wire Rod Comments : Billet Heat #1 NF10102538 Chemical Properties -WL% 0 0000 0.001 **Physical Properties** Tensile: Yield: Elongation (in 8 inches): Elongation (in 2 inches): The testing was conducted in accordance with the requirements of this specification. All melting and manufacturing processes were performed in the United States of America. AmthOD Jim Hill Division Metal project 11.3 (8 (10.26)

Figure A-31. 5% in. x 22 in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

Page 5 of 7 #2120 i

Mill Certification Details NUCOR NUCOR CORPORATION NUCOR STEEL NEBRASKA Mill Certification Details - 8/5/2010 11:22 AM Customer: KRUEGER & CO - ELMNURST Bill of Lading #s-179281-----
 Chief Metallurgist : Jim Hill
 Date : 7/13/2010

 Heat # : NF1020257001
 Tag # : NF1011097111

 Product : W;RE
 Size : .594-19/32 Wire Rod
 Grade: 1010 Division : Norfolk, NE Billet Heat #: NF102025/0 Comments : Chemical Properties -Wt.% 9.0000 0.001 **Physical Properties** Tensile: Yield: Elongation (in Binches): Elongation (in 2 inches): The testing was conducted in accordance with the requirements of this specification. All melting and manufacturing processes were performed in the United States of America. AmthOD Jim Hill D-vision MetaFurgist

Figure A-32. ⁵/₈ in. x 22 in. Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

5/ 10

	10-05-09;04:15PM;Benn	ett-Bolt-Works	Midwest M	achinery	:31568	393999	
			77				
		INSPECTIC					
		126 N ROCKE	BOLT & STEEL CO. IILL STREET ORD, IL 61101 FAX# 815-968-3111				
	CUSTOMER NAME:	BENNETT BOLT WORKS	S a				
	CUSTOMER P.O. :	6005874					
	INVOICE #: 941845	1. 17	DATE SHIPPED:	7/24/09			
	SPECIFICATION:	ASTM A307, GRADE A M	LD CARBON STEEL B	OLTS			
		TENSILE RESULTS:	SPECIFICATION 60,000 min.		75,053 74,699		76,876 76,938
		HARDNESS RESULTS:	SPECIFICATION 100 MAX	81.22	86.60 85.25	85.95 87.10	81.62 81.00
	COATING: ASTM SPE	CIFICATION F2329 HOT D	P GALVANIZE				
	STEEL SUPPLIER:	NUCOR, NUCOR, NU	JCOR, NUCOR				
1	HEAT NO. 848653, 7	49237, 849289, 846672		1			
	QUANTITY AND DESCR	UPTION:					
	600 PCS 5/8" X	22" GUARD RAIL BOLT					
	AND MANUFACTURED IN THE U.S./ BY THE MATERIALS SUPPLIER, AN	BOLTS HAVE BEEN MANUFACTUR A. WE HURTHER CERTIFY THAT TH D THAT OUR PROJEDURES FOR TH T OR EXCEED ALL APPLICABLE TRS	IS DATAIS A TRUE REPRESEN IE CONTROL OF PRODUCT OU	ITATION OF INF ALITY ASSURE	ORMATION THAT ALL IT	PROVIDED	TED
	STATE OF ILUNCIS COUNTY OF WIMMEBAGO STONED BEFORE ME ON THIS 2704 DAY OF JULIS (JUDO) A. BE		Jenda Me APPROVED SIGNAT	lonas orv	76 DATE	7/09	73
	OFFICIAL, SEAL USA A, BERG Notary Public: State of Illinois My Commission Expires Dec 11, 20						

4 FAC JRED BY ROCKORDER THUS DATA IS A THIS THUS DATA IS A THIS THUS DATA IS A THIS

Figure A-33. ⁵/₈ in. x 22 in. Bolts, Test No. MGSSYP-2

BALLEST

	10-05-09:04:15PM;Bennett-Bolt-Works Midwest Machinery ;3156893999	# 6/ 10
0	NUCOR HAR MILL GROUP	
	Mill Certification Details - 2/11/2009 9:43 AM	
	Customer: KING STORL Bill of Lading #:	
ł	Chief Metallurgijst : Jim Hill Date : 1/11/2009 Heat # : 848053 Tag # : 12172921A Product : Wire Rod Size : .594-19/32 Grade : 1010 Division : Norfelk, NG	
î	Comments ; Test conform to ASTM A29, ASTM 6415 and ASTM E1019-resulphonized grades. Certification: 0780-01 Expires: 02/28/09 Coarse Grain Printiple	
	Chemical Properties -WL96	
	Physical Properties Freedory Part 2 days Tensile: 66,201 456	
•	Yield: 47,546 338 Elongation (in 8 inches): 26 % 26 Biongation (in 2 inches):	
	Reduction Ratio: 159:1	
	in the second	
	The testing was conducted in accordance with the requirements of this specification. All melting and manufacturing processes were performed in the United States of Amorica.	
	Jim Hill D'vision Metal urg at	
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Figure A-34. ⁵/₈ in. x 22 in. Bolts, Test No. MGSSYP-2 (cont.)

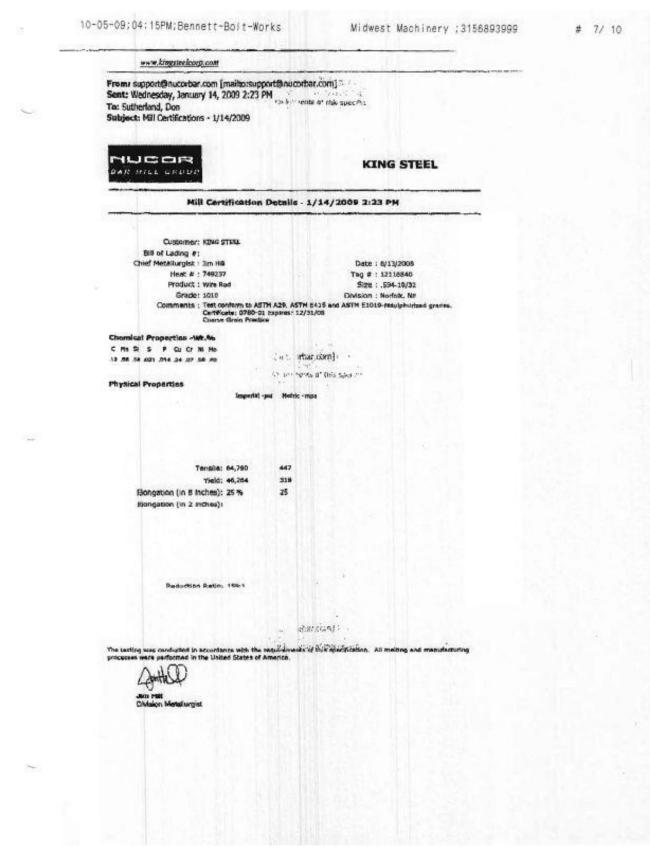


Figure A-35. ⁵/₈ in. x 22 in. Bolts, Test No. MGSSYP-2 (cont.)

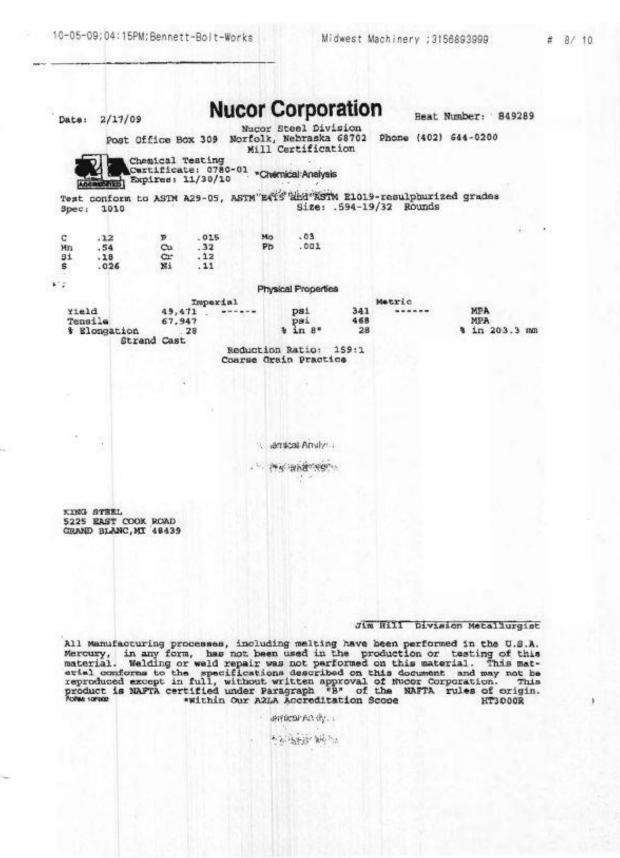


Figure A-36. ⁵/₈ in. x 22 in. Bolts, Test No. MGSSYP-2 (cont.)

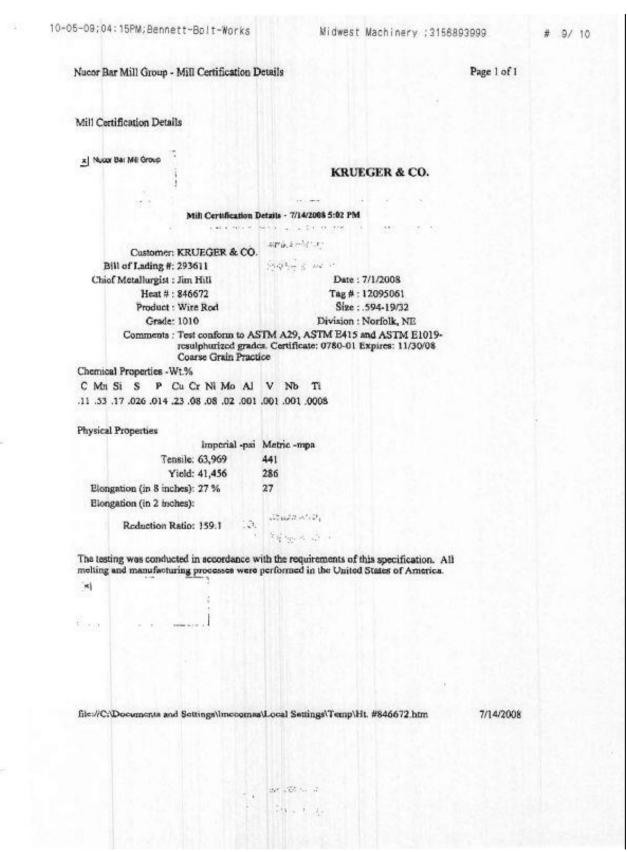


Figure A-37. ⁵/₈ in. x 22 in. Bolts, Test No. MGSSYP-2 (cont.)



TRINITY HIGHWAY PRODUCTS, LLC. 425 E. O'CONNOR AVENUE LIMA, OHIO 45801 419-227-1296

MATERIAL CERTIFICATION

CUSTOMER: STOCK	DATE: SEPTEMBER 29, 2009
	INVOICE #:
	LOT #: 090123B
PART NUMBER: 3380G	QUANTITY: 119,201
DESCRIPTION: 5/8" X 1 ½ HH BOLT	DATE SHIPPED:
SPECIFICATIONS: ASTM A307-A/A153	HEAT #: 7367052, 7366484,7368369

MATERIAL CHEMISTY

C	MN	P	S	SI	CU	NI	CR	MO	AL	v	N	CB	SN	B	TI	NB
.15	.49	.008	.002	.06	.03	.02	.05	.01	.029	.002	.005	.901	.001	.000	.000	.000
.13	.38	.007	.002	.10	.03	.04	.06	.02	.037	.002	.064	.001	.001	.000	.000.	.000
.14	.43	.006	.008	.06	.04	.02	.06	.02	.034	.002	.005	.001	.001	.000	.000	.000

PLATING AND/OR PROTECTIVE COATING

HOT DIP GALVANIZING (OZ. PER SQ. FT.)	2.7-	4 AVG.
****THIS PRODUCT WAS MANUFACTI	URED IN THE UNITED STA	TES OF AMERICA***
THE MATERIAL USED IN THIS PRODUCT	WAS MELTED AND MANU	FACTURED IN THE U.S.A.
WE HEREBY CERTIFY THAT TO THE B CONTAINED	EST OF OUR KNOWLEDG HEREIN IS CORRECT.	E AND INFORMATION
STATE OF OHIO, COUNTY OF ALLEN SWORN AND SUBSCRIBED BEFORE ME FHIS 29 TH DAY SEPTEMBER, 2009		22
Allon Alpline NO	TARY PUBLIC	
425 E. O'CONNOR AVENUE	LIMA, OHIO 45801	419-227-1296

Figure A-38. ⁵/₈ in. x 1¹/₂ in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2

A DIVISION OF TRINITY INDUSTRIES ROTHRVING BLVD, 75247 - P.O. BOX SI DALLAS, TX 75358-8887 Phone: 214-589,7591 FAX: 214-589,7594 Lab No: 9010250F SUE HENLINE TRINITY HWY PRODUCTS, LLC #55 ROLLFORM JMA, OH 45801	10007	Received Date: 01/27/2009 Heat Code: Heat Number: 7387052, 7388484 PO or Work Order: Lot#: 0901238 Test Spec: F606 ASTM METH Other Information: 30#: 55-46502	Material Size: 5/8" x 1-1/2" HHB
OTHER TEST: Type: HARDNESS ROCKW A) 90-91-90-89 B) 88-90-91-91 C) 89-91-91-91 D) 89-89-91-91 E) 91-91-90-88	ELL BW		Quantity amount: 20
Type: HEAD MARKINGS TRN 307A USA			Quantity amount: 0
	-		
e certify the above results to be a true an port will void certification. NVLAP Certific rtill catton, approval, or endorsement by h	Fhancing In edg		nelian or partial reproduction of this may not be used to claim product Michael Bitton process, Minuel 3, Beats, PE

Figure A-39. 5/8 in. x 11/2 in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

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		oubli	c .	807 EAST				LORAIN		
		INCINETERD PRODU	1.10	262077 : 330	120000-005			FATI	2010-2016-2	~51
	OF TESTS		REPU	BLIÇ ENGENEE	RED PROD	UCTS		July 9, 26		
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ERANA CHARGE		1. 201		***********	S.S.L. S.L.	SHIP TO		diungle4+	CBRENC .	
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ALGRA	AY SAUETY P	RODUCTS INC		이 있는 것이		S METALS PR				
				A	5800 8	TERLING AVS				
DALLA	8, 7X 75356	-8887		2. 10	MAPLE	HT8, OH 441	37			
				9.2		1 5.0				
	16			(F _ 6)	11	1. 1. 18				
**		***********								
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			FINISH	ED SIXE RESUL	75	********				
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PCE 10427			72.4	49.0						
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	MID-RADIUS	(1) 調整			80 E.	1.				
PCE 10428	107	2.603		- NOTES						
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						S				
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ALL TROTING	KAS MER PE	RECOMED USING T	E CURR	THT REVISION	OF THE T	RETING SPEC	FIGATION	15.		
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		POSED TO MERCURY			THAT IS		AND I DAT 1	INPERATO	RB	
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Figure A-40. ⁵/₈ in. x 1¹/₂ in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

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HIGH P 0 1	TTY INCUSTRIE HAY SAGETY PR BOX 548987 47 AS, TE 75336-	ODUCTS INC W FLOOR			C/ 58	0 808	INDUSTRIES METALS PRI RELING AVE EIGNTS, OH	69			
1463016-20		1411					(4) 生活	2 Marine	SI 14		
		12000	C. S. S. L.				ALL CAR				
MÈCHANICAL SIZE: RDG	PROPERTIES FO .6390 DIAM X	W X COTL	TRA TES	TING	THE GRAI	N COL	1942195 1912 - 1913	1046-117 -11	LST REPL	ats or	
	**********		LADLI	8 CHEMEST	RY 4						
C 0.15	0.49	p. 9.000	5 0.00		0.06		CU	NI 0.02		0.05	
V	HO HO	SN	AL	4	CS.		N	0.02		4192	
0.002	0.01	5M D.001	0.025	9	0.001		0.0050	22			
	ATIO 112.3 TO		- CALCU	LATED TRA	78		1965111	·			
TENSILE TRS	TENSILE	NMAT	RA RA	2012/02/02/02	RESULTS CESULTS					*****	
PCE 14133	60850	PS1 45000	64.4	44.0			the letter	en de la com			
HARDNESS TE		E10/ASTM A17	HBN	AS-RLD/	св ним 1		ALC C				
PCE 14114	MID-RADIUS	State State	St. 65		1. 16.		A Start	38. AN			
CHEMICAL AN	ALYSIS CONFOR	ME TO APPLICAN	LE SPECI		M15, LBL	10129	. LBL10130	ASTM E	019	******	
TESTED IN A RESULTS OF	COORSANCE WIT SUCH INSPECTS	NOTS HEREBY CONTRACTIONS	ERIIFY TH PRESCRIP (HAS DES	BAT THE P BED IN TH EN APPROV	WTERIAL CE GOVERN	ING S	PECIFICATE	CHAR AND BA	SED UPO	347 W	
CERTIFICATE	OF TESTS SHA	LL NOT BE (RED)	CODUCED 1	EXCEPT IN	FULL		1.688	Ref and			
ALL TESTING	HAS BEEN PER	FORMED USING 7	THE CURRE	ENT REVIS	TON OF T	HE TE	B7103 SPEC	TELEVITON	8		
		TTIODS OR FRAN NATUES TITLE 14			S OR ENT	RJES	00 81HT 00	CUMENT MAX	r BE PUN	1899D	
	a second second second	OSEU TO REPORT	Y OR AN	Y METAL A	LLOY THE	T IS	LIQUID AT .	ANDIANT TR	INPERATU	22	
THE NATERIA DURING PROC		LE IN OUN POSS									
DOBTING PROC	ESSING OR WHI		ESSION.	ATERIAL							

Figure A-41. 5% in. x 11/2 in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

Republic 1807 EAST 28TH ST. LORAIN, OH 44055 PHONE: 330-430-5594 PAX: 330-438-5695 CERTIFICATE OF TESTS REPUBLIC ENGINEERED PRODUCTS October 31, 2008 PACE 1 OF 2 PERCHASE ORDER DATE: 8/27/2008 ACCOUNT HUMBER: 5550-3007-01 FURCHASE ORD: 129120M ACCOUNT HIMBER: PART NUMBER: 300941B SCHEDOLR: 9510-85 ORDER NUMBER: 1396303 - 01 1 HEAT : T368369 REVISION: SHIDE TO SHIDE ADDRESS TRINITY INDUSTRIES INC TRINITY INDUSTRIES INC. HIGHNAY SAGETY PRODUCTS INC C/O BCS METALS DEEP P O BOE SERSE? 4TH FLOOR SEDD STERLING AVE OALLAS, TX 75356-8887 MAPLE HEIGHTS, OH 44117 NATERIAL DESCRIPTION NOT ROLLED STEEL COILS CABBON AISI-1015 AK AL KILLED FINE GRAIN COLD WORKING QUALITY TEST REPORTS OF MECHANICAL PROPERTIES FOR INPO ONLY EXTRA TESTING SI28: RDS .6390 DIAM X COLL RDS 16.2306HM DIAM X COIL LUDLE CISHISTRY \$ ---
 C
 MS
 P
 S
 S1
 CU

 0.14
 0.43
 0.005
 0.008
 0.06
 0.04

 V
 MO
 SN
 SL
 CB
 N

 0.002
 0.02
 0.001
 0.034
 0.001
 0.0050
 NI 0.02 CH. 0.06 0.0050 -------REDUCTION RATIO 112.3 TO 1 AUSTENITIC GRAIN SIZE 5 OR FINER BASED ON A TOTAL ALUMENTM CONTENT FOURL TO OR GREATER THAN .021% PER SEMI - FINISHED RESOLTS FINISHED SIZE RESOLTS ASTM A29. TENSILE VIELD(0,24) RA 5 82200 63 9 47.0 129 1.52 PCE 15938 58500 HARDNESS TEST ASTM B10/ASTM A170 HEW AS-RLD/CD HEW MID-RADIUS 1.1.18-30 PCE 15911 111 11.1.1.1.1.1.1 ----- NOTER -----CREMICAL ANALYSIS CONFORMS TO APPLICABLE SPECE: ASTM E415, LBL10129, LBL10130, ASTM E1019, LELIGISS, LELIGISS: AND ASTN EIGES LELIGISS, LELIGISS. REPUBLIC ENGINEERED PRODUCTS HEREBY CRETIFY THAT THE MATERIAL LISTED HEREIN HAS BEEN INSPECTED AND TESTED IN ACCORDANCE WITH THE HETHODS PRESCRIBED IN THE COMERNING SPECIFICATIONS AND EASED UPON THE RESULTS OF SUCH INSPECTION AND TESTING RAS BEEN ASPROVED FOR CONTRANCE TO THE SPECIFICATIONS. CERTIFICATE OF TESTS SHALL NOT BE REPRODUCED EXCEPT IN FULL. ALL TESTING HAS NERN PERFORMED USING THE CURRENT REVISION OF THE TESTING SPECIFICATIONS. RECORDING OF FALSE. FICTIVIOUS OR FRAMEWLENT STATEMENTS OR ENTRIES ON THIS SOCIMENT MAY BE PUNISHED AS & FELONY UNDER FED STATUES TITLE 10 CHAFTER 47. THE MATERIAL WAS NOT EXPOSED TO MERCURY OR ANY METAL ALLOY TRAT IS LIGHTLAN AMBIENT TEMPERATURE EURING PROCESSING OR WHILE 19 OUR POSSESSION. NO WELD OR WELD REPAIR WAS PERFORMED ON THIS MATERIAL. R. A. SZELIGA BY JANET E. HARTLINE

HANGADER TECH. SERVICES R. A. Szelagón

Figure A-42. % in. x 11/2 in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2 (cont.)

225 E. O'C Lime, OH	Connor						· #	TF
Customer:	MIDWEST MACH & SUPPLY CO. P. O. BOX \$1097	Concerning and the second s	2030 43073	Shipped To:	RESALE			5
	LINCOLN, NE 68501-1097	Document #	1	Use State:	<u>K.5</u> .			
		Tri	nity Highway Pro	lucis, LLC				
	Certificate (W Compliance For T	Finity Industries. In	. ** SLOTTED RAIL T	ERMINAL **		43	
		87	CHRP Report 350			202		
		110	And mapon 550				\$ <u>1</u>	
Discor	Baundation							
Pieces 32 32 32 32 64 32 32 32	Description 12/12/6/S SRT-1				and a second science of the second science of the second science of the second science of the second science of		1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -	
32	12/25'0/SPEC/S SRT-2							
32	3/16X12.5X16 CAB ANC BRKT							
32	2" X 5 1/2" PIPE (LONG)							
64 32	6'0 TUBE SL/.188X8X6 5/8 X 6 X 8 BEARING PLATE							
32	12/BUFFER/ROLLED							
32	CBL 3/4X6'6/DBL SWG/NOHWD							
640	5/8" RD WASHER 1 3/4 OD							
1,728	5/8" GR HEX NUT			0				
1,152	5/8"X1.25" GR BOLT							
256	5/8"X1.5" HEX BOLT A307							
654	5/8"X9.5" HEX BOLT A307							
Upon deliv	ery, all materials subject to Trinity Highway	Products , LLC Store	age Stain Policy No. I	.G-002.			2312	
			•				20	
FHGE-	<i></i>		13				8	
r -			10		\$.)			
					~~~~		2	
	IL USED WAS MELTED AND MANUFA				Ci			
	RDRAIL MEETS AASHTO M-190, ALL S ER GALVANIZED MATERIAL CONFOR							
	DMPLY WITH ASTM A-307 SPECIFICAT			CONTANCH WITTE ASTA	A-153 TINUES	OTHERN	USE STATE	D.
NTTS CO	MPLY WITH ASTM A-363 SPECIFICATI	IONS AND ARE GAL	WANIZED IN ACC	ORDANCE WITH ASTM.	A-153. UNLESS	OTHERWI	SE STATED	
14" DIA C	ABLE 6X19 ZINC COATED SWAGED END	AISI C-1035 STEEL AT	NNEALED STUD 1" I	IA ASTM 449 AASHTO M	10, TYPE II BREA	KING		
	H-49100 LB				6	Δ	٩	2
State of Ohi	o, County of Allen. Syrorn and Subscribed befo	re mothis Mik day of I	lune, 2008		N/	(A)	10	r
7	ma	JUN'	namente e verdicitado distrito	Trinity Highway Products	LICKA	1/0/1	Nin X	~
<b>.</b>		A 4 1 1			10 4 22 3 4	F 7 1 1A	# 113A / 3	
o Stotary Pul	tion ( I ALA MA A YYV	un		Certified By:	ALL IN	an we		

Figure A-43. ⁵/₈ in. x 9¹/₂ in. Hex Bolt, Test No. MGSSYP-1

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Southeastern Bolt & Screw, Inc. 1037 16th Avenue West Birmingham, AL 35204

### **Certification Of Compliance**

### DATE: September 28, 2010

CUSTOMER: Midwest Machinery & Supply RE: Purchase Order No. 2351 P.O. Box 703 SBS Shop Order No. 1093439 Milford, NE 68405

ΩΤΥ	DESCRIPTION	SPECIFICATION	HEAT/LOT NO.	
150	5/8-11 X 10 Hex Bolt	A307 Grade A	DL10101333405	34
100	5/8-11 X 12 Hex Bolt	A307 Grade A	1077688-1 DL10101383405	
500	5/8-11 X 19 Hex Bolt	A307 Grade A	1077688-2 DL10101333405	
150	3/4-10 X 8 Hex Bolt	A307 Grade A	1077688-3 11893810	•
500	7/8-9 X 14 Hex Bolt	A307 Grade A	1077688-4 DL1010333403	1
100	7/8-9 X 16 Hex Bolt	A807 Grade A	1077688-5 DL1010333403 1077688-6	

### Surface coating: A153 Grade C

12

We certify the materials listed meet or except the latest ASTM specification as shown.

Quality Assurance Manager

402 40 3288 646E 01/10

ROCOUNTING

3962934827 25:80 0102/28/01

Figure A-44. 5% in. x 10 in. Hex Bolt, Test No. MGSSYP-2

PILICE NUCOR CORPO	RATION	ROLINA	ñ,	Ailf Cer 9/8/20	tification 10				Joo Sa DARLINGTO [84 Fax: [84	eel Mill Road N SC 29840 (3) 983-6841 (3) 995-8701	5 0 1
Sold To 1037 16T FO BOX BIRMING (205) 326 Fax: (205)	ASTERIN BOLT ( H AVE W 758 HAM, AK 96201- 4651 ( 460-1627	L SCREW IN	c	1	Ship Te: SCUT 1037 PO B BIM (205) Pax (	THEASTER 16TH AVE OX 758 INGHAM 328-4661 205) 458-1	N BOLT & SCHEW W AL 35201-0000 527	INC			
Customer P.O.	05947	freedown and the Cog				1	Sales Order	120158			1
Product Group	Merchant Bar (	Duality	10.00			-	Part Number	Read and the state of the state	324805740		
Grade	ASTM A572/AL	and only in the second second	50 TY2/30			-	LociO	DL10103			
Size	5615" Round		the second s				Heat ID	OL 10100			
Product	.5815" Round 4	0" A572-55					B.L. Number	C1-5570	the second s		2
Description	A572-05 - AST	And an owner of the local division of				-	Load Number	C1-2234	18		
Outlomer Spec							Customer Part #				
soby confy that the mature	/ described horein has	bien Minulastur	ad in accordance of	ich ung speichtt	alions and standards	litted filmer	and thus is satisfies those re	ouromano			
C Mn 0.24% 1.25%	р 0.007%	s 0.036%	Si 0.18%	Cu 0.34%	NI 0.09%	Cr 0.12%		V 15% (	СЪ 0.008%		
eld 1:63000psi (494) ald 2:63000psi (494)			Tensile 1: ( Tensile 2: (						8°(% in 203.3 8'(% in 203.3n		
MERCURY, RADIUM	OF ALPHASO	URCE MATE	PIALS IN ANY	FORM H	AVE NOT BEEN	(USED IN	THE PRODUCTION	«ОКТНІЗ	MATERIAL		
MERCURY, RADIUM	, of Alpha so		PIALS IN ANY	FORM H	AVE NOT BEEN	I USED IN	THE PRODUCTION	«О́ГТНІЗ	MATERIAL		
MERCURY, RADIUM	OF ALPIASO		fials in any	FORM H	ave not been	I USED IN	THE PRODUCTION	OF THIS			10 10
MERCURY, RADIUM	OF ALPIASO		frals in any	FORM HV	ave not been	I USED IN	THE PRODUCTION	4 OF ТН S			
MERCURY, RADIUM	OF ALPIASO		frals in any	FORM H	AVE NOT BEEN	USED IN	THE PRODUCTION	• OF ТН S			
MERCURY, RADIUM	OF ALPHASO		RALS IN ANY	FORM H		I USED IN	THE PRODUCTION	€ OF ТН S			* *
MERCURY, RADIUM	OF ALPIA SO		RALS IN ANY	FORM H		USED IN	THE PRODUCTION	« О́Г ТН З			
MERCURY, RADIUM	OF ALPIASO			mer	- Alexan		THE PRODUCTION	«Of тнз			
KE-H9 May Is, 2000	OF ALPIASO			was Jame	5			« О́Г ТН З			

Figure A-45. 5% in. x 10 in. Hex Bolt, Test No. MGSSYP-2 (cont.)



Figure A-46. ⁵/₈ in. Hex Nut, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-47. ⁵/₈ in. Flat Washer, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-48. 5% in. x 71/2 in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-49. 7/8 in. x 8 in. Hex Bolts, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-50. 7/8 in. Flat Washer, Test Nos. MGSSYP-1 and MGSSYP-2



Figure A-51. Double Head Nail, Test Nos. MGSSYP-1 and MGSSYP-2

## Appendix B. Vehicle Center of Gravity Determination

Test	MGSSYP-1	Vehicle	2270P/Ram 1500		
		Vehicl	e CG Determination		
		Weight	Vert CG		Vert M
VEHICLE	Equipment	(lb)	(in.)		(lb-in.)
+	Unbalasted Truck(Curb)	5130	28.14805		144399.5
+	Brake receivers/wires	6	49		294
+	Brake Frame	5	24		120
+	Brake Cylinder (Nitrogen)	22	26		572
+	Strobe/Brake Battery	6	31		186
+	Hub	26	14.4375		375.375
+	CG Plate (EDRs)	7.5	32		240
-	Battery	-37	41		-1517
-	Oil	-8	16		-128
-	Interior	-59	22		-1298
-	Fuel	-165	19		-3135
-	Coolant	-21	33.5		-703.5
-	Washer fluid	-3	34		-102
BALLAST	Water	100	19		1900
	Misc.				0
	Misc.				0
					. <u> </u>
				313208.5 496.125	141203.4
	TOTAL WEIGHT	5009.5 lb	CG location (in.)	62.5229 0.099037	28.18712

whee

el base	140.5	Calculated Test Ine	rtial Weight	
	MASH Targets	Targets	CURRENT	Difference
	Test Inertial Weight (lb)	5000 ± 110	5009.5	9.5
	Long CG (in.)	63 ± 4	62.52	-0.47710
	Lat CG (in.)	NA	0.10	NA
	Vert CG (in.)	≥ 28	28.19	NA

Note: Long. CG is measured from front axle of test vehicle

Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

Curb Weight (lb)			Actual tes	t inertial we	ight (lb)
	Left	Right	( ,	Left	Right
Front	1470	1386	Front	1424	1374
Rear	1097	1177	Rear	1090	1141
FRONT	2856	b	FRONT	2798	lb
REAR	2274	lb	REAR	2231	lb
TOTAL	5130	lb	TOTAL	5029	lb

Figure B-1. Vehicle Mass Distribution, Test No. MGSSYP-1

	Test: MGSSYP-2 Vehicle:	1100C				
	Vehicle C	G Determin	nation			
		Weight	Long CG	Lat CG	Long M	Lat M
VEHICLE	Equipment	(lb)	(in.)	(in.)	(lb-in.)	(lb-in.)
+	Unbalasted Car (curb)	2402	35.27841	0.211464	84738.75	507.9375
+	Brake receivers/wires	6	129.25	0	775.5	0
+	Brake Frame	5	27	-12	135	-60
+	Brake Cylinder	22	62.5	-15	1375	-330
+	Strobe Battery	6	56.75	0	340.5	0
+	Hub	20	0	-35.5	0	-710
+	CG Plate (EDRs)	7.5	39	0	292.5	0
+	DTS	18	63	9.5	1134	171
-	Battery	-29	-8.5	-15	246.5	435
-	Oil	-3	-6.5	10	19.5	-30
-	Interior	-38	40	0	-1520	0
-	Fuel	-6	81	-4	-486	24
-	Coolant	-8	-17	0	136	0
-	Washer fluid	-7	-14	22	98	-154
BALLAST	Water	25	81	-4	2025	-100
	Misc.				0	0
	Misc.				0	0
				TEMP	89310.25	-246.063
	Estimated Total Weight	2420.5	lb	CG location	36.89744	-0.10166
wheel base	95.75 in.				r	
MASH targets		Tact Inarti	<b>a</b> l			

### Test: MGSSYP-2 Vehicle: 1100C

Test Inertia	I
)55 2442	22.0
)4 37.09	-1.90766
-0.02311	NA
	)4 37.09

Note: Long. CG is measured from front axle of test vehicle

Note: Lateral CG measured from centerline - positive to vehicle right (passenger) side

					Du
CURB WEIGHT (Ib)					TE
					(fro
	Left		Right		
Front		778		739	Fro
Rear		414		471	Re
FRONT		1517	lb		FR
REAR		885	lb		RE
TOTAL		2402	lb		то
					-

Dummy = 166lbs. TEST INERTIAL WEIGHT (Ib)									
TEST INERTIAL WEIGHT (ID)									
(from scales)									
	Left		Right						
Front		765		731					
Rear		457		489					
FRONT		1496	lb						
REAR		946	lb						
TOTAL		2442	lb						

Figure B-2. Vehicle Mass Distribution, Test No. MGSSYP-2

# Appendix C. Dynamic and Static Soil Tests

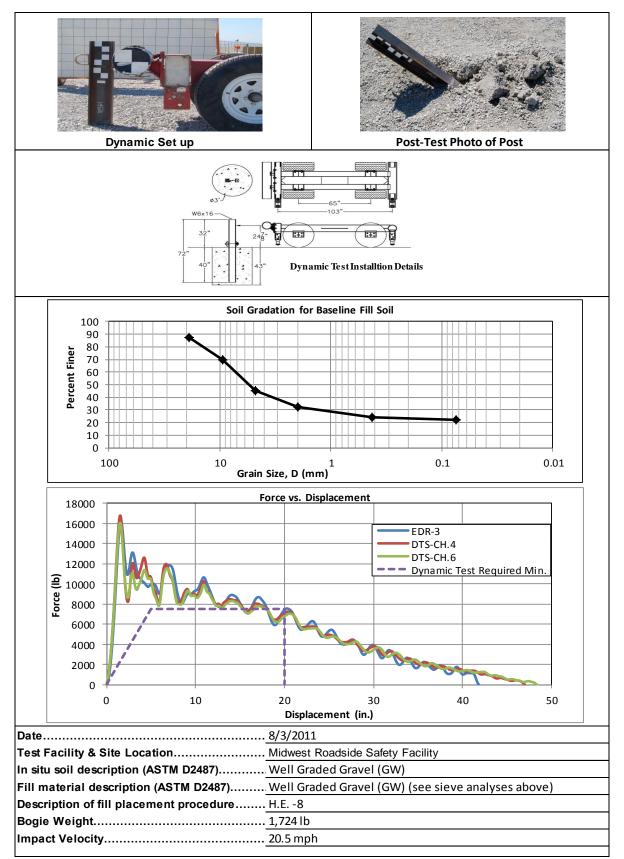


Figure C-1. Test Day Dynamic Soil Test, Test No. MGSSYP-1

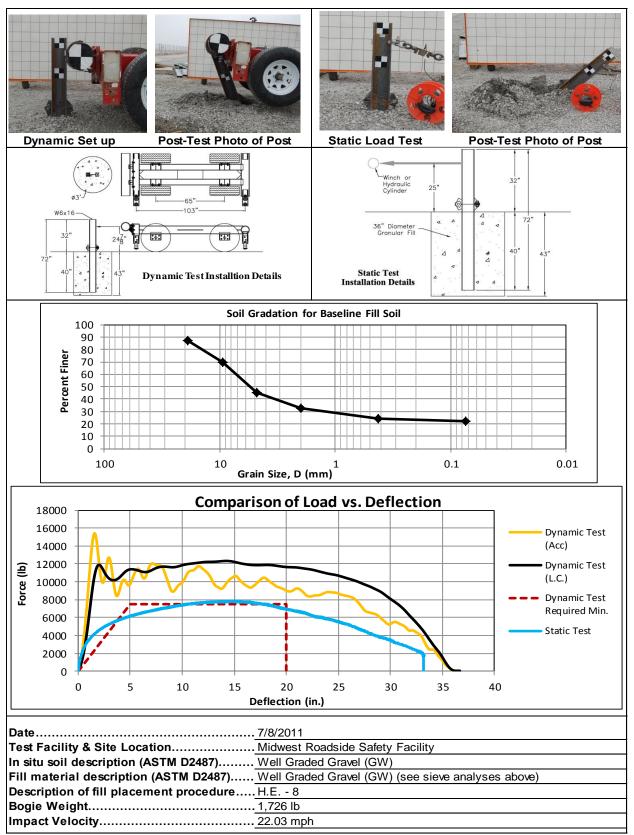


Figure C-2. Summary Sheet for Strong Soil Test Results, Test No. MGSSYP-2

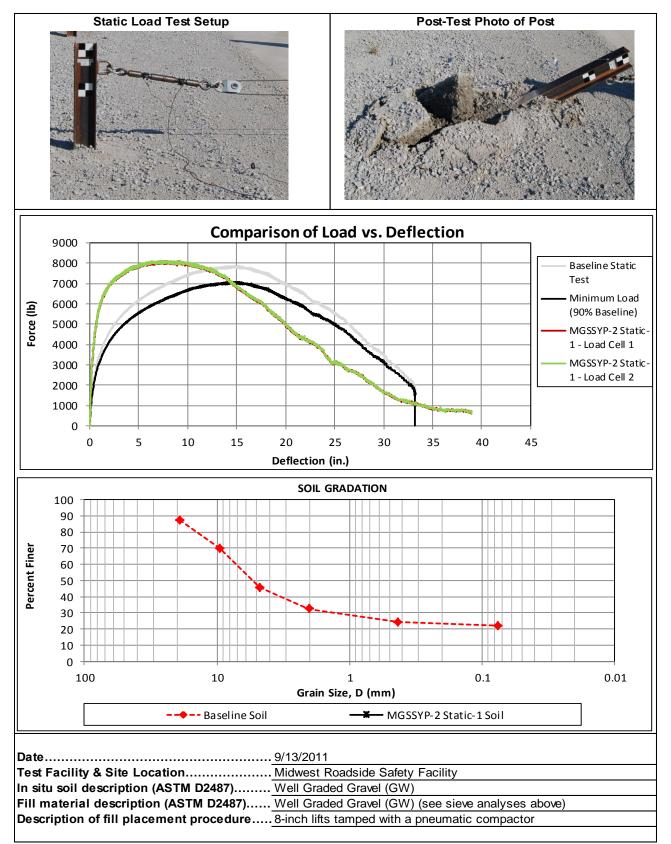


Figure C-3. Test Day Static Soil Test, Test No. MGSSYP-2

## Appendix D. Vehicle Deformation Records

### VEHICLE PRE/POST CRUSH FLOORPAN - SET 1

TEST: MGSSYP-1 VEHICLE: 2270P/Ram 1500 Note: If impact is on driver side need to enter negative number for Y

	Х	Y	Z	Х	Y'	Z	ΔX	ΔΥ	۵Z
POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)
1	25	12 3/4	-1	25	13	- 1/2	0	1/4	1/2
2	30	19 1/4	-4	30	19 1/2	-3 3/4	0	1/4	1/4
3	30	25	-3	30	25	-2 1/2	0	0	1/2
4	28 3/4	29	-1 1/4	28 1/2	29	-1	- 1/4	0	1/4
5	21	10	-1 1/4	21 1/4	10	-1	1/4	0	1/4
6	22	14 1/2	-3 3/4	22	14 1/2	-3 1/2	0	0	1/4
7	23 1/2	21 1/2	-7	23 1/4	21 1/2	-7	- 1/4	0	0
8	23 3/4	29 1/4	-6 3/4	23 1/2	29 3/4	-6 1/2	- 1/4	1/2	1/4
9	12 1/2	3 3/4	-2 1/2	12 1/2	3 3/4	-2 1/4	0	0	1/4
10	18	9	-2 3/4	18	9 1/4	-2 3/4	0	1/4	0
11	19	13 3/4	-5 1/2	19	13 1/2	-5 1/4	0	- 1/4	1/4
12	20 1/2	18	-8 3/4	20 1/2	18	-8 1/2	0	0	1/4
13	20 3/4	24 1/4	-8 1/2	20 1/2	24	-8 1/4	- 1/4	- 1/4	1/4
14	20 3/4	28 3/4	-8 1/2	20 3/4	28 3/4	-8 1/4	0	0	1/4
15	11	6	-2 3/4	11	6	-2 1/2	0	0	1/4
16	16 3/4	15	-8 3/4	16 3/4	15	-8 3/4	0	0	0
17	16 3/4	21 1/2	-8 1/2	16 1/2	21 1/2	-8 1/2	- 1/4	0	0
18	17	29 1/4	-8 1/2	17	28 3/4	-8 1/4	0	- 1/2	1/4
19	8	6 1/2	-3	8	6 1/4	-2 3/4	0	- 1/4	1/4
20	11	13	-8 3/4	11	12 3/4	-8 1/2	0	- 1/4	1/4
21	11 3/4	19	-8 1/2	11 1/2	18	-8 1/4	- 1/4	-1	1/4
22	11 1/2	24 1/2	-8 1/4	11 1/4	24 1/4	-8	- 1/4	- 1/4	1/4
23	11 1/4	29 1/2	-8	11 1/4	29 1/4	-8	0	- 1/4	0
24	1 1/2	6 1/2	-2 1/2	1 1/2	6 1/2	-2 1/4	0	0	1/4
25	3/4	13 1/4	-4 1/2	3/4	13 1/4	-4 1/2	0	0	0
26	1	20 3/4	-4 1/4	1	20 1/2	-4	0	- 1/4	1/4
27	1	27 1/2	-4	1	27 3/4	-4	0	1/4	0
28							0	0	0
29							0	0	0
30							0	0	0
31							0	0	0

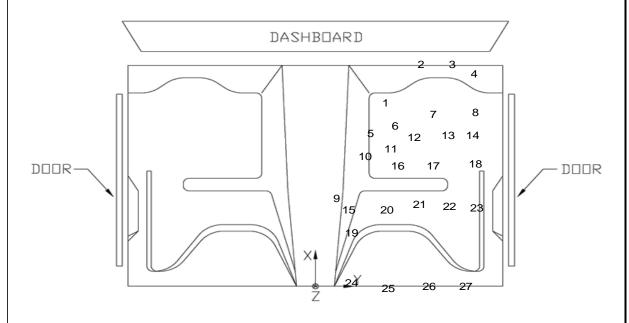


Figure D-1. Floor Pan Deformation Data – Set 1, Test No. MGSSYP-1

### VEHICLE PRE/POST CRUSH FLOORPAN - SET 2

TEST: MGSSYP-1 VEHICLE: 2270P/Ram 1500 Note: If impact is on driver side need to enter negative number for Y

	Х	Y	Z	Х	Υ'	Z	ΔX	ΔΥ	۵Z
POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)
1	40 3/4	19 1/4	- 1/4	40 1/2	19 3/4	0	- 1/4	1/2	1/4
2	46	25 1/2	-3 1/4	46	25 1/4	-3	0	- 1/4	1/4
3	46	31 3/4	-2	46	31 1/2	-1 1/2	0	- 1/4	1/2
4	44 1/2	35 3/4	0	44	35 1/2	1/4	- 1/2	- 1/4	1/4
5	37 1/4	16 3/4	- 3/4	37	16 1/4	- 1/2	- 1/4	- 1/2	1/4
6	38	21	-3	38	21	-2 3/4	0	0	1/4
7	39 1/2	28	-6 1/4	39 1/2	28	-6	0	0	1/4
8	39 3/4	35 1/2	-5 1/2	39 3/4	35 1/2	-5 1/2	0	0	0
9	28 1/2	10 1/2	-2 1/4	28 1/2	10 1/2	-2	0	0	1/4
10	34	16	-2 1/2	34	16	-2 1/4	0	0	1/4
11	35 1/4	20 1/4	-4 3/4	35	20 1/4	-4 1/2	- 1/4	0	1/4
12	36 3/4	24 1/4	-8	36 1/2	24 1/2	-8	- 1/4	1/4	0
13	37	30 3/4	-7 1/2	36 3/4	30 3/4	-7 1/2	- 1/4	0	0
14	37	35 1/4	-7 1/4	37	35	-7	0	- 1/4	1/4
15	27	12 3/4	-2 1/4	27	12 3/4	-2 1/4	0	0	0
16	33	21 3/4	-8 1/4	33	21 1/4	-8 1/4	0	- 1/2	0
17	32 3/4	28 1/4	-7 3/4	32 3/4	28	-7 1/2	0	- 1/4	1/4
18	33 1/4	35 1/4	-7 1/4	33	35	-7	- 1/4	- 1/4	1/4
19	24 1/4	13 1/2	-2 1/2	24	13 1/2	-2 1/4	- 1/4	0	1/4
20	27 1/2	19 1/4	-8	27	18 3/4	-8	- 1/2	- 1/2	0
21	27 3/4	25 1/2	-7 3/4	27 1/2	25	-7 1/2	- 1/4	- 1/2	1/4
22	27 1/2	31 1/4	-7 1/4	27 1/2	31	-7	0	- 1/4	1/4
23	27 1/2	36 1/2	-7	27 1/4	36	-6 3/4	- 1/4	- 1/2	1/4
24	17 1/2	13 1/4	-2	17 1/2	13 1/4	-1 3/4	0	0	1/4
25	17	20 1/4	-4	16 3/4	20	-3 3/4	- 1/4	- 1/4	1/4
26	17	27 1/2	-3 1/4	17	27 1/2	-3 1/4	0	0	0
27	17	34 1/2	-3	17	34 1/4	-2 3/4	0	- 1/4	1/4
28							0	0	0
29							0	0	0
30							0	0	0
31							0	0	0

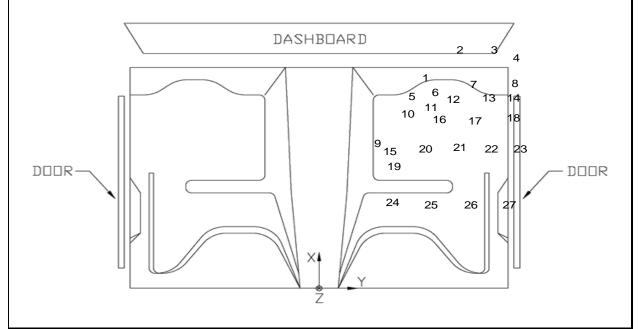


Figure D-2. Floor Pan Deformation Data – Set 2, Test No. MGSSYP-1

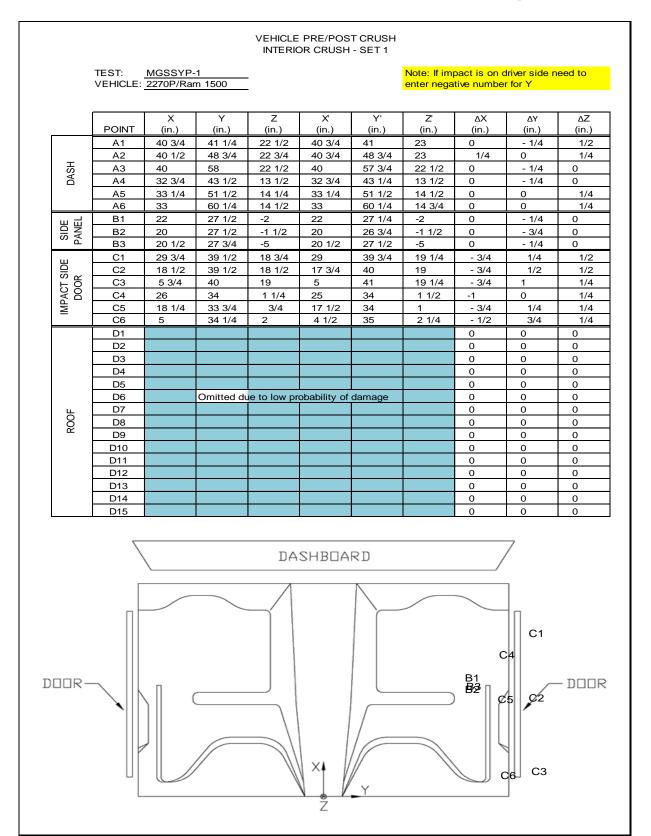


Figure D-3. Occupant Compartment Deformation Data - Set 1, Test No. MGSSYP-1

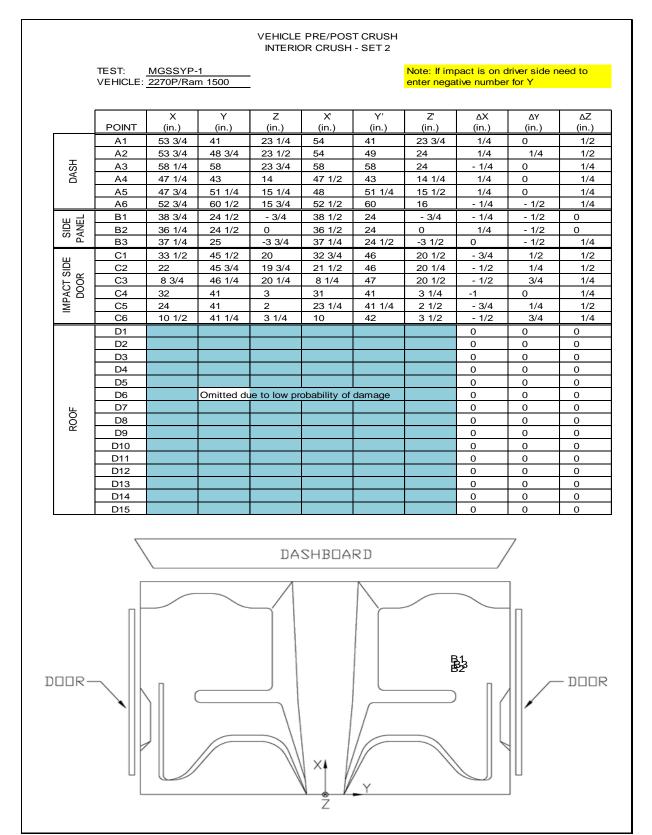


Figure D-4. Occupant Compartment Deformation Data – Set 2, Test No. MGSSYP-1

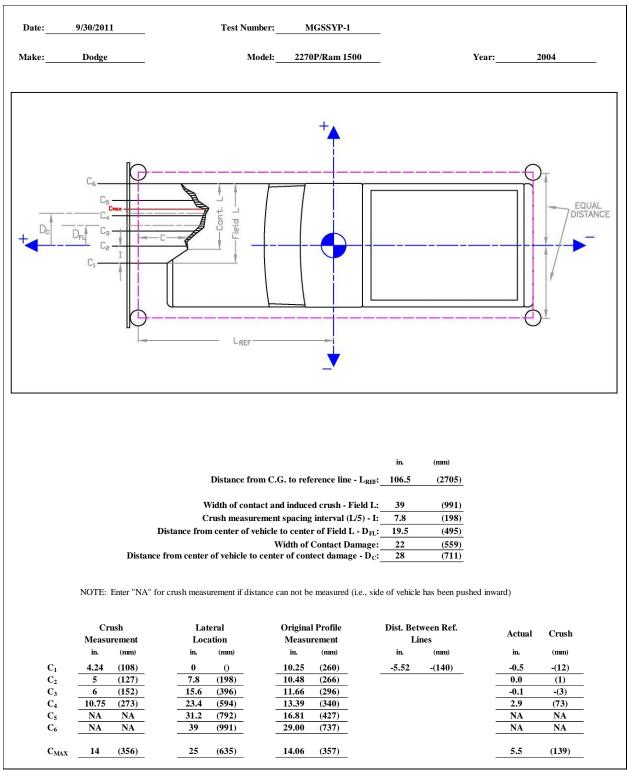


Figure D-5. Exterior Vehicle Crush (NASS) - Front, Test No. MGSSYP-1

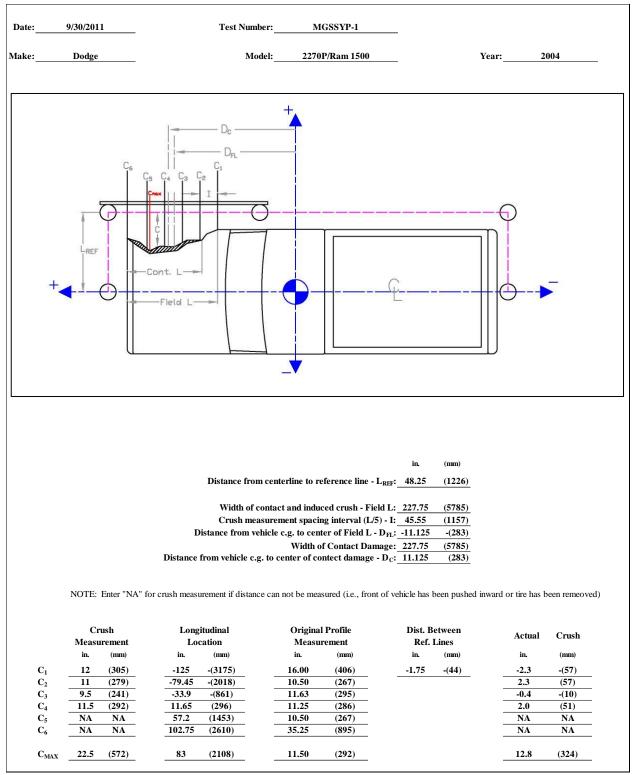


Figure D-6. Exterior Vehicle Crush (NASS) - Side, Test No. MGSSYP-1

## VEHICLE PRE/POST CRUSH FLOORPAN - SET 1

TEST: <u>MGSSYP-2</u> VEHICLE: <u>1100C</u> Note: If impact is on driver side need to enter negative number for Y

	Х	Y	Z	Х	Υ'	Z	ΔX	ΔY	۵Z
POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)
F1	28 3/4	3 3/4	- 1/4	28 1/2	4 1/4	0	- 1/4	1/2	1/4
2	30	11 1/4	-1	29 1/2	11	- 3/4	- 1/2	- 1/4	1/4
3	28 1/2	16	-1 1/2	28 1/4	16	-1 1/2	- 1/4	0	0
4	25 1/2	21 1/2	0	25 1/4	21 3/4	0	- 1/4	1/4	0
5	24 3/4	4	-3 1/4	24 3/4	4 1/4	-3 1/4	0	1/4	0
6	27	8 3/4	-3 3/4	27	8 3/4	-3 1/2	0	0	1/4
7	26 1/2	13	-3 3/4	26 1/2	13 1/4	-3 3/4	0	1/4	0
8	24 3/4	19 1/4	-3	24 3/4	19 3/4	-3	0	1/2	0
9	22	5 1/2	-6	22	5 1/2	-6 1/4	0	0	- 1/4
10	22 1/2	11	-5 1/2	22 1/2	11 1/4	-5 1/2	0	1/4	0
11	22 1/4	16	-5 1/2	22 1/2	16 1/4	-5 1/2	1/4	1/4	0
12	21 3/4	21	-6	21 3/4	20 3/4	-6	0	- 1/4	0
13	17 1/2	5 1/4	-6 1/4	17 1/2	5 1/2	-6 1/4	0	1/4	0
14	18	11 1/4	-5 3/4	18	11 1/2	-5 3/4	0	1/4	0
15	19	15 3/4	-6	19	15 3/4	-6	0	0	0
16	18 1/2	21	-6	18 1/2	21	-6	0	0	0
17	13	3	-6	12 3/4	3	-6	- 1/4	0	0
18	14	9 3/4	-6	14	9 1/2	-6	0	- 1/4	0
19	14 1/2	14 1/2	-5 3/4	14 1/2	14 1/2	-5 3/4	0	0	0
20	15	20 3/4	-6	15	20 3/4	-6	0	0	0
21	8 1/4	5	-6 1/4	8 1/4	5 1/4	-6 1/4	0	1/4	0
22	7 3/4	9 3/4	-6 1/4	7 3/4	9 1/2	-6 1/4	0	- 1/4	0
23	7 1/4	14 1/2	-6	7 1/4	14 3/4	-6	0	1/4	0
24	8 1/4	19 3/4	-6	8 1/4	20	-6 1/4	0	1/4	- 1/4
25	1 1/2	3 3/4	-2 3/4	1 1/2	3 3/4	-2 3/4	0	0	0
26	1	8 1/2	-3 1/2	1	8 1/2	-3 1/2	0	0	0
27	1	13 3/4	-3 1/2	1 1/4	13 3/4	-3 3/4	1/4	0	- 1/4
28	1 1/2	20 1/2	-3 1/4	1 1/2	20 1/2	-3 1/4	0	0	0
29							0	0	0
30							0	0	0
31							0	0	0

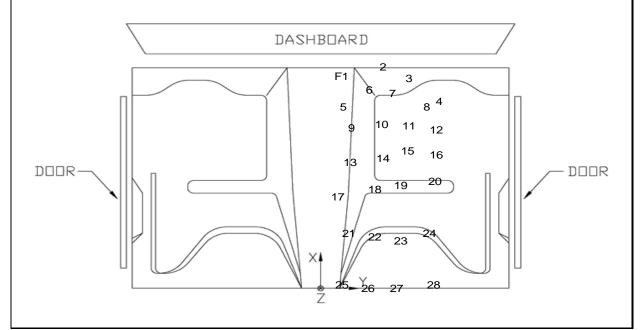


Figure D-7. Floor Pan Deformation Data – Set 1, Test No. MGSSYP-2

## VEHICLE PRE/POST CRUSH FLOORPAN - SET 2

TEST: <u>MGSSYP-2</u> VEHICLE: <u>1100C</u> Note: If impact is on driver side need to enter negative number for Y

	Х	Y	Z	X	Υ'	Z	ΔX	ΔY	ΔZ
POINT	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	(in.)
1	37 1/4	9 3/4	0	37 1/4	9 3/4	0	0	0	0
2	38 1/2	16 3/4	-1	38 1/4	16 1/2	- 3/4	- 1/4	- 1/4	1/4
3	37 1/4	21 1/2	-1 3/4	36 3/4	21 1/2	-1 1/2	- 1/2	0	1/4
4	34	27 1/4	- 1/4	33 3/4	26 3/4	0	- 1/4	- 1/2	1/4
5	33 1/4	8 3/4	-3	33 1/2	9 1/2	-3	1/4	3/4	0
6	35 3/4	14 1/4	-3 1/2	35 3/4	14 1/2	-3 1/2	0	1/4	0
7	35 1/4	18 1/2	-4	35 1/4	19	-3 3/4	0	1/2	1/4
8	33 1/2	25 1/4	-3 1/4	33 1/2	24 3/4	-3 1/2	0	- 1/2	- 1/4
9	31	10 1/4	-6	30 3/4	10 3/4	-6	- 1/4	1/2	0
10	31 1/4	15 3/4	-5 1/2	31 1/4	16 1/4	-5 1/2	0	1/2	0
11	31 1/4	21	-5 3/4	31 1/4	21 1/2	-5 3/4	0	1/2	0
12	30 1/2	26 1/4	-6 1/4	30 1/2	26	-6 1/4	0	- 1/4	0
13	26 1/4	10 1/4	-6	26 1/4	10 1/2	-6	0	1/4	0
14	27	16 1/2	-5 3/4	26 3/4	16 3/4	-5 3/4	- 1/4	1/4	0
15	28	20 3/4	-6	28	21 1/4	-6	0	1/2	0
16	27 1/4	26 1/2	-6 1/4	27 1/4	26 1/2	-6 1/4	0	0	0
17	21 1/2	8	-6	21 1/2	8	-6	0	0	0
18	22 3/4	14 3/4	-6 1/4	22 3/4	14 3/4	-6 1/4	0	0	0
19	23 1/2	20	-6	23 1/2	20 1/2	-6	0	1/2	0
20	23 3/4	26 1/4	-6 1/2	24	26	-6 1/2	1/4	- 1/4	0
21	17	10 1/4	-6 1/4	17	10 3/4	-6 1/4	0	1/2	0
22	16 3/4	14 1/2	-6 1/2	16 3/4	15	-6 1/2	0	1/2	0
23	16	19 1/2	-6 1/4	16 1/4	20	-6 1/4	1/4	1/2	0
24	17 1/4	25 1/4	-6 1/2	17 1/4	25 1/2	-6 1/2	0	1/4	0
25	10 1/4	9	-3	10 1/4	9	-2 3/4	0	0	1/4
26	9 3/4	14	-3 3/4	10	13 3/4	-3 3/4	1/4	- 1/4	0
27	10	19 1/4	-4	10	19 1/4	-4	0	0	0
28	10 1/4	25 3/4	-3 1/2	10 1/2	26	-3 1/2	1/4	1/4	0
29							0	0	0
30							0	0	0
31							0	0	0

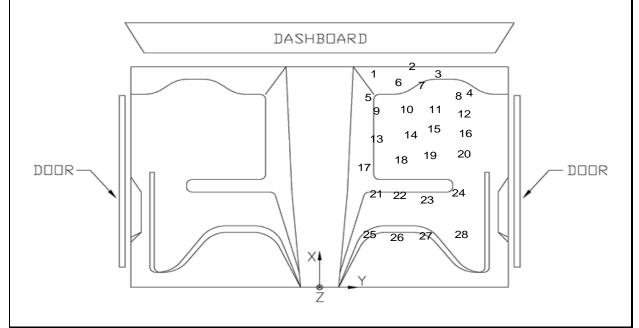


Figure D-8. Floor Pan Deformation Data – Set 2, Test No. MGSSYP-2

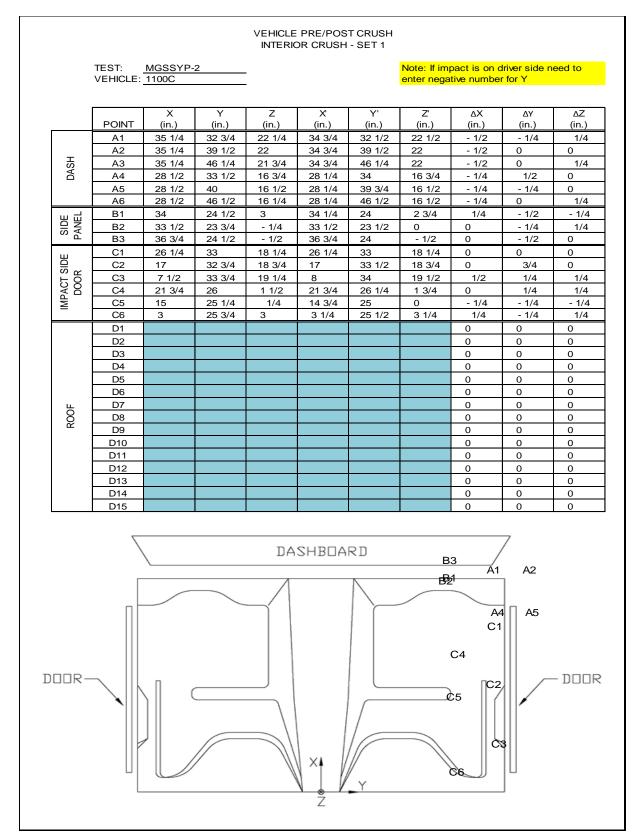


Figure D-9. Occupant Compartment Deformation Data – Set 1, Test No. MGSSYP-2

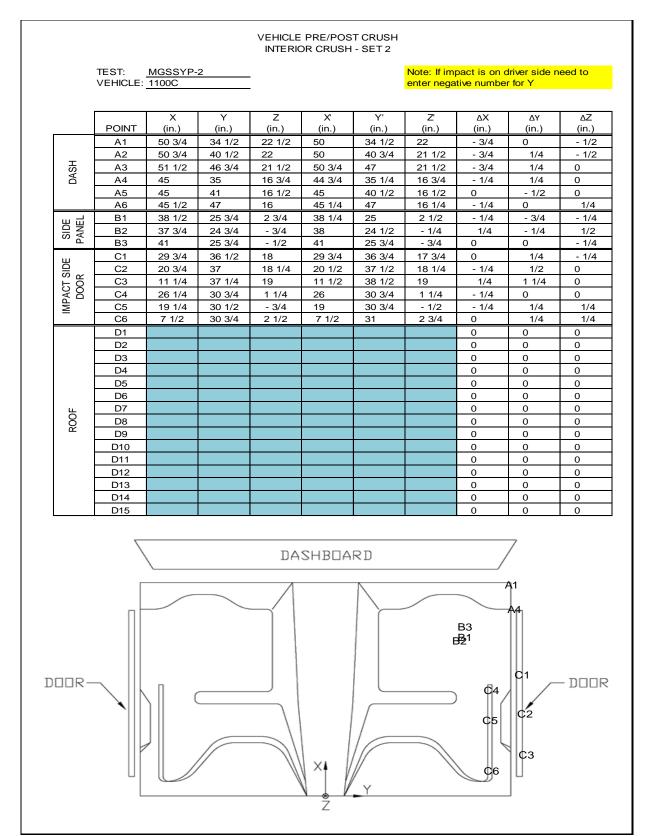


Figure D-10. Occupant Compartment Deformation Data – Set 2, Test No. MGSSYP-2

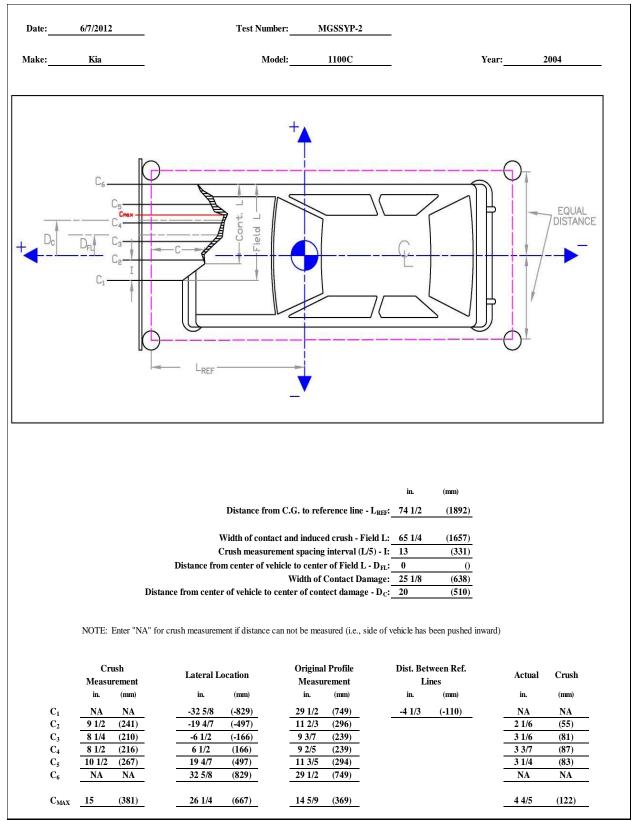


Figure D-11. Exterior Vehicle Crush (NASS) - Front, Test No. MGSSYP-2

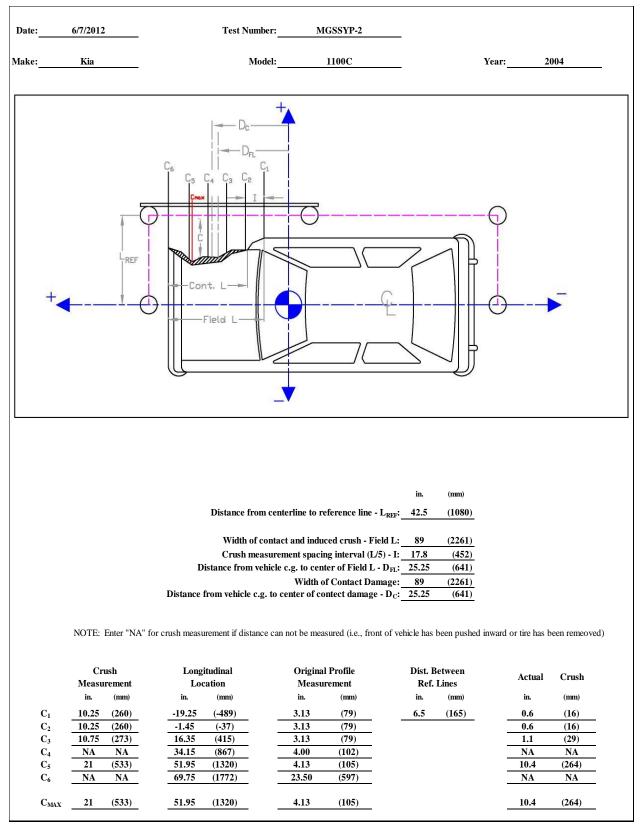


Figure D-12. Exterior Vehicle Crush (NASS) - Side, Test No. MGSSYP-2

## Appendix E. Accelerometer and Rate Transducer Data Plots, Test No. MGSSYP-1

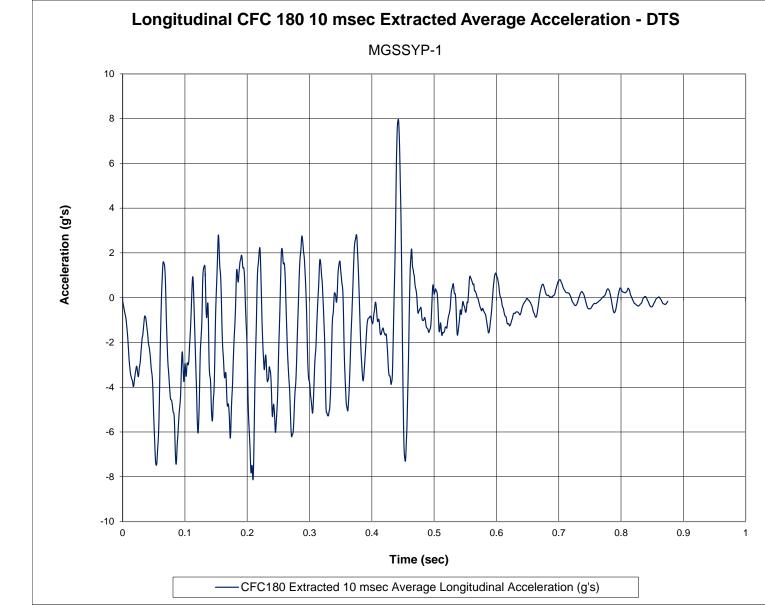


Figure E-1. 10-ms Average Longitudinal Deceleration (DTS), Test No. MGSSYP-1

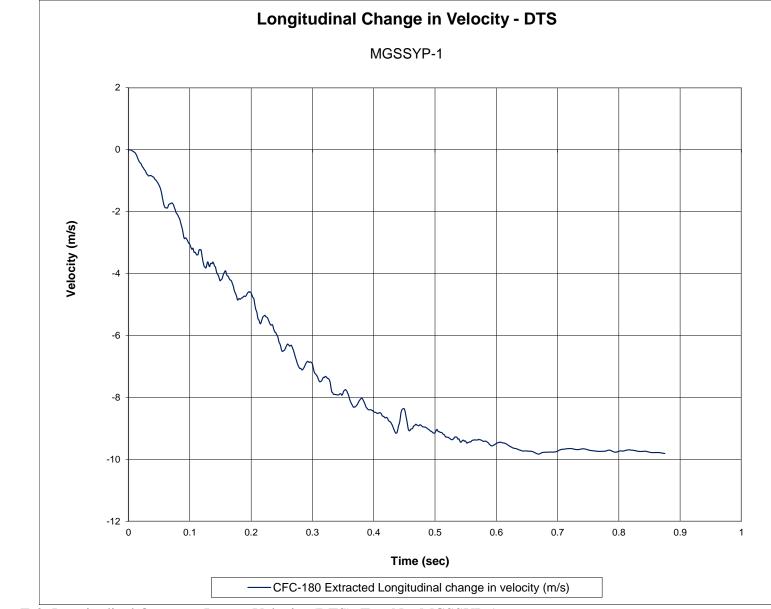


Figure E-2. Longitudinal Occupant Impact Velocity (DTS), Test No. MGSSYP-1

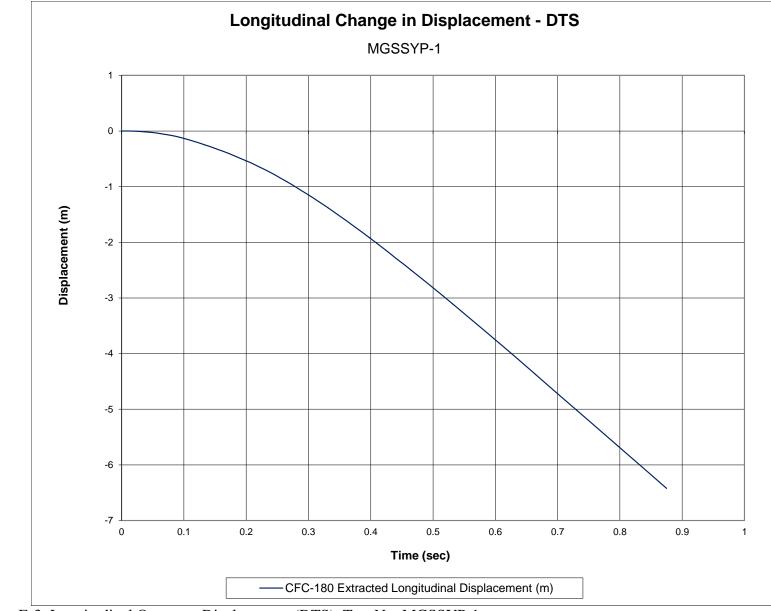


Figure E-3. Longitudinal Occupant Displacement (DTS), Test No. MGSSYP-1

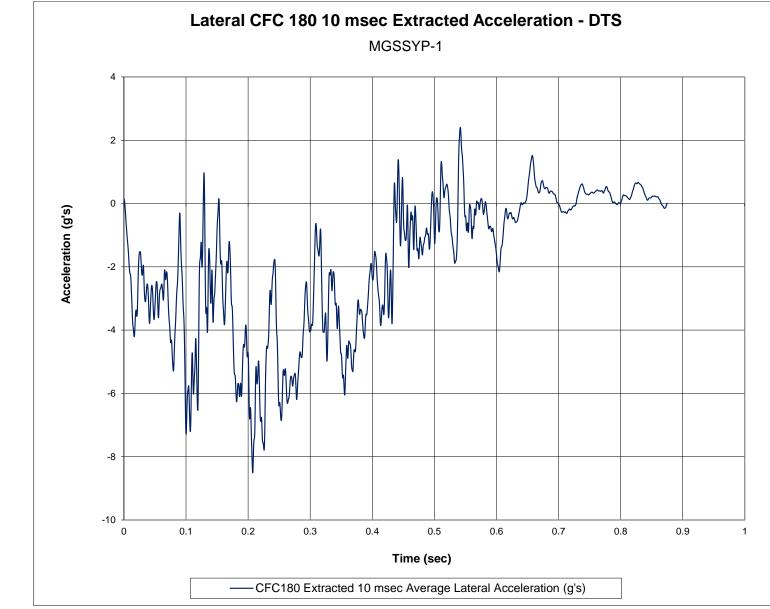


Figure E-4. 10-ms Average Lateral Deceleration (DTS), Test No. MGSSYP-1

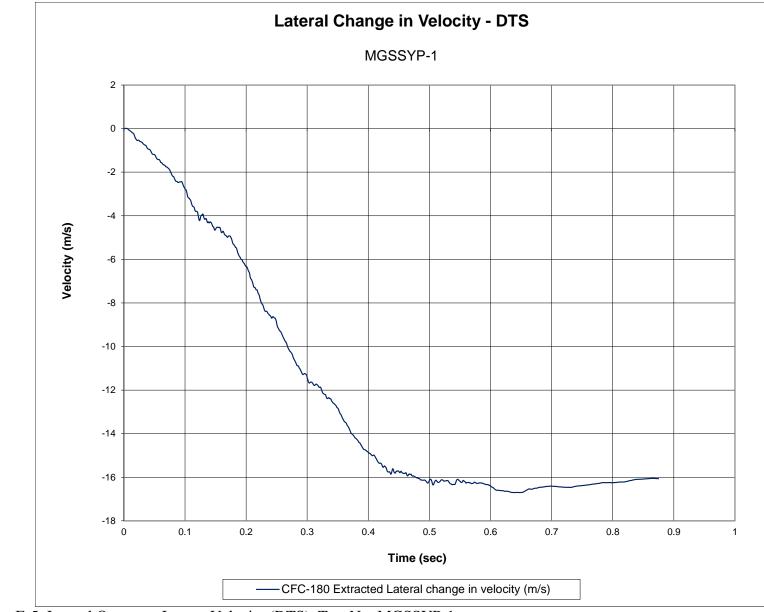


Figure E-5. Lateral Occupant Impact Velocity (DTS), Test No. MGSSYP-1

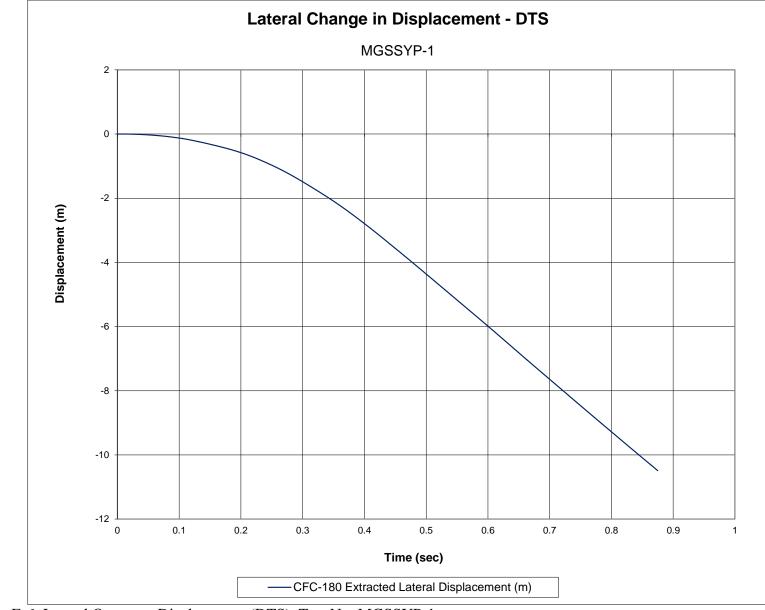
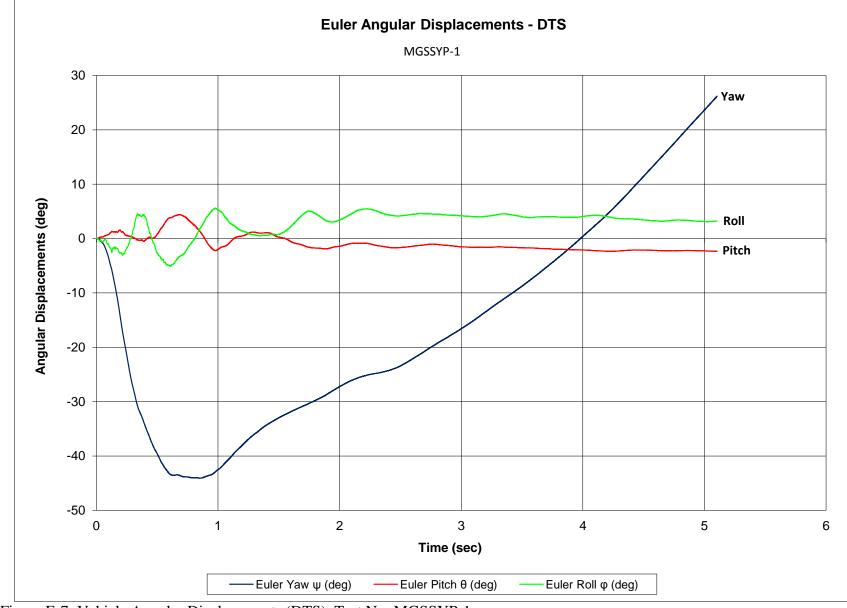


Figure E-6. Lateral Occupant Displacement (DTS), Test No. MGSSYP-1



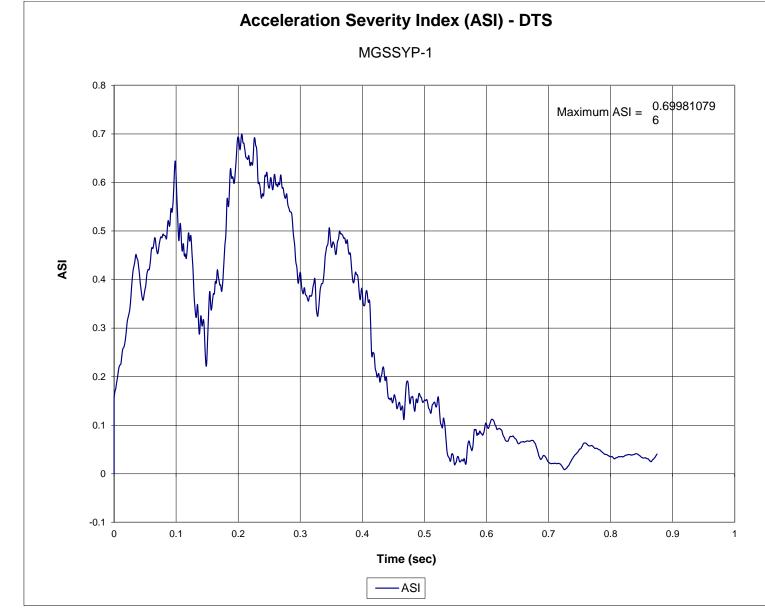


Figure E-8. Acceleration Severity Index (DTS), Test No. MGSSYP-1

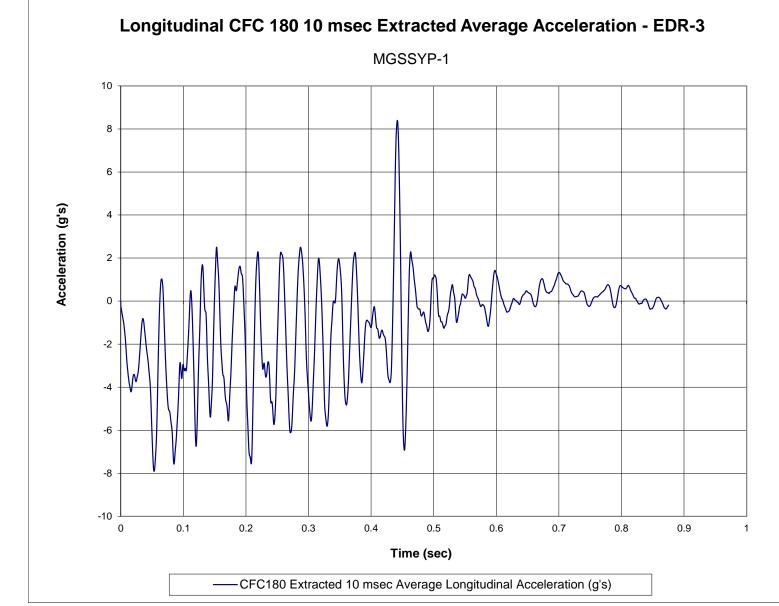


Figure E-9. 10-ms Average Longitudinal Deceleration (EDR-3), Test No. MGSSYP-1

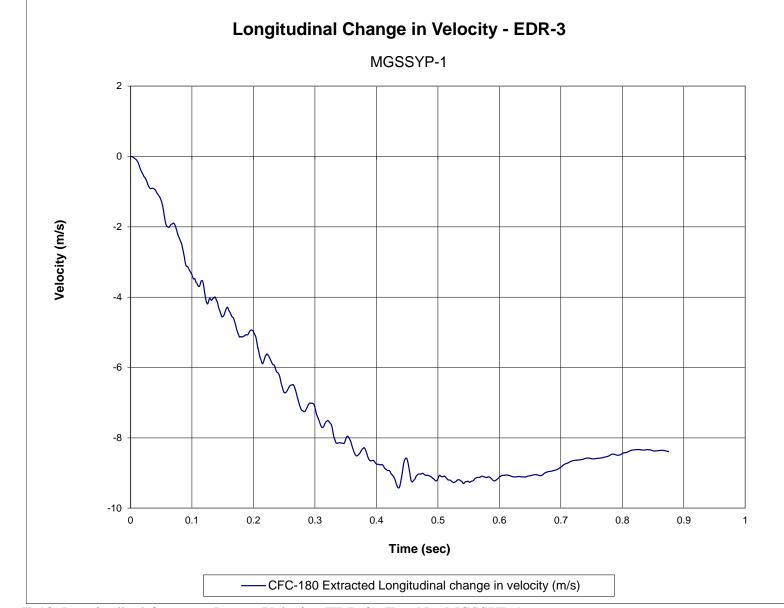


Figure E-10. Longitudinal Occupant Impact Velocity (EDR-3), Test No. MGSSYP-1

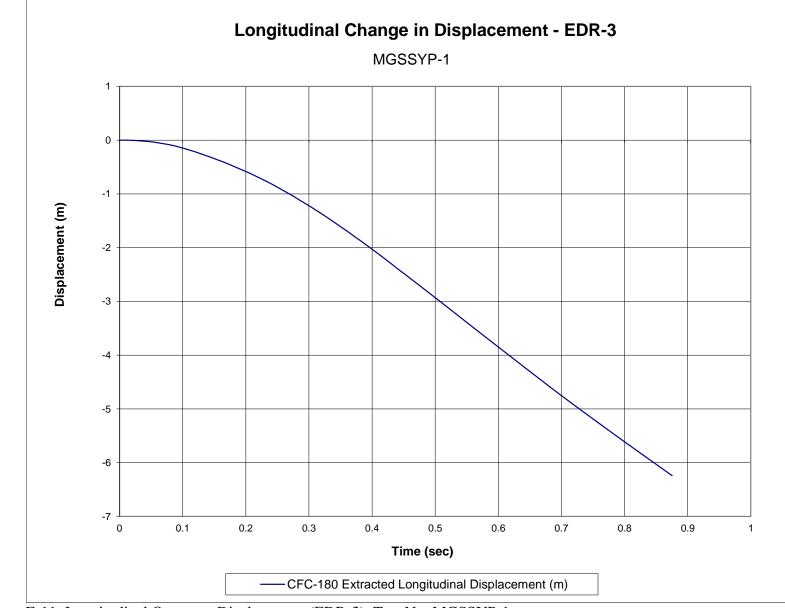


Figure E-11. Longitudinal Occupant Displacement (EDR-3), Test No. MGSSYP-1

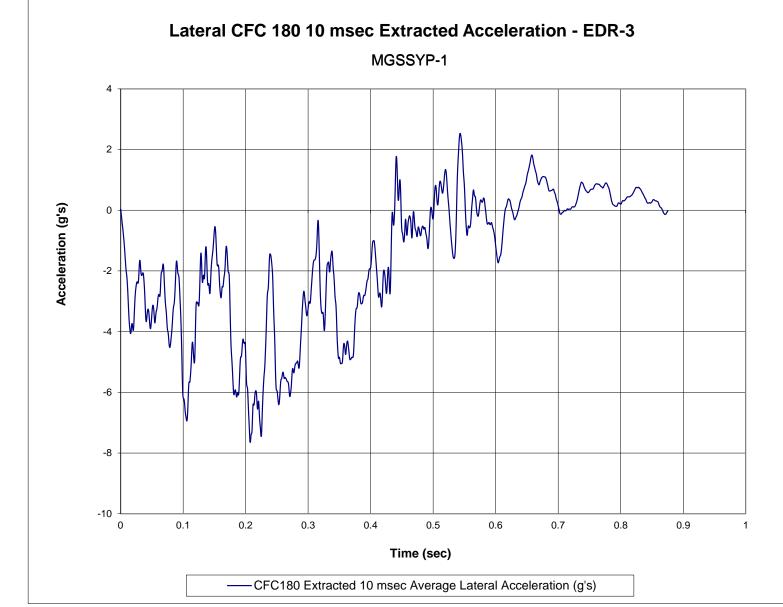


Figure E-12. 10-ms Average Lateral Deceleration (EDR-3), Test No. MGSSYP-1

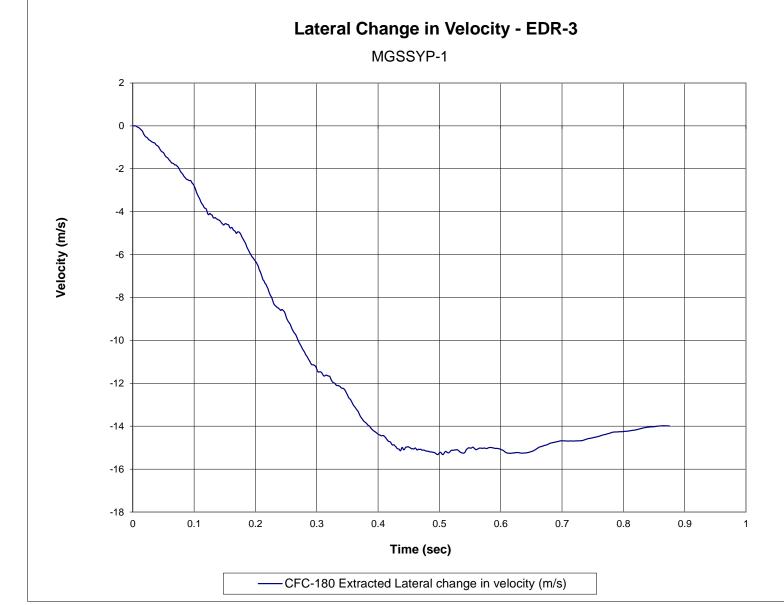


Figure E-13. Lateral Occupant Impact Velocity (EDR-3), Test No. MGSSYP-1



Figure E-14. Lateral Occupant Displacement (EDR-3), Test No. MGSSYP-1

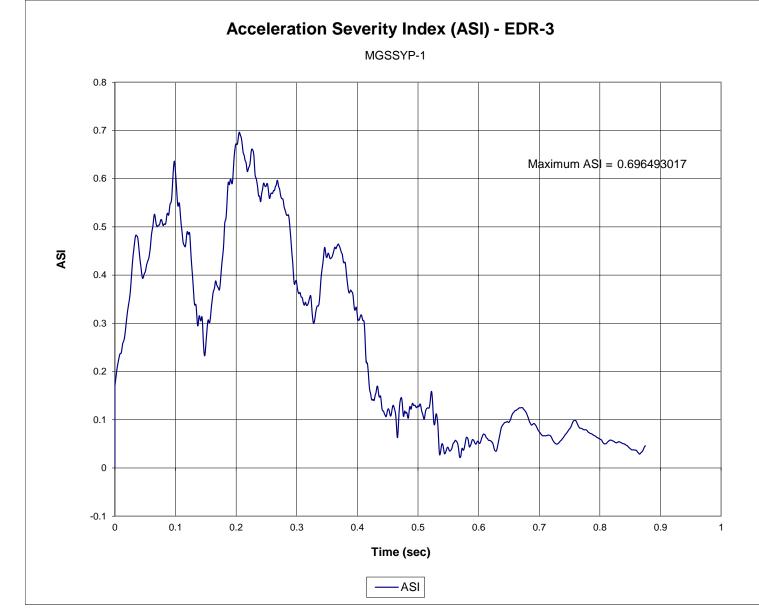


Figure E-15. Acceleration Severity Index (EDR-3), Test No. MGSSYP-1

## Appendix F. Accelerometer and Rate Transducer Data Plots, Test No. MGSSYP-2

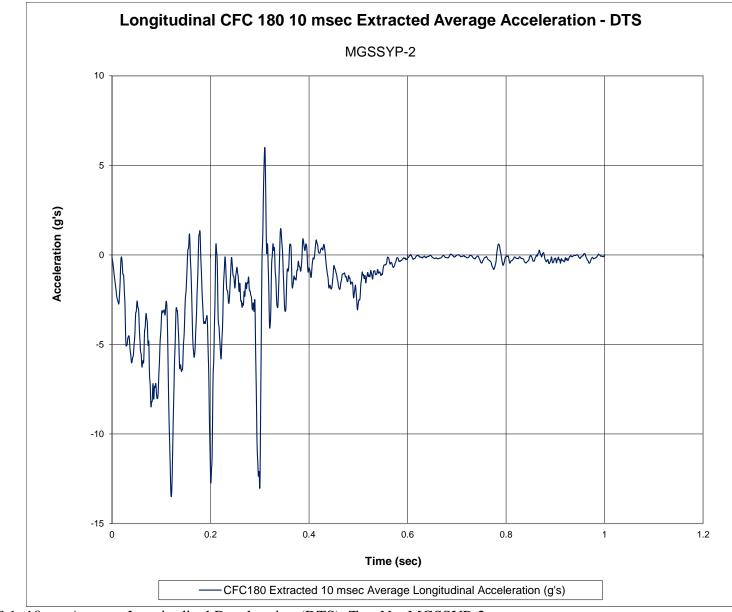


Figure F-1. 10-ms Average Longitudinal Deceleration (DTS), Test No. MGSSYP-2

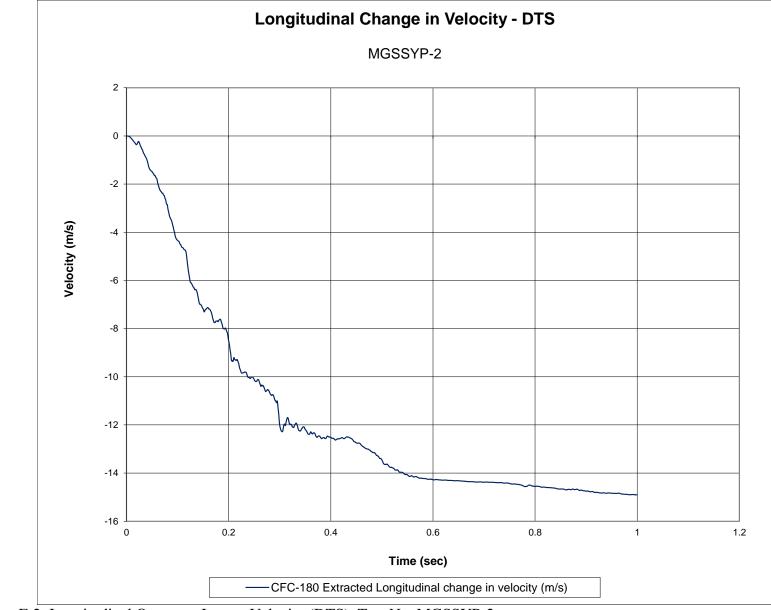


Figure F-2. Longitudinal Occupant Impact Velocity (DTS), Test No. MGSSYP-2

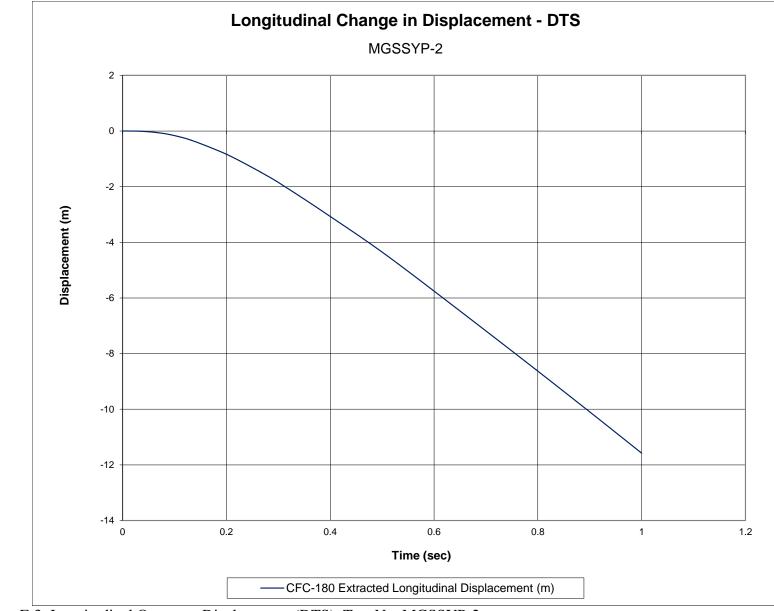


Figure F-3. Longitudinal Occupant Displacement (DTS), Test No. MGSSYP-2

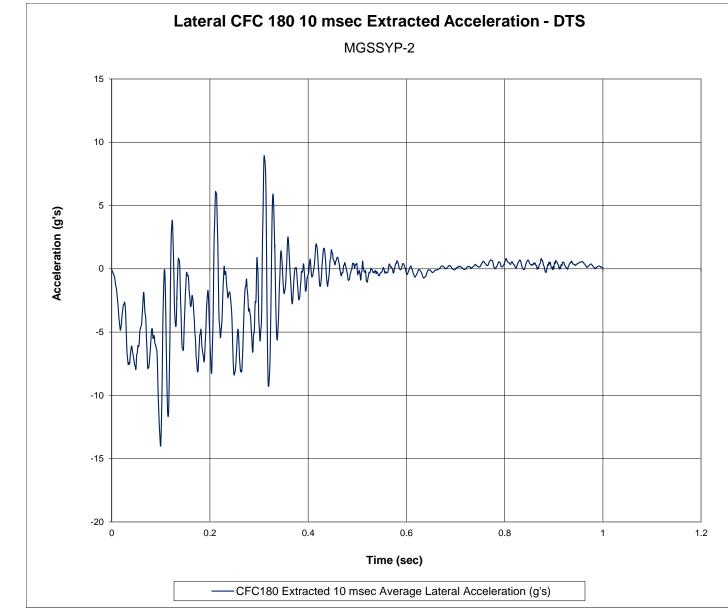


Figure F-4. 10-ms Average Lateral Deceleration (DTS), Test No. MGSSYP-2

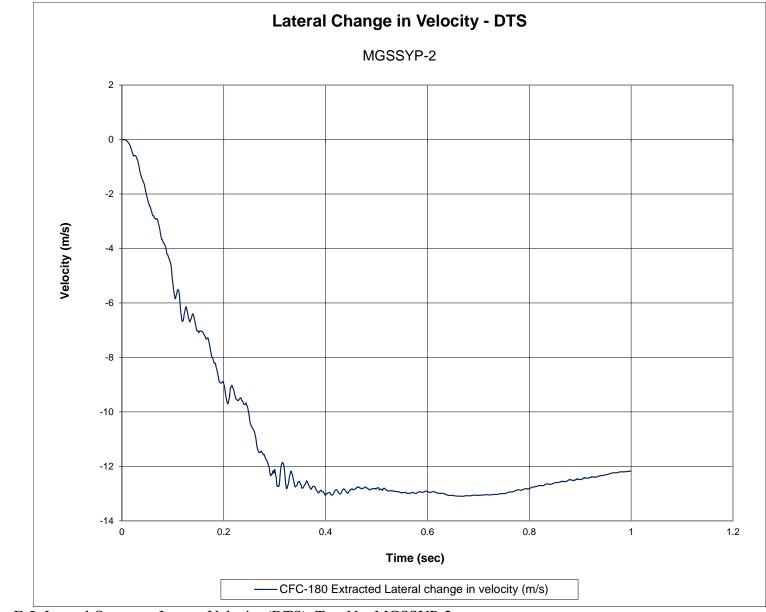


Figure F-5. Lateral Occupant Impact Velocity (DTS), Test No. MGSSYP-2

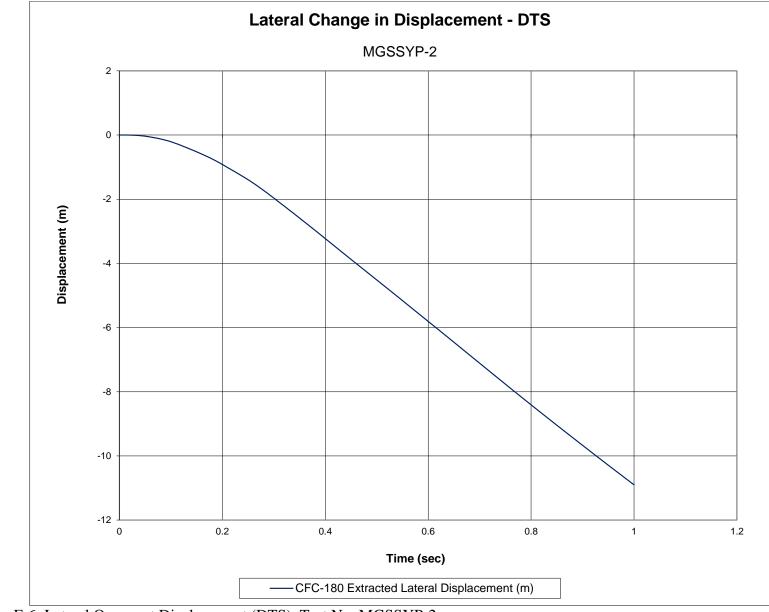


Figure F-6. Lateral Occupant Displacement (DTS), Test No. MGSSYP-2

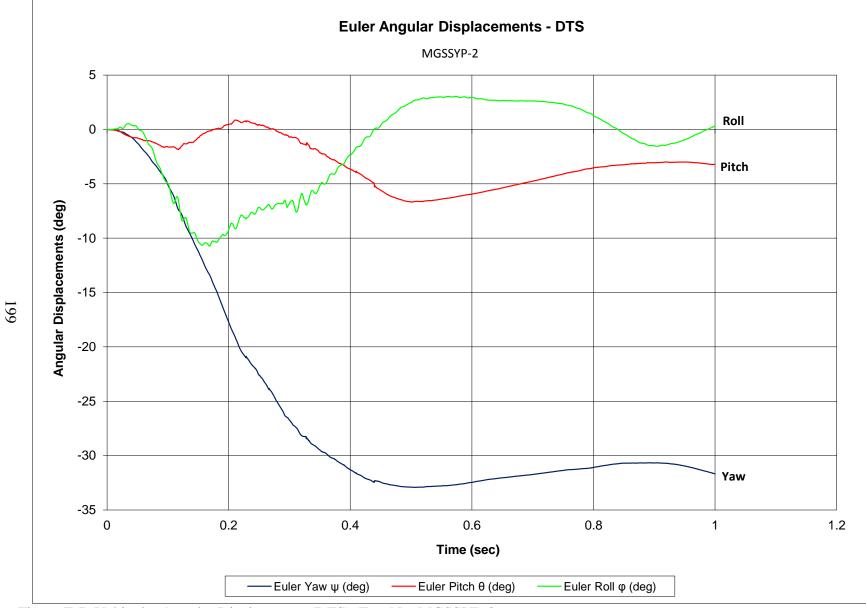


Figure F-7. Vehicular Angular Displacement (DTS), Test No. MGSSYP-2

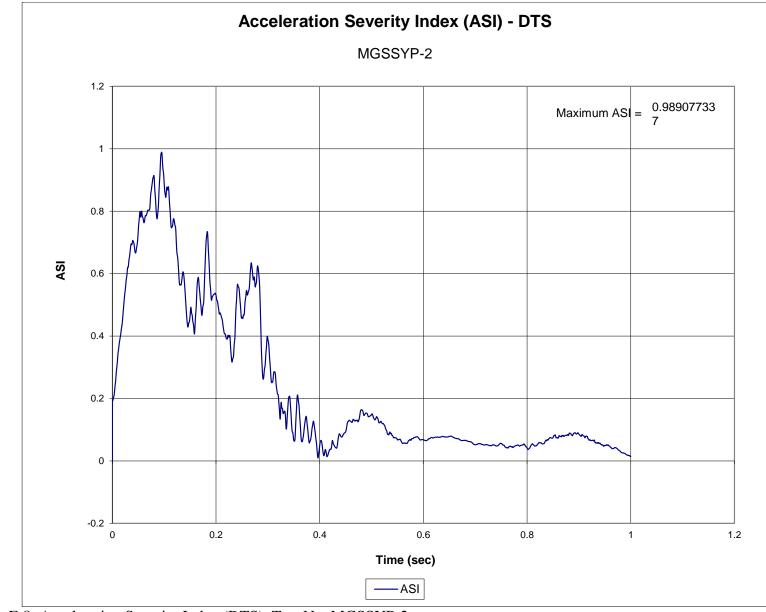


Figure F-8. Acceleration Severity Index (DTS), Test No. MGSSYP-2

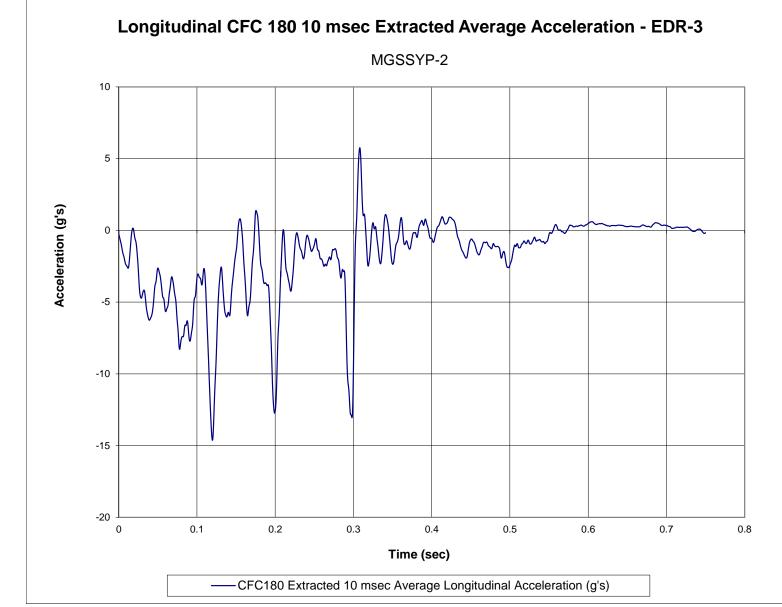


Figure F-9. 10-ms Average Longitudinal Deceleration (EDR-3), Test No. MGSSYP-2

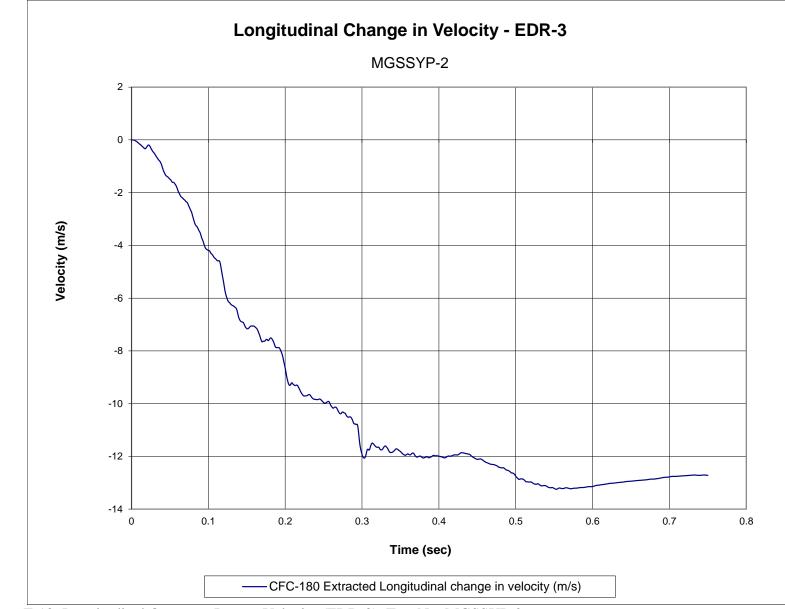


Figure F-10. Longitudinal Occupant Impact Velocity (EDR-3), Test No. MGSSYP-2



Figure F-11. Longitudinal Occupant Displacement (EDR-3), Test No. MGSSYP-2

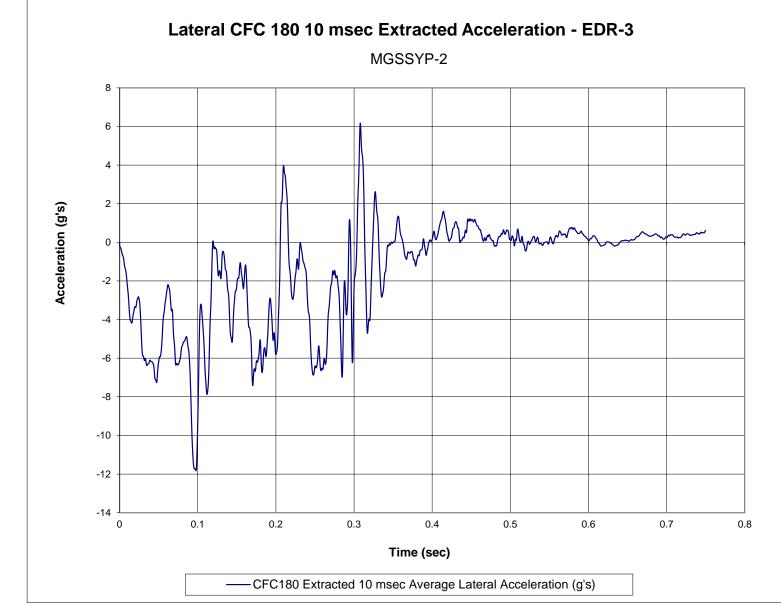


Figure F-12. 10-ms Average Lateral Deceleration (EDR-3), Test No. MGSSYP-2

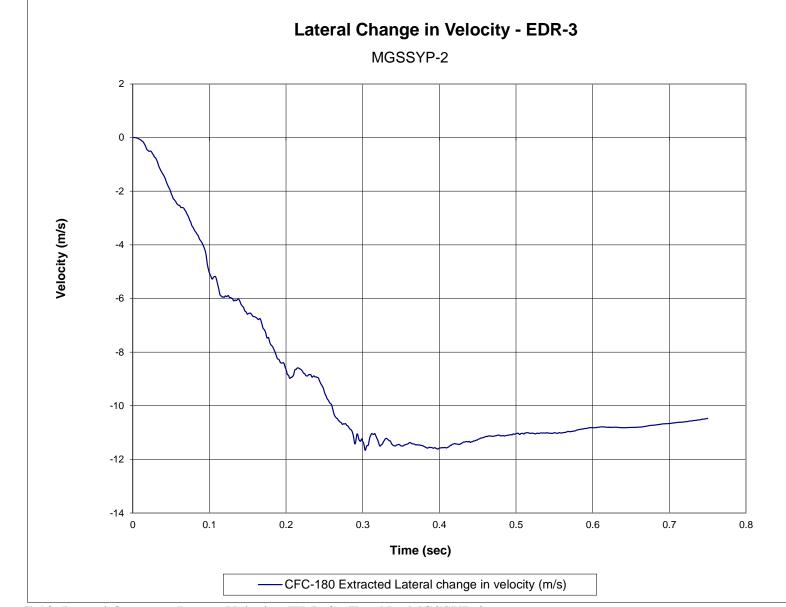


Figure F-13. Lateral Occupant Impact Velocity (EDR-3), Test No. MGSSYP-2



Figure F-14. Lateral Occupant Displacement (EDR-3), Test No. MGSSYP-2

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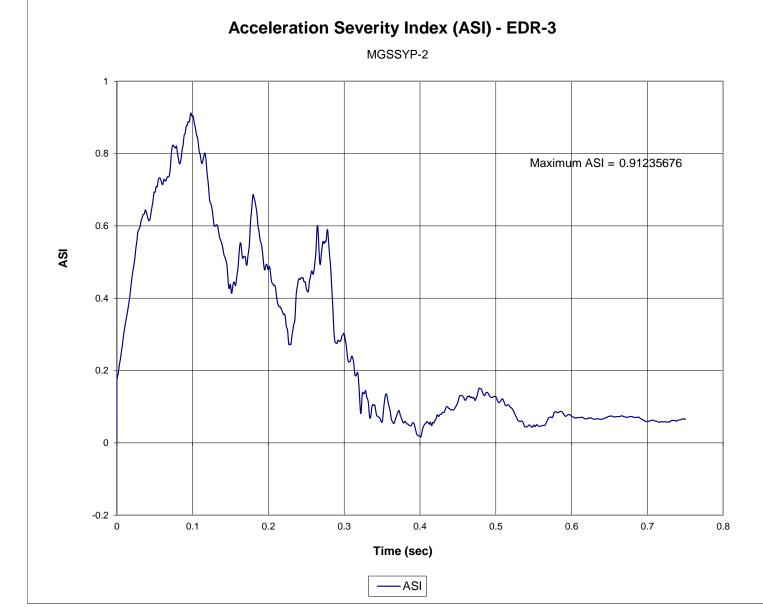


Figure F-15. Acceleration Severity Index (EDR-3), Test No. MGSSYP-2

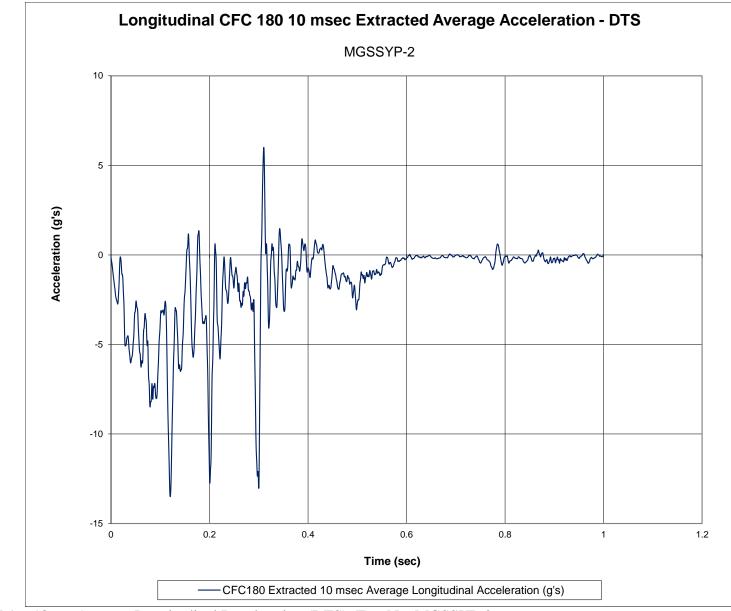


Figure F-16. 10-ms Average Longitudinal Deceleration (DTS), Test No. MGSSYP-2

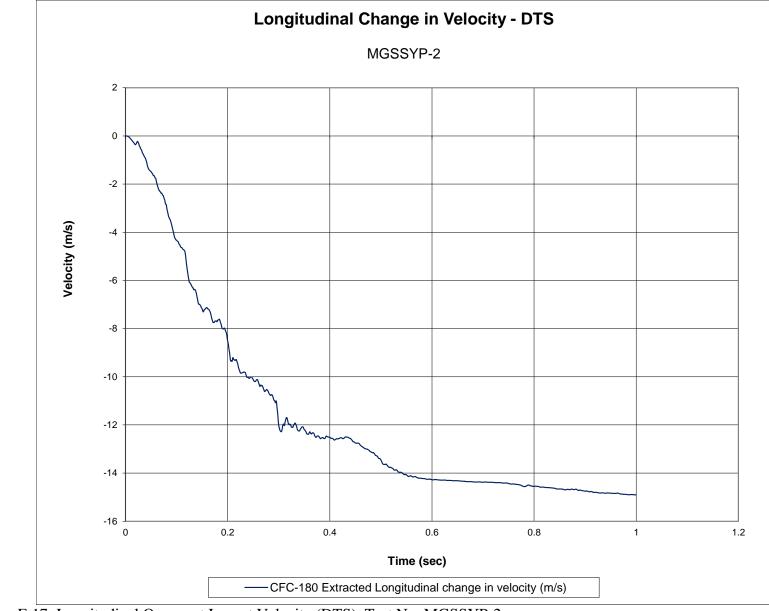


Figure F-17. Longitudinal Occupant Impact Velocity (DTS), Test No. MGSSYP-2

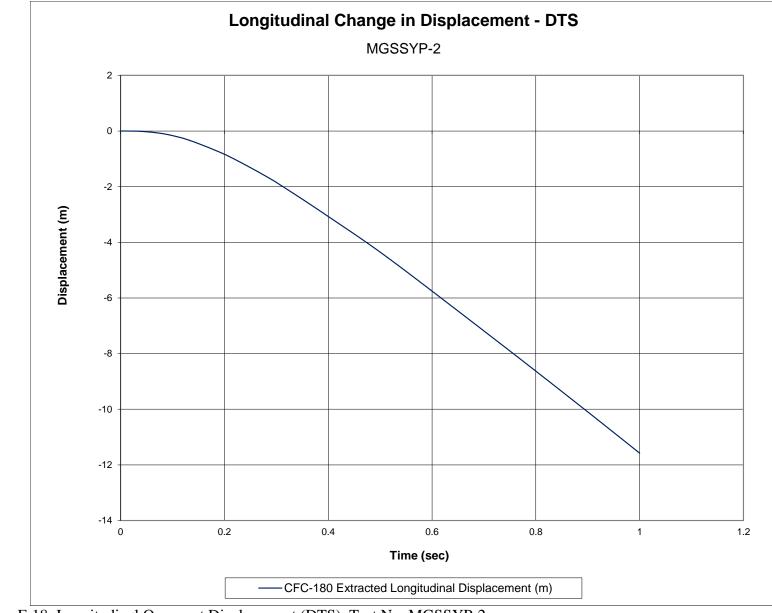


Figure F-18. Longitudinal Occupant Displacement (DTS), Test No. MGSSYP-2

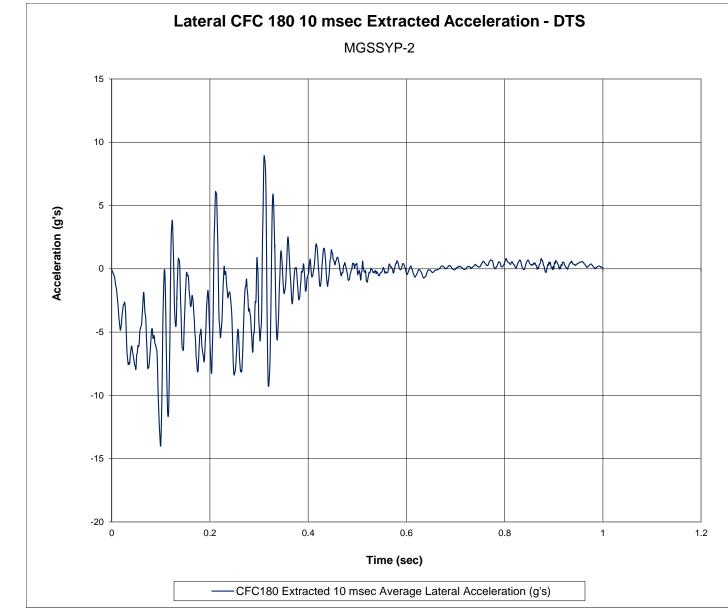


Figure F-19. 10-ms Average Lateral Deceleration (DTS), Test No. MGSSYP-2

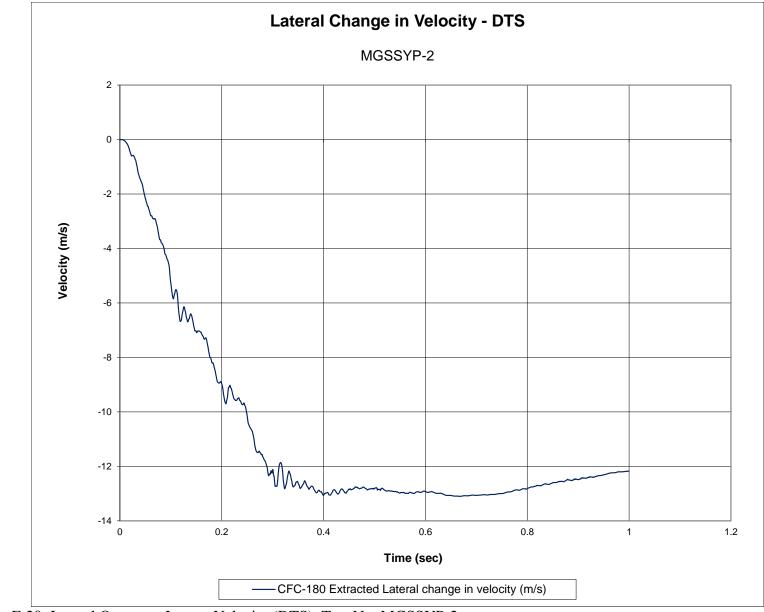


Figure F-20. Lateral Occupant Impact Velocity (DTS), Test No. MGSSYP-2

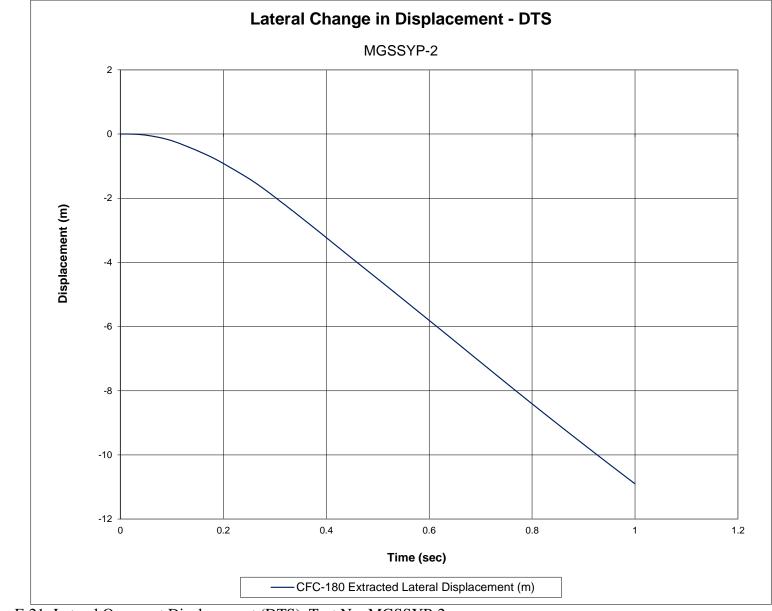


Figure F-21. Lateral Occupant Displacement (DTS), Test No. MGSSYP-2



Figure F-22. Vehicular Angular Displacement (DTS), Test No. MGSSYP-2

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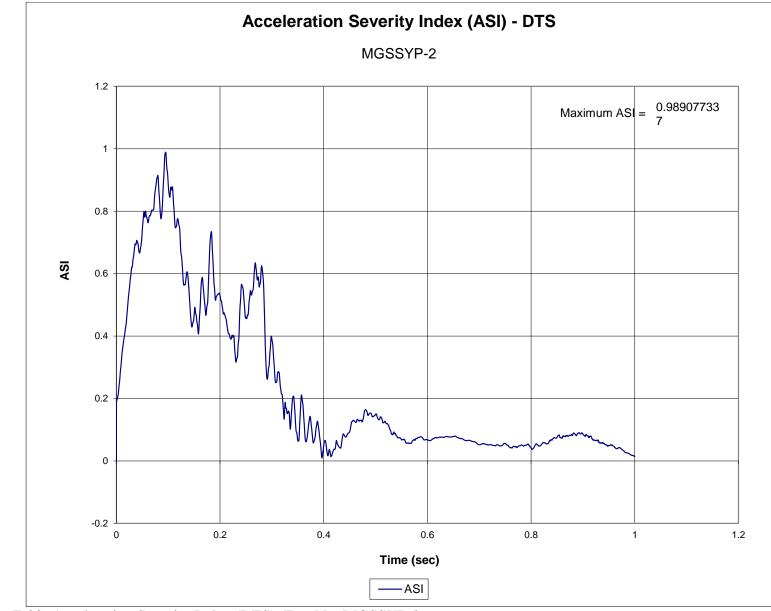


Figure F-23. Acceleration Severity Index (DTS), Test No. MGSSYP-2

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