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Implementation of Conductive Concrete for Deicing (Roca Bridge)

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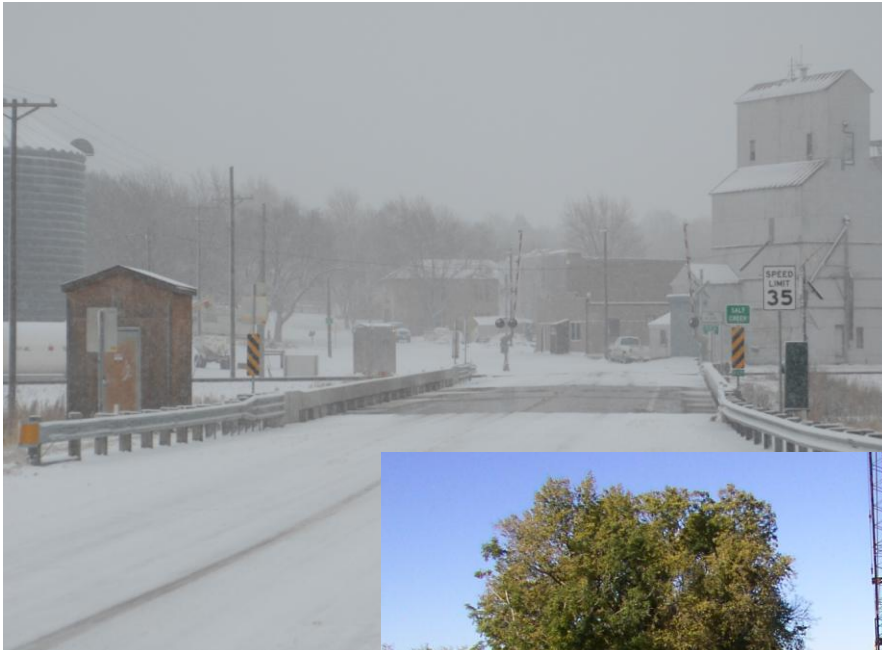
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IMPLEMENTATION OF CONDUCTIVE CONCRETE FOR DEICING (ROCA BRIDGE)

Nebraska Department of Roads
Project No. SPR-P1(04) P565



July 2008

IMPLEMENTATION OF CONDUCTIVE CONCRETE FOR DEICING (ROCA BRIDGE)

A Final Report

Submitted to

Nebraska Department of Roads

For

Project No. SPR-P1(04) P565

by

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16. Abstract <p>The search for improved deicing methods has been a research focus for quite some time. Existing technologies perform deicing by chemical, electrical or thermal energy sources. Electrically conductive concrete is produced by adding electrically conductive components to a regular concrete mix to attain stable electrical conductivity to enable conduction of electricity through the concrete. In the application for bridge deck deicing, a thin layer of conductive concrete can generate enough heat due to its electrical resistance to prevent ice formation on the pavement surface when connected to a power source.</p> <p>The heated deck of Roca Spur Bridge is the first implementation in the world using conductive concrete for deicing. The Roca Spur Bridge is a 150-ft long and 36-ft wide, three-span highway bridge over the Salt Creek at Lincoln, Nebraska, located near U.S. Route 77 South. This experimental bridge deck, after 5 years of evaluation, has shown that using conductive concrete has the potential to become a very cost-effective bridge deck deicing method. The technology provides an environment-friendly solution to address the looming crisis of water supply contamination by road salts, particularly on bridge decks over streams and rivers in the cold regions.</p>			
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TABLE OF CONTENTS

TECHNICAL REPORT DOCUMENTATION	i
DISCLAIMER	ii
ACKNOWLEDGMENTS	iii
TABLE OF CONTENTS	iv
LIST OF FIGURES	vii
LIST OF TABLES	ix
 CHAPTER 1 INTRODUCTION	
1.1 Background	1
1.2 The Roca Spur Bridge.....	2
1.3 Organization of the Report.....	3
 CHAPTER 2 REVIEW OF DEICING TECHNOLOGIES	
2.1 Deicing Technologies.....	5
2.2 Fixed Automated Spray Systems.....	5
2.3 Pavement Heating Systems.....	6
2.3.1 Electric Heating Cables	6
2.3.2 Hydronic Systems.....	7
2.4 Others.....	8
 CHAPTER 3 ELECTRICALLY CONDUCTIVE CONCRETE	
3.1 Electric Conduction Mechanism.....	9
3.2 Concrete Mixes with Steel Fibers and Steel Shavings	10
3.3 Concrete Mixes with Steel Fibers and Carbon Particles.....	13
3.3.1 Workability and Finishability.....	14
3.3.2 Compressive Strength.....	15
3.3.3 Heating Rate.....	15
3.3.4 Electric Resistivity.....	16
3.3.4.1 Long-term Stability of Electric Resistivity.....	21

CHAPTER 4 THE ROCA SPUR BRIDGE – DESIGN AND CONSTRUCTION

4.1 Construction Sequence.....	23
4.2 Integration of Power Supply, Sensors and Control Circuit.....	26
4.2.1 Software Requirements.....	27
4.3 Construction Costs.....	27

CHAPTER 5 THE ROCA SPUR BRIDGE – DEICING PERFORMANCE

5.1 Deicing Operations.....	29
5.2 Deicing Performance.....	30
5.3 Relationship Between Electrical Conductivity and Temperature.....	32

CHAPTER 6 LESSONS LEARNED

6.1 Electrical Wiring Scheme.....	34
6.1.1 Diagnostics of Stray Current and Remedy.....	35
6.2 Concerns for Electric Shock.....	37
6.2.1 Applying Epoxy Coating.....	38
6.2.2 Adding a Regular Concrete Layer.....	39
6.2.2.1 Effect on Heating Rate.....	39
6.2.2.2 Effect on Stray Current.....	40
6.3 Bridge Smoothness Tests and Surface Grinding.....	43
6.4 Bridge Deck Inspections.....	44
6.4.1 Mapping of Spalls.....	46
6.4.2 Samples Coring and Locations.....	46
6.4.3 Epoxy Patching.....	49
6.4.4 Further Inspections.....	49
6.4 Public Awareness	51

CHAPTER 7 CONCLUSIONS AND RECOMMENDATIONS

7.1 Conclusions.....	52
7.2 Recommendation for Future Research.....	54
7.2.1 Automation of the Deicing System.....	54

7.2.2 Adjustable Power Source.....	54
7.2.3 Implementation Plan.....	54
REFERENCE.....	55
APPENDICES	
Appendix A – Construction Drawings.....	59
Appendix B – Roca Bridge Deicing System Software User’s Manual.....	75
Appendix C – Weather Data.....	83

LIST OF FIGURES

Figure 1	Deicing Experiment.....	12
Figure 2	Heating tests conducted with slabs in the freezer.....	16
Figure 3	Electric Resistivity vs. Temperature – EC-All Mix	19
Figure 4	Electric Resistivity vs. Temperature – Slag+25% EL Mix.....	20
Figure 5	Comparison of Heating Rates of Trial Mixes.....	20
Figure 6	Time Effect on Electric Resistivity.....	21
Figure 7	Conductive Concrete Panel Layout.....	22
Figure 8	Angle iron electrodes and thermocouple wiring layout	25
Figure 9	PVC Conduits and Junction Boxes pre-positioned in the Regular Reinforced Concrete Bridge Deck.....	25
Figure 10	Electrodes connection to power chords.....	26
Figure 11	Ice-free Bridge Deck	29
Figure 12	Average Slab Current vs. Slab Temperature Relationship.....	33
Figure 13	Hot spots along the Centerline of the Bridge Deck.....	34
Figure 14	Application of Epoxy Coating and utility sand	39
Figure 15	Effects of Concrete Cover on Heating Rate	40
Figure 16	Conductive concrete test slab submerged in water.....	41
Figure 17	Stray Current Measurements	42
Figure 18	Reduction of Stray Current by adding a 0.25 in. topping.....	43
Figure 19	Cement paste cover was milled off leaving steel fibers exposed ..	45

Figure 20	Close-up of exposed steel fibers and spalls.....	45
Figure 21	Damage to the Epoxy Coating along Bridge Centerline	46
Figure 22	Locations of Cored Samples.....	47
Figure 23	Cored Samples from Roca Bridge Deck.....	48
Figure 24	Deterioration of Eastbound Lane Slabs.....	49
Figure 25	Close-up of Surface Spalls in Eastbound Lane.....	50
Figure 26	No Noticeable Deterioration in Westbound Lane Slabs.....	51
Figure 27	Deicing Performance in an Ice Storm – November 30, 2007.....	52
Figure 28	Roca Spur Bridge Deicing Operation	53

LIST OF TABLES

Table 1	Properties of Conductive Concrete with Steel Fibers and Shavings.....	11
Table 2	Eutectic and Effective Temperatures of various Deicing Chemicals	12
Table 3	Deicing Data of Conductive Concrete with Steel Fibers and Shavings...	13
Table 4	Workability and finishability of the trial mixes with carbon and graphite products.....	15
Table 5	Average 28-day compressive strength.....	15
Table 6	Comparisons of heating rate, operating voltage, and average current for conductive concrete mixes.....	17
Table 7	Electrical resistivity for carbon concrete mixes.....	18
Table 8	Properties of Conductive Concrete with Steel Fibers and Carbon Particles.....	22
Table 9	Comparison of different deicing systems	28
Table 10	Deicing Performance of Roca Spur Bridge	31
Table 11	Power Chord Wiring Reconfiguration.....	36

CHAPTER 1

INTRODUCTION

1.1 Background

Electrically conductive concrete is an emerging concrete technology that has many practical applications, including bridge deck deicing, radiant heating, roadway health monitoring, electromagnetic wave shielding, cathodic rebar protection, just to name a few. Electrically conductive concrete is produced by adding electrically conductive components to a regular concrete mix to attain stable electrical conductivity to enable conduction of electricity through the concrete. In the application for bridge deck deicing, a thin layer of conductive concrete can generate enough heat due to its electrical resistance to prevent ice formation on the pavement surface when connected to a power source.

Under a previous research sponsored by Nebraska Department of Roads, a concrete mix containing steel fibers and steel shavings^[1] was developed specifically for concrete bridge deck deicing. Steel shavings are industrial waste from metal fabrications. Several drawbacks were noted about using steel shavings during development of the conductive concrete: (1) there was a lack of consistency of sizes and compositions from various sources of steel shavings; (2) steel shavings acquired were usually contaminated with oil, which required cleaning; and (3) steel shavings required a specialized mixing procedure to ensure uniform dispersal in the concrete.

As a follow-up effort, carbon and graphite products were used to replace steel shavings in the conductive concrete mix design. Seven carbon and graphite products were evaluated experimentally^[2].

The electrical conductivity and the associated heating rate were improved with the carbon products. A concrete mix containing 1.5 percent of steel fibers and about 15 percent of carbon powder by volume was developed specifically for concrete bridge deck deicing. Crushed limestone of 0.5 in. maximum size and Nebraska 47B fine aggregate were also used in the mix. The mix has adequate strength and is able to provide adequate thermal power density for deicing under subfreezing temperature.

1.2 The Roca Spur Bridge

Based on promising laboratory testing results, the Nebraska Department of Roads approved a demonstration project at Roca, located about 15 miles south of Lincoln, Nebraska. The heated deck of Roca Spur Bridge is the first implementation in the world using conductive concrete for deicing. The Roca Spur Bridge is a 150-ft long and 36-ft wide, three-span highway bridge over the Salt Creek at Roca, Nebraska, located near U.S. Route 77 South. The Roca Bridge project was let in December 2001 and construction was completed in November 2002. The bridge deck consists of a 115-ft by 28-ft, 4-in thick conductive concrete inlay. The inlay has been instrumented with temperature and current sensors to provide data for monitoring deicing operations during winter storms. The deicing performance has been satisfactory and consistent for the past five years. The average energy cost was about \$250 per snow storm. Conductive concrete has the potential to become a very cost-effective bridge deck deicing method when compared with other deicing technologies.

The successful deicing demonstration at the Roca Spur Bridge has attracted much attention from the transportation industry and researchers from all over the world. The project has been featured in numerous national as well as international news media and publications.

For instance, the **Discovery Channel** aired a technology report featuring this innovative deicing technology, which can be viewed at <http://www.exn.ca/dailyplanet/view.asp?date=2/20/2004>.

The Roca Bridge project won the **2003 Award of Excellence** bestowed by the Nebraska Chapter of the American Concrete Institute (ACI) for the innovative use of concrete.

This demonstration project has national and international implications. Statistics indicate that 10 to 15 percent of all roadway accidents are directly related to weather conditions. This percentage alone represents thousands of human injuries and deaths and millions of dollars in property damage annually. Ice accumulation on paved surfaces is not merely a concern for motorists; ice accumulation on pedestrian walkways accounts for numerous personal injuries, due to slipping and falling. The conductive concrete deicing technology is readily available for implementation at accident-prone areas such as bridge overpasses, exit ramps, airport runways, street intersections, sidewalks, and driveways.

1.3 Organization of the Report

This report documents the details of a demonstration project at Roca, Nebraska, to implement a 4 in. deck inlay using conductive concrete for deicing.

Chapter 2 provides a review of existing pavement surface deicing technologies. The advantages and disadvantages of the various systems are presented. The construction and operating costs are compared. Chapter 3 documents the development of a conductive concrete mix at the University of Nebraska especially for bridge deck deicing and anti-icing. Chapter 4 discusses the construction sequence and the integration of an instrumented conductive concrete inlay for bridge deck deicing. Chapter 5 presents the heating performance and operational costs

during a five-year long evaluation. Chapter 6 summarizes the lessons learned during the operations of the Roca Spur Bridge deicing system. Chapter 7 provides conclusions and recommendations.

CHAPTER 2

REVIEW OF DEICING TECHNOLOGIES

2.1 Deicing Technologies

Most highway winter maintenance depends upon using chemicals and fine granular particles as a primary means for deicing and anti-icing^[3]. The use of road salts and chemicals for deicing is an effective method for ice removal but causes damage to concrete and corrosion of reinforcing steel in concrete bridge decks. This problem is a major concern to transportation and public works officials due to rapid degradation of existing concrete pavements and bridge decks. The search for improved deicing methods has been a research focus for quite some time.

Many deicing technologies exist and have been previously reviewed by Yehia and Tuan^[1,4]. These technologies can be categorized as deicing by chemical, electrical or thermal energy sources. The use of electric cables and heated fluid in pipes has been attempted. Deicing technologies using microwave have also been under development by Long et al.^[5] and Hopstock and Zanko^[6]. The various types of deicing systems are summarized as follows.

2.2 Fixed Automated Spray Systems

Since the use of road salt has contaminated ground water to a harmful level and caused leaching of heavy metals from the soils, especially in the northeastern U.S. and Canada, expensive but “green” deicing chemicals, such as potassium acetate, are used. Fixed automated systems of spraying deicing chemicals have been used by many states, including Colorado, Maryland, Minnesota, North Dakota, Oregon, and Wisconsin. Installation of spray systems is site-specific and requires large storage tanks, large spaces and pumping hardware, resulting in an

initial cost of about \$600,000^[7]. Pinet et al.^[8] reported that annual chemical cost was about \$12,000 for a system installed for the Ontario Ministry of Transportation. Annual maintenance for a spray system consists of draining and rinsing the system and storage tank at the end of the winter season and preventive maintenance to the system pump, with an estimated cost of \$32,800^[7]. In addition, the service life of a pump is about 5 years, and the cost for pump and control software replacement is estimated at \$3,500.

Based on a research conducted for the National Cooperative Highway Research Program (NCHRP) Project 20-7/Task 200, Shi et al.^[9] reported that the experience with these spray systems in North America and Europe has revealed mixed findings. Several studies have indicated significant reductions in accident frequency and in mobile operations costs, while others reported many problems related to system activation, maintenance and training. For instance, the Denver International Airport had one system installed in 1998 but it has not functioned as anticipated.

2.3 Pavement Heating Systems

2.3.1 Electric Heating Cables

Heating systems for bridge decks and ramps have typically been embedded resistive electrical cables or pipes containing heated fluid. Electric heating cables were installed on the approach to a highway drawbridge in Newark, New Jersey, in 1961^[10]. The heat generated was sufficient to melt 1 in. of snow per hour. However, this installation was later abandoned because the electric cables were pulled out of the asphaltic concrete overlay due to traffic movement. A similar system was installed in two ramps and a bridge deck in Teterboro, New Jersey, in 1964^[11]. This system was reported to have been deicing satisfactorily. The power consumption

was about 35 W/ft^2 and the annual operating cost was approximately $\$0.45/\text{ft}^2$. Electric heating cables were also embedded in a concrete bridge deck in Omaha, Nebraska, in 1970^[11]. However, the sensing elements activating the heating unit were unreliable and manual operation was necessary.

2.3.2 Hydronic Systems

Gravity-operated heat pipes with a geothermal heat exchanger were implemented in a bridge deck in Laramie, Wyoming, in 1981^[12]. This system utilized the latent heat of vaporization released from condensation of an evaporated liquid (e.g., ammonia) to heat the bridge deck. The heated surface was about 4°F to 25°F warmer than the unheated portion of the bridge during operation. The heating was sufficient to prevent freezing of the deck surface and to melt snow. The main disadvantages were the complication of the construction and the assembly of the heat pipes. Approximately 40 percent of the total cost was related to drilling and grouting the pipes. Copper pipes containing heated anti-freeze by a geothermal source were installed in a canal bridge deck in Oregon in 1950^[11]. The system successfully kept the deck free of ice. Rubber hoses containing heated anti-freeze by a gas boiler were embedded in a concrete pedestrian overpass in Lincoln, Nebraska, in 1993^[13]. The fluid used was propylene glycol with water at a flow rate of 454 L/min . to deliver 473 W/m^2 heat flux to the deck, sufficient to keep the walkway ice free. However, the system has not been in service due to a leak in the polyvinyl chloride (PVC) supply and return lines. The installation cost of the heating system was $\$15/\text{ft}^2$, and the operating cost per storm was about $\$250$ to melt 3 in. of snow. Steel pipes carrying Freon heated up to 300°F by a propane boiler were installed in the deck of Buffalo River Bridge in Amherst, Virginia, in 1996^[14]. However, the freon cooled off and condensed before it could

reach the upper third of the bridge deck. Several different working fluids were being tested to identify a replacement for Freon. The installation cost was about \$181,000 and the estimated operating cost was about \$1000 annually. Similar hydronic systems have been installed in Ohio, Oregon, Pennsylvania, South Dakota, Texas and West Virginia. High construction costs and frequent maintenance were reported^[11] about these systems.

2.4 Others

Other ice control schemes which were attempted but found to be ineffective included using infrared heat lamps^[11] and insulating bridge deck with urethane foam^[15].

CHAPTER 3

ELECTRICALLY CONDUCTIVE CONCRETE

3.1 Electric Conduction Mechanism

Using electrically conductive concrete for deicing is an emerging material technology. Conventional concrete is not electrically conductive. The electric resistivity of normal weight concrete ranges between 6 – 11 $\text{k}\Omega\cdot\text{m}$ ^[16]. Conduction of electricity through concrete may take place in two ways: electronic and electrolytic. Electronic conduction occurs through the motion of free electrons in the conductive media, while electrolytic conduction takes place by the motion of ions in the pore solution. In fresh concrete and during hydration, conduction of electricity is achieved by the motion of ions. However, in hardened concrete where little moisture is available, conduction can only take place by free electrons. Therefore, metallic or other conductive fibers and particles must be added to the concrete matrix to achieve stable and relatively high electrical conductivity.

Whittington et al.^[16] investigated conduction of electricity through conventional concrete using cement paste and concrete specimens. The electric resistivity was found to increase with time for both specimens because conduction in these specimens depended on the ions motion in the pore solution. In addition, the electric resistivity of the concrete specimens was higher than that of the cement paste specimens, due to the restricted ions movement from non-conductive aggregates used in the concrete specimens. Farrar^[17] in 1978 used “Marconite,” a carbon by-product from oil refining, to replace sand in a conductive concrete mix. The electric resistivity of the conductive concrete using Marconite ranges between 0.5 to 15 $\Omega\cdot\text{cm}$. The use of Marconite was limited to small-scale applications such as electromagnetic shielding and anti-

static flooring because it was expensive. Conduction of electricity in this case was through the movement of electrons, and the particles must be in continuous contact within the concrete. This phenomenon is called “electrical percolation” in concrete^[17,18].

Heating tests have been conducted using both AC and DC power to study the conduction of electricity through the conductive concrete mix developed at the University of Nebraska. The conductive concrete behaved like a semiconductor or a capacitor^[19]. As electrical current flows through the conductive concrete, its temperature rises and the heating rate increases. The electrical conductivity of the conductive concrete will increase as its temperature rises. The increase in electrical conductivity will cause more current to flow through under a constant voltage. Hence, the applied voltage must be controlled to maintain a gradual heating rate to avoid thermal shock to the conductive concrete.

Since the conductive components added only amounted to about 20 percent by volume of the total materials, there are probably not enough conductive fibers and particles to form a fully interconnected electronic circuit within the concrete. Instead, these dispersed conductive materials would act as capacitors when a voltage is applied across the material. Electrical current will flow through the material if the applied voltage is high enough to cause dielectric breakdown of the material. There is a critical threshold of voltage, above which large current will go through the material like a short circuit. If the applied voltage is kept below this “break down” voltage, a “controllable” amount of current proportional to the voltage will go through the material. This behavior is similar to that of a surge protector used in computers^[19].

3.2 Concrete Mixes with Steel Fibers and Steel Shavings

Under a previous research sponsored by Nebraska Department of Roads, a conductive concrete mix specifically for bridge deck deicing^[1] was developed in 1998. In this mix, steel fibers of variable lengths and steel shavings with different particle sizes were added to the concrete mix to provide conductive materials. More than 150 trial mixes were tested^[19] to quantify the volumetric ratios of the steel fibers and steel shavings for optimum performance. The mechanical and physical properties of the optimized mix are given in Table 1. The compressive strength, flexural strength, modulus of elasticity, and rapid freeze-thaw resistance of the conductive concrete mixes tested have met or exceeded the American Association of State Highway and Transportation Officials (AASHTO) requirements for bridge deck construction.

Table 1. Properties of Conductive Concrete with Steel Fibers and Shavings

Properties	Test Result
Unit weight	150 pcf
Compressive strength	5000 psi
Flexural strength	670 psi
Modulus of Elasticity	527 ksi
Rapid Freeze-thaw Resistance	no failure during 312 cycles
Shrinkage	less than ACI-209 by 20~30%
Permeability	0.004~0.007 cm ³ /sec
Thermal Conductivity	7.8 W/m-°K
Electrical Resistivity	500~1000 Ω-cm

A 4-in. thick conductive concrete layer was cast on the top of a 6-in. thick, 4 ft by 12 ft conventional reinforced concrete slab for conducting deicing experiments during three winters (1998-2000). As shown in Fig.1, the overlay was preheated before and heated during a storm,

which is more energy efficient than heating the overlay after snow has accumulated. The applied voltage and the associated current as well as the climatic data were recorded in each experiment.



Figure 1. Deicing Experiment

For a deicing chemical, there is an “effective temperature” below which the amount of chemical required to melt the snow and ice will be unreasonably excessive. The effective temperatures of common deicing chemicals^[20] are given in Table 2.

Table 2. Eutectic and Effective Temperatures of various Deicing Chemicals

Deicing Chemical	Eutectic Temp (°C)	Effective Temp (°C)
Sodium chloride (NaCl)	-6	+15
Calcium chloride (CaCl)	-60	-20
Magnesium chloride (MgCl)	-28	+5
Potassium acetate (KAc)	-76	-15
Calcium magnesium acetate (CMA)	-17	+21
Urea	+10	+25

In the winter of 2000, most of the experiments were conducted while the initial overlay temperature was about 16°F. Most deicing chemicals would become ineffective at this temperature. The heating rate of the conductive concrete depends upon the amount of current going through, which, in turn, depends upon the ambient temperature, humidity, wind speed and time of day. The deicing performance of the conductive concrete was satisfactory, as demonstrated by Fig. 1. Typical data from deicing experiments are summarized in Table 3.

Table 3. Deicing Data of Conductive Concrete with Steel Fibers and Shavings

Date	Snow accumulation (in.)	Wind speed (mph)	Air temperature (°F)	Power consumption (kW-hr)	Unit Energy Cost (\$/ft²)
Feb. 11, 1999	3	6	24	32.48	0.052
Feb. 17, 1999	8	4	34	42.64	0.068
Feb. 20, 1999	2	4	37	9.84	0.016
Feb. 22, 1999	11	19	26	33.76	0.054
Mar. 8, 1999	10	15	32	46.16	0.074

3.3 Concrete Mixes with Steel Fibers and Carbon Particles

Steel shavings are waste materials produced by steel fabricators in the form of small particles of random shapes. Several drawbacks were noted about using steel shavings during development of the conductive concrete: (1) there was a lack of consistency of sizes and compositions from various sources of steel shavings; (2) steel shavings acquired were usually contaminated with oil and required cleaning; and (3) steel shavings required a specialized mixing procedure to ensure uniform dispersal in the concrete mix.

In the spring of 2001, carbon products were used to replace the steel shavings in the conductive concrete mixes. Seven commercial carbon and graphite products were tested^[2]. Ten trial mixes were prepared from the seven products as follows:

1. 20% Black Diamond
2. 25 % Earth Link
3. 41 % Earth Link - Replacing all cement content
4. 25% EC- 98C 10×0
5. 25% EC- 100 10×0
6. 25% EC- 97 3/8×0
7. 25% EC-100 3/8×0
8. 25% FP-428 100×0
9. 25% ALL - All graphite products were used in this mix except Black Diamond
10. 25% Earth Link + Slag aggregate

Black Diamond (BD) is the trade name of a natural graphite crystalline in the form of pellets. Earth Link (EL) is the trade name of graphite cement, which contains approximately 70 percent of portland cement and 30 percent of graphite powder. The EC designations are used to distinguish carbon products of different particle sizes. FP-428 is a product of small carbon particles. Crushed limestone of 0.5 in. maximum size was used in the trial mixes. However, 0.5-in. 25A-BF blast furnace slag was used in one trial mix to replace the limestone with an intent to improve the electrical conductivity. Coarse blast furnace slag is the co-product of molten iron production in a blast furnace. When molten, slags float on the metal. Separating the two is not exact and there is some iron residue in the slags. All mixes contained 1.5 percent of steel fibers per unit volume. The added carbon amounted to 20 percent per volume of the conductive concrete. The criteria used for evaluating of one cubic feet of each trial batch were workability and finishability, compressive strength, heating rate, and electric resistivity.

3.3.1 Workability and Finishability

Workability and finishability were the two primary criteria used in the preliminary evaluation of the trial mixes, and the observations are summarized in Table 4.

Table 4. Workability and finishability of the trial mixes with carbon and graphite products

Product	Workability	Finishability	Comments
1.Black Diamond	Good	Good	Gas release during hydration causes increase in volume
2.Earth Link	Good	Good	Mixes with 41% “EL” require more Superplasticizer
3.EC- 98C 10X0	Good	Good	
4.EC- 100 10X0	Good	Good	
5.EC- 97 3/8X0	Good	Good	
6.EC-100 3/8X0	Good	Good	
7.FP-428 100X0	Good	Good	Requires more Superplasticizer

3.3.2 Compressive Strength

Three cylinders from each trial mix were tested after 28 days. The average compressive strength is summarized in Table 5.

Table 5. Average 28-day compressive strength

Trial Mix	Average 28-day Compressive Strength (psi)
1. 20% Black Diamond	3483
2. 25% Earth Link	5770
3. 41% Earth Link	4735
4. 25% EC- 98C 10X0	6811
5. 25% EC- 100 10X0	5870
6. 25% EC- 97 3/8X0	6061
7. 25% EC-100 3/8X0	5416
8. 25% FP-428 100X0	3817
9. 25% All	4997
10. 25% Earth Link with Slag aggregate	6750

3.3.3 Heating Rate

Small-scale heating tests using 18 in. × 13 in. × 2.5 in. slabs were conducted to measure the electrical resistivity. Two steel plates were embedded in a slab as the electrodes. A thermocouple was embedded in the middle of each test slab to monitor the temperature. Alternate current was applied under constant voltage, and the resulting current and temperature from each slab were recorded. The slabs were kept inside a freezer during the tests to maintain constant ambient temperature. Fig. 2 shows a slab under heating test. Heating tests were conducted with two initial temperatures, 25°F and 35°F. Alternate current (AC) power with a constant voltage of 140 volts was applied while the current and slab temperature were recorded for 30 minutes. The results are summarized in Table 6.



Figure 2. Heating tests conducted with slabs in the freezer

Table 6. Comparisons of heating rate, operating voltage, and average current for conductive concrete mixes

Specimen	Condition	Heating Rate	Breakdown Voltage	Operating Voltage	Average Current
EC-100(3/8x0)	25°F	0.45	N/A	140	0.93
EC-100(3/8x0)	35°F	0.48	N/A	140	1.13
EC-100(10x0)	25°F	0.46	N/A	140	0.67
EC-100(10x0)	35°F	0.68	N/A	140	0.95
EC-98C(10x0)	25°F	0.16	N/A	140	0.48
EC-98C(10x0)	35°F	0.19	N/A	140	0.61
EC-97(3/8x0)	25°F	0.69	N/A	140	0.89
EC-97(3/8x0)	35°F	0.68	N/A	140	1.00
FP-428(100x0)	25°F	0.25	N/A	140	0.43
FP-428(100x0)	35°F	0.13	N/A	140	0.47
EC-all	25°F	2.80	N/A	140	4.26
EC-all	35°F	3.08	N/A	140	4.82
41% EL	25°F	0.65	140	84	0.62
41% EL	35°F	0.56	140	84	0.69
BD 20%	25°F	0	N/A	140	0.11
BD 20%	35°F	0.16	N/A	140	0.17
Slag + 25% EL	25°F	5.88	N/A	140	2.39
Slag + 25% EL	35°F	4.11	N/A	140	1.97
25% EL	25°F	0.69	N/A	140	0.8
25% EL	35°F	0.67	N/A	140	1.13

3.3.4 Electric resistivity

Approximate values of the impedance and the electric resistivity were calculated for each trial mix using the following equations:

$$R = \frac{V}{I} \quad (1)$$

and

$$\rho = \frac{RA}{L} = \frac{VA}{IL} = \frac{1}{\text{Conductivity}} \quad (2)$$

where R is the resistance, V is the applied AC voltage, I is the AC current, ρ is the average electrical resistivity of the conductive concrete, L is the spacing between the electrodes, and A is the area of the conductive concrete cross-section parallel to the electrodes. The electrical conductivity of a material is the reciprocal of the electrical resistivity of that material. Since V , A , and L are constants in this application, the electrical conductivity is proportional to I . The electrical resistivity (or conductivity) of conductive concrete is temperature dependent, as illustrated below. A range of the electrical resistivity with respect to the initial temperature is given in Table 7.

Table 7. Electrical resistivity for carbon concrete mixes

Specimen	Initial Temperature	Temperature Range (°F)	Electrical Resistivity (Ohm.cm)
EC-100 (3/8×0)	25°F	25° - 40°	564 - 381
EC-100 (3/8×0)	35°F	35° - 50°	451 - 323
EC-100 (10×0)	25°F	25° - 40°	721 - 576
EC-100 (10×0)	35°F	35° - 60°	519 - 392
EC-98C (10×0)	25°F	25° - 30°	939 - 853
EC-98C (10×0)	35°F	35° - 40°	733 - 669
EC-97 (3/8×0)	25°F	25° - 50°	564 - 403
EC-97 (3/8×0)	35°F	35° - 60°	518 - 357
FP-428 (100×0)	25°F	25° - 35°	1048 - 958
FP-428 (100×0)	35°F	35° - 40°	902 - 900
EC-all	25°F	25° - over 100°	435 - 208
EC-all	35°F	35° - over 100°	395 - 184
41% EL	25°F	25° - 45°	789 - 600
41% EL	35°F	35° - 55°	665 - 580
BD 20%	25°F	25° - 25°	3507 - 3911

BD 20%	35°F	35° - 45°	2481 - 2533
slag + 25% EL	25°F	25° - over 100°	808 - 207
slag + 25% EL	35°F	35° - over 100°	705 - 206
25% EL	25°F	25° - 40°	847 - 346
25% EL	35°F	35° - 40°	394 - 369

Two trial mixes, EC-All and Slag+25% EL showed high electrical conductivity and heating rates. Experimental data from the heating tests of these two mixes are presented in Figs. 3 and 4, respectively. The electric resistivity of these materials is a function of temperature. As temperature increases, the materials become more electrically conductive. The higher electrical conductivity is probably due to the good gradation of carbon particles in the EC-All and the added slag in the Slag+25%EL mix. The heating rates of all the trial mixes are compared in Fig.5.

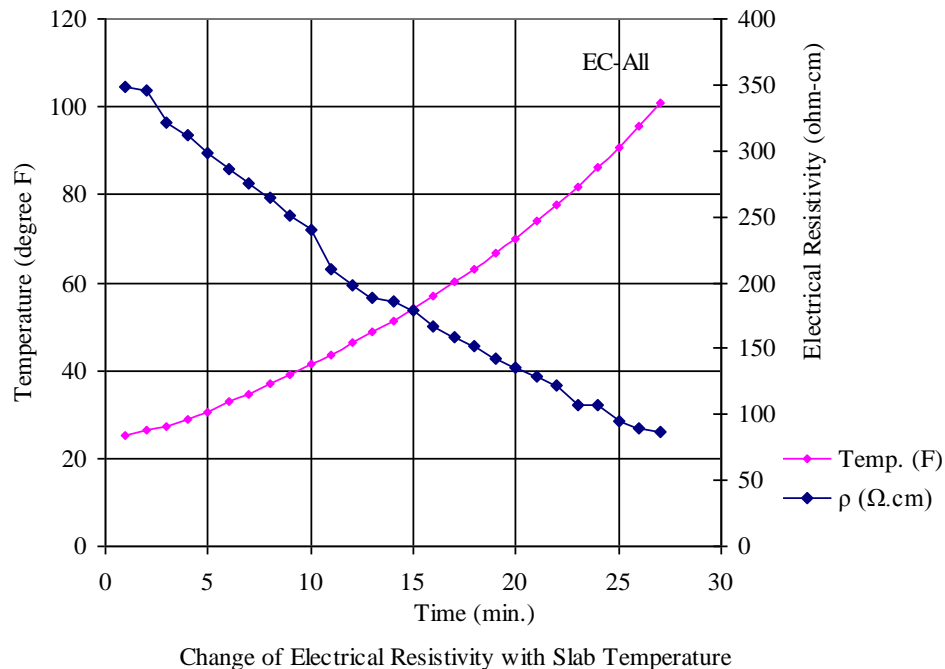
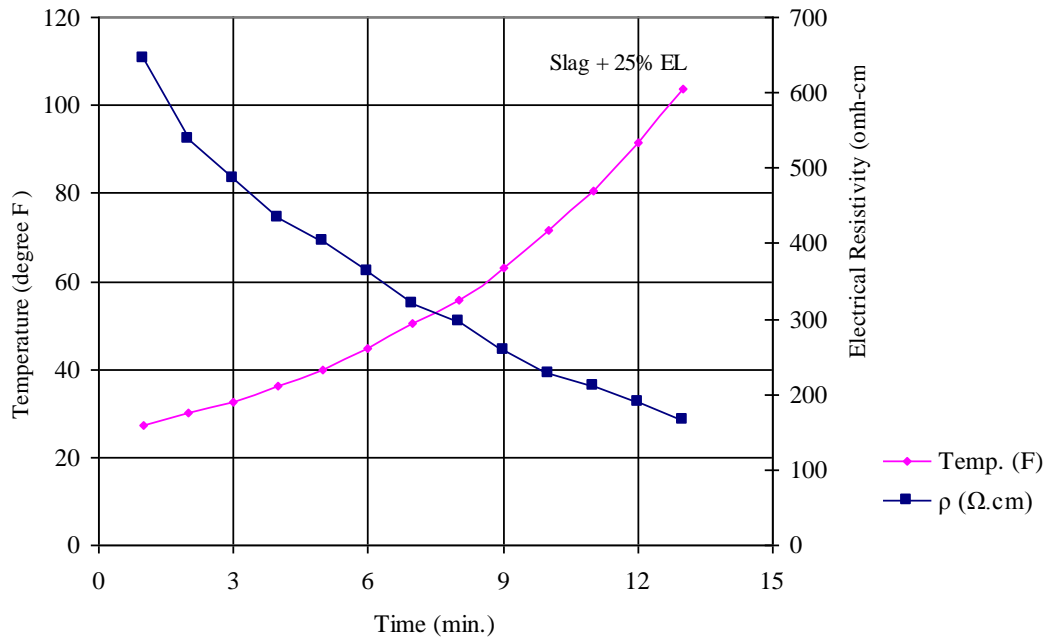


Figure 3. Electric Resistivity vs. Temperature – EC-All Mix



Change of Electrical Resistivity with Slab Temperature

Figure 4. Electric Resistivity vs. Temperature – Slag+25% EL Mix

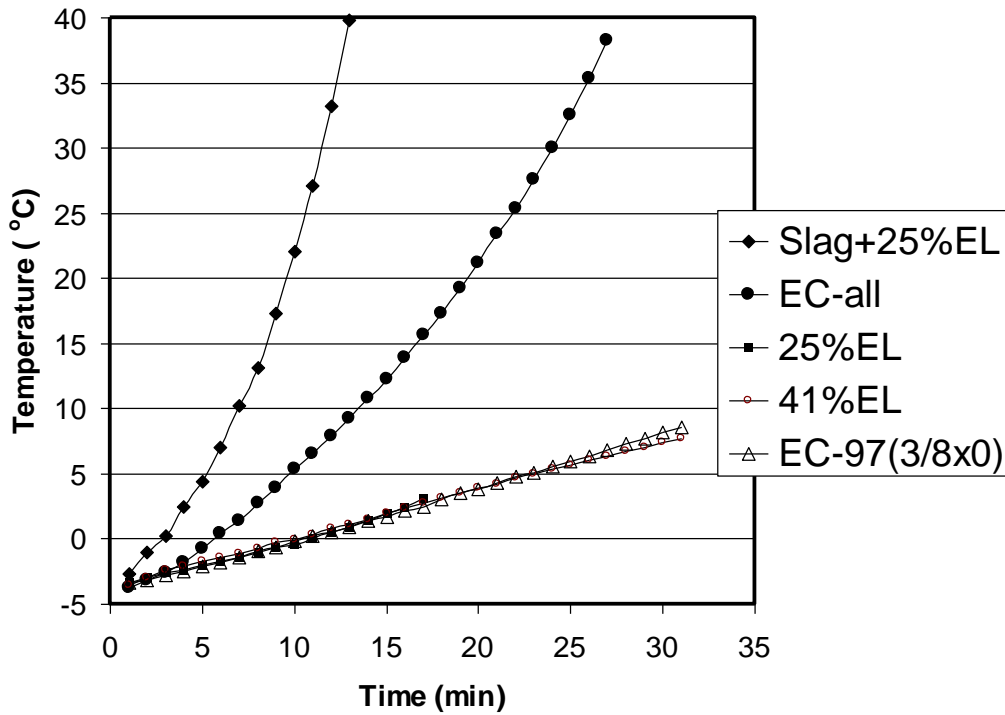


Figure 5. Comparison of Heating Rates of Trial Mixes

3.3.4.1 Long-term Stability of Electric Resistivity

The electric resistivity of the conductive concrete is relatively low during hydration, due to the ionic conduction in the pore solution. The breakdown voltage would thus depend upon the moisture content in the material. However, Yehia and Tuan^[1] showed that there exists a stable but higher breakdown voltage after the moisture in the conductive concrete has completely dried out. For instance, no degradation in the heating performance has been observed after 5 years of deicing experiment with the 4 ft × 12 ft conductive concrete test slab using steel fibers and steel shavings. To prove the same is true with the carbon concrete, a heating test was conducted on the EC-All test slab two years later. The data from the two tests are compared in Fig. 6. The lower electric resistivity and higher heating rate are probably due to the higher moisture content in the specimen during the earlier test.

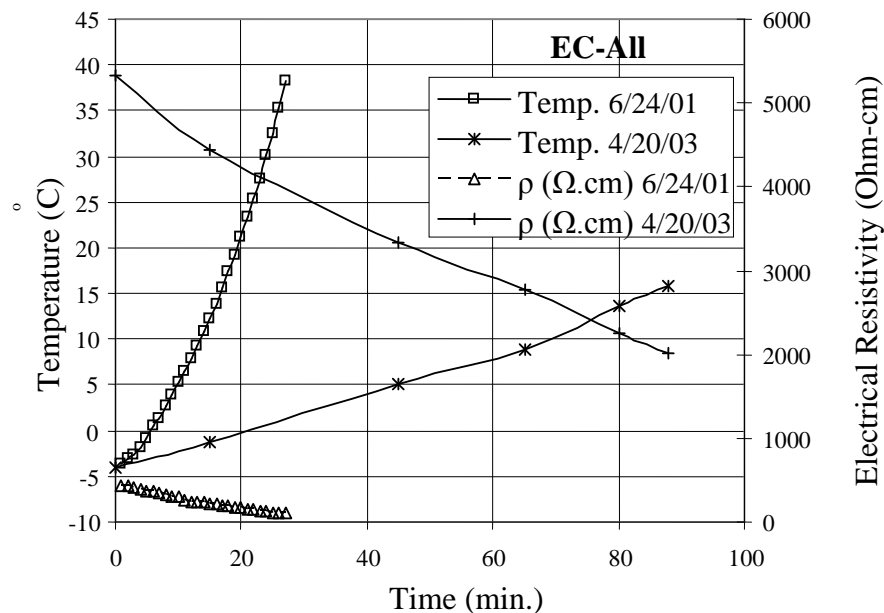


Figure 6. Time Effect on Electric Resistivity

Material testing was also conducted, and the results are presented in Table 8. Due to its superior strength and electrical conductivity, this conductive concrete was used for the Roca Spur Bridge project.

Table 8. Properties of Conductive Concrete with Steel Fibers and Carbon Particles

Properties	Test Result
Unit weight	145 pcf
Compressive strength	6950 psi
Flexural strength	820 psi
Rapid freeze-thaw resistance	no failure during 300 cycles
Electrical resistivity	300~500 Ω -cm

CHAPTER 4

THE ROCA SPUR BRIDGE – DESIGN AND CONSTRUCTION

Roca Spur Bridge is a 150-ft long and 36-ft wide, three-span highway bridge over the Salt Creek at Roca, located about 15 miles south of Lincoln, Nebraska. A railroad crossing is located immediately following the end of the bridge, making it a prime candidate for deicing application. The bridge deck has a 117 ft by 28 ft and 4 in. thick conductive concrete inlay, which is instrumented with thermocouples to provide data for monitoring deicing operations during winter storms.

The Roca Spur Bridge was designed by the Bridge Division of the Nebraska Department of Roads, as a conventional reinforced concrete slab bridge. However, a 117 ft by 28 ft by 4 in. thick space was reserved in the bridge deck for a conductive concrete inlay, as shown in Fig. 7. The conductive concrete inlay was cast after the reinforced concrete bridge had reached the 28-day strength. The design details are provided in the construction drawings, which are given in the Appendix A.

4.1 Construction Sequence

The Roca Bridge project was let in December 2001 and construction began in the summer of 2002. The bridge construction was completed in November 2002. A 4-in. thick inlay of conductive concrete inlay was cast on top of a 10.5-in. thick regular reinforced concrete deck. The inlay consists of 52 individual 4 ft × 14 ft conductive concrete slabs. In each slab, two 3-1/2 × 3-1/2 × 1/4 in. angle irons spaced 3.5 ft apart were embedded for electrodes, as shown in Fig. 8. Threaded sleeves were welded to one end of the angle irons for making electrical connection.

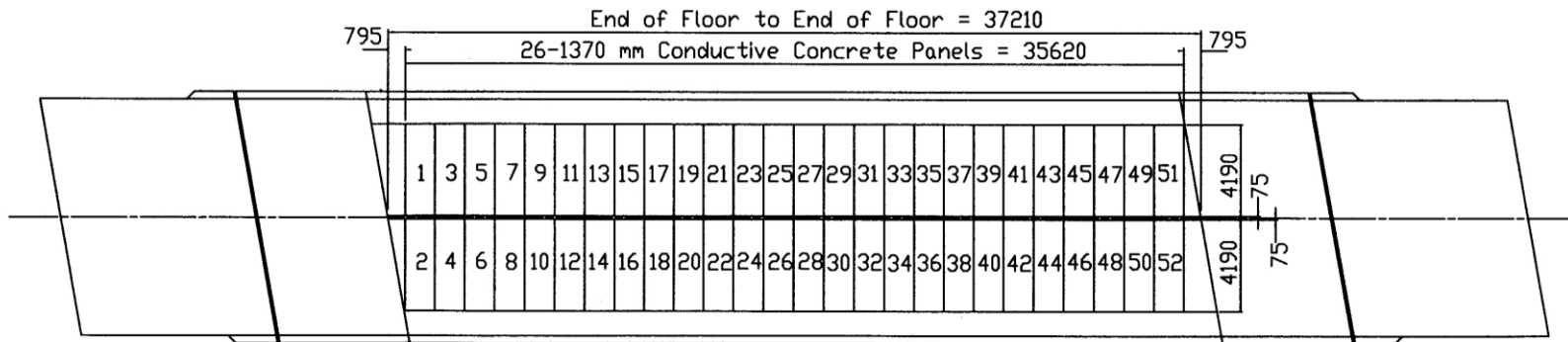


Figure 7. CONDUCTIVE CONCRETE PANEL LAYOUT
 (Dimensions in mm)



Figure 8. Angle iron electrodes and thermocouple wiring layout

A Type TX thermocouple was installed at the center of each slab at about 0.5 in. below the surface to measure the slab temperature. The power chords and thermocouple wiring for each slab were secured in two PVC conduits and are accessible from junction boxes along the centerline of the bridge deck, as shown in Fig. 9.



Figure 9. PVC Conduits and Junction Boxes pre-positioned in the Regular Reinforced Concrete Bridge Deck

The conductive concrete inlay was cast after the regular bridge deck had been cured for 30 days. The westbound lane was poured first and the eastbound lane next. After hardening, the conductive concrete inlay was saw cut to a 4 in. depth along the perimeters of the individual slabs and the gaps were filled with polyurethane sealant. There was a 6 in. gap along the centerline of the bridge to allow power chord connections with the threaded sleeves of the angle irons, as shown in Fig. 10. The gap was filled with a non-shrink, high-strength grout afterwards.

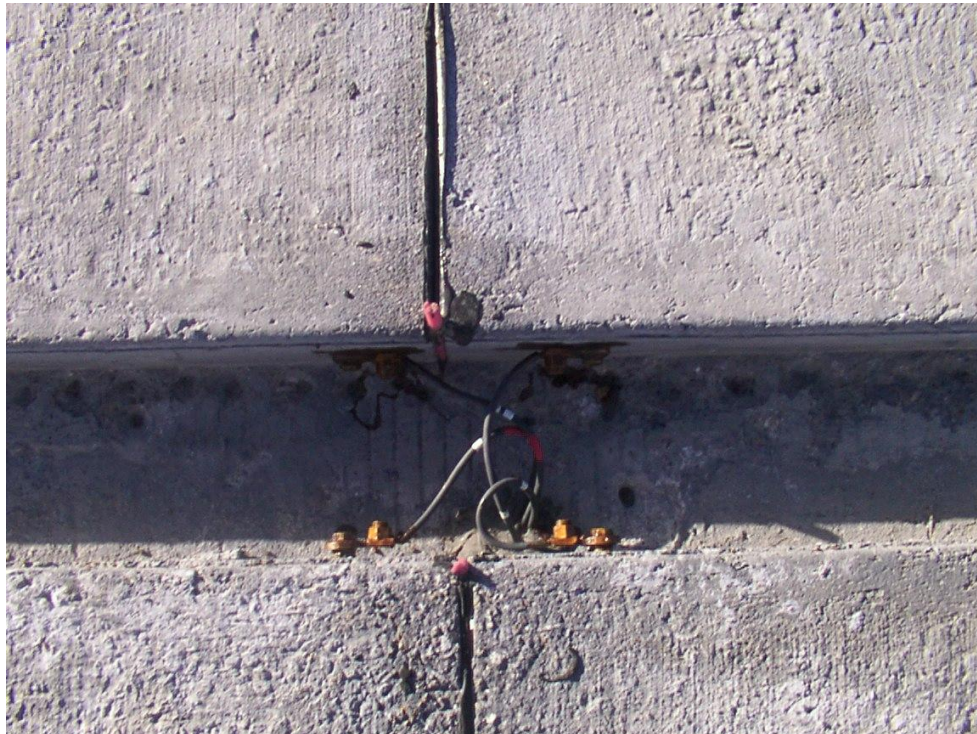


Figure 10. Electrodes connection to power chords

4.2 Integration of Power Supply, Sensors and Control Circuit

A three-phase, 600 A and 220 V AC power is available from a power line nearby. A microprocessor-based controller system was installed in a control room to monitor and control the deicing operation of the 52 slabs. The system includes four main elements: a temperature-sensing unit, a power-switching unit, a current-monitoring unit, and an operator-interface unit. The temperature-sensing unit takes and records the thermocouple readings of the slabs every 15

minutes. A slab's power will be turned on by the controller if the temperature of the slab is below 40°F and turned off if the temperature is above 55°F. The power-switching unit will control power relays to perform the desired on/off function. To ensure safety, a current-monitoring unit will limit the current going through a slab to a user-specified amount. The operator-interface unit will allow a user to connect to the controller with a PC or laptop via a phone modem. The operator interface displays all the temperature and electrical current readings of every slab in real time. A user also has the option of using a PC or laptop to download the controller-stored data into a spreadsheet.

4.2.1 Software Requirements

To remotely control the deicing operations via a phone modem, the software **RSLinx™** by Rockwell Software is required to establish a communication link with the deicing control module. The software for controlling the power on/off and monitoring the sensors was developed by Teamwork Technology Integration (TTI), Clear Lake, Iowa. To run the bridge control software, it is necessary to run **RSLinx™** first to activate the modem communication. A user's guide for the bridge control software is given in Appendix B.

4.3 Construction Costs

The construction costs of the conductive concrete inlay are itemized as follows:

- Placing, finishing, curing and saw cutting conductive concrete – \$50,020
- Procuring conductive concrete materials – \$80,620
- Building and installing control cabinet with sensors and power relays – \$43,685
- Integrating and programming the deicing operation controller – \$18,850

The total construction cost of the Roca Spur Bridge deicing system was therefore \$193,175. The cost per unit surface area of the conductive concrete inlay is \$59/ft². Life-cycle costs, including system maintenance costs and deck repair costs and vehicle depreciation caused by deicing chemicals, should be used as the basis for cost-effectiveness comparisons of different deicing systems. The construction costs of conductive concrete overlay/inlay are expected to drop significantly when the technology becomes widely accepted. The construction costs of the various deicing systems are compared in Table 9.

Table 9. Comparison of different deicing systems

Deicing System	Initial cost*	Annual operating cost*	Power consumption
Automated Spray System, 2004	\$600,000	\$12,000	Not applicable
Electric heating cable, 1961	\$54/m ²	\$4.8/m ²	323 - 430 W/m ²
Hot water, 1993	\$161/m ²	\$250/storm [76 mm snow]	473 W/m ²
Heated gas, 1996	\$378/m ²	\$2.1/m ²	Not available
Conductive concrete, 2003	\$635/m ²	\$0.80/m ² /storm	350 W/m ²

*Cost figures were quoted directly from the literature, and conversion to present worth was not attempted.

CHAPTER 5

THE ROCA SPUR BRIDGE – DEICING PERFORMANCE

5.1 Deicing Operations

The deicing controller system at the Roca Spur Bridge was completed in March 2003. Although major snow storms of 2002 were missed, the system was tested successfully under freezing temperature.

On December 9, 2003, the 52 slabs were energized in an alternating fashion during a storm. Groups of every other two slabs (1, 2, 5, 6, 9, 10, ..., 49 and 50 first, then 3, 4, 7, 8, 11, 12, ..., 51 and 52) (see Fig. 7) with a total of 26 slabs were powered for 30 minutes. This alternating powering scheme could not keep up with the low temperature, high wind and a snow rate of 25 mm/hr. As a result, the bridge deck was partially covered with snow and ice. The operating scheme has thus been changed and all the slabs are powered if the ambient temperature drops below 40°F. This revised powering scheme has worked well in many major storms. Fig. 11 shows an ice-free deck surface during the February 6, 2008 storm.



Figure 11. Ice-free Bridge Deck

5.2 Deicing Performance

The controller could store data for a 3-day period. Air temperature, slab temperatures and the current going through each slab (at 208 V) were recorded at 15-min intervals during each storm. The deicing data from eleven major storms has been analyzed for the past four winters. The climatic data of these storms were obtained for a weather station in Lincoln, Nebraska, from the National Climatic Data Center^[21] (NCDC). The weather data downloaded from the NCDC site for the snow/ice storms for the past 5 years are given in Appendix C. Generally, a major snow storm would last about 3 days and is followed by colder temperature. The Roca Spur Bridge deicing system has performed satisfactorily under these adverse conditions. However, the applicability of the conductive concrete deicing technology has not been tested in regions with sustained low temperature during winter, such as Alaska, Canada and Northern Europe. The deicing performance of the Roca Spur Bridge is summarized in Table 10. The temperature and current readings acquired by the controller are in Excel spreadsheet format. A computer CD containing the Excel spreadsheets obtained during the winter storms of the past 5 years is attached to this report.

Table 10. Deicing Performance of Roca Spur Bridge

Storm Date	Snow depth (in.)	Air temp. (°F)	Wind speed (mph)	Energy (kW-hr)	Unit Cost (\$/ft²)	Power Density (W/ft²)
Dec 8-9, '03	6.5	20.7	16.2	2,023	0.050	40.04
Jan 25-26, '04	10.1	14.9	14.4	2,885	0.070	30.74
Feb 1-2, '04	5.7	14.4	11.1	2,700	0.066	26.57
Feb 4-6, '04	7.8	19.2	11.5	3,797	0.093	35.94
Jan 2-5, '05	8.5	15.6	14.3	3,128	0.076	33.01
Feb 6-8, '05	4.6	17.3	12.7	3,327	0.081	32.25
Mar 18-21, '06	9.9	32.5	16.2	2,786	0.068	29.97
Jan 13-14, '07	3.3	10.9	21.7	2,366	0.058	18.86
Jan 20-21, '07	6.0	19.4	17.4	2,573	0.063	30.19
Feb 12-13, '07	3.8	17.6	16.2	2,653	0.065	33.54
Mar 1-3, '07	7.1	29.8	19.9	2,893	0.071	36.79
Dec 5-7, '07	3.5	22.5	20.5	2,866	0.070	35.02
Jan 15-18, '08	3.8	18.1	24.8	2,445	0.059	34.56
Feb 4-7, '08	4.6	21.9	22.4	3,046	0.074	36.98

*Average ambient temperature readings during deicing at the bridge site.

**Energy cost: \$0.08/kW-hr.

5.3 Relationship between Electrical Conductivity and Temperature

The conductive concrete behaves like a semiconductor^[19]. When the applied voltage exceeds a threshold value, the conductive concrete becomes electrically conductive. The electrical conductivity of the conductive concrete is a function of the temperature. As the concrete temperature increases, the concrete becomes more electrically conductive. When the amount of current going through the concrete increases, the heating rate will increase and the concrete temperature rises. Thus, the electrical resistivity (or conductivity) of conductive concrete is temperature dependent.

Based on the current and temperature data acquired from the 52 slabs at the Roca Spur Bridge, a relationship between the averaged slab temperature and the averaged electrical current can be established, as shown in Fig. 12. Since the data have been collected over the past 5 years, the results also indicate that the long-term electrical conductivity of the conductive concrete has been very stable. A significant shift to the right of the curves would have indicated a decrease in electrical conductivity over time. The temperature readings from the 52 individual slabs have indicated uniform heating over the bridge deck. The average slab temperature was consistently about 18°F higher than the ambient temperature at any point in time during the storms. The energy consumption from powering the slabs simultaneously averaged about 3000 kW-hr with an associated unit cost of \$0.07/ft² per storm. The operating cost for the Roca Bridge deicing system would thus be about \$250 for each major storm.

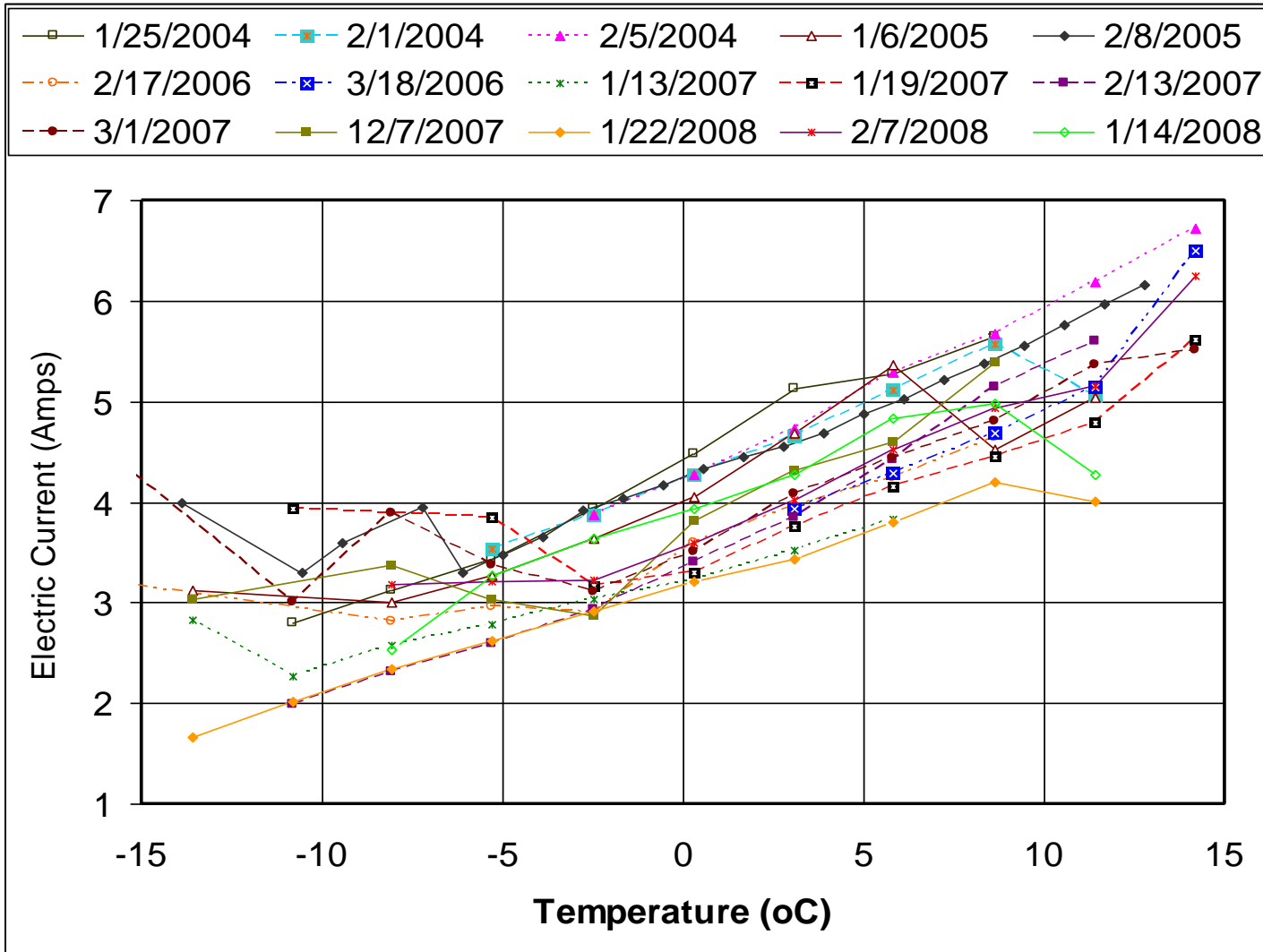


Figure 12. Average Slab Current vs. Slab Temperature Relationship

CHAPTER 6

LESSONS LEARNED

6.1 Electrical Wiring Scheme

During the December 9, 2003 snow storm, hot spots were reported at several locations along the centerline of the bridge deck (see Fig. 13). Engineers from Nebraska Department of Roads inspected the conductive concrete slabs after the storm and reported that there was tinkling sensation when touching the slab at one location, indicating potential electric shock hazard.



Figure 13. Hot spots along the Centerline of the Bridge Deck

The step potential and stray current levels were measured on December 12, 2003. All 52 slabs were powered at the time, and the temperature and current readings of the slabs were monitored on site with a laptop computer. The peak step potential measured across an 8-ft distance (i.e., two slabs widths) was 175 V, given that the applied voltage across the electrodes the same distance apart was 208 V. The maximum stray current level was about 0.6 A.

6.1.1 Diagnostics of stray current and remedy

An inspection of the current levels of the 52 slabs revealed that only slabs No. 20, 26, 42 and 44 had much higher values (11, 14, 15 and 18 Amps, respectively) while the rest of the slabs had current in the range of 4 to 5 Amps. These 4 slabs are exactly where the hot spots were reported. The small number of hot spots indicated the wiring of these slabs may be incorrect. It was suspected some adjacent electrodes (across the 6-in. gap along the centerline) had opposite polarities due to incorrect wiring. Water from melted snow filled voids under the polyurethane sealant at those 4 slabs and provided a path for stray current, thus explaining the high current readings. Steam was coming out of saw cut gaps with burning plastic smell, indicating high temperature due to electric current going through the water in saw cut gap.

The wiring of a three-phased, AC source is quite different from that of a two-phased power source. The wiring of the slabs was reconfigured such that the four electrodes located along a saw cut line will have the same voltage, thus completely eliminate any possible stray current path. There was no need to pull wires in the PVC conduits, except that power wiring connected to some slabs was simply switched at the control panel. The corrected wiring scheme is shown in Table 11. A series of tests was conducted on the electrical wiring of the “tagged-out” slabs on January 7, 2004. All 52 slabs were powered and the temperature and current readings of the slabs were monitored with a laptop computer. A digital current meter was used to measure the return current from each slab. A hand-held temperature gun was also used to monitor the temperature along the centerline of the bridge where hotspots had been observed. It was confirmed that the previous high current readings in slabs 20, 26, 42 and 44 were eliminated after reconfiguration of the wiring.

Table 11 Power Chord Wiring Reconfiguration

	Power Panel 1						Power Panel 2						Power Panel 3					
Phase	Circuit	New Slab	Old Slab	Circuit	New Slab	Old Slab	Circuit	New Slab	Old Slab	Circuit	New Slab	Old Slab	Circuit	New Slab	Old Slab	Circuit	New Slab	Old Slab
A	1	1	1	2	2	2	1	25	21	2	26	22	1	43	41	2	44	42
B	3	1	1	4	2	2	3	25	21	4	26	22	3	43	41	4	44	42
C	5	5	3	6	6	4	5	23	23	6	24	24	5	41	43	6	42	44
A	7	5	3	8	6	4	7	23	23	8	24	24	7	41	43	8	42	44
B	9	3	5	10	4	6	9	21	25	10	22	26	9	45	45	10	46	46
C	11	3	5	12	4	6	11	21	25	12	22	26	11	45	45	12	46	46
A	13	7	7	14	8	8	13	31	27	14	32	28	13	49	47	14	50	48
B	15	7	7	16	8	8	15	31	27	16	32	28	15	49	47	16	50	48
C	17	11	9	18	12	10	17	29	29	18	30	30	17	47	49	18	48	50
A	19	11	9	20	12	10	19	29	29	20	30	30	19	47	49	20	48	50
B	21	9	11	22	10	12	21	27	31	22	28	32	21	51	51	22	52	52
C	23	9	11	24	10	12	23	27	31	24	28	32	23	51	51	24	52	52
A	25	13	13	26	14	14	25	37	33	26	38	34	25			26		
B	27	13	13	28	14	14	27	37	33	28	38	34	27			28		
C	29	17	15	30	18	16	29	35	35	30	36	36	29			30		
A	31	17	15	32	18	16	31	35	35	32	36	36	31			32		
B	33	15	17	34	16	18	33	33	37	34	34	38	33			34		
C	35	15	17	36	16	18	35	33	37	36	34	38	35			36		
A	37	19	19	38	20	20	37	OPEN	39	38	OPEN	40	37			38		
B	39	19	19	40	20	20	39	39	39	40	40	40	39			40		
C	41			42			41	39		42	40		41			42		

The slabs that had been identified previously to have high levels of stray currents were rewired first according to the revised scheme. The surface step potentials and currents were then monitored along the bridge centerline after soaking it with more than 5 gallons of water. The measured peak voltage across a slab width was 172 V, and the measured peak surface current was 12 mA. This is a significant reduction from the previously measured current level that was as high as 0.6 A. No hot spots were observed with the surface temperature probe.

6.2 Concerns for Electric Shock

The use of high voltage and high current causes a safety concern, even though the conductive concrete behaves as a semi-conductor. A model commonly used to describe the behavior of a diode^[19] as a resistor in parallel with a variable resistor and a capacitor, may be used to describe the electrical conduction behavior of the conductive concrete. The isolated conductive particles within the concrete act as capacitors when a voltage is applied across the material. The current flows through the material due to dielectric breakdown. The summation of the potential drops of all the viable current paths between the two electrodes is equal to the applied voltage. Likewise, the total current going through all the viable paths is equal to the current corresponding to the applied voltage. This behavior has been confirmed by field measurements. Several measurements were taken at different locations on the inlay surface under 208 V during heating experiments, and “step potential” readings at 2 ft apart were in the range of 10 to 20 volts. The current readings were in the range of 15 to 30 mA. These voltage and current levels pose no hazard to the human body. On another occasion, the researchers touched the surface of a 4 ft by 12 ft conductive concrete slab containing steel fibers and shavings during deicing experiment without feeling any electric shock, while the slab was

energized with 410 V of AC power and had about 10 Amps of current going through it. Although the power will be turned on only when snow/ice storms are anticipated, it may be prudent to check the step potential and stray current whenever the power is turned on to ascertain that there is no electric shock hazard to the public. There are effective ways to eliminate the potential stray current and the associated electric shock hazard.

6.2.1 Applying Epoxy Coating

An effective measure to eliminate potential stray current on the surface is to apply 1/16 to 1/8 in. coating of a low-modulus and low-viscosity epoxy on the conductive concrete surface. Nebraska 47B sand and gravel or fine aggregate will then be spread on before the epoxy sets to form a skid-resistant surface. The centerline of the Roca Spur Bridge deck was coated with two layers of Unitex Pro-poxy Type III DOT epoxy on July 23, 2003. Fig. 14 shows the application of epoxy coating along the centerline of Roca Spur Bridge. The two-part epoxy material was donated by Unitex.



Figure 14. Application of Epoxy Coating and utility sand

6.2.2 Adding a Regular Concrete Layer

Regular concrete is not electrically conductive. Using a thin layer of regular concrete on top of a conductive concrete pavement can be an effective way to minimize stray current. Heating tests showed that a 0.25 to 0.5-in. thick topping would only reduce the heating rate slightly. Silica fume should be added to make the regular concrete topping less permeable.

6.2.2.1 Effect on Heating Rate

Regular concrete toppings of 0.25 in., 0.50 in. and 0.75 in. were added to 1 ft by 1 ft by 2 in. conductive concrete test slabs for heating tests in a freezer. A conductive concrete test slab without a regular concrete topping was used for reference. The effect of adding a regular concrete topping on the heating rates is illustrated in Fig. 15. It can be seen that adding a regular

concrete topping of 0.25 to 0.50 in. will have about the same heating rate, with 6% reduction in 2 hours compared to having no topping.

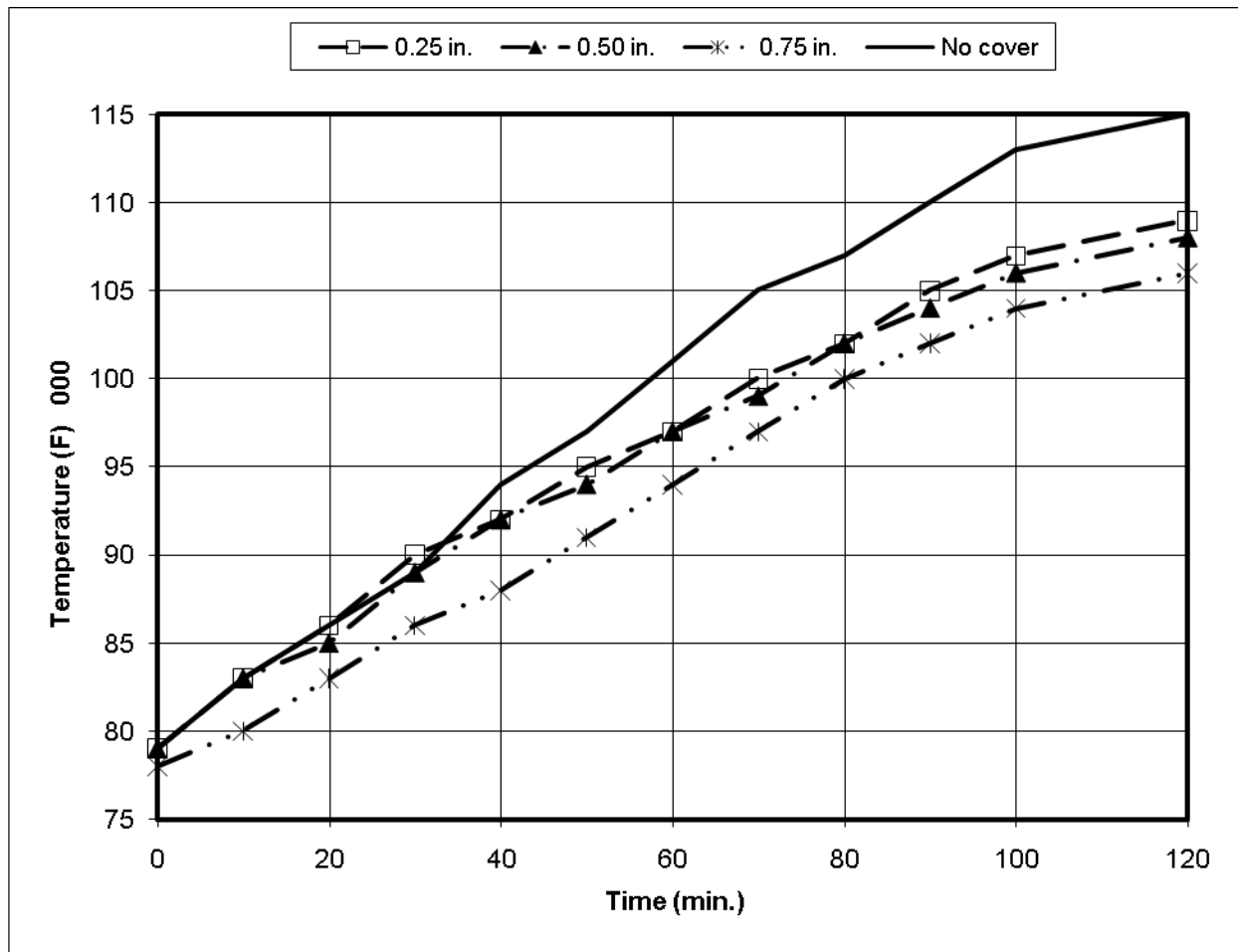


Figure 15. Effects of Concrete Cover on Heating Rate

6.2.2.2 Effect on Stray Current

The effect of adding a 0.25 in. regular concrete topping to reduce the electrical stray current on the test slabs was also evaluated. Measurements of stray currents on the slab surfaces were taken under both dry and soaked conditions. Under soaked condition, a test slab was

submerged in water for one hour before testing. Fig. 16 shows a conductive concrete test slab with 0.25 in. concrete topping under soaking.

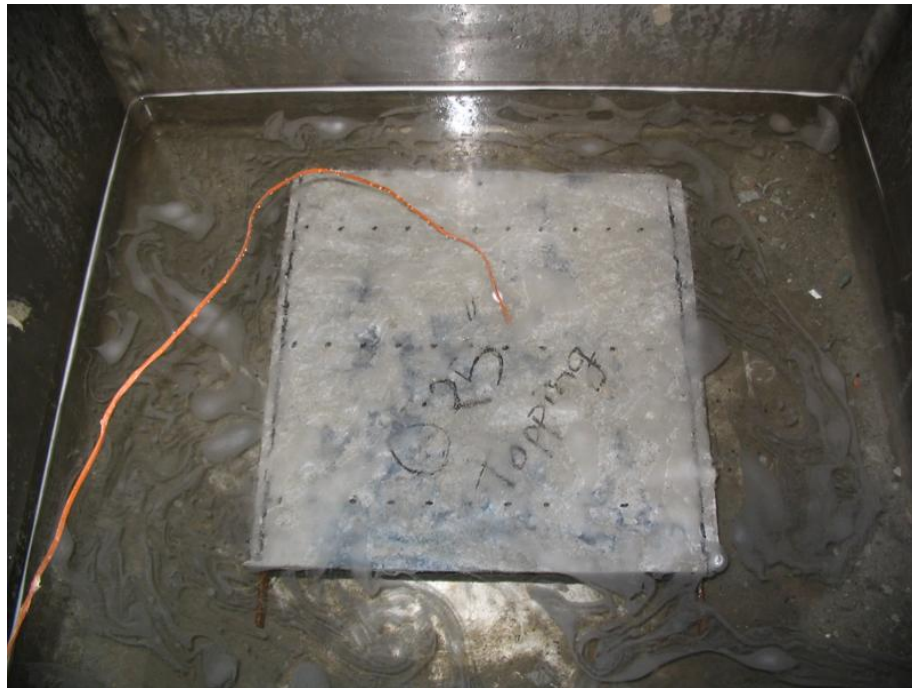


Figure 16. Conductive concrete test slab submerged in water

Before stray current measurements, the excess water on the surface was wiped off and pieces of wet paper towel were used to ensure good contact of the probes with the slab surface. The stray currents were then measured with a multimeter and recorded as a function of the distance between the two probes, as shown in Fig. 17. The effectiveness of adding a 0.25 in. concrete topping for minimizing stray current is presented in Fig. 18. The reduction from 0.6 mA to 0.15 mA for the soaked test slabs is very significant.

Step potential and stray current levels at the Roca Bridge deck were monitored during the fall when the bridge was powered up. Measurements were either taken after a rain storm or gallons of water were poured on the deck to simulate wet pavement. On the average, the peak step potential measured at the electrode locations (8 ft apart) was about 172 V with peak stray

current of about 12 mA. Even though the Roca Bridge deck does not have a regular concrete topping, there is no electric shock hazard when the conductive concrete is energized. No injuries of people or small animals attributable to the conductive concrete deck have been reported for the past 5 years.

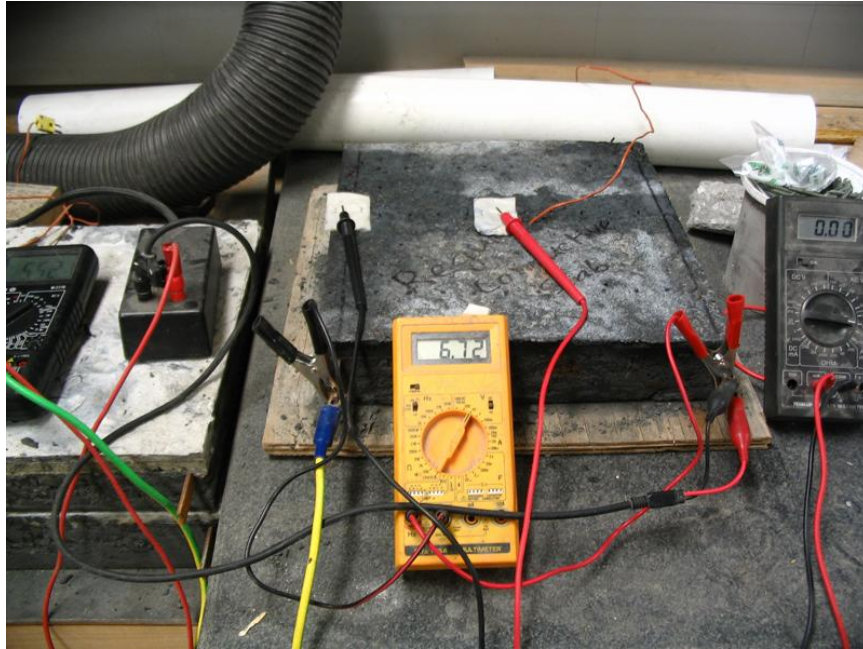


Figure 17. Stray Current Measurements

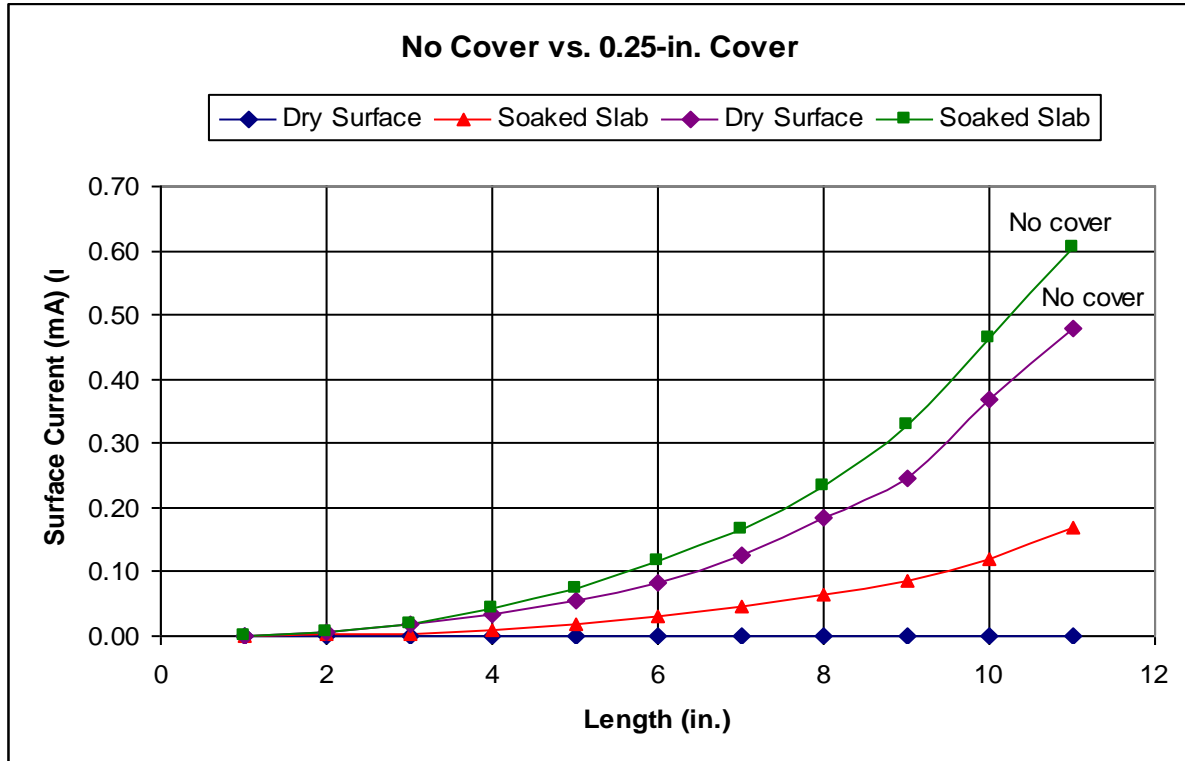


Figure 18. Reduction of Stray Current by adding a 0.25 in. topping

6.3 Bridge Smoothness Tests and Surface Grinding

Shortly after Roca Bridge was open to traffic in December 2002, the bridge pavement was considered too bumpy for a ride at the speed limit of 35 mph. Nebraska Department of Roads ran a profilometer to determine the surface roughness, and rough spots were milled. As a result, portions of cement paste cover on top of the conductive concrete deck were ground off and some steel fibers were exposed. The profilograph showed excessive milling especially in the eastbound lane, when comparing the surface roughness results before and after surface grinding.

6.4 Bridge Deck Inspections

The bridge deck was routinely inspected once in the fall before the winter season and once in mid-summer each year. The cracks, if any, would be sealed using epoxy before deicing operation. On October 24, 2003, Roca Bridge was inspected for cracks and none were found. The bridge deck was saturated with water by a water tanker. No short circuits were detected. Roca Bridge was inspected on April 15, 2004 after four successful deicing operations during the 2003 winter storms. No cracks in the slabs were visible by the naked eye. The Roca bridge deck was inspected for cracks on November 18, 2004. No visible cracks or severe rusting were observed. The power relays were turned on manually for selected panels to check surface stray current. The measured current level was about 0.3~0.4 mA, which posed no shock hazard.

An inspection of the Roca Bridge deck was conducted on May 19, 2006. Several areas of surface spalls were noticed. The spalls in the eastbound lane were severe compared to the westbound lane. The spalls were probably caused by a combination of using deicing salt and snow plows. NDOR maintenance crew was asked not to spray salt on bridge, since NDOR maintained the bridge approach leading to Roca. It was suspected that deicing salt was tracked on the bridge in the eastbound lane by the traffic. The epoxy coating along the centerline of the bridge deck also showed chips and cracks, possibly by snow plows during snow removal. NDOR engineers independently inspected the bridge deck on June 16, 2005, and the exposed steel fibers were found significantly rusted and many spalls in the conductive concrete deck became visible, as shown in Figs. 19 and 20. The rust from steel fibers was suspected to cause delamination and concrete spalls. It was also noted the epoxy coating along the centerline of the bridge deck was chipped or damaged (see Fig. 21).



Figure 19. Cement paste cover was milled off leaving steel fibers exposed



Figure 20. Close-up of exposed steel fibers and spalls

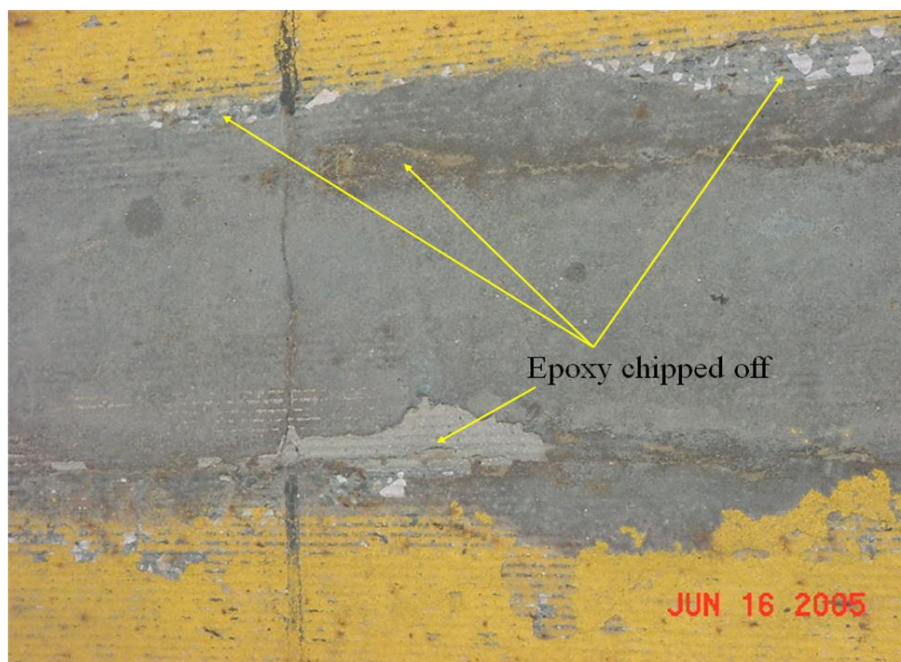


Figure 21. Damage to the Epoxy Coating along Bridge Centerline

6.4.1 Mapping of Spalls

Slabs 1, 12, 14, 16, 18, 23, 24, 26, 28, 30, 34, 38, 40, 42, 44, 46, 47, 48, 50 and 52 had most significant spalls. All the even-numbered slabs are in the eastbound lane (south side) of the bridge, where the surface was milled to a much greater extent than the westbound lane (north side). Slabs 16, 28, 30 and 46 had the worst deterioration in terms of the numbers and sizes of spalls. The sizes and shapes of the spalls were traced onto transparencies on July 15, 2005, for future reference.

6.4.2 Samples Coring and Locations

Nebraska Department of Roads engineers cored samples from the conductive concrete deck to investigate the deterioration. The locations of the cored samples are marked in Fig. 22.

Core Locations

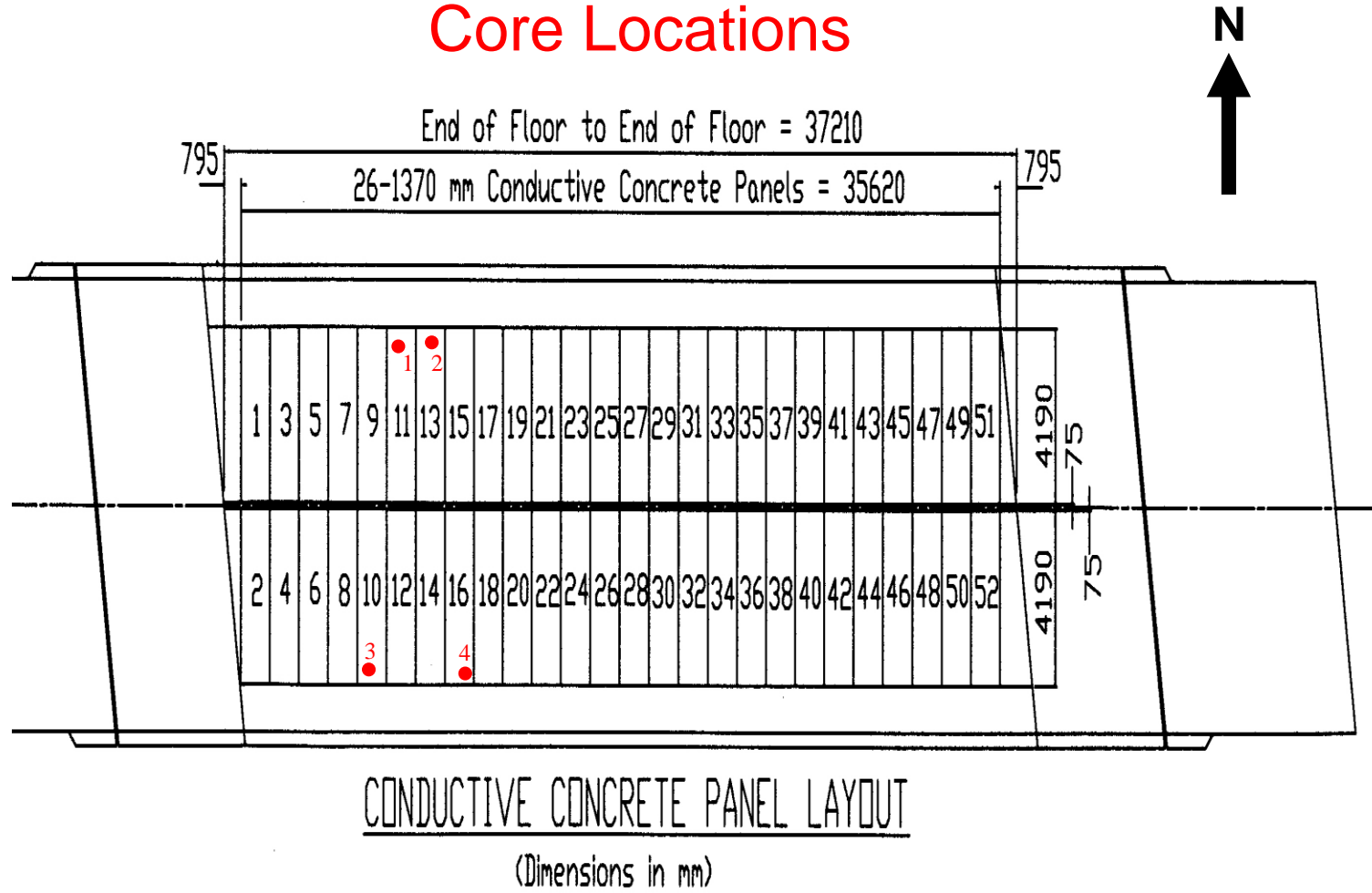


Figure 22. Locations of Cored Samples

The cored samples were inspected by the Nebraska Department of Roads engineers and found the rust of the steel fibers was limited to less than 1/16 in. of the top layer of the bridge deck. Fig. 23 shows the cored samples. It was concluded that the conductive concrete mix was sound and had adequate freeze-thaw resistance. The concrete spalls and extensive steel fiber rusting were most likely due to excessive surface milling. It was also noted that the westbound lane (north side) did not have noticeable amount of spalls as did the eastbound lane.



Figure 23. Cored Samples from Roca Bridge Deck

6.4.3 Epoxy Patching

On Oct 17, 2005, the damaged epoxy coating along the centerline of the bridge deck was removed by two passes of bead/shot blasting conducted by Trafcon, Inc., Lincoln, Nebraska. The centerline was recoated with the Unitex Pro-poxy Type III DOT epoxy and fine sand afterwards. The spalled areas in pavement were also patched with the same epoxy and fine sand. The bead blasting cost \$250 and the epoxy material cost \$220.80, with a total maintenance cost of \$470.80 incurred during 2 years of service.

6.4.4 Further Inspections

The bridge deck was further inspected on September 27, 2006 and July 17, 2007. No further deterioration was observed after the spalls were patched with epoxy. However, during a post-project inspection on June 16, 2008, significant deterioration in many even-numbered slabs (i.e., eastbound lane) was noticeable, as shown in Fig. 24.



Figure 24. Deterioration of Eastbound Lane Slabs

A close-up of the surface spalls on slabs 28 and 30 is shown in Fig. 25. The rust condition of the exposed steel fibers also worsened significantly. It was surprising to see the rapid deterioration that took place in one year. It is surmised that most spalls occurred during thawing in the late March-early April timeframe. There were 25 days below freezing during January and February 2008, so the freeze-thaw action was severe this winter.



Figure 25. Close-up of Surface Spalls in Eastbound Lane

On the other hand, the westbound lane was also closely scrutinized and there was hardly any noticeable deterioration since the surface grinding. The exposed steel fibers in the odd-number slabs (i.e., westbound lane) did not show deterioration, as evidenced in Fig. 26. It is evident that the surface milling really did a lot of damage to the eastbound lane when compared the progress of the deterioration against that in the westbound lane. The excessive milling has compromised the durability of the conductive concrete deck.



Figure 26. No Noticeable Deterioration in Westbound Lane Slabs

6.5 Public Awareness

Current operation of the Roca Bridge deicing system relies on a manual switch to turn the power on/off via a phone modem and on weather forecast to determine the probability of icing. The power to the bridge will be turned on if the probability is deemed high. The effectiveness of this system is seriously limited by manual operation, since the personnel may not always be available to turn the power on and the weather forecast may not always provide accurate weather information at the bridge site. Therefore, local residents driving over the Roca Spur Bridge should be aware that the bridge may still be icy. A kiosk may be used to inform the drivers if the bridge is powered.

CHAPTER 7

CONCLUSIONS AND RECOMMENDATIONS

7.1 Conclusions

- The Roca Bridge deicing system using an implemented conductive concrete deck has been functional for the past 5 years (2003-2008). Data recorded from 15 major winter storms has indicated excellent deicing performance with no signs of deterioration.
- The conductive concrete technology is very energy-efficient when used against freezing rain, since the air temp usually is close to the freezing point (see Fig. 27).

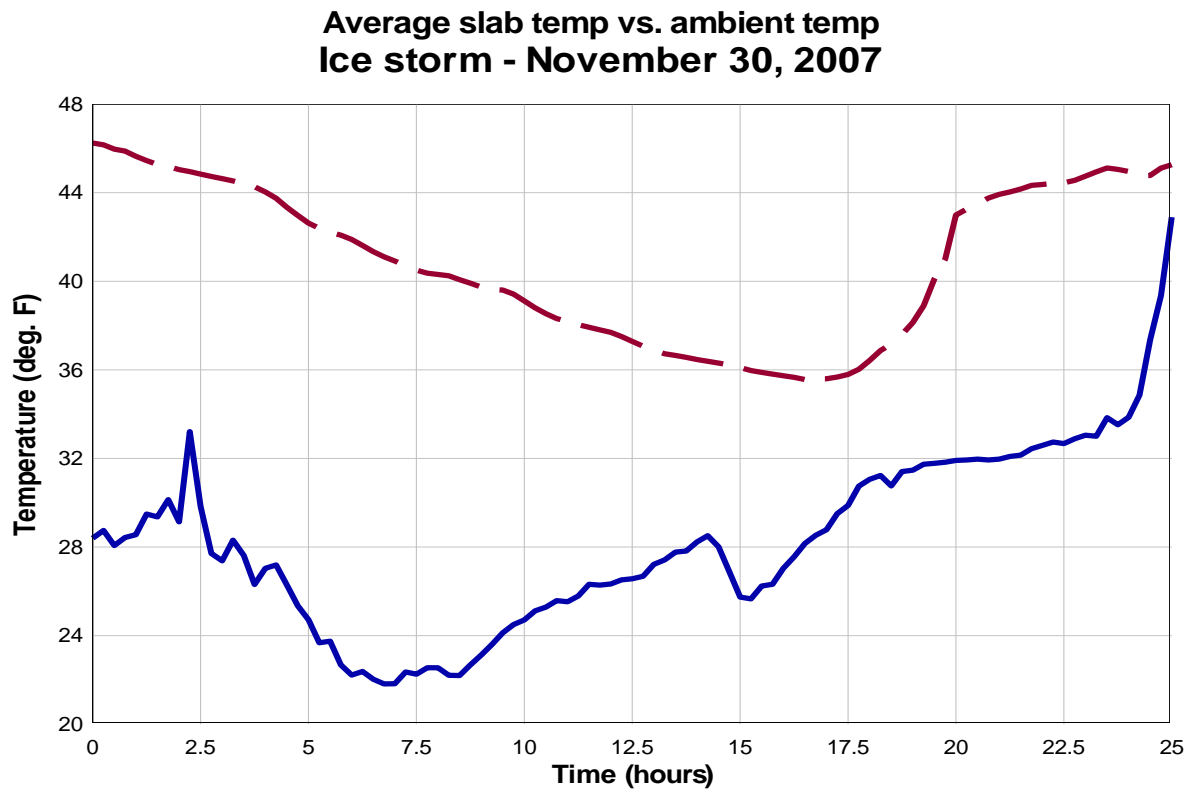


Figure 27. Deicing Performance in an Ice Storm – November 30, 2007

- Due to the use of steel fibers in the conductive concrete mix design, concrete cover is essential for durability of a bridge deck made of conductive concrete.

- The deck surface inspections should be made in the fall before the system is powered and soon after the winter is over. The spring inspection should be conducted preferably in late March or early April.
- The electrical conductivity of the conductive concrete has been very stable over a 5-year period, as evidenced by Fig. 12. The most challenging task in the mix design was to achieve the long-term stability of the electrical conductivity.
- The operating cost of the Roca Bridge deicing system was about \$250 per major snow storm. Comparisons of conductive concrete technology against other deicing technologies are provided in Table 9.
- Using a 1/16-in. epoxy or a 0.25 in. regular concrete topping on a conductive concrete deck can significantly reduce the electric shock potential without compromising heating rate.
- The success of the Roca Bridge demonstration project has attracted much attention from the transportation industry and researchers from all over the world. The project has been featured in numerous national as well as international news media and publications, including the **Discovery Channel**. The heated deck has worked very well for the past 5 winter seasons, as evidenced by Fig. 28.



Figure 28. Roca Spur Bridge Deicing Operation

- The conductive concrete deicing technology is readily deployable at any accident-prone roadways, bridge decks and interstate exit ramps.

7.2 Recommendations for Future Research

7.2.1 Automation of the Deicing System

Current operation of the deicing system relies on a manual switch to turn the power on/off using a phone modem. Icing sensors and a weather station may be integrated into the control circuitry to fully automate the system. It has long been recognized that icing on the deck may take place in early mornings under freezing temperature. Since it is more energy efficient to preheat the conductive concrete before an icing occurrence, a weather monitoring system could be developed to automatically control the power delivered to the bridge deck based on local and regional weather forecast. Energy consumption costs due to “false alarm” as well as undetected icing events would be greatly reduced.

7.2.2 Adjustable Power Source

The combination of low temperature, high wind and heavy snow rate (e.g., 1~2 in./hr), usually caused the pavement to be covered by snow and ice. This is due to the fact that heat generated in conductive concrete is slower than the heat dissipation from the bridge deck surface. Therefore, it is desirable to have an adjustable transformer to increase electric current under a higher applied voltage.

7.2.3 Implementation Plan

This project provided an opportunity for Nebraska Department of Roads and University of Nebraska-Lincoln to jointly monitor the operations of this new technology. There were many

valuable lessons learned throughout the life of this project which will enhance future applications of the technology. The Nebraska Department of Roads will continue to monitor the condition of the deck surface in Roca and conduct maintenance as needed. At this time, there are no plans to duplicate the conductive concrete system which was implemented in Roca, on the state highway system.

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Appendix A – Construction Drawing

- ROCA SPUR -

- NOTES -

This structure is designed in accordance with the 16th edition of the AASHTO "Standard Specifications for Highway Bridges".

The superstructure of this bridge is designed by load factor design method. The structure is designed for a future wearing surface of 900 Pa.

The contractor may substitute any one of the alternate designs shown on the plans for the original design. All quantities are based on the original design and no additions or deductions will be allowed for the use of an alternate design.

Concrete for slabs, approach slabs and rails shall be Class "47B", with a 28-day strength of 30 MPa.

All other cast-in-place concrete shall be Class "47B" concrete, with a 28-day strength of 20 MPa.

All reinforcing steel shall be epoxy coated and conform to the requirements of ASTM A615/A615M, Grade 420 steel.

The minimum clearances, measured from the face of the concrete of any reinforcing bar, shall be 80 mm, except where otherwise noted.

All structural steel shall conform to the requirements of ASTM A709/A709M, Grade 250.

The items, "STRUCTURAL STEEL FOR SUBSTRUCTURE", shall include nose angles at the bents.

All dimensions shown are in horizontal plane only. No allowance have been made for vertical curve or roadway cross slopes.

All tele-communications shall furnish all conduit and hardware for the telephone attachments; and coordinate the installation with the contractor. The cost of installation shall be subsidiary to the item CLASS 47B-30 CONCRETE FOR BRIDGES. When the materials furnished by the utility are required, the contractor shall notify the utility company at least 72 hours in advance. Contact: Mr. Bruce Wood at 402-436-5944.

The cost of furnishing and installing all items related to the installation and operation of the conductive concrete deck surface, including, but not limited to, conduits, junction boxes, electrodes, FRP reinforcement, epoxy adhesive, temperature sensors, wiring and data cables, will not be paid for directly, but will be considered subsidiary to the item "CONDUCTIVE CONCRETE".

The cost for furnishing and installing the concrete pad for the Conductive Concrete equipment building, non-shrink grout, and saw cuts and saw cut sealant in the Conductive Concrete, will not be paid for directly, but will be considered subsidiary to the item "PLACING, FINISHING, AND CURING CONDUCTIVE CONCRETE".

The non-shrink grout shall be from the Approved Product List, conforming to the requirements of ASTM C1107.

- QUANTITIES -

ABUTMENT NO. 1 EXCAVATION _____		/ Lump Sum
BENT NO. 1 EXCAVATION _____		/ Lump Sum
BENT NO. 2 EXCAVATION _____		/ Lump Sum
ABUTMENT NO. 2 EXCAVATION _____		/ Lump Sum
CLASS 47B-30 CONCRETE FOR BRIDGES _____	139.0 m ³	
ABUTMENTS _____	45.0 m ³	
BENTS _____	94.0 m ³	
CLASS 47B-30 CONCRETE FOR BRIDGES _____	176.6 m ³	
SLAB _____	167.0 m ³	
CONCRETE RAILS _____	12.6 m ³	
EPOXY COATED REINFORCING STEEL _____	35215 kg	
SLAB _____	26130 kg	
CONCRETE RAILS _____	1577 kg	
ABUTMENTS _____	3230 kg	
BENT _____	4278 kg	
STRUCTURAL STEEL FOR SUBSTRUCTURE _____	490 kg	
STEEL SHEET PILING _____	243.3 m ²	
HP 250mm x 62kg STEEL PILING _____	274.0 m	
GRANULAR BACKFILL _____	94.0 m ³	
CONCRETE FOR PAVEMENT APPROACHES CLASS 47B-30 _____	126.2 m ³	
SLAB _____	119.2 m ³	
CONCRETE RAILS _____	7.0 m ³	
EPOXY COATED REINFORCING STEEL FOR PAVEMENT APPROACHES _____	4022 kg	
SLAB _____	7664 kg	
CONCRETE RAILS _____	1320 kg	
DRILLED SHAFT _____	39.2 m	
ROCK SOCKET _____	19.3 m	
CONDUCTIVE CONCRETE _____	31.2 m ³	
PLACING, FINISHING, AND CURING CONDUCTIVE CONCRETE _____	311.8 m ³	

- INDEX -

GENERAL NOTES, QUANTITIES AND INDEX _____	1
GENERAL PLAN AND ELEVATION _____	2
GEOLOGICAL PROFILE AND PILE LAYOUT _____	3
ROCK SOCKET FOUNDATION, DETAIL, AND NOTES _____	4
PLAN AND ELEVATION OF ABUTMENT _____	5
ABUTMENT DETAILS AND BILL OF BARS _____	6
BENT DETAILS AND BILL OF BARS _____	7
SLAB REINFORCEMENT LAYOUT & SECTION _____	8
CONCRETE RAIL ON BRIDGE _____	9
CROSS SECTION OF ROADWAY AND BILL OF BARS _____	10
CONDUCTIVE CONCRETE PANEL LAYOUT & MISCELLANEOUS DETAILS _____	11
CONDUCTIVE CONCRETE PANEL DETAILS _____	12
APPROACH SLAB _____	13
RAIL ON APPROACH SLAB _____	14
BILL OF BARS - APPROACH SLAB _____	15


-BILL OF BARS INDEX-

ABUTMENT BILL OF BARS _____	6
BENT BILL OF BARS _____	7
SLAB BILL OF BARS _____	10
APPROACH SLAB WITH CONCRETE RAIL BILL OF BARS _____	13

SS55F(102)
CONTRACT NUMBER

17853
PROJECT NUMBER

SS55F00229



BRIDGE NUMBER

36.6 m THREE SPAN CONCRETE SLAB BRIDGE

GENERAL NOTES, QUANTITIES AND INDEX


DESIGNED BY: J.H. CHECKED BY: J.L. DATE: JUNE 2001


COUNTY: DECATUR ROADWAY: 40.8 m DESIGN DATE: 4/12/01

SECTION: 140.8 m DESIGN DATE: 4/12/01

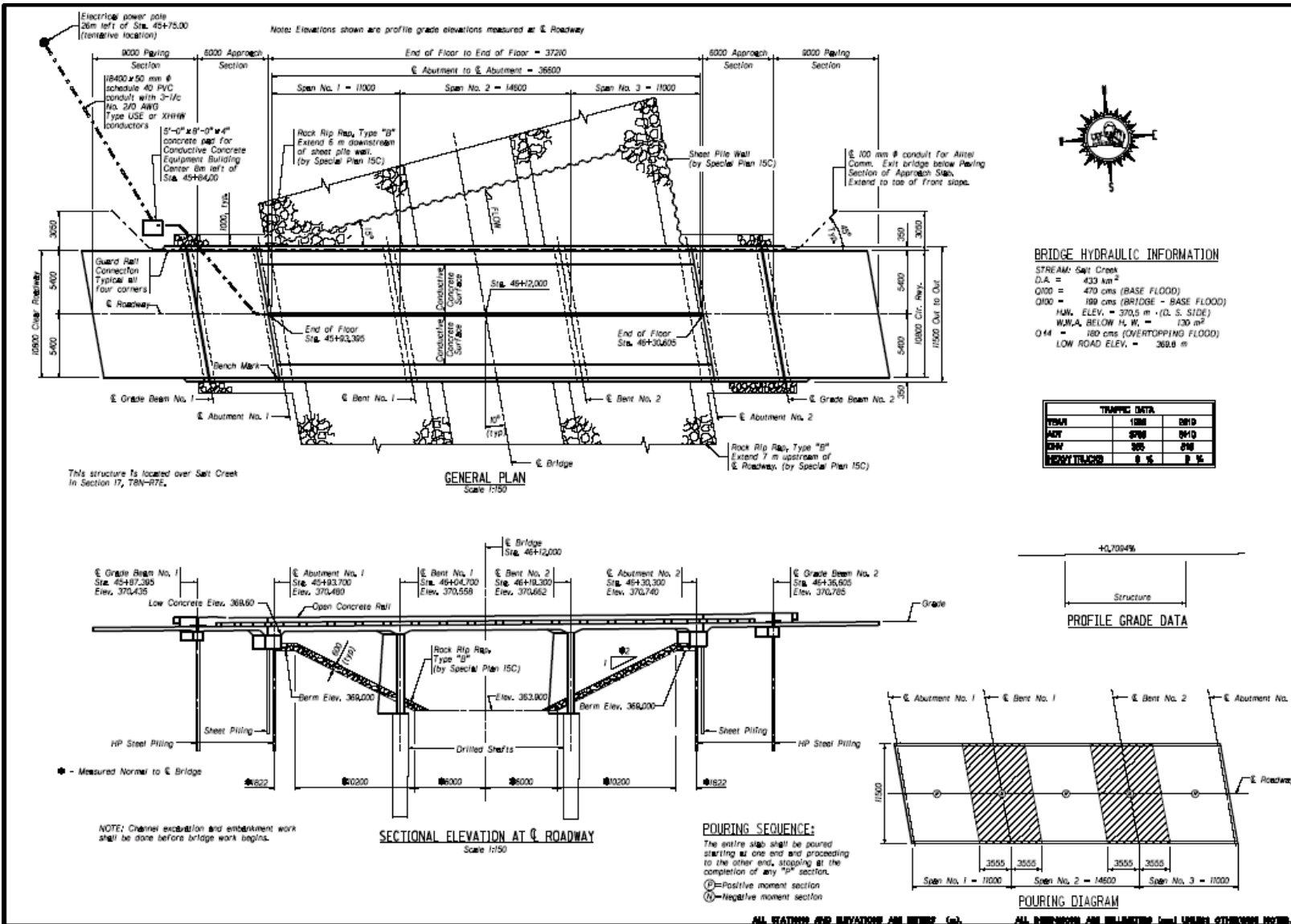
DESIGNED BY: J.H.

STATE OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION





SPECIAL PRICE 1/15



SS55F(102)
17803
SS55F00229

STATE OF NEBRASKA
DEPARTMENT OF ROADS - BRIDGE DIVISION

36.6 m THREE SPAN CONCRETE SLAB BRIDGE

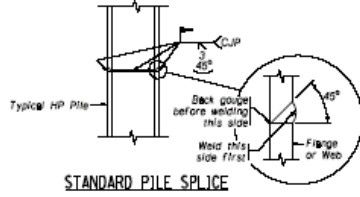
LOCATION: ROAD 400P
SEEK 40P L&B
ROADWAY 10.6 m
DESIGN LIVE LOAD MS18
DESIGNED BY T.H. DATE: JUNE 2001

COUNTY: LINCOLN
DIST. NO. 5555
REF. POINT: 2-29
STA. 46+12

DESIGNED BY T.H.

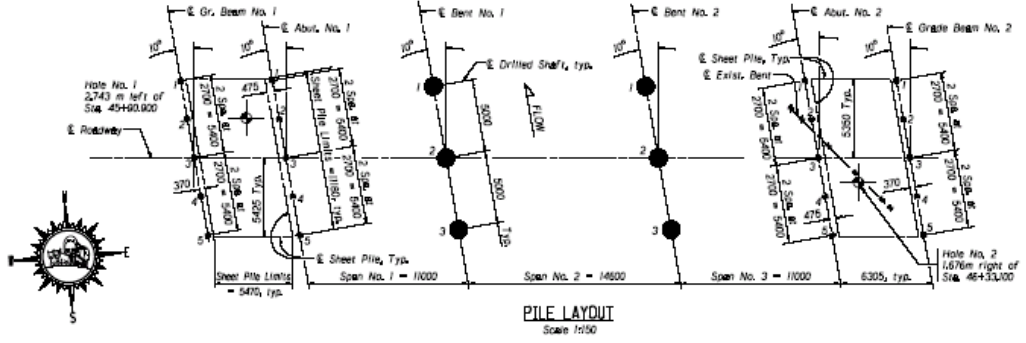
NOBILIT

2
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STANDARD PILE SPLICE

ⓐ Approvals location of existing abutment; location of piles is not known. Field verify existing pile locations. Adjust new piles for proper clearance after approval of Bridge Engineer.

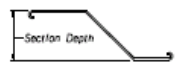


FILE DATA						
LOCATION	PILE NUMBER	OUT-OFF ELEVATION	MINIMUM PENETRATION BELOW CUT-OFF (mm)	PILE CORNER LENGTH (mm)	DESIGN PILE BEARING (kN/PILE)	PILE TYPE
Grade Beam No. 1	1 - 5	368540	110	13,2	400	HP258 x 62
Abutment No. 1	1 - 5	368300	110	13,7	584	HP258 x 62
Abutment No. 2	1 - 5	368560	12,5	15,2	584	HP258 x 62
Grade Beam No. 2	1 - 5	368890	12,5	13,7	400	HP258 x 62

Bents are designed for scour to elevation 361,0 m.

All steel sheet piling shall conform to ASTM A328 steel and meet the following minimum requirements:

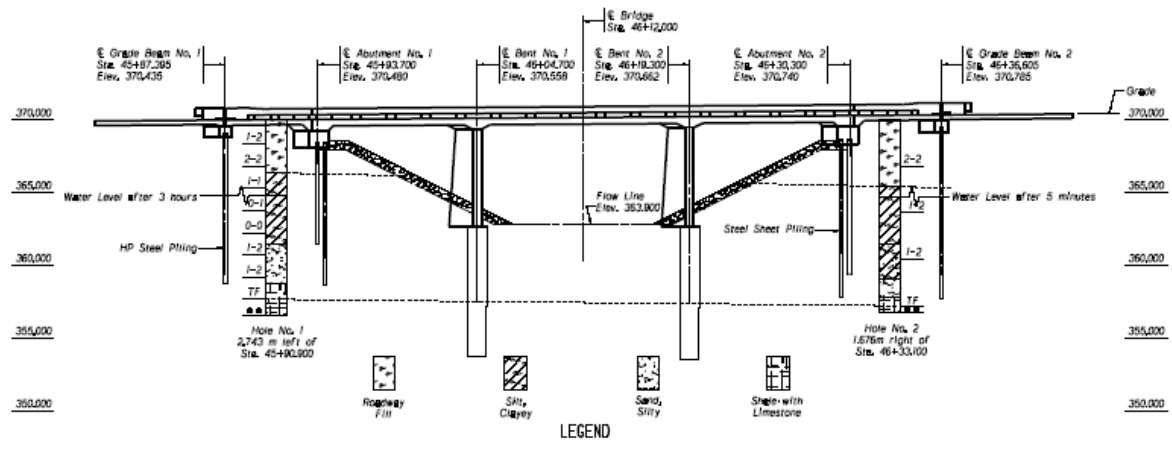
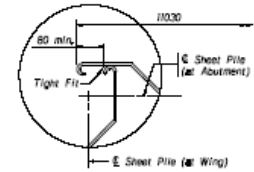
- Section length: 5,2 m
- Minimum section depth: 250 mm
- Minimum section thickness: 6 mm
- Section modulus: 297 x 10³ mm³/m



The contractor shall submit for approval a shop plan of the sheet pile layout showing all pertinent dimensions, details and section properties.

The pay quantity will be based on the sheet pile wall dimensions shown. The constructed wall length will be within ±500 mm of the sheet pile wall dimensions shown.

Prefabricated cast steel points will be required on all HP pile in this structure in accordance with the 1007 NDR Standard Specifications, Division 703. Approved manufacturers of prefabricated pile points are shown on the NDR Approved Products List.



GEOLOGICAL NOTES

The borings, as logged on the plans, represent the character of the subsol at the location indicated. No guarantee is made that the subsol conditions vary uniformly between or outside the given location.

Figures beside the column of borings indicate the number of blows required to drive a standard penetrometer, of 50 mm G, D, the second and third 150 mm using a 63,5 kg mass falling 760 mm, in accordance with A.S.T.M. D1586 procedures.

STATE OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION

LOCATION: 36.6 m THREE SPAN CONCRETE SLAB BRIDGE

COUNTY: LINCOLN

PROJECT NO.: S555

DESIGN DATE: 12-20

DESIGNED BY: J.H.

CHECKED BY: J.H.

DATE: June 2021

DESIGN LIVE LOAD: MS18

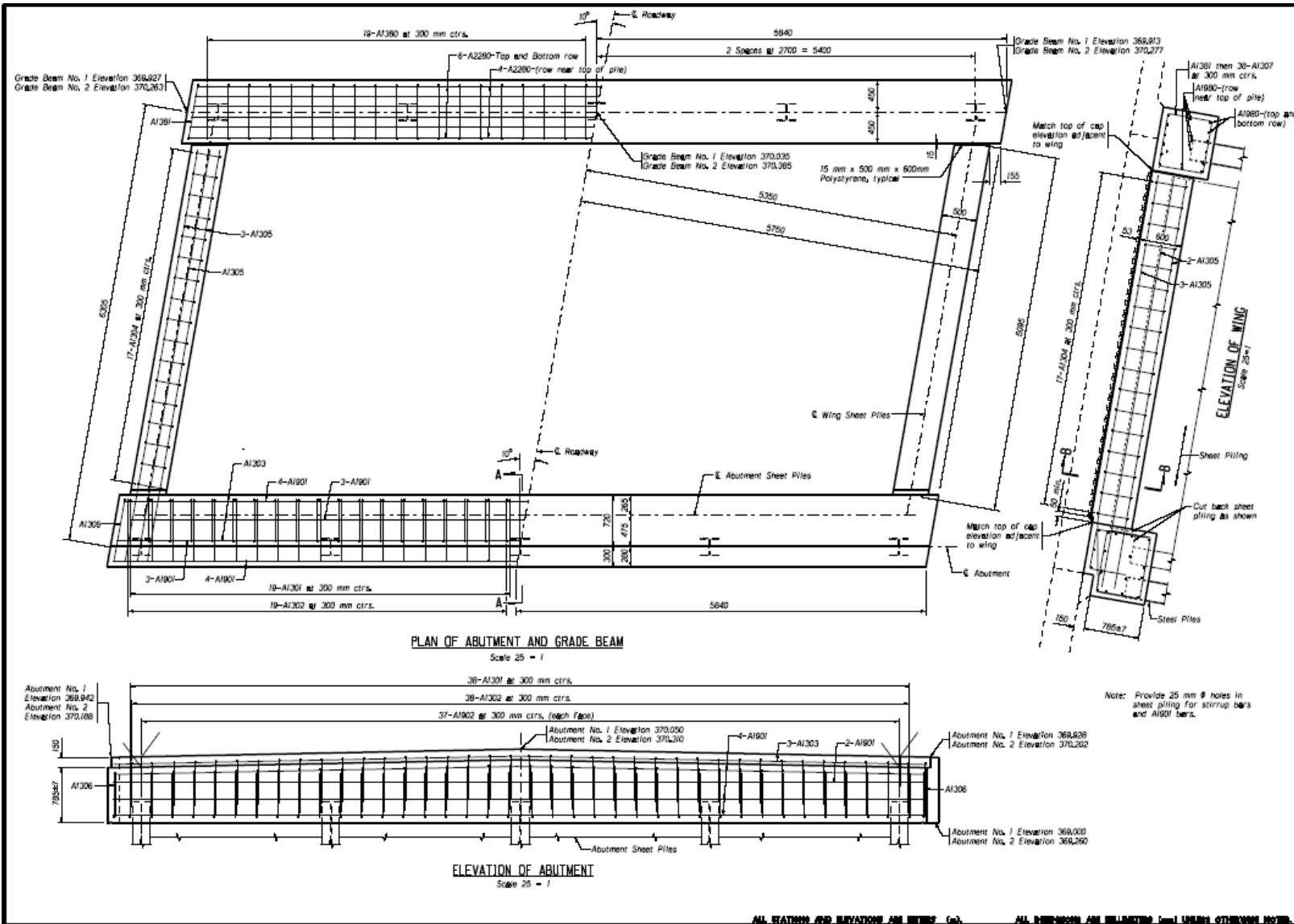
GEOLOGICAL PROFILE AND PILE LAYOUT

SS55F(102)

17803

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SS55F(102)
11853
SS55P00229

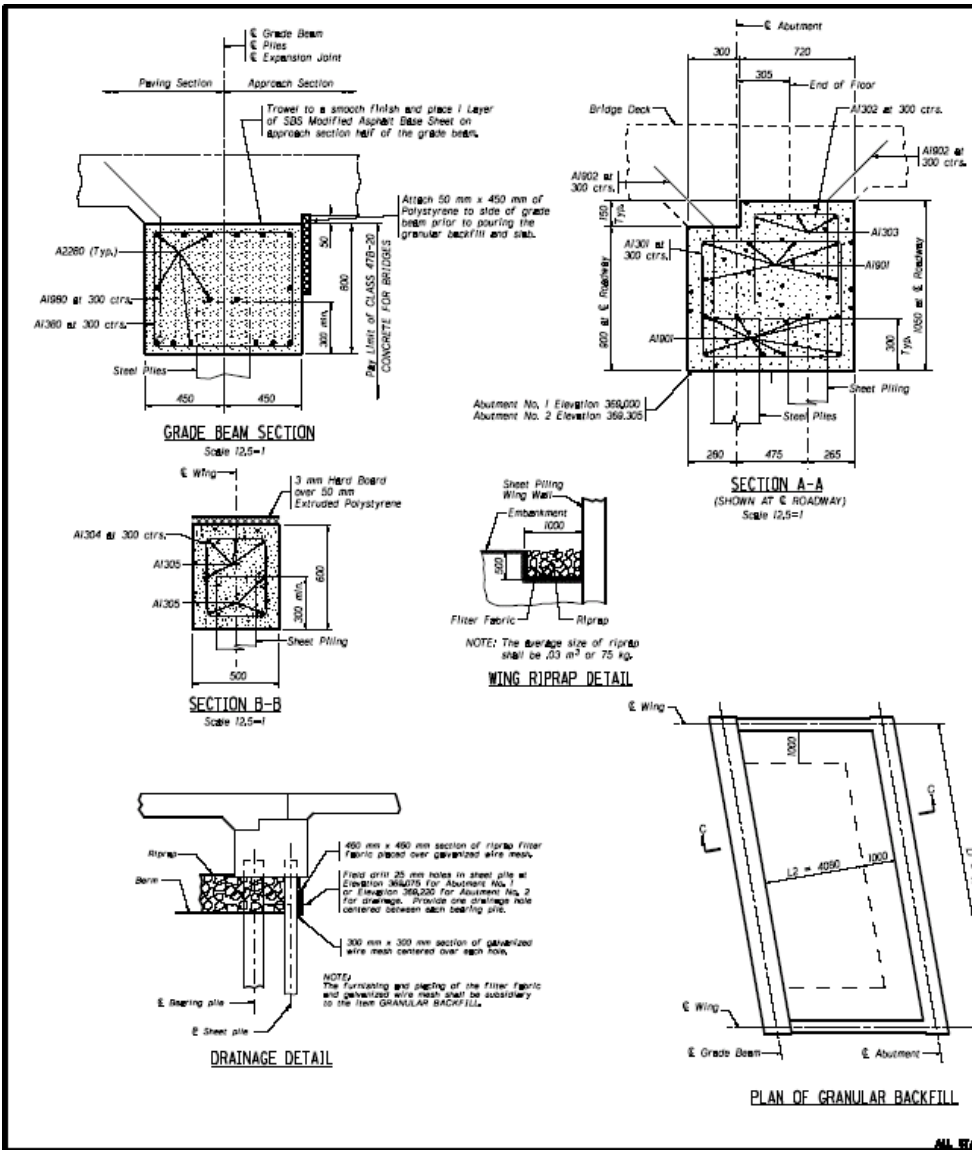
STATE OF NEBRASKA
DEPARTMENT OF ROADS - BRIDGE DIVISION

36.6 m THREE SPAN CONCRETE SLAB BRIDGE
ABUTMENT PLAN AND ELEVATIONS
DATE: JUNE 2001
CHECKED BY: F.J.

LACROIX Rock spur
NEW 10' LHB
ROADWAY 10.8 m
MINOR LANE LOAD 4/MSB
DESIGNED BY: CRP
DATE: JUNE 2001

STATE OF NEBRASKA
DEPARTMENT OF ROADS - BRIDGE DIVISION

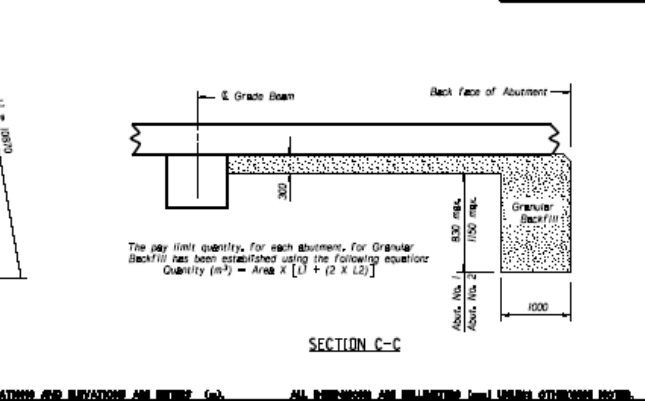
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15



BILL OF BARS

MARK	NO.	LENGTH	TYPE	"A"	"B"	"C"	"D"	"E"	"F"	PIN	HOOK	kg	MSS
A2880	16	11510	STR.									560	SS556F(102)
A1901	14	11510	STR.									360	11853
A1802	74	730	106	360	360	255				115		119	SS556F00229
A1890	87	680	106	360	300	233				115		57	
A1901	88	4160	106	620	660	600	480	m/n.		58		187	
A1802	88	1560	100	510	500	510				58		60	
A1803	3	11510	STR.									34	
A1804	34	1760	107	440	340					58	115	60	
A1805	14	5950	STR.									83	
A1806	2	3210	107	620	670					58	115	6	
A1880	38	2980	107	640	740					58	115	113	
A1881	2	3010	107	640	750					58	115	6	
SUBTOTAL = 1875												kg	
TOTAL = 3230												kg	

NOTE: FOR PIN DIAMETERS, HOOK LENGTHS, AND BENDING DIAGRAMS, SEE SHEET 15 OF 15.



STATE OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION

DESIGNED BY CRP
CHECKED BY E.J.
DATE: June 2001

36.6 m THREE SPAN CONCRETE SLAB BRIDGE
ABUTMENT SECTIONS, BILL OF BARS
AND GRANULAR BACKFILL DETAILS

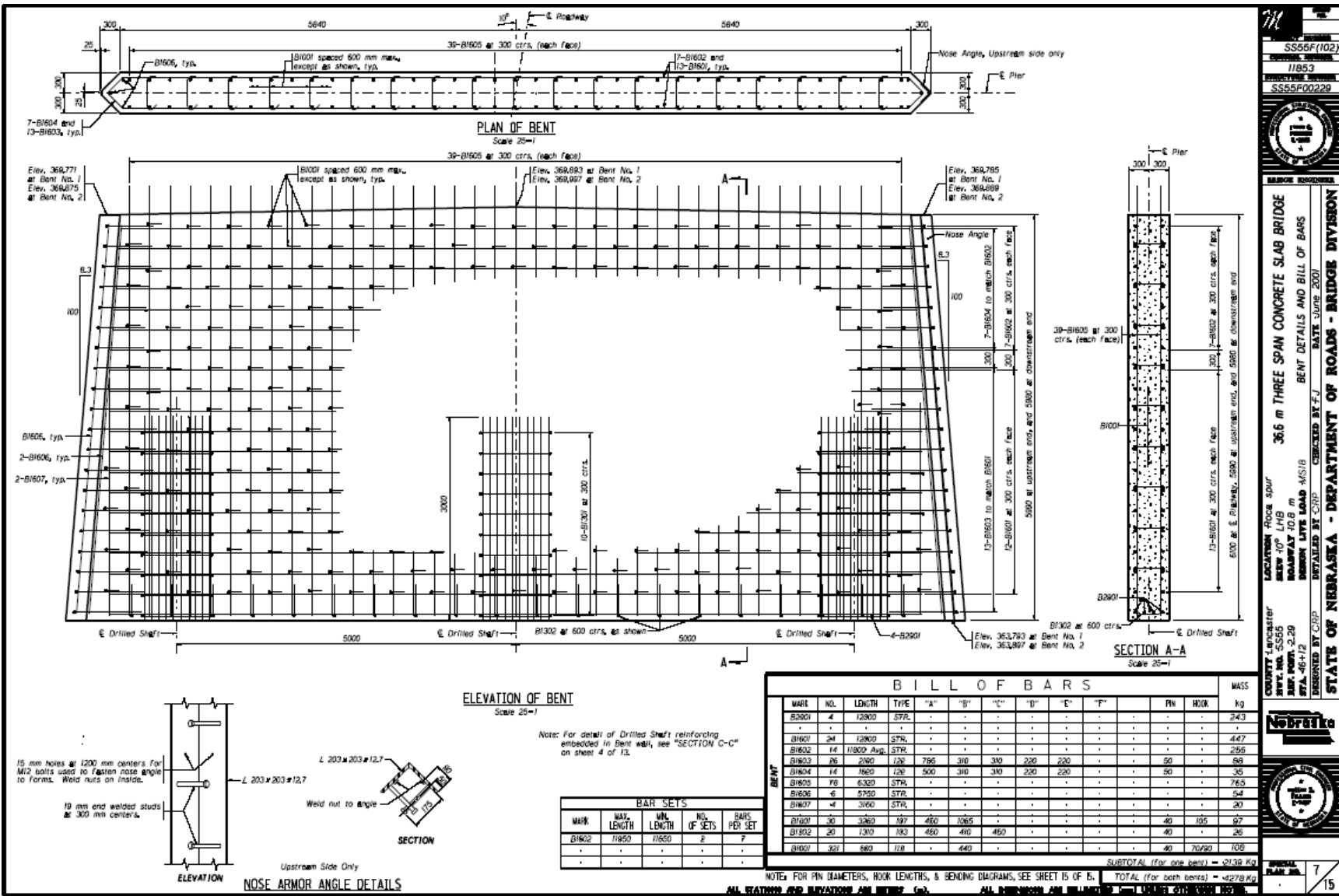
COUNTY Engineer
SHEET NO. SS555
SHEET TOTAL 2-29
DESIGNED BY CRP
CHECKED BY E.J.

LACRAMON ROAD BRIDGE
NEAR 10th LHB
ROADWAY 10.8 m
DESIGN LANE LOAD 45.8 kN/m

SS555F(102)
11853
SS556F00229

6

15



ELEVATION OF BENT
Scale 25=1

BILL OF BARS

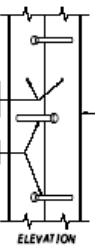
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B2001	4	12800	STR.	243
B1601	24	12800	STR.	447
B1602	14	11800	STR.	256
B1603	26	2160	STR.	120	795	310	330	220	220	.	50	68
B1604	14	1660	STR.	120	500	310	330	220	220	.	50	35
B1605	18	6320	STR.	76.5
B1606	6	5750	STR.	54
B1607	4	3160	STR.	20
B1001	30	3260	STR.	197	450	1065	.	.	.	40	105	97
B1802	20	1310	STR.	193	450	410	450	.	.	40	.	26
B1001	321	680	STR.	.	440	40	70/90	108
SUBTOTAL (for 200 bars) = 2139 kg												
TOTAL (for both bents) = 4278 kg												

BAR SETS

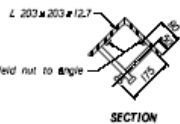
MARK	MAX. LENGTH	MIN. LENGTH	NO. OF SETS	BARS PER SET
B1602	11850	11850	2	7
.
.

NOTE: FOR FN DIAMETERS, HOOK LENGTHS, & BENDING DIAGRAMS, SEE SHEET 15 OF 6.
ALL REINFORCING AND BENDING ARE IN METRIC (mm).

15 mm holes at 1200 mm centers for M12 bolts used to fasten nose angle to forms. Weld nuts on inside.



NOSE ARMOR ANGLE DETAILS



SECTION

SS55F(102)
BRIDGE DESIGN
11853
SS55F00229

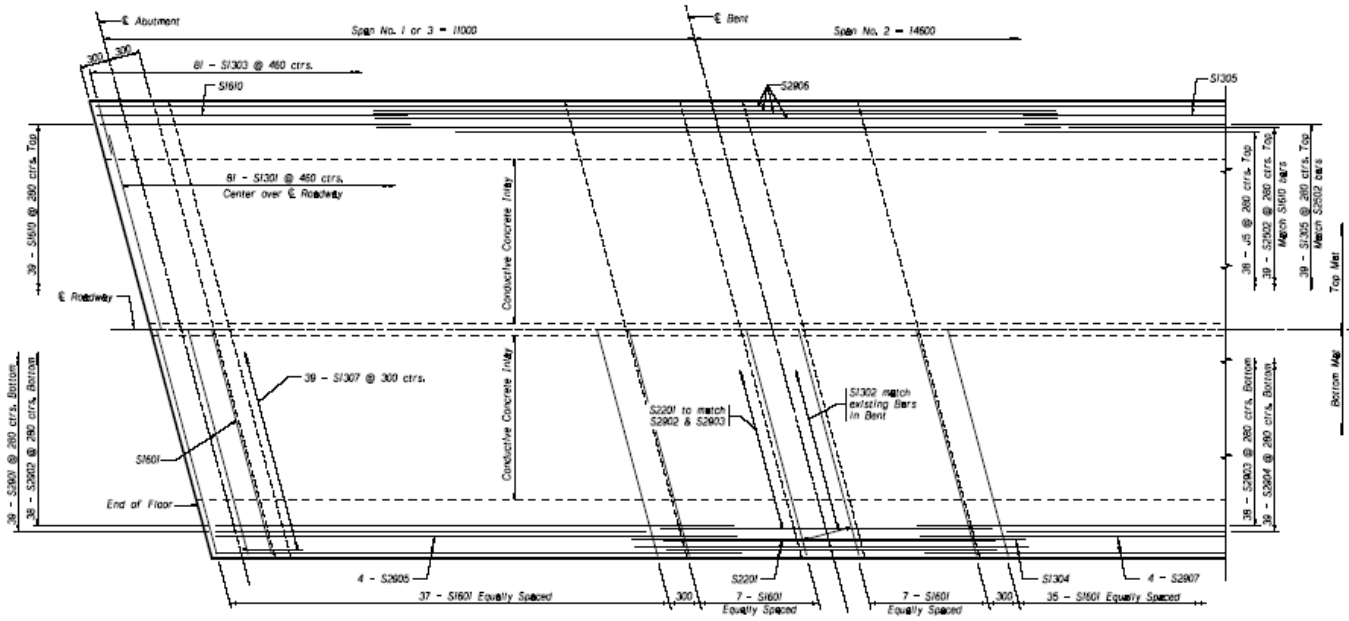
STATE OF NEBRASKA
DEPARTMENT OF ROADS - BRIDGE DIVISION

LACATION: Rock spur
NEW 10' LHB
ROADWAY 10.8 m
DESIGN LIVE LOAD 45/18
BENT DETAILS AND BILL OF BARS
DESIGNED BY CRP
CHECKED BY F.J. DATE: June 2001

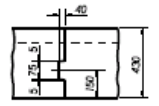
COUNTY Engineer
REV. NO. SS55
REV. DATE 2-20
STA. 46+12

DESIGNED BY CRP

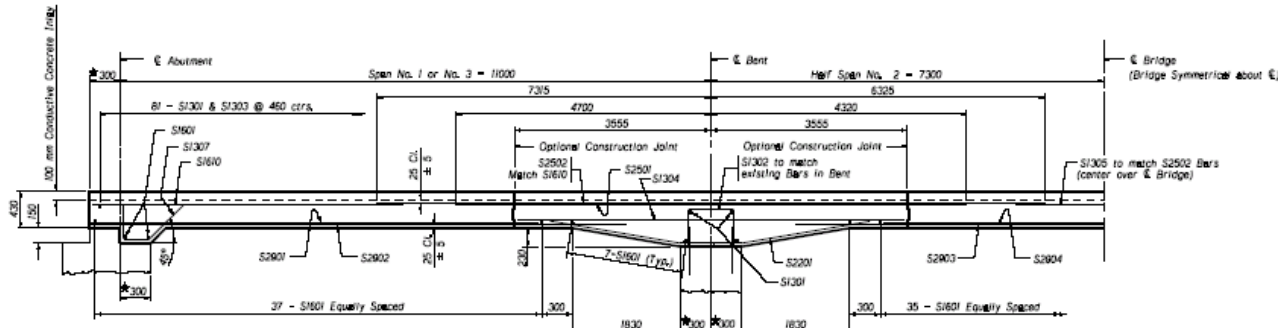
PROJECT NAME NO. 7
15



SLAB REINFORCEMENT LAYOUT
Not to Scale



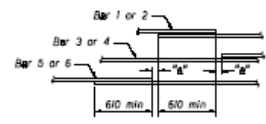
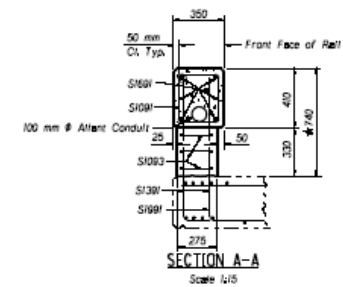
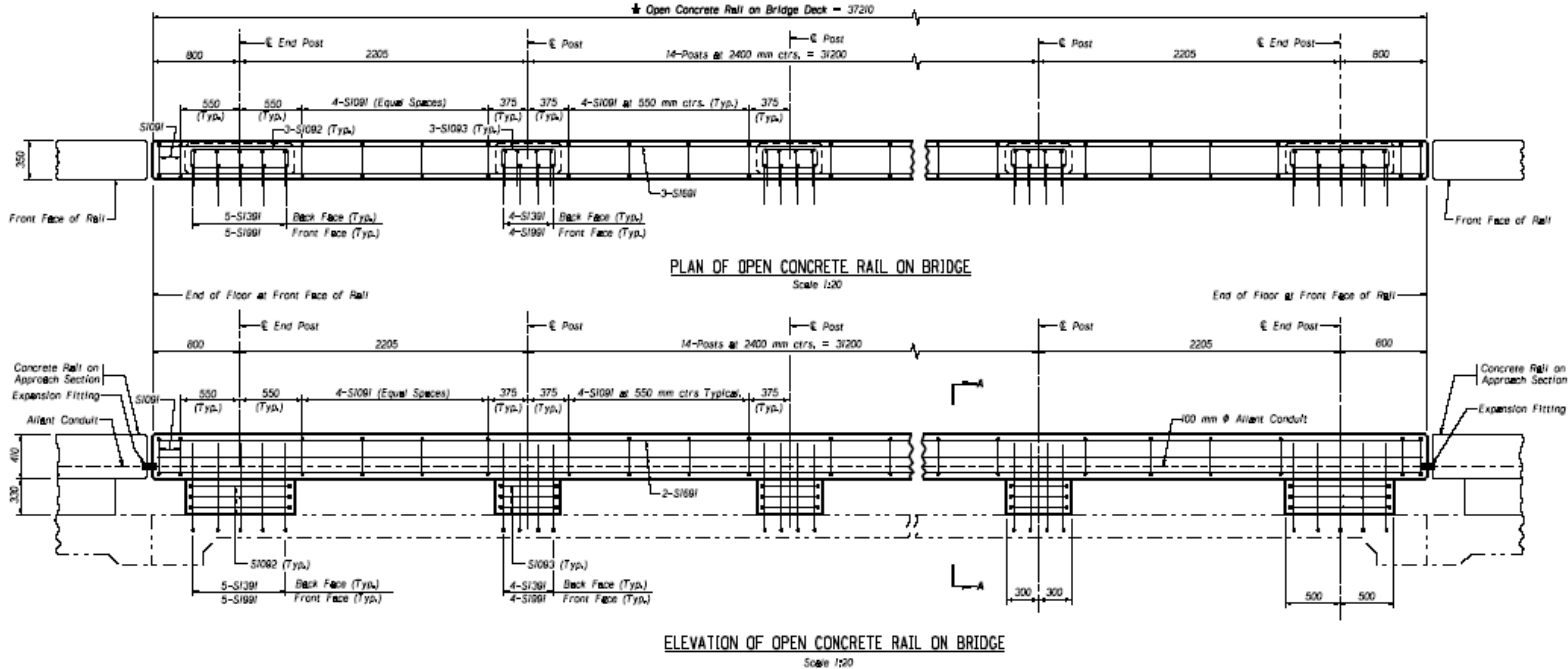
CONSTRUCTION JOINT



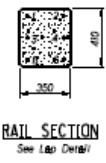
LONGITUDINAL SECTION
Not to Scale

NOTE
When the falsework is removed, the anticipated slab deflection will be 1 mm for each meter of clear span or fraction thereof.

COUNTY: Lancaster DIST. NO.: S555F ROADWAY: 40.8 m DESIGN LANE LOAD: MS/18 DESIGNED BY: J.H. CHECKED BY: J.L. DATE: June 2001	LOCATION: 400 ft SPAN: 40' x 145' m ROADWAY: 40.8 m DESIGN LANE LOAD: MS/18 DESIGNED BY: J.H. CHECKED BY: J.L. DATE: June 2001
SS55F(102) 11853 SS55F00229	
36.6 m THREE SPAN CONCRETE SLAB BRIDGE SLAB REINFORCEMENT LAYOUT BRIDGE DIVISION - DEPARTMENT OF ROADS - STATE OF NEBRASKA	
SPECIAL PLATE NO.	15



▲ Laps for Bars 1 and 5 shall be staggered.
 Laps for Bars 2 and 6 shall be staggered.
 Bar 3 to be continuous through laps for Bars 1 and 5
 Bar 4 to be continuous through laps for Bars 2 and 6
 "a" = Zero



NOTES:
 Posts must be plumb.
 * Measured at front face of rail

SS55F(102)
 1/1853
 SS55F00229

STATE OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION

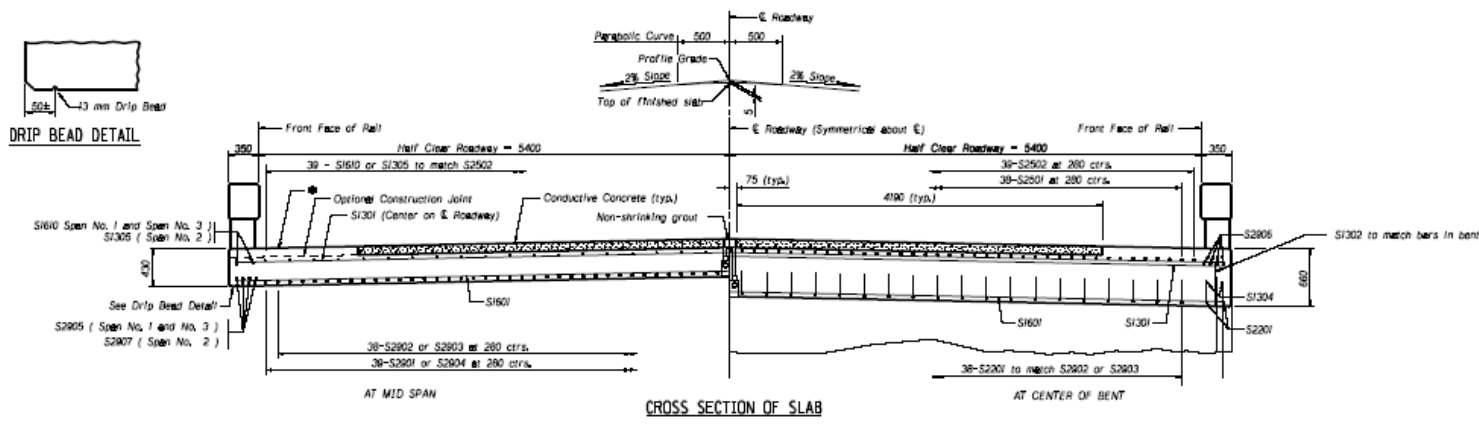
36.6 m THREE SPAN CONCRETE SLAB BRIDGE
 CONCRETE RAIL ON BRIDGE

LACATION: Rock Spur
 DRAWN: J.H.B.
 ROADWAY: 10.8 m
 DESIGN: LITE LOAD 4KSI/8
 CHECKED BY: F.J.
 DATE: June 2001

COUNTY Engineer
 DIST. NO. 5525
 REV. FORM: 2-29
 DESIGNED BY: J.H.

NEBRASKA
 STATE ENGINEER

15



BILL OF BARS													MSS		
MARK	NL	LENGTH	TYPE	"A"	"B"	"C"	"D"	"E"	"F"		PN	HOOK	kg		
S2901	70	8740	STR	3450
S2902	75	9525	STR	3663
S2903	38	11580	STR	2227
S2904	39	8740	STR	1725
S2905	16	9520	STR	771
S2906	16	13640	STR	1104
S2907	8	11580	STR	469
S2901	76	8020	STR	2724
S2902	76	13640	STR	4227
S2901	86	4710	185	2065	580	260	260	2065	.	.	135	.	.	.	1232
S1691	132	1660	184	1060	660	115	.	.	.	497
S1601	741	11510	STR	2819
S1610	86	4750	STR	684
S1691	132	36940	STR	.	includes 3	→ 610 mm Lap	785
S1801	85	11810	STR	873
S1802	70	1440	183	580	440	580	50	.	.	.	112
S1804	8	7000	STR	56
S1805	43	3710	STR	159
S1807	70	1095	119	250	380	485	350	.	.	.	50	.	.	.	85
S1891	132	1360	184	1060	460	80	.	.	.	178
S1891	136	1300	187	310	260	40	90	90	.	99
S1892	10	2330	187	890	175	40	90	16	.	16
S1893	84	1500	187	580	175	40	90	72	.	72
SUBTOTAL =													27707	Kg	
TOTAL =													27707	Kg	

NOTE: FOR PN DIAMETERS, HOOK LENGTHS & BENDING DIAGRAMS SEE SHEET 5 OF 15.

* As an alternate, the contractor may extend the 100 mm Conductive Concrete surface to the edge of the deck.
If the Conductive Concrete is extended to the edge of the deck, a continuous saw cut is required 425 mm left and right of center line of roadway, extending the entire length of the bridge deck. The saw cut must penetrate completely through the Conductive Concrete and be filled with joint sealant.

SS55F(102)
77853
SS55P00229

BRIDGE DIVISION

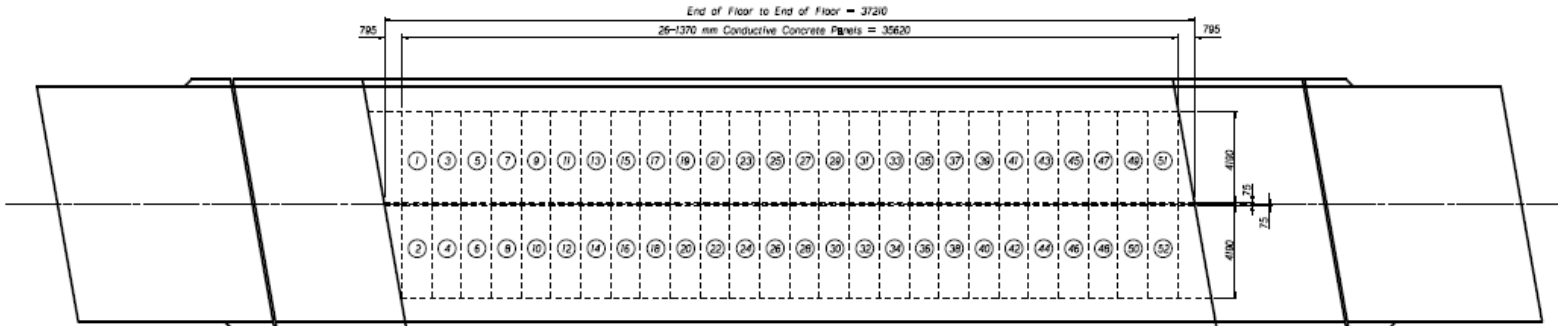
36.6 m THREE SPAN CONCRETE SLAB BRIDGE
CROSS SECTION OF SLAB & BILL OF BARS

LOCATION: 402nd St
SEEN 40° LHB
ROADWAY: 10.6 m
DESIGN LIVE LOAD: MSB
DESIGNED BY: J.H. DATE: June 2001

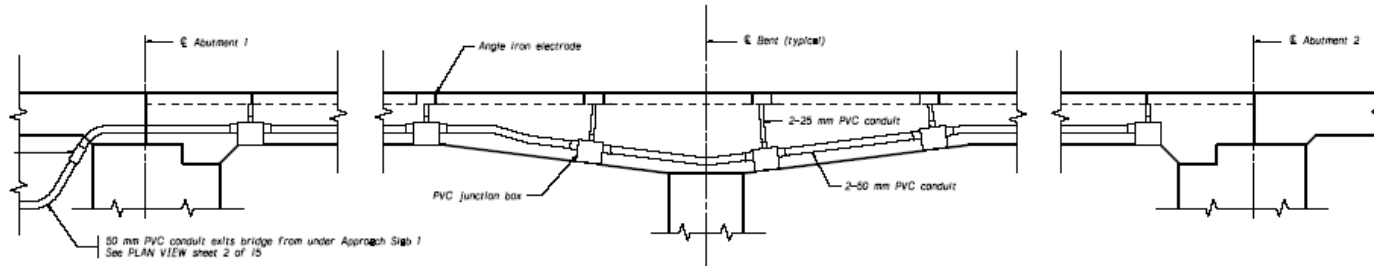
COUNTY: Lancaster
DIST. NO.: SS55
REF. POST.: 2-29
STA.: 6+41.2

STATE OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION

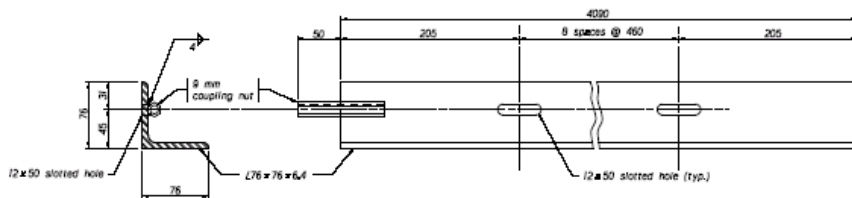
10
15



CONDUCTIVE CONCRETE PANEL LAYOUT



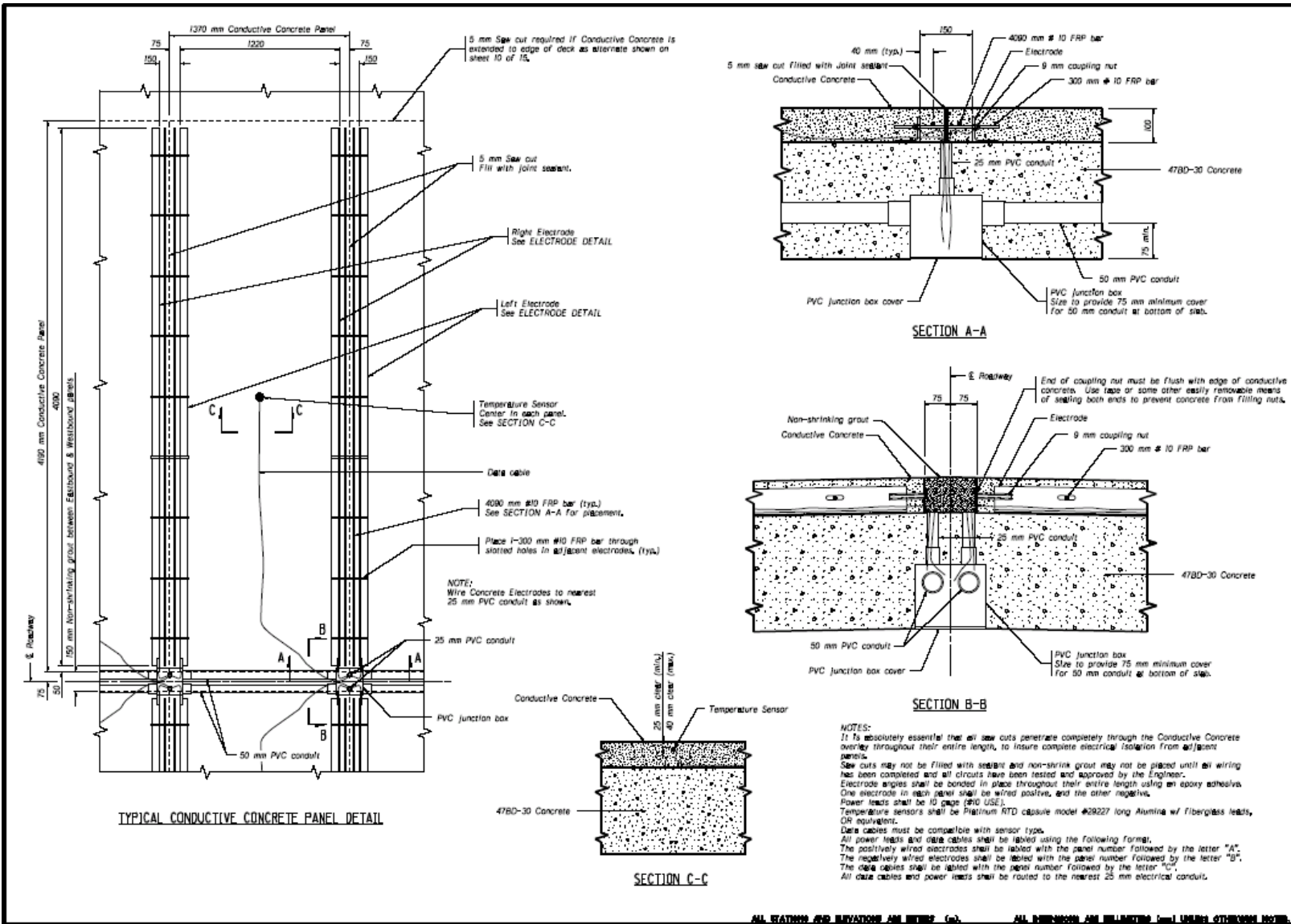
PARTIAL LONGITUDINAL SECTION SHOWING ELECTRICAL CONDUIT



ELECTRODE DETAIL
(Left electrode shown)

NOTES:
52 each Left and Right electrodes are required.
Left electrodes will have the coupling nut welded to left end of the angle when viewed as shown in the detail.
Right electrodes will have the coupling nut welded to the right end of the angle when viewed as shown in the detail.
Electrodes must be blast cleaned to SSPC - PA.

PROJECT NO. SS55F(102)
 DRAWING NO. 11853
 PROJECT TITLE BRIDGE
 SS55F00229
 STATE OF NEBRASKA
 DEPARTMENT OF ROADS - BRIDGE DIVISION
 LOCATION: ROAD 4808
 BEWING RD LHB
 ROADWAY 10.8 m
 DESIGN LANE LOAD 4MS18
 DATE: JUNE 2001
 DESIGNED BY F.H.
 CHECKED BY F.J.
 COUNTY Lancaster
 DIST. NO. SS55
 REF. PROJ. 2-29
 STA. 46+12
 COUNTY OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION
 NEBRASKA
 SPECIAL PERMIT NO. N
 15



SS55F(102)
 11853
 SS55P00229

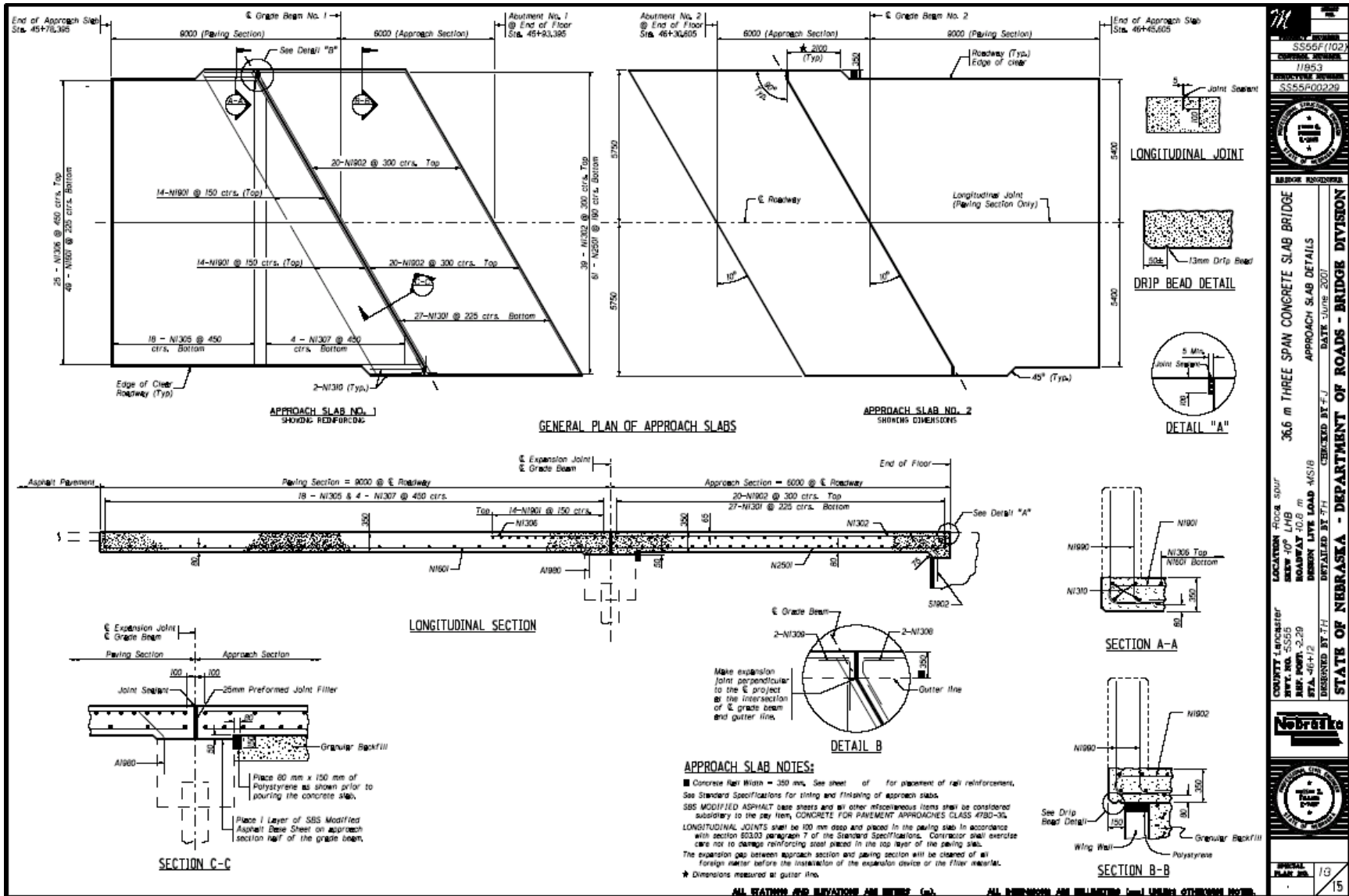
STATE OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION

36.6 m THREE SPAN CONCRETE SLAB BRIDGE
 CONDUCTIVE CONCRETE PANEL DETAILS
 DATE: JUNE 2001
 CHECKED BY: J.H.
 DESIGNED BY: J.H.

LOCATION: 4000' span
 BEYOND 40' LHB
 ROADWAY: 10.8 m
 DESIGN LIVE LOAD: 4KSI/8
 COUNTY: Lancaster
 DIST. NO. SS55
 REF. PROJ. 2-29
 STA. 46+12

NEBRASKA
 STATE ENGINEER

12
 15



SS55F(102)
11853
SS55P00229

STATE OF NEBRASKA
DEPARTMENT OF TRANSPORTATION

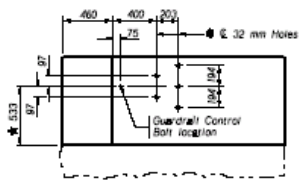
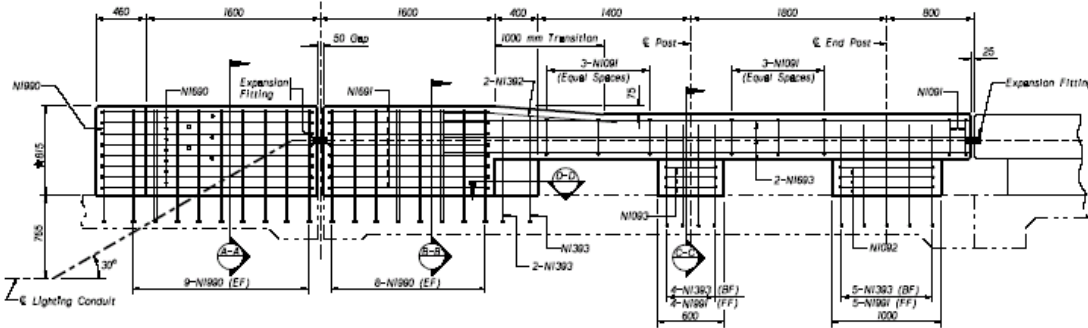
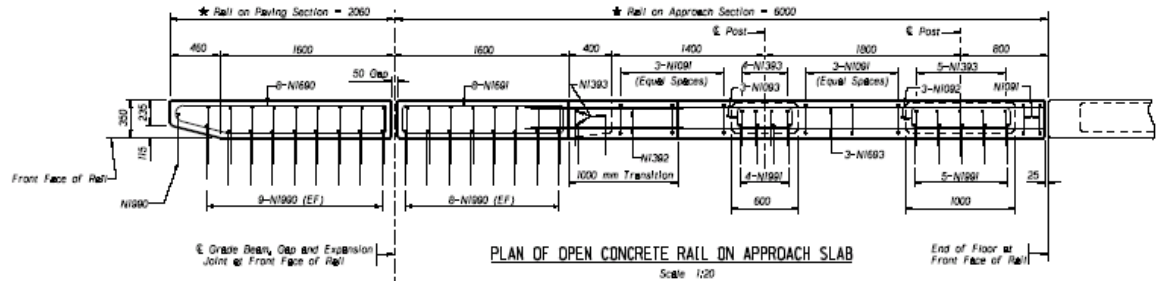
36.6 m THREE SPAN CONCRETE SLAB BRIDGE
APPROACH SLAB DETAILS
DATE: JUNE 2001
CHECKED BY: F.J.
DESIGNED BY: F.H.

COUNTY ENGINEER
REF. NO. 5555
REF. DATE 2-29
STA. 46+12

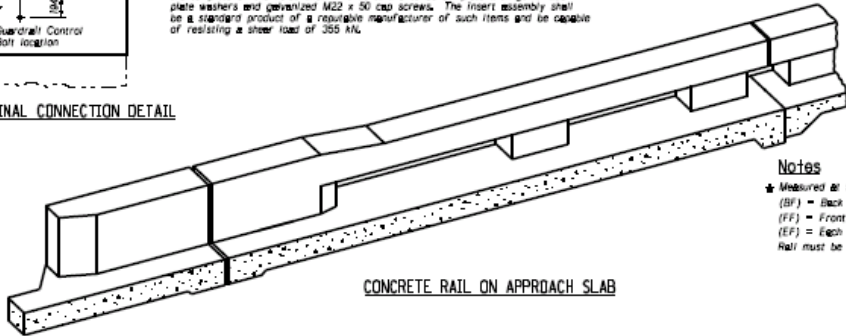
LOCATION: ROCK SPUR
NEAR 10th LHB
ROADWAY 10.8 m
DESIGN LANE LOAD 4518

NEBRASKA
STATE OF NEBRASKA
DEPARTMENT OF TRANSPORTATION

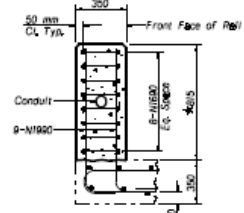
SPECIAL PLANS NO. 1/3
15



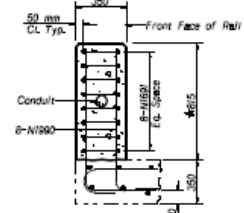
As an alternate method, the contractor shall furnish and cast into the concrete an approved welded assembly consisting of threaded inserts, held accurately to the template of the holes shown. Inserts are to be complete with galvanized plate washers and galvanized M22 x 50 cap screws. The insert assembly shall be a standard product of a reputable manufacturer of such items and be capable of resisting a shear load of 355 kN.



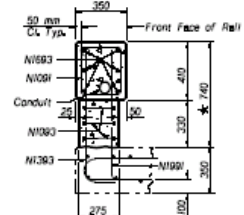
Notes
 * Measured at front face of rail.
 (BF) = Back Face
 (FF) = Front Face
 (EF) = Each Face
 Rail must be plumb.



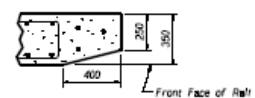
SECTION A-A
Scale 1/15



SECTION B-B
Scale 1/15



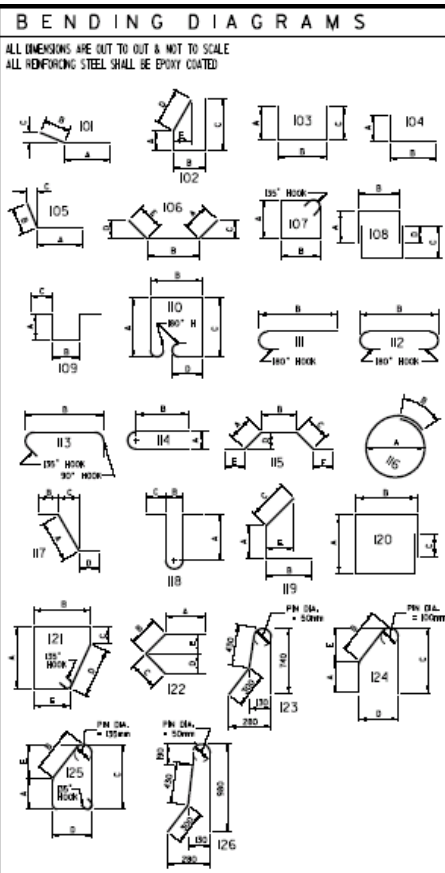
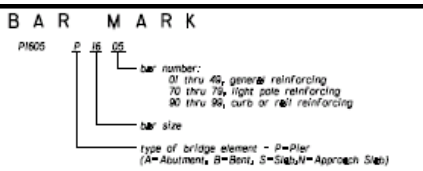
SECTION C-C
Scale 1/15



SECTION D-D
Scale 1/15

COUNTY ENGINEER DIST. NO. 5555 REV. POINT 2-29 STA. 46+12	LOCATION: Rock Spur BEW 10' LHB ROADWAY 10.8 m DESIGN LANE LOAD 4MS18 DATE: JUNE 2001 CHECKED BY: E.J.
STATE OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION	
PROJECT NO. 14 SHEET NO. 15	

BILL OF BARS													
MARK	NUMBER OF BARS		LENGTH	TYPE	"A"	"B"	"C"	"D"	"E"	"F"	PN	HOOK	MASS
	AP SLAB	ON RAIL											
N12501	61		5815	STR.									1409
N1901	20		5810	III		5200					125	200	370
N1902	40		6365	III		6145					125	200	569
N1990	70		1640	104	880	880							257
N1991	19		1500	104	960	960							60
N1601	49		8815-Avg.	STR.									670
N1800	16		4430	125	1520	400	1840	250	380		135/65	140	180
N1801	16		3740	107	1480	250					65	140	93
N1803	12		4700	STR.									88
N1001	27		71510	STR.									389
N1202	30		5945	STR.									227
N1205	18		10640	STR.									180
N1206	25		2000	STR.									50
N1207	4		5565-Avg.	STR.									20
N1208	4		1460	104	280	600	600		580				5
N1209	4		1200	104	960	960							5
N1310	8		1865	STR.									16
N1992	4		1460	104	1160	300	25				65		5
N1993	24		1300	104	960	250					80		31
N1091	16		1300	107	300	250					40	90	12
N1992	6		2330	107	960	175					40	90	8
N1993	6		1530	107	500	175					40	90	5
N12601	61		5815	STR.									1409
N1901	20		5810	III		5200					125	200	370
N1902	40		6365	III		6145					125	200	569
N1990	70		1640	104	880	880							257
N1991	19		1500	104	960	960							60
N1601	49		8815-Avg.	STR.									670
N1800	16		4430	125	1520	400	1840	250	380		135/65	140	180
N1801	16		3740	107	1480	250					65	140	93
N1803	12		4700	STR.									88
N1301	27		71510	STR.									389
N1202	30		5945	STR.									227
N1205	18		10640	STR.									180
N1206	25		2000	STR.									50
N1207	4		5565-Avg.	STR.									20
N1208	4		1460	104	280	600	600		580				5
N1209	4		1200	104	960	960							5
N1310	8		1865	STR.									16
N1992	4		1460	104	1160	300	25				65		5
N1993	24		1300	104	960	250					80		31
N1091	16		1300	107	300	250					40	90	12
N1992	6		2330	107	960	175					40	90	8
N1993	6		1530	107	500	175					40	90	5
SUBTOTAL = 4502 KG													
TOTAL = 9024 KG													



BAR SETS

MARK	MAX LENGTH	MIN LENGTH	NO. OF SETS	BARS PER SET
N1601	9255	7860	2	49
N1207	9365	1735	2	4

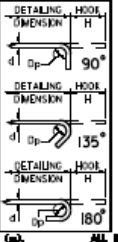
STANDARD HOOK LENGTH

BAR SIZE	HOOK H	
	90°	180°
12	170	65
16	26	80
18	260	30
22	306	290
28	348	280
36	440	380
42	460	425
56	92	470

PIN DIAMETER

BAR SIZE	STIRRUPS & TIES	
	90°	135°
10	80	10
12	95	15
16	115	20
22	155	25
28	185	30
36	260	35
42	285	40

d = BAR SIZE
Dp = PIN DIAMETER



COUNTY ENGINEER
 DIST. NO. 5535
 REF. PLAN 2-29
 STA. 46+12
 DESIGNED BY J.H.
 CHECKED BY J.H.
 DATE: JUNE 2001

LOCATION: 3000' 500'
 BEW 10' LHB
 ROADWAY 70.8 m
 DESIGN LANE LOAD 4KSI/8
 STATE OF NEBRASKA - DEPARTMENT OF ROADS - BRIDGE DIVISION

36.6 m THREE SPAN CONCRETE SLAB BRIDGE
 APPROACH SLAB BILL OF BARS AND
 BRIDGE BENDING DIAGRAMS

S556F(102)
 11853
 S556F00229

SPECIAL PERMITS
 15
 15

APPENDIX B – Bridge Software User’s Guide

Nebraska DOR
Roca Spur Bridge Application User's Guide



Nebraska DOR

**Roca Spur Bridge Application
User's Guide**







Teamwork Technology & Integration

Billing & Acc. Receivable:
TTI, Inc.
P.O. Box 307
Wellsburg, IA 50680-0307
Phone: 641-869-3704
Fax: 641-869-3651

Office Address:
TTI, Inc.
805 Buddy Holly Pl.
Clear Lake, IA 50428
Phone: 641-357-1406
Fax: 641-357-0739

1. Before Starting the Roca Spur Bridge Application

- a. Connect the laptop to the ControlLogix with a null modem DB9 female-to-female cable.
- b. Start RSLinx
 - i. Click: Start  Programs  Rockwell Software  RSLinx  RSLinx

2. Start The Roca Spur Bridge Application

- a. Click: Start  Programs  Roca Spur Bridge  Roca Spur Bridge

Note: The program will take a few moments to load and establish communication; please be patient. If the following message appears, the program is not communicating to the ControlLogix.



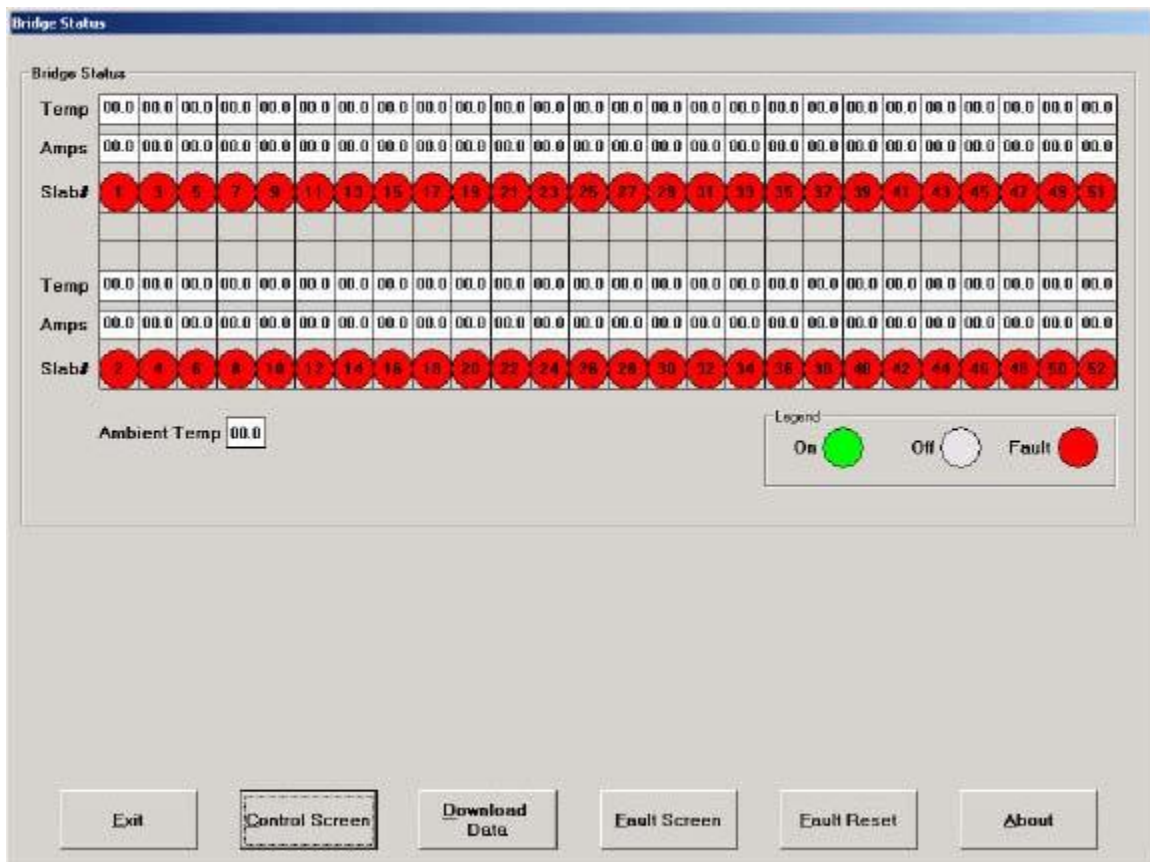
Check your cable connections, verify that RSLinx is running, and try opening the program again.



3. The Status Screen

- a. The first screen that appears when the application is launched.
- b. Features of the Status Screen:

- i. Temperature reading of each slab
- ii. Amperage reading of each slab
- iii. Ambient temperature reading
- iv. Status indicator for each slab
- v. Function and navigation buttons



4. Control Screen

- a. Features of the Control Screen
 - i. On/Off control buttons
 - ii. Temperature setpoints
 - iii. Amperage setpoints
- b. Navigate to the Control Screen by clicking the "Control Screen" button on the Status Screen.
- c. On/Off Control
 - i. Clicking the "Start" button will turn on the bridge.
 - ii. Clicking the "Stop" button will turn off the bridge.
 - iii. If the bridge is running, the "Start" button will be gray, and the "Stop"

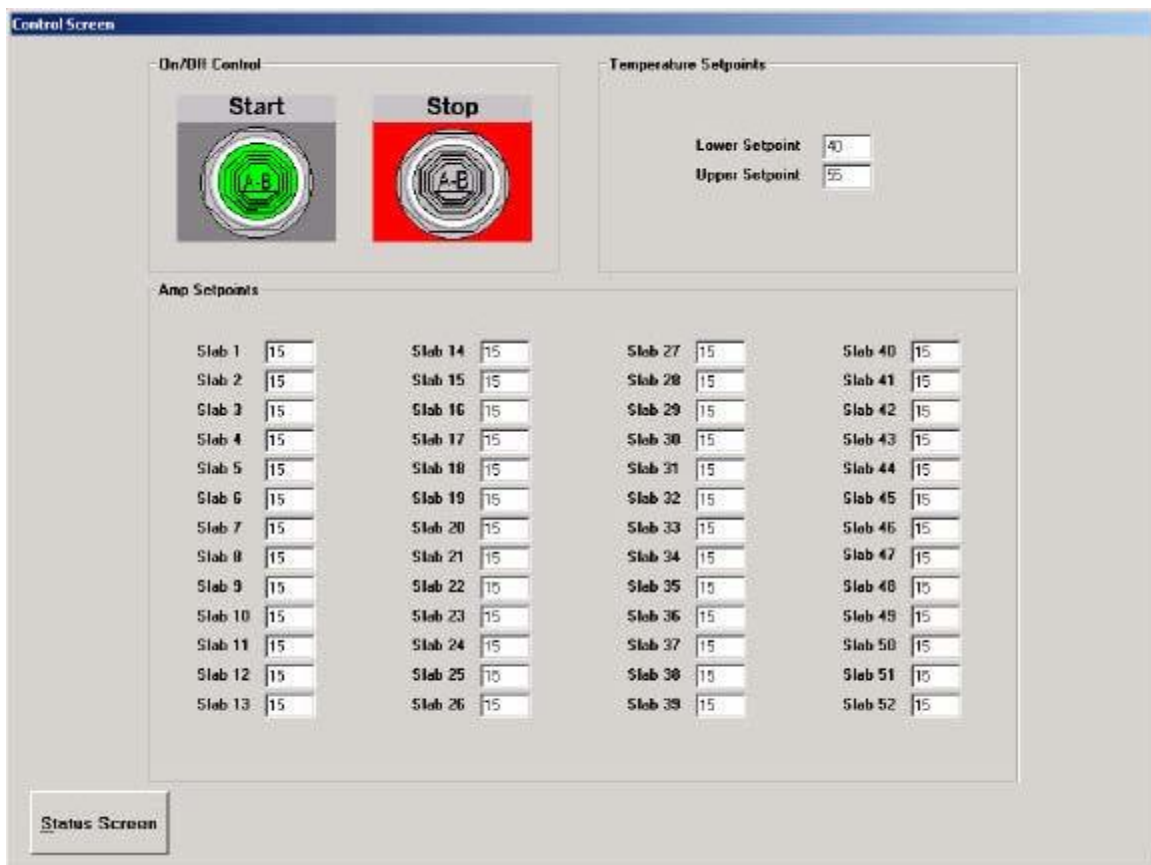
button will be red.

iv. If the bridge is not running, the “Start” button will be green, and the “Stop” button will be gray.

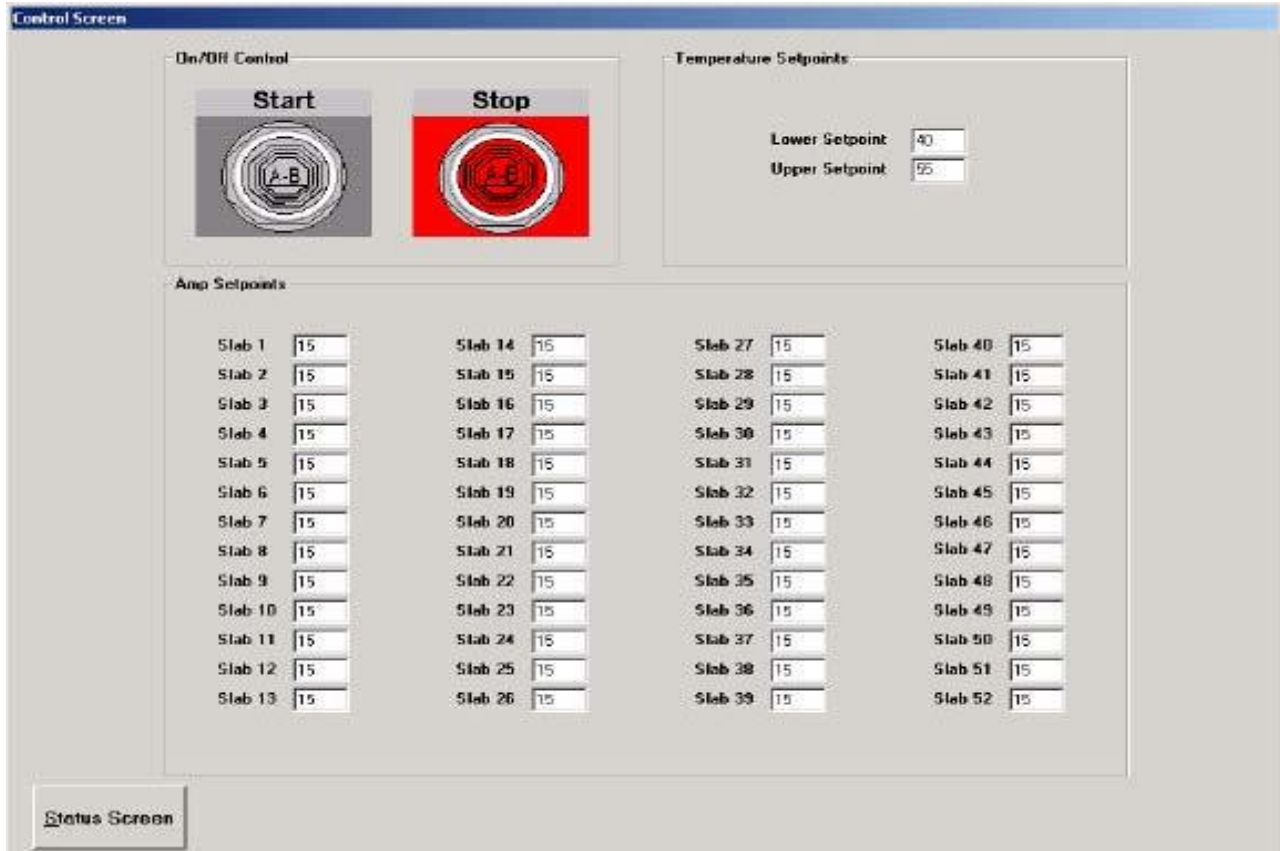
d. Adjusting Setpoints

- i. Type a value into a temperature or amperage field.
- ii. New settings will not take effect until the “Status Screen” button is pressed.

Screen appearance when the bridge is not running

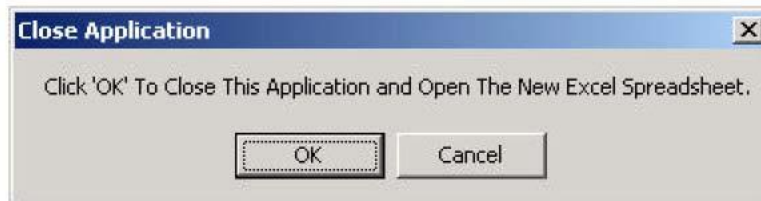


Screen appearance when the bridge is running



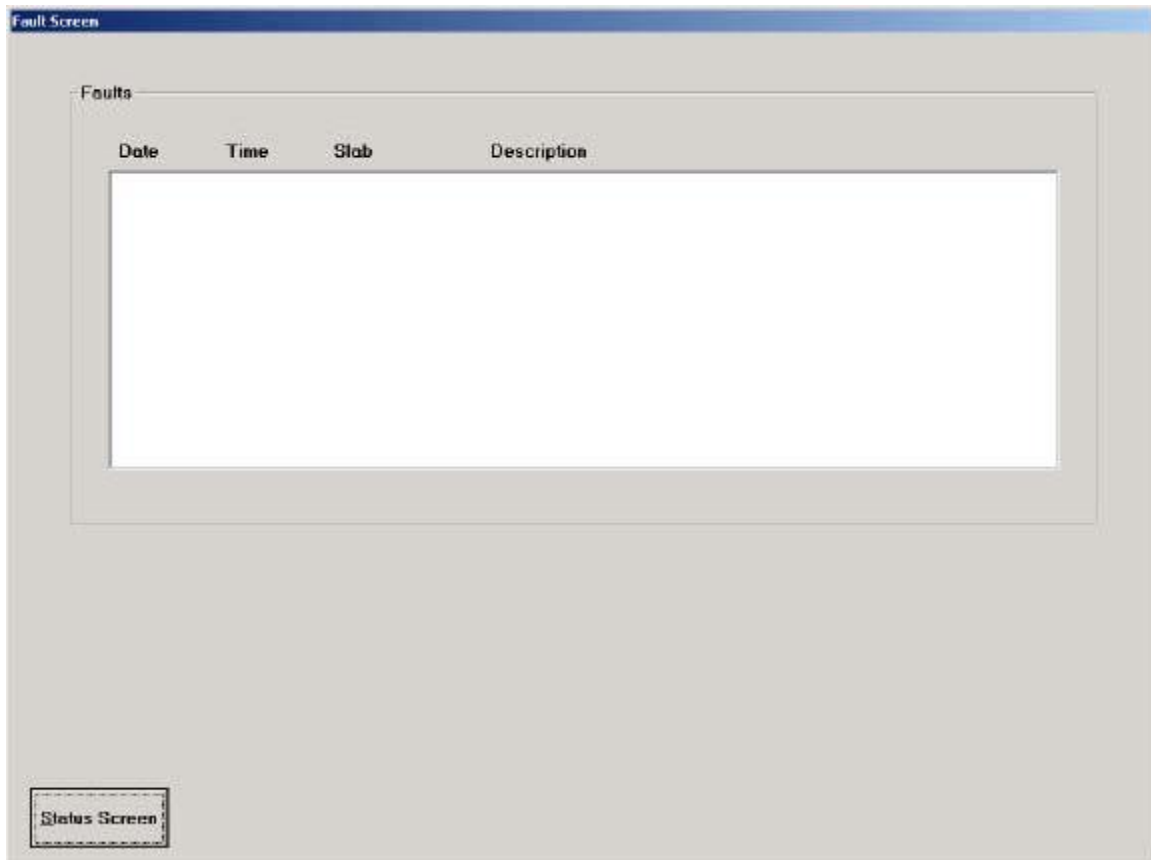
5. Download Data

- a. Clicking the “Download Data” button will download the previous 3 days of temperature and amperage data to an Excel spreadsheet.
- b. This process will take between 10 and 20 minutes.
- c. Text on the Status Screen will indicate the progress of the download.
- d. A message box, confirming a completed download, will appear when the download is finished.
- e. The new Excel file will be located in the “C:\Program Files\Bridge\Data” directory.
- f. The new Excel file will be named ‘Bridge Data MMDDYY HHmm’. For example: If the download finished on April 8, 2003 at 8:33 AM, the file will be called ‘Bridge Data 040803 0833’.
- g. Before the excel file can be opened, the Bridge Application must be closed. The user will be prompted to do this.



6. Fault Screen

- a. Displays a list of the last 25 faults that occurred in the operation of the bridge.
 - i. Date of fault
 - ii. Time of fault
 - iii. Slab number of fault
 - iv. Description of fault
- b. Navigate to the Fault Screen by clicking the "Fault Screen" button.
- c. The faults may take a few minutes to download.
- d. Exit by clicking the "Status Screen" button.



7. Resetting Faults

- a. Clicking the “Fault Reset” button on the Status Screen will reset faults.
- b. Faults will be reset, but they will still appear in the fault history list in the Fault Screen.

8. Closing Your Bridge Session

- a. Click the “Exit” button on the Status Screen.
- b. Close RSLinx.

APPENDIX C – Weather Data

STATION: LINCOLN
 MONTH: DECEMBER
 YEAR: 2003
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:		SKY		:PK WND			
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	43	30	37	6	28	0	0.00	0.0	0	5.0	12	350	M	M	6		14	350
2	43	25	34	3	31	0	0.09	0.0	0	10.4	22	130	M	M	6	1	25	140
3	35	31	33	3	32	0	T	T	T	7.5	14	70	M	M	10	1	16	80
4	37	31	34	4	31	0	0.01	T	0	9.2	31	330	M	M	10	18	43	350
5	31	19	25	-5	40	0	0.00	0.0	0	17.0	38	330	M	M	10	1	45	330
6	32	18	25	-4	40	0	0.00	0.0	0	10.3	20	170	M	M	5	1	24	170
7	47	29	38	9	27	0	0.00	0.0	0	10.5	22	190	M	M	0	1	24	170
8	46	21	34	5	31	0	T	T	0	9.9	22	20	M	M	4	1	25	20
9	33	18	26	-2	39	0	0.40	6.5	0	22.4	31	340	M	M	10	128	37	350
10	23	6	15	-13	50	0	0.00	0.0	6	14.3	28	340	M	M	1	8	32	340
11	19	5	12	-16	53	0	T	T	6	4.2	12	70	M	M	6	1	13	70
12	20	-2	9	-18	56	0	0.00	0.0	5	1.9	8	180	M	M	1	18	9	170
13	28	13	21	-6	44	0	T	0.1	5	6.7	15	160	M	M	10	18	16	170
14	32	23	28	1	37	0	0.00	0.0	2	13.0	22	200	M	M	5	18	26	190
15	35	26	31	4	34	0	0.01	0.2	1	15.6	33	330	M	M	8	189	41	320
16	37	17	27	1	38	0	0.00	0.0	1	13.2	39	340	M	M	4		44	340
17	43	15	29	3	36	0	0.01	0.0	1	10.3	37	330	M	M	3		47	330
18	47	33	40	14	25	0	0.00	0.0	T	17.2	35	330	M	M	1		41	330
19	42	24	33	8	32	0	0.00	0.0	0	6.9	16	330	M	M	0		20	310
20	46	22	34	9	31	0	0.00	0.0	0	11.7	22	190	M	M	0		25	200
21	53	35	44	19	21	0	0.00	0.0	0	6.3	18	210	M	M	0		22	210
22	50	28	39	14	26	0	0.00	0.0	0	8.8	20	10	M	M	6		22	360
23	37	15	26	2	39	0	0.00	0.0	0	7.9	15	310	M	M	0		20	320

24	40	12	26	2	39	0	0.00	0.0	0	5.6	15	200	M	M	0	1	17	190
25	48	23	36	12	29	0	0.00	0.0	0	11.2	20	160	M	M	0		23	160
26	50	34	42	18	23	0	0.00	0.0	0	15.6	25	160	M	M	6	8	31	160
27	56	33	45	21	20	0	0.00	0.0	0	15.6	29	180	M	M	2	1	37	180
28	43	24	34	11	31	0	0.00	0.0	0	10.7	22	290	M	M	3		26	280
29	42	22	32	9	33	0	T	T	0	7.6	18	310	M	M	3		23	320
30	49	19	34	11	31	0	0.00	0.0	0	9.8	23	210	M	M	1		26	190
31	39	15	27	4	38	0	0.00	0.0	0	6.7	13	120	M	M	0		16	100

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SM 1226 664 1065 0 0.52 6.8 323.1 M 121
=====
AV 39.5 21.4 10.4 FASTST PSBL % 4 MAX(MPH)
MISC ----> 39 340 47 330
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NOTES:

LAST OF SEVERAL OCCURRENCES
 COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: DECEMBER
 YEAR: 2003
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 30.5	TOTAL FOR MONTH: 0.52	1 = FOG
DPTR FM NORMAL: 4.0	DPTR FM NORMAL: -0.34	2 = FOG REDUCING VISIBILITY
HIGHEST: 56 ON 27	GRTST 24HR 0.40 ON 9- 9	TO 1/4 MILE OR LESS
LOWEST: -2 ON 12		3 = THUNDER
	SNOW, ICE PELLETS, HAIL	4 = ICE PELLETS
	TOTAL MONTH: 6.8 INCHES	5 = HAIL
	GRTST 24HR 6.5 ON 9- 9	6 = GLAZE OR RIME
	GRTST DEPTH: 6 ON 11,10	7 = BLOWING DUST OR SAND:
		VSBY 1/2 MILE OR LESS

[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]	
MAX 32 OR BELOW: 7	0.01 INCH OR MORE: 5	8 = SMOKE OR HAZE
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 1	9 = BLOWING SNOW
MIN 32 OR BELOW: 27	0.50 INCH OR MORE: 0	X = TORNADO
MIN 0 OR BELOW: 1	1.00 INCH OR MORE: 0	
[HDD (BASE 65)]		
TOTAL THIS MO. 1065	CLEAR (SCALE 0-3) 16	
DPTR FM NORMAL -123	PTCLDY (SCALE 4-7) 9	
SEASONAL TOTAL 2314	CLOUDY (SCALE 8-10) 6	
DPTR FM NORMAL -163		
[CDD (BASE 65)]		
TOTAL THIS MO. 0		
DPTR FM NORMAL 0	[PRESSURE DATA]	
SEASONAL TOTAL 1132	HIGHEST SLP 30.68 ON 1	
DPTR FM NORMAL -22	LOWEST SLP 29.40 ON 15	

STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2004
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:			SKY		:PK WND		
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG MX		2MIN						
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	56	21	39	16	26	0	0.00	0.0	0	5.8	14	260	M	M	0		16	260
2	63	26	45	22	20	0	0.00	0.0	0	7.4	23	10	M	M	2	12	26	10
3	31	19	25	3	40	0	0.01	0.2	0	17.7	24	30	M	M	9		29	30
4	19	10	15	-7	50	0	0.28	4.8	2	18.1	29	10	M	M	10	1	35	20
5	10	-6	2	-20	63	0	T	T	5	11.8	21	360	M	M	4		24	10
6	13	-9	2	-20	63	0	0.00	0.0	5	6.0	15	230	M	M	0		18	270
7	29	-5	12	-10	53	0	0.00	0.0	4	5.3	21	180	M	M	0		25	180
8	31	15	23	1	42	0	0.00	0.0	4	7.2	21	350	M	M	5	18	24	360
9	27	13	20	-2	45	0	0.00	0.0	3	3.7	14	340	M	M	6	18	17	340
10	40	9	25	3	40	0	0.00	0.0	3	5.7	18	210	M	M	0	18	24	200
11	52	22	37	15	28	0	0.00	0.0	2	5.5	13	310	M	M	0		16	310
12	47	18	33	11	32	0	0.00	0.0	T	3.2	12	230	M	M	0	1	14	240
13	44	19	32	10	33	0	0.00	0.0	0	4.6	14	210	M	M	0	1	17	210
14	47	19	33	11	32	0	0.00	0.0	0	11.4	29	330	M	M	0		33	330
15	51	18	35	13	30	0	0.00	0.0	0	8.8	21	210	M	M	0	18	26	220
16	47	31	39	17	26	0	0.04	0.0	0	3.4	9	340	M	M	7	12	12	340
17	42	24	33	11	32	0	T	0.0	0	14.1	25	10	M	M	6	1	32	350
18	28	7	18	-4	47	0	0.00	0.0	0	13.9	24	10	M	M	0		30	20
19	23	3	13	-9	52	0	0.00	0.0	0	5.5	13	170	M	M	3		15	160
20	33	22	28	6	37	0	0.00	0.0	0	7.0	15	180	M	M	10		17	170
21	52	19	36	14	29	0	0.00	0.0	0	11.0	25	20	M	M	2		30	20
22	26	14	20	-2	45	0	0.00	0.0	0	9.9	23	360	M	M	6		26	20

23	62	26	44	22	21	0	0.00	0.0	0	12.5	24	300	M	M	0	29	310	
24	34	23	29	6	36	0	0.00	0.0	0	12.7	18	110	M	M	5	18	22	80
25	26	21	24	1	41	0	0.28	4.5	0	10.6	16	100	M	M	10	16	21	100
26	21	2	12	-11	53	0	0.19	5.6	5	18.0	29	340	M	M	10	128	36	340
27	7	-8	0	-23	65	0	0.00	0.0	10	7.4	25	340	M	M	0	29	350	
28	3	-8	-2	-25	67	0	0.00	0.0	10	10.1	20	10	M	M	2	23	10	
29	3	-8	-2	-25	67	0	0.00	0.0	9	9.9	18	30	M	M	6	21	30	
30	6	-7	0	-24	65	0	0.00	0.0	9	6.8	13	80	M	M	3	15	70	
31	19	4	12	-12	53	0	0.01	0.2	9	7.8	15	70	M	M	6	18	17	80

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SM 992 354 1333 0 0.81 15.3 282.7 M 112

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AV 32.0 11.4 9.1 FASTST PSBL % 4 MAX(MPH)

MISC ----> 29 330 36 340

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NOTES:
 # LAST OF SEVERAL OCCURRENCES
 COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2
 STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2004
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 21.7	TOTAL FOR MONTH: 0.81	1 = FOG
DPTR FM NORMAL: -0.7	DPTR FM NORMAL: 0.14	2 = FOG REDUCING VISIBILITY
HIGHEST: 63 ON 2	GRTST 24HR 0.28 ON 25-25	TO 1/4 MILE OR LESS
LOWEST: -9 ON 6		3 = THUNDER
	SNOW, ICE PELLETS, HAIL	4 = ICE PELLETS
	TOTAL MONTH: 15.3 INCHES	5 = HAIL
	GRTST 24HR 5.6 ON 26-26	6 = GLAZE OR RIME
	GRTST DEPTH: 10 ON 28,27	7 = BLOWING DUST OR SAND:

[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]	
MAX 32 OR BELOW: 17	0.01 INCH OR MORE: 6	VSBY 1/2 MILE OR LESS
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 3	8 = SMOKE OR HAZE
MIN 32 OR BELOW: 31	0.50 INCH OR MORE: 0	9 = BLOWING SNOW
MIN 0 OR BELOW: 7	1.00 INCH OR MORE: 0	X = TORNADO
[HDD (BASE 65)]		
TOTAL THIS MO. 1333	CLEAR (SCALE 0-3) 17	
DPTR FM NORMAL 5	PTCLDY (SCALE 4-7) 9	
SEASONAL TOTAL 3647	CLOUDY (SCALE 8-10) 5	
DPTR FM NORMAL -158		
[CDD (BASE 65)]		
TOTAL THIS MO. 0		
DPTR FM NORMAL 0	[PRESSURE DATA]	
SEASONAL TOTAL 0	HIGHEST SLP 30.76 ON 5	
DPTR FM NORMAL 0	LOWEST SLP 29.61 ON 2	

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2004
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:		SKY		:PK WND			
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG MX 2MIN								
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	20	16	18	-6	47	0	0.30	4.6	8	9.4	15	20	M	M	10	12	18	20
2	18	8	13	-11	52	0	0.05	1.1	13	12.7	23	340	M	M	7	189	30	330
3	19	-7	6	-19	59	0	0.00	0.0	13	3.9	10	170	M	M	0	18	13	170
4	26	10	18	-7	47	0	0.02	0.4	12	9.8	17	130	M	M	9	1	22	120
5	26	22	24	-1	41	0	0.38	7.0	13	9.5	15	100	M	M	10	128	20	110
6	22	9	16	-10	49	0	0.02	0.4	18	15.0	25	330	M	M	9	18	29	330
7	13	-5	4	-22	61	0	T	T	17	8.1	18	320	M	M	2	8	21	330
8	34	-7	14	-12	51	0	T	0.0	15	15.7	36	230	M	M	2	168	44	240
9	34	13	24	-2	41	0	0.00	0.0	13	7.8	15	240	M	M	2		18	280
10	32	13	23	-4	42	0	0.00	0.0	12	9.1	16	210	M	M	1		20	220
11	36	12	24	-3	41	0	T	T	11	14.5	30	320	M	M	4		36	320
12	15	1	8	-19	57	0	0.00	0.0	10	10.3	21	330	M	M	1		23	330
13	32	4	18	-10	47	0	0.00	0.0	9	9.0	20	240	M	M	0		22	230
14	22	4	13	-15	52	0	0.00	0.0	9	11.1	24	20	M	M	0	18	26	20
15	17	-6	6	-22	59	0	0.00	0.0	9	5.2	10	10	M	M	0		12	10
16	36	9	23	-6	42	0	0.00	0.0	9	3.0	10	180	M	M	0	18	12	180
17	40	7	24	-5	41	0	0.00	0.0	8	5.7	17	190	M	M	1	18	20	190
18	43	30	37	8	28	0	0.00	0.0	7	10.1	24	210	M	M	0	18	30	200
19	50	28	39	9	26	0	0.00	0.0	6	7.6	23	340	M	M	2	18	28	340
20	47	33	40	10	25	0	T	0.0	5	17.7	31	330	M	M	4	18	37	340
21	49	22	36	6	29	0	T	0.0	2	6.4	15	170	M	M	2		17	170
22	56	28	42	11	23	0	0.00	0.0	T	9.1	18	190	M	M	5		22	180

23	40	26	33	2	32	0	0.00	0.0	T	12.9	21	20	M	M	7	18	26	50
24	34	31	33	2	32	0	0.00	0.0	T	9.6	15	70	M	M	10	18	17	70
25	40	22	31	-1	34	0	0.00	0.0	0	6.2	13	110	M	M	7	18	15	130
26	50	17	34	2	31	0	0.00	0.0	0	8.6	20	170	M	M	0	18	24	170
27	59	34	47	14	18	0	0.00	0.0	0	17.0	29	170	M	M	0		35	170
28	57	39	48	15	17	0	0.00	0.0	0	17.0	28	180	M	M	2		32	180
29	49	44	47	14	18	0	0.40	0.0	0	16.8	41	160	M	M	10	18	47	170

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SM 1016 457 1142 0 1.17 13.5 298.8 M 107

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AV 35.0 15.8 10.3 FASTST PSBL % 4 MAX(MPH)

MISC ----> 41 160 47 170

=====

NOTES:

LAST OF SEVERAL OCCURRENCES
 COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2004
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 25.4	TOTAL FOR MONTH: 1.17	1 = FOG
DPTR FM NORMAL: -2.9	DPTR FM NORMAL: 0.51	2 = FOG REDUCING VISIBILITY TO 1/4 MILE OR LESS
HIGHEST: 59 ON 27	GRTST 24HR 0.40 ON 29-29	3 = THUNDER
LOWEST: -7 ON 8, 3		4 = ICE PELLETS
	SNOW, ICE PELLETS, HAIL	5 = HAIL
	TOTAL MONTH: 13.5 INCHES	6 = GLAZE OR RIME
	GRTST 24HR 7.0 ON 5- 5	7 = BLOWING DUST OR SAND: VSBY 1/2 MILE OR LESS
	GRTST DEPTH: 18 ON 6	8 = SMOKE OR HAZE

[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]	
MAX 32 OR BELOW: 12	0.01 INCH OR MORE: 6	9 = BLOWING SNOW
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 3	X = TORNADO
MIN 32 OR BELOW: 25	0.50 INCH OR MORE: 0	
MIN 0 OR BELOW: 4	1.00 INCH OR MORE: 0	
[HDD (BASE 65)]		
TOTAL THIS MO. 1142	CLEAR (SCALE 0-3) 17	
DPTR FM NORMAL 67	PTCLDY (SCALE 4-7) 6	
SEASONAL TOTAL 4789	CLOUDY (SCALE 8-10) 6	
DPTR FM NORMAL -59		
[CDD (BASE 65)]		
TOTAL THIS MO. 0		
DPTR FM NORMAL 0	[PRESSURE DATA]	
SEASONAL TOTAL 0	HIGHEST SLP 30.61 ON 12	
DPTR FM NORMAL 0	LOWEST SLP 29.36 ON 29	

STATION: LINCOLN
 MONTH: MARCH
 YEAR: 2004
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:	WIND		:SUNSHINE:		SKY	:PK WND					
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG MX 2MIN								
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	47	34	41	8	24	0	0.11	T	0	19.3	38	180	M	M	10	18	45	180
2	39	33	36	2	29	0	0.00	0.0	0	8.6	16	310	M	M	10	8	21	320
3	41	33	37	3	28	0	0.04	T	0	5.1	12	320	M	M	9	18	13	320
4	38	32	35	0	30	0	0.72	T	0	12.5	26	10	M	M	10	12	31	10
5	41	32	37	2	28	0	0.26	T	0	13.6	25	340	M	M	10	1	30	340
6	63	25	44	9	21	0	0.00	0.0	0	14.7	36	330	M	M	0	1	43	320
7	52	30	41	5	24	0	0.00	0.0	0	14.8	32	330	M	M	0		40	310
8	68	27	48	12	17	0	0.00	0.0	0	12.9	32	340	M	M	0		38	330
9	57	33	45	8	20	0	0.00	0.0	0	8.6	17	330	M	M	0		22	330
10	58	33	46	9	19	0	0.01	0.0	0	15.1	36	340	M	M	2	1	40	340
11	44	21	33	-4	32	0	0.00	0.0	0	15.0	32	330	M	M	0		38	330
12	59	15	37	-1	28	0	0.00	0.0	0	9.4	20	170	M	M	1		23	160
13	62	43	53	15	12	0	T	0.0	0	17.4	32	210	M	M	6	8	41	180
14	54	32	43	4	22	0	0.00	0.0	0	11.5	28	320	M	M	1		35	320
15	47	30	39	0	26	0	0.56	T	0	14.2	28	150	M	M	10	1	33	130
16	42	29	36	-3	29	0	T	T	T	7.2	17	210	M	M	7	18	20	220
17	58	29	44	4	21	0	T	T	0	4.9	15	50	M	M	4		17	50
18	56	38	47	7	18	0	T	0.0	0	10.9	21	360	M	M	3	1	24	350
19	74	34	54	13	11	0	0.00	0.0	0	17.1	32	200	M	M	3	18	38	200
20	61	34	48	7	17	0	0.00	0.0	0	18.3	31	10	M	M	0	18	38	20
21	44	23	34	-7	31	0	0.00	0.0	0	9.6	18	360	M	M	1		21	10
22	56	32	44	2	21	0	0.00	0.0	0	11.9	23	180	M	M	4		28	190

23	65	37	51	9	14	0	T	0.0	0	8.6	21	190	M	M	2	8	26	190
24	76	53	65	22	0	0	0.00	0.0	0	13.8	22	210	M	M	1	8	26	230
25	72	60	66	23	0	1	0.00	0.0	0	13.2	22	200	M	M	9	18	28	190
26	77	58	68	25	0	3	0.00	0.0	0	9.0	22	170	M	M	8	18	26	160
27	67	45	56	12	9	0	0.98	0.0	0	17.9	33	170	M	M	9	138	44	160
28	59	39	49	5	16	0	0.02	0.0	0	8.4	33	310	M	M	3	3	40	320
29	58	34	46	1	19	0	0.13	0.0	0	8.2	24	270	M	M	3	3	31	290
30	47	29	38	-7	27	0	0.00	0.0	0	9.3	21	10	M	M	3		25	330
31	54	23	39	-6	26	0	0.00	0.0	0	2.3	13	80	M	M	0	18	15	80

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SM 1736 1050          619  4  2.83    T    363.4          M    129
=====
AV 56.0 33.9          11.7 FASTST  PSBL  %    4    MAX(MPH)
                        MISC ---->  38 180          45 180
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NOTES:

LAST OF SEVERAL OCCURRENCES
 COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: MARCH
 YEAR: 2004
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]
 AVERAGE MONTHLY: 44.9
 DPTR FM NORMAL: 5.5
 HIGHEST: 77 ON 26
 LOWEST: 15 ON 12

[PRECIPITATION DATA]
 TOTAL FOR MONTH: 2.83
 DPTR FM NORMAL: 0.62
 GRTST 24HR 0.98 ON 27-27
 SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: T
 GRTST 24HR T ON 17-17
 GRTST DEPTH: 0

SYMBOLS USED IN COLUMN 16
 1 = FOG
 2 = FOG REDUCING VISIBILITY
 TO 1/4 MILE OR LESS
 3 = THUNDER
 4 = ICE PELLETS
 5 = HAIL
 6 = GLAZE OR RIME
 7 = BLOWING DUST OR SAND:

[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]	VSBY 1/2 MILE OR LESS
		8 = SMOKE OR HAZE
		9 = BLOWING SNOW
		X = TORNADO
MAX 32 OR BELOW: 0	0.01 INCH OR MORE: 9	
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 6	
MIN 32 OR BELOW: 15	0.50 INCH OR MORE: 3	
MIN 0 OR BELOW: 0	1.00 INCH OR MORE: 0	
[HDD (BASE 65)]		
TOTAL THIS MO. 619	CLEAR (SCALE 0-3) 18	
DPTR FM NORMAL -180	PTCLDY (SCALE 4-7) 4	
SEASONAL TOTAL 5408	CLOUDY (SCALE 8-10) 9	
DPTR FM NORMAL -239		
[CDD (BASE 65)]		
TOTAL THIS MO. 4		
DPTR FM NORMAL 3	[PRESSURE DATA]	
SEASONAL TOTAL 4	HIGHEST SLP M ON M	
DPTR FM NORMAL 3	LOWEST SLP M ON M	

STATION: LINCOLN
 MONTH: DECEMBER
 YEAR: 2004
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND			:SUNSHINE:			SKY		:PK WND		
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18	
										AVG MX		2MIN							
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR	
1	39	17	28	-3	37	0	0.00	0.0	T	2.0	8	330	M	M	0		9	340	
2	45	21	33	2	32	0	0.00	0.0	T	4.7	17	260	M	M	0		23	270	
3	47	19	33	3	32	0	0.00	0.0	0	6.8	15	260	M	M	1		18	280	
4	57	25	41	11	24	0	0.00	0.0	0	5.2	17	250	M	M	0		25	250	
5	39	25	32	2	33	0	0.42	0.0	0	4.4	12	140	M	M	5	12	14	140	
6	39	34	37	8	28	0	0.00	0.0	0	3.7	13	190	M	M	10	12	14	220	
7	35	27	31	2	34	0	0.00	0.0	0	6.9	20	310	M	M	9	12	22	310	
8	47	25	36	7	29	0	0.00	0.0	0	1.9	14	150	M	M	1	12	18	150	
9	54	23	39	11	26	0	T	0.0	0	7.8	23	340	M	M	5	12	30	340	
10	40	25	33	5	32	0	0.00	0.0	0	17.3	29	330	M	M	8		36	320	
11	48	17	33	5	32	0	0.00	0.0	0	6.9	18	180	M	M	1	1	22	180	
12	51	32	42	15	23	0	0.00	0.0	0	19.0	37	340	M	M	1		40	330	
13	32	11	22	-5	43	0	0.00	0.0	0	13.0	28	350	M	M	1		31	350	
14	39	8	24	-3	41	0	0.00	0.0	0	7.5	16	190	M	M	0		21	200	
15	44	26	35	8	30	0	0.00	0.0	0	11.9	24	220	M	M	0		32	210	
16	51	21	36	10	29	0	0.00	0.0	0	4.7	17	340	M	M	0		20	320	
17	49	19	34	8	31	0	0.00	0.0	0	4.2	13	280	M	M	2		15	290	
18	49	20	35	9	30	0	0.00	0.0	0	11.5	31	340	M	M	3		37	340	
19	20	2	11	-14	54	0	0.00	0.0	0	6.5	22	360	M	M	1		26	20	
20	52	19	36	11	29	0	0.01	0.0	0	11.7	28	320	M	M	2		32	320	
21	37	9	23	-2	42	0	0.00	0.0	0	13.0	25	310	M	M	0		33	300	
22	18	3	11	-14	54	0	0.00	0.0	0	8.1	14	20	M	M	0		18	350	

23	13	-4	5	-19	60	0	0.00	0.0	0	8.1	22	350	M	M	2	26	350
24	32	-4	14	-10	51	0	0.00	0.0	0	14.8	31	220	M	M	4	38	220
25	55	20	38	14	27	0	0.00	0.0	0	7.0	22	320	M	M	3	26	330
26	36	16	26	2	39	0	0.00	0.0	0	8.5	17	120	M	M	4 1	20	110
27	47	23	35	11	30	0	0.00	0.0	0	5.8	14	140	M	M	0 18	17	130
28	49	18	34	11	31	0	0.00	0.0	0	1.8	12	360	M	M	0 18	14	360
29	57	14	36	13	29	0	0.00	0.0	0	7.3	20	190	M	M	0 18	22	160
30	65	44	55	32	10	0	T	0.0	0	14.7	30	210	M	M	1	37	220
31	50	21	36	13	29	0	0.00	0.0	0	7.2	13	320	M	M	0	M	M

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SM	1336	576	1051	0	0.43	0.0	253.9	M	64
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AV	43.1	18.6	8.2	FASTST	PSBL	%	2	MAX (MPH)	
			MISC	---->	37	340		40	330

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NOTES:
 # LAST OF SEVERAL OCCURRENCES
 COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2
 STATION: LINCOLN
 MONTH: DECEMBER
 YEAR: 2004
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 30.8	TOTAL FOR MONTH: 0.43	1 = FOG
DPTR FM NORMAL: 4.3	DPTR FM NORMAL: -0.43	2 = FOG REDUCING VISIBILITY
HIGHEST: 65 ON 30	GRTST 24HR 0.42 ON 4- 5	TO 1/4 MILE OR LESS
LOWEST: -4 ON 24,23		3 = THUNDER
	SNOW, ICE PELLETS, HAIL	4 = ICE PELLETS
	TOTAL MONTH: 0.0 INCH	5 = HAIL
	GRTST 24HR 0.0	6 = GLAZE OR RIME
	GRTST DEPTH: 0	7 = BLOWING DUST OR SAND:

[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]
MAX 32 OR BELOW: 5	0.01 INCH OR MORE: 2
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 1
MIN 32 OR BELOW: 29	0.50 INCH OR MORE: 0
MIN 0 OR BELOW: 2	1.00 INCH OR MORE: 0
[HDD (BASE 65)]	
TOTAL THIS MO. 1051	CLEAR (SCALE 0-3) 24
DPTR FM NORMAL -137	PTCLDY (SCALE 4-7) 4
SEASONAL TOTAL 2111	CLOUDY (SCALE 8-10) 3
DPTR FM NORMAL -366	
[CDD (BASE 65)]	
TOTAL THIS MO. 0	
DPTR FM NORMAL 0	[PRESSURE DATA]
SEASONAL TOTAL 992	HIGHEST SLP 30.78 ON 14
DPTR FM NORMAL -162	LOWEST SLP 29.44 ON 20

VSBY 1/2 MILE OR LESS
8 = SMOKE OR HAZE
9 = BLOWING SNOW
X = TORNADO

STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2005
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:		SKY		:PK WND			
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG MX		2MIN						
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	45	23	34	11	31	0	T	0.0	0	13.3	21	340	M	M	10	1	24	350
2	29	15	22	-1	43	0	0.04	T	0	10.9	20	20	M	M	6	6	24	10
3	25	18	22	0	43	0	0.03	0.1	0	11.5	18	20	M	M	10	16	23	10
4	20	11	16	-6	49	0	0.34	2.5	T	16.6	29	20	M	M	10	16	32	20
5	11	4	8	-14	57	0	0.49	5.9	4	18.1	29	10	M	M	10	126	32	10
6	11	-8	2	-20	63	0	T	T	8	8.8	17	210	M	M	1	1	21	200
7	25	-1	12	-10	53	0	0.00	0.0	8	8.1	17	340	M	M	8	1	18	340
8	29	-9	10	-12	55	0	0.00	0.0	7	6.9	18	170	M	M	4	1	21	170
9	35	14	25	3	40	0	0.00	0.0	6	9.9	26	330	M	M	6	1	32	340
10	20	11	16	-6	49	0	0.00	0.0	5	10.0	16	20	M	M	7	18	21	60
11	22	17	20	-2	45	0	T	0.0	5	7.0	16	20	M	M	10	16	18	20
12	29	19	24	2	41	0	T	T	4	5.6	17	340	M	M	9	12	20	340
13	25	-6	10	-12	55	0	0.00	0.0	4	14.6	29	340	M	M	1		33	340
14	2	-7	-2	-24	67	0	0.10	2.0	5	7.6	14	10	M	M	10	1	16	10
15	4	-18	-7	-29	72	0	T	T	6	3.2	9	30	M	M	3		10	30
16	11	-18	-3	-25	68	0	0.00	0.0	6	1.2	6	20	M	M	1		6	330
17	24	-2	11	-11	54	0	0.00	0.0	6	6.4	16	170	M	M	4	18	18	170
18	39	6	23	1	42	0	0.00	0.0	6	15.0	31	210	M	M	1	18	39	200
19	41	26	34	12	31	0	0.00	0.0	4	6.2	14	310	M	M	0		16	310
20	48	27	38	16	27	0	0.00	0.0	2	4.9	16	30	M	M	1	1	20	30
21	38	27	33	11	32	0	0.00	0.0	T	13.9	41	340	M	M	10	1	52	340
22	27	5	16	-6	49	0	T	T	0	17.8	39	340	M	M	2	19	45	340

23	30	10	20	-2	45	0	0.00	0.0	0	13.3	25	190	M	M	3	29	210
24	55	22	39	16	26	0	0.00	0.0	0	2.7	13	210	M	M	0	15	210
25	58	26	42	19	23	0	0.00	0.0	0	5.4	14	350	M	M	0 1	16	350
26	36	26	31	8	34	0	0.00	0.0	0	11.3	20	20	M	M	8	25	20
27	32	25	29	6	36	0	0.00	0.0	0	10.9	16	130	M	M	10 18	21	140
28	36	27	32	9	33	0	T	T	0	8.8	15	150	M	M	8 18	17	150
29	39	26	33	10	32	0	T	T	0	2.6	8	40	M	M	9 18	9	40
30	36	32	34	10	31	0	0.03	T	0	2.1	7	150	M	M	10 1	7	130
31	40	32	36	12	29	0	T	0.0	0	1.5	9	140	M	M	10 128	13	120

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SM	922	380	1355	0	1.03	10.5	276.1		M	182
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AV	29.7	12.3				8.9	FASTST	PSBL	%	6	MAX (MPH)
						MISC	---->	41	340		52 340

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NOTES:

LAST OF SEVERAL OCCURRENCES
 COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2005
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 21.0	TOTAL FOR MONTH: 1.03	1 = FOG
DPTR FM NORMAL: -1.4	DPTR FM NORMAL: 0.36	2 = FOG REDUCING VISIBILITY
HIGHEST: 58 ON 25	GRTST 24HR 0.49 ON 5- 5	TO 1/4 MILE OR LESS
LOWEST: -18 ON 16,15		3 = THUNDER
	SNOW, ICE PELLETS, HAIL	4 = ICE PELLETS
	TOTAL MONTH: 10.5 INCHES	5 = HAIL
	GRTST 24HR 5.9 ON 5- 5	6 = GLAZE OR RIME
	GRTST DEPTH: 8 ON 7, 6	7 = BLOWING DUST OR SAND:

[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]	
MAX 32 OR BELOW: 18	0.01 INCH OR MORE: 6	VSBY 1/2 MILE OR LESS
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 3	8 = SMOKE OR HAZE
MIN 32 OR BELOW: 31	0.50 INCH OR MORE: 0	9 = BLOWING SNOW
MIN 0 OR BELOW: 8	1.00 INCH OR MORE: 0	X = TORNADO
[HDD (BASE 65)]		
TOTAL THIS MO. 1355	CLEAR (SCALE 0-3) 11	
DPTR FM NORMAL 27	PTCLDY (SCALE 4-7) 5	
SEASONAL TOTAL 3466	CLOUDY (SCALE 8-10) 15	
DPTR FM NORMAL -339		
[CDD (BASE 65)]		
TOTAL THIS MO. 0		
DPTR FM NORMAL 0	[PRESSURE DATA]	
SEASONAL TOTAL 0	HIGHEST SLP 30.97 ON 15	
DPTR FM NORMAL 0	LOWEST SLP 29.54 ON 12	

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2005
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:		SKY		:PK WND			
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG MX		2MIN						
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	41	28	35	11	30	0	0.00	0.0	0	5.0	10	150	M	M	10	18	12	170
2	47	23	35	11	30	0	0.00	0.0	0	4.6	15	180	M	M	1	18	17	180
3	61	23	42	17	23	0	0.00	0.0	0	6.3	15	230	M	M	0	18	17	240
4	63	23	43	18	22	0	0.00	0.0	0	9.3	21	220	M	M	0		25	210
5	62	38	50	25	15	0	0.00	0.0	0	19.7	38	200	M	M	1		44	190
6	49	23	36	10	29	0	0.87	2.2	0	15.5	26	10	M	M	10	1	31	10
7	23	10	17	-9	48	0	0.04	1.0	3	13.5	28	10	M	M	9	1	32	10
8	15	9	12	-14	53	0	0.18	1.4	3	9.2	18	40	M	M	10	12	20	40
9	22	-5	9	-17	56	0	0.00	0.0	4	3.1	12	240	M	M	2	128	13	240
10	35	5	20	-7	45	0	0.00	0.0	4	4.3	16	250	M	M	1	1	20	250
11	46	12	29	2	36	0	0.00	0.0	3	3.6	14	220	M	M	0	1	16	220
12	42	23	33	6	32	0	0.64	0.0	2	5.3	12	120	M	M	4	128	14	150
13	45	39	42	14	23	0	0.43	0.0	0	10.3	24	310	M	M	10	1	28	320
14	66	27	47	19	18	0	0.00	0.0	0	6.7	21	360	M	M	1	18	25	10
15	40	25	33	5	32	0	0.00	0.0	0	10.4	20	10	M	M	6		25	20
16	45	17	31	2	34	0	0.00	0.0	0	7.1	25	290	M	M	1	1	29	320
17	49	18	34	5	31	0	0.00	0.0	0	5.2	17	290	M	M	0		21	270
18	45	16	31	2	34	0	0.00	0.0	0	5.8	18	10	M	M	1		22	10
19	43	35	39	9	26	0	0.01	T	0	11.2	18	150	M	M	10	1	21	150
20	47	32	40	10	25	0	0.03	0.0	0	10.2	23	310	M	M	10	12	28	310
21	42	29	36	6	29	0	T	0.0	0	7.7	16	80	M	M	9	18	18	90
22	50	28	39	8	26	0	0.00	0.0	0	6.4	15	30	M	M	6	18	17	30

23	42	25	34	3	31	0	0.00	0.0	0	4.5	9	190	M	M	7	18	12	50
24	43	25	34	3	31	0	0.00	0.0	0	8.1	22	340	M	M	3	8	26	330
25	60	25	43	11	22	0	0.00	0.0	0	5.5	15	10	M	M	0		18	10
26	60	21	41	9	24	0	0.00	0.0	0	8.8	20	170	M	M	1	18	23	180
27	50	24	37	4	28	0	0.02	0.0	0	11.8	26	340	M	M	2	18	30	330
28	29	17	23	-10	42	0	T	0.0	0	14.4	29	340	M	M	5	18	32	330

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SM 1262 615 875 0 2.22 4.6 233.5 M 120

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AV 45.1 22.0 8.3 FASTST PSBL % 4 MAX(MPH)

MISC ----> 38 200 44 190

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NOTES:

LAST OF SEVERAL OCCURRENCES
 COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2005
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 33.5	TOTAL FOR MONTH: 2.22	1 = FOG
DPTR FM NORMAL: 5.2	DPTR FM NORMAL: 1.56	2 = FOG REDUCING VISIBILITY
HIGHEST: 66 ON 14	GRTST 24HR 1.07 ON 12-13	TO 1/4 MILE OR LESS
LOWEST: -5 ON 9		3 = THUNDER
	SNOW, ICE PELLETS, HAIL	4 = ICE PELLETS
	TOTAL MONTH: 4.6 INCHES	5 = HAIL
	GRTST 24HR 2.2 ON 6- 6	6 = GLAZE OR RIME
	GRTST DEPTH: 4 ON 10, 9	7 = BLOWING DUST OR SAND:
		VSBY 1/2 MILE OR LESS
		8 = SMOKE OR HAZE
[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]	9 = BLOWING SNOW

X = TORNADO

MAX 32 OR BELOW:	4	0.01 INCH OR MORE:	8
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	4
MIN 32 OR BELOW:	25	0.50 INCH OR MORE:	2
MIN 0 OR BELOW:	1	1.00 INCH OR MORE:	0
[HDD (BASE 65)]			
TOTAL THIS MO.	875	CLEAR (SCALE 0-3)	15
DPTR FM NORMAL	-168	PTCLDY (SCALE 4-7)	5
SEASONAL TOTAL	4341	CLOUDY (SCALE 8-10)	8
DPTR FM NORMAL	-507		
[CDD (BASE 65)]			
TOTAL THIS MO.	0		
DPTR FM NORMAL	0	[PRESSURE DATA]	
SEASONAL TOTAL	0	HIGHEST SLP 30.44 ON	18
DPTR FM NORMAL	0	LOWEST SLP 29.44 ON	13

STATION: LINCOLN
 MONTH: MARCH
 YEAR: 2005
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND			:SUNSHINE:			SKY		:PK WND		
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18	
										AVG MX		2MIN							
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR	
1	43	13	28	-5	37	0	0.00	0.0	0	4.8	10	340	M	M	0		13	360	
2	58	21	40	6	25	0	0.00	0.0	0	4.4	12	40	M	M	2		14	190	
3	57	21	39	5	26	0	0.00	0.0	0	4.1	12	40	M	M	3	18	12	40	
4	64	22	43	8	22	0	0.00	0.0	0	9.0	28	330	M	M	0		31	340	
5	61	22	42	7	23	0	0.00	0.0	0	6.7	13	240	M	M	0		18	260	
6	73	36	55	20	10	0	0.00	0.0	0	15.3	35	220	M	M	1		40	200	
7	54	22	38	2	27	0	0.00	0.0	0	20.5	35	340	M	M	6		41	360	
8	40	20	30	-6	35	0	T	0.0	0	3.3	12	30	M	M	7		13	20	
9	45	28	37	0	28	0	T	T	0	8.5	16	200	M	M	7		20	190	
10	58	32	45	8	20	0	T	0.0	0	24.5	48	340	M	M	3		56	320	
11	64	27	46	9	19	0	0.00	0.0	0	10.6	31	290	M	M	4		38	290	
12	47	27	37	-1	28	0	0.00	0.0	0	9.2	28	20	M	M	1		32	20	
13	48	17	33	-5	32	0	0.00	0.0	0	7.5	26	330	M	M	3		32	320	
14	44	16	30	-9	35	0	0.00	0.0	0	4.3	15	260	M	M	6		18	270	
15	54	14	34	-5	31	0	0.00	0.0	0	7.9	23	230	M	M	3		30	190	
16	62	20	41	2	24	0	T	0.0	0	9.8	22	250	M	M	1		25	200	
17	64	36	50	10	15	0	0.00	0.0	0	16.2	29	200	M	M	3		36	200	
18	49	29	39	-1	26	0	0.00	0.0	0	18.9	28	340	M	M	6	8	33	330	
19	48	25	37	-4	28	0	0.00	0.0	0	11.3	28	340	M	M	5		33	350	
20	55	26	41	0	24	0	0.01	0.0	0	12.1	20	100	M	M	4	8	25	90	
21	54	40	47	6	18	0	0.05	0.0	0	18.5	30	100	M	M	10	8	40	80	
22	42	33	38	-4	27	0	0.30	T	0	13.2	24	80	M	M	10	18	29	90	

23	54	32	43	1	22	0	0.00	0.0	0	7.8	14	150	M	M	5	18	18	160
24	43	35	39	-4	26	0	0.19	0.0	0	10.1	16	20	M	M	10	1	18	20
25	39	34	37	-6	28	0	0.08	T	0	10.0	18	10	M	M	10	1	22	10
26	49	28	39	-4	26	0	0.00	0.0	0	3.2	12	310	M	M	7	18	15	320
27	61	24	43	-1	22	0	0.00	0.0	0	5.1	15	260	M	M	0	18	18	240
28	75	36	56	12	9	0	0.00	0.0	0	11.6	26	210	M	M	0		31	170
29	78	53	66	21	0	1	0.00	0.0	0	13.9	22	170	M	M	1		28	210
30	62	35	49	4	16	0	0.02	0.0	0	14.2	38	350	M	M	5	13	46	360
31	61	29	45	0	20	0	0.00	0.0	0	10.3	21	360	M	M	0		26	20

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SM	1706	853		729	1	0.65	T		326.8		M		123					
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AV	55.0	27.5							10.5	FASTST	PSBL	%	4		MAX (MPH)			
								MISC	---->	48	340				56	320		

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NOTES:

LAST OF SEVERAL OCCURRENCES
 COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: MARCH
 YEAR: 2005
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]
 AVERAGE MONTHLY: 41.3
 DPTR FM NORMAL: 1.9
 HIGHEST: 78 ON 29
 LOWEST: 13 ON 1

[PRECIPITATION DATA]
 TOTAL FOR MONTH: 0.65
 DPTR FM NORMAL: -1.56
 GRTST 24HR 0.30 ON 22-22
 SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: T
 GRTST 24HR T ON 25-25
 GRTST DEPTH: 0

SYMBOLS USED IN COLUMN 16
 1 = FOG
 2 = FOG REDUCING VISIBILITY
 TO 1/4 MILE OR LESS
 3 = THUNDER
 4 = ICE PELLETS
 5 = HAIL
 6 = GLAZE OR RIME
 7 = BLOWING DUST OR SAND:

[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]	
MAX 32 OR BELOW: 0	0.01 INCH OR MORE: 6	VSBY 1/2 MILE OR LESS
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 2	8 = SMOKE OR HAZE
MIN 32 OR BELOW: 22	0.50 INCH OR MORE: 0	9 = BLOWING SNOW
MIN 0 OR BELOW: 0	1.00 INCH OR MORE: 0	X = TORNADO
[HDD (BASE 65)]		
TOTAL THIS MO. 729	CLEAR (SCALE 0-3) 16	
DPTR FM NORMAL -70	PTCLDY (SCALE 4-7) 11	
SEASONAL TOTAL 5070	CLOUDY (SCALE 8-10) 4	
DPTR FM NORMAL -577		
[CDD (BASE 65)]		
TOTAL THIS MO. 1		
DPTR FM NORMAL 0	[PRESSURE DATA]	
SEASONAL TOTAL 1	HIGHEST SLP 30.32 ON 5	
DPTR FM NORMAL 0	LOWEST SLP 29.21 ON 30	

STATION: LINCOLN
 MONTH: DECEMBER
 YEAR: 2005
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND			:SUNSHINE:			SKY		:PK WND	
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG		MX		2MIN				
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	23	12	18	-13	47	0	0.00	0.0	1	7.3	26	340	M	M	2	189	32	340
2	26	18	22	-9	43	0	0.00	0.0	1	11.0	21	110	M	M	6		25	110
3	21	5	13	-17	52	0	0.23	2.8	1	9.7	16	350	M	M	5	1289	20	340
4	17	-2	8	-22	57	0	0.00	0.0	2	5.4	15	10	M	M	5	18	16	10
5	28	-3	13	-17	52	0	0.09	1.8	2	12.2	35	290	M	M	3	1289	45	290
6	9	-4	3	-26	62	0	T	T	3	7.9	22	340	M	M	2	8	24	340
7	9	-6	2	-27	63	0	0.07	1.1	3	8.5	13	360	M	M	6	1	14	20
8	12	-5	4	-25	61	0	0.02	0.3	4	5.9	14	290	M	M	4	18	16	300
9	21	-10	6	-22	59	0	0.00	0.0	4	7.1	16	210	M	M	0		22	210
10	40	16	28	0	37	0	T	0.0	4	12.1	25	310	M	M	7		32	310
11	46	29	38	10	27	0	0.00	0.0	1	10.5	20	270	M	M	2		23	280
12	45	24	35	8	30	0	0.00	0.0	T	8.1	16	310	M	M	0	1	20	310
13	44	23	34	7	31	0	0.06	0.0	T	12.7	28	170	M	M	4	12	37	150
14	42	32	37	10	28	0	0.01	T	0	13.2	26	290	M	M	8	1	33	300
15	33	27	30	3	35	0	T	T	0	18.3	33	300	M	M	6	1	39	320
16	28	17	23	-3	42	0	T	T	0	12.3	28	310	M	M	5		35	300
17	27	16	22	-4	43	0	0.00	0.0	0	5.8	14	10	M	M	7		16	20
18	22	7	15	-11	50	0	0.00	0.0	0	7.1	15	20	M	M	2		17	310
19	31	5	18	-7	47	0	0.00	0.0	0	7.3	17	230	M	M	2		21	220

20	37	11	24	-1	41	0	0.00	0.0	0	3.3	12	220	M	M	1	18	13	220
21	44	11	28	3	37	0	0.00	0.0	0	6.3	10	190	M	M	0	18	12	190
22	58	25	42	17	23	0	0.00	0.0	0	9.2	20	210	M	M	0	18	22	200
23	49	28	39	15	26	0	0.01	0.0	0	7.4	23	320	M	M	2		29	330
24	49	28	39	15	26	0	0.02	0.0	0	14.7	26	340	M	M	6		32	340
25	36	18	27	3	38	0	0.00	0.0	0	3.8	9	160	M	M	6	12	10	70
26	58	26	42	18	23	0	0.00	0.0	0	5.9	14	160	M	M	3	1	16	160
27	40	21	31	7	34	0	0.00	0.0	0	8.1	18	360	M	M	4	128	23	10
28	53	23	38	15	27	0	0.00	0.0	0	9.6	21	330	M	M	5	8	25	340
29	37	23	30	7	35	0	0.01	0.0	0	6.5	17	130	M	M	8	12	21	130
30	41	24	33	10	32	0	0.00	0.0	0	13.1	30	290	M	M	5	1	36	300
31	46	18	32	9	33	0	0.00	0.0	0	5.7	16	170	M	M	0		18	170

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SM 1072 457 1241 0 0.52 6.0 276.0 M 116

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AV 34.6 14.7 8.9 FASTST PSBL % 4 MAX (MPH)

MISC ----> 35 290 45 290

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NOTES:
LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
MONTH: DECEMBER
YEAR: 2005
LATITUDE: 40 50 N
LONGITUDE: 96 45 W

[TEMPERATURE DATA] [PRECIPITATION DATA] SYMBOLS USED IN COLUMN 16

AVERAGE MONTHLY: 24.7 TOTAL FOR MONTH: 0.52 1 = FOG OR MIST

DPTR FM NORMAL: -1.8 DPTR FM NORMAL: -0.34
 HIGHEST: 58 ON 26,22 GRTST 24HR 0.23 ON 3- 3
 LOWEST: -10 ON 9

SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: 6.0 INCHES
 GRTST 24HR 2.8 ON 3- 3
 GRTST DEPTH: 4 ON 10, 9

- 2 = FOG REDUCING VISIBILITY TO 1/4 MILE OR LESS
- 3 = THUNDER
- 4 = ICE PELLETS
- 5 = HAIL
- 6 = FREEZING RAIN OR DRIZZLE
- 7 = DUSTSTORM OR SANDSTORM: VSBY 1/2 MILE OR LESS
- 8 = SMOKE OR HAZE
- 9 = BLOWING SNOW
- X = TORNADO

[NO. OF DAYS WITH]

MAX 32 OR BELOW: 13
 MAX 90 OR ABOVE: 0
 MIN 32 OR BELOW: 31
 MIN 0 OR BELOW: 6

[WEATHER - DAYS WITH]

0.01 INCH OR MORE: 9
 0.10 INCH OR MORE: 1
 0.50 INCH OR MORE: 0
 1.00 INCH OR MORE: 0

[HDD (BASE 65)]

TOTAL THIS MO. 1241
 DPTR FM NORMAL 53
 TOTAL FM JUL 1 2319
 DPTR FM NORMAL -158

CLEAR (SCALE 0-3) 14
 PTCLDY (SCALE 4-7) 15
 CLOUDY (SCALE 8-10) 2

[CDD (BASE 65)]

TOTAL THIS MO. 0
 DPTR FM NORMAL 0
 TOTAL FM JAN 1 1432
 DPTR FM NORMAL 278

[PRESSURE DATA]

HIGHEST SLP 30.80 ON 18
 LOWEST SLP 29.57 ON 29

STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2006
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND			:SUNSHINE:			SKY		:PK WND	
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG		MX		2MIN				
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	54	29	42	19	23	0	0.01	0.0	0	12.2	23	20	M	M	3	18	28	10
2	39	22	31	8	34	0	0.21	T	0	11.2	32	350	M	M	7	18	37	350
3	51	28	40	18	25	0	0.00	0.0	0	10.5	29	320	M	M	5	128	33	320
4	54	36	45	23	20	0	0.00	0.0	0	14.2	24	320	M	M	2		29	320
5	45	20	33	11	32	0	0.00	0.0	0	9.0	24	340	M	M	0	1	28	340
6	49	14	32	10	33	0	0.00	0.0	0	5.4	23	230	M	M	0	1	26	240
7	54	26	40	18	25	0	0.00	0.0	0	4.5	10	10	M	M	0		12	10
8	38	20	29	7	36	0	0.00	0.0	0	12.2	26	330	M	M	6	18	31	330
9	35	21	28	6	37	0	0.00	0.0	0	9.1	24	10	M	M	10	18	32	20
10	45	16	31	9	34	0	0.00	0.0	0	6.4	14	170	M	M	0	18	16	180
11	62	24	43	21	22	0	0.00	0.0	0	8.7	17	220	M	M	0		20	220
12	55	24	40	18	25	0	T	0.0	0	15.0	37	340	M	M	3		43	10
13	43	20	32	10	33	0	0.00	0.0	0	13.0	31	330	M	M	5		38	330
14	59	17	38	16	27	0	0.00	0.0	0	8.6	20	180	M	M	0		23	170
15	69	33	51	29	14	0	0.00	0.0	0	6.1	13	160	M	M	0		15	220
16	44	31	38	16	27	0	T	T	0	20.0	33	340	M	M	8		38	340
17	40	18	29	7	36	0	0.00	0.0	0	9.5	26	330	M	M	1		32	340
18	63	17	40	18	25	0	0.00	0.0	0	6.9	21	200	M	M	2		23	200
19	46	24	35	13	30	0	0.00	0.0	0	9.1	24	340	M	M	2		28	340
20	34	20	27	5	38	0	0.01	T	0	8.1	17	10	M	M	8	18	20	350

21	52	16	34	12	31	0	0.00	0.0	0	9.5	28	200	M	M	0	1	32	190
22	36	17	27	5	38	0	0.00	0.0	0	8.4	21	10	M	M	5	18	24	10
23	50	23	37	15	28	0	0.00	0.0	0	11.6	24	210	M	M	5	18	30	210
24	54	18	36	13	29	0	0.00	0.0	0	11.9	33	310	M	M	0		41	310
25	55	15	35	12	30	0	0.00	0.0	0	7.1	18	180	M	M	0		21	180
26	62	30	46	23	19	0	T	0.0	0	21.4	37	190	M	M	3		44	190
27	60	37	49	26	16	0	0.00	0.0	0	10.3	26	190	M	M	1		33	200
28	48	38	43	20	22	0	0.68	0.0	0	8.6	20	310	M	M	9	138	22	310
29	48	27	38	15	27	0	0.00	0.0	0	7.8	18	300	M	M	2		22	300
30	41	23	32	8	33	0	0.00	0.0	0	7.8	18	330	M	M	2	1	23	330
31	63	24	44	20	21	0	0.00	0.0	0	8.5	28	330	M	M	1	1	33	320

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SM 1548 728 870 0 0.91 T 312.6 M 90

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AV 49.9 23.5 10.1 FASTST PSBL % 3 MAX (MPH)

MISC ----> # 37 190 44 190

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NOTES:

LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2006
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 36.7	TOTAL FOR MONTH: 0.91	1 = FOG OR MIST
DPTR FM NORMAL: 14.3	DPTR FM NORMAL: 0.24	2 = FOG REDUCING VISIBILITY

HIGHEST:	69 ON 15	GRTST 24HR	0.68 ON 28-28	TO 1/4 MILE OR LESS
LOWEST:	14 ON 6			3 = THUNDER
		SNOW, ICE PELLETS, HAIL		4 = ICE PELLETS
		TOTAL MONTH:	T	5 = HAIL
		GRTST 24HR	T ON 20-20	6 = FREEZING RAIN OR DRIZZLE
		GRTST DEPTH:	0	7 = DUSTSTORM OR SANDSTORM: VSBY 1/2 MILE OR LESS

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW:	0	0.01 INCH OR MORE:	4
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	2
MIN 32 OR BELOW:	27	0.50 INCH OR MORE:	1
MIN 0 OR BELOW:	0	1.00 INCH OR MORE:	0

[HDD (BASE 65)]

TOTAL THIS MO.	870	CLEAR (SCALE 0-3)	21
DPTR FM NORMAL	-458	PTCLDY (SCALE 4-7)	6
TOTAL FM JUL 1	3189	CLOUDY (SCALE 8-10)	4
DPTR FM NORMAL	-616		

[CDD (BASE 65)]

TOTAL THIS MO.	0		
DPTR FM NORMAL	0	[PRESSURE DATA]	
TOTAL FM JAN 1	0	HIGHEST SLP 30.54 ON 25	
DPTR FM NORMAL	0	LOWEST SLP 29.59 ON 28	

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2006
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND			:SUNSHINE:			SKY		:PK WND	
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG		MX		2MIN				
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	53	28	41	17	24	0	0.00	0.0	0	7.8	14	240	M	M	2		16	230
2	59	26	43	19	22	0	0.00	0.0	0	6.0	20	330	M	M	1		23	340
3	40	20	30	5	35	0	0.00	0.0	0	13.1	28	340	M	M	3		35	340
4	36	14	25	0	40	0	0.00	0.0	0	9.4	20	340	M	M	0		22	10
5	36	13	25	0	40	0	0.00	0.0	0	6.9	15	70	M	M	5		17	80
6	44	12	28	2	37	0	0.00	0.0	0	6.1	20	320	M	M	6		23	330
7	46	21	34	8	31	0	0.00	0.0	0	7.2	16	10	M	M	8		20	20
8	34	13	24	-2	41	0	T	T	0	10.9	22	10	M	M	5 8		24	20
9	41	14	28	2	37	0	0.00	0.0	0	10.8	24	200	M	M	2		32	200
10	39	24	32	5	33	0	T	T	0	16.5	32	330	M	M	5 8		39	310
11	27	15	21	-6	44	0	T	0.1	T	15.8	26	340	M	M	9 18		32	340
12	30	11	21	-6	44	0	T	T	T	12.1	29	340	M	M	6		35	340
13	61	11	36	8	29	0	0.00	0.0	T	9.9	24	330	M	M	0		31	300
14	68	20	44	16	21	0	0.00	0.0	0	10.3	28	340	M	M	0		33	340
15	41	26	34	6	31	0	0.00	0.0	0	16.4	28	60	M	M	4		33	60
16	26	10	18	-11	47	0	0.07	0.6	0	17.4	28	350	M	M	7 168		32	340
17	11	0	6	-23	59	0	T	T	T	16.1	24	10	M	M	5		29	10
18	14	-4	5	-24	60	0	0.00	0.0	T	4.8	16	10	M	M	1		18	20
19	28	1	15	-15	50	0	0.00	0.0	T	8.4	15	210	M	M	3		17	220
20	47	9	28	-2	37	0	0.00	0.0	T	9.5	22	250	M	M	0		25	260

21	51	12	32	2	33	0	0.00	0.0	T	5.8	18	220	M	M	1	23	210
22	53	13	33	2	32	0	0.00	0.0	0	8.5	29	290	M	M	0	36	300
23	48	21	35	4	30	0	0.00	0.0	0	5.7	15	70	M	M	0	16	80
24	65	18	42	11	23	0	0.00	0.0	0	11.3	30	10	M	M	0	36	10
25	36	18	27	-5	38	0	0.00	0.0	0	12.2	29	10	M	M	7	35	10
26	53	9	31	-1	34	0	0.00	0.0	0	8.6	22	200	M	M	0	26	200
27	71	27	49	16	16	0	0.00	0.0	0	5.1	13	210	M	M	0 8	15	210
28	73	26	50	17	15	0	0.00	0.0	0	4.1	12	160	M	M	0 8	14	160

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SM 1231 428          983 0 0.07      0.7 276.7          M          80
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AV 44.0 15.3                9.9 FASTST PSBL % 3      MAX (MPH)
                               MISC ----> 32 330                39 310
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NOTES:
LAST OF SEVERAL OCCURRENCES
COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
MONTH: FEBRUARY
YEAR: 2006
LATITUDE: 40 50 N
LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 29.6	TOTAL FOR MONTH: 0.07	1 = FOG OR MIST
DPTR FM NORMAL: 1.3	DPTR FM NORMAL: -0.59	2 = FOG REDUCING VISIBILITY
HIGHEST: 73 ON 28	GRTST 24HR 0.07 ON 16-16	TO 1/4 MILE OR LESS
LOWEST: -4 ON 18		3 = THUNDER
	SNOW, ICE PELLETS, HAIL	4 = ICE PELLETS

TOTAL MONTH: 0.7 INCH 5 = HAIL
 GRST 24HR 0.6 ON 16-16 6 = FREEZING RAIN OR DRIZZLE
 GRST DEPTH: 0 7 = DUSTSTORM OR SANDSTORM:
 VSBY 1/2 MILE OR LESS
 8 = SMOKE OR HAZE
 9 = BLOWING SNOW
 X = TORNADO

[NO. OF DAYS WITH]	[WEATHER - DAYS WITH]
MAX 32 OR BELOW: 6	0.01 INCH OR MORE: 1
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 0
MIN 32 OR BELOW: 28	0.50 INCH OR MORE: 0
MIN 0 OR BELOW: 2	1.00 INCH OR MORE: 0

[HDD (BASE 65)]	
TOTAL THIS MO. 983	CLEAR (SCALE 0-3) 17
DPTR FM NORMAL -60	PTCLDY (SCALE 4-7) 9
TOTAL FM JUL 1 4172	CLOUDY (SCALE 8-10) 2
DPTR FM NORMAL -676	

[CDD (BASE 65)]	
TOTAL THIS MO. 0	
DPTR FM NORMAL 0	[PRESSURE DATA]
TOTAL FM JAN 1 0	HIGHEST SLP 30.96 ON 17
DPTR FM NORMAL 0	LOWEST SLP 29.54 ON 2

STATION: LINCOLN
 MONTH: MARCH
 YEAR: 2006
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:			SKY		:PK WND		
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG		MX		2MIN				
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	76	35	56	23	9	0	0.00	0.0	0	10.4	31	330	M	M	0	8	37	330
2	47	21	34	0	31	0	0.00	0.0	0	12.4	23	360	M	M	0		29	340
3	49	14	32	-2	33	0	T	0.0	0	5.9	14	120	M	M	2		17	120
4	47	36	42	7	23	0	0.04	T	0	14.8	25	140	M	M	9	138	30	140
5	60	28	44	9	21	0	0.25	0.0	0	9.2	28	340	M	M	2	138	31	340
6	56	23	40	5	25	0	0.00	0.0	0	7.7	16	130	M	M	0		18	140
7	70	34	52	16	13	0	0.00	0.0	0	12.2	23	150	M	M	2	1	28	150
8	44	30	37	1	28	0	0.07	0.0	0	13.3	25	20	M	M	7	18	30	20
9	56	34	45	8	20	0	0.00	0.0	0	6.1	17	340	M	M	4		22	340
10	62	29	46	9	19	0	0.00	0.0	0	11.4	26	150	M	M	1		32	140
11	55	30	43	6	22	0	0.00	0.0	0	10.0	24	310	M	M	1	1	29	310
12	42	34	38	0	27	0	0.16	T	0	12.7	21	10	M	M	8	135	25	40
13	40	24	32	-6	33	0	0.05	T	0	17.9	35	330	M	M	6	1	40	330
14	56	17	37	-2	28	0	0.00	0.0	0	6.9	22	290	M	M	0	18	28	310
15	66	20	43	4	22	0	T	0.0	0	15.4	37	180	M	M	1		43	170
16	50	30	40	1	25	0	0.00	0.0	0	20.3	37	310	M	M	7		47	310
17	44	28	36	-4	29	0	0.00	0.0	0	7.3	18	20	M	M	7		22	10
18	41	32	37	-3	28	0	0.07	T	0	12.8	25	120	M	M	10	1	29	120
19	40	31	36	-5	29	0	0.43	2.6	T	15.0	29	90	M	M	10	12	33	90
20	34	30	32	-9	33	0	0.75	6.5	3	17.4	28	90	M	M	10	12	35	90

21	32	23	28	-13	37	0	0.09	0.8	9	11.8	21	40	M	M	10	168	24	30
22	31	23	27	-15	38	0	0.00	0.0	8	6.7	10	330	M	M	5	18	13	330
23	34	17	26	-16	39	0	0.00	0.0	6	10.5	17	330	M	M	0		20	320
24	35	17	26	-17	39	0	0.00	0.0	4	7.0	14	10	M	M	2		16	300
25	39	20	30	-13	35	0	0.00	0.0	3	2.6	9	90	M	M	6	1	10	90
26	53	29	41	-2	24	0	0.04	0.0	1	16.4	32	130	M	M	2		40	130
27	46	38	42	-2	23	0	0.05	0.0	T	13.9	26	330	M	M	8	18	33	140
28	53	37	45	1	20	0	0.00	0.0	0	7.6	16	320	M	M	6	18	20	320
29	75	39	57	12	8	0	0.04	0.0	0	19.9	32	170	M	M	3	18	39	180
30	67	50	59	14	6	0	0.99	0.0	0	16.3	44	210	M	M	6	1238	55	240
31	59	38	49	4	16	0	0.00	0.0	0	16.2	32	290	M	M	4		39	300

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SM 1559 891 783 0 3.03 9.9 368.0 M 139

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AV 50.3 28.7 11.9 FASTST PSBL % 4 MAX (MPH)

MISC ----> 44 210 55 240

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NOTES:

LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: MARCH
 YEAR: 2006
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA] [PRECIPITATION DATA] SYMBOLS USED IN COLUMN 16

AVERAGE MONTHLY: 39.5 TOTAL FOR MONTH: 3.03 1 = FOG OR MIST
 DPTR FM NORMAL: 0.1 DPTR FM NORMAL: 0.82 2 = FOG REDUCING VISIBILITY

HIGHEST:	76 ON 1	GRTST 24HR 0.99 ON 30-30	TO 1/4 MILE OR LESS
LOWEST:	14 ON 3		3 = THUNDER
		SNOW, ICE PELLETS, HAIL	4 = ICE PELLETS
		TOTAL MONTH: 9.9 INCHES	5 = HAIL
		GRTST 24HR 6.5 ON 20-20	6 = FREEZING RAIN OR DRIZZLE
		GRTST DEPTH: 9 ON 21	7 = DUSTSTORM OR SANDSTORM:
			VSBY 1/2 MILE OR LESS

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW:	2	0.01 INCH OR MORE:	13
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	5
MIN 32 OR BELOW:	21	0.50 INCH OR MORE:	2
MIN 0 OR BELOW:	0	1.00 INCH OR MORE:	0

[HDD (BASE 65)]

TOTAL THIS MO.	783	CLEAR (SCALE 0-3)	14
DPTR FM NORMAL	-16	PTCLDY (SCALE 4-7)	10
TOTAL FM JUL 1	4955	CLOUDY (SCALE 8-10)	7
DPTR FM NORMAL	-692		

[CDD (BASE 65)]

TOTAL THIS MO.	0		
DPTR FM NORMAL	-1	[PRESSURE DATA]	
TOTAL FM JAN 1	0	HIGHEST SLP 30.55 ON	17
DPTR FM NORMAL	-1	LOWEST SLP 29.34 ON	9

STATION: LINCOLN
 MONTH: DECEMBER
 YEAR: 2006
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:			SKY		:PK WND		
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	42	3	23	-8	42	0	0.00	0.0	0	4.6	18	310	M	M	1		22	310
2	30	10	20	-11	45	0	0.00	0.0	0	9.8	24	330	M	M	0		28	310
3	24	4	14	-16	51	0	0.00	0.0	0	8.0	22	210	M	M	0		26	200
4	44	19	32	2	33	0	0.00	0.0	0	7.1	22	210	M	M	3		26	210
5	61	21	41	11	24	0	0.00	0.0	0	8.6	21	230	M	M	0		24	220
6	51	15	33	4	32	0	0.00	0.0	0	13.9	33	350	M	M	1		39	350
7	21	4	13	-16	52	0	0.00	0.0	0	8.4	26	360	M	M	1		33	360
8	44	10	27	-2	38	0	0.00	0.0	0	11.9	18	200	M	M	0		22	210
9	58	27	43	15	22	0	0.00	0.0	0	12.5	25	200	M	M	0		32	210
10	54	30	42	14	23	0	0.00	0.0	0	13.3	24	190	M	M	0	1	30	180
11	51	21	36	8	29	0	0.03	0.0	0	6.9	17	340	M	M	8	18	20	330
12	42	27	35	8	30	0	0.00	0.0	0	8.1	15	320	M	M	6	18	18	320
13	60	23	42	15	23	0	0.00	0.0	0	7.4	20	210	M	M	0		25	220
14	59	33	46	19	19	0	0.00	0.0	0	8.3	21	210	M	M	2		25	270
15	52	23	38	11	27	0	0.00	0.0	0	6.1	16	170	M	M	2		18	180
16	52	32	42	16	23	0	0.00	0.0	0	7.0	20	10	M	M	0	18	23	10
17	42	22	32	6	33	0	0.00	0.0	0	6.2	20	20	M	M	5		23	20
18	44	14	29	3	36	0	0.00	0.0	0	1.6	8	350	M	M	2	8	10	350
19	47	13	30	5	35	0	0.00	0.0	0	4.2	13	180	M	M	3		15	180
20	41	32	37	12	28	0	0.37	T	0	10.3	22	30	M	M	10	18	25	30

21	45	35	40	15	25	0	0.21	0.0	0	5.6	13	330	M	M	9	128	15	340
22	38	30	34	9	31	0	0.06	T	0	10.5	16	320	M	M	8	1	20	320
23	45	21	33	9	32	0	0.00	0.0	0	5.1	14	300	M	M	0		17	300
24	48	19	34	10	31	0	0.00	0.0	0	8.9	23	340	M	M	2		28	340
25	38	20	29	5	36	0	0.00	0.0	0	10.9	22	330	M	M	1		26	340
26	47	16	32	8	33	0	0.00	0.0	0	5.8	17	260	M	M	3		21	260
27	53	25	39	15	26	0	0.00	0.0	0	9.0	20	200	M	M	1		23	190
28	45	23	34	11	31	0	0.00	0.0	0	4.3	13	100	M	M	2		14	100
29	42	37	40	17	25	0	0.36	0.0	0	9.2	18	10	M	M	10	1	22	10
30	52	35	44	21	21	0	1.17	T	0	11.1	22	350	M	M	10	1	26	360
31	35	26	31	8	34	0	0.85	7.5	T	21.7	32	350	M	M	8	1268	40	330

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SM 1407 670 970 0 3.05 7.5 266.3 M 98

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AV 45.4 21.6 8.6 FASTST PSBL % 3 MAX(MPH)

MISC ----> # 33 350 # 40 330

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NOTES:

LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: DECEMBER
 YEAR: 2006
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]

[PRECIPITATION DATA]

SYMBOLS USED IN COLUMN 16

AVERAGE MONTHLY: 33.5

TOTAL FOR MONTH: 3.05

1 = FOG OR MIST

DPTR FM NORMAL: 7.0

DPTR FM NORMAL: 2.19

2 = FOG REDUCING VISIBILITY

HIGHEST:	61 ON 5	GRTST 24HR	1.28 ON 30-31	TO 1/4 MILE OR LESS
LOWEST:	3 ON 1			3 = THUNDER
		SNOW, ICE PELLETS, HAIL		4 = ICE PELLETS
		TOTAL MONTH:	7.5 INCHES	5 = HAIL
		GRTST 24HR	7.5 ON 31-31	6 = FREEZING RAIN OR DRIZZLE
		GRTST DEPTH:	-1 ON M	7 = DUSTSTORM OR SANDSTORM: VSBY 1/2 MILE OR LESS
				8 = SMOKE OR HAZE
[NO. OF DAYS WITH]		[WEATHER - DAYS WITH]		9 = BLOWING SNOW
				X = TORNADO
MAX 32 OR BELOW:	3	0.01 INCH OR MORE:	7	
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	5	
MIN 32 OR BELOW:	27	0.50 INCH OR MORE:	2	
MIN 0 OR BELOW:	0	1.00 INCH OR MORE:	1	
[HDD (BASE 65)]				
TOTAL THIS MO.	970	CLEAR (SCALE 0-3)	22	
DPTR FM NORMAL	-218	PTCLDY (SCALE 4-7)	3	
TOTAL FM JUL 1	2281	CLOUDY (SCALE 8-10)	6	
DPTR FM NORMAL	-196			
[CDD (BASE 65)]				
TOTAL THIS MO.	0			
DPTR FM NORMAL	0	[PRESSURE DATA]		
TOTAL FM JAN 1	1327	HIGHEST SLP	30.95 ON 7	
DPTR FM NORMAL	173	LOWEST SLP	29.59 ON 16	

STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2007
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:			SKY		:PK WND			
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18	
										AVG MX 2MIN									
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR	
1	34	15	25	2	40	0	0.00	0.0	4	5.9	22	310	M	M	0	1	26	310	
2	37	13	25	2	40	0	0.00	0.0	3	8.3	17	190	M	M	0	1	21	200	
3	43	25	34	12	31	0	0.00	0.0	2	14.4	25	220	M	M	0		30	200	
4	52	36	44	22	21	0	0.00	0.0	1	10.6	20	200	M	M	1	1	23	220	
5	44	29	37	15	28	0	0.01	0.0	0	9.6	20	340	M	M	3		24	10	
6	44	25	35	13	30	0	0.00	0.0	0	8.4	22	230	M	M	0		26	230	
7	39	28	34	12	31	0	0.00	0.0	0	13.3	30	330	M	M	2		35	330	
8	53	28	41	19	24	0	T	0.0	0	17.3	33	300	M	M	1		40	310	
9	38	21	30	8	35	0	0.00	0.0	0	13.8	33	310	M	M	2		45	310	
10	53	24	39	17	26	0	0.00	0.0	0	15.5	30	200	M	M	0		35	210	
11	45	13	29	7	36	0	T	T	0	15.8	30	350	M	M	5	8	36	350	
12	17	5	11	-11	54	0	T	T	0	17.4	25	350	M	M	6		29	340	
13	13	5	9	-13	56	0	0.09	1.4	T	3.4	22	10	M	M	10	18	24	10	
14	17	12	15	-7	50	0	0.15	1.9	1	9.2	22	10	M	M	10	128	25	10	
15	15	-9	3	-19	62	0	T	T	3	11.4	24	350	M	M	2	8	26	340	
16	16	-15	1	-21	64	0	0.00	0.0	3	3.9	12	160	M	M	0		15	160	
17	28	5	17	-5	48	0	0.00	0.0	2	14.4	24	180	M	M	2		28	160	
18	34	18	26	4	39	0	0.00	0.0	2	11.7	30	330	M	M	1		37	330	
19	39	11	25	3	40	0	0.00	0.0	1	2.6	13	290	M	M	0		15	290	
20	36	7	22	0	43	0	0.12	2.0	1	7.5	17	190	M	M	4	18	20	180	
21	29	15	22	0	43	0	0.25	4.0	7	8.0	18	360	M	M	10	128	21	10	

22	24	10	17	-5	48	0	0.00	0.0	7	7.6	14	250	M	M	6	8	15	260
23	41	6	24	2	41	0	0.00	0.0	6	6.5	15	330	M	M	5		18	330
24	38	20	29	6	36	0	0.00	0.0	4	7.7	17	340	M	M	3	1	20	340
25	40	16	28	5	37	0	0.00	0.0	4	4.1	10	190	M	M	1	128	12	180
26	46	23	35	12	30	0	0.00	0.0	4	10.2	23	350	M	M	0	18	26	350
27	27	12	20	-3	45	0	T	T	2	16.6	32	330	M	M	3		39	330
28	27	5	16	-7	49	0	0.00	0.0	2	8.2	15	210	M	M	0		21	340
29	36	8	22	-1	43	0	T	T	2	14.5	32	320	M	M	2		38	310
30	17	3	10	-14	55	0	0.00	0.0	2	10.0	24	330	M	M	0		28	330
31	28	4	16	-8	49	0	0.02	0.7	2	9.1	17	250	M	M	6	18	21	230

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SM 1050 418 1274 0 0.64 10.0 316.9 M 85
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AV 33.9 13.5 10.2 FASTST PSBL % 3 MAX(MPH)
MISC ----> # 33 300 # 45 310
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NOTES:
LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
MONTH: JANUARY
YEAR: 2007
LATITUDE: 40 50 N
LONGITUDE: 96 45 W

[TEMPERATURE DATA] [PRECIPITATION DATA] SYMBOLS USED IN COLUMN 16

AVERAGE MONTHLY: 23.7 TOTAL FOR MONTH: 0.64 1 = FOG OR MIST
 DPTR FM NORMAL: 1.3 DPTR FM NORMAL: -0.03 2 = FOG REDUCING VISIBILITY
 HIGHEST: 53 ON 10, 8 GRTST 24HR 0.37 ON 20-21 TO 1/4 MILE OR LESS

LOWEST: -15 ON 16

SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: 10.0 INCHES
 GRTST 24HR 4.0 ON 21-21
 GRTST DEPTH: 7 ON 22,21

3 = THUNDER
 4 = ICE PELLETS
 5 = HAIL
 6 = FREEZING RAIN OR DRIZZLE
 7 = DUSTSTORM OR SANDSTORM:
 VSBY 1/2 MILE OR LESS
 8 = SMOKE OR HAZE
 9 = BLOWING SNOW
 X = TORNADO

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW:	12	0.01 INCH OR MORE:	6
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	3
MIN 32 OR BELOW:	30	0.50 INCH OR MORE:	0
MIN 0 OR BELOW:	2	1.00 INCH OR MORE:	0

[HDD (BASE 65)]

TOTAL THIS MO.	1274	CLEAR (SCALE 0-3)	21
DPTR FM NORMAL	-54	PTCLDY (SCALE 4-7)	7
TOTAL FM JUL 1	3555	CLOUDY (SCALE 8-10)	3
DPTR FM NORMAL	-250		

[CDD (BASE 65)]

TOTAL THIS MO.	0		
DPTR FM NORMAL	0	[PRESSURE DATA]	
TOTAL FM JAN 1	0	HIGHEST SLP 30.78 ON	16
DPTR FM NORMAL	0	LOWEST SLP 29.52 ON	4

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2007
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:			SKY		:PK WND		
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	30	3	17	-7	48	0	T	T	3	12.3	31	340	M	M	2	8	38	340
2	21	2	12	-12	53	0	0.00	0.0	3	13.5	26	240	M	M	0		32	230
3	15	0	8	-17	57	0	0.00	0.0	3	9.0	21	310	M	M	0		24	310
4	17	-1	8	-17	57	0	0.00	0.0	3	6.6	16	310	M	M	1		20	310
5	21	12	17	-8	48	0	0.00	0.0	3	10.1	16	70	M	M	8		17	70
6	43	14	29	3	36	0	0.00	0.0	3	12.0	25	350	M	M	3		30	350
7	18	11	15	-11	50	0	0.04	0.6	3	9.6	20	10	M	M	8	8	21	10
8	19	15	17	-9	48	0	0.01	0.1	3	6.3	13	40	M	M	10		14	40
9	17	10	14	-12	51	0	0.01	0.3	3	7.4	13	20	M	M	9	18	16	10
10	27	2	15	-12	50	0	T	T	3	5.1	13	210	M	M	7		15	200
11	37	27	32	5	33	0	0.00	0.0	3	10.3	20	180	M	M	10	18	22	190
12	34	21	28	1	37	0	0.18	2.3	2	11.5	23	20	M	M	10	16	26	20
13	21	0	11	-17	54	0	0.16	1.5	4	20.4	28	10	M	M	7	189	33	10
14	9	-6	2	-26	63	0	T	T	4	9.1	15	350	M	M	2	8	17	340
15	8	-4	2	-26	63	0	T	T	4	8.1	15	340	M	M	3	8	16	340
16	44	-3	21	-8	44	0	T	0.1	4	18.5	41	320	M	M	5	1	52	310
17	35	22	29	0	36	0	T	T	2	12.5	37	340	M	M	7	18	43	340
18	46	16	31	2	34	0	0.00	0.0	2	7.9	15	180	M	M	0	1	20	200
19	48	30	39	9	26	0	0.00	0.0	1	10.2	24	340	M	M	1		26	340
20	52	28	40	10	25	0	0.09	0.0	0	5.7	20	250	M	M	3	1	22	260
21	59	27	43	13	22	0	0.00	0.0	0	9.0	23	310	M	M	0		26	310

22	48	23	36	5	29	0	0.00	0.0	0	7.7	15	110	M	M	0	20	110	
23	62	34	48	17	17	0	0.00	0.0	0	18.3	29	150	M	M	3	33	160	
24	53	32	43	12	22	0	0.82	1.5	0	15.6	32	100	M	M	10	1345	38	130
25	33	25	29	-3	36	0	T	T	2	18.1	29	320	M	M	9	1	36	310
26	35	17	26	-6	39	0	0.00	0.0	1	5.1	14	340	M	M	5		15	340
27	37	19	28	-5	37	0	0.00	0.0	1	6.2	16	100	M	M	2	18	23	90
28	41	34	38	5	27	0	T	T	0	12.5	24	350	M	M	10	18	29	340

SM	930	410		1142	0	1.31		6.4	298.6				M		135			
----	-----	-----	--	------	---	------	--	-----	-------	--	--	--	---	--	-----	--	--	--

AV	33.2	14.6						10.7	FASTST	PSBL	%	5		MAX (MPH)				
								MISC	---->	#	41	320		#	52	310		

NOTES:

LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2007
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]

AVERAGE MONTHLY: 23.9
 DPTR FM NORMAL: -4.4
 HIGHEST: 62 ON 23
 LOWEST: -6 ON 14

[PRECIPITATION DATA]

TOTAL FOR MONTH: 1.31
 DPTR FM NORMAL: 0.65
 GRTST 24HR 0.82 ON 24-24
 SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: 6.4 INCHES

SYMBOLS USED IN COLUMN 16

1 = FOG OR MIST
 2 = FOG REDUCING VISIBILITY
 TO 1/4 MILE OR LESS
 3 = THUNDER
 4 = ICE PELLETS
 5 = HAIL

GRTST 24HR 2.3 ON M 6 = FREEZING RAIN OR DRIZZLE
 GRTST DEPTH: 4 ON 16,15 7 = DUSTSTORM OR SANDSTORM:
 VSBY 1/2 MILE OR LESS
 8 = SMOKE OR HAZE
 9 = BLOWING SNOW
 X = TORNADO

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW:	12	0.01 INCH OR MORE:	7
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	3
MIN 32 OR BELOW:	26	0.50 INCH OR MORE:	1
MIN 0 OR BELOW:	6	1.00 INCH OR MORE:	0

[HDD (BASE 65)]

TOTAL THIS MO.	1142	CLEAR (SCALE 0-3)	14
DPTR FM NORMAL	99	PTCLDY (SCALE 4-7)	6
TOTAL FM JUL 1	4697	CLOUDY (SCALE 8-10)	8
DPTR FM NORMAL	-151		

[CDD (BASE 65)]

TOTAL THIS MO.	0		
DPTR FM NORMAL	0	[PRESSURE DATA]	
TOTAL FM JAN 1	0	HIGHEST SLP 30.61 ON	14
DPTR FM NORMAL	0	LOWEST SLP 29.31 ON	24

STATION: LINCOLN
 MONTH: MARCH
 YEAR: 2007
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:		SKY		:PK WND				
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18	
										AVG MX 2MIN									
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR	
1	34	28	31	-2	34	0	0.60	6.6	4	20.2	31	310	M	M	5	1289	40	310	
2	32	18	25	-9	40	0	T	0.1	6	23.9	37	300	M	M	5	128	44	300	
3	28	17	23	-11	42	0	0.02	0.4	6	16.2	30	330	M	M	3	8	37	340	
4	50	8	29	-6	36	0	0.00	0.0	6	5.6	17	310	M	M	0		21	340	
5	43	24	34	-1	31	0	0.00	0.0	1	9.7	21	20	M	M	0		22	60	
6	44	20	32	-3	33	0	0.00	0.0	T	6.7	14	80	M	M	0	18	17	80	
7	31	26	29	-7	36	0	0.00	0.0	0	9.4	21	20	M	M	9	18	24	10	
8	56	28	42	6	23	0	0.00	0.0	0	11.4	18	190	M	M	5	18	21	170	
9	60	30	45	8	20	0	0.09	0.0	0	8.0	22	20	M	M	3	138	26	10	
10	61	28	45	8	20	0	0.00	0.0	0	5.6	14	130	M	M	2		17	150	
11	63	32	48	11	17	0	0.00	0.0	0	7.6	17	180	M	M	4	18	20	180	
12	78	41	60	22	5	0	0.00	0.0	0	11.6	21	220	M	M	3	18	24	260	
13	80	50	65	27	0	0	0.00	0.0	0	13.8	26	240	M	M	0		30	210	
14	60	33	47	8	18	0	0.00	0.0	0	16.2	32	30	M	M	2		38	30	
15	55	29	42	3	23	0	0.00	0.0	0	11.2	20	20	M	M	4		24	10	
16	48	21	35	-4	30	0	0.00	0.0	0	8.8	16	120	M	M	5	18	20	120	
17	52	35	44	4	21	0	0.00	0.0	0	11.8	20	120	M	M	3	8	22	120	
18	66	31	49	9	16	0	0.00	0.0	0	13.8	28	180	M	M	3	18	33	180	
19	61	37	49	8	16	0	0.00	0.0	0	13.4	30	20	M	M	1	18	35	10	
20	57	34	46	5	19	0	T	0.0	0	12.7	22	130	M	M	8	18	26	140	
21	80	47	64	23	1	0	0.02	0.0	0	15.4	31	190	M	M	7	18	36	200	

22	61	35	48	6	17	0	0.00	0.0	0	8.5	18	140	M	M	3		22	140
23	74	40	57	15	8	0	0.00	0.0	0	5.7	15	180	M	M	3	18	22	180
24	77	56	67	24	0	2	0.21	0.0	0	12.8	35	200	M	M	5	138	40	210
25	78	55	67	24	0	2	0.00	0.0	0	16.9	31	220	M	M	0		36	220
26	80	57	69	26	0	4	0.00	0.0	0	11.6	20	200	M	M	2	18	25	220
27	66	50	58	14	7	0	0.17	0.0	0	8.1	18	190	M	M	5	138	22	200
28	76	55	66	22	0	1	0.00	0.0	0	11.6	23	150	M	M	5	18	28	170
29	71	60	66	21	0	1	0.23	0.0	0	8.3	21	120	M	M	5	138	26	120
30	74	51	63	18	2	0	0.86	0.0	0	7.0	22	10	M	M	5	13	26	10
31	58	44	51	6	14	0	0.59	0.0	0	13.1	28	290	M	M	10	13	37	270

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=====
SM 1854 1120          529 10 2.79      7.1 356.6          M      115
=====
AV 59.8 36.1          11.5 FASTST  PSBL  %    4    MAX(MPH)
                        MISC ---->  # 37 300          # 44 300
=====

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NOTES:
LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
MONTH: MARCH
YEAR: 2007
LATITUDE: 40 50 N
LONGITUDE: 96 45 W

[TEMPERATURE DATA] [PRECIPITATION DATA] SYMBOLS USED IN COLUMN 16

AVERAGE MONTHLY: 48.0 TOTAL FOR MONTH: 2.79 1 = FOG OR MIST
DPTR FM NORMAL: 8.6 DPTR FM NORMAL: 0.58 2 = FOG REDUCING VISIBILITY
HIGHEST: 80 ON 26,21 GRTST 24HR 0.86 ON 30-30 TO 1/4 MILE OR LESS

LOWEST: 8 ON 4

SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: 7.1 INCHES
 GRTST 24HR 6.6 ON M
 GRTST DEPTH: 6 ON 4, 3

3 = THUNDER
 4 = ICE PELLETS
 5 = HAIL
 6 = FREEZING RAIN OR DRIZZLE
 7 = DUSTSTORM OR SANDSTORM:
 VSBY 1/2 MILE OR LESS
 8 = SMOKE OR HAZE
 9 = BLOWING SNOW
 X = TORNADO

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW:	3	0.01 INCH OR MORE:	9
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	6
MIN 32 OR BELOW:	14	0.50 INCH OR MORE:	3
MIN 0 OR BELOW:	0	1.00 INCH OR MORE:	0

[HDD (BASE 65)]

TOTAL THIS MO.	529	CLEAR (SCALE 0-3)	12
DPTR FM NORMAL	-270	PTCLDY (SCALE 4-7)	17
TOTAL FM JUL 1	5226	CLOUDY (SCALE 8-10)	2
DPTR FM NORMAL	-421		

[CDD (BASE 65)]

TOTAL THIS MO.	10
DPTR FM NORMAL	9
TOTAL FM JAN 1	10
DPTR FM NORMAL	9

[PRESSURE DATA]

HIGHEST SLP 30.12 ON 30
 LOWEST SLP 29.40 ON 31

STATION: LINCOLN
 MONTH: DECEMBER
 YEAR: 2007
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:		SKY		:PK WND			
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG MX		2MIN						
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	57	27	42	11	23	0	0.87	T	T	10.6	22	170	M	M	10	126	26	180
2	35	16	26	-5	39	0	0.01	0.2	T	13.1	26	330	M	M	5	18	33	320
3	49	14	32	2	33	0	0.00	0.0	T	6.9	29	220	M	M	0		35	230
4	54	23	39	9	26	0	0.00	0.0	0	3.5	13	320	M	M	1	18	17	320
5	46	17	32	2	33	0	T	T	0	13.9	35	350	M	M	7	8	44	340
6	29	17	23	-6	42	0	0.33	3.3	0	5.7	14	190	M	M	9	128	16	180
7	29	23	26	-3	39	0	T	T	3	6.0	12	20	M	M	9	18	14	20
8	26	13	20	-9	45	0	T	T	3	15.8	23	20	M	M	10	168	25	30
9	17	8	13	-15	52	0	0.02	0.5	3	8.1	20	20	M	M	9	18	24	30
10	29	2	16	-12	49	0	0.34	0.0	3	4.6	14	30	M	M	5	168	15	30
11	30	25	28	0	37	0	0.16	0.1	2	11.5	23	30	M	M	10	168	26	30
12	28	23	26	-1	39	0	0.00	0.0	2	6.7	18	220	M	M	10	18	22	210
13	39	16	28	1	37	0	0.00	0.0	2	5.2	18	230	M	M	1		22	230
14	26	13	20	-7	45	0	0.10	1.5	1	7.7	16	20	M	M	5	18	18	20
15	24	3	14	-13	51	0	0.25	3.1	5	6.6	14	20	M	M	6	128	15	10
16	23	0	12	-14	53	0	0.00	0.0	6	2.4	8	260	M	M	0	18	9	210
17	34	5	20	-6	45	0	0.00	0.0	6	5.5	17	190	M	M	0	18	21	200
18	41	15	28	2	37	0	0.00	0.0	5	2.9	12	300	M	M	0	18	15	300
19	41	13	27	2	38	0	0.00	0.0	3	3.0	13	160	M	M	0	18	14	180
20	38	14	26	1	39	0	0.00	0.0	2	2.0	8	160	M	M	3	128	8	160
21	42	14	28	3	37	0	T	0.0	2	4.9	22	330	M	M	1	18	26	330

22	35	10	23	-2	42	0	0.00	0.0	2	16.4	33	350	M	M	4	8	41	330
23	30	14	22	-2	43	0	0.00	0.0	2	12.4	25	290	M	M	2		32	290
24	35	16	26	2	39	0	0.00	0.0	1	5.9	14	190	M	M	0		18	200
25	43	28	36	12	29	0	0.00	0.0	1	9.4	17	190	M	M	1	18	21	190
26	33	12	23	-1	42	0	T	T	1	9.0	17	360	M	M	6	18	21	350
27	24	10	17	-7	48	0	T	T	1	6.0	15	50	M	M	8	128	18	50
28	28	17	23	0	42	0	0.01	0.2	1	7.4	16	20	M	M	5	18	20	30
29	32	10	21	-2	44	0	0.00	0.0	1	6.2	15	200	M	M	0	18	18	200
30	26	8	17	-6	48	0	0.00	0.0	1	4.3	12	230	M	M	0	18	13	270
31	32	22	27	4	38	0	0.00	0.0	1	11.4	32	310	M	M	7		39	310

SM	1055	448	1254	0	2.09	8.9	235.0	M	134
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AV	34.0	14.5	7.6	FASTST	PSBL	%	4	MAX(MPH)		
			MISC	---->	#	35	350	#	44	340

NOTES:
LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
MONTH: DECEMBER
YEAR: 2007
LATITUDE: 40 50 N
LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 24.2	TOTAL FOR MONTH: 2.09	1 = FOG OR MIST
DPTR FM NORMAL: -2.3	DPTR FM NORMAL: 1.23	2 = FOG REDUCING VISIBILITY
HIGHEST: 57 ON 1	GRTST 24HR 0.87 ON 1- 1	TO 1/4 MILE OR LESS

LOWEST: 0 ON 16

SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: 8.9 INCHES
 GRTST 24HR 3.3 ON M
 GRTST DEPTH: 6 ON 17,16

- 3 = THUNDER
- 4 = ICE PELLETS
- 5 = HAIL
- 6 = FREEZING RAIN OR DRIZZLE
- 7 = DUSTSTORM OR SANDSTORM:
 VSBY 1/2 MILE OR LESS
- 8 = SMOKE OR HAZE
- 9 = BLOWING SNOW
- X = TORNADO

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW: 16	0.01 INCH OR MORE: 9
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 6
MIN 32 OR BELOW: 31	0.50 INCH OR MORE: 1
MIN 0 OR BELOW: 1	1.00 INCH OR MORE: 0

[HDD (BASE 65)]

TOTAL THIS MO. 1254	CLEAR (SCALE 0-3) 14
DPTR FM NORMAL 66	PTCLDY (SCALE 4-7) 9
TOTAL FM JUL 1 2343	CLOUDY (SCALE 8-10) 8
DPTR FM NORMAL -134	

[CDD (BASE 65)]

TOTAL THIS MO. 0
 DPTR FM NORMAL 0
 TOTAL FM JAN 1 1431
 DPTR FM NORMAL 277

[PRESSURE DATA]

HIGHEST SLP 30.58 ON 2
 LOWEST SLP 29.42 ON 1

STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2008
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:		SKY		:PK WND				
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18	
										AVG MX 2MIN									
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR	
1	23	7	15	-8	50	0	0.00	0.0	1	13.0	26	330	M	M	3		32	300	
2	23	-1	11	-12	54	0	0.00	0.0	1	4.9	12	170	M	M	0		13	170	
3	37	14	26	4	39	0	0.00	0.0	1	18.1	30	200	M	M	0		39	200	
4	37	25	31	9	34	0	0.00	0.0	1	11.0	20	200	M	M	0		25	180	
5	44	20	32	10	33	0	0.00	0.0	1	7.0	15	150	M	M	0	18	18	160	
6	47	28	38	16	27	0	0.00	0.0	1	3.2	12	280	M	M	0	1	14	290	
7	44	28	36	14	29	0	0.09	0.0	1	4.2	16	110	M	M	2	18	18	110	
8	40	25	33	11	32	0	0.00	0.0	1	9.5	22	330	M	M	3		26	320	
9	41	23	32	10	33	0	0.00	0.0	T	7.8	22	170	M	M	1		26	170	
10	37	23	30	8	35	0	0.02	0.3	T	12.2	25	340	M	M	6	18	29	320	
11	39	17	28	6	37	0	0.00	0.0	T	1.8	12	230	M	M	1		16	220	
12	32	25	29	7	36	0	0.00	0.0	T	11.1	20	340	M	M	7	8	23	340	
13	39	17	28	6	37	0	0.00	0.0	T	7.3	17	10	M	M	4	18	21	360	
14	26	11	19	-3	46	0	0.00	0.0	0	6.5	16	330	M	M	3	8	18	10	
15	39	13	26	4	39	0	0.00	0.0	0	9.7	23	170	M	M	1		29	180	
16	32	16	24	2	41	0	0.21	3.0	0	14.1	29	360	M	M	8	1	36	350	
17	17	9	13	-9	52	0	0.05	0.5	4	7.6	16	360	M	M	3	18	18	350	
18	25	-1	12	-10	53	0	0.02	0.3	4	10.3	32	360	M	M	4	189	36	350	
19	13	-9	2	-20	63	0	T	T	4	3.5	10	310	M	M	3		13	310	
20	19	-1	9	-13	56	0	0.00	0.0	4	9.8	21	100	M	M	7		28	100	
21	19	8	14	-8	51	0	0.01	0.1	4	12.7	22	340	M	M	6	8	26	340	

22	20	-1	10	-12	55	0	0.00	0.0	4	7.9	18	250	M	M	0	23	250	
23	30	-3	14	-8	51	0	0.02	0.5	4	8.8	33	350	M	M	4	9	38	350
24	19	-10	5	-18	60	0	0.00	0.0	4	7.0	18	180	M	M	0	8	21	190
25	36	15	26	3	39	0	T	T	4	11.0	23	180	M	M	4		29	170
26	45	14	30	7	35	0	0.00	0.0	2	7.6	17	290	M	M	0		24	290
27	54	21	38	15	27	0	0.00	0.0	1	7.2	17	180	M	M	0		21	200
28	60	32	46	23	19	0	T	0.0	T	11.6	29	290	M	M	2		36	290
29	39	5	22	-1	43	0	0.02	0.2	0	18.3	37	350	M	M	5	189	44	350
30	19	4	12	-12	53	0	0.00	0.0	T	11.3	23	80	M	M	4		26	80
31	21	9	15	-9	50	0	0.00	0.0	T	9.3	20	30	M	M	4		23	20

SM	1016	383	1309	0	0.44	4.9	285.3	M	85
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AV	32.8	12.4	9.2	FASTST	PSBL	%	3	MAX(MPH)		
			MISC	---->	#	37	350	#	44	350

NOTES:
 # LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: JANUARY
 YEAR: 2008
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 22.6	TOTAL FOR MONTH: 0.44	1 = FOG OR MIST
DPTR FM NORMAL: 0.2	DPTR FM NORMAL: -0.23	2 = FOG REDUCING VISIBILITY
HIGHEST: 60 ON 28	GRTST 24HR 0.21 ON 16-16	TO 1/4 MILE OR LESS

LOWEST: -10 ON 24

SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: 4.9 INCHES
 GRTST 24HR 3.0 ON 16-16
 GRTST DEPTH: 4 ON 25,24

3 = THUNDER
 4 = ICE PELLETS
 5 = HAIL
 6 = FREEZING RAIN OR DRIZZLE
 7 = DUSTSTORM OR SANDSTORM:
 VSBY 1/2 MILE OR LESS
 8 = SMOKE OR HAZE
 9 = BLOWING SNOW
 X = TORNADO

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW:	15	0.01 INCH OR MORE:	8
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	1
MIN 32 OR BELOW:	31	0.50 INCH OR MORE:	0
MIN 0 OR BELOW:	7	1.00 INCH OR MORE:	0

[HDD (BASE 65)]

TOTAL THIS MO.	1309	CLEAR (SCALE 0-3)	18
DPTR FM NORMAL	-19	PTCLDY (SCALE 4-7)	13
TOTAL FM JUL 1	3652	CLOUDY (SCALE 8-10)	0
DPTR FM NORMAL	-153		

[CDD (BASE 65)]

TOTAL THIS MO.	0		
DPTR FM NORMAL	0	[PRESSURE DATA]	
TOTAL FM JAN 1	0	HIGHEST SLP 30.97 ON	2
DPTR FM NORMAL	0	LOWEST SLP 29.16 ON	28

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2008
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:		SKY		:PK WND				
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18	
										AVG MX 2MIN									
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR	
1	40	6	23	-1	42	0	0.00	0.0	T	7.3	21	160	M	M	1	18	24	150	
2	38	18	28	4	37	0	0.00	0.0	T	2.6	15	340	M	M	0	18	17	340	
3	39	18	29	4	36	0	0.07	0.3	T	7.2	17	110	M	M	8	18	20	120	
4	36	32	34	9	31	0	0.00	0.0	0	10.0	18	10	M	M	10	128	23	10	
5	33	19	26	1	39	0	0.32	4.5	0	20.4	31	10	M	M	10	128	38	360	
6	24	5	15	-11	50	0	0.01	0.1	4	7.8	23	350	M	M	5	89	28	350	
7	32	6	19	-7	46	0	0.00	0.0	4	3.4	12	300	M	M	3	18	14	290	
8	43	15	29	3	36	0	0.00	0.0	3	8.5	22	320	M	M	0		29	310	
9	40	15	28	2	37	0	T	T	2	12.6	24	360	M	M	5		29	350	
10	16	8	12	-15	53	0	T	T	1	11.8	24	350	M	M	3		28	350	
11	20	7	14	-13	51	0	T	T	1	10.0	17	120	M	M	4		21	120	
12	21	9	15	-12	50	0	0.00	0.0	1	7.2	14	310	M	M	3	8	18	320	
13	47	13	30	2	35	0	0.00	0.0	1	9.4	22	160	M	M	1	18	28	160	
14	39	9	24	-4	41	0	T	T	T	15.3	33	360	M	M	5	1689	40	360	
15	32	7	20	-8	45	0	0.00	0.0	T	4.7	14	190	M	M	0		17	190	
16	44	16	30	1	35	0	0.00	0.0	T	7.9	21	180	M	M	2		24	180	
17	42	29	36	7	29	0	T	T	0	21.6	39	340	M	M	7	1	53	320	
18	29	11	20	-9	45	0	0.00	0.0	T	12.3	28	330	M	M	0		33	330	
19	46	7	27	-3	38	0	0.00	0.0	0	9.9	28	10	M	M	3		32	10	
20	15	-3	6	-24	59	0	T	T	0	13.3	28	360	M	M	0	8	32	360	
21	20	8	14	-16	51	0	0.00	0.0	0	4.0	13	120	M	M	9		15	120	

22	41	7	24	-7	41	0	0.00	0.0	0	3.0	10	160	M	M	1	18	14	180
23	50	17	34	3	31	0	0.00	0.0	0	7.9	18	180	M	M	0	18	22	180
24	55	25	40	9	25	0	0.00	0.0	0	8.7	17	250	M	M	4	18	21	240
25	42	23	33	1	32	0	0.11	0.2	0	18.5	39	350	M	M	9	18	44	350
26	32	19	26	-6	39	0	0.00	0.0	T	13.0	26	340	M	M	4		31	350
27	46	16	31	-2	34	0	0.00	0.0	T	2.8	12	290	M	M	1		15	290
28	46	33	40	7	25	0	0.04	0.0	0	8.8	20	170	M	M	7	1	24	160
29	51	29	40	7	25	0	0.00	0.0	0	8.4	20	310	M	M	0	8	24	280

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SM	1059	424		1138	0	0.55		5.1	278.3				M		105			
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AV	36.5	14.6						9.6	FASTST	PSBL	%	4		MAX (MPH)				
								MISC	---->	#	39	340		#	53	320		

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NOTES:

LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
 MONTH: FEBRUARY
 YEAR: 2008
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

[TEMPERATURE DATA]

AVERAGE MONTHLY: 25.6
 DPTR FM NORMAL: -2.7
 HIGHEST: 55 ON 24
 LOWEST: -3 ON 20

[PRECIPITATION DATA]

TOTAL FOR MONTH: 0.55
 DPTR FM NORMAL: -0.11
 GRTST 24HR 0.32 ON 5- 5
 SNOW, ICE PELLETS, HAIL

SYMBOLS USED IN COLUMN 16

1 = FOG OR MIST
 2 = FOG REDUCING VISIBILITY
 TO 1/4 MILE OR LESS
 3 = THUNDER
 4 = ICE PELLETS

TOTAL MONTH: 5.1 INCHES 5 = HAIL
 GRTST 24HR 4.5 ON 5- 5 6 = FREEZING RAIN OR DRIZZLE
 GRTST DEPTH: 4 ON 7, 6 7 = DUSTSTORM OR SANDSTORM:
 VSBY 1/2 MILE OR LESS
 8 = SMOKE OR HAZE
 9 = BLOWING SNOW
 X = TORNADO

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW: 10	0.01 INCH OR MORE: 5
MAX 90 OR ABOVE: 0	0.10 INCH OR MORE: 2
MIN 32 OR BELOW: 28	0.50 INCH OR MORE: 0
MIN 0 OR BELOW: 1	1.00 INCH OR MORE: 0

[HDD (BASE 65)]

TOTAL THIS MO. 1138	CLEAR (SCALE 0-3) 14
DPTR FM NORMAL 95	PTCLDY (SCALE 4-7) 11
TOTAL FM JUL 1 4790	CLOUDY (SCALE 8-10) 4
DPTR FM NORMAL -90	

[CDD (BASE 65)]

TOTAL THIS MO. 0	
DPTR FM NORMAL 0	[PRESSURE DATA]
TOTAL FM JAN 1 0	HIGHEST SLP M ON M
DPTR FM NORMAL 0	LOWEST SLP 29.48 ON 17

STATION: LINCOLN
 MONTH: MARCH
 YEAR: 2008
 LATITUDE: 40 50 N
 LONGITUDE: 96 45 W

TEMPERATURE IN F:					:PCPN:		SNOW:		WIND		:SUNSHINE:			SKY		:PK WND		
1	2	3	4	5	6A	6B	7	8	9	10	11	12	13	14	15	16	17	18
										AVG MX		2MIN						
DY	MAX	MIN	AVG	DEP	HDD	CDD	WTR	SNW	DPTH	SPD	SPD	DIR	MIN	PSBL	S-S	WX	SPD	DR
1	69	32	51	18	14	0	0.00	0.0	0	10.6	24	230	M	M	0		31	230
2	60	34	47	13	18	0	0.11	0.1	0	18.5	33	360	M	M	5	18	44	350
3	34	19	27	-7	38	0	0.00	0.0	T	15.3	33	350	M	M	2		41	350
4	41	15	28	-7	37	0	0.00	0.0	0	8.8	18	160	M	M	2		23	190
5	36	19	28	-7	37	0	0.00	0.0	0	15.0	33	340	M	M	5		43	340
6	44	14	29	-6	36	0	0.04	1.0	0	4.0	23	10	M	M	2	1	28	10
7	27	1	14	-22	51	0	T	T	1	14.0	31	10	M	M	3	1	37	10
8	45	5	25	-11	40	0	0.00	0.0	T	7.3	20	190	M	M	1		24	190
9	43	18	31	-6	34	0	0.00	0.0	T	5.5	16	30	M	M	2	18	21	20
10	49	14	32	-5	33	0	0.00	0.0	0	4.5	M	M	M	M	0		M	M
11	71	29	50	13	15	0	0.00	0.0	0	7.5	22	240	M	M	0	8	26	240
12	67	27	47	9	18	0	0.00	0.0	0	8.1	36	330	M	M	0	8	41	330
13	64	27	46	8	19	0	0.00	0.0	0	4.6	14	180	M	M	0		17	170
14	54	30	42	3	23	0	0.00	0.0	0	11.4	24	30	M	M	6		30	30
15	43	24	34	-5	31	0	0.00	0.0	0	11.4	18	20	M	M	5	8	24	30
16	40	17	29	-10	36	0	0.01	T	0	8.7	17	100	M	M	3	18	22	100
17	42	36	39	-1	26	0	0.14	T	0	6.3	15	110	M	M	10	18	21	120
18	58	25	42	2	23	0	0.00	0.0	0	10.0	28	350	M	M	2	128	32	10
19	61	22	42	1	23	0	0.01	0.0	0	5.8	21	170	M	M	2	1	25	170
20	68	26	47	6	18	0	0.00	0.0	0	13.7	24	120	M	M	0	18	32	120
21	56	32	44	3	21	0	0.00	0.0	0	15.0	30	330	M	M	3		37	330

22	45	30	38	-4	27	0	T	0.0	0	11.9	26	350	M	M	9	18	31	350
23	45	21	33	-9	32	0	0.00	0.0	0	10.3	23	310	M	M	3		29	340
24	64	19	42	-1	23	0	0.00	0.0	0	18.4	31	170	M	M	0		38	210
25	61	31	46	3	19	0	0.00	0.0	0	11.5	25	350	M	M	0		32	350
26	60	33	47	4	18	0	0.00	0.0	0	9.8	18	100	M	M	8		23	90
27	49	34	42	-2	23	0	T	0.0	0	14.7	22	30	M	M	10	18	26	40
28	51	28	40	-4	25	0	0.00	0.0	0	3.6	12	360	M	M	5	18	15	90
29	58	38	48	3	17	0	0.00	0.0	0	15.7	25	160	M	M	6	8	33	170
30	53	40	47	2	18	0	T	0.0	0	12.2	25	10	M	M	10	18	30	10
31	42	35	39	-6	26	0	0.82	0.0	0	18.1	28	350	M	M	10	13	31	350

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SM 1600 775          819 0 1.13      1.1 332.2          M      114
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AV 51.6 25.0                10.7 FASTST PSBL % 4      MAX(MPH)
                               MISC ----> # 36 330                # 44 350
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NOTES:
LAST OF SEVERAL OCCURRENCES

COLUMN 17 PEAK WIND IN M.P.H.

PRELIMINARY LOCAL CLIMATOLOGICAL DATA (WS FORM: F-6) , PAGE 2

STATION: LINCOLN
MONTH: MARCH
YEAR: 2008
LATITUDE: 40 50 N
LONGITUDE: 96 45 W

[TEMPERATURE DATA]	[PRECIPITATION DATA]	SYMBOLS USED IN COLUMN 16
AVERAGE MONTHLY: 38.3	TOTAL FOR MONTH: 1.13	1 = FOG OR MIST
DPTR FM NORMAL: -1.1	DPTR FM NORMAL: -1.08	2 = FOG REDUCING VISIBILITY
HIGHEST: 71 ON 11	GRTST 24HR 0.82 ON 31-31	TO 1/4 MILE OR LESS

LOWEST: 1 ON 7

SNOW, ICE PELLETS, HAIL
 TOTAL MONTH: 1.1 INCHES
 GRTST 24HR 1.0 ON 6- 6
 GRTST DEPTH: 1 ON 7

- 3 = THUNDER
- 4 = ICE PELLETS
- 5 = HAIL
- 6 = FREEZING RAIN OR DRIZZLE
- 7 = DUSTSTORM OR SANDSTORM:
 VSBY 1/2 MILE OR LESS
- 8 = SMOKE OR HAZE
- 9 = BLOWING SNOW
- X = TORNADO

[NO. OF DAYS WITH]

[WEATHER - DAYS WITH]

MAX 32 OR BELOW:	1	0.01 INCH OR MORE:	6
MAX 90 OR ABOVE:	0	0.10 INCH OR MORE:	3
MIN 32 OR BELOW:	24	0.50 INCH OR MORE:	1
MIN 0 OR BELOW:	0	1.00 INCH OR MORE:	0

[HDD (BASE 65)]

TOTAL THIS MO.	819	CLEAR (SCALE 0-3)	18
DPTR FM NORMAL	20	PTCLDY (SCALE 4-7)	8
TOTAL FM JUL 1	5609	CLOUDY (SCALE 8-10)	5
DPTR FM NORMAL	-38		

[CDD (BASE 65)]

TOTAL THIS MO.	0		
DPTR FM NORMAL	-1	[PRESSURE DATA]	
TOTAL FM JAN 1	0	HIGHEST SLP 30.55 ON	10
DPTR FM NORMAL	-1	LOWEST SLP 29.40 ON	2