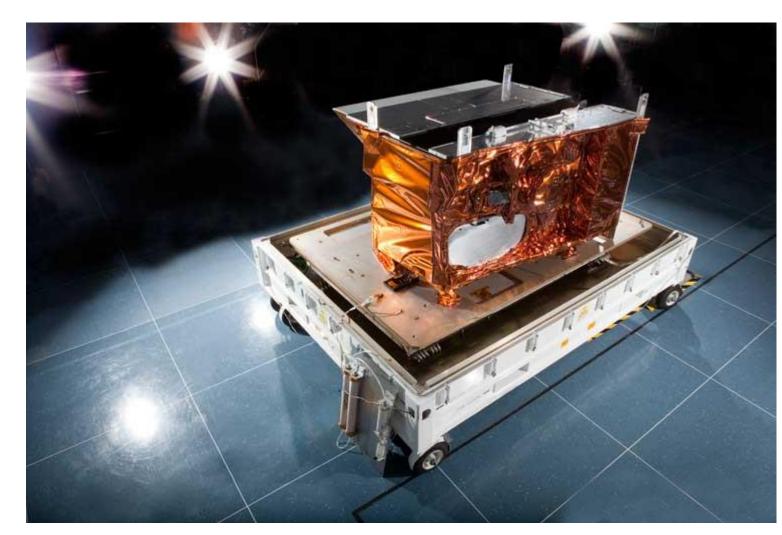
Benefits of an explicit calibration procedure for VIIRS reflective solar bands



1. Background

Visible Infrared Imaging Radiometer Suite (VIIRS) radiometer with reflective solar bands (RSB) and thermal bands (TEB). The RSB is calibrated prelaunch using an integrating sphere.



RSB	Wavelength
N / 1	(nm)
M1	412
M2	445
M3	488
M4	555
M5	672
M6	746
M7	865
M8	1240
M9	1378
M10	1610
M11	2250
11	640
12	865
13	1610

VIIRS Photo courtesy of Raytheon Space and Airborne Systems (http://npp.gsfc.nasa.gov/viirs.html)

2. Calibration

$$L = c_0 + c_1 x + c_2 x^2$$

The equation can be solved using *linear* algebra, but all c_0 , c_1 , and c_2 are affected by the calibration of L. An attenuator method adds

$$\tau \cdot L = c_0 + c_1 y + c_2 y$$

The two equations with $h_0 = c_0 / c_1$ and $h_2 = c_2 / c_1$ lead to

$$\tau = \frac{h_0 + y + h_2 y^2}{h_0 + x + h_2 x^2} \text{ and } c_1 = \frac{L}{h_0 + x + h_2 x^2}$$

where L only affects c_1 (which is calibrated on-orbit). However, the equation for τ (the attenuator transmittance), h_0 and h_2 (which are fixed on-orbit) becomes *nonlinear*.

3. Motivation

Nonlinear procedures for solving τ , h_0 , and h_2 together can be tricky to track and to verify. For example, there are hidden assumptions in minimization routines, and the solutions are asymptotic.

We want to visualize step by step how a procedure works.

4. New procedure

Rewrite the two calibration equations into

$$\frac{\tau \cdot x - y}{1 - \tau} = h_0 + h_2 \frac{y^2 - \tau \cdot x^2}{1 - \tau}$$

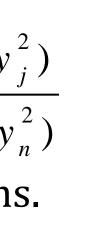
and using measurements from 3 or 4 radiance levels

$$\frac{(\tau \cdot x_i - y_i) - (\tau \cdot x_j - y_j)}{(\tau \cdot x_i) - (\tau \cdot x_j)} = \frac{(\tau \cdot x_i^2 - y_i^2) - (\tau \cdot x_j^2 - y_j)}{(\tau \cdot x_j^2 - y_j)}$$

 $(\tau \cdot x_m - y_m) - (\tau \cdot x_n - y_n) \quad (\tau \cdot x_m^2 - y_m^2) - (\tau \cdot x_n^2 - y_n^2)$ which is a quadratic equation of τ , with *analytical* solutions. Once τ is calculated across all combinations of measurements, h_0 is the intercept, and h_2 is the slope of a *linear* fit.

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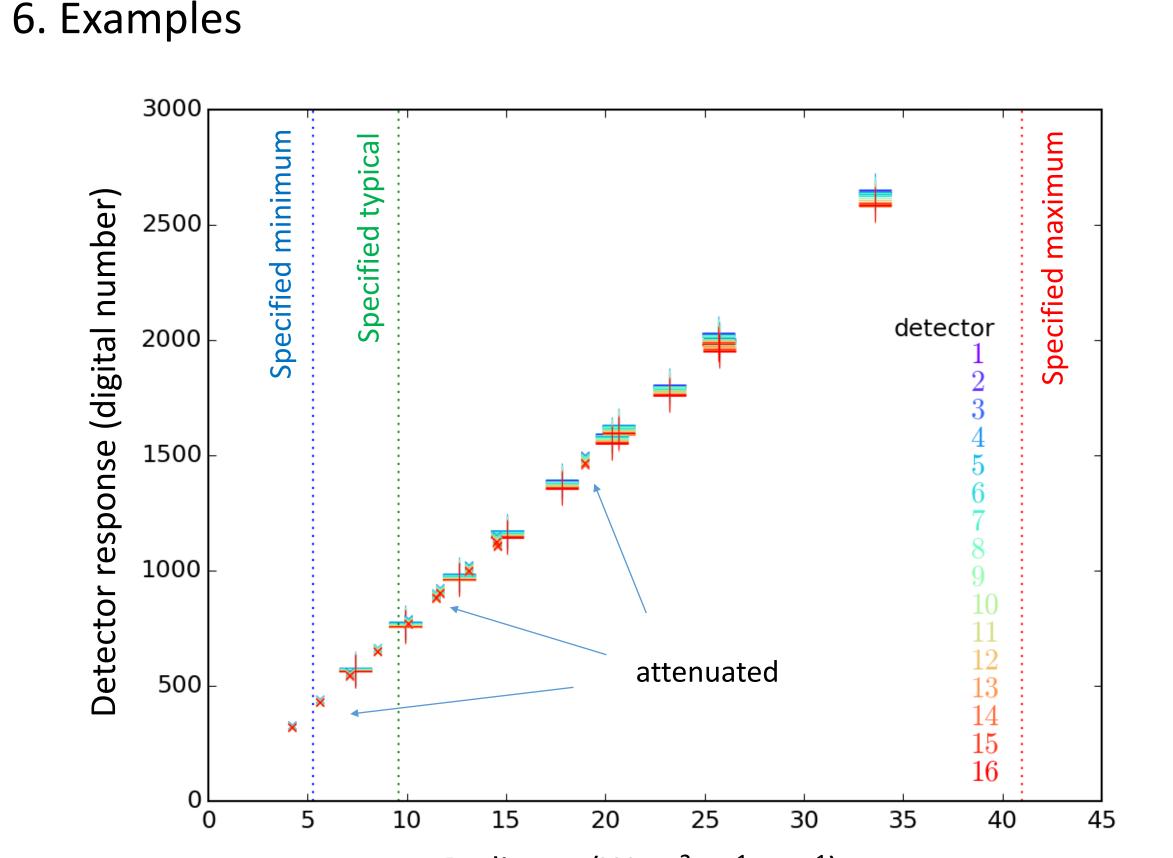
5. Benefits of the new procedure

The new procedure is straightforward. Solving for τ is similar to driving it using a calibrated detector, simply repeat the measurement at various radiance levels and look at the statistics.

The nonparametric technique is numerically stable, without the nonlinear fitting, the guesses plus inexplicit iterations, and the hidden assumptions, associated with those existing procedures.

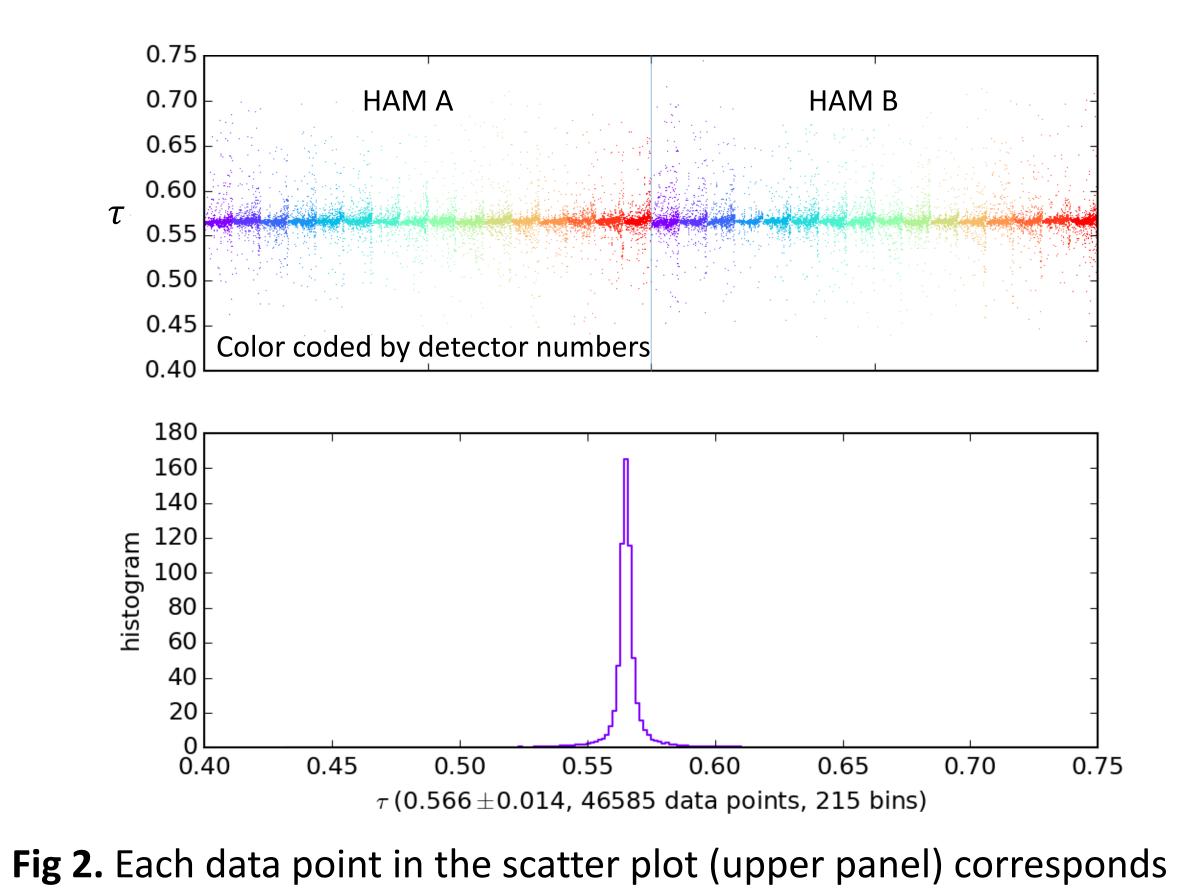
Also becomes straightforward is the uncertainty analysis, with the impact of individual data points easily seen.

By making the selections of τ and the relative calibration coefficients explicit, how the new procedure works is directly exposed. A tradeoff, depending on perspective, is that the consistency of results and a global optimization may have to be considered explicitly.

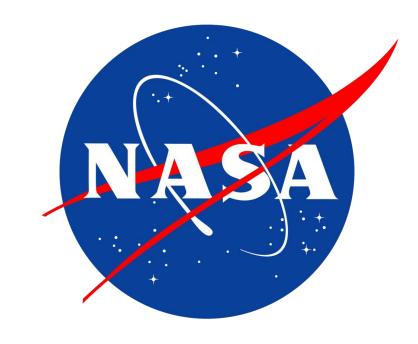


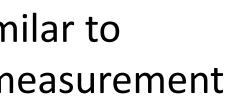
Radiance (W m⁻² sr⁻¹ μ m⁻¹)

Fig 1. There are 16 detectors in band M6. The response of detector is almost linear to the given radiance.



to a combination of measurements.





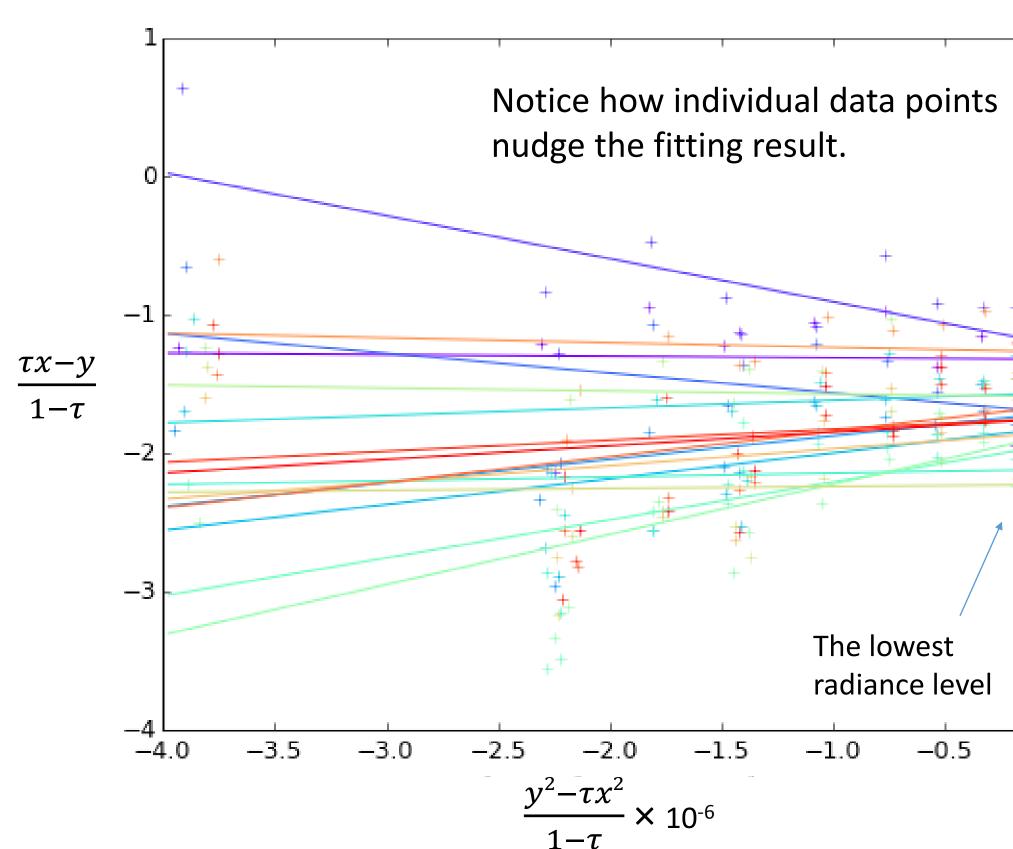


Fig. 3. The data points for a detector would follow a straight line if the measurements obeyed a quadratic calibration equation. The choice of fitting method is subjective. The results shown are from an ordinary least squares method.

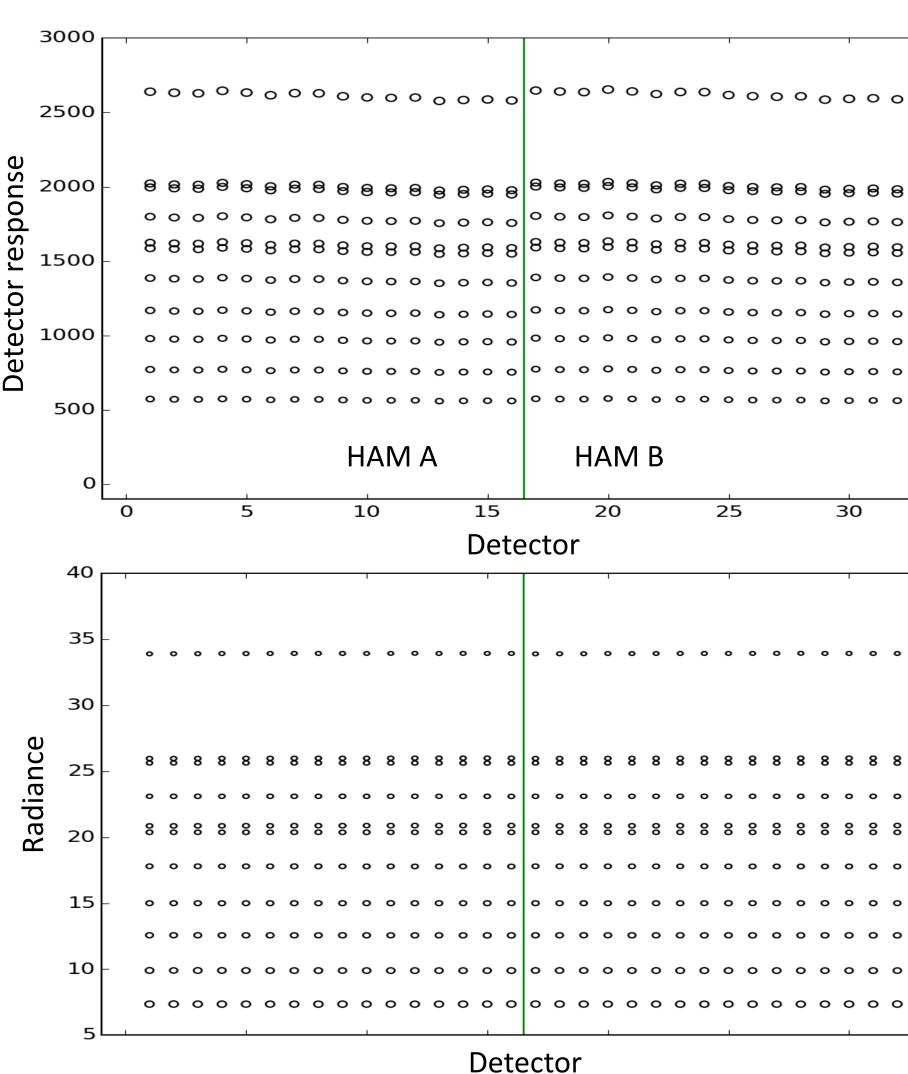


Fig. 4. Before calibration each detector has its own response (top panel); after calibration all detectors report the same radiance at a given radiance level (bottom panel).

7. Summary

Visualizing step by step how the new procedure works helped us gaining insight on our measurements and the calibration.

Reference: Ji et al, A robust method for determining calibration coefficients for VIIRS reflective solar bands, SPIE, 2015.

