

Seismic Volcanic Risk Assessment Puna Geothermal Prospect Area Hawaii

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for the
Seismic Risk Assessment

and
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for the
Volcanic Risk Assessment

prepared for
**Thermal Power Company
Dillingham
AMFAC**

October 1981

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1.0 EXECUTIVE SUMMARY

1.1 Introduction

This report summarizes the geologic, volcanologic, and seismicologic data that relate to evaluation of the Seismic-Volcanic Risk Assessment (SVRA) for the Puna Geothermal Prospect (PGP) of the Lower East Rift Zone (LERZ) on the volcano, Kilauea, Hawaii. The basis for the assessment sections is developed in detail in the Geology Section (3.0), with the volcanic and seismic assessments discussed in Sections 4.0 and 5.0, respectively.

The Volcanic Risk Assessment leads to conclusions that the hazards and risk from volcanic activity and associated fissuring and faulting are high and diverse, but the risk to engineered structures and installations can be mitigated by proper procedures in siting and design. Recommendations are made as to the methods and factors that should be considered for mitigation. The Seismic Risk Assessment demonstrates that the hazard and risk from ground motion is of three general sources: frequent low magnitude volcanic earthquakes with epicenters near the site, infrequent earthquakes of deep focus, low to moderate magnitudes and generally from Kilauea, and tectonic earthquakes of about 6.5 to 7.2 magnitude from the Hilina fault zone with epicenters at distances of from 20 to 50 km (12 to 30 mi).

1.2 Volcanic Risk Assessment

The Puna Geothermal Project is sited in one of the most active eruptive centers of one of the most rapidly growing volcanoes in the world. Important eruptions of lava have affected the area in 1750, 1790, 1840, 1955, and 1960.

Evidence from the log of the HGP-A well indicates that, on a

long term basis, an individual site is over-run by lava about once every 900 years, but on a shorter time scale, the frequency is strongly influenced by topography; low areas are covered by flows much more frequently than high areas.

Although eruptions are frequent, they are also quite regular in their behavior and can be predicted with a much higher degree of certainty than is possible in other volcanic regions of the world. Large explosions of ash or pumice are highly unlikely; almost certainly, future eruptions will be like earlier ones, i.e. voluminous discharges of very fluid lava preceded or accompanied by earthquakes and surface deformation.

Future eruptions will be preceded by volcanic and seismic activity in the summit region and by extension and faulting of the ground surface near the site of the eruptive outbreak. They will be accompanied by numerous earthquakes and will form new fissures, avoiding previously active vents in favor of new ground. Fissures will almost certainly be located within the well-defined boundaries of the rift zone. Vents outside that zone are highly unlikely. Fountaining to heights of three or four hundred meters will cover the surrounding region with scoriaceous material, but ejection of explosive debris rarely has a serious effect beyond a few hundred meters from the vent.

The principal volcanic hazards to facilities sited in the East Puna zone are surface rupture, ground motion, and inundation by lava. By comparison, all other hazards are relatively minor. These hazards can be greatly reduced by a modest amount of planning and consideration of a few simple precautions.

If at all possible, permanent installations should not be

constructed in low areas where lava is likely to be channeled. Old cinder cones and other areas of relatively high ground are unlikely to be over-run within the next four or five decades. Diversion barriers, if well situated and properly constructed, can deflect lava into an alternative course, but they are ineffective as dams opposing the flow of lava directly.

By orienting buildings and other permanent structures with their shortest dimensions parallel to the axis of the rift, the longest effects of ground deformation and surface rupture can be materially reduced.

Close coordination with the Hawaiian Volcano Observatory and the Hawaiian Institute of Geophysics will help ensure timely warnings of impending eruptions.

1.3 Seismic Risk Assessment

The maximum earthquake that is probable for the next 40 year period is an assumed tectonic earthquake from the Hilina fault zone, with an estimated magnitude of 6.75 and an epicentral distance of 25 km (15 miles). An earthquake of this magnitude would have a mean peak horizontal acceleration of about 0.25 g, a mean peak horizontal velocity of 25 cm/sec, and mean peak horizontal displacement of 10 cm, with a duration of more than 0.05 g motion for about 15 to 25 seconds. This strength and duration of motion, is the strongest motion to be expected from a 100 year earthquake of about $M_s = 7.2$, and is within the range that can be readily mitigated by appropriate design.

The two earthquake hazards that may constitute a risk to future engineering structures and installations are primarily the strong ground motion from tectonic earthquakes, and to a minor

amount, landsliding, slumping or other secondary ground failures of steep slopes near the epicenter of earthquakes of above 5 magnitude. Surface faulting may occur in the site area in response to volcanic related activity, as is discussed in the volcanic risk assessment section of the report. Other seismic hazards and risks, including liquefaction, tsunamis and seiches are considered to be unimportant for this siting area.

2.0 INTRODUCTION

2.1 Purpose of Study

The goal of this report is to provide a seismic-volcanic risk assessment (SVRA) for the Puna Geothermal Prospect (PGP) located within the Lower East Rift Zone (ERZ) of Kilauea volcano, on the island of Hawaii (Fig. 2.1). The assessment is for the general siting area and is not intended to apply to any site-specific domain within the general prospect area.

2.2 Scope of Work and Quality of Data Base

The scope of our work includes a preliminary study of available geologic literature, aerial photographs, maps, historical records, and limited bore hole data. The aerial photographs were used to assist in the field review of the siting areas and to search for faults and fissures near the site. Reports on the geology, seismology, tectonic, and volcanic settings are used to prepare this evaluation of the general volcanic and seismic hazards and risk to engineering structures. The site visits included a review of the faults, eruptive vents and other linear structures defined on the aerial photographs or shown on geologic maps of the area. These visits also permitted discussions with seismologists and geologists at the Hawaiian Volcano Observatory (HVO) and the Hawaiian Institute of Geophysics (HIG). This report integrates the catalogs of eruptions and earthquakes and the newer instrumental seismologic data of the latest listings of the National Oceanic and Atmospheric Administration (NOAA) hypocenter data file for worldwide earthquakes, and the HVO summaries of seismic data (Appendices A, B, and C). The above

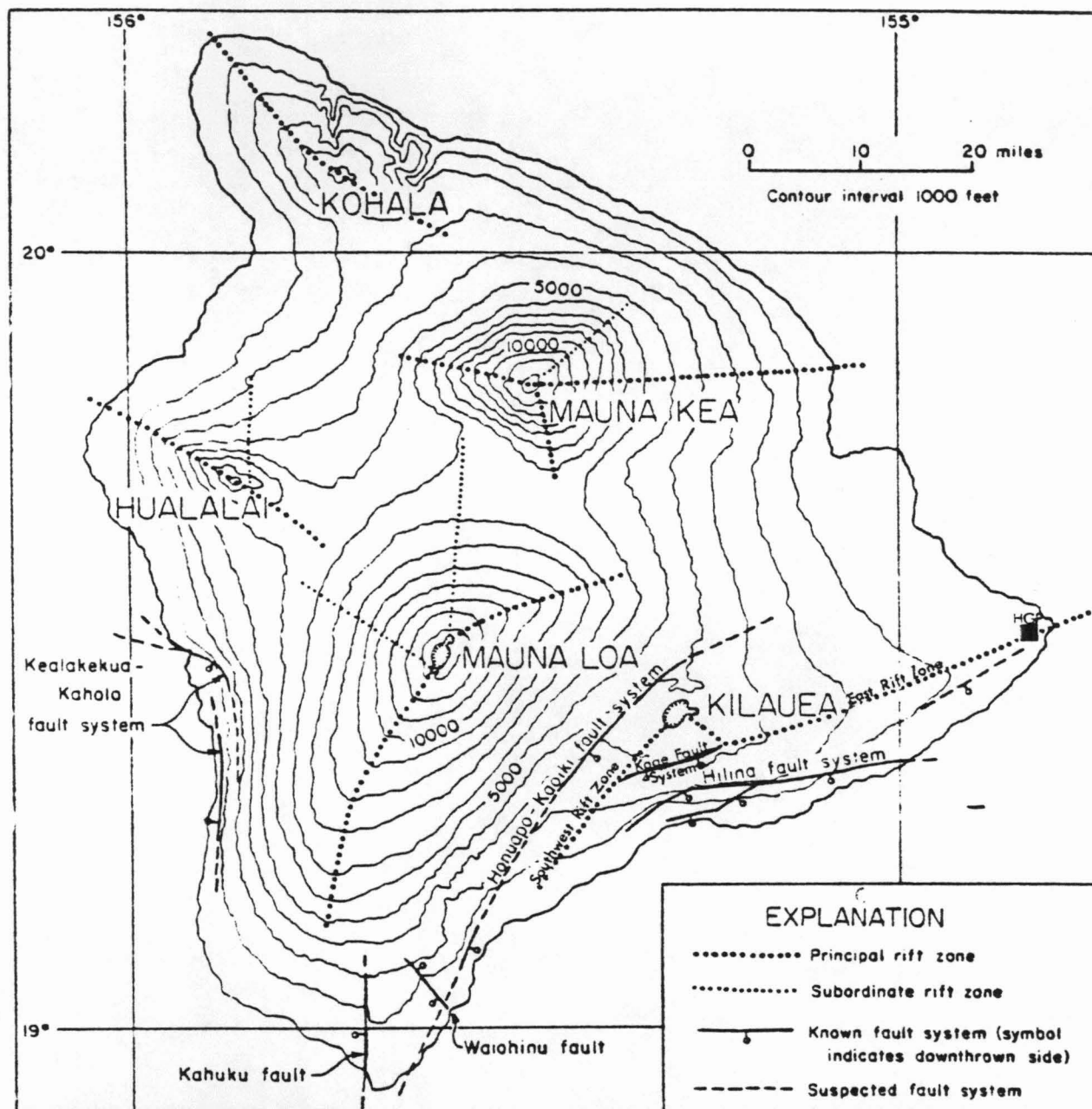


Figure 2.1. Map of major volcanoes, volcanic rift zones and faults on the island of Hawaii (from Macdonald and Abbott, 1970).

elements of the program are synthesized to provide a general evaluation of the maximum possible and maximum probable volcanic eruptions and earthquakes for structures of an assumed 40 year life-span. The general assessment for volcanic and seismic hazards is adequate for evaluation of the broad siting area, but risk assessment for specific structures or sites within the area are not included in the scope of this report.

This project was proposed and completed in the following stages:

- A. Literature search, fault and lineament analysis of the aerial photographs supplied by Thermal Power Company.
- B. Preliminary data collection and discussions with personnel of the HIG and HVO by George Bergantz and his preparation of a preliminary draft of this report.
- C. Field Study by Mr. George Bergantz in June 1981, and by Dr. D. Burton Slemmons, Alexander R. McBirney, and Brian H. Baker in August 1981.
- D. Preparation of the draft report.
- E. Review and revision of draft report and final submission of the report.

The data base for the seismic risk assessment varies greatly in quality and scope, with poor documentation for early historic earthquake activity, and variable quality and accuracy of cataloging in the National Oceanic and Atmospheric Administration (NOAA) earthquake hypocenter data file of Appendix A. The HVO summaries since about 1962 are good and the data for the period 1975 to 1979 are excellent for most of the region.

2.3 Abbreviations

Abbreviations that are used in this report include the following:

ERZ, East Rift Zone

HIG, Hawaiian Institute of Geophysics

HGP, Hawaiian Geothermal Prospect

HVO, Hawaiian Volcano Observatory

LERZ, Lower East Rift Zone, between about 800 ft elevation
and sea level

NOAA, National Oceanic and Atmospheric Administration

PGP, Puna Geothermal Project

SRZ, Southwest Rift Zone

3.0 GEOLOGY

3.1 Regional Geologic Setting

Kilauea is the southern-most of a chain of immense basaltic shield volcanoes extending northwestward across the north central Pacific. This chain has grown southeastward with time, so that the volcanoes are progressively older toward the northwest. Kilauea, the youngest and most active volcano of the chain, has grown to its present height of 1247 meters above sea level (nearly 6 kilometers above the sea floor) in a remarkably short period of about 500,000 years.

The chain has been described as the results of mid-plate volcanism, with northwestward movement of the Pacific plate over a "hot spot" or magmatic source, to form a series of islands and seamounts that vary in age and location from oldest at the northern end of the Emperor Seamount Chain, to the youngest on the south end of Hawaii in the Hawaiian Ridge segment of the chain (fig. 3.1 and 3.2). The potassium-argon dating of lava from these islands and seamounts (fig. 3.2) show a southeast migration of volcanism with time, with a mean migration rate of 11.0 cm/yr (Dalrymple and others, 1973). The volcanoes on the island of Hawaii conform to this general pattern with the northern volcanoes (Kohala and Mauna Kea) showing older ages and deeper dissection by erosion than the two southern, actively growing volcanoes, Mauna Loa and Kilauea which have prolific historic and neohistoric volcanic activity.

The five major volcanoes of Hawaii (pls. 1 and 2, and fig. 2.1) are built from flows and pyroclastic debris from central

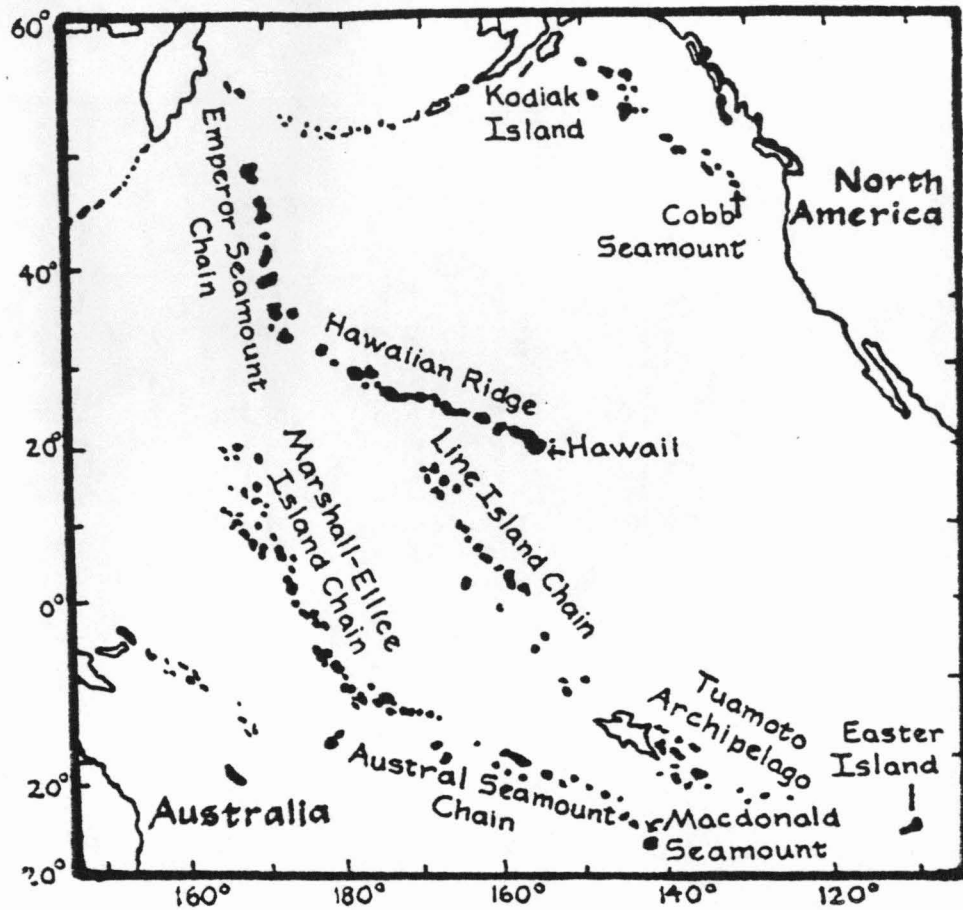


Figure 3.1. Chains of seamounts and volcanic islands in the Pacific Ocean (from Williams and McBirney, 1979).

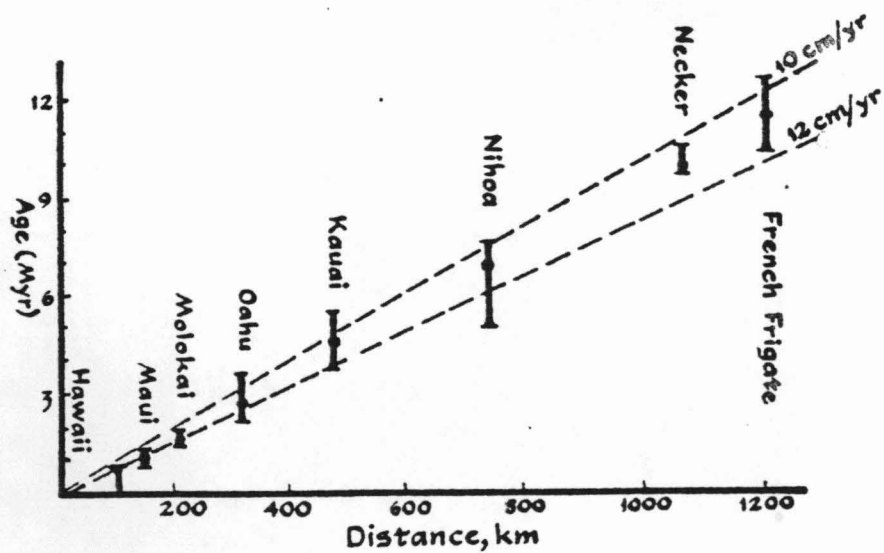


Figure 3.2. Relations of potassium-argon ages of lavas from the Hawaiian-Emperor chain north from Kilauea at the southeast end of the chain (from Williams and McBirney, 1979; and after Dalrymple and others, 1973).

conduits and rift zones. Cleaving these volcanic centers are radial rift zones which intersect at the central dome volcano, and which are the sites of, and passageways for, the bulk of the eruptive materials (Stearns, 1946). Mauna Loa and Kilauea are the southern-most major volcanoes of the island and of the chain. Both have many historic flows from their summits and northeast-trending rift zones.

Rocks in the vicinity of the Puna District and adjacent districts are typically aa and, less commonly, pahoehoe flows of olivine-bearing tholeiitic basalt and associated pyroclastic and hyaloclastic deposits (Stearns and Macdonald, 1946; Macdonald and Abbot, 1970). Three time-stratigraphic units are recognized, the Hilina Volcanic Series, the Pahala ash and the Puna Volcanic Series (fig. 3.3). The bulk of the older Hilina Volcanic Series is related to eruptive events from the Kilauea caldera with magmatic communication at moderate crustal depths inferred to connect with adjoining rifts (fig. 3.4). The Puna Volcanic Series include lavas that appear to have been differentiated from source magmas of the central conduit at Kilauea (Stearns and Macdonald, 1946).

3.2 Structural Features of Kilauea

Kilauea Volcano (fig. 3.5) can be divided into six structural zones (modified from the scheme of Swanson and others, 1976):

1. The summit area includes the caldera and two large pit-craters and has been the site of numerous eruptions and repeated surface deformation over the main reservoir of magma.

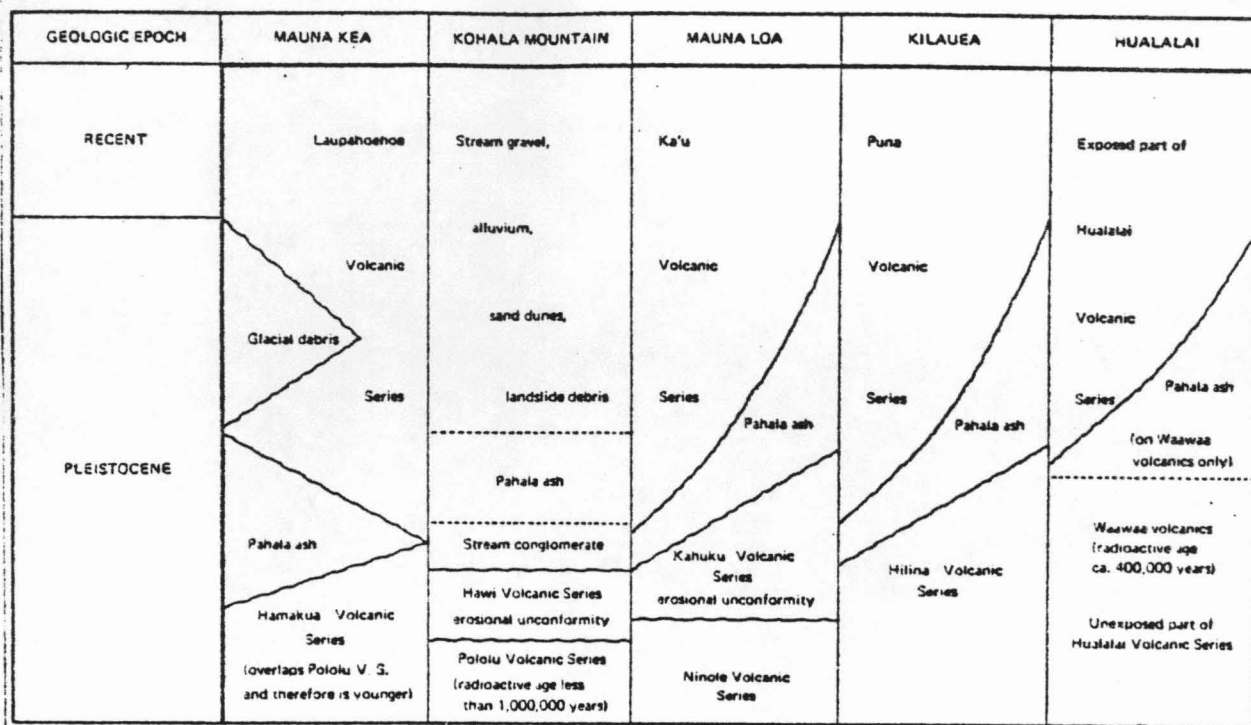


Figure 3.3. Geologic column for the main rock units on the island of Hawaii. All units have ages of less than 1,000,000 years; Recent extends to approximately 10,000 years ago (from Macdonald and Abbott, 1970).

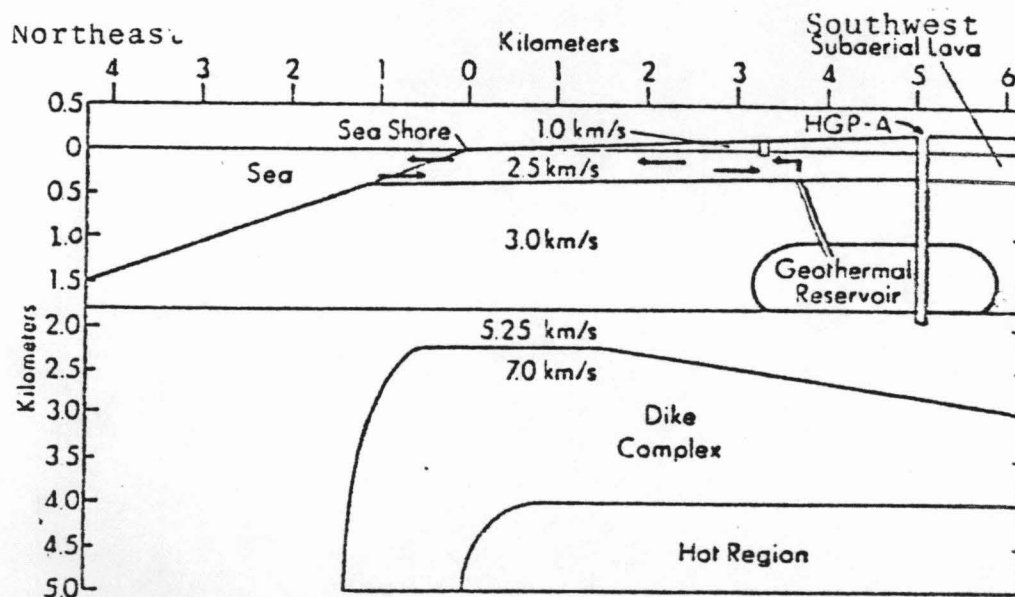
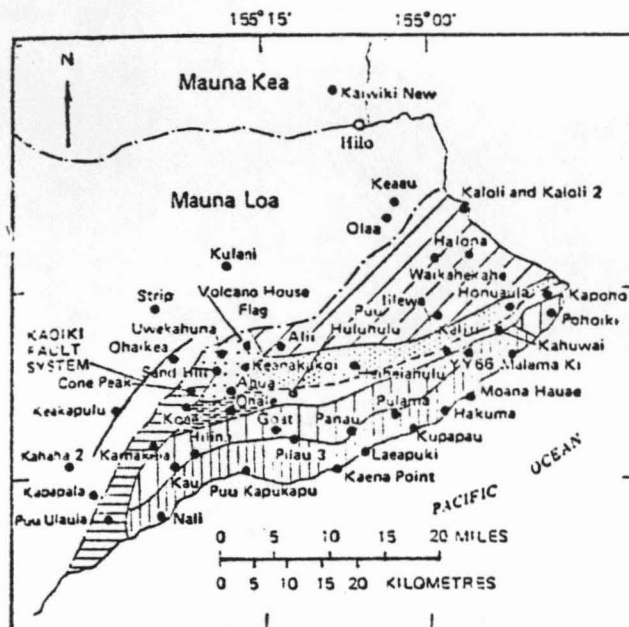


Figure 3.4. Inferred subsurface geologic structure of the East Rift Zone of Kilauea based on seismic refraction and gravity data (from Furumoto, 1978).



EXPLANATION

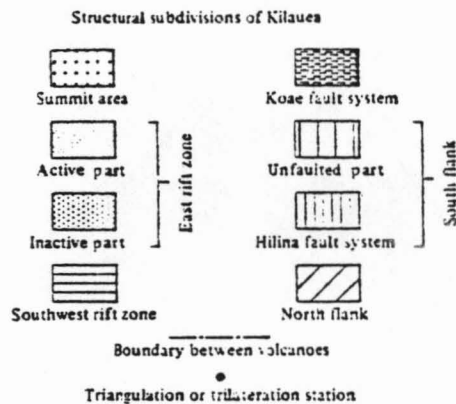


Figure 3.5. Structural subdivisions of Kilauea Volcano and locations of triangulation stations shown in Figure 4.5. Boundaries of subdivisions are gradational in most places (Swanson and others, 1976).

2. The Chain-of-Craters zone (fig. 3.6) comprises a SE-trending belt of small satellite shields and pit craters. This is cut by ENE-trending fissures and merges into the East Rift Zone.

3. The ENE-trending East Rift Zone (ERZ) consists of small shields, pit craters, fissures, and faults. It is 3 to 5 km wide, extends 45 km from Mauna Ulu to Cape Kumakahi, and continues as a submarine ridge another 70 km to the northeast.

4. The Koa'e fault system of 20 km length is a 3 km wide zone of normal faults cutting the upper south flank of Kilauea. It is the direct structural continuation of the ERZ and links the East and Southwest Rift Zones.

5. The Southwest Rift Zone (SRZ) of about 20 km length is a less active counterpart of the East Rift Zone.

6. The Hilina fault zone of about 50 km length cuts the lower, southern flank of the Kilauea shield.

The SRZ and ERZ, together with the summit area and the Chain of Craters zone comprise the eruptive zone of Kilauea, whereas the Koa'e and Hilina fault systems are fracture zones from which little or no lava has been issued.

3.3 Crustal Structure of Kilauea and the East Rift Zone

In order to understand the nature of volcanic and seismic activity of Kilauea, it is helpful to review briefly the structure and evolution of the volcano and the mechanisms governing its behavior.

Seismic data indicate that the crust under Kilauea consists of 9 kilometers of volcanic rocks resting on 5 to 6 kilometers of older oceanic crust and a mantle composed of rocks with the

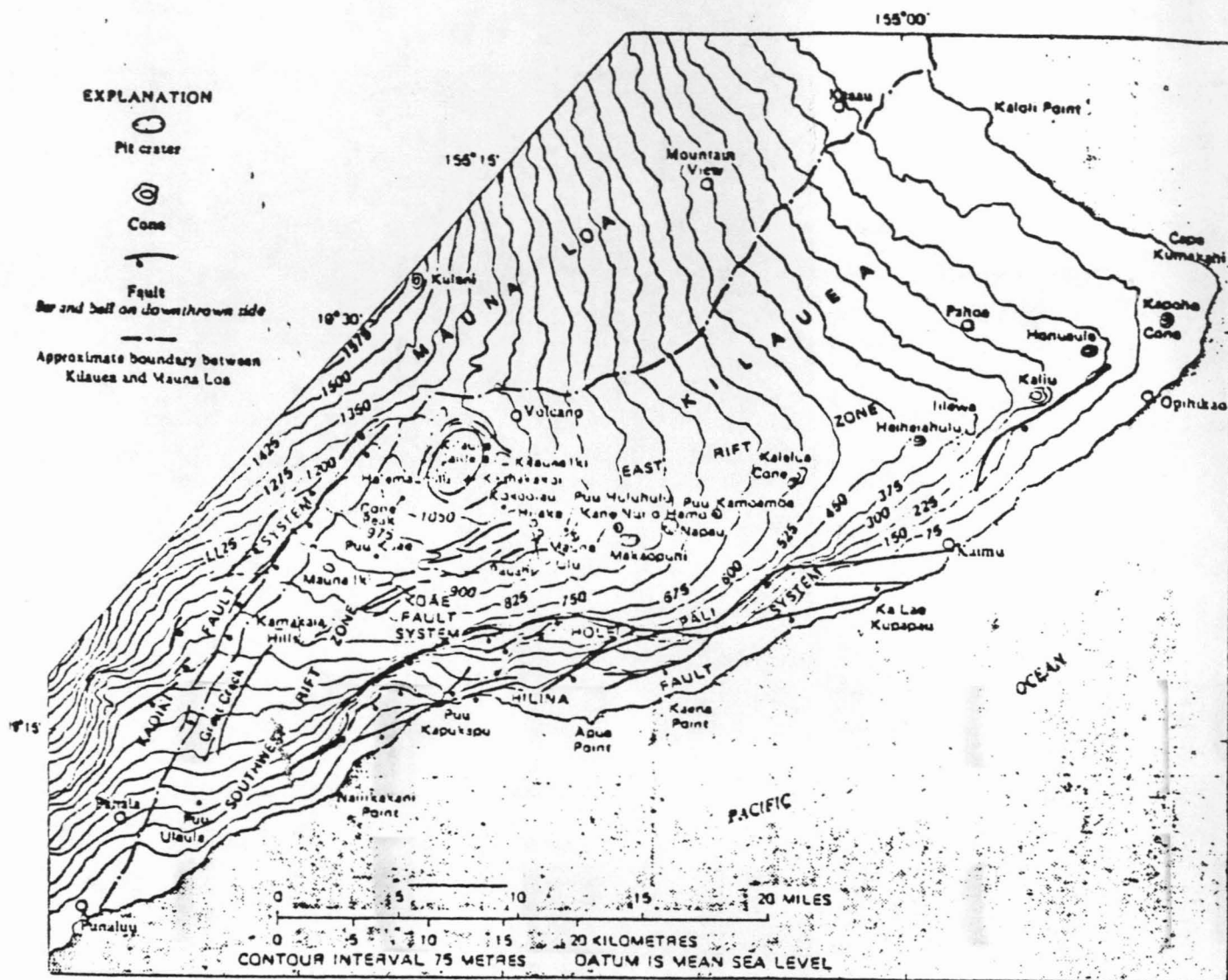


Figure 3.6. Map of Kilauea and the adjacent part of Mauna Loa Volcanoes showing the summit caldera and the south-west and south-east rift zones, and the Koae and Hilina fault systems on the south flank. The Chain of Craters sector of the East Rift Zone extends from Halemaumau to Mauna Ulu (Swanson and others, 1976).

seismic properties of serpentinized peridotite (Crosson and Koyanagi, 1979). The top of the mantle under the island is depressed by the great weight of the volcanoes from its normal depth of 10 km to about 14 km below sea-level.

Seismic refraction, gravity and seismic velocity surveys of the lower ERZ have shown (fig. 3.5, 3.7 and 3.8) a shallow surface layer of low and varied seismic velocities corresponding to young porous volcanic rocks ($V_p = 2.5$ to 3.0 km/sec), overlying a water-saturated zone extending to a depth of 1.8 km below sealevel. From 1.8 to 5 km, velocities average 5.25 km/sec, with a zone of higher velocity (about 7.0 km/sec) corresponding to a presumed dike complex along the ERZ (Broyles and others, 1979). Their gravity data indicate that the high-density zone of dikes is 12 km to 17 km wide, in contrast to the 4 km width of the ERZ. Part of the zone of high density lies to the north of the ERZ, supporting the suggestion (Swanson and others, 1976) that the ERZ has migrated to the south as the volcano has grown.

Seismicity in the ERZ is concentrated at depths of less than 10 km and has been related to lateral movement of magma from the summit region into a reservoir complex under the ERZ (Koyanagi and others, 1981). Swarms of shallow earthquakes commonly precede eruptions in the upper part of the ERZ, but near Puu Honaula (in the lower ERZ) shallow earthquake swarms have occurred without surface deformation or eruption, and these are thought to result from local movement in a magmatic storage zone isolated from the remainder of the rift (Koyanagi and others, 1974 and 1981).

3.4 Characteristics of Volcanism of Kilauea

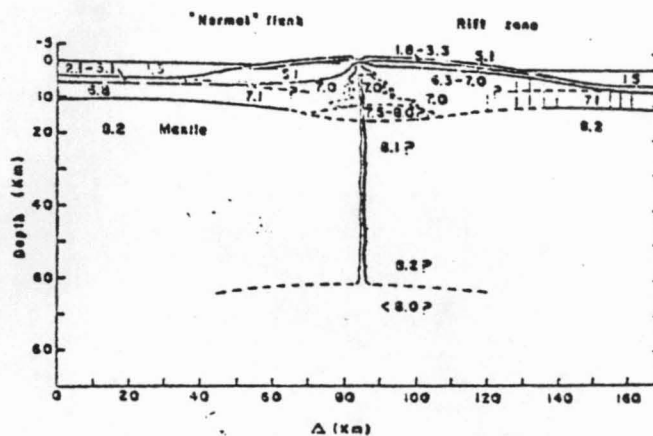


Figure 3.7 Schematic cross section showing idealized crustal structure of Hawaiian Volcano (based largely on Kilauea). Numbers indicate P-wave velocity in km/sec (Hill, 1969).

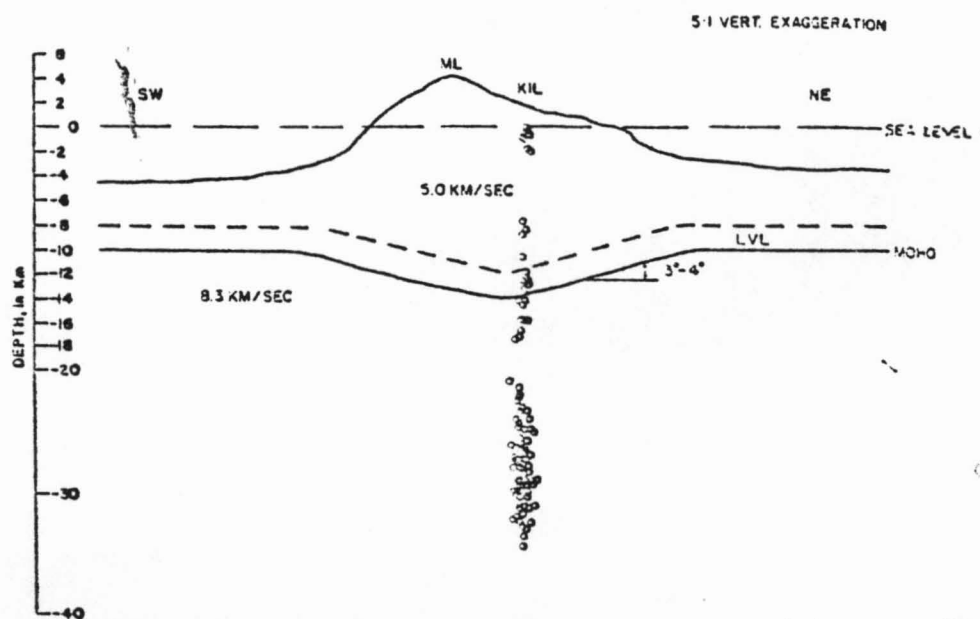


Figure 3.8 Hypothetical cross section through the island of Hawaii (SW to NE) showing principal features of structure as suggested by the seismic velocity interpretations of Crosson and Koyanagi (1979). Velocities are meant to denote averages for the crust and upper mantle. Small open circles are representative of earthquake depth distribution beneath Kilauea volcano (from Crosson and Koyanagi, 1979).

Because of the frequency of eruptions and many detailed studies carried out by the Hawaiian Volcano Observatory, the activity of Kilauea is more clearly understood than that of any other volcano. Techniques for monitoring and forecasting eruptions have reached a highly sophisticated and successful level of development.

While it is generally true that volcanism has a variety of forms and no two eruptions are exactly identical, Hawaiian activity is more regular than that of other types of volcanoes. The characteristics of the eruptive activity of Kilauea during its present mature stage of evolution have been well defined.

Eruptions are centered in two general regions, the summit caldera and the rift zones. In general, summit eruptions have a more localized effect, because they tend to be confined to depressions that restrict the flow of lava to a relatively small area. In recent years, however, activity in the summit region has shifted to the vicinity of the new eruptive center around Mauna Ulu, a short distance south of the caldera. Flows from this area have moved down the south flank of the volcano, but have no effect on the lower ERZ. Their significance for our present purposes is in the close connection between activity at the summit and eruptions farther down the rift zones.

Eruptions on the flanks of Kilauea are frequently linked with earlier activity in the summit region. The magma feeding flows discharged from the lower ERZ has been shown to come from a reservoir much higher in the volcanic structure. Swelling of the summit region is commonly observed before an outbreak on the

flanks, and monitoring of this swelling provides a means of anticipating when the volcano is charged with magma at a high level and is capable of erupting. In all the eruptions for which good data are available, earthquakes and tumescence have been recorded around the caldera, and regardless of whether or not these subsurface events were followed by an eruption at the summit, outbreaks on the rift rarely occur except after notable swelling of the upper parts of the volcano.

Many, but by no means all eruptions have been preceded by broadly distributed deep earthquakes followed by more localized seismic activity at a shallow level beneath the immediate region of the impending eruption. In some instances there may be little deep-focussed seismicity and only shallow localized earthquakes. While many of the earthquakes are small, they are recorded in large numbers by the seismic network operated by the U.S. Geological Survey for many days or weeks prior to the outbreak of magma at the surface. For this reason, it is highly unlikely that a major eruption will come as a surprise. It will be preceded by swelling, tilting, and extensive seismic activity well before any lava is discharged.

The chemical and physical character of the magma at Kileaua is also very consistent. It is a very fluid tholeiitic basalt that commonly contains conspicuous crystals of olivine and, more rarely, plagioclase. Apart from minor variations in some of its components, mainly trace elements and concentrations of olivine crystals, it can be expected to vary little for many decades to come. It is normally erupted at temperatures between 1150 and 1200 degrees centigrade and has a low viscosity (in the range of

300 to 1000 poises). Its density ranges widely according to the proportion of gas bubbles but the interiors of flows can reach density of 2.7 grams per cubic centimeter.

Lava is generally of the pahoehoe type near the vent but commonly changes to the clinkery aa type as it flows downslope and cools. Some eruptions, such as that of 1790, produced lavas that were almost exclusively pahoehoe, whereas others, such as that of 1955, have been dominantly aa. There is no simple way of anticipating which type of lava will be erupted in a particular location.

Eruptions usually break out relatively quietly at one or two points on the rift and quickly spread along a well defined fissure for distances of a few hundred meters to as much as several kilometers. The initial eruptive phase is characterized by spectacular fire-fountaining, which quickly increases in height and intensity. It normally lasts for a period of hours, days, or, more rarely, weeks. Along most of the eruptive fissure, the products of these early stages are incandescent bombs, spatter, and fine glassy filaments known as "Pele's hair". Ash is usually subordinate to coarser material, and scoriaceous cinders may accumulate to thicknesses of many meters around a centralized vent that persists in activity for several days or weeks.

Close to the coast, particularly in the area of Kapoho where the ground water table is shallow and rocks are very permeable, water may enter the upper levels of the fissure and greatly augment the explosivity of the eruption. When this occurs, the ejecta are more voluminous and tend to be gray ash, quenched glass, and blocky lithic debris. Regardless of the mode of erup-

tion, however, the deposits are confined to an area close to the vent and seldom accumulate to depths of more than a few meters at distances of more than half a kilometer. Violent explosions hurled large blocks several hundred meters during the steam-blast eruption at the summit of Kilauea in 1790 and 1924, but large events of this kind have been uncommon in historic times and have been confined to the summit area.

Subsidence may occur either as linear troughs or as cylindrical collapse pits up to one or two hundred meters in diameter. These latter features are more typical of the upper parts of the rift where magma has been drained by intrusions or eruptions at a lower elevation. But the connection between subsidence and eruptions may not be an obvious one. In 1924, for example, the area of Kapoho subsided several feet even though no surface eruption was observed. It is thought that magma drained into a submarine section of the rift zone and may have erupted below sea level.

Lava flows begin to emerge concurrent with or very soon after the initial episode of fire fountaining. They seldom pour from the entire width of the fissure, except in the earliest stages. More typically, the eruptive vent quickly becomes localized in a short section of the rift. Lava is often discharged at rates of two to five million cubic meters per hour and commonly flows reach lengths of the order of ten kilometers, widths of two or three hundred meters, and thicknesses of about four meters, but these dimensions vary within wide limits. The widths and thicknesses of flows depend mainly on the steepness of the slope and on how much of the fissure is active at a particular time. As the lava moves away from the source, its width may either

increase or decrease depending on the local topography. Flows on the south side of the rift tend to become narrower where the slope steepens, and in many cases well-defined channels only a few meters wide develop after the first broad front of the flow has passed. The velocity of flow varies directly with the slope angle and rate of discharge and inversely with the viscosity and width. Velocities as high as 40 miles per hour have been measured in narrow steep channels of pahoehoe lava.

Upon reaching the sea, lava may interact with the water to produce a spray of quenched granular basaltic glass, and if fed by a well-defined and rapidly flowing channel, a flow may develop a littoral cone that can grow to the size of a moderately large cinder cone. Again, the area affected by this explosive activity is confined to the immediate area of the point at which the flow enters the sea.

Taking the volcano as a whole, at least 50 eruptions have been recorded since Europeans first visited the islands, but it is only since 1912, when the Hawaiian Volcano Observatory was established, that reliable records have been available. Table 3.1 lists 46 eruptions and a number of suspected intrusive events that have occurred in this period of 69 years or an average of one every 1.5 years. Of these, 19 occurred in the ERZ and only two, those of 1955 and 1960, affected the East Puna District.

Klein (in press) recently examined this record and found that the timing of eruptions had no detectable periodicity. He observed that subsequent eruptions were independent of the date of the previous eruption. He has, however, found a number of fairly regular (or at least non-random) relationships. These can

TABLE 3.1

Kilauea Eruptions (1918-1979) and intrusions (1959-1980).

EVENT	STARTING DATE	DURATION (d)	LOCATION ¹ & TYPE OF EVENT			DAYS SINCE LAST ERUPTION	DAYS SINCE LAST INTRUSION	ERUPTED VOLUME (10 ⁶ m ³)	DEFLATION (TILT AT HVO, IN MICRORADS)
			SUMMIT	ER	SWR				
1	2/23/18	14	E	---	---	---	---	.2	---
2	2/7/19	294	E	---	---	349	---	27	---
3	12/21/19	221	---	---	E	317	---	49	---
4	3/18/21	7	E	---	---	453	---	7	---
5	5/28/22	2	---	E	---	436	---	?	---
6	8/25/23	1	---	E	---	454	---	.1	---
7	5/10/24	17	E	---	---	259	---	ASH	---
8	7/19/24	11	E	---	---	70	---	.3	---
9	7/7/27	13	E	---	---	1083	---	2.5	---
10	2/20/29	2	E	---	---	594	---	1.5	---
11	7/25/29	4	E	---	---	155	---	2.8	---
12	11/19/30	19	E	---	---	482	---	7	---
13	12/23/31	14	E	---	---	399	---	8	---
14	9/6/34	33	E	---	---	988	---	8	---
15	6/27/52	136	E	---	---	6504	---	51	---
16	5/31/54	3	E	---	---	703	---	7	---
*17	2/28/55	88	---	E	---	273	---	95	---
18	11/14/59	36	E	---	---	1720	---	40	-45
*19	1/13/60	36	---	E	---	60	60	119	-300
20	2/24/61	1	E	---	---	408	408	.2	<2
21	3/3/61	22	E	---	---	7	7	.3	-6
22	7/10/61	7	E	---	---	129	129	13	-8
*23	9/22/61	4	---	E	---	74	74	2.5	-166
24	12/7/62	3	---	E	---	441	441	.3	-18
	5/9/63	1	---	---	I	---	153	---	-32
	7/1/63	2	---	I	---	---	53	---	-20
25	8/21/63	3	---	E	---	257	51	.8	-11
*26	10/5/63	2	---	E	---	45	45	8	-79
*27	3/5/65	11	---	E	---	517	517	18	-84
	8/25/65	1	I	I	---	---	173	---	+8
28	12/24/65	2	---	E	---	294	121	.8	-45
*29	11/5/67	251	E	---	---	681	681	84	-11
30	8/22/68	5	---	E	---	291	291	.01	-54
31	10/7/68	16	---	E	---	46	46	7	-60
32	2/22/69	7	---	E	---	138	138	17	-46
*33	5/24/69	875	---	EP	---	91	91	185	-24
	11/3/69	1	---	I	---	---	163	---	-6
	1/22/70	1	I	---	---	---	80	---	-6
	2/3/70	8	---	I	I	---	12	---	-4
	4/5/70	5	---	I	I	---	61	---	-9
	5/15/70	2	---	I	---	---	40	---	-8
	6/11/71	3	---	---	I	---	392	---	-4
34	8/14/71	1	E	---	---	812	64	10	-16
35	9/24/71	5	E	---	(E)	41	41	8	+12
	12/24/71	6	---	---	I	---	91	---	-3
*36	2/4/72	455	---	EP	---	133	42	125	-2
37	5/5/73	1	---	E	---	456	456	1	-23
38	5/7/73	187	---	EP	---	2	2	2.5	<2
	6/9/73	1	---	I	---	---	33	---	-8
39	11/10/73	30	---	E	---	187	154	3	-14
40	12/12/73	222	---	EP	---	32	32	30	-2
	3/24/74	1	---	I	---	---	102	---	-5

TABLE 3.1. Continued.

EVENT	STARTING DATE	DURATION (d)	LOCATION ¹ & TYPE OF EVENT			DAYS SINCE LAST ERUPTION	DAYS SINCE LAST INTRUSION	ERUPTED VOLUME ($10^6 m^3$)	DEFLATION (TILT AT HVO, IN MICRORADS)
			SUMMIT	ER	SWR				
41	7/19/74	3	E	--	--	219	117	10	-17
42	9/19/74	1	E	--	--	62	62	11	+25
*43	12/31/74	1	--	--	E	103	103	15	-155
*44	11/29/75	1	E	(I)	--	333	333	.2	-221
	6/21/76	1	--	I	--	--	205	--	-7
	7/14/76	1	--	I	--	--	23	--	-7
	2/8/77	1	--	I	--	--	209	--	-6
45	9/12/77	20	--	E	--	653	216	40	-109
	5/29/79	1	--	I	--	--	624	--	-3
	8/12/79	1	--	I	--	--	75	--	-2
46	11/16/79	1	--	E	--	795	96	.4	-8
	3/2/80	1	--	I	--	--	107	--	-3
	3/10/80	1	--	I	--	--	8	--	-16
	8/27/80	1	--	I	--	--	170	--	-7
	10/22/80	1	--	I	--	--	56	--	-2
	11/2/80	1	--	I	--	--	11	--	-6

¹Location codes: Summit, Kilauea summit caldera or its margin; ER, east rift zone; SWR, southwest rift zone; Event codes: E, eruption; I, intrusion with no surface lava; EP, major phase of Mauna Ulu eruption of 1969-74. Data are complete through November 1980.

*Largest eruptions: volume exceeds $70 \times 10^6 m^3$, or deflation exceeds 70 microradians.

be briefly summarized as follows.

1. Large-volume eruptions tend to be followed by longer repose, which are interpreted as the time required for the shallow magma reservoirs refill to the extent that another eruption is possible.

2. The mean repose time between eruptions has been 282 days. Long periods of repose lasting several years are correlated with periods when Mauna Loa is active. The short repose times of a few days are probably due to brief physical obstructions that interrupt an eruption that would otherwise be continuous. Intermediate repose time appear to be of random duration and cannot be correlated with any known phenomenon.

3. Summit and flank eruptions are often paired with flank eruptions following a summit eruption rather than vice versa, but the pattern is far from regular, and the time of the last summit eruption cannot be used to forecast the next flank eruption. Moreover, long sequences of summit eruptions have continued without a flank eruption. Conversely, long runs of flank eruption rarely occur without an intervening summit eruption.

3.5 Rift Zones

Rift zones radiate from calderas of historically active Hawaiian volcanoes and are sites of most of the eruptive and seismic activity. The rifts are defined by broad zones of linear grabens, fissures, aligned cinder cones, spatter cones, pit craters and associated earthquake foci and geophysical anomalies. Subsurface data and exposure by erosion of the older underlying volcanic foundations on other Hawaiian islands to the north show

the rifts to be composed of multiple, narrow dikes of basalt, generally with steep dips. They generally show continuity to the summit calderas or their deeper, central magmatic sources.

The PGP (fig. 3.3 and 3.6) is on the ERZ of the eastern flank of Kilauea. The volcanic geology of the ERZ has been studied in detail by Holcomb, (1981). Most of this east flank is covered with lavas of no more than a few tens of thousands of years age, with most of its surface less than one thousand years old. The ERZ originates near the summit of Kilauea as a southeasterly trending alignment of vents, craters, and small calderas (figs. 3.3, 3.6, and 3.9). About 5 km south of Kilauea it joins the eastern end of the Kaoe fault zone where it changes in trend to a nearly straight ENE zone that passes through the PGP and continues offshore (Furumoto and Kovach, 1979).

The zone is a very straight topographic high, with a plateau-like character, that appears to be defined by the width of the zone of fissures. The ERZ extends at least 60-80 km ENE (Suyenaga and other, 1978) to the coastline, and the submarine topography indicate ENE extension of several tens of kilometers beyond. The extensional features in the zone, such as normal faults, linear cracks and fissures, and tilted fault blocks, delineate a zone of about 5 km width at the HGP-A well site. The volcanic eruptions on the zone are tabulated (tbl. 3.1) and are described in Section 4.0 of this report. They have been accompanied by seismic activity as is discussed in Section 4.0 and 5.0 and listed in Appendices A, B and C. All, or at least most, of the earthquake activity of the ERZ is directly associated with the volcanic activity. The nearest tectonic activity is along the

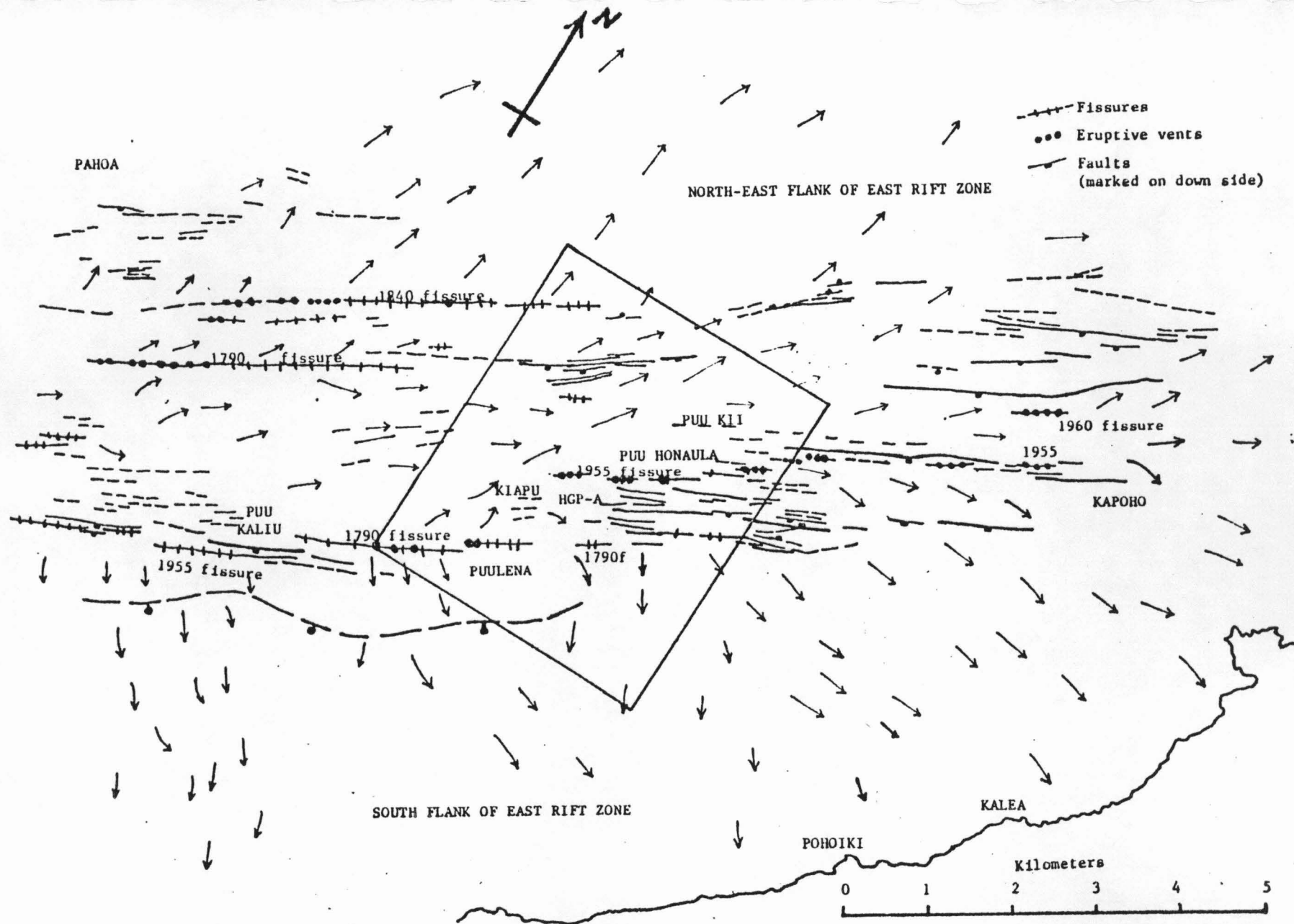


Figure 3.9. Structural map of the Lower East Rift (after Holcomb, 1981). Arrows denote the direction of flowage.

Hilina fault zone, a few kilometers south of and sub-parallel to the rift.

The instrumentation for earthquake studies of the ERZ was poor before about 1960. Since 1960 improvements in the seismologic network have provided good data. Koyanagi and others (1981) document a major improvement in ability to assess the seismicity of this zone in about 1976, although the eastern part of the Puna district has not been fully instrumented. The most recent major eruptions on the ERZ near the PGP were in 1955 and 1960. Furumoto (1978) has modeled the subsurface geologic structure of the ERZ at the PGP, using on seismic refraction and gravity data (fig. 3.5).

The relationship between the ERZ and the central summit caldera has been reviewed by Koyanagi and others (1981). They state:

From seismic and tilt data, Eaton (1962) developed a structural model of Kilauea where magma traced to nearly 60 km depth rises to fill a small storage system a few kilometers beneath the summit. His data further indicated that magma is transported laterally through shallow rift zones to feed eruptions along these linear fissure systems.

The mechanics of magmatic movement in the rift zones were later studied in detail by Fiske and Jackson (1972). The laboratory experiments they conducted using gelatin models demonstrated how stresses from magmatic pressures could create extensive swarms of thin magma-transporting dikes within the rift zones. Also studied in their investigation was how the orientation of shallow rift zones could be influenced by gravitational loading of existing volcanic masses.

Koyanagi and others (1972) described the asymmetric distribution of crustal earthquakes along the East Rift Zone to support the concept that stresses generated by magmatic intrusions are relieved on the seaward, free slopes of the volcano: the north flank is buttressed against the massive Mauna Loa volcano and

remains stable and relatively immobile. Epicenter maps prepared in summary bulletins from HVO since 1962, such as in Koyanagi and others, 1978a, 1978b, 1978c, show the high concentration of crustal earthquakes on the seaward slopes of Kilauea, particularly in 1975-77 during the intensive aftershock activity following a 7.2-magnitude earthquake on November 29, 1975 (see fig. 3.10 of this report). The aftershocks clustered in the south flank along an elongate zone that extended from the southwest rift eastward to about Puu Honuaua on the east rift. The areas north of the east rift, as well as east of Puu Honuaua are contrastingly aseismic. Swanson and others (1976) verified the crustal instability and showed the trend of southward movement of Kilauea's south flank with detailed deformation surveys. They contend that magma forcefully intrudes the rift zones by forming many thin and near vertical dikes. The intrusion forces the wallrocks apart normal to the direction of intrusion ultimately causing the seaward displacement of the south flank.

Zablocki (in Keller and others, 1977) summarized these concepts by putting into perspective his findings from geoelectric surveys of the East Rift Zone, with particular emphasis in the lower part of the subaerial rift southeast of the Pahoia in an area of known microearthquake localization. He described a positive thermal anomaly elongated transverse to the major axis of the rift zone at a place that corresponds to an apparent left-lateral offset of the principal volcanic features that define the surface of the rift zone. He suggested that the buttressing effect of Mauna Loa north of the rift lessens with increasing distance away to the east, and eastward from Puulena the more symmetrical topography and deformation pattern accordingly indicate symmetry in the distribution of stress normal to the rift zone. Such changes in the stress field may cause structural offsets to develop in the rift and may cause magma fed laterally from the summit to accumulate, forming secondary storage zones.

Furumoto (1978), using seismic and gravity data and information gathered from the geothermal well, proposed a crustal model for the geothermal area (see fig. 3.5 of this report). He described the core of the rift as a broad zone that extends downward from a depth of 4 km. This hot zone is overlain by a 2 km thick dike swarm.

The Southwest Rift Zone (SRZ) is similar to the ERZ, and currently is the focus of frequent earthquakes activity, major tilting and probable magmatic movement. This zone appears to be

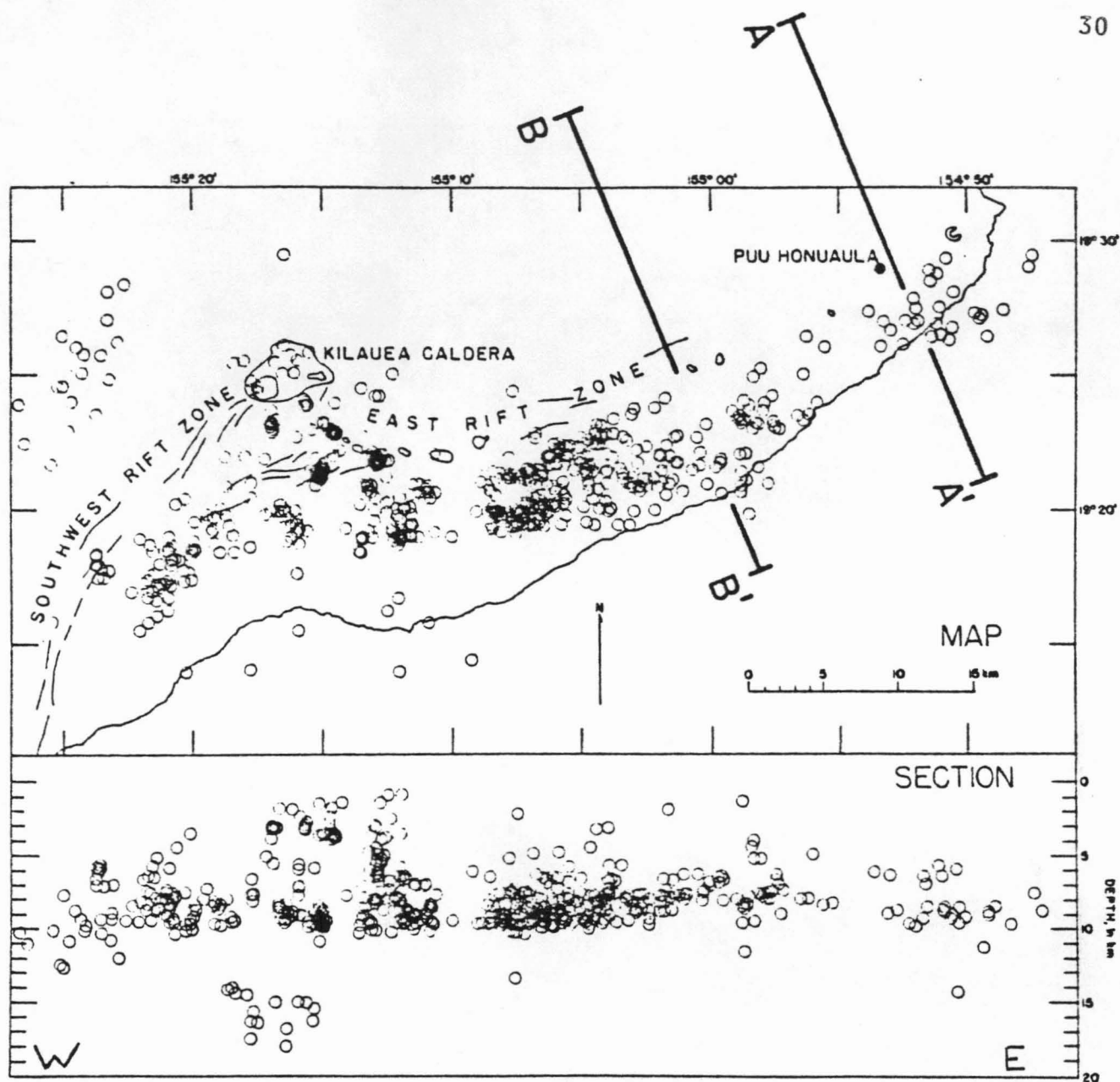


Figure 3.10. Locations of $M_A > 3.0$ earthquakes with focal depth of 0-20 km at Kilauea from December 1975 to December 1977. The Quality of location for most of the events plotted are less than 2 km in standard errors of epicenter (upper plot) and depth (lower plot). A-A' and B-B' are center lines for cross-sectional hypocenter plots prepared in the following figure 4b (Koyanagi and others, 1981).

narrower than the ERZ and does not extend as far offshore. (fig. 3.3 and 3.6). Forceful injection of dikes does not appear to initiate earthquakes of larger size (Swanson and others, 1976), but, like the ERZ, may be associated with frequent and, at times, rhythmic earthquakes. Eruptions from this zone are less frequent than in the ERZ and the total volume of historically erupted material is much smaller.

Historic eruptions, with associated earthquake activity at Kilauea and on its rift systems is summarized in Table 3.1. Sixteen of forty-nine eruptions (about 33 percent) are associated with the ERZ. Many eruptions were preceded within five years by deeper focus upper mantle to shallow-focus crustal earthquakes associated with magmatic movement in the summit region of Kilauea.

3.6 Fault Zones

3.6.1. General Comments

Four prominent fault zones are identified on the island of Hawaii, and in order of increasing distance from the site (fig. 3.3 and pls. 1 and 2) are:

- A. Hilina fault zone,
- B. Koae fault zone,
- C. Hanuapo-Kaoiki fault zone, and
- D. Kealakekua-Kholo fault zone.

The Hilina fault zone is the most significant zone to the PGP, because of both its proximity, and its high magnitude earthquakes. The Koae fault zone has a short length and historically has only low-magnitude earthquakes. This zone is located just south of Kilauea. The Hanuapo-Kaoiki fault zone at the base

of the southeast flank of Mauna Loa and the northwest flank of Kilauea may be an inactive, or less active, antecedent structure to the Hilina fault zone (fig. 3.3 and pls. 1 and 2) and shows little or no historic earthquake activity. The Kealakekua-Kholo fault zone is a subarcuate zone along the western edge of the island.

3.6.2 Hilina Fault Zone

The Hilina fault zone is a branching, complex normal fault zone with an arcuate surface expression trending east-west across the southern flank of Kilauea (fig. 3.3). The zone extends offshore from both its eastern and western ends, and this offshore extent is not well defined. From aftershock distribution following the 1975 earthquake and the tsunami source parameters, the zone appears to have a large offshore extent (Swanson and others, 1976). This fault zone has south-facing, sub-parallel and en eche-
lon fault scarps of up to 500 m height in late Quaternary basalts. The fault morphology of the Hilina fault zone is characterized by block failures that are suggestive of slumping or landsliding. Lavas at the base of the scarp have dips that are rotated landward. This rotation is similar to that observed on blocks affected by landsliding.

This fault has two large historic earthquakes, the 1868 earthquake of poorly known magnitude, about 7.5 to 8.0 as inferred from intensity (Tilling and others, 1976), and the $M_s = 7.2$ earthquake of 1975. The tsunami effects of the 1868 earthquake were greater than that of the 1975 earthquake. The 1868 earthquake is assigned an estimated magnitude of $M_s = 7.75 \pm 0.25$.

The Hilina fault zone appears to be a gravity controlled fault that is affected by dilation from intrusive activity and associated pressure effects by magmas of the south flank of Kilauea and the ERZ. Various workers (Fiske and Kinoshita, 1969; Koyanagi and others, 1972; Swanson and others, 1976) propose that the stress regime and the geodetic deformation is affected by progressive intrusion of dikes and dilation of the ERZ. Failure during the 1975 earthquake by southeastward sliding or thrusting led to an observed geodetic decrease in elevation and southeastward movement of the land area and the companion uplift at the toe of the transported block to cause the tsunami (fig. 3.11). The direction of displacement (fig. 3.12) is in agreement with the maximum stress axis determined from the focal mechanism of the earthquakes (Swanson and others, 1976). During the 1975 deformation, there were associated swarms of earthquakes and ground cracking on the ERZ.

Geodetic data from stations on the north and south sides of the Hilina fault system shows displacements in the same direction but of different magnitudes, with both elongation and shortening of lines across the fault. Surveys of lines across the fault zone in 1970 prove that shortening does occur (Swanson and others, 1976), moreover, the net strain across the zone since 1914 shows overall shortening.

Leveling surveys across the south flank of Kilauea between 1958 and 1971 shows that the north side of the Hilina fault system has been uplifted relative to the south coast by 1.8 to 2.1 m.

The Hilina fault system has long been interpreted as a

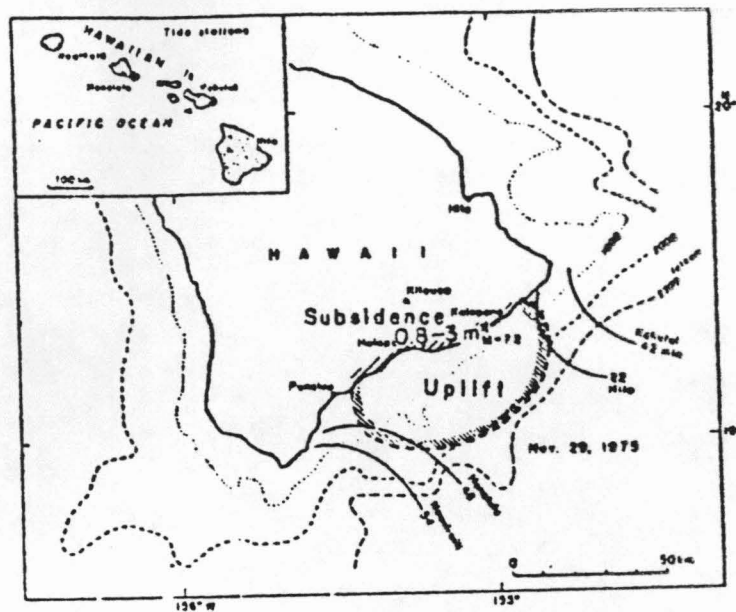


Figure 3.11. Inverse refraction diagram to obtain tsunami generation area showing area of landward subsidence and offshore uplift (from Furumoto and Kovach, 1979).

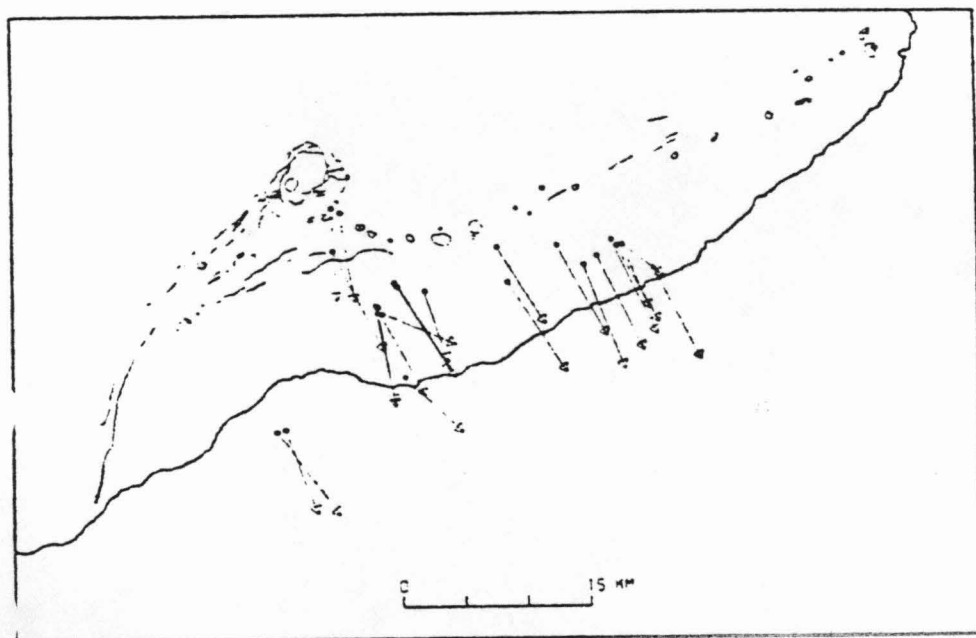


Figure 3.12. Map of south flank of Kilauea on the island of Hawaii showing slip directions. Arrow lengths linearly indicate dip of slip vector with 9 km being horizontal and 0 km vertical (from Crosson and Endo, 1981).

gravity fault zone, the analogy being made with large landslides (Stearns and Macdonald, 1946; Moore and Krivoy, 1964), but this interpretation conflicts with the data suggesting historical horizontal shortening across the system, uplift of its northern side, and southward tilt of the fault blocks. Macdonald (1956) later abandoned the 'landslide' hypothesis, and suggested that tumescence in the summit and rift zones causes near vertical faults with the inland side upthrown.

Study of the focal mechanism of the November, 1975, Kalapana earthquake at the east end of the Hilina fault system led Ando (1979) to propose a near-horizontal slip-plane at a depth of 10 km, with southward movement of the southern flank of Kilauea owing to magma injection of the ERZ. Study of the aftershocks by Crosson and Endo (1981) confirmed a sub-horizontal slip-plane and SSE directed slip vectors, and emphasized the role of a weak horizontal (low velocity) layer at a depth of 10 km on which the south flank of the Kilauea shield is supposed to slide southwards in response to magmatic injection in the rift zone. This model is preferable to the 'landslide' models (Swanson and others, 1976), in that it provides for the accumulation of compressive stresses and vertical uplift of the zone between the Hilina fault system and the ERZ during phases of magmatic injection, and subsequent stress release by southward sliding on a weak layer at or below the base of the volcanic pile.

The available data suggest that the faulting at depth does not break cleanly to the surface, but is distributed or compensated by broad subsidence on the land area, with gently dipping listric faults that extend along the hyaloclastic deposits at

depth and dip SE at between 4° and 10° . Furumoto and Kovach (1979) suggest that the interface is on the ancient sea floor, with the toe of the block moving as a thrust at a depth of 5 to 7 km. These models are in general agreement with the geomorphic, seismologic, geodetic and tsunami data.

3.6.3. Koae Fault Zone

The Koae fault zone defines the northern edge of the mobile south flank of Kilauea (Swanson and others, 1976), as shown in Figure 3.3 and Plates 1 and 2. This fault zone spans the gap between the southwest and ERZ and trends EW a few kilometers south of Kilauea caldera. This fault zone consists of a pattern of en echelon cracks and normal faults with north-facing scarps that are usually less than 5 m high. During initial stages of eruptions or ground-cracking events on the East or Southward rift zones, the Koae fault zone has many more earthquakes from seismic swarms than does the Hilina fault zone (Swanson and others, 1976). Swanson and others (1976) indicate that the Koae fault zone is not generally the site for eruptions, but is more of a "tear away zone" as the result of dilation due to magma intrusion into the neighboring SRZ and ERZ.

3.6.4. Hanuapo-Kaoiki Fault Zone

The Hanuapo-Kaoiki fault zone follows the SE boundary of Mauna Loa (fig. 3.3), and is of uncertain activity. No historic flows or eruptions have occurred along this zone and it is not characterized by well defined seismic activity, although some earthquake epicenters are on, or near, this zone. This zone is farther from the siting area than the Hilina fault zone and is of

shorter exposed length and presumably of lower seismic potential. No maximum magnitudes are assigned to this fault zone.

3.6.5. Kealakekua-Kholo Fault Zone

This zone has an accurate pattern that is similar to the Hilina fault zone on the south flank of Kilauea, and may have a similar gravitational relation to the actively growing western flank of Mauna Loa. The length is poorly defined, because much of the fault zone is offshore. The $M_s = 6.25$ earthquake of 1950 is the maximum historic earthquake for this fault zone.

4.0 VOLCANIC-RISK ASSESSMENT OF THE PUNA DISTRICT

4.1 Volcanic and Structural Features of Lower East Rift Zone

4.1.1 Structure

For the purpose of this report, the Lower East Rift Zone (LERZ) is the sector ENE of Puu Kaliu (elevation 800 ft or 200 m above sea level) to sea level. Topographically, the zone runs along the crest of a broad ridge 3 km wide, from which gentle slopes descend to the NE and steeper slopes to the SE. Structural and volcanic features consist of faults and open fissures, some without lava and others with aligned spatter cones and ramparts of agglutinate. Faults and fissures are remarkably linear and parallel along a trend of N 55-60 E for distances of up to 10 km (fig. 3.9). Cinder cones and small lava shields (with and without craters), steep-sided tuff rings with deep craters resulting from phreatic eruptions, and broad expanses of lava are scattered along the central part of the rift zone.

The distribution of faults in the lower ERZ (fig. 3.9) suggests a concentration in the Kapoho area, and a scarcity in the PuuKaliu - Kiapu area. Numerous faults have been mapped in the middle part of the ERZ (west of the area shown in fig. 3.9), especially on its northern side (Holcomb, 1981). The scarcity of faults in the western side of the map is because they have been buried under the extensive lavas of the 1790 and 1840 eruptions.

4.1.1.1 Fissures The 3 km-wide zone of fissures and faults coincides with a zone of eruptive vents. No vents have been identified outside the zone on the flanks of the ridge. There is

abundant evidence of vent alignment along fissures, but there is no example of vents that were fed from faults, and this indicates that the mechanisms of fissuring and faulting are different. Since the surface rocks of the LERZ are mostly less than 500 years old, the structural features are well preserved and commonest in the oldest lavas that have escaped inundation during more recent eruptions. The oldest identifiable fissure in the LERZ fed a chain of small shields, spatter cones, and cinder cones along the 3 km long Puu Kii-Halemahina alignment, which is thought to be 300 to 500 years old by Holcomb (1981), but is thought to be more than 750 years old by R. J. Moore (personal communication, 1981). This fissure is centrally located in the LERZ and flows from it descended the LERZ to sea level east of Kapoho.

The next youngest activity was from the Puu Honaula fissure located immediately south of the Puu Kii zone. Three cinder cones, were built on low lava shields along this fissure. Another fissure close to the south edge of the LERZ was also active and both are dated at 500 to 750 years B.P. (R. J. Moore, pers. comm.).

Very extensive lavas of the eruptive phase of 1750 issued from fissures along much of the length of the ERZ. Just west of the LERZ long fissures from this eruption follow the northern and southern edges of the rift zone (fig. 3.9), and the flows flooded much of the crest and SE flank.

A 9 km fissure at the northern extremity of the ERZ opened during 1840 (fig. 3.9) and discharged lava about one mile down the NE flank. The volume of this flow totalled about 281,000 cubic yards and covered an area of 6.6 square miles. An addi-

tional discharge of lava is believed to have come from vents below sea level.

The fissures formed during the 1955 eruption are short and are off-set en echelon to the left toward to NE. In the middle part of the ERZ the main fissure is at the southern margin of the zone; to the ENE it steps toward the center of the rift. A gap of about 2 miles separates the two offset sections, and the HGP-A well is sited near the NNE end of this gap.

The 1960 eruptions took place from a short fissure near the NE end of LERZ, near the center of the Kapoho graben (right side of fig. 3.9). The 1977 flank eruptions occurred in the middle part of the ERZ, to the WSW of LERZ, on a single fissure near the center of the zone.

Historic fissures have formed immediately prior to eruptions, and developed by rapid growth of cracks to widths of up to 30 cm in a few hours, during swarms of microearthquakes. Fissures rarely exceed 1 meter in width and extend laterally at rates of up to 100 meters per hour. For each eruptive episode they have developed in different places within the width of the ERZ, and no case of regeneration of a pre-existing fissure is known. Each phase of fissuring and eruption typically occurs along a single linear fissure system. During one eruption, that of 1750, there may have been simultaneous eruption from parallel fissures, but this is very exceptional. The fissures represent the result of surface dilation and tensile fracture of rock due to dike injection at depth. The mechanism by which they are formed is summarized in a later section (Section 4.2.4.3).

4.1.1.2 Faults Zones of parallel normal faults of small displacement occur throughout the ERZ and are best developed within the northern part of the middle rift zone and in the Kapoho area of the LERZ (fig. 3.9). The displacement pattern gives rise to step-faults downthrown to the NW and SE. Along the southern edge of the LERZ there is a predominance of minor faults downthrown to the SE.

The ERZ faults show displacements of only a few meters, even where they cut the oldest rocks, and they are remarkably linear, with no tendency to curve or branch. In these respects they differ markedly from faults of the Koa'e and Hilina fault systems, which are long systems of curving and branching faults with large displacements (up to 500 meters) that evolved over long periods of time. The ERZ faults and the systems cutting the south flank of Kilauea are not only spatially separate but show contrasts of form and history reflecting their distinctly different origins.

Faulting in the LERZ normally occurs during or immediately before an eruption in the same part of the rift. Examples are the eruptions of 1955 and 1960. In 1924, however, strong faulting was observed in the LERZ without an observed eruption of lava (Jaggard and Finch, 1924). Many earthquakes were felt at Kapoho on April 21, 1924, and the next day a fissure 15 feet wide opened across the coast road. Vertical displacement reached 8 to 12 feet. Near Kukii a graben block 20 feet wide sank 6 feet, and numerous cracks up to 3 feet wide developed nearby. This episode is thought to have been due to flow of magma into the lower ERZ, because it was accompanied by rapid drainage of the Halemaumau pit crater. The occurrence of earthquakes in the submarine part

of the ERZ during the same period suggests that an eruption below sea level may have drained magma from the ERZ.

4.1.2 Examples of Recent Flank Eruptions

4.1.2.1 1955 East Puna Eruption (Macdonald and Eaton, 1964): After a repose of 273 days, Kilauea began to erupt on the morning of February 28 from a new fissure on the southwest slope of Puu Honaula, 24.5 miles ENE of Kilauea caldera (fig. 4.1). The outbreak was preceded for several months by earthquakes, which gradually increased in number to several hundred a day just before the eruption. Discharge of lava continued at the initial vents for only 28 hours and on March 1 was replaced by mild phreatic explosions and clouds of steam.

On March 2, a new series of earthquakes accompanied the formation of fault scarps and opening of fissures 2 miles farther northeast, and at 1415 hours lava broke out on the fissures. Through the next 2 days the eruptive fissures gradually extended another 2 miles NE, to the outskirts of Kapoho village. Lava fountains at the main vents reached a height of at least 800 feet, and flows from them covered approximately 1,100 acres. Activity in that area stopped on March 6.

On March 6 a new series of earthquakes commenced, originating in the area 2 to 12 miles southwest of the initial outbreak, and a new outbreak in that area was predicted. On March 12 lava broke out in that region, and between then and March 27 a series of new vents developed along the rift zone for 4 miles to the southwest. Three lava flows from these vents entered the ocean.

Activity ceased on April 7 but resumed weakly on April 24

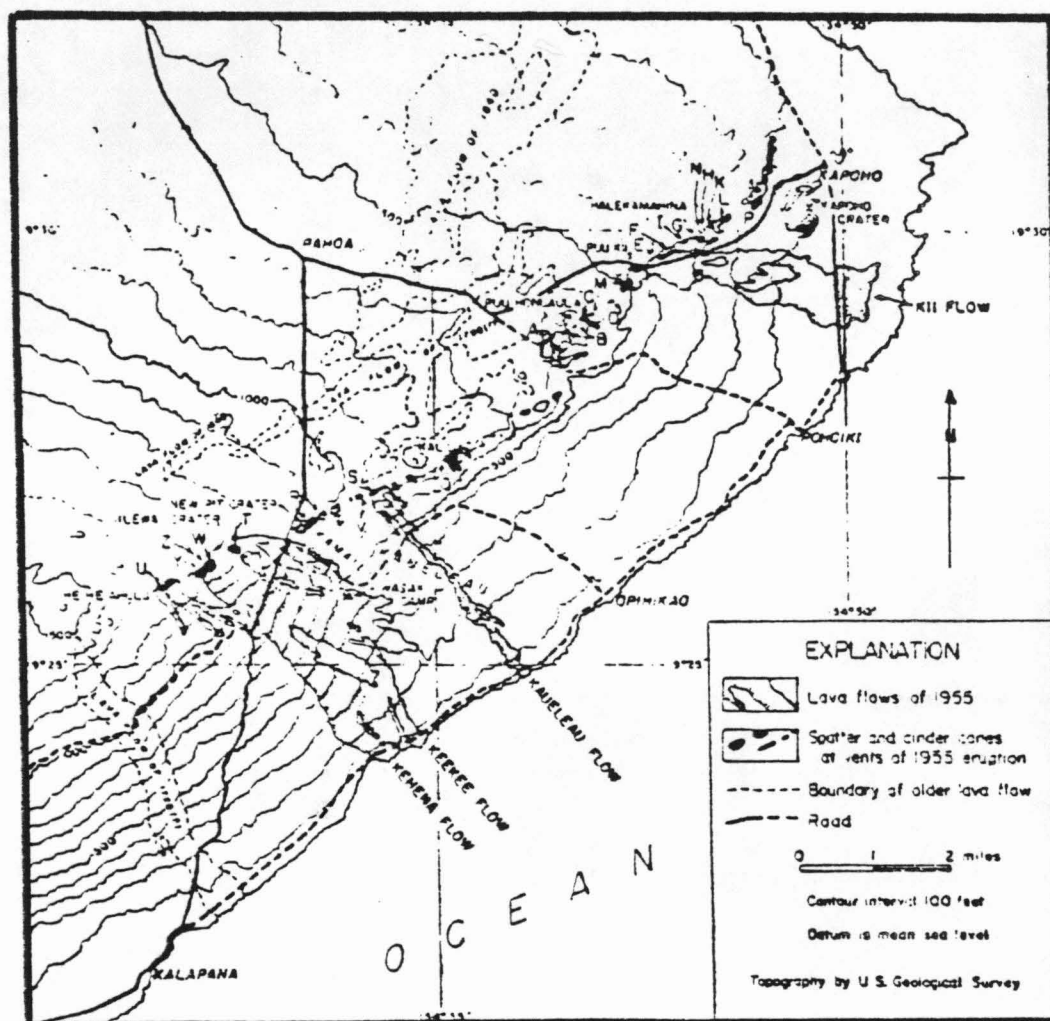


Figure 4.1. Map of the eastern part of the Puna District, Island of Hawaii, showing the vents and lava flows of the 1955 eruption of Kilauea Volcano (Macdonald, 1959).

and gradually increased until a strong resurgence occurred on May 16. New flows covered the upper parts of earlier flows, and some new area, including one village. The eruption ended abruptly on May 26.

The volume of erupted material was approximately 141 million cubic yards. The flows covered an area of about 3,900 acres, of which 1,100 acres was under cultivation. Approximately 6.3 miles (10 km) of public road and many miles of cane-field road were buried, and 21 houses were destroyed. There were no human casualties.

The erupted lavas were basalts, becoming slightly more mafic as the eruption progressed. The temperature of lava as it was erupted was approximately 1,100 degrees centigrade.

Tilt records at the Pahoa seismograph station (north of the ERZ), and remeasurement of a triangulation network, showed that northward tilt began two days before the start of the 1955 eruption, and occurred again before the second and major eruptive phase. This suggests that dilation of the ERZ took place before and during the ground fissuring and shallow microseismic activity that immediately preceded the eruption. Ground deformation consisted of a general uplift of the LERZ of at least 0.4 m, accompanied by a 0.3 - 0.4 m subsidence of the zone adjacent to active fissures. Horizontal displacements were normal to the LERZ and ranged from 0.2 to 1.6 m. During the easterly extension of the fissure a pre-existing fault NW of Kapoho was rejuvenated, with a new displacement of 1.6 m (SE side down).

4.1.2.2 1960 Kapoho Eruption (Richter and others, 1970): On

the evening of November 14, 1959, after a quiet period of nearly five years, Kilauea Volcano renewed activity with an eruption in Kilauea Iki, a collapse crater adjacent to the main caldera. The eruption consisted of 17 separate eruptive phases, which ranged in duration from one week to less than two hours. At the cessation of activity on December 20, 1959, Kilauea Iki Crater held 50 million cubic yards of lava in a lake 335 feet deep.

After the summit eruption, shallow earthquake hypocenters migrated out along the ERZ and rose from 2 km to very shallow depths. On 13 January, an intense series of earthquakes near Kapoho was accompanied by subsidence of a graben bounded by two parallel faults trending N 60 E (fig. 4.2). The southern boundary fault running through the village of Kapoho had been active in 1924, when a maximum of 3.8 meters displacement was measured, and again in 1955 when minor displacement was observed at the west end of Kapoho. By the end of the day displacement reached a maximum of about 1.1 meters and the total length of the fault measured about 2.7 km. Similar movement on the northern fault (near the town of Koae; see fig. 4.2) reached a maximum displacement of 4 feet (1.3 meters) and a length of 3.04 km. At 1935 hours an eruption broke out along a 320 meter fissure somewhat north of the center of the graben and parallel to the boundary faults. No lava emerged from the faults. Fountaining up to heights of 100 meters was soon accompanied by a discharge of lava, mainly from the east end of the fissure. The fissure reached a maximum length of 370 meters around 2130 hours at which time activity began to concentrate in the central part of the fissure, and the rate of discharge of lava continued to increase.

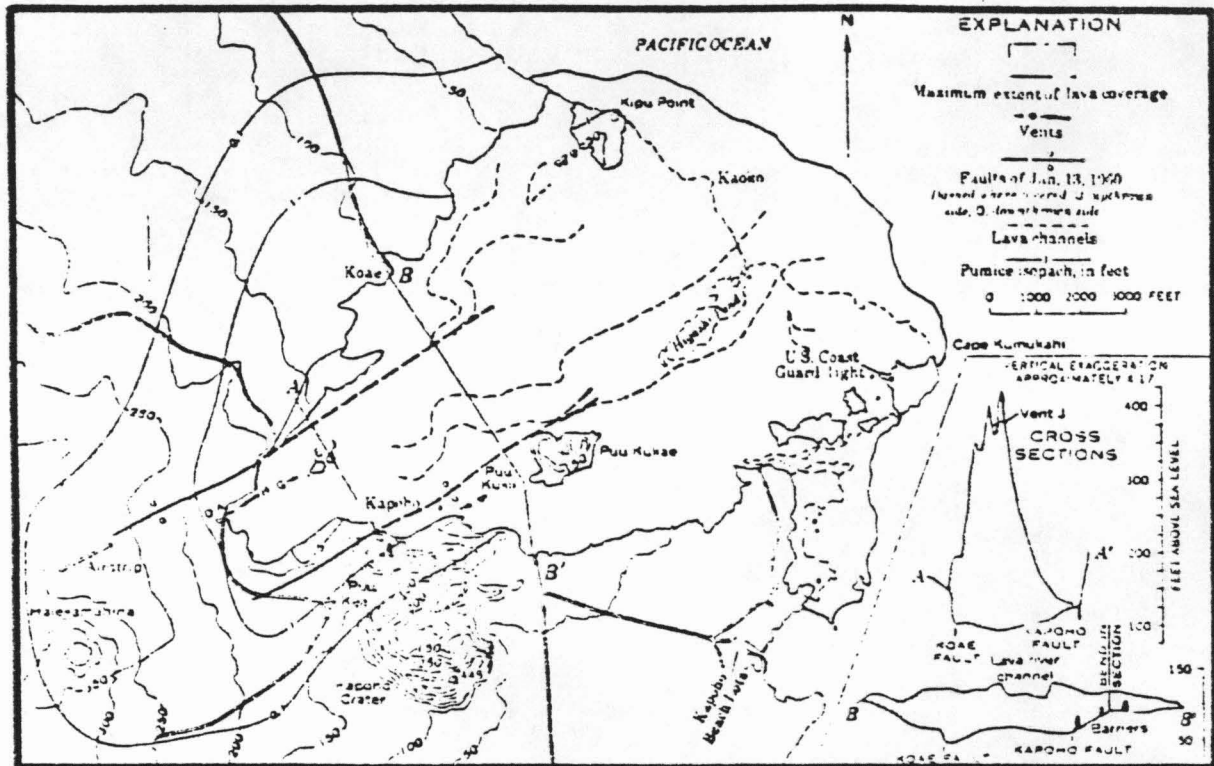


Figure 4.2 Map showing the eruptive fissure of the 1960 eruption (Richter and others, 1970) in the Kapoho area of the Lower East Rift Zone, and the active faults of the Kapoho graben. The maximum extent of the lava field, and isopachs of the pumice blanket are also shown. The 1960 lavas were unusually thick - see cross-section B-B' (inset).

4.1.2.3 The 1977 eruption (Moore and others, 1980; Dzurisin and others, 1980): Kilauea volcano began to erupt on September 13, 1977, after a 21.5-month period of quiescence. The eruption was preceded by four intrusive events during 1976 and early 1977. Motion of magma was reflected in deflation of the summit area, migration of shallow earthquakes into the upper and middle ERZ, extensional deformation across the Koa'e fault, and inflation of the ERZ. Harmonic tremor in the upper and central ERZ and rapid deflation of the summit area occurred for 22 hours before the outbreak of surface activity.

On the first night, spatter ramparts formed along a discontinuous, en echelon, 5.5 km-long fissure system (fig. 4.3) that trends N 70 degrees E between two prehistoric cones, Kalalua and Puu Kauka. Activity soon became concentrated at a central vent that erupted sporadically until September 23 and extruded flows that moved a maximum distance of 2.5 km to the east. On September 18, new spatter ramparts began forming west of Kalalua, extending to 7 km the length of the new vent system. A vent near the center of this latest fissure became the focus of sustained fountaining and continued to extrude spatter and short flows intermittently until September 20.

The most voluminous phase of the eruption began late on September 25. A discontinuous spatter rampart formed on a 700 m long segment near the center of the new, 7 km-long fissure system; within 24 hours activity became concentrated at the east end of this segment. One flow from the 35 m-high cone that formed at this site moved rapidly southeast and eventually reached an area 10 km from the vent and 700 m from the nearest house in the

Sea water appears to have entered the east end of the fissure about this time, because dark ash-laden steam began to be discharged from the east end of the fissure.

During the next 37 days of virtually uninterrupted activity, 160 million cubic yards of lava, covering about 2,500 acres, were erupted (fig. 4.2). The lava was at first confined to the graben and flowed down the northern side until it reached the sea around 800 hours on the 15th. After the 19th the lava began to over-top the margins of the graben and spread to both the north and south. An effort was made to restrict the southward flow by a series of three successive artificial barriers, but all of these were eventually overrun. Nearly all the lava was of the aa type; the main exceptions were channels within the central interior of the flow and small toes that from time to time broke out from the advancing front or through the base of barriers.

A cinder cone at the main eruptive vent grew to a height of about 64 meters and discharged fountains of incandescent scoria to heights of 300 meters above the vent. The small villages of Kapoho and Koa'e, a United States Coast Guard station, and a number of residences along the coast were destroyed.

Almost concurrent with the beginning of the flank eruption, the summit area of Kilauea rapidly deflated as magma moved from beneath the summit into the rift zone to the flank eruption. Culmination of the summit subsidence occurred on February 7, 1960, when the floor of Halemaumau - a deep crater in Kilauea caldera - collapsed because of the withdrawal of the still-fluid core of the 1942 lava lake. Two smaller collapses on March 9 and March 11 in Halemaumau marked the end of the eruption.

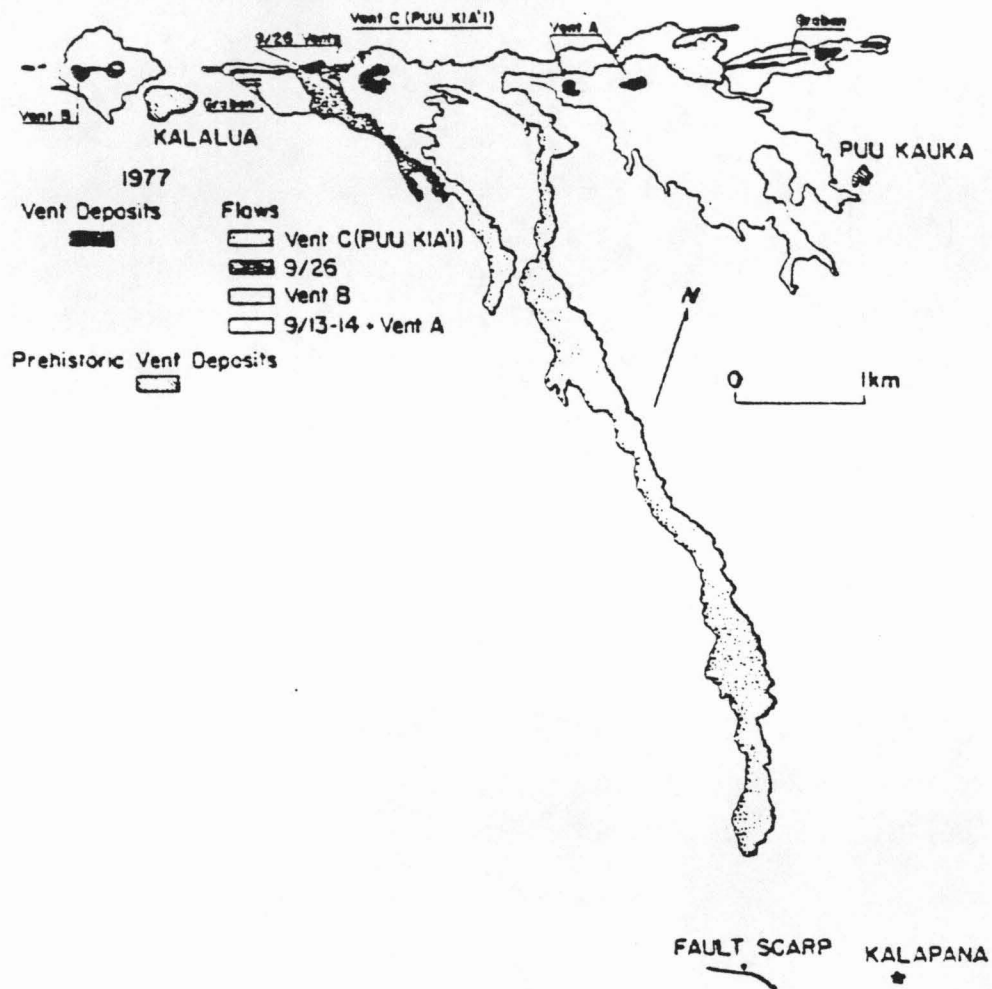


Figure 4.3. Map showing eruptive products and active structures of the 1977 eruption in the middle East Rift Zone (Moore and others, 1980).

evacuated village of Kalapana.

An estimated total volume of 35 million cubic meters was produced during the 18-day eruption. Samples from active vents and flows are differentiated quartz-normative tholeiitic basalt, similar in composition to lavas erupted from Kilauea in 1955 and 1962. Plagioclase is the only significant phenocryst; augite, minor olivine, and rare orthopyroxene and opaque oxides accompany it as microphenocrysts. Sulfide globules occur in fresh glass and as inclusions in phenocrysts in early 1977 lavas; their absence in chemically-similar basalt from the later phases of the eruption suggests that more extensive intratelluric degassing occurred as the eruption proceeded. Bulk composition of lava varies somewhat during the eruption, but the last basalt produced also is differentiated, suggesting that magma withdrawn from the summit reservoir during the rapid deflation had not yet been erupted.

4.1.3 Frequency of Eruptions in the East Puna District

Considering only the lower ERZ, the average frequency of lava flows for the 231 years of recorded activity has been one eruption per 46 years. Because the spacing of eruptions is so irregular and the historic record contains only a small number of such events, this average has little meaning in terms of the probability of an eruption in a given period of time. Moreover, the frequency of lava flows at an individual site within this zone is much lower than that of the zone as a whole.

4.1.4 Deformation Associated with ERZ Eruptive Phases

A wealth of data suggests that the Kilauea magmatic system

consists of a vertical holding reservoir 2 to 5 km beneath the summit caldera. This reservoir is periodically fed by primary magma from depths of about 65 km, which usually causes inflation of the summit region and numerous shallow earthquakes owing to failure of the volcano superstructure. Inflation may be followed by summit eruptions, or by deflation accompanied by migration of seismic activity as a result of lateral movement of magma into a rift zone at depths of 3-5 km. Upward movement of magma under the rift zone (probably displacement of magma remaining from previous injections) causes tensile failure and dike injection accompanied by shallow earthquakes, dilation and uplift of the rift zone. As dikes ascend, fissures extend to the surface and widen rapidly, begin to emit fumes, and often emit lava fountains along their central parts. The fissures extend laterally at rates of up to 100 meters per hour.

The sequence of events during a typical ERZ eruption starts with shallow earthquake swarms of decreasing focal depth, followed by dilation of the active zone, formation of fissures, faulting and/or rejuvenation of nearby pre-existing faults, followed by eruption. The premonitory seismic and dilational phases may last as little as two days, and fissuring followed by eruption may occur in a few hours. This sequence may be repeated as a fissure extends laterally, or as successive phases of magmatic injection take place during a protracted eruption.

Seismicity of the rift zones is concentrated in a zone 8 km wide under the rift zones and immediately to the south. Hypocenters are concentrated at depths of 5 to 10 km (fig. 4.4), with a very sharp decrease in the number of earthquakes at focal

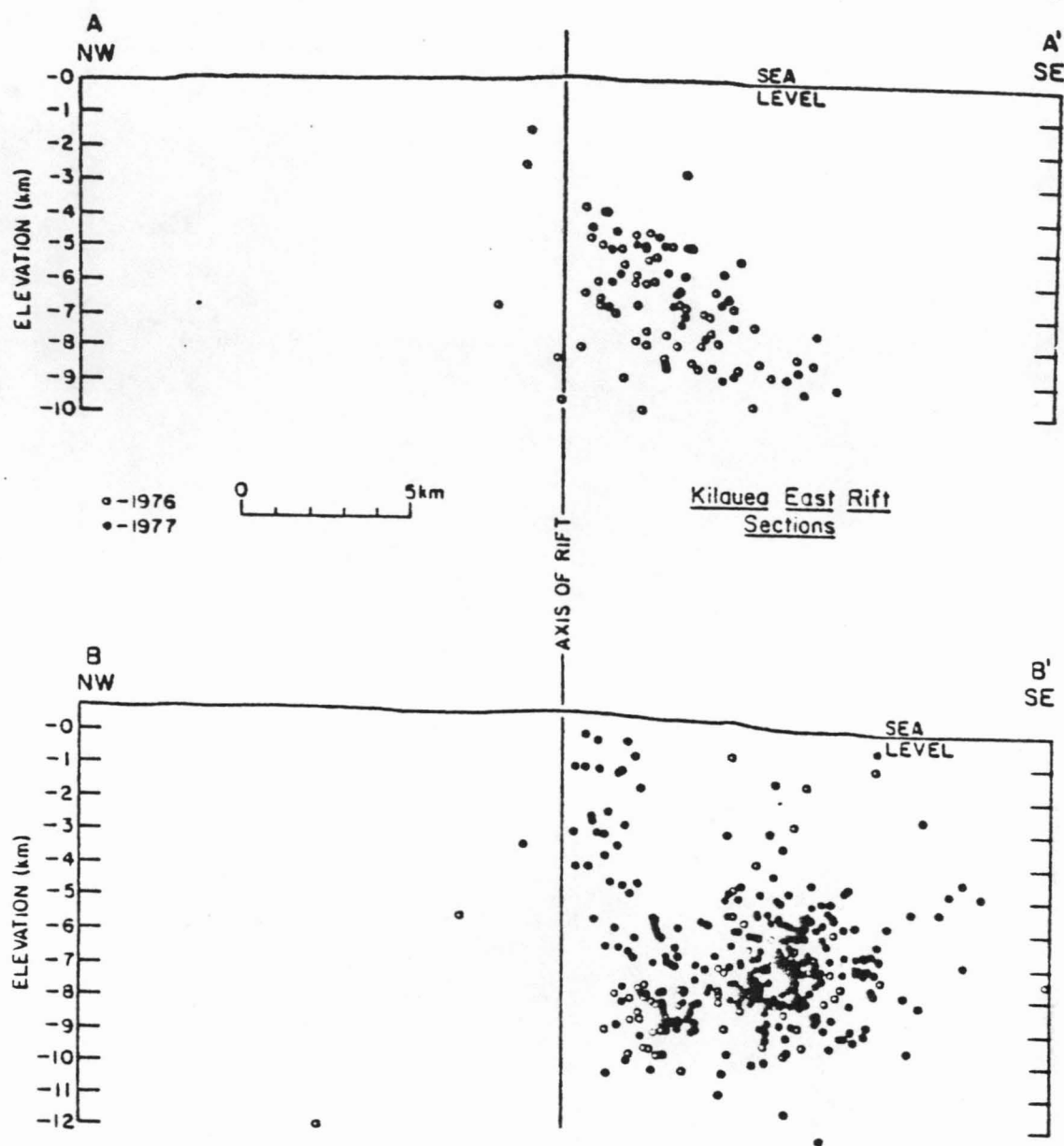


Figure 4.4. Earthquake hypocenters plotted within 10-km wide sections centered on lines A-A' and B-B' oriented normal to the rift zone as shown in Figure 3.10. Earthquakes of all magnitudes and with standard errors in epicenter and depth less than 2.5 km are included. Hypocenters for earthquakes in 1976 are marked with open circles and those in 1977 are indicated by black dots. The column of progressively shallow earthquakes immediately south of the axis of the rift in the middle East Rift Zone in section B-B' mainly occurred about the time of the September 1977 mid-east rift eruption (Koyanagi and others, 1981).

depths greater than 10 km (fig. 3.10). Earthquake epicenters cluster along the ERZ during the early period of an eruption, but are dispersed in the area of the Hilina fault system during the middle and later periods (Swanson and others, 1976). The north flank of the ERZ is strikingly aseismic, and the seismicity is strongly asymmetrical in a north-south direction, showing the tectonic instability is concentrated in the ERZ, within its south flank, and at depths of less than 10 km within the lower part of the volcanic superstructure and above the depressed top of the prevolcanic oceanic crust. Seismic sections across the ERZ (fig. 4.4) show that hypocenters define a diffuse zone dipping at about 45 deg. to the SSE (Koyanagi and others, 1981).

4.1.4.1 Horizontal Displacements in the ERZ: Horizontal displacements across the ERZ and the south flank of Kilauea have been obtained from triangulation surveys in 1896, 1914, 1949, 1958, and 1961, and from geodimeter trilateration surveys in 1970 and 1971 (Swanson and others, 1976). The observed displacements are large and systematic: displacement vectors are normal to the trend of the ERZ, and displacements are associated in time and space with fissuring and eruptive events (figs. 4.5A and B). During the 1955 eruption the Puu Kaliu and Puu Honaula stations north of the fissure were displaced north relative to stations far to the north (fig. 4.6). Stations to the south of eruptive fissures and on the south coast show larger SSE displacements (fig. 4.5; B, D, E and F). In a few cases horizontal displacements can be related to specific events in the ERZ: During the 1955 eruption there was 210 cm of extension near Puu Honaula, and in 1969 a 2 km wide zone west of Alae Crater in the upper ERZ

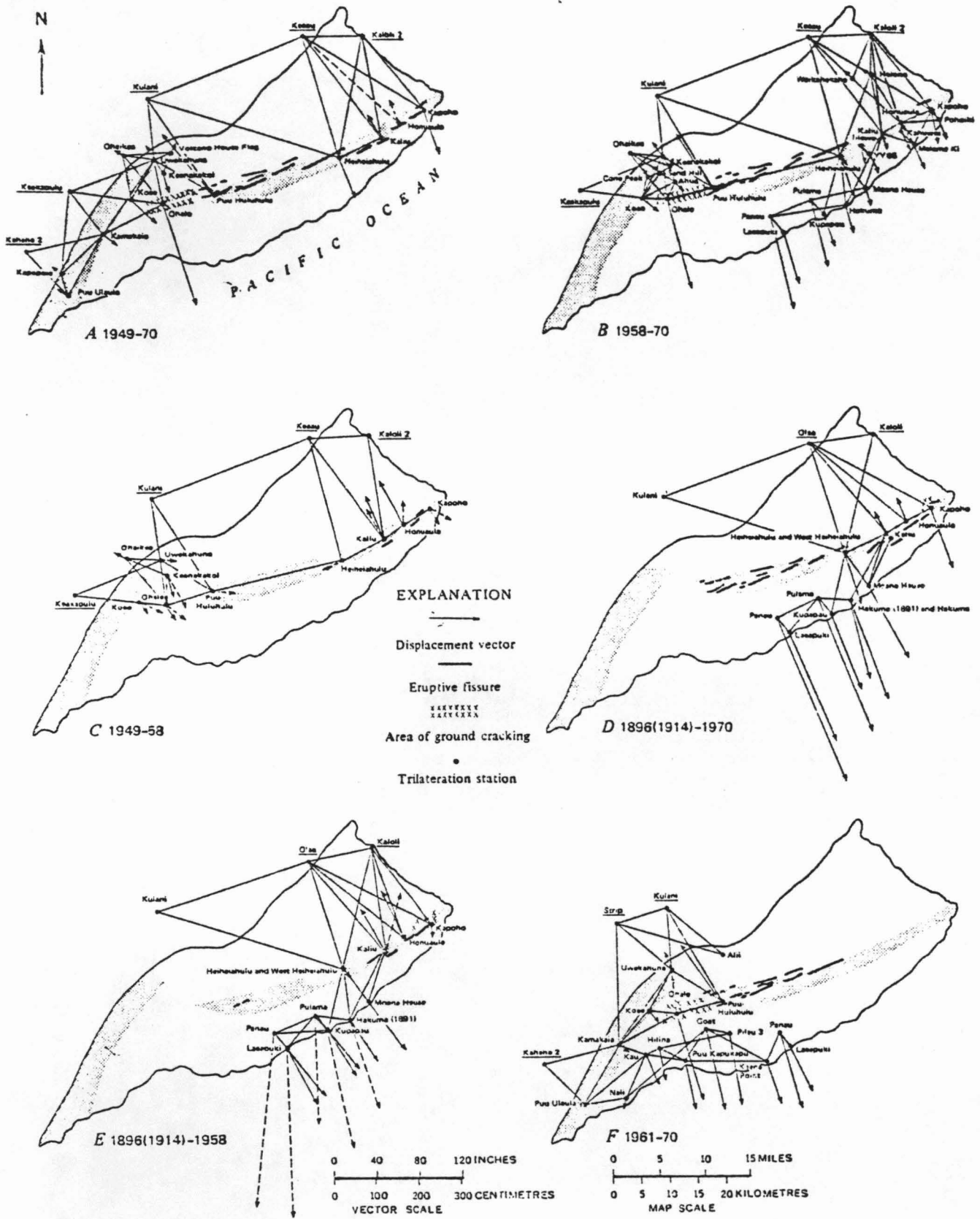


Figure 4.5. Horizontal displacements of trilateration stations for various periods during the years 1896 - 1970. Base stations for the determination of displacement vectors (arrows) are underlined (Swanson and others, 1976).

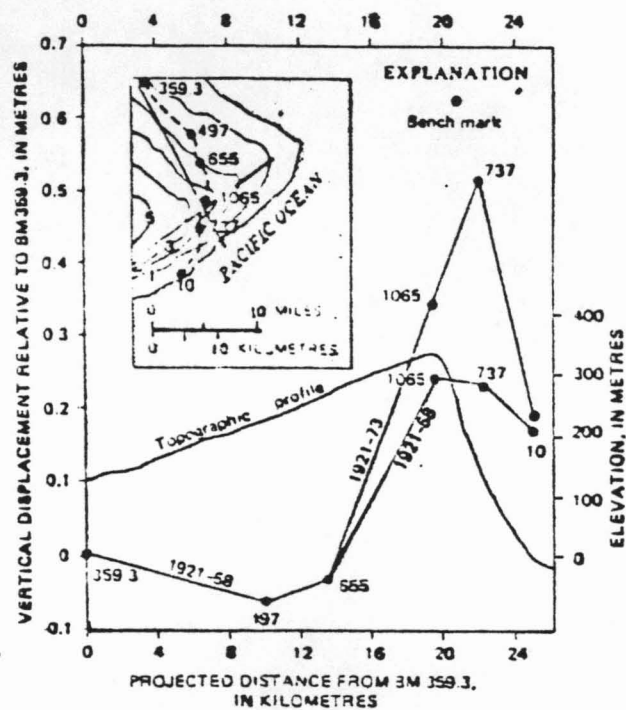


Figure 4.6. Vertical displacement and topographic profiles across Lower East Rift Zone and eastern part of south flank between 1921, 1958, and 1973. Datum is 1958 elevation of BM 359.3. Inset shows location of bench marks, leveling route (dashed line), line of topographic profile (light solid line), and generalized eruptive fissures for 1955 eruption (heavier solid lines). Displacement data are projected onto line of topographic profile. Contour interval on inset map is 100 m (Swanson and others, 1976).

extended 105 cm. These extensions are of the same magnitude as the aggregate width of observed fissures, showing that the fissures, and to a much lesser degree the faults, are responsible for most of the strain. The evidence suggests that the dilations of the ERZ immediately preceding eruptive events, are accompanied by surface fissuring, which result in relative horizontal displacements of the order of 1-2 meters.

4.1.4.2 Vertical Displacements in the ERZ: Surveys of benchmarks along the Pahoia-Kalapana highway were made in 1921, 1958, 1969, and 1973. These indicate 0.2 m of uplift of the ERZ during 1921-1958 (fig. 4.6), and a progressive uplift of 0.3 m during 1958-1973 (fig. 4.7A). These uplifts are broadly sinusoidal in shape and are centered 0.5 to 1.5 km south of the axis of the ERZ. The 1958-1973 displacement profiles show development of a narrow graben at an elevation of 270 m (840 feet) on the south flank of the middle ERZ, but this cannot be identified with any mapped structure.

Another levelling line extends along the Pahoia-Pohoiki highway, which passes the HGP-A well site (fig. 4.7B). This shows progressive development of a 0.12 m subsidence with its axis close to the line of 1955 fissures, which has been interpreted as due to thermal contraction following the 1955 eruption (Swanson and others, 1976). We prefer to interpret this subsidence as due to residual elastic extensional strain, or to withdrawal of magma from the deeper parts of the 1955 dike system.

Data on vertical displacement therefore suggest that the south flank of Kilauea has been increasingly uplifted toward the ERZ and Koa'e fault system, with a maximum displacement within or

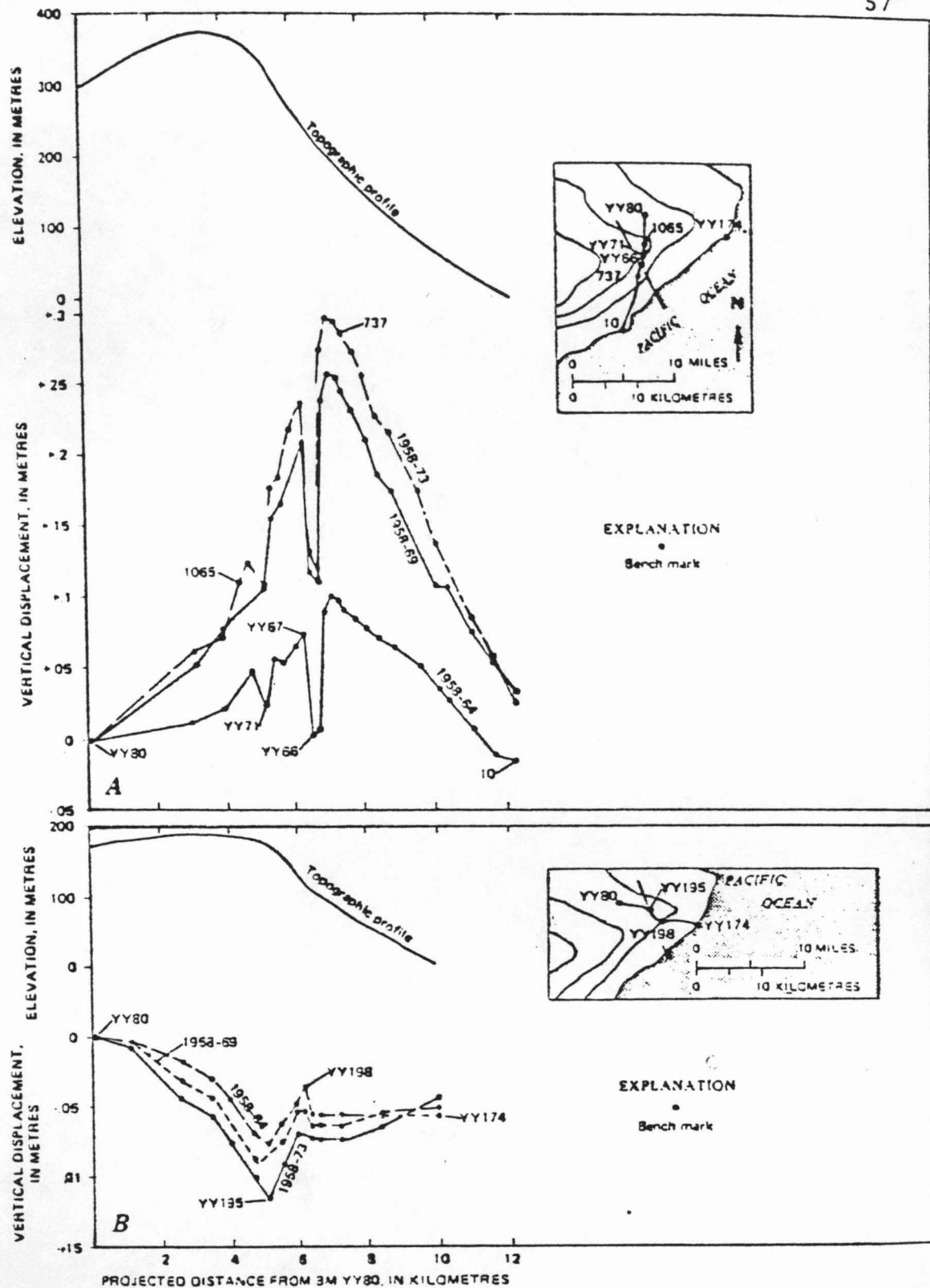


Figure 4.7. Vertical displacement and topographic profiles across Lower East Rift Zone of Kilauea between 1958 and 1973. (A) Profiles between BM YY80 (Pahoa) and BM 10 (Kalaupana); (B) Profiles between BM YY80 and BM YY174 (Pa hoiki). Datum is 1958 elevation of BM YY80. Inset maps show locations of leveling route, key bench marks, and line of topographic profile. Displacement data are projected onto line of topographic profile. Contour interval of inset maps is 150 m (Swanson and others, 1976).

just south of the rift zone. Records of tilt near the ERZ show that phases of uplift correlate with periods of shallow seismicity that precede or accompany intrusive and/or eruptive events.

4.1.4.3 Mechanical Models of ERZ Deformation: The curvature of the Kilauea rift zones, their parallelism to the strike of the southeast flank of Mauna Loa, and the asymmetry of structure across the volcano have been attributed to the gravitational loading of the Kilauea volcanic pile on the flank of Mauna Loa. The north flank of the volcano is buttressed, whereas the south flank is free to move SSE in response to dilations caused by magma injections in the rift zones (fig. 4.8) The injections into the rift zone occur during the filling of the high level magma reservoir beneath the summit, and are a result of the ascent of magma to the surface and the tumescence of the summit region. This creates a hydraulic head in the magma column adequate to cause lateral injection of magma into the still molten roots of the rift zone. Increased magmatic pressure then results in lateral and upward injection of dikes.

The deformation that accompanies upward injection of a dike has been analyzed theoretically (Koide and Bhattacharji, 1975a and b; Dieterich and Decker, 1975; Pollard and Holzhausen, 1979), and excellent observations of such deformation have been made in Iceland (Bjornsson and others, 1979). When the fluid pressure at the top of a dike exceeds the least horizontal stress in the adjacent rock, tensile failure can occur at the apex of the dike, and a fissure can propagate upward in a plane normal to the least principal stress in the rock. Under a ridge such as the ERZ the plane of tensile failure would be steep and located below the

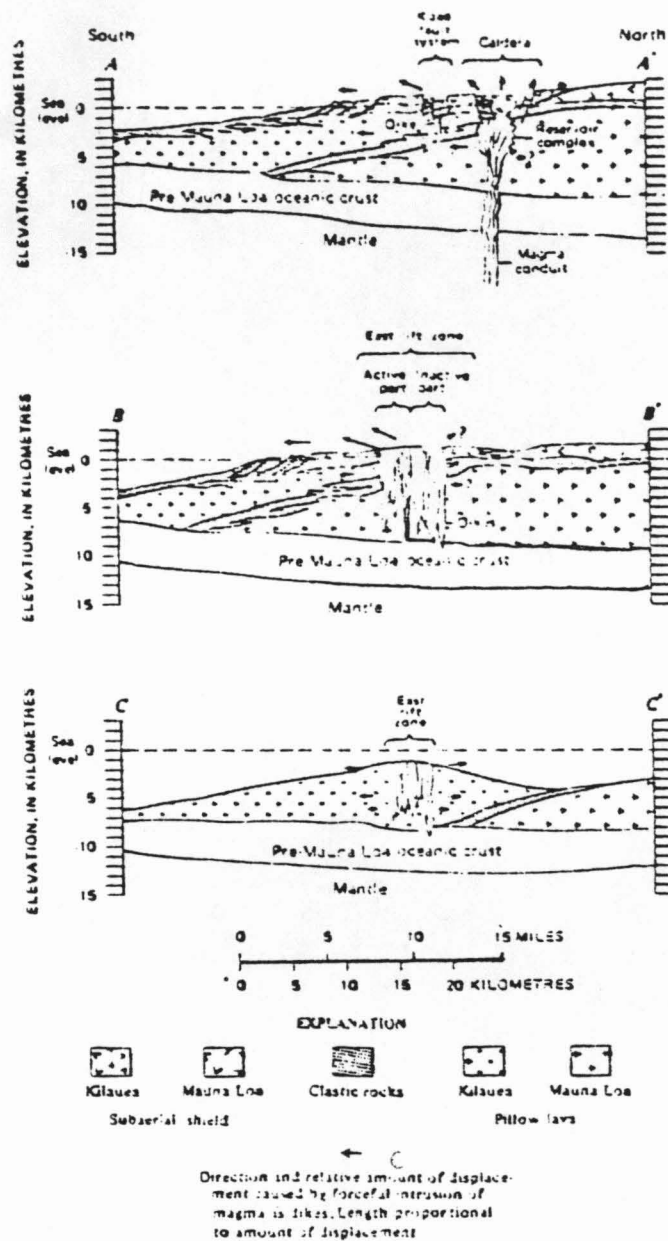


Figure 4.8. Crustal structure models across the summit region (A-A'), East Rift Zone (B-B'), and the submarine part of the Lower East Rift Zone (C-C'), showing the relation between injection into the rift zone and faulting in the Hilina fault system according to the "landslide" model (Swanson and others, 1976).

axis of the ridge (Fiske and Jackson, 1972). The rate of upward propagation of the crack depends on the magmatic pressure and on the speed with which magma can rise. At any instant during ascent the region between the apex of the dike and the free surface consists of two parts: A far field in which horizontal compressive stress is increased, and slight upward deformation of the surface occurs, and a near field of conical cross-section above the dike in which horizontal stresses are decreased and the surface subsides. Between these two regions there are two surfaces of maximum shearing stress that are potential fault surfaces. Thus the surface deformation above an ascending dike, when it has reached 100 - 200 m below the surface, consists of a broad, slight uplift, with a narrow central depression cut by a fissure. On each side of the fissure normal faults of small-displacement may develop to form a graben, or pre-existing faults may be re-activated.

The width of the zone that is affected by faulting during a dike injection episode is determined by several unpredictable factors, such as the number of dikes and their widths (the total horizontal strain), the depth of the top of the dikes, their attitude, the presence of pre-existing planes of weakness, and the cohesive shear strength of the rocks (Koide and Bhattacharji, 1975a and b; Dietrich and Decker, 1975). The graben that formed during the 1977 eruption was only 100 m wide, whereas the Kapoho graben that subsided during the 1960 eruption was 900 m wide. Leveling along the Pahoa-Kalapana road between 1958 and 1964 indicated subsidence of a sharply defined zone 600 m wide, presumably during the 1960 eruption further to the northeast.

This was probably the effect of a dike that failed to reach the surface, and the subsidence was located to the south of the projection of the 1960 fissure, which led Dietrich and Decker (1975) to propose that the dike dipped to the south.

At present the ground deformation data for a LERZ eruptive event are not adequate for predicting the distribution of faulting, but the zone of faulting is not likely to be more than 1 km wide, and commonly will be much narrower than this. During intrusion events faulting may occur without fissuring, and the fault zone is likely to be on the south side of the ERZ. During fissuring and eruption events faulting may occur a few hundred meters on either side of the fissure. In either case vertical displacements of 1 to 2 meters are to be expected, with a maximum of 4 meters, and fault movement will occur during a period of a few hours to a few days immediately before an eruption.

When magma finally reaches the surface the axial zone of subsidence with its marginal faults becomes stabilized and uplifted. When dikes are not vertical the surface deformation is asymmetrical, with greater uplift over the hanging wall of the dike (Dieterich and Decker, 1975). The asymmetry of the vertical displacement profiles across the ERZ led Dietrich and Decker (1975) to suggest that the dikes dip SSE at 45 degrees, and this dip is similar to that of the zone of earthquake hypocenters under the ERZ (see fig. 4.4). Swanson and others, (1976) prefer a vertical dip for the dikes, but the attitude of the dikes remains unknown.

The factors that determine whether a summit inflation will be followed by magma flow into the rift zones, and whether such a



flow would result in a flank intrusion or eruption, are impossible to evaluate with our present knowledge. Similarly it is not possible to predict where in the rift zone an eruption is likely to occur.

4.2 The Puu Honaula Area

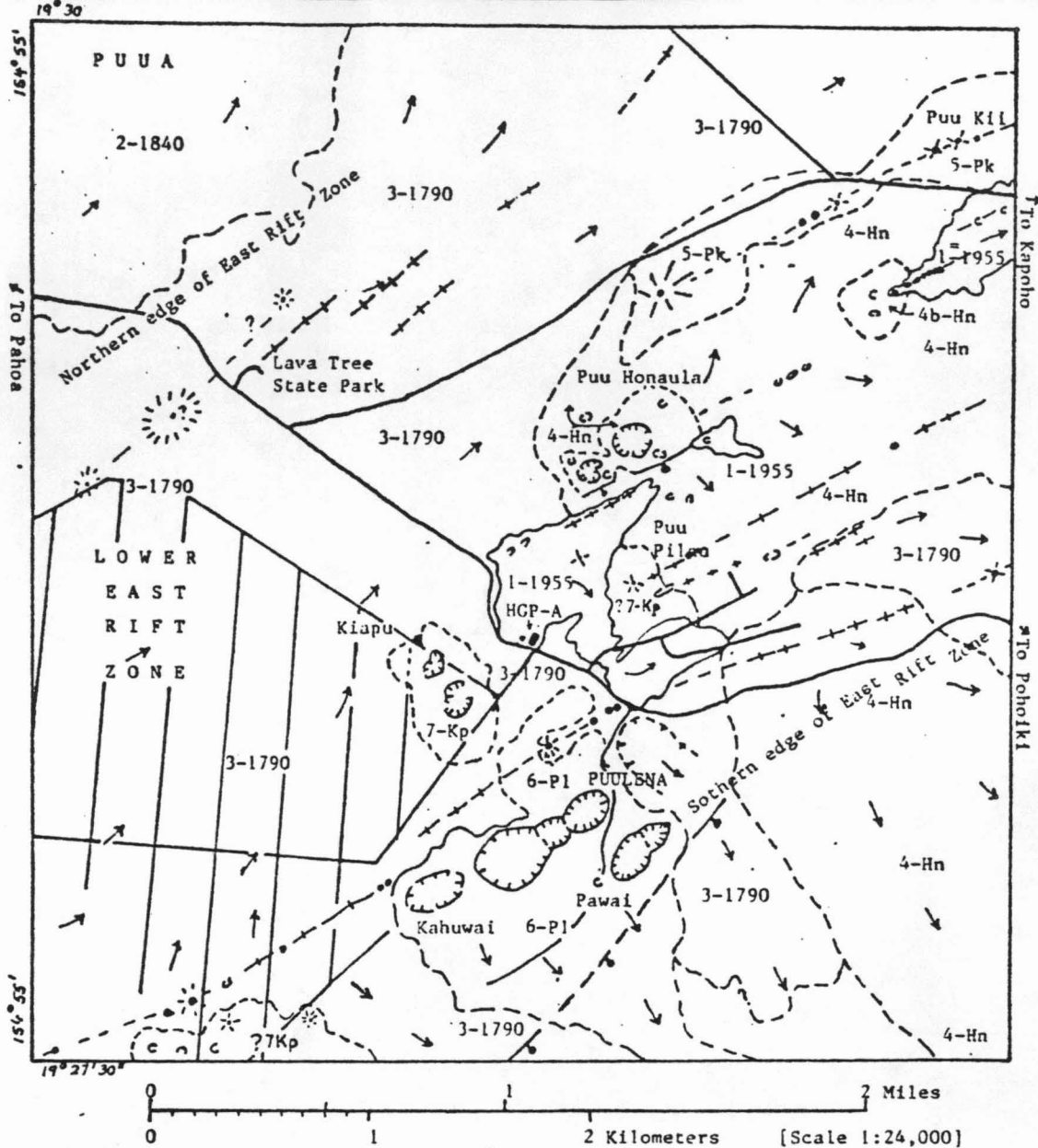
4.2.1 Outline of the Geology and Structure

The following summary, and the accompanying geological map (fig. 4.9) are based on detailed maps by Holcomb (1981), and on the unpublished map of the Kapoho quadrangle by R.J. Moore. We have made slight modifications as a result of our own photo-geological interpretation and a brief visit to the area.

The area lies across the upper part of the Lower East Rift Zone (LERZ), which is a broad shallow ridge between sea level and 800 feet elevation. In the western part of the area the top of the ridge is a shallow trough-like depression bordered by higher ground formed by the Puu Kaliu vent-fissure zone to the south, and by fissure zones of the 1790 and 1840 eruptions to the north. Further east the rift zone has a central low ridge composed of small shields and cones of the Puu Kii and Puu Honaula fissure zones. The southeast slope of the rift zone south of Puulena is unusually steep, and a lava mantled fault scarp is inferred to underlie this slope.

The oldest rocks are the cinder and spatter cones of Kiapu, which underlie a lithic tuff dated at 1,000 years before present (R.J. Moore, pers. comm., 1981). Small cones southwest of Puulena and at Puu Pilau may be of similar age.

The Puulena crater walls expose thin lava flows that are



1-1955	Spatter, cinders, flows of 1955 eruption
2-1840	Flows from Pahoia fissures (to west)
3-1790	Spatter, cinders, flows of 1790 eruption
4-Hn	Cinder cone, small shields of Puu Honaula (500-750 yrs BP)
4b-Hn	Small shield pre-dating Puu Honaula flows (age unknown)
5-Pk	Small lava shields & spatter cones of Puu Kii fissure (?750-1000 yrs BP)
6-P1	Thin flows capped by lithic tuff, of Puulena Craters (1,000 yrs BP)
7-Kp	Cinder/spatter cones of Klapu (>1,500 yrs BP)

- Spatter cones
- ☼ Small lava shields
- ⊖ Cinder cones with craters
- ↘ Lava flow directions
- ↔ Faults, ball on downthrow side

Figure 4.9. Geological map of the Puu Honaula area, East Puna Hawaii (modification of map of Holcomb, 1981, by B. Baker using field studies, photogeology, and pers. comm. with R. Moore).

capped by a lithic tuff dated at 1,000 years before present (YBP) and represent a small shield built on fissures along which deep pit craters developed, probably during a phase of magma withdrawal.

In the northeast, an alignment of small low shields, spatter cones, and cinder cones marks the line of the Puu Kii eruptive fissure. Holcomb (1981) estimated the age of these rocks at 350-500 YBP, whereas R.J. Moore (pers. comm., 1981) reports they are older than the Puu Honaula vents to the south, which he dates at 500-750 YBP.

The most extensive lavas are those of the 1790 eruption, which flooded a large portion of the crest of the ERZ. In the northwest of the area these flows were derived from a fissure system higher up the rift zone, but in the south they were erupted from a fissure zone extending from the southwest corner of the area past the northern flank of Puulena. These flows ponded around Kiapu and almost covered the Puulena shield.

The northwest portion of the area consists of flows from the 1840 fissure, which lies at the northern edge of the middle ERZ, to the west of the area. These flows descended the northeast flank of the rift zone.

The most recent lavas were erupted in 1955 from a discontinuous en echelon fissure south and east of Puu Honaula. They are of limited extent and thickness in the mapped area (fig. 4.9).

The steep southern flank of the Puulena craters is believed to represent a buried normal fault downthrown to the southeast (Holcomb, 1981). A localized normal fault cuts the south side of the Puu Honaula cinder cones. The western end of the southern

fault of the Kapoho graben ends at the eastern boundary of the area, at the junction of the Puu Kii and 1955 flows. The last two faults are downthrown to the southeast less than 2 meters.

4.2.2 Frequency of Eruptions

It is difficult to estimate the average frequency of flows accumulating in a vertical sequence at a given site in the Puu Honaula area because there is no dated horizon in the prehistoric lavas. A crude estimate can be obtained from the measured depth of the interface between submarine and subaerial lavas in the HGP-A well. This horizon was logged at a depth of 1750 feet (533 m) or 1175 feet (358 m) below present sea level. The rate of subsidence measured by tide gauges is about 4.1 mm per year. If this rate is assumed for the area of the HGP-A bore hole, the age of the first subaerial lava would be approximately 87,313 YBP. Assuming an average thickness of 18.3 feet for individual lava flows above this level, an average frequency of one flow per 898 years is obtained for the site of HGP-A well. This estimate may be too low, as some data suggest the rate of subsidence in the LERZ is greater than that of the coast line at Hilo, but this factor cannot be determined from the presently available data. Conversely, if some of the section of HGP-A well is made up of sills injected between lava flows, the frequency of surface flows would be correspondingly less.

Within the Puu Honaula area (fig. 3.9), an area of about 20 square kilometers, there have been at least 6 periods of eruptive activity in the last 1,000 years, with an average recurrence interval of 166 years. Three events have occurred in the last 191 years for a recurrence interval of 64 years. In the entire LERZ,

4 major eruptions have occurred in 191 years, with an average recurrence of 48 years. This is a low level of activity compared to the ERZ as a whole, for which Klein (in press) lists 20 extrusive and 19 intrusive events since 1918, with an average recurrence interval of 3 years for each type of event. We estimate that a conservative recurrence interval of 40 years applies to the Puu Honaula area.

4.3 Volcanic Hazards

4.3.1 Introduction

A survey of the volcanic hazards of the island of Hawaii by the U.S. Geological Survey (Mullineau and Peterson, 1974) concludes that lava flows and volcanic related ground rupture to be the main hazards to property in the East Rift Zone (ERZ). We consider the probabilities for occurrence of these hazards to be the highest for any region on the island (and possibly in the world). Other hazards such as falling rock fragments, volcanic fumes, earthquakes, and tsunamis are much less serious.

4.3.2 Surface Deformation

Surface deformation in the LERZ consists of periodic uplift and horizontal extension, accompanied by fissuring and possibly normal faulting. All the evidence suggests that such deformation takes place before eruptions, or before renewed eruptions during lengthy periods of activity. Relatively slight deformation also occurs during periods of intrusive activity.

The broad arching, uplift, and tilting that accompanies extrusive events is not of sufficient magnitude or rate to constitute a hazard to property. The significant deformation hazards

are fissuring and faulting.

Within the area mapped (fig. 4.9) there are 16 individual fissure systems, and others may lie buried under lava flows. These have formed during a minimum of 6 eruptive episodes during the last 1,000 years in a zone 3 km wide extending from Pawaii Crater to the Lava Tree State Park.

The majority of fissuring events have formed lines of en echelon fissures, and development of parallel fissures is rare. Therefore we adopt a conservative model of formation of a single fissure 1 m wide every 40 years. The area affected by such a fissure would be 5,000 square meters, which is about 0.002 per cent of the area of the LERZ in Figure 4.9. There appears to be no control for the location of new fissures, which randomly form anywhere in the active zone. The risk to property is therefore a function of the frequency of fissuring (1 in 40 years), the average width of a fissure (1m), the width of the zone liable to fissuring (3,000 m), and the dimensions of the engineered structure at risk in a directional normal to the rift zone. The probability of a fissure intersecting a structure during a period of 40 years (the effective life of a plant) is shown in Table 4.2.

The risk of damage is proportional to the dimensions, shape, and orientation of the structure under consideration. For extensive structures, such as steam pipelines, that must cross some part of the rift zone the risk of damage is considerable, unless the structure is specially designed to accommodate large displacements. For smaller structures, such as generating plants, the risk is less, but the cost of damage may be greater.

TABLE 4.2

Dimensions of engineered structures versus probability of damage for a 40 year period in the LERZ.

<u>Horizontal dimension of structure in direction normal to rift zone (ft)</u>	<u>Probability (per cent) of damage in a 40 year period</u>
3,000	100
500	17
100	3
50	2

4.3.3 Hazards from Eruptions of Lava

The risk of an installation being destroyed by lava is the highest of all potential risks in the Puu Honaula area, because for a single eruptive event, the surface area affected is greater than the surface area affected by a fissuring and/or faulting event. Two types of risks from lava flows can be distinguished; (1) those associated with lava from an eruptive vent directly under or adjacent to the site and, (2) those due to lava flows coming from a more distant source.

Eruptive vents that have been active in the recent past are of three types. In the opening stages of an eruption, they are linear fissures that discharge fountains of incandescent spatter and scoria. With time these become more localized and discharge flows of lava. Cinder cones may form where there is prolonged ejection of pyroclastic material. Finally, in those areas where ground water is abundant or where sea water has access to the fissure system, steam blast eruptions may eject lithic debris, including blocks a foot or more in diameter. The effective radius of the effects of explosive discharge from these three types is essentially the same. They are unlikely to have a serious effect beyond a distance of a kilometer.

The fact that no eruptive vents have been found outside the boundaries of the LERZ makes it unlikely that one will occur there in the future, but this possibility cannot be completely discounted. Within the rift zone, most eruptions have been on the south side. It has been suggested the rift zone is moving southeastward (Swanson and others, 1976), but the evidence for this interpretation is not conclusive. There is convincing evi-

dence, however, that new vents rarely coincide with old ones, and by this reasoning, one of the safest siting areas in the rift zone may be on an old cinder cone.

From these relations we conclude that the danger from a new eruptive vent is lowest outside the northern or southern boundaries of the rift zone. Within the rift zone, there is a marginally lower risk at a site situated on an older vent, especially within the northern half of the rift zone. These risks must be weighed against the practical disadvantages of increasing the distances steam must be transmitted.

The risk of a site being overrun by lava from a vent outside its immediate vicinity is largely a function of topography. Low areas into which lava is likely to be channeled have the highest risk, and elevated ground or areas in the lee of hills standing between the site and possible sources would have a much lower risk. Ground with a high slope angle will be covered by thinner flows than flat ground or depressions into which lava could be ponded, but flow velocities on these slopes here would be higher.

Figure 4.10 assesses the level of risk in the study area from lava flows as highest, intermediate, and lowest, using the principles of risk assessment outlined in this section. These are intended as general guidelines, and should be examined on a site-specific basis following the final selection of a site for installation of permanent structures.

Average thickness and rate of advance of lava flows may also be crudely calculated. Neglecting the eruption below sea level in 1884 and another event of a similar nature in 1924, five eruptions have occurred at elevations below 1,000 feet. Lava flows

MAP OF VOLCANIC RISK LEVELS - PUU HONAUOLA AREA, E. PUNA, HAWAII

(Scale 1:24,000)

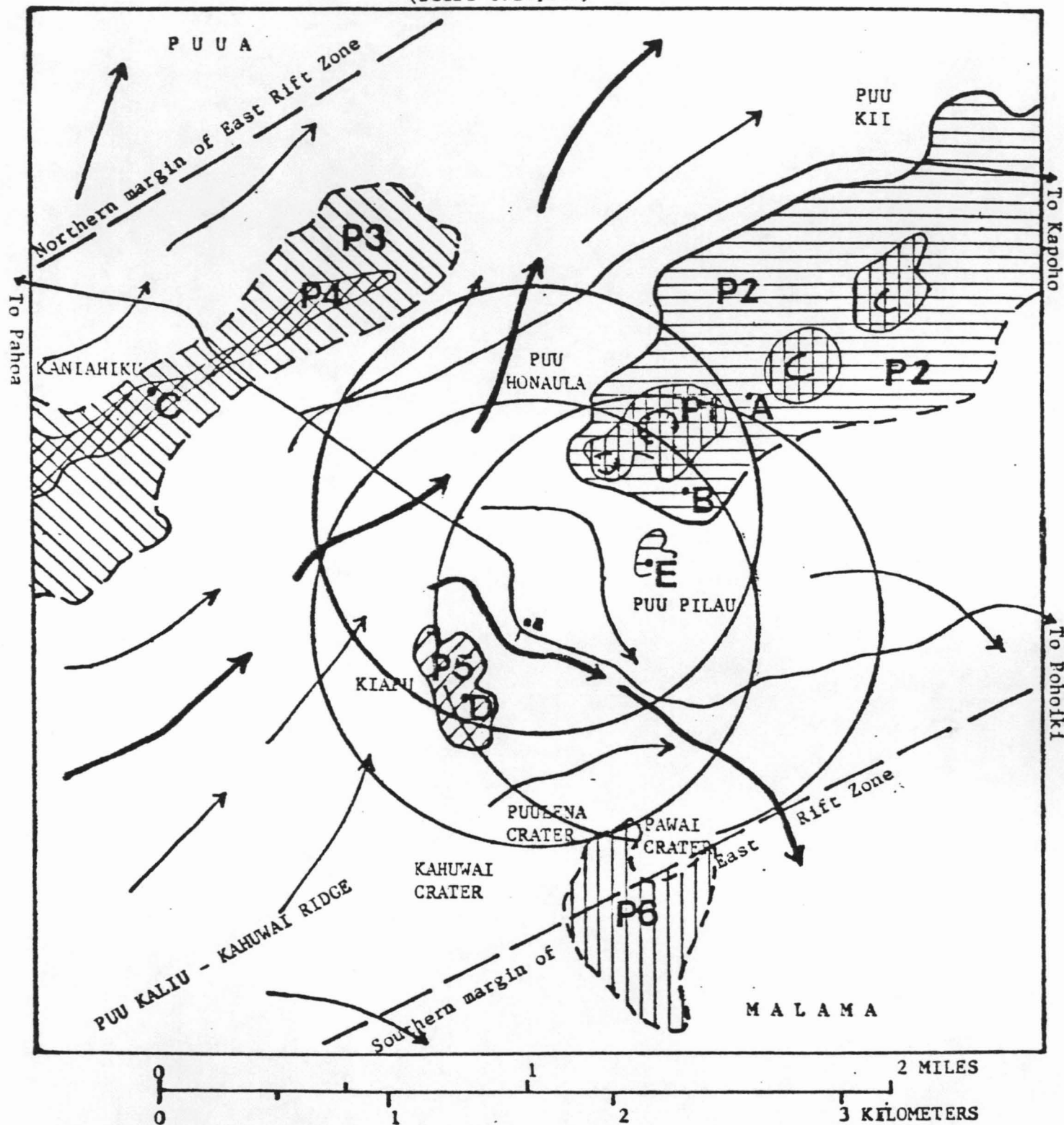


Figure 4.10. Map showing relative risk of lava flow incursions. Arrows show likely directions of flow of lavas in future eruptions. The most likely paths of flow are shown with thick arrows. P1 marks areas with least risk of lava incursion and P6 marks areas of intermediate risk. Unshaded areas are those of greatest risk.

from eruptions, such as that of 1977, which occurred at higher elevations would not affect a site in the Pahoia district.

An average thickness of 18.3 feet (5.6 m) can be calculated from the total volumes and areas of the five historic flows. This average is strongly affected by the exceptional thickness of the lava of 1960, which averaged 36.7 feet (11.2 m) because it accumulated in a depression on a very gentle slope. Flows on steeper slopes average about 12 feet (3.6 m) in thickness. Thickness also varies from place to place according to the local topography and rate of discharge. It is greatest where ponding occurs or narrow constrictions limit the flow and cause the lava to form thicker flows in an upstream direction.

It must also be stressed that the thicknesses of lavas are greater during active flow than they are after forward motion is arrested. This is especially apparent in fluid pahoehoe flows on moderate to steep slopes. At a given point in the lava stream, the thickness normally diminishes as the flow spreads downslope and drains lava from higher elevations. This effect is dramatically illustrated at Lava Forest Park, where tree molds stand two or three meters above the final surface. Therefore, it should be anticipated that, for pahoehoe flows, transient thicknesses may be as much as twice the observed final thicknesses of about 12 feet (3.6 m). The exact magnitude of this difference will depend on the viscosity, rate of discharge, gradient and course of the flow, and the local topographic variations. Because of these factors, thickness of a flow cannot be predicted, but thicknesses of 30 feet or more can be attained at certain points during the course of an eruption.

Rates of advance of flow fronts are governed by the slope angle, viscosity of the lava, and rate of discharge at the vent. During historic eruptions, measured rates have ranged from as much as a few hundred feet per hour to as little as a few feet per day. In the East Puna District, rates of advance are much slower than on higher segments of the rift where slope angles are greater. During a prolonged eruption, it is common for the flow front to advance in one area for a day or two, and then shift to another front before returning to the earlier front, so that with time, advance may be highly sporadic for any particular portion of the front.

4.3.4 Alleviating Volcanic Hazards

4.3.4.1 Monitoring: Volcanic eruptions in the LERZ have an abundance of premonitory phenomena that make it possible to foresee a coming eruption for several days or weeks. This allows adequate warning time to evacuate personnel and portable equipment. For this reason, hazards to persons working in the area, and hazards to portable equipment, are not as serious as hazards to fixed facilities.

The methods currently in use to monitor the LERZ and to forecast eruptions and their accompanying deformation employ seismographic records, tiltmeter readings, resurvey of trilateration networks, and geodimeter measurements. These methods are applied by the staff of the Hawaiian Volcano Observatory (HVO) operated by the U.S. Geological Survey. Members of the staff of the Hawaiian Institute of Geophysics have established a geodimeter network around the existing geothermal well (HGP-A) to monitor ground deformation resulting from extraction of geothermal

fluids. The seismographs provide continuous records, whereas the tiltmeters and geodetic techniques provide data at infrequent intervals. Currently the HVO staff re-levels the trilateration stations twice a year and measure tilt two or three times a year. Geodimeter measurements have not been made since 1978.

Seismological techniques are the most effective methods of forecasting impending events in the ERZ, and the HVO network appears adequate for monitoring seismic activity. In the event that large-scale geothermal development takes place in East Puna, consultation with the staff of HVO should be accomplished to determine whether additional seismographs would be needed to improve the capacity to monitor shallow, very low magnitude activity. There is probably no advantage to be gained from installation of additional tiltmeters, but it is desirable to maintain the present HIG geodimeter network, to allow ground deformation in the area of any future geothermal plant to be monitored, especially during nearby extrusive or intrusive events. This would serve to locate zones of potential fissuring and faulting during any activity that may occur in the future. Such data are important for design considerations before construction of permanent installations in the area of the geothermal development.

Apart from these preliminary data bearing on the design and siting criteria of new facilities, the basic objectives of monitoring seismic activity and ground deformation should be to provide warnings of possible eruptions or ground rupture to allow time for precautionary measures. Frequent remeasurement of a geodimeter network, particularly before and after swarms of earthquakes in the LERZ, would provide more detailed information on

the location of tectonically active zones that are likely to be affected by an eruptive event.

4.3.4.2 Site Selection: By judicious site selection and design, it is also possible to greatly reduce the probability of inordinate losses to permanent facilities by taking advantage of topographic relief. For future development in the Puu Honaula area the question of selection of one or more sites for generating plants will become increasingly important. Figure 4.10 shows areas within a radius of one kilometer of the HPG-A well and proposed drilling sites to the north and east which are prime targets for future plant site locations.

Current knowledge of eruptive processes provides no basis for long term predictions of the locations where future eruptions are likely within the ERZ, but as historic eruptions have been more common on the south side, an outbreak in that part of the zone is more probable.

Topography is the controlling factor determining the risk of lava incursion on a selected site. The area at greatest risk within 1 km at HGP-A well or proposed wells is the shallow depression bounded by the Kaniahiku ridge to the north, and the Puu Kaliu - Kahuwai Kiapu - Puu Honaula - Puu Kii line to the south (fig. 4.11). Lavas originating within this area and in the ERZ up to 4 km west of the area are likely to be channeled down into this depression as indicated by the heavy arrows in fig. 4.11. Ponding of lavas on the nearly level ground immediately northwest and southwest of Kiapu could result in overflow between Kiapu and the HGP-A site. This would result in the flow of lava down the

southeast flank of the rift (heavy arrows in fig. 4.11). Lavas originating in the northern part of the area would flow to the northeast, and those erupted south of the Puu Honaula ridge would flow to the southeast.

Areas of reduced risk from lava flows are primarily hills and, secondarily ridges, that rise at least 40 feet above the pathways of flows and are not within areas subject to ponding. Such areas are shown on fig. 4.11 and are graded from P1 (having the lowest risk) to P6 (intermediate risk). Unshaded areas have the highest risk.

The southeast flank of Puulena Crater (P6) is protected by the north rim of Kuhawai Crater, and by the Puulena Crater itself, which, if it were filled by lava, would overflow its eastern end. This site is located close to a buried fault (fig. 4.9) and is too distant from the geothermal area. This site has the advantage of being close to the edge of the southern (but most active) side of the LERZ.

Kiapu Hill (P5) rises 60 feet above the surrounding plain but lies in the path of any lava erupted in the southern third of the rift zone. The NE-trending Kaniahiku ridge (P4) rises 20 to 60 feet above the surrounding area, and, according to Holcomb (1981), is formed by 17th century lavas cut by normal faults. No evidence of faulting was found in a photogeological interpretation of this area. The ridge provides well protected sites close to a paved highway, but may not be feasible because of distance from the HGP.

We have selected five sites strictly on the basis of risk from lava flows, with little regard for distance from the geo-

thermal area. The safest of these (A in fig. 4.10) is in the saddle between Puu Honaula and the next cone to the northeast, at an elevation of 660 feet. The site is 90 feet above the low ground to the north.

The second site (B) is 350 m south-southeast of the summit of Puu Honaula at an elevation of 650 feet, 45 feet above the low ground 800 m to the west. The site is on a shallow ridge 850 m from HGP-A.

The third site (C) is on the Kaniahiku ridge 310 m southwest of the Pahoia highway at an elevation of 700 feet. This site is 60 feet above the low ground on each side of the ridge. The ridge is shown as a zone of short normal faults by Holcomb (1981), but photogeologic methods do not confirm the existence of these faults. Should this site be seriously considered, the question of the existence of these faults should be investigated by trenching. The site is 2000 m from HGP-A.

A fourth site (D) is on Kiapu, an old spatter and cinder cone, at an elevation of 700 feet, 50 feet above the western base of the hill. A disadvantage of this site is that it lies in the path of flows that could descend from a considerable area higher in the ERZ, but it is unlikely that these flows would be thicker than 50 feet. Site D is 530 m southwest of HGP-A.

The last site (E) is on a low, horseshoe shaped ridge of old spatter immediately northwest of Puu Pilau, at an elevation of 630 feet. It is somewhat restricted in size (200 by 50 m) and is only about 30 feet above the level of ground to the west. The northwest side of the low cone on which the site is situated is partly protected by a ridge of boulders dozed from cultivated

fields. The ridge served as a diversion barrier during the 1955 eruption and could be enlarged in height and width to provide added protection. Site E is 550 m from HGP-A.

While site A is undoubtedly the safest of the ones we have listed, based on the listed criteria, there is little to choose between sites B and C, which are slightly less secure, and between sites D and E, which we consider more exposed.

4.3.4.3 Diversion Barriers: Efforts to influence the directions and rates of advance of lava flows have, for the most part, been unsuccessful in Hawaii, but elsewhere, particularly at Mt. Etna in Sicily, they have been more effective. During the 1960 eruption near Kapoho, large-scale efforts were made to construct barriers along the south side of the graben, and although in some instances they delayed the advance for a few hours or at most a day or two, all were eventually overrun.

Barriers fail either by being bodily pushed ahead of the flow or by penetration of their base by fluid injections. The high density and mass of thick basaltic flows, even when moving slowly, exerts such a large force against any obstacle in its path that it can simply force it ahead or aside. The bulk density of basaltic lava (about 2.7 grams per cubic centimeter) is considerably greater than that of the fragmented, scoriaceous rock and cinders used in hastily constructed barriers. To be effective, barriers of loose material would have to be wide and much higher than the anticipated level of encroaching lava flows.

If a flow can be diverted into an open channel, especially one having a smooth floor and steep gradient, the barrier does not receive the full force of the flow and may survive. This

principle accounts for the success of barriers at Mt. Etna. Owing to the steeper and more irregular topography on that volcano, it is easier to divert flows from one channel to another. In addition, the lavas of Etna, being more viscous, are less likely to penetrate the base of the barrier.

A well anchored barrier constructed of dense material, such as concrete, may be capable of protecting a narrow front at a given locality if the force of the flow can be diverted into a channel of lower resistance. In general, pahoehoe flows have a lower viscosity and can flow around obstacles, such as trees or small cones, more readily than aa lavas, but when ponded they also have a greater capacity for flowing beneath a light structure resting on the surface. The important principle governing the success of barriers is to deflect the flow into a more favorable course rather than attempting to oppose it directly.

4.3.4.4. Design Considerations: Of the various structures associated with a geothermal project - steam wells, pipelines, power plant, and associated facilities - wells and pipelines must be sited in accordance with relatively inflexible geological requirements, whereas more freedom is possible in placing the remaining facilities. It has been shown that the risk of lava flows is mainly a function of topography, and the risk of surface displacement is mainly a function of the dimensions and orientation of a structure across the trend of the ERZ.

The safety of pipelines, power lines, and large buildings can be enhanced by observing certain general guidelines.

1. Long linear structures within the ERZ may be subjected to horizontal ground displacements of at least 2 meters in a

direction N 30 W (normal to the rift axis) and up to 4 meters in a vertical direction. Pipelines, powerlines, and their supports can be constructed with sufficient vertical and horizontal compliance to withstand this magnitude of ground deformation.

2. Under favorable conditions diversion barriers may be capable of diverting lavas but are of little use as dams to oppose a flow directly. Short barriers on the north side of site B, the southwest side of site C, the west side of site D, and the northwest and northeast sides of site E would enhance the security of these sites.

3. To minimize the probability of failure by surface deformation, fixed facilities entailing relatively high costs, such as generating and auxiliary plants, should have a minimum dimension transverse to the trend of the LERZ (N 60 E). These facilities should, where possible, be built to withstand ground deformation of the magnitude indicated above (see 1).

4. It would be desirable to design roofs of buildings capable of shedding scoriaceous pyroclastic debris or supporting the load of a 1-meter layer of ash or cinders having a bulk density of 2 grams per cubic centimeter.

5.0 SEISMIC RISK ASSESSMENT OF THE PUNA DISTRICT, HAWAII

5.1 Introduction

5.1.1 Purpose of Study

This part of our study evaluates the earthquake hazard and general risk to future facilities for the Puna Geothermal Prospect (PGP) in the Puna District of Hawaii. Section 5.0 only considers ruptures of tectonic origin. Volcanic related fissures and faults are considered in Section 4.0.

5.1.2 Approach

Current state-of-the-art methods call for the detection, delineation, and definition of the character of seismogenic faults of a region to prepare an assessment of the location and faulting potential of active tectonic faults, and to evaluate the potential strong ground motion that could affect engineering structures at the site (Slemmons, 1977; and Glass and Slemmons, 1978). The usual methods of assessment include consideration of:

- A. Seismicity and source mechanisms of regional earthquakes.
- B. Geomorphic expression for fault rate of activity and fault slip type.
- C. Geologic assessment of stratigraphic and soil-stratigraphic evidence for fault activity.
- D. Assignment of maximum or maximum credible, and maximum probable earthquakes for the province and each seismogenic fault effecting the study area, with an estimation of future earthquake frequency and expected attenuated ground motion at the engineering site.

Review of aerial photographs, consideration of the youthful

and active historic and geologic record and the nature of the historic earthquake activity, support the classification of faults and fissures into two, very different, categories:

1. Volcanic faults, fissures, and rifts, including the fractures of the East Rift Zone and the Southwest Rift Zone, along nearly straight volcanic alignments.
2. Tectonic faults of the Hilina and Kealaekua-Kaholo fault type, with dipping fault planes and common arcuate traces.

These two types provide the source of most shallow-focus earthquakes, the former associated with magmatic movements, as discussed in Sections 3 and 4 of this report, and the latter with higher magnitude tectonic earthquakes.

5.1.3. Terminology

The following terms are defined for use in this report:

The maximum or maximum credible earthquake is defined as the severest earthquake that is believed to be possible at the site, or to be generated by a fault, as determined by geological and/or seismological evidence. The maximum earthquake for a site has a ground motion that is based on one or more assumed future earthquake sources or source areas, with the motion attenuated to the site as a function of the distance from the source to the site.

The maximum probable earthquake is the strongest earthquake that is likely to provide motion at a given site or area, for a specified period of time, generally assumed to be the life expectancy of an engineered structure. This is approximately 40 years for the purpose of this study.

5.2 Regional Seismicity

The regional seismicity of the island of Hawaii is high compared with many tectonically active regions of the world, and appears to be related mainly, or solely, to volcanic activity and processes. The seismic activity is generally very low along the old Emperor segment north of the island chain and along the northern, old part of the Hawaiian chain (fig. 3.1). Most of the activity is concentrated at the southern, currently active, end of this zone of "hot spot" volcanoes. No known major fault zones affect the chain in terms of major active tectonic plate boundaries.

The record of seismicity, particularly for low magnitude earthquakes is not well documented for the entire historic record and there is no unified catalog of earthquakes available. The main sources of information for earthquake hypocenters are:

1. The NOAA earthquake hypocenter data file (app. A),
2. The Gutenberg and Richter (1954) catalog of pre-1951 data for moderate to high magnitude earthquakes, and
3. The HVO summary reports of regional seismicity.

These data bases all have significant deficiencies in quality and sensitivity of earthquake detection and location that change with time. The post-1960 NOAA file has many duplicate listings for the 100 mile (160 km) radius of HGP (see app. A). The epicentral map prepared from the data of Appendix A (fig. 5.1 and pls. 1 and 2) show a broad pattern of earthquake epicenters for earthquakes of more than about 25 km hypocentral depth, with a denser cluster near the deep central conduits of Kilauea and Mauna Loa; the

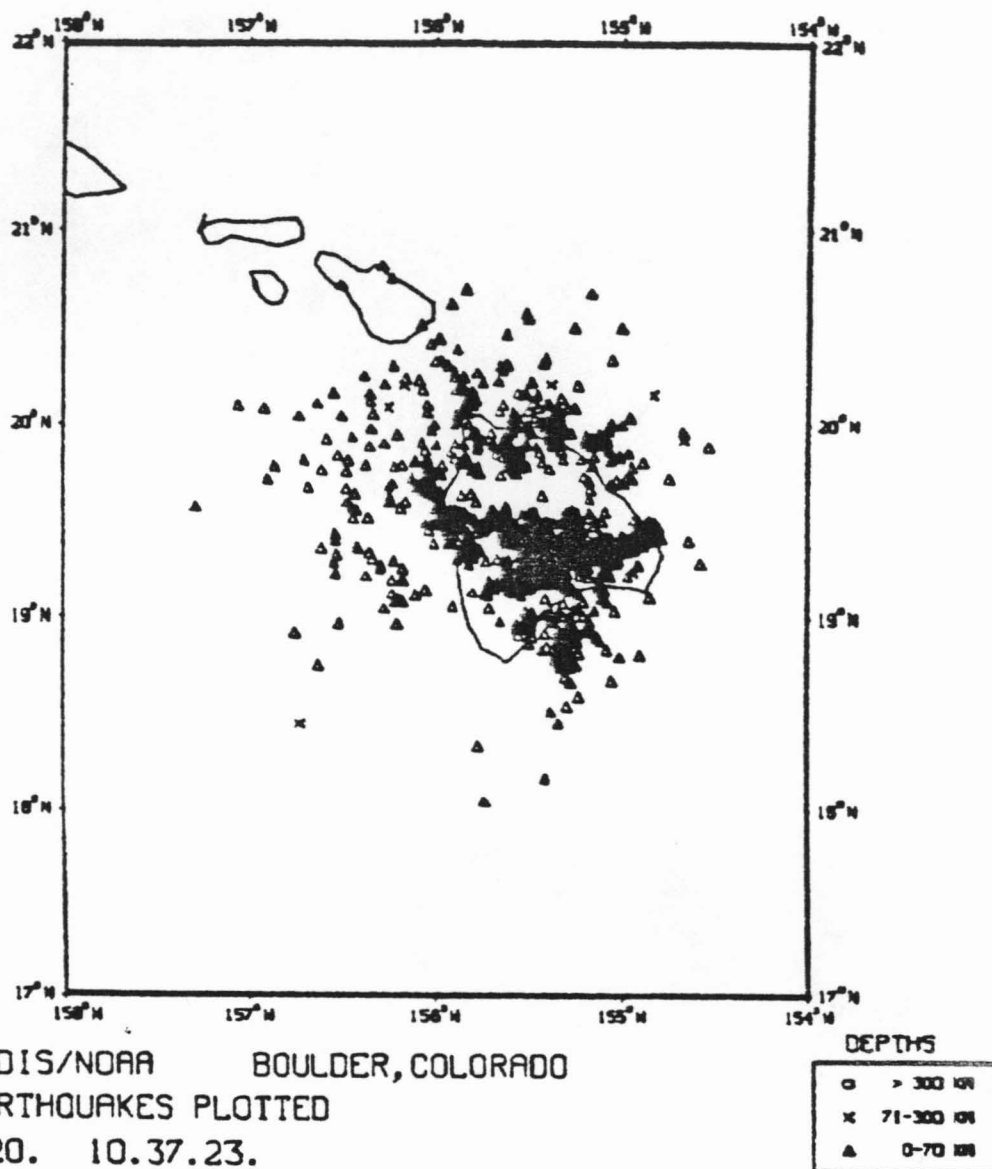


Figure 5.1 Earthquakes of greater than magnitude 3 within a 100 mile (160 km) radius of the Puna Geothermal Project. Many of these events are plotted twice because of duplication in the NOAA file - see Explanation for Appendicies A, B, and C.

epicentral pattern for earthquakes of less than 25 km focal depth show concentrated activity along and near the ERZ, SRZ, the rift zones of Mauna Loa, and along the Hilina fault zone and its offshore southeastern extension.

Two patterns are apparent on the epicentral map of deeper focus earthquakes (pl. 1):

1. A clustering along the deep conduits of Mauna Loa and Kilauea, where pulses of new magma from the upper mantle are accompanied by earthquake activity, and
2. A broad pattern around the edges of the island of Hawaii, where crustal loading from the recent loading by rapid volcanic growth is believed to cause upper mantle tectonic adjustments, although mechanisms of these deep earthquakes is not well understood (Unger and Ward, 1979).

The maximum magnitude for earthquakes of more than about 25 km depth is about 7 for the west flank of the volcano (August 21, 1951) and 6.2 for the east flank of the volcano (April 26, 1973). These deeper focus earthquakes have caused less damage than shallower focus earthquakes of similar magnitude (Nielsen and others, 1977). The likelihood of future activity of this type near the site is considered by us to be low, with only two earthquakes of above 6 magnitude within the 31,400 sq mi area centered on the site for a 30 year period. Adjustments of this type should be more common to the north of the site, since the volcanic heights of Mauna Loa and Mauna Kea are greater and the volume of eruptive material is greater than in the Kilauea-East Rift Zone sector of the island.

Earthquakes of less than about 25 km focal depth are localized along the central conduits, but also have narrow and concentrated clustering along the active volcanic rifts. In addition a broad zone of distributed, very shallow focus earthquakes are described for zones of magmatic movement as has been summarized by Koyanagi and other (1981). The relationship of the ERZ to the Hilina fault zone is described in Section 2.0 and Section 5.3.

5.3 Seismicity of Faults near the Puna Geothermal Prospect

5.3.1 Hilina Fault Zone

The historic record shows a high rate of activity along the Hilina fault zone, with a large earthquake, perhaps of 7.5 to 8 magnitude in 1868 and a $M_s = 7.2$ earthquake in 1975. This zone shows a long history of small earthquakes as suggested by the earthquake catalog (app. A, B and C and pls. 1 and 2), and the activity shown in pre-1975 epicentral plots. The activity from 1963 to 1969 is shown in Figure 5.2 with volcanic related epicenters along the ERZ and epicenters on and near the Hilina fault zone. The epicenter map of all earthquakes for 1976 and 1977 (fig. 5.3) shows the earthquake activity in Hawaii, including the epicentral and aftershock area for the 1975 Kalapana earthquake, with a dense distribution of earthquakes to the south of the ERZ and the offshore zone of submarine uplift and tsunami generation (fig. 3.11). The focal mechanisms of earthquakes of this zone are compatible with a southeastward movement (figs. 3.11 and 3.12) of a block bounded on the northwest by the surface trace of the Hilina fault and extending into the offshore region (Fitch and Kinoshita, 1969; Furumoto and Kovach, 1979; Crosson and Endo,

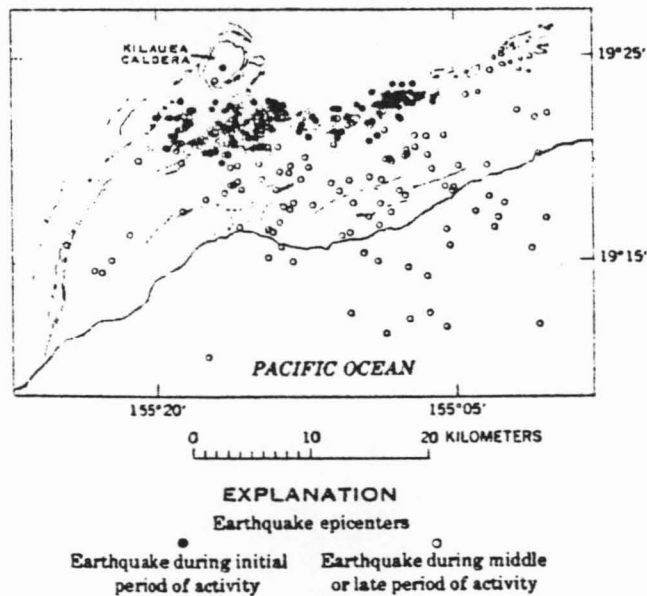


Figure 5.2. Compilation of earthquake epicenters from short seismic swarms that are associated with magmatic processes from 1963 to 1969. Earthquakes selected are of magnitude 2.0 and greater, and depths less than 15 km. The epicenters were plotted according to two time categories in which they occurred. Earthquakes during the initial stages of activity were concentrated near the outbreak area along the Koaie faults and the ERZ. Earthquakes during the middle and late stages scattered far to the south toward the Hilina fault zone (Koyanagi and others, 1972). Note the close spatial association of the earthquakes associated with the eruption (solid dots) with the ERZ.

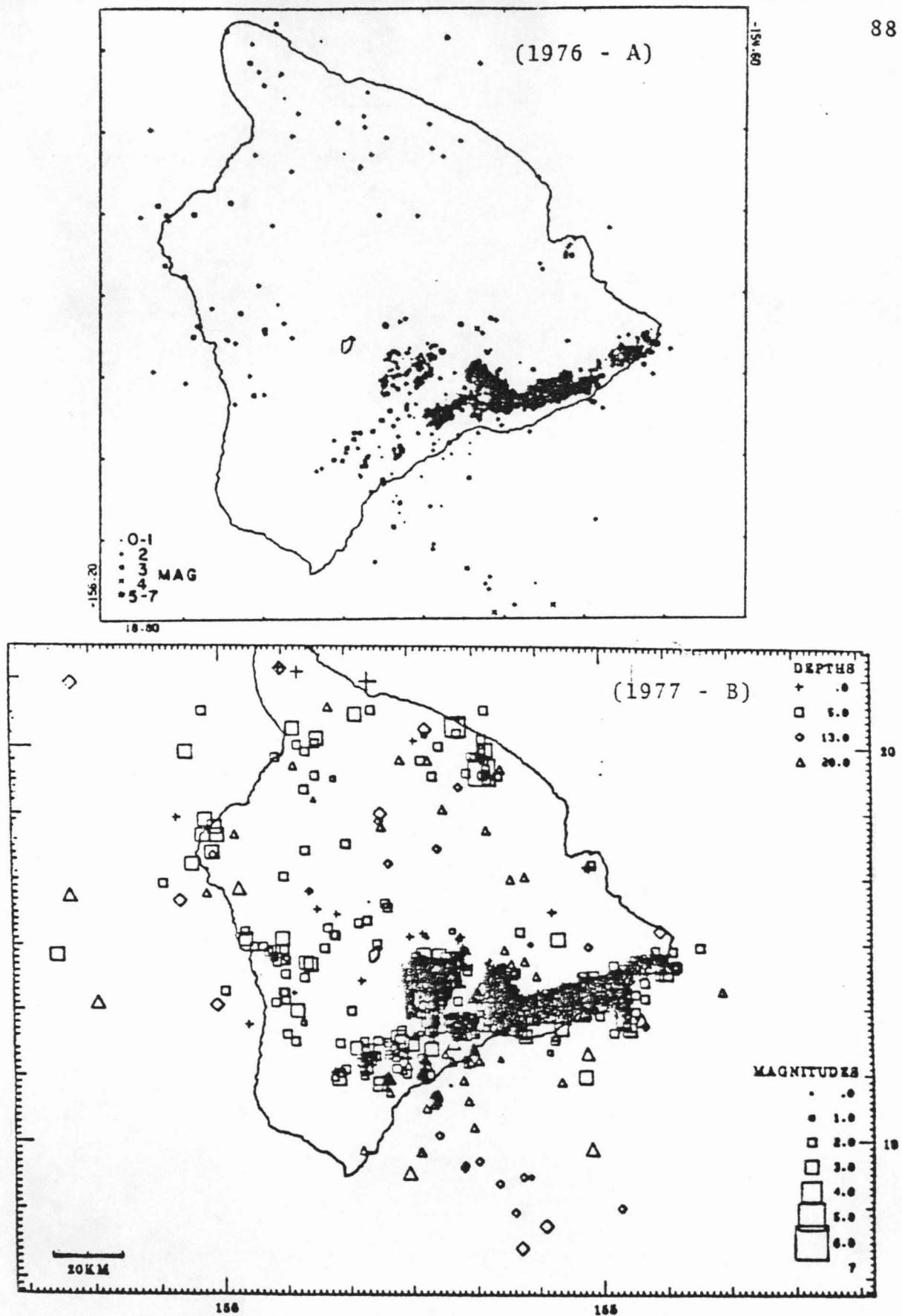


Figure 5.3. Epicenter plots presented in Hawaiian Volcano Observatory Summaries 76 and 77 for 1976 (A) and 1977 (B) showing the concentration of earthquakes in the south flank of Kilauea (from Koyanagi and others, 1981).

1981); Crosson and Endo (1981) show (fig. 3.12) vectors for displacements in this block. Wyss and others (1981) show that precursors to the Kalapana earthquake may have included aseismic stress drop by fault creep in the area indicated in fig. 5.4. Wyss (in press) also indicates that this event may represent three earthquakes of $m_b = 6.5$ in close temporary association, to give the higher M_s value of 7.2.

The average seismic moment for the Kalapana earthquake ($M_s = 7.2$) was 1.2×10^{27} dyn cm, with an inferred stress drop of 12 bars (Furumoto and Kovach, 1979). These calculations, the geologic and tsunami relations for this earthquake, and the after-shock data suggest rupture of a large percentage of the total fault surface. The size of the faulted surface for the 1868 earthquake is unknown, but it does not appear likely that it could have been much greater than for the 1975 earthquake. The possibly larger magnitude (M_s greater than about 7.5) may be from a larger average displacement on a similar fault surface area, or more multiple events in a very short time period.

5.3.2 Koae Fault Zone

The Koae fault zone has frequent earthquake activity and appears to be related to combined tectonic and volcanic activity. The maximum volcanic earthquake is about 5.5 magnitude, which is approximately the maximum noted for volcanic related activity on any of the rift zones. Earthquake epicenters from this fault zone are more than 45 km from the site. When ground motion is attenuated, they are not likely to result in damaging motion at the HGP site.

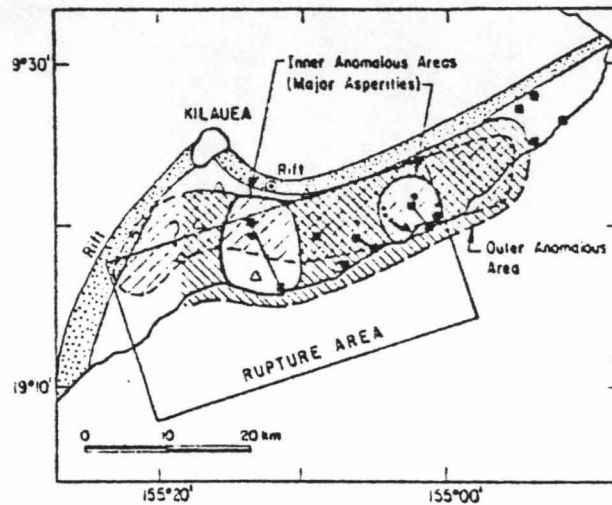


Figure 5.4. Map of the rupture area of the Kalapana earthquake of 1975 in relation to the distribution of crustal anomalies. The one month aftershock zone is shown. The rupture area was estimated by Ando (1979) and is indicated by the rectangle. Squares indicate triangulation benchmarks, small dots show foreshock locations, the medium size dot marks the location of the $M = 5.0$ foreshock and the large dot indicates the epicenter of the magnitude 7.2 main shock (Wyss and others, 1981).

5.3.3 Honuapo-Kaoiki Fault Zone.

This zone has no known evidence for youthful or current activity. It may represent an older, ancestral Hilina fault zone type of feature. The zone is near some epicenters (pl. 1), but its current activity is uncertain. The 35 km distance of this fault zone from the PGP eliminates the need to consider it as an important source of damaging ground motion at PGP.

5.3.4 Kealakekua-Kaholo Fault Zone

This zone is near the source of the 1950 earthquake of $M_s = 6.25$. The zone is a system of arcuate to linear patterns of fractures similar to the Hilina fault zone. Earthquakes of more than $M_s = 6.25$ are possible, perhaps with a maximum of about 7.0. If the poorly known character of this structure is assumed to be similar to the Hilina fault zone, the 110 km distance from PGP eliminates the need to consider this fault zone as an important source of damaging ground motion at PGP.

5.4 East Rift Zone

The general geological and geophysical setting of the ERZ is discussed in Sections 3 and 4. The recent high quality data on seismicity and focal depths show frequent, low magnitude earthquakes of volcanic origin for this zone (figs. 3.10 and 5.3). Koyanagi (pers. comm., 1981) believes that the lack of deeper foci events on the ERZ is due to doming effects from intrusions on the ERZ which cause the high number of events and shallow area of activity. These data show a high level of volcanic activity related to uplift from magmatic injection, with modification from aftershocks of the 1975 earthquake. The depth profile of these

aftershocks is suggestive of a possible southwest dip of a fault plane or rift zone (fig. 4.4).

The maximum magnitude for volcanic-related activity on the ERZ is about 5, based on the maximum historic earthquake. The historic record suggests that earthquakes of about $M_s = 5$ to 5.5 could occur at PGP. Planning for seismic design at this site should, for conservatism, assume that earthquakes of up to this magnitude range could occur during a 40 year time interval. This upper bound magnitude value may be limited by the high frequency of volcanic activity along the ERZ limiting the amount of stress and strain accumulation on this zone, and the frequent relief of such accumulations.

5.5 Earthquake Magnitude and Ground Motion

5.5.1 East Rift Zone

The strongest historic earthquakes on the ERZ are of volcanic origin, and for the NOAA hypocenter data file (app. A) of the last 20 years, indicate a maximum earthquake of about $M_s = 5$. The high frequency of volcanic activity suggests that relief of stress and strain on faults and dikes may occur every few years. Since the magnitude 5 earthquakes that have been recently observed may not represent the long-term maximum, we recommend that a higher maximum earthquake magnitude of 5.5 be assumed for the PGP, with an epicentral distance of from 0 to 10 km. High acceleration, displacement and velocity may occur at the site, but with only a few high frequency cycles of short duration. Motion of this type is not likely to cause structural damage to engineered structures. The following are the estimated ground motion

parameters, defined by data on figs. 5.4 to 5.7.

- A. Mean Peak Horizontal Acceleration: The mean peak horizontal acceleration is 0.2 to 1 g (fig. 5.5).
- B. Mean Peak Horizontal Velocity: The mean peak horizontal velocity is 10 to 100 cm/sec (fig. 5.6).
- C. Mean Peak Horizontal Displacement: The mean peak horizontal displacement is 5 to 15 cm (fig. 5.7).
- D. Duration: The duration of ground motion greater than 0.05 g is 5 to 12 seconds (fig. 5.8).

5.5.2 Hilina Fault Zone

The relief of stress and strain by the 1972 earthquake, which ruptured most of the known length of the Hilina fault zone, is likely to mark the start of a new seismic cycle of accumulating stress and strain. Residual strain on possible unruptured parts of this fault zone, or aftershocks appear to have a potential for generating earthquakes of about $M_s = 6.5$. The gradual increase in strain could lead to another 7.2 magnitude earthquake in approximately 100 years. We estimate the earthquake potential to gradually increase during the next 100 years from $M_s = 6.5$ to $M_s = 7.2$ and assume for planning purposes that the maximum credible earthquake for the next 40 year period is about $M_s = 6.75$ for the PGP area.

The distance from PGP to the epicenter of a potential earthquake on the Hilina fault zone is difficult to determine from the present geologic and seismologic data base. Future specific design of vital engineered structures may need a special assessment of this problem. Alternative methods of measuring the length include the following:

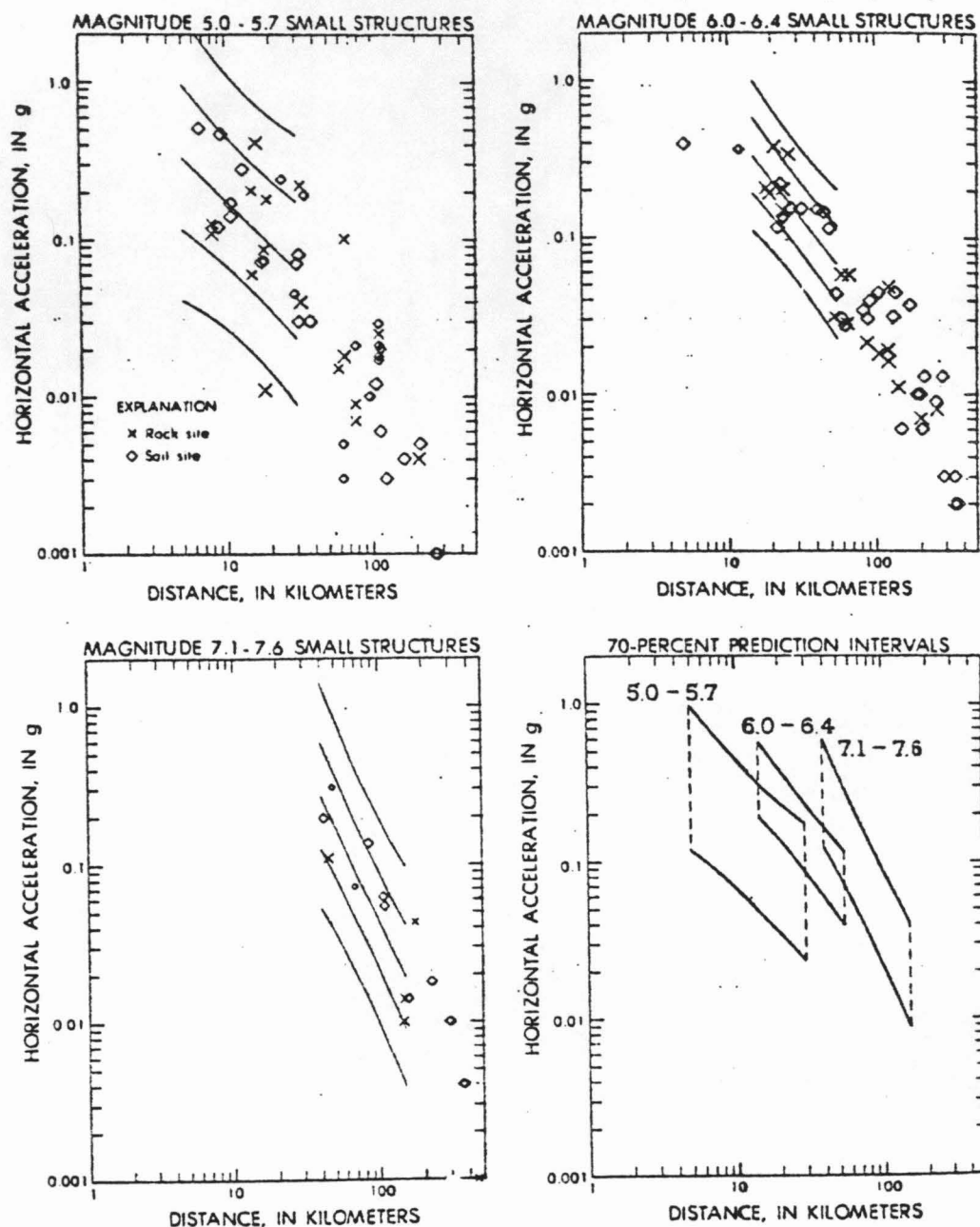


Figure 5.5. Peak horizontal acceleration recorded at base of small structures versus distance to the slipped fault for three magnitude ranges. Center line, mean regression line. Outer pair of lines represent 95 percent prediction interval; inner pair, 70 percent prediction interval. Length of lines represent distance interval considered in regression analysis. Uncertainty in distance is inversely related to symbol size. The lower right figure shows a comparison of the 70 percent prediction intervals for the three magnitude ranges (from Boore and others, 1981).

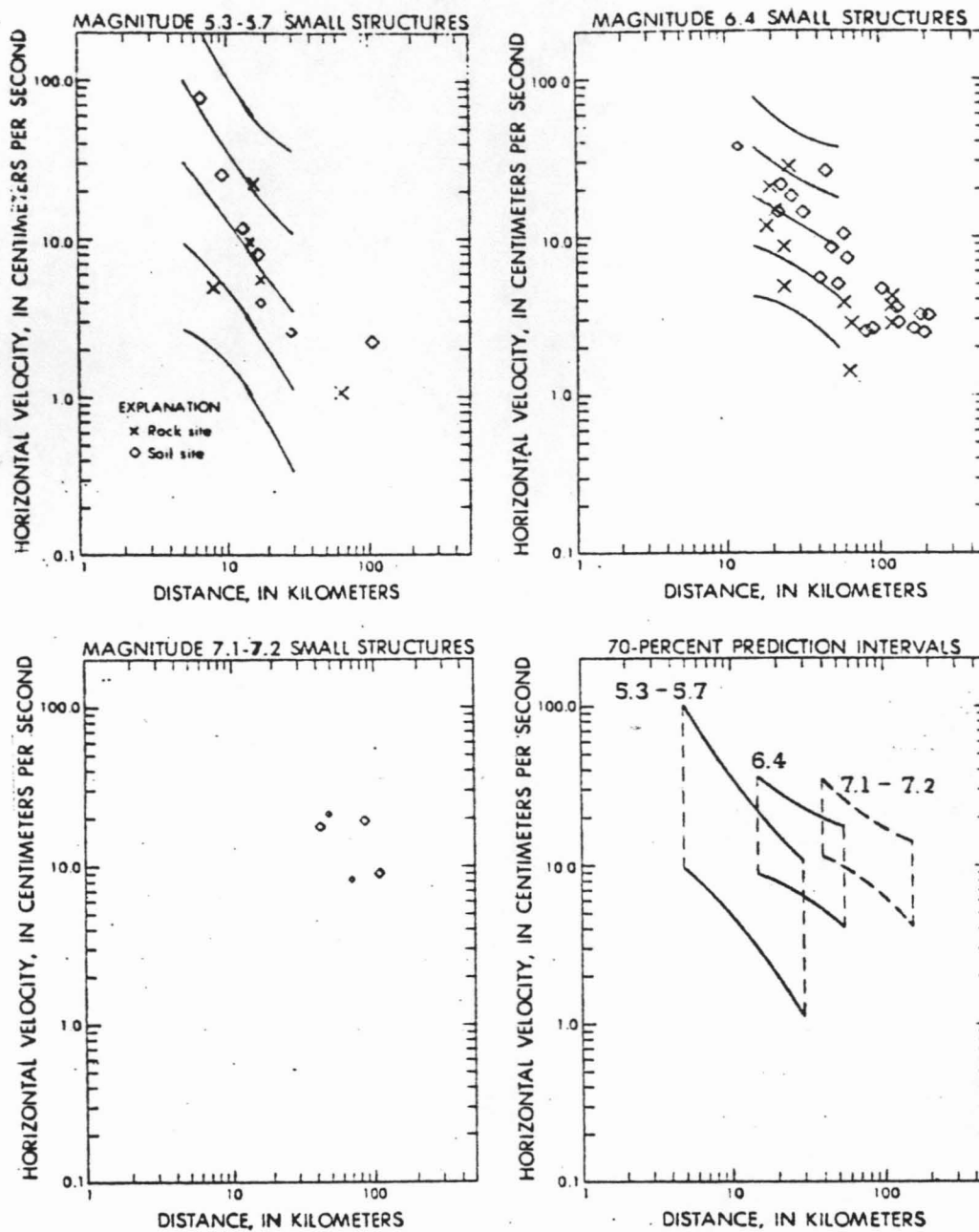


Figure 5.6. Peak horizontal velocity. See Figure 5. for explanation of symbols and curves. Dashed curves the lower right figure for Magnitude 7.1 to 7.2 emphasize uncertainty in slope (from Boore and others, 1981).

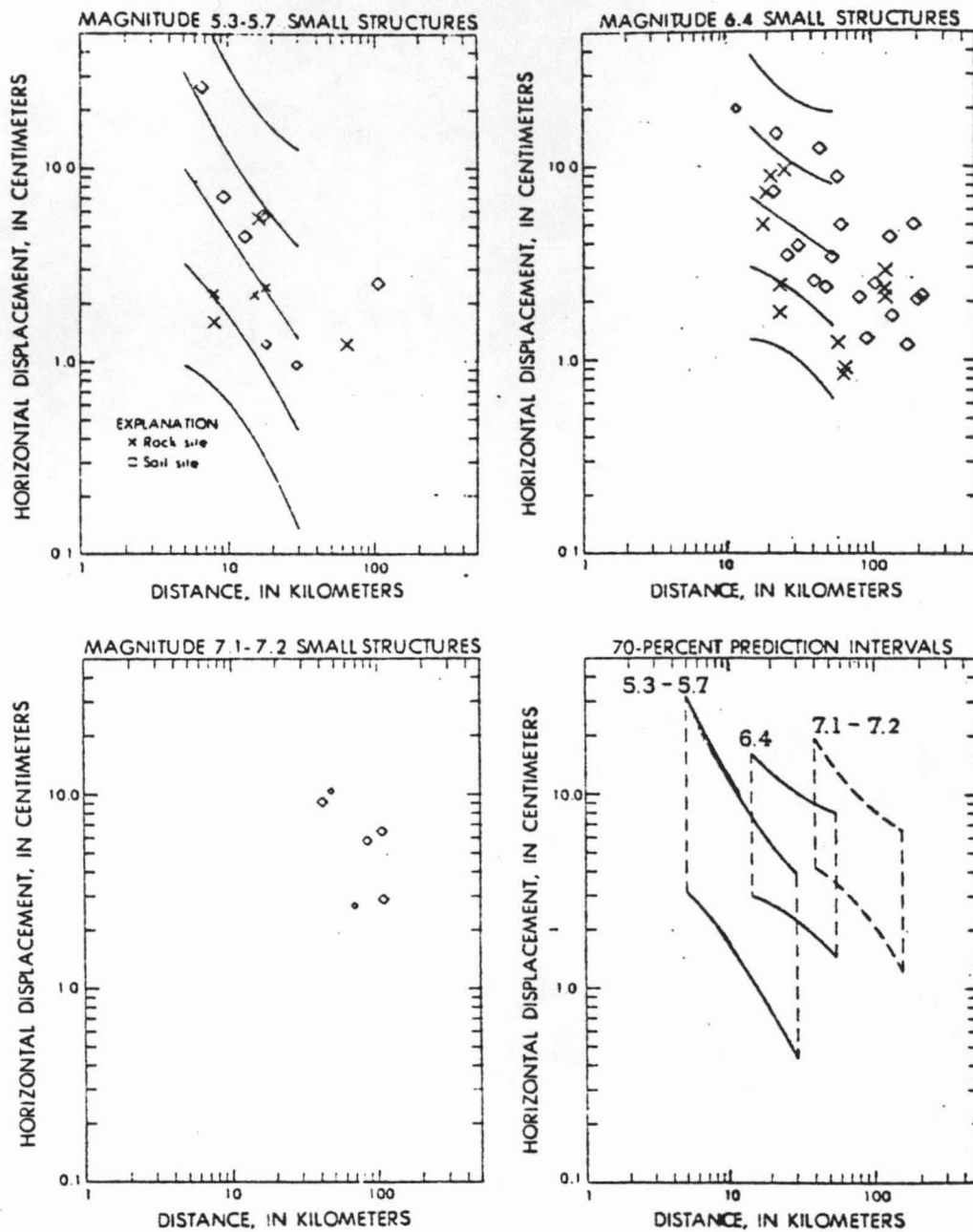


Figure 5.7. Peak horizontal displacement. See Figure 5. for explanation of symbols and curves (from Boore and others (1981)).

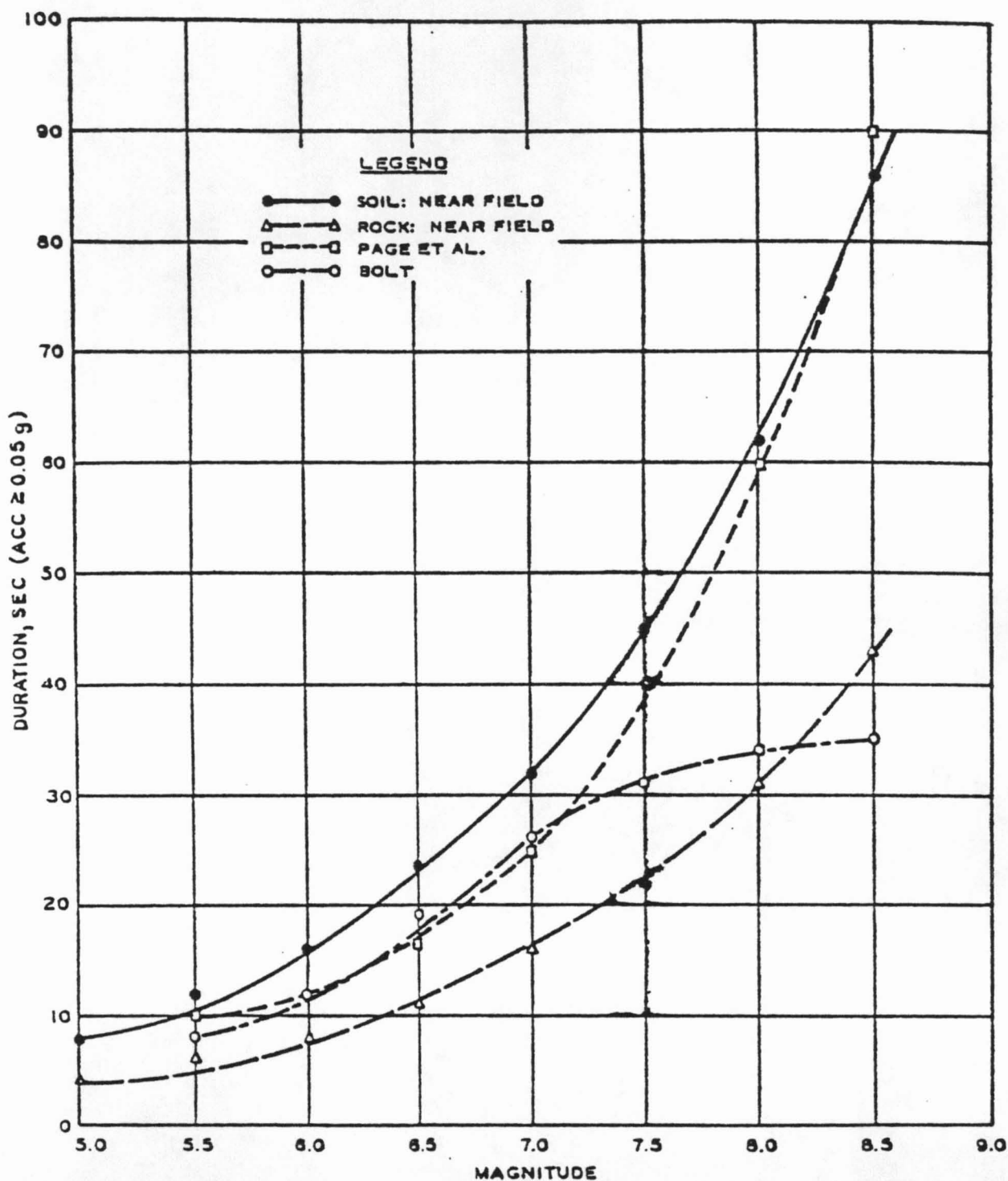


Figure 5.8. Near field duration of ground motion with acceleration greater than or equal to 0.05 g from historic earthquakes (Chang and Krinitzsky, 1977).

1. From PGP to the nearest point on the surface trace of the Hilina fault, about 20 km.
2. From PGP to the nearest potential hypocenter to the southwest on the bottom of the tectonically active block, about 25 to 30 km.
3. From PGP to the center of energy release, about 40 to 50 km.

For conservative planning purposes, the nearest hypocenter for a large magnitude tectonic earthquake on this fault zone can be assumed at 25 km from PGP.

The estimated ground motion at PGP, is assumed to be an earthquake of about 6.75 magnitude for the next 40 year time period, with a source earthquake distance of 25 km. This provides the following estimate of ground motion:

A. Mean Peak Horizontal Acceleration: The estimated mean peak horizontal acceleration from figure 5.4 is about 0.15 for $M = 6.0-6.4$ and 0.4 for $M = 7.1-7.6$. The peak acceleration from fig. 5.9 is about 0.16 for an earthquake of about 6.6 magnitude and 0.28 for 7.6 magnitude. These values are consistent with the recorded 0.22 g for the $M_s = 7.2$ earthquake in 1975, at Hilo with an epicentral distance of 43 km (Rojahn and Morrill, 1977). These data lead to an estimate of a mean peak horizontal acceleration of 0.25 g for the next 40 year period at the site.

B. Mean Peak Horizontal Velocity: The estimated mean peak horizontal velocity from fig. 5.5 is about 15 cm/sec for $M = 6.4$ and 35 cm/sec for an earthquake of $M = 7.1-7.2$. These data lead to an estimate of mean peak horizontal velocity of 25 cm/sec for the next 40 year period at the site.

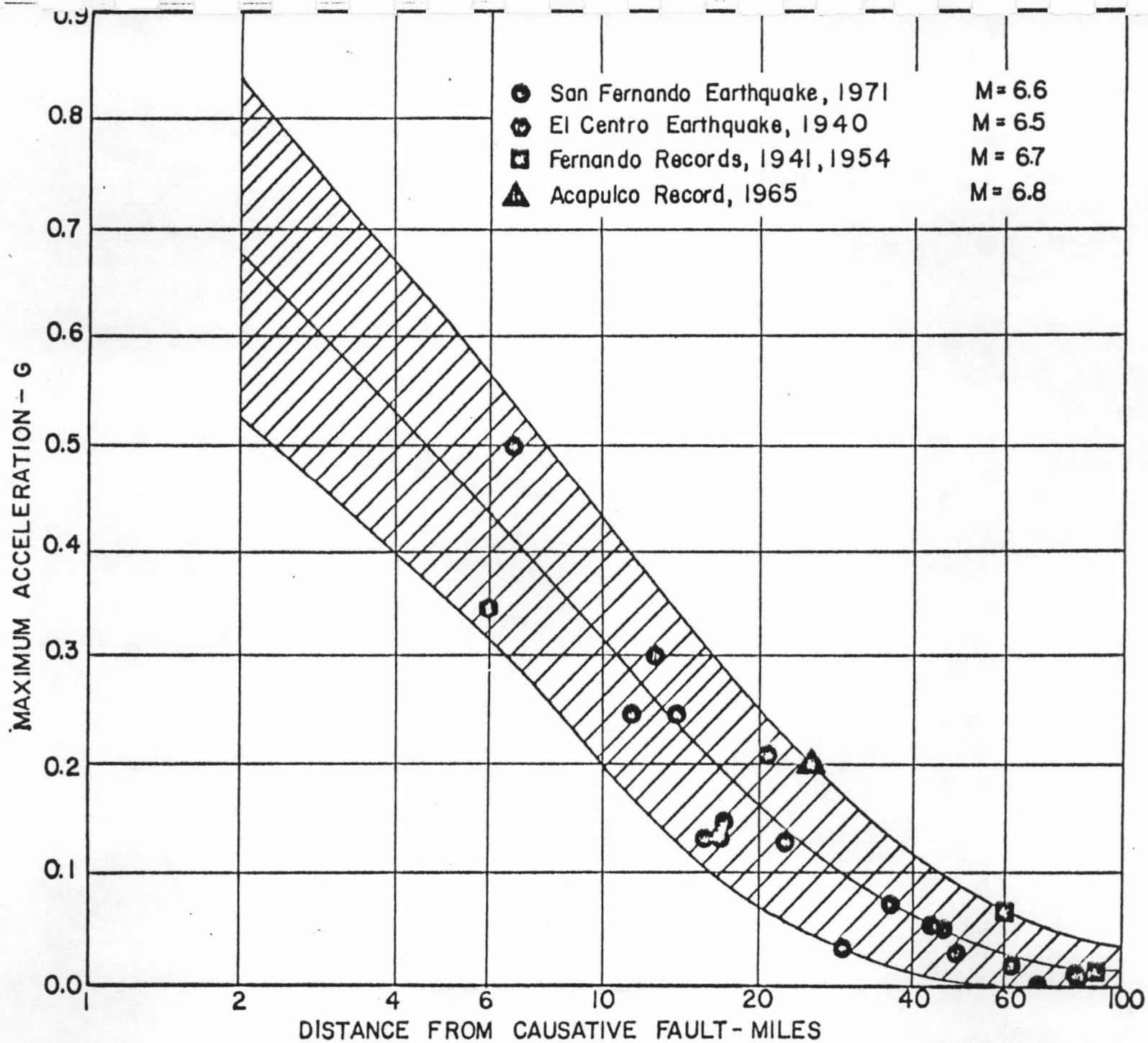


Figure 5.9. Maximum accelerations in rock for earthquakes with magnitude of about 6.6 (Schnable and Seed, 1972).

C. Mean Peak Horizontal Displacement: The estimated mean peak horizontal displacement from fig. 5.6 is about 5 cm for $M = 6.4$ and 15 cm for $M = 7.1-7.2$. The relative displacement was 3.4 cm at Hilo for the $M_s = 7.2$ earthquake in 1975, at an epicentral distance of 43 km (Rojahn and Morrill, 1977). These data lead to our estimate of mean peak horizontal displacement of 10 cm for the next 40 year period at the site.

5.6 Seismic Hazards at the Puna Geothermal Prospect

The main earthquake hazards are, in a general decreasing order of risk:

1. Ground motion
2. Landslides, slumps, and other secondary ground failures
3. Liquefaction
4. Surface faulting
5. Tsunamis and seiches

The principal hazard for the PGP is from strong ground motion from tectonic and volcanic related earthquakes. Tectonic earthquakes and their probable ground motions at the site are discussed in Section 5.4. Earthquakes caused by magmatic movements, although of high frequency and closer sources, have lower magnitudes and are expected to result in only minor damage and other effects (see Section 4.0).

Landslides, slumps and other gravity failures induced by strong earthquake motion are likely to affect the siting area. Liquefaction and tsunami effects are not important in the siting area, which is well above sea level and is generally devoid of materials that are susceptible to liquefaction. Surface faulting in the siting area is considered in Section 4.0.

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EXPLANATION OF ABBREVIATIONS AND SYMBOLS IN APPENDICES A, B, AND C

SOURCE CODES

CGS - Coast and Geodetic Survey
 ERL - Environmental Research Laboratories
 G-R - Gutenberg and Richter, 1954
 GS - U.S. Geological Survey, Denver, CO, U.S.A.
 HVO - Hawaiian Volcano Observatory, Hawaii National Park, HI, U.S.A.
 ISS - International Seismological Summary, Kew, England, U.K.
 NOS - National Ocean Survey
 USE - United States Earthquakes

TIME

Date and Origin time in Universal (Greenwich) Time. (Note: Many earthquakes from HVO given in Hawaiian Standard Time in Appendix A, and duplicated with data from other sources in Greenwich Time. Those events in Appendix A preceded by a (●) are duplicated because of this use of two time zones in the NOAA listing. Those events in Appendix A preceded by a (■) are duplicated in Appendix B. These two types of duplications are omitted from the data in use in this report).

AUTHORITY (follows origin time)

H - Parameters of hypocenter supplied by the USGS Hawaiian Volcano Observatory

MAGNITUDES

For source, see source codes above. Under surface wave, SH = Horizontal components used.

INTENSITY

Maximum in Modified Mercalli (MM) scale or converted to MM scale.

PHENOMENA

D	Diastrophism	-F, surface faulting; -U, uplift/subsidence; -D, faulting and uplift/subsidence
T	Tsunami	-t, tsunami generated; -Q, possible tsunami
S	Seiche	-S, seiche; -Q, possible seiche
V	Volcanism	-V, earthquake associated with volcanism
N	Non-tectonic	-C, coal bump or rockburst in coal mine; -E, explosion, accidental, controlled, or suspected explosion; -I, collapse; -L, lights or other such visual phenomena seen; -M, meteoritic source; -R, rockburst
O	Waves Generated	-A, acoustic wave; -G, gravity wave, -B, both A and G; -T, T-wave

REGION NUMBER (RN)

Geographic region number as described in Flinn, Engdahl, and Hill, 1974

CULTURAL EFFECTS (CE)

C - casualties
D - damage
F - felt

QUALITY/NUMBER OF STATIONS (Q/S)

Quality indicators are usually on an A, B, C, or D basis (A-very accurate; B-good; C-fair; D-poor). When used in combination for deep shocks, these represent the accuracy of (in order) epicenter, origin time, and depth.

MARSDEN/DEGREE SQUARE (MAR DG)

Numbering system dividing the world into 10° squares (MAR) and 1° subsquares (DG).

DISTANCE (DIST)

The distance in kilometers between the earthquake location and the designated point for radius searches.

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EARTHQUAKE DATA FILE

DR. D.B. STEMMONS UNIVERSITY OF NEVADA

160-KM RADIUS OF 19.467N.. 155.023W.

R1/07/17. 14.55.45.

PRINTED OUTPUT WILL BE DISPOSED TO THE EGIS SITE LINE PRINTER

SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES	INT PHENOM	PK CE Q/S	MAP DG	DIST (KM)	
										-----	-----	-----	-----	-----	
										BODY	SURF	OTHER	LOCAL	MAX DTSVNO	(KM)
*** INDICATES A POSSIBLE DUPLICATE															
S-R	1929	09	26	04	50	56.0	19.750N	156.000W		5.60FAS	VII	613 D	052 96	34.	
S-R	1933	12	16	07	31	31.0	19.750N	156.000W		6.50FAS	VII	613 D	052 96	34.	
S-R	1935	05	26	19	59	05.0F	19.500N	155.250W		5.60FAS	V	613 D	052 95	66.	
S-R	1940	05	17	10	26	47.0	20.500N	155.250W		6.00FAS	VI	613 D	068 05	133.	
S-R	1942	07	16	03	17	33.0M	20.500N	155.000W		5.60FAS		613 F	058 05	147.	
S-R	1941	09	25	17	48	36.0	19.500N	155.500W		6.00FAS	VII	613 D	052 95	40.	
S-R	1944	12	27	14	11	41.0	19.500N	155.500W		5.60FAS	VI	613 D	052 95	40.	
S-R	1947	05	31	11	15	15.0	19.500N	156.000W		6.25FAS	VI	613 D	052 96	13.	
USE	1948	04	24	11	00	21.0	19.400N	155.500W		6.50FAS	VII	613 D	052 95	66.	
S-R	1941	05	01	17	07	00.0	19.700N	156.000W	60.	6.90FAS	VI	613 C	052 96	34.	
USE	1943	05	27	02	17	26.0F	19.400N	155.400W				613 D	052 95	42.	
S-R	1953	03	03	16	40	20.0	19.500N	155.000W		6.00FAS		613 F	052 95	42.	
USE	1954	03	31	03	47	03.0M	20.500N	155.000W				613 D	052 95	42.	
S-R	1954	03	31	03	47	03.0M	20.500N	155.000W		6.50FAS	VII	613 D	068 05	116.	
USE	1954	02	10	01	51.0F	19.100N	155.000W	005				613 F	052 95	64.	
USE	1957	02	23	05	51.0F	19.100N	155.000W	005				613 F	052 95	78.	
USE	1959	01	15	15	30	10.0F	19.333N	155.250W	005			613 F	052 95	65.	
USE	1959	03	17	02	43	15.0F	19.733N	155.250W	015			613 F	052 95	77.	
USE	1959	03	04	14	20	42.0	19.173N	155.033W	015	3.50		613 F	052 95	44.	
USE	1959	01	19	17	54	55.0F	20.115N	155.416W	015			613 F	052 95	71.	
USE	1959	05	17	17	40	17.0F	19.400N	155.033W	015			613 F	052 95	37.	
S-R	1961	01	17	13	07	50.0F	19.000N	156.175W	005			613 F	052 96	30.	
S-R	1961	01	15	19	44	40.3M	19.000N	155.625W	005			613 F	052 95	55.	
S-R	1961	01	14	12	54	24.0F	19.300N	155.422W	003			613 F	052 95	10.	
USE	1961	01	21	11	11	36.0F	19.200N	155.033W	001			613 F	052 95	39.	
USE	1961	01	24	04	07	40.0F	19.000N	155.473W	005			613 F	052 95	68.	
USE	1961	01	14	13	16	01.0F	19.400N	155.013W	005			613 F	052 95	61.	
USE	1961	03	31	14	41	14.0F	19.557N	155.260W	025			613 F	052 95	66.	
USE	1961	04	02	18	09	10.0F	20.000N	155.400W	005			613 F	068 05	76.	
USE	1961	04	18	10	37	47.0F	19.100N	155.450W	008			613 F	052 95	49.	
USE	1961	04	11	14	11	24.0F	19.400N	155.250W	030			613 F	052 95	61.	
USE	1961	04	21	01	11	14.0F	19.300N	155.192W	005			613 F	052 95	51.	
USE	1961	04	21	02	11	10.0F	19.400N	155.400W	005			613 F	052 95	41.	
USE	1961	04	27	16	01	21.0F	19.100N	155.500W	008			613 F	052 95	52.	
USE	1961	05	17	11	27	22.0F	19.400N	155.000W	030			613 F	052 95	60.	
USE	1961	05	18	10	31	50.0F	19.500N	155.033W	013			613 F	052 95	60.	
USE	1961	05	27	08	12	48.0F	19.400N	155.437W	001			613 F	052 95	47.	
USE	1961	05	17	03	13	05.0F	19.400N	155.260W	008			613 F	052 95	64.	
USE	1961	06	24	13	00	29.5F	19.300N	155.322W	005			613 F	052 95	60.	
USE	1961	06	21	14	13	17.0F	19.400N	155.250W	030			613 F	052 95	63.	
USE	1961	06	31	13	24	25.0F	19.400N	155.000W	030			613 F	052 95	63.	
USE	1961	06	31	16	41	55.0F	19.515N	155.172W	024			613 F	052 95	60.	
USE	1961	07	02	10	34	10.7F	19.400N	155.250W	030			613 F	052 95	60.	
USE	1961	07	14	01	51	21.0F	19.200N	155.470W	015			613 F	052 95	44.	
USE	1961	07	25	13	24	17.1F	19.400N	155.250W	030.			613 D	052 95	64.	
USE	1961	07	21	15	21	27.0F	19.400N	155.250W	030.			613 F	052 95	60.	
USE	1961	07	21	15	30	51.0F	19.400N	155.000W	030			613 F	052 95	60.	
USE	1961	07	24	13	22	42.0F	19.400N	155.250W	030			613 F	052 95	60.	
USE	1961	07	23	02	53	40.4F	19.400N	155.250W	030			613 F	052 95	60.	
USE	1961	07	24	01	14	21.0F	20.000N	155.217W	003			613 F	052 95	93.	

SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES			INT MAX	FPHOM DTSVNO	RN	CE	G/S	MAR	DG	DISI (KM)
										BODY	SURF	OTHER								
**N INDICATES A POSSIBLE DUPLICATE																				
USE	1961	08	21	16	55	11.0F	19.420N	155.220W	003											
USE	1961	08	25	18	45	35.1F	19.865N	155.070W	035											
USE	1961	09	13	14	24	29.5H	19.855N	155.435W	013											
USE	1961	09	23	08	19	37.5H	19.333N	155.093W	003											
USE	1961	09	22	00	33	00.5H	19.333N	155.083W	003											
USE	1961	09	22	00	54	21.7H	19.333N	155.083W	003											
USE	1961	09	23	03	31	32.4Z	19.400N	155.110W	003											
USE	1961	09	25	15	19	39.6H	19.400N	155.263W	030											
USE	1961	09	25	18	25	08.7H	19.358N	155.100W	003											
USE	1961	09	25	18	25	53.5H	19.400N	155.100W	003											
USE	1961	09	25	06	29	21.8F	19.400N	155.100W	003											
USE	1961	09	25	06	38	27.0H	19.358N	155.100W	003											
USE	1961	09	25	03	12	30.5H	19.358N	155.100W	003											
USE	1961	09	28	17	24	01.0H	19.358N	155.100W	003											
USE	1961	09	28	17	24	41.0F	19.358N	155.100W	003											
USE	1961	10	04	16	34	27.0H	19.777N	155.640W	013											
USE	1961	10	10	19	37	21.0H	19.433N	155.313W	012											
FVJ	1961	11	14	14	01	07.0H	19.400N	155.020W	003											
FVJ	1961	11	14	15	58	43.0H	19.777N	155.600W	003											
FVJ	1961	11	14	15	57	14.0H	19.433N	155.012W	003											
USE	1961	11	22	19	24	39.0H	19.400N	155.070W	030											
USE	1961	11	22	19	48	01.0H	19.400N	155.083W	030											
USE	1961	11	22	00	55	55.0H	19.400N	155.083W	030											
USE	1961	11	24	11	27	39.0H	19.400N	155.263W	030											
USE	1961	11	24	13	14	59.0H	19.400N	155.263W	030											
USE	1961	11	24	11	14	31.0H	19.400N	155.093W	030											
USE	1961	11	23	13	34	11.0F	19.400N	155.083W	030											
USE	1961	11	27	14	01	21.0H	19.400N	155.083W	030											
USE	1961	12	03	4	57	58.0H	19.400N	155.083W	030											
USE	1961	12	12	17	55	31.0H	19.400N	155.263W	030											
USE	1961	12	15	21	17	57.4H	19.400N	155.263W	030											
FVJ	1961	12	17	17	57	50.0H	19.433N	155.013W	013											
USE	1961	12	31	16	13	23.0H	19.777N	155.630W	009											
USE	1961	12	31	16	52	09.0H	19.400N	155.263W	030											
USE	1962	01	17	12	57	53.4H	19.400N	155.083W	005											
USE	1962	02	17	17	04	35.0H	19.400N	155.265W	030											
USE	1962	03	13	19	45	19.0H	19.777N	155.030W	015											
USE	1962	03	24	19	06	40.0H	19.400N	155.265W	030											
USE	1962	03	31	19	15	56.1H	19.400N	155.083W	030											
USE	1962	03	24	19	06	57.0H	19.400N	155.083W	030											
USE	1962	05	17	15	55	14.0H	19.400N	155.083W	030											
USE	1962	05	11	16	17	03.4H	19.400N	155.265W	030											
USE	1962	05	23	21	17	09.0H	19.400N	155.265W	012											
USE	1962	05	24	19	57	09.0H	19.400N	155.265W	045											
USE	1962	05	37	17	11	08.0H	19.317N	155.600W	001											
USE	1962	06	19	09	35	21.0H	19.217N	155.217W	005											
USE	1962	06	19	07	43	16.0H	19.400N	155.417W	005											
USE	1962	06	14	13	34	50.0H	19.417N	155.265W	030											
USE	1962	06	28	13	38	56.0H	19.400N	155.417W	005											
USE	1962	07	14	14	41	41.0H	19.200N	155.601W	005											

01/27/17.

SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KMS)	-----MAGNITUDES-----				INT PHENOM MAX DTSVVO	RN	CE	Q/S	MAR	DG	DIST (KMS)
										PODY	SURF	OTHR	LOCAL							
*** INDICATES A POSSIBLE DUPLICATE																				
USE	1962	07	14	17	37	53.1P	19.747N	155.637W	010											
USE	1962	07	24	09	52	41.1H	19.442N	155.987W	005											
JSE	1962	07	31	12	46	44.0H	19.425N	155.000W	005											
USE	1962	07	31	15	24	15.0P	19.333N	155.082W	005											
JSE	1962	08	18	09	30	06.5H	19.180N	155.533W	001											
USE	1962	08	19	00	56	41.9H	19.303N	155.195W	008											
USE	1962	08	18	11	58	58.0H	19.316N	155.142W	008											
USE	1962	09	11	05	11	15.0P	19.333N	155.105W	003											
USE	1962	09	11	17	22	49.4P	19.477N	155.233W	003											
USE	1962	09	11	17	25	27.5P	19.477N	155.233W	004											
USE	1962	09	20	00	02	37.3P	19.083N	155.070W	012											
USE	1962	09	25	23	22	53.4H	19.252N	155.503W	008											
USE	1962	10	19	16	43	29.0P	19.660N	156.100W	012											
USE	1962	10	31	23	30	50.0P	19.197N	155.550W	003											
JSE	1962	11	22	11	54	55.0P	20.277N	155.190W	012											
USE	1962	11	22	18	16	21.7P	19.333N	155.083W	005											
JSE	1962	12	14	06	21	31.7H	19.320N	155.353W	007											
USE	1962	12	14	07	56	16.7H	19.400N	155.285W	008											
JSE	1962	12	16	11	04	10.0P	19.370N	155.013W	001											
USE	1962	12	31	03	47	19.0P	19.077N	155.096W	003											
JSE	1963	01	14	19	34	44.0P	19.311N	155.315W	007											
JSE	1963	01	19	11	41	06.0P	19.401N	155.285W	003											
USE	1963	03	13	03	57	26.9P	19.413N	155.500W	005											
FVJ	1963	03	22	21	54	40.0P	19.341N	155.431W	012											
USE	1963	03	26	06	31	51.0P	19.700N	155.563W	012											
FVJ	1963	03	25	17	14	35.0H	20.700N	155.033W	005											
FVJ	1963	03	12	00	25	57.0P	20.17N	155.010W	008											
JSE	1963	05	19	12	21	05.0P	19.040N	155.110W	001											
JSE	1963	05	07	08	25	31.0P	19.190N	155.551W	003											
JSE	1963	06	14	01	17	57.0P	19.417N	155.279W	003											
JSE	1963	07	11	12	43	57.5H	19.353N	155.166W	003											
JSE	1963	07	11	15	10	14.7H	19.360N	155.215W	003											
CJS	1963	08	24	18	49	16.6	19.100N	155.600W	005											
USE	1963	08	13	02	54	30.0P	19.410N	155.411W	005											
FVJ	1963	08	06	15	11	01.0H	19.495N	156.048W	003											
JSE	1963	08	14	18	17	57.5P	19.348N	155.543W	012											
CJS	1963	09	21	16	24	24.1	19.210N	155.500W	005											
JSE	1967	01	23	04	26	17.4P	19.470N	155.471W	005											
JSE	1963	01	22	16	27	24.4P	19.400N	155.411W	005											
JSE	1963	1	08	08	20	33.7P	19.200N	155.175W	005											
JSE	1963	1	12	02	02	47.0P	19.134N	155.083W	008											
CJS	1963	1	03	20	24	16.5	19.400N	155.500W	005											
USE	1963	1	23	21	24	47.0P	19.400N	155.400W	005											
USE	1963	1	24	04	25	25.0P	19.400N	155.400W	005											
USE	1963	1	26	11	05	34.0H	19.400N	155.400W	005											
USE	1963	1	26	10	03	54.7H	19.400N	155.400W	00											
FVJ	1963	11	14	17	23	05.4P	20.185N	155.400W	012											
USE	1963	11	15	19	01	26.5P	19.410N	155.285W	003											
USE	1963	11	30	04	00	00.0P	19.335N	155.100W	008											
JSE	1964	01	17	11	16	25.0P	19.310N	155.025W	008											

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT F-PHENOM MAX DTSVNO	RN	CE	Q/S	MAP	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
*** INDICATES A POSSIBLE DUPLICATE																				
JSE	1964	02	21	01	31	44.5H	20.700N	155.133W	012											
USE	1964	03	13	10	54	38.0H	19.275N	155.182W	008											
JSE	1964	03	12	05	30	56.4H	19.202N	155.097W	011											
JSE	1964	04	01	12	28	53.0H	19.415N	155.417W	033											
USE	1964	06	04	18	34	31.9H	19.447N	155.280W	045											
JSE	1964	06	04	21	22	30.0H	19.300N	155.077W	004											
JSE	1964	06	06	22	35	57.5H	19.630N	155.418W	008											
JSE	1964	07	11	27	43	04.5H	19.313N	155.115W	005											
USE	1964	07	17	23	16	56.4H	19.590N	155.987W	013											
USE	1964	07	20	04	05	51.2H	19.400N	155.160W	025											
JSE	1964	07	23	20	36	01.7H	19.190N	155.051W	004											
CSS	1964	08	13	18	27	35.4	19.500N	155.400W	011	4.10MB										
JSE	1964	08	26	19	37	45.5H	20.233N	156.150W	012											
USE	1964	09	01	16	53	13.5H	19.482N	154.925W	005											
JSE	1964	09	14	19	10	12.1H	19.440N	154.937W	003											
JSE	1964	09	18	10	08	09.1H	19.315N	155.116W	005											
JSE	1964	09	19	10	17	08.4H	19.200N	155.122W	005											
JSE	1964	10	11	15	16	40.1H	19.700N	156.617W	018											
JSE	1964	10	18	12	27	17.0H	19.330N	155.095W	008											
JSE	1964	10	24	05	17	18.4H	19.110N	155.413W	010											
USE	1964	10	27	19	05	61.7H	19.400N	155.095W	017											
JSE	1964	12	03	18	08	4.7H	19.400N	155.065W	030											
JSE	1964	12	03	24	31	43.3H	19.400N	155.065W	030											
JSE	1964	12	03	19	08	01.5H	19.400N	155.065W	030											
JSE	1964	12	11	11	53	49.1H	19.700N	155.013W	010											
USE	1964	12	14	05	31	17.7H	19.300N	155.025W	008											
JSE	1964	01	11	19	17	43.4H	19.200N	155.400W	013											
JSE	1964	01	14	06	10	20.2	20.100N	155.042W	020											
JSE	1964	01	26	18	18	13.2H	19.760N	155.575W	012											
USE	1964	02	19	19	40	31.0H	19.000N	155.500W	013											
JSE	1964	03	16	03	06	29.3	19.700N	155.067W	013											
USE	1964	03	16	11	12	12.0H	19.300N	155.000W	005											
JSE	1964	03	01	05	37	19.0H	19.365N	155.412W	007											
USE	1964	03	22	17	33	10.0H	19.000N	155.500W	000											
JSE	1964	04	17	02	17	07.4H	19.360N	155.076W	011											
JSE	1964	05	16	14	27	3.7	19.700N	156.135W	008											
JSE	1964	05	16	19	19	40.4H	19.337N	155.445W	004											
JSE	1964	05	25	18	17	04.4H	19.100N	155.100W	010											
JSE	1964	06	01	11	11	43.1H	19.300N	155.023W	025											
JSE	1964	07	17	17	31	36.1	19.700N	156.500W	022											
JSE	1964	07	18	03	02	04.1H	19.300N	155.034W	000											
JSE	1964	07	22	01	07	04.2H	19.335N	155.510W	007											
JSE	1964	08	11	02	18	16.8H	19.000N	155.107W	002											
JSE	1964	08	23	21	25	07.0H	19.200N	155.197W	010											
USE	1964	09	25	11	34	17.0H	19.300N	155.163W	008											
USE	1964	10	25	12	53	35.0H	19.700N	155.152W	005											
JSE	1964	09	11	04	11	57.0H	19.500N	155.333W	032											
JSE	1964	09	09	11	42	40.0H	19.200N	155.163W	003											
JSE	1964	11	23	19	09	59.3H	19.300N	155.300W	031											
JSE	1964	12	02	12	38	17.7H	19.770N	154.940W	045											

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SOURCE	YEAR	MO	DA	HR	MM	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES	INT	PHENOM	RN	CE	C/S	MAP	DG	DIST (KM)	

										BODY	SURF	OTHER	LOCAL	MAX	DTSVNO				
*** INDICATES A POSSIBLE DUPLICATE																			
COS	1965	12	26	09	35	37.3	19.400N	155.200W	003	4.3CMR			613	F	C11	C52	95	72.	
USE	1966	01	08	23	43	57.3H	19.428N	155.478W	008				613	F		C52	95	42.	
USE	1966	01	19	12	44	12.2H	19.405N	155.328W	013				613	F		C52	95	58.	
USE	1966	01	20	00	01	37.4H	19.397N	155.558W	013				613	F		C52	95	35.	
HVO	1966	01	22	07	02	26.9	19.465N	155.178W	008				613	F		C52	95	0.	
USE	1966	02	13	05	56	16.3H	19.372N	155.310W	030				613	F		C52	95	61.	
HVO	1966	02	22	01	59	33.3	19.645N	155.670W	033				613	F		C52	95	41.	
USE	1966	03	01	06	01	11.0H	19.412N	155.453W	010				613	F		C52	95	45.	
HVO	1966	03	10	18	00	23.3	19.783N	155.767W	008				613	F		C52	95	37.	
USE	1966	03	15	00	04	53.6H	19.317N	155.442W	001				613	F		C52	95	49.	
USE	1966	03	16	00	43	02.7H	19.377N	155.310W	032				613	F		C52	95	62.	
USE	1966	05	27	11	05	46.0H	19.218N	155.060W	040				613	F		C52	95	91.	
HVO	1966	06	19	07	21	26.9	19.352N	155.752W					613	F		C52	95	15.	
USE	1966	07	01	15	04	28.0H	19.325N	155.485W	010				613	F		C52	95	47.	
USE	1966	07	31	10	54	21.3H	19.417N	155.420W	001				613	F		C52	95	49.	
USE	1966	08	07	06	57	37.1H	19.461N	154.934W	001				613	F		C52	94	103.	
JSC	1966	08	15	17	15	41.2H	19.443N	154.718W	003				613	F		C52	94	101.	
USE	1966	08	19	10	21	43.2H	19.433N	155.140W	030				613	F		C52	95	61.	
USE	1966	09	05	16	30	21.0H	19.453N	155.437W	001	4.7CMP			613	F		C52	95	48.	
JSC	1966	09	08	00	17	21.0H	19.473N	155.431W	005				613	F		C52	95	49.	
USE	1966	10	13	13	47	17.0H	19.375N	155.092W	025				613	F		C52	95	63.	
USE	1966	11	31	04	49	20.0H	19.321N	155.467W	008				613	F		C52	95	46.	
HVO	1966	11	05	09	42	30.0	19.480N	155.703W	003				613	F		C52	95	4.	
USE	1966	11	17	15	17	01.0H	19.440N	154.833W					613	F		C52	94	100.	
USE	1966	11	27	01	54	01.0H	19.320N	155.230W	010				613	F		C52	95	71.	
HVO	1966	12	10	05	44	11.0	19.475N	155.673W	002				613	F		C52	95	1.	
HVO	1966	12	13	18	41	15.0	19.366N	156.773W	008				613	F		C52	96	48.	
USE	1967	01	26	17	01	32.0H	19.335N	155.117W	001				613	F		C52	95	61.	
USE	1967	01	01	13	14	51.5H	19.392N	155.211W	022				613	F		C52	95	61.	
USE	1967	01	11	05	10	19.0H	19.372N	155.333W	027				613	F		C52	95	58.	
COS	1967	02	02	01	37	41.0H	19.353N	155.920W	005	4.6CMR			613	F	042	C52	95	54.	
COS	1967	02	04	05	20	34.0H	19.374N	155.453W	008	4.43MB			613	F	036	C52	95	46.	
USE	1967	02	26	15	47	01.0H	19.415N	155.401W	007				613	F		C52	95	77.	
USE	1967	06	09	20	20	14.0H	19.318N	155.267W	007				613	F		C11	C5	62.	
USE	1967	06	14	10	50	53.7H	19.716N	155.384W	005				613	F		C52	95	72.	
USE	1967	06	24	17	40	05.0H	19.665N	155.666W	005				613	F		C52	95	55.	
COS	1967	07	01	04	01	54.1H	19.481N	155.015W	02				613	F		C52	95	64.	
COS	1967	07	01	15	17	40.0	19.470N	155.210W	030	4.2CMR			613	F	(13)	C52	95	61.	
USE	1967	07	10	11	03	40.0H	19.450N	155.212W	028				613	F		C52	95	71.	
USE	1967	07	13	11	01	01.0H	19.466N	155.415W	005				613	F		C52	95	53.	
USE	1967	07	16	12	01	18.0H	19.380N	155.425W	008				613	F		C52	95	46.	
USE	1967	07	17	03	14	17.0H	19.553N	155.215W	020				613	F		C52	95	63.	
USE	1967	07	17	02	04	23.0H	19.441N	155.617W	002				613	F		C52	95	28.	
USE	1967	07	22	07	34	27.0H	19.351N	155.414W	008				613	F		C52	95	50.	
JSC	1967	08	14	05	27	00.0H	19.218N	155.045W	007				613	F		C52	95	42.	
USE	1967	08	05	15	01	01.2H	19.715N	155.269W	026				613	F		C52	95	65.	
USE	1967	08	15	05	23	30.0H	19.367N	155.214W	001				613	F		C52	95	76.	
USE	1967	08	18	06	41	21.7H	19.393N	155.366W	008				613	F		C52	95	79.	
USE	1967	08	19	01	11	22.4H	19.460N	155.352W	003				613	F		C52	95	79.	
USE	1967	08	19	02	07	36.4H	19.417N	155.264W	001				613	F		C52	95	72.	

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SOURCE YEAR MO DA FR M SEC LA L G DEPT -----MAGNITUDES----- INT PHENOM RN CE C/S MAR DG DIST
 (KM) BODY SURF OTHER LOCAL MAX DTSVNO (KM)

**N INDICATES A POSSIBLE DUPLICATE

USE	1967	08	22	08	02	58.3H	19.150N	155.518W	001							3.40ML	HVO		613 F		052	95	52.		
JSE	1967	08	27	17	46	19.2H	19.302N	155.216W	001							3.50ML	FVO		613 F		052	95	72.		
USE	1967	08	31	17	56	23.5H	19.318N	155.416W	009							3.20ML	FVO		613 F		052	95	52.		
USE	1967	09	12	19	33	52.1H	19.352N	155.267W	039							3.30ML	HVO		613 F		052	95	66.		
USE	1967	09	17	05	11	08.9H	19.265N	155.301W	030							3.10ML	FVO		613 F		052	95	64.		
**1	055	1967	09	08	12	22	29.9	19.300N	155.600W	017									613		019	052	95	35.	
**2	JSE	1967	09	08	12	22	32.5H	19.417N	155.215W	013									613 F			052	95	35.	
USE	1967	09	23	16	37	23.5H	19.293N	155.367W	010							3.65ML	FVO		613 F		052	95	51.		
USE	1967	09	26	22	59	25.4H	19.150N	155.168W	045							3.40ML	HVO		613 F		052	95	76.		
JSE	1967	09	28	10	05	55.0H	19.483N	155.019W	029							3.20ML	FVO		613 F		052	95	70.		
USE	1967	10	10	09	43	31.0H	19.383N	155.483W	010							3.20ML	HVO		613 F		052	95	43.		
USE	1967	10	15	15	57	58.7H	19.417N	155.466W	005							3.70ML	FVO		613 F		052	95	44.		
USE	1967	10	27	22	42	32.0H	19.333N	155.251W	032							3.00ML	FVO		613 F		052	95	69.		
JSE	1967	10	29	13	34	37.2	19.394N	155.552W	010									3.80				052	95	67.	
JSE	1967	11	01	14	16	56.5H	19.350N	155.652W	025							3.10ML	HVO		613 F		052	95	64.		
JSE	1967	11	05	13	21	16.8H	19.400N	155.270W	006							3.40ML	HVO		613 F		052	95	63.		
JSE	1967	11	05	16	58	14.6H	19.350N	155.416W	010							3.20ML	FVO		613 F		052	95	51.		
JSE	1967	11	26	10	39	43.5H	19.350N	155.293W	009							3.30ML	FVO		613 F		052	95	64.		
JSC	1967	12	06	10	14	13.9H	19.334N	155.002W	010							3.10ML	HVO		613 F		052	95	73.		
JSE	1967	12	08	25	7	32.0H	19.416N	155.416W	005							3.10ML	FVO		613 F		052	95	49.		
USE	1968	01	10	4	14	15.7H	19.380N	155.335W	007							3.00ML	FVO		613 F		052	95	65.		
JSE	1968	01	15	17	10	47.7H	19.380N	155.133W	010							3.00ML	FVO		613 F		052	95	60.		
USE	1968	01	17	05	10	11.0H	19.267N	155.367W	040							3.50ML	FVO		613 F		052	95	58.		
JSE	1968	01	25	07	43	44.5H	19.350N	155.180W	008							3.70ML	HVO		613 F		052	95	92.		
USE	1968	02	02	13	38	34.6H	19.334N	155.119W	009							3.50ML	FVO		613 F		052	95	61.		
USE	1968	02	15	16	37	47.8H	19.350N	155.120W	004							3.10ML	FVO		613 F		052	95	62.		
JSE	1968	04	14	01	06	11.1H	19.383N	155.450W	008							3.70ML	FVO		613 F		052	95	46.		
USE	1968	04	15	11	17	24.0H	19.350N	155.269W	007							3.70ML	HVO		613 F		052	95	65.		
JSE	1968	04	19	00	31	25.5H	19.350N	155.417W	010							3.00ML	FVO		613 F		052	95	54.		
JSE	1968	04	14	16	13	40.8H	19.356N	155.266W	009							3.20ML	FVO		613 F		052	95	65.		
USE	1968	04	26	14	08	59.0H	19.380N	155.085W	031							4.50ML	FVO		613 F		052	95	64.		
USE	1968	04	26	16	35	25.1H	19.402N	155.435W	008							3.40ML	FVO		613 F		052	95	47.		
JSE	1968	05	29	21	42	34.5H	19.417N	155.266W	002							3.70ML	HVO		613 F		052	95	65.		
USE	1968	05	23	17	17	25.4H	19.380N	155.117W	009							3.10ML	FVO		613 F		052	95	62.		
JSE	1968	06	03	16	27	28.9H	19.380N	155.285W	030							3.00ML	FVO		613 F		052	95	64.		
JSE	1968	06	19	14	34	18.7H	19.400N	155.264W	005							3.00ML	FVO		613 F		052	95	63.		
JSE	1968	07	12	20	55	08.3	19.380N	155.017W	008									3.40				052	95	69.	
JSE	1968	07	13	17	20	17.2H	19.380N	155.209W	013							3.50ML	FVO		613 F		052	95	72.		
JSE	1968	07	22	17	15	24.0H	19.380N	155.050W	010							3.30ML	FVO		613 F		052	95	68.		
JSE	1968	07	29	16	21	11.9H	19.380N	155.050W	009							3.30ML	FVO		613 F		052	95	64.		
JSE	1968	07	30	05	35	44.7H	19.380N	155.001W	010							3.70ML	HVO		613 F		052	95	63.		
JSE	1968	08	01	16	34	37.8H	19.380N	155.112W	010							4.00ML	HVO		613 F		022	052	95	83.	
USE	1968	08	03	04	56	56.4H	19.450N	155.016W	040									3.80				017	052	95	43.
JSE	1968	08	05	20	37	19.0	19.380N	155.033W	005									3.10				052	95	48.	
JSE	1968	08	17	20	58	25.3	19.380N	155.000W	008									4.40				052	95	19.	
USE	1968	08	09	11	04	53.4H	19.384N	155.283W	030													016	052	95	61.
JSE	1968	08	16	23	14	01.4H	19.400N	155.283W	015							3.20ML	FVO		613 F		052	95	63.		
JSE	1968	08	17	02	23	37.6H	19.380N	155.269W	008							4.10ML	FVO		613 F		052	95	71.		
JSE	1968	08	21	02	29	47.9H	19.380N	155.416W	009							3.50ML	FVO		613 F		052	95	50.		
JSE	1968	08	21	21	25	56.0H	19.410N	155.001W	008							3.00ML	HVO		613 F		052	95	45.		

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT	PHENOM	RN	CE	Q/S	MAR	DG	CIST (KM)
										BODY	SURF	OTHER	LOCAL								
**V INDICATES A POSSIBLE DUPLICATE																					
USE	1964	08	22	14	09	56.0H	19.367N	155.233W	004												
USE	1964	09	03	00	58	23.4H	19.352N	155.450W	006												
USE	1964	09	05	16	12	43.7H	19.352N	155.365W	008												
USE	1964	09	08	13	03	44.3H	19.433N	155.266W	020												
USE	1964	09	24	04	11	53.3	20.167N	155.201W	008												
USE	1964	10	26	00	47	09.9H	19.152N	155.501W	008												
USE	1964	11	10	20	24	45.4H	19.401N	155.484W	007												
USE	1964	11	14	09	52	59.0H	19.217N	154.966W	007												
USE	1964	11	20	06	43	21.1H	19.366N	155.300W	030												
USE	1964	12	17	02	33	03.5H	19.319N	155.200W	010												
USE	1964	12	20	08	19	11.1H	19.333N	155.102W	009												
USE	1964	01	16	03	25	00.2H	19.318N	155.217W	010												
USE	1964	01	15	07	37	08.2H	19.785N	155.502W	009												
USE	1964	01	20	15	54	26.0H	19.367N	155.485W	008												
USE	1964	01	21	17	34	37.1H	19.401N	155.402W	008												
USE	1964	02	07	09	33	51.1H	19.201N	155.350W	045												
USE	1964	02	07	10	00	56.0H	19.300N	155.383W	030												
USE	1964	02	09	05	05	40.3H	19.334N	155.150W	010												
USE	1964	02	11	02	04	40.2H	19.333N	155.133W	010												
USE	1964	02	17	11	42	01.0H	19.571N	155.116W	010												
USE	1964	02	22	02	04	10.1	19.444N	155.025W	010												
USE	1964	02	22	17	33	35.0H	19.302N	155.401W	010												
USE	1964	03	01	13	01	41.0H	19.414N	155.433W	008												
USE	1964	03	05	14	15	10.3	19.504N	155.404W	035												
USE	1964	03	11	13	38	07.6H	19.314N	155.269W	027												
USE	1964	03	12	20	10	17.2H	19.217N	155.452W	008												
USE	1964	04	14	17	01	07.0H	19.573N	155.435W	008												
USE	1964	04	24	14	40	29.1H	19.402N	155.481W	009												
USE	1964	05	15	11	00	13.1H	19.404N	155.619W	008												
USE	1964	04	18	01	35	27.8H	19.366N	155.169W	011												
USE	1964	05	10	14	51	40.0H	19.300N	155.017W	010												
USE	1964	05	17	15	39	46.0H	19.333N	155.385W	047												
USE	1964	05	17	22	32	51.4H	19.235N	155.417W	034												
USE	1964	05	23	13	07	21.8H	19.000N	155.034W	010												
USE	1964	05	25	13	59	50.8H	19.318N	155.119W	008												
USE	1964	05	25	13	43	18.1H	19.300N	155.633W	009												
USE	1964	05	26	14	21	49.7H	19.334N	155.111W	004												
USE	1964	05	27	19	10	20.0H	19.414N	155.264W	010												
USE	1964	05	28	03	33	51.0H	19.333N	155.110W	011												
USE	1964	05	24	13	30	50.0H	19.300N	155.201W	010												
USE	1964	05	25	01	43	41.3H	19.317N	155.211W	009												
USE	1964	05	26	19	41	46.0H	19.401N	155.450W	011												
USE	1964	05	25	11	55	31.0	19.300N	155.266W	010												
USE	1964	06	17	11	41	26.2H	19.207N	155.183W	010												
USE	1964	05	17	05	14	53.1H	19.945N	155.102W	061												
USE	1964	05	18	10	01	49.4H	19.300N	155.050W	007												
USE	1964	07	03	16	57	30.6H	19.302N	155.200W	005												
USE	1964	07	05	01	37	04.0H	19.300N	155.351W	032												
USE	1964	07	13	11	28	03.0H	19.207N	155.165W	009												
USE	1964	07	20	14	47	11.1	19.300N	155.492W	010												

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES				INT PHENOM MAX DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
**N INDICATES A POSSIBLE DUPLICATE																				
USE	1969	09	07	04	42	17.2	19.685N	156.035W	004		3.50									
USE	1969	09	13	19	40	20.4M	19.333N	155.416W	031			4.30ML	FVO							
USE	1969	10	11	22	00	07.2	20.333N	155.050W	005		3.00									
USE	1969	10	14	22	55	31.9H	19.369N	155.367W	008			4.00ML	HVO							
USE	1969	10	23	13	26	30.0H	19.368N	155.384W	011			3.30ML	FVO							
USE	1969	11	05	15	21	24.6H	19.968N	155.351W	009			3.60ML	FVO							
USE	1969	11	10	05	12	12.2H	19.149N	155.501W	006			4.50ML	HVO							
USE	1969	11	11	07	25	25.7H	19.982N	155.350W	010			3.10ML	HVO							
USE	1969	11	23	00	00	44.0H	19.581N	155.083W	017			3.60ML	HVO							
USE	1969	11	23	23	34	16.0H	19.113N	155.516W	032			3.20ML	FVO							
USE	1969	11	24	19	12	22.9	19.685N	155.081W	035		4.50									
USE	1969	12	01	09	56	23.3H	19.980N	155.334W	009			3.50ML	HVO							
USE	1969	12	07	08	34	20.9H	19.333N	155.100W	010			3.10ML	FVO							
USE	1969	12	25	15	39	34.1H	19.500N	155.135W	025			3.20ML	FVO							
USE	1969	12	25	13	28	25.7H	19.301N	155.203W	032			3.30ML	FVO							
USE	1969	12	25	12	57	44.0	19.113N	155.516W	019			4.10ML	FVO							
USE	1969	12	27	10	00	52.7H	19.333N	155.460W	010			3.60ML	HVO							
FVO	1970	01	10	10	00	39.5	19.416N	155.435W	007			3.3 ML	FVO							
USE	1970	01	10	22	30	32.6H	19.333N	155.081W	011			3.30ML	FVO							
FVO	1970	01	13	15	00	29.4	19.333N	155.101W	007			3.2 ML	FVO							
FVO	1970	01	17	05	07	20.0	19.333N	155.117W	008			3.1 ML	HVC							
FVO	1970	01	27	09	09	10.1	19.301N	155.160W	009			3.6 ML	FVO							
USE	1970	01	27	19	10	09.1H	19.264N	155.145W	004			3.10ML	FVO							
FVO	1970	02	03	16	37	09.7	19.416N	155.163W	009			3.3 ML	FVO							
FVO	1970	02	03	07	07	19.2	19.333N	155.475W	011			3.4 ML	HVO							
FVO	1970	02	04	16	00	08.0	19.416N	155.170W	008			3.1 ML	FVO							
USE	1970	02	04	16	00	08.0H	19.333N	155.310W	020			3.10ML	FVO							
FVO	1970	02	05	10	30	58.0	19.333N	155.473W	004			3.4 ML	FVO							
USE	1970	02	05	10	30	58.0H	19.333N	155.467W	008			3.50ML	FVO							
FVO	1970	02	07	00	00	35.0	19.333N	155.052W	020			3.3 ML	HVO							
USE	1970	02	08	06	40	35.0H	19.367N	155.367W	027			3.40ML	FVO							
FVO	1970	02	08	16	00	41.0	19.416N	154.193W	002			3.4 ML	FVO							
FVO	1970	02	25	16	00	20.0	19.467N	155.194W	045			3.4 ML	FVO							
FVO	1970	03	02	14	30	17.2	19.500N	154.035W	041			3.9 ML	FVO							
FVO	1970	03	02	19	30	11.5	19.372N	155.274W	030			3.0 ML	FVO							
USE	1970	03	03	00	30	02.0	19.000N	155.551W	000		4.00									
FVO	1970	03	07	05	00	01.4	19.467N	154.860W	001			3.1 ML	FVO							
FVO	1970	03	15	00	00	41.0	19.372N	155.240W	008			4.0 ML	FVO							
USE	1970	03	16	00	00	31.7H	19.333N	155.516W	007			4.10ML	FVO							
USE	1970	03	19	10	00	20.0H	19.333N	155.052W	030			3.00ML	FVO							
FVO	1970	03	30	00	00	26.0	19.000N	155.257W	024			4.0 ML	FVO							
USE	1970	03	31	12	30	26.7H	19.000N	155.051W	020			4.30ML	FVO							
FVO	1970	03	31	20	30	12.0	19.333N	155.166W	008			3.7 ML	HVO							
USE	1970	04	01	00	30	13.5H	19.333N	155.150W	007			3.80ML	FVO							
FVO	1970	04	04	01	10	11.0	19.333N	155.155W	000			3.0 ML	HVO							
FVO	1970	04	12	09	15	43.0	19.400N	155.433W	010			4.2 ML	FVO							
USE	1970	04	12	19	15	43.7H	19.365N	155.417W	011			4.30ML	FVO							
FVO	1970	04	13	01	00	40.4	19.416N	155.423W	000			3.0 ML	HVO							
FVO	1970	04	14	11	00	07.0	19.400N	155.433W	021			3.5 ML	FVO							
FVO	1970	04	14	00	00	25.1	19.000N	155.167W	039			3.1 ML	FVO							

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LA	L'G	DEPT	-----MAGNITUDES-----			INT	PHENOM	RN	CE	Q/S	MAR	DG	DIST		
										(KM)	BODY	SURF									OTHER	LOCAL
**N INDICATES A POSSIBLE DUPLICATE																						
●	USE	1970	04	14	21	37	57.4N	19.451N	155.234W	024												61.0
	FVO	1970	04	15	24	28	31.9	23.033N	155.571W	011												71.0
	FVJ	1971	04	16	02	25	33.5	19.335N	155.246W	029												68.0
●	JSE	1971	04	16	12	25	33.5N	19.302N	155.250W	028												69.0
	FVJ	1971	04	17	12	12	13.6	19.558N	155.670W	009												10.0
●	USE	1971	04	17	22	12	13.6	19.518N	155.916W	010												7.0
	FVO	1971	04	19	30	33	38.8	19.273N	155.427W	027												52.0
●	JSE	1971	04	19	15	31	38.3N	19.251N	155.418W	026												54.0
	FVO	1971	04	24	27	08	15.0	20.241N	156.375W	017												101.0
	FVO	1971	04	26	02	26	17.0	19.417N	155.425W	009												48.0
	FVO	1971	04	26	15	23	02.0	19.401N	154.638W	002												131.0
●	JSE	1971	04	29	01	23	25.3N	19.435N	154.902W	002												103.0
	FVO	1971	04	31	05	32	14.1	14.335N	155.098W	008												84.0
	FVO	1971	04	30	16	17	11.1	14.378N	155.081W	011												85.0
●	JSE	1971	04	31	16	07	11.6N	19.367N	155.118W	011												81.0
	FVO	1971	04	31	21	12	51.7	19.227N	155.355W	037												58.0
	FVO	1971	05	11	04	11	57.8	19.051N	155.463W	004												65.0
●	JSE	1971	05	11	17	11	54.2	20.002N	155.383W	014												65.0
	USE	1971	05	12	18	47	33.7N	19.441N	155.154W	017												63.0
	FVO	1971	05	13	19	26	12.5	20.001N	155.49W	041												78.0
	FVO	1971	05	16	05	21	37.4	19.318N	155.204W	009												69.0
●	JSE	1971	05	16	18	21	38.7N	19.300N	155.250W	009												69.0
	FVO	1971	05	17	05	31	53.6	19.306N	155.351W	008												81.0
●	USE	1971	05	17	18	31	53.2N	19.369N	155.452W	009												81.0
	FVO	1971	05	13	15	12	57.4	19.418N	155.426W	008												48.0
●	JSE	1971	05	14	11	12	57.1N	19.384N	155.417W	009												53.0
	FVO	1971	05	14	11	12	21.7	19.401N	155.789W	010												20.0
	FVO	1971	05	15	03	13	15.1	19.441N	155.614W	001												8.0
	FVO	1971	05	15	05	55	57.8	19.382N	155.247W	009												67.0
	FVJ	1971	05	15	16	52	15.2	19.365N	155.741W	000												68.0
	FVO	1971	05	15	14	24	25.7	19.333N	155.629W	011												71.0
●	USE	1971	05	15	17	55	57.9N	19.388N	155.234W	004												69.0
	FVJ	1971	05	15	23	59	47.0	19.388N	155.346W	000												67.0
●	JSE	1971	05	16	09	59	44.3N	19.345N	155.234W	005												69.0
	FVO	1971	05	18	13	30	38.3	19.724N	154.743W	007												123.0
	FVO	1971	05	19	05	05	33.2	19.395N	155.452W	001												46.0
	FVO	1971	05	25	18	59	12.3	19.275N	155.612W	010												22.0
	FVO	1971	05	26	17	45	35.3	19.355N	155.157W	009												77.0
	FVJ	1971	05	28	02	31	25.3	19.417N	155.443W	010												46.0
	FVO	1971	05	30	13	17	41.4	19.817N	154.781W	131												137.0
	FVO	1971	06	06	05	31	46.5	19.420N	155.406W	012												50.0
	FVO	1971	06	10	23	03	50.6	19.217N	155.604W	010												40.0
	FVO	1971	06	11	11	22	22.5	19.390N	155.284W	030												63.0
●	USE	1971	06	11	21	22	22.4N	19.369N	155.369W	031												65.0
	FVO	1971	06	15	16	31	51.6	19.341N	155.122W	001												81.0
	FVO	1971	06	17	14	57	32.2	19.335N	155.412W	009												51.0
	FVO	1971	06	17	21	34	47.3	19.505N	155.779W	009												12.0
●	JSE	1971	06	18	11	57	51.4N	19.316N	155.401W	009												53.0
	FVO	1971	06	14	14	44	27.1	20.038N	154.953W	007												116.0
	FVO	1971	06	20	06	04	11.4	19.364N	155.070W	013												15.0

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT PHENOM MAX DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
*** INDICATES A POSSIBLE DUPLICATE																				
HVO	1970	06	22	12	36	42.0	19.347N	155.462W	039											
HVO	1970	07	15	21	40	12.9	19.377N	155.063W	008											
HVO	1970	07	15	21	52	32.8	19.418N	155.072W	010											
USE	1970	07	11	07	40	12.5H	19.349N	155.066W	006											
HVO	1970	07	11	12	38	21.5	19.392N	155.277W	031											
HVO	1970	07	15	16	12	20.3	19.346N	155.126W	059											
● USE	1970	07	16	02	12	19.6H	19.317N	155.161W	056											
FVO	1970	07	22	16	15	58.5	20.144N	155.435W	038											
● USE	1970	07	23	02	15	51.1H	19.914N	155.400W	011											
HVO	1970	08	03	12	02	55.5	20.058N	156.035W	018											
HVO	1970	08	07	10	23	07.7	20.036N	155.333W	038											
HVO	1970	08	07	17	46	35.9	20.070N	155.328W	058											
● USE	1970	08	07	20	23	01.0H	19.800N	155.367W	000											
FVO	1970	08	16	07	41	54.2	19.407N	154.788W	041											
● USE	1970	08	16	17	41	53.1H	19.415N	154.785W	051											
HVO	1970	08	17	03	24	00.6	19.303N	155.072W	032											
● USE	1970	08	18	09	06	01.5H	19.318N	155.066W	032											
FVO	1970	08	18	17	00	22.8	19.815N	155.334W	019											
FVO	1970	08	18	18	05	16.4	19.744N	156.065W	012											
HVO	1970	08	07	17	04	53.1	19.117N	155.469W	044											
HVO	1970	08	18	11	51	27.5	19.870N	156.426W	035											
FVO	1970	08	14	11	48	03.0	19.670N	156.679W	007											
FVO	1970	09	17	20	02	07.2	19.401N	155.447W	011											
FVO	1970	09	02	10	20	17.7	19.877N	156.014W	027											
FVO	1970	09	21	11	35	36.2	19.344N	155.201W	013											
● USE	1970	09	21	11	34	34.1H	19.333N	155.200W	010											
FVO	1970	09	21	02	35	04.7	19.071N	155.083W	009											
HVO	1970	09	28	01	00	14.3	19.745N	156.065W	011											
FVO	1970	09	26	14	37	17.5	19.433N	155.463W	010											
● USE	1970	09	27	00	37	17.7H	19.416N	155.460W	010											
● USE	1970	10	02	06	17	51.0H	19.352N	155.314W	032											
FVO	1970	10	08	15	13	05.0	19.345N	155.135W	007											
● USE	1970	10	08	16	13	04.5H	19.357N	155.117W	004											
FVO	1970	10	13	14	40	01.1	19.514N	155.246W	024											
● USE	1970	10	13	14	40	01.0H	19.454N	155.235W	027											
FVO	1970	10	14	01	32	42.7	19.400N	155.547W	012											
HVO	1970	10	17	15	05	46.8	19.396N	155.057W	013											
FVO	1970	10	25	00	00	03.0	19.135N	155.047W	005											
● USE	1970	10	25	00	00	02.4H	19.310N	155.034W	036											
FVO	1970	10	29	07	47	07.6	19.058N	156.417W	017											
● USE	1970	10	29	17	47	07.6H	19.517N	156.433W	010											
HVO	1970	10	30	15	30	09.2	19.304N	155.100W	009											
● USE	1970	10	31	14	50	07.4H	19.069N	155.083W	005											
FVO	1970	11	07	22	41	01.8	19.703N	156.102W	031											
HVO	1970	11	11	17	12	41.6	19.214N	155.345W	036											
● USE	1970	11	12	03	12	41.4H	19.211N	155.334W	037											
FVO	1970	11	12	19	46	15.1	19.943N	155.792W	008											
FVO	1970	11	12	19	57	07.9	19.904N	155.772W	008											
FVO	1970	11	12	21	36	00.3	20.114N	155.011W	021											
● USE	1970	11	13	05	45	15.8	20.044N	155.034W	020											

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT MA	PHENOM DTSVNO	RN	CE	G/S	MAR	DG	DIST (KM)
										BODY	SURF	OTFR	LOCAL								
*** INDICATES A POSSIBLE DUPLICATE																					
HVO	1970	11	16	04	02	52.1	19.346N	155.119W	00P												
HVO	1970	11	16	04	23	52.2	19.788N	156.365W	00R												
●	JSE	1970	11	16	14	02	51.6P	19.333N	155.101W	00S											
HVO	1970	11	16	06	07	58.8	19.585N	155.765W	001												
●	JSE	1970	11	16	16	07	57.8	19.867N	155.766W	000											
HVO	1970	11	25	10	02	13.2	19.115N	156.099W	004												
HVO	1970	12	04	16	45	32.0	19.237N	155.364W	009												
HVO	1970	12	04	21	51	41.7	19.226N	155.352W	001												
●	JSE	1970	12	05	02	45	31.1P	19.202N	155.352W	002											
HVO	1970	12	05	16	34	31.5	19.115N	155.710W	012												
HVO	1970	12	05	17	59	45.2	19.401N	155.625W	011												
●	JSE	1970	12	06	03	58	45.1P	19.403N	155.616W	012											
HVO	1970	12	10	20	28	16.0	19.489N	155.376W	000												
●	JSE	1970	12	11	05	26	05.9P	19.394N	155.366W	009											
HVO	1970	12	13	08	00	26.9	19.409N	156.041W	005												
●	JSE	1970	12	13	18	02	26.9	19.604N	156.030W	017											
HVO	1970	12	17	11	02	41.5	19.483N	155.451W	013												
HVO	1970	12	20	17	00	27.2	19.245N	155.507W	033												
HVO	1970	12	21	12	17	30.7	19.203N	155.623W	009												
JSE	1970	12	21	08	44	16.8	20.000N	155.000W	011												
HVO	1970	12	21	14	00	20.7	19.346N	155.102W	007												
JSE	1970	12	26	11	41	11.1P	19.473N	155.001W	005												
HVO	1970	12	27	15	01	29.2	20.000N	155.000W	000												
HVO	1971	01	01	01	03	35.2	20.000N	156.000W	001												
HVO	1971	01	02	04	11	18.3	19.016N	156.009W	007												
HVO	1971	01	13	10	36	41.7	20.000N	156.000W	005												
HVO	1971	01	14	07	26	45.3	19.757N	156.461W	009												
HVO	1971	01	15	00	00	48.3	19.589N	157.000W	017												
HVO	1971	01	15	18	11	15.7	20.000N	155.000W	000												
HVO	1971	01	19	01	47	46.1	20.000N	155.000W	010												
HVO	1971	01	21	07	26	21.6	19.447N	156.029W	029												
HVO	1971	01	23	03	47	55.7	19.100N	155.701W	001												
HVO	1971	01	24	02	12	37.0	19.346N	155.705W	000												
HVO	1971	01	26	18	07	36.9	19.689N	155.000W	010												
HVO	1971	02	01	13	43	44.3	19.016N	156.009W	009												
HVO	1971	02	03	01	06	25.3	19.371N	155.024W	000												
HVO	1971	02	06	17	00	24.2	19.545N	155.169W	026												
HVO	1971	02	08	01	04	30.7	19.346N	155.125W	009												
HVO	1971	02	13	04	00	25.9	19.346N	155.770W	010												
HVO	1971	02	13	09	47	34.0	19.400N	155.401W	017												
HVO	1971	02	15	16	00	53.5	19.394N	155.403W	010												
HVO	1971	02	16	21	03	27.3	19.100N	155.634W	011												
HVO	1971	02	18	04	34	24.5	19.200N	155.501W	010												
HVO	1971	02	19	16	00	41.5	19.400N	155.000W	027												
HVO	1971	02	19	21	04	04.0	19.000N	155.000W	029												
HVO	1971	02	26	06	03	10.5	20.000N	156.000W	013												
HVO	1971	02	27	09	00	50.7	19.304N	155.017W	033												
HVO	1971	03	08	14	23	32.1	19.000N	155.000W	007												
HVO	1971	03	16	20	01	32.1	19.465N	155.000W	012												
HVO	1971	03	27	23	04	51.9	19.701N	156.000W	009												

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT PHENOM MA> DTSVNO	RN	CE	G/S	MAR	DG	DIST (KM)
										BODY	SURF	OT-HER	LOCAL							
**N INDICATES A POSSIBLE DUPLICATE																				
HVO	1971	03	28	17	32	57.4	19.338N	155.175W	010											
HVO	1971	03	30	34	37	34.9	20.108N	156.625W	037											
NJS	1971	03	31	11	08	56.0F	20.300N	156.217W	010											
HVO	1971	04	05	05	52	05.1	19.392N	155.155W	037											
HVO	1971	04	10	05	14	39.9	19.340N	155.136W	010											
HVO	1971	04	14	10	02	32.0	19.154N	155.618W	009											
HVO	1971	04	17	01	09	31.9	18.863N	155.116W	036											
HVO	1971	04	21	00	06	23.0	19.119N	155.456W	006											
HVO	1971	04	25	08	03	01.4	19.346N	155.267W	013											
HVO	1971	04	25	23	56	12.5	19.399N	155.291W	029											
NJS	1971	04	26	09	56	12.8H	19.342N	155.293W	025	4.40MB										
HVO	1971	04	27	18	06	18.1	19.693N	156.223W	027											
HVO	1971	05	02	19	16	09.7	20.040N	156.324W	062											
HVO	1971	05	06	21	05	05.3	19.929N	155.337W	009											
HVO	1971	05	08	03	11	54.8	19.311N	155.249W	031											
HVO	1971	05	10	07	05	06.7	19.811N	155.156W	037											
HVO	1971	05	13	01	27	05.9	19.948N	156.133W	046											
NJS	1971	05	14	16	03	05.0	19.900N	156.067W	017	3.70MB										
HVO	1971	05	17	19	05	44.5	19.432N	155.464W	005											
HVO	1971	05	26	12	04	10.8	19.836N	155.205W	047											
HVO	1971	05	27	07	14	1.5	19.323N	156.517W	031											
HVO	1971	06	09	05	32	24.1	18.977N	155.195W	047											
HVO	1971	06	16	18	23	37.7	19.841N	156.513W	008											
HVO	1971	06	18	16	54	54.7	19.725N	156.115W	009											
HVO	1971	06	19	22	34	23.1	19.341N	155.116W	009											
HVO	1971	06	23	02	10	07.0	19.340N	155.430W	011											
HVO	1971	06	28	12	12	47.4	20.107N	155.076W	030											
HVO	1971	06	28	16	49	24.5	19.311N	155.919W	010											
HVO	1971	06	28	02	10	04.5	19.406N	155.403W	004											
HVO	1971	06	28	02	57	01.1	20.076N	156.914W	011											
HVO	1971	07	03	20	03	11.6	19.242N	155.012W	015											
HVO	1971	07	03	09	16	15.6	19.422N	155.354W	011											
HVO	1971	07	03	12	15	47.4	19.645N	156.149W	011											
HVO	1971	07	04	14	45	13.3	19.376N	155.283W	002											
HVO	1971	07	05	00	19	44.5	19.312N	155.221W	010											
HVO	1971	07	07	21	15	44.9	19.654N	156.164W	017											
HVO	1971	07	11	19	43	22.8	19.155N	155.679W	009											
HVO	1971	07	20	11	01	34.2	19.643N	156.134W	016											
HVO	1971	07	24	17	15	31.7	20.198N	155.856W	031											
HVO	1971	07	26	15	10	05.5	19.441N	155.427W	017											
HVO	1971	07	28	22	15	39.7	19.356N	155.163W	009											
HVO	1971	07	29	17	17	25.2	20.107N	155.782W	023											
HVO	1971	07	31	11	57	57.9	19.364N	155.254W	013											
HVO	1971	08	01	01	38	23.3	19.614N	155.860W	009											
HVO	1971	08	02	14	17	56.0	20.440N	155.976W	010											
HVO	1971	08	03	14	09	15.0	19.119N	155.221W	010											
HVO	1971	08	04	01	36	43.0	20.143N	155.787W	025											
ERL	1971	08	04	11	36	45.0F	20.110N	155.980W	010											
HVO	1971	08	10	01	12	25.8	19.340N	155.172W	003											
HVO	1971	08	11	21	00	41.5	19.335N	155.455W	071											

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT PHENOM MAX DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
**N INDICATES																				
A POSSIBLE DUPLICATE																				
HVO	1971	08	15	15	36	06.7	19.362N	155.267W	035.											
HVO	1971	08	15	22	18	37.3	19.314N	155.218W	010											
HVO	1971	08	16	11	35	28.5	19.367N	155.263W	035.	4.50MB										
HVO	1971	08	25	13	15	24.2	19.791N	155.959W	043											
HVO	1971	08	28	05	03	43.4	20.286N	155.373W	107											
HVO	1971	09	07	19	56	07.5	19.317N	155.221W	010											
HVO	1971	09	10	20	53	46.0	19.933N	156.437W	001											
HVO	1971	09	19	17	00	46.3	19.234N	155.576W	039											
HVO	1971	09	22	11	46	31.3	18.795N	155.314W	013											
HVO	1971	09	24	23	53	33.1	19.345N	155.289W	009											
HVO	1971	09	25	13	39	31.5	19.425N	155.419W	008											
HVO	1971	09	26	22	41	59.4	19.391N	155.426W	010											
HVO	1971	09	26	02	56	49.2	19.390N	155.403W	005											
HVO	1971	09	28	02	24	08.6	19.202N	155.358W	008											
HVO	1971	09	28	14	00	54.1	19.391N	155.411W	008											
HVO	1971	09	30	01	28	30.0	19.248N	155.348W	005											
HVO	1971	10	02	20	07	35.9	19.378N	155.420W	014											
HVO	1971	10	04	04	43	21.4	19.140N	155.743W	028											
HVO	1971	10	11	23	04	19.6	19.835N	155.289W	011											
HVO	1971	10	12	11	48	53.7	19.854N	155.250W	019											
HVO	1971	10	17	08	49	37.5	19.917N	155.277W	014											
HVO	1971	10	18	04	33	04.4	20.677N	155.165W	007											
HVO	1971	10	14	12	27	11.4	19.538N	155.113W	009											
HVO	1971	10	15	18	18	01.2	19.814N	155.268W	014											
HVO	1971	10	25	18	08	01.4	20.138N	155.362W	008											
HVO	1971	10	25	23	42	54.3	20.141N	155.734W	011											
HVO	1971	10	25	20	41	17.3	19.143N	155.673W	009											
HVO	1971	10	27	05	4	11.7	19.313N	155.225W	011											
HVO	1971	10	28	14	47	11.2	19.152N	155.731W	024											
HVO	1971	10	27	07	55	19.7	19.581N	155.692W	001											
HVO	1971	10	28	12	17	58.9	19.141N	155.110W	009											
HVO	1971	10	29	02	13	01.5	19.383N	155.423W	011											
HVO	1971	10	29	12	15	57.2	19.500N	155.113W	008											
HVO	1971	10	14	03	05	33.1	19.384N	155.393W	009											
HVO	1971	10	15	03	05	39.6	19.449N	155.219W	034											
HVO	1971	10	15	04	42	34.7	19.410N	155.478W	009											
HVO	1971	10	15	12	57	24.7	18.785N	155.272W	012											
HVO	1971	10	14	09	13	38.9	18.810N	155.244W	009											
HVO	1971	10	18	04	17	41.8	18.144N	155.323W	010											
HVO	1971	10	17	17	13	30.8	18.771N	155.310W	009											
HVO	1971	10	19	11	01	34.4	18.787N	155.363W	025											
HVO	1971	10	20	01	18	23.4	18.737N	155.391W	011											
HVO	1971	10	20	01	43	15.0	19.828N	155.307W	007											
HVO	1971	10	20	01	49	11.6	18.741N	155.317W	046											
HVO	1971	10	20	01	54	33.5	18.915N	155.490W	013											
HVO	1971	10	20	04	12	54.3	18.902N	155.322W	012											
HVO	1971	10	20	05	43	06.4	18.793N	155.266W	018											
HVO	1971	10	20	09	43	17.9	18.592N	155.321W	043											
HVO	1971	10	20	22	10	49.4	18.162N	155.121W	012											
HVO	1971	10	21	09	27	49.5	18.874N	155.325W	013											

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES			INT PHENOM MA) DTSVNO	RN	CE	G/S	MAR DG	DIST (KM)	
										BODY	SURF	OTHR	LOCAL						
*** INDICATES A POSSIBLE DUPLICATE																			
HVO	1971	12	21	09	34	00.2	18.864N	155.309W	009										
HVO	1971	12	21	09	51	31.9	18.831N	155.319W	013										
FVO	1971	12	21	10	43	50.5	18.841N	155.305W	012										
HVO	1971	12	21	14	17	22.7	18.810N	155.317W	010										
HVO	1971	12	22	14	40	56.1	18.674N	155.256W	041										
HVO	1971	12	23	14	05	34.5	18.666N	155.271W	029										
HVO	1971	12	23	20	29	16.5	19.280N	155.338W	007										
HVO	1971	12	23	22	02	16.7	18.848N	155.325W	013										
HVO	1971	12	24	08	00	56.5	18.772N	155.285W	011										
HVO	1971	12	24	08	39	37.1	18.805N	155.296W	009										
HVO	1971	12	24	16	11	13.1	19.191N	155.360W	009										
HVO	1971	12	24	17	39	12.5	19.197N	155.357W	008										
FVO	1971	12	24	19	54	44.4	19.190N	155.351W	007										
HVO	1971	12	24	20	47	23.9	19.188N	155.326W	009										
HVO	1971	12	25	10	34	13.4	19.137N	155.350W	010										
HVO	1971	12	26	01	14	01.7	19.244N	155.364W	009										
FVO	1971	12	26	02	57	30.5	19.234N	155.369W	004										
HVO	1971	12	26	11	04	07.8	19.202N	155.359W	007										
HVO	1971	12	26	12	25	11.7	19.209N	155.357W	010										
HVO	1971	12	26	16	17	46.3	19.244N	155.360W	008										
HVO	1971	12	26	16	24	40.4	19.211N	155.343W	007										
HVO	1971	12	26	16	37	35.4	19.275N	155.339W	009										
FVO	1971	12	26	16	34	55.9	19.241N	155.361W	006										
HVO	1971	12	26	21	31	21.4	19.254N	155.354W	008										
HVO	1971	12	26	21	46	40.2	19.236N	155.349W	009										
HVO	1971	12	26	22	31	44.9	19.218N	155.357W	006										
HVO	1971	12	26	23	35	43.6	19.274N	155.339W	010										
HVO	1971	12	27	07	00	36.8	19.219N	155.356W	008										
HVO	1971	12	27	10	05	47.5	19.248N	155.376W	006										
HVO	1971	12	27	10	11	52.3	19.217N	155.370W	001										
HVO	1971	12	27	16	13	10.6	19.252N	155.364W	002										
HVO	1971	12	27	17	01	54.6	19.217N	155.373W	001										
HVO	1971	12	27	18	07	51.7	18.846N	155.331W	010										
HVO	1971	12	27	19	03	51.4	19.276N	155.361W	009										
HVO	1971	12	27	19	01	55.6	19.259N	155.341W	011										
HVO	1971	12	28	16	00	08.6	19.240N	155.364W	006										
HVO	1971	12	28	16	59	11.7	19.278N	155.373W	006										
HVO	1971	12	28	17	09	20.9	19.212N	155.364W	006										
HVO	1971	12	29	01	42	10.9	19.212N	155.378W	009										
HVO	1971	12	29	01	39	43.8	19.246N	155.359W	006										
HVO	1971	12	29	01	46	25.3	19.238N	155.366W	009										
HVO	1971	12	29	04	01	04.2	19.234N	155.355W	002										
HVO	1971	12	29	06	17	04.4	19.230N	155.361W	009										
HVO	1971	12	29	11	23	17.6	19.237N	155.346W	012										
HVO	1971	12	30	22	32	22.1	18.843N	155.344W	011										
HVO	1972	01	05	08	00	24.7	18.935N	155.395W	036										
HVO	1972	01	10	14	47	34.3	19.005N	155.297W	009										
HVO	1972	01	13	06	44	05.3	18.846N	155.317W	009										
HVO	1972	01	13	13	59	31.9	18.844N	155.313W	011										
HVO	1972	01	13	20	07	51.8	18.808N	155.297W	009										

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT PHENOM MAX DTSVHO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
*** INDICATES A POSSIBLE DUPLICATE																				
HVO	1972	01	18	16	33	43.5	19.468N	155.464W	009											
HVO	1972	01	19	18	11	03.9	18.901N	155.127W	051											
HVO	1972	01	19	20	37	23.7	19.812N	155.283W	012											
HVO	1972	01	20	11	42	41.9	18.767N	155.293W	012											
HVO	1972	01	20	12	14	59.2	18.791N	155.256W	007											
HVO	1972	01	20	13	35	32.8	18.847N	155.306W	023											
HVO	1972	01	21	09	26	21.7	18.926N	155.298W	013											
HVO	1972	01	22	12	40	19.3	19.240N	155.393W	009											
HVO	1972	01	22	15	46	20.4	18.783N	155.359W	007											
HVO	1972	01	23	07	05	45.6	20.302N	155.930W	048											
HVO	1972	01	23	19	23	17.8	18.645N	155.289W	013											
HVO	1972	01	27	05	21	40.7	18.791N	155.257W	007											
HVO	1972	01	29	02	14	49.7	19.821N	155.293W	011											
HVO	1972	01	30	05	01	48.3	19.779N	155.123W	026											
HVO	1972	02	02	05	53	30.9	19.217N	155.643W	012											
HVO	1972	02	04	08	05	31.4	19.398N	155.492W	010											
HVO	1972	02	06	11	14	47.4	18.887N	155.336W	013											
HVO	1972	02	07	13	17	50.6	19.392N	155.403W	010											
HVO	1972	02	08	04	25	47.7	18.426N	155.340W	018											
HVO	1972	02	08	09	52	20.7	20.137N	155.799W	028											
HVO	1972	02	08	11	47	43.8	18.364N	155.430W	009											
HVO	1972	02	08	09	16	15.0	19.504N	156.469W	010											
HVO	1972	02	21	01	05	51.3	19.807N	155.273W	009											
HVO	1972	02	24	02	43	37.0	19.860N	155.733W	034											
HVO	1972	02	28	10	19	09.1	18.759N	155.320W	013											
HVO	1972	02	28	02	47	07.6	19.267N	155.523W	009											
HVO	1972	02	29	12	00	21.9	19.394N	156.525W	011											
HVO	1972	02	29	12	55	50.1	19.393N	156.403W	040											
HVO	1972	02	29	22	00	21.9H	19.263N	156.533W	015											
HVO	1972	03	01	03	30	19.2	19.362N	156.411W	033											
HVO	1972	03	03	02	32	53.1	19.245N	156.287W	042											
HVO	1972	03	03	08	09	02.7	18.799N	155.347W	013											
HVO	1972	03	04	00	07	08.4	19.776N	155.354W	026											
HVO	1972	03	06	07	11	06.8	18.752N	155.396W	007											
HVO	1972	03	09	03	11	52.3	18.832N	155.316W	013											
HVO	1972	03	10	03	13	03.3	19.339N	155.731W	000											
HVO	1972	03	11	10	00	01.2	20.173N	155.890W	041											
HVO	1972	03	11	14	00	26.3	19.343N	155.190W	009											
HVO	1972	03	15	02	00	01.4	18.890N	155.301W	010											
HVO	1972	03	15	14	00	01.2	18.939N	155.514W	020											
HVO	1972	03	31	15	20	34.9	19.350N	155.175W	007											
HVO	1972	03	31	15	53	08.9	19.365N	155.158W	009											
HVO	1972	04	05	01	03	43.2	19.314N	155.227W	033											
HVO	1972	04	08	08	00	16.3	19.316N	155.091W	033											
HVO	1972	04	09	11	29	17.7	19.317N	155.264W	033											
HVO	1972	04	11	23	08	55.8	18.756N	155.354W	020											
HVO	1972	04	14	11	08	42.9	18.902N	155.324W	029											
HVO	1972	04	15	11	47	02.5	18.892N	155.394W	010											
HVO	1972	04	15	12	10	20.8	19.333N	155.128W	009											
HVO	1972	04	17	20	16	20.3	18.977N	155.326W	010											

11/07/17.

SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT	FENOM	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHR	LOCAL								
**N INDICATES A POSSIBLE DUPLICATE																					
HVJ	1972	04	19	10	16	40.0	18.980N	155.643W	042.0				4.0	ML	HVO						60.
FVO	1972	04	21	11	20	59.5	18.842N	155.319W	010				3.0	ML	HVO						66.
FVO	1972	04	26	07	10	15.8	18.905N	155.310W	010				3.0	ML	FVO						66.
FVO	1972	04	29	19	39	53.7	18.922N	155.318W	018				3.0	ML	FVO						65.
HVO	1972	05	02	37	39	54.2	19.486N	155.247W	031				3.0	ML	HVO						67.
HVO	1972	05	14	06	20	06.0	20.077N	157.054W	051				3.3	ML	FVO						141.
FVO	1972	05	15	04	05	35.7	19.527N	155.272W	027				3.2	ML	HVO	E					64.
FVO	1972	05	18	22	27	14.0	19.357N	155.051W	006				3.0	ML	FVO						67.
HVO	1972	05	27	12	36	11.4	18.974N	155.305W	012				3.5	ML	FVO						77.
HVO	1972	05	30	19	22	10.2	19.221N	156.524W	046				3.2	ML	HVO						73.
HVO	1972	06	11	10	34	02.3	19.365N	155.126W	009				3.1	ML	FVO	E					80.
FVO	1972	06	21	11	38	20.6	19.347N	155.029W	009				3.6	ML	HVO						90.
FVO	1972	06	24	09	03	50.1	19.467N	155.311W	006				3.0	ML	FVO	E					53.
FVO	1972	06	25	06	19	59.8	19.378N	155.441W	009				3.2	ML	FVO	E					47.
HVO	1972	06	28	12	18	17.4	19.044N	155.380W	030				3.0	ML	HVO						71.
HVO	1972	07	03	02	08	16.2	19.037N	155.310W	055				3.0	ML	FVO						100.
FVO	1972	07	12	07	51	49.1	19.174N	155.417W	010				3.3	ML	HVO	E					50.
FVO	1972	07	14	10	56	07.5	19.308N	155.301W	036.				4.4	ML	FVO						76.
FVO	1972	07	14	18	50	31.7	18.073N	154.800W	047				3.3	ML	HVO						126.
FVO	1972	07	14	02	57	03.6	19.300N	155.344W	034				3.4	ML	HVO						51.
FVO	1972	07	17	20	17	03.3	18.304N	155.013W	010				3.2	ML	FVO						67.
FVO	1972	07	17	22	11	17.3	18.437N	155.216W	007				3.3	ML	FVO						69.
FVO	1972	07	18	09	17	07.6	18.931N	155.331W	011				3.1	ML	HVO						63.
FVO	1972	07	18	05	03	36.9	18.266N	155.370W	021				3.0	ML	HVO						90.
FVO	1972	07	18	07	07	55.1	18.944N	155.332W	018				3.2	ML	FVO						65.
FVO	1972	07	18	09	14	10.1	18.810N	155.315W	009				3.1	ML	FVO						65.
FVO	1972	07	20	17	39	01.3	19.450N	155.045W	031				3.1	ML	FVO	E					67.
FVO	1972	07	25	23	30	33.3	19.244N	155.430W	030				3.0	ML	HVO						67.
FVO	1972	07	29	17	01	33.5	20.270N	155.452W	037				3.1	ML	HVO						89.
FVO	1972	07	30	00	46	59.9	19.306N	155.183W	010				3.0	ML	FVO						15.
FVO	1972	08	03	17	49	16.4	19.130N	155.406W	033				3.0	ML	FVO	E					53.
FVO	1972	08	05	02	18	07.1	19.240N	155.393W	019				3.2	ML	FVO						74.
FVO	1972	08	09	17	11	13.9	19.484N	155.696W	009				3.0	ML	FVO	E					20.
FVO	1972	08	05	11	51	03.6	19.315N	155.016W	010				5.1	ML	FVO	E					72.
FVO	1972	08	15	11	51	33.4	19.333N	155.210W	010	4.4	0MB		4.5	ML	FVO						73.
FVO	1972	08	15	23	01	06.2	19.344N	155.113W	009				4.1	ML	FVO	E					62.
FVO	1972	08	16	03	02	13.9	18.944N	155.088W	014				3.1	ML	HVO						65.
FVO	1972	08	16	24	12	31.8	18.700N	155.317W	013				3.4	ML	FVO						66.
FVO	1972	08	18	09	41	09.0	19.307N	155.117W	010	3.7	0MB		4.0	ML	FVO		F				61.
FVO	1972	08	17	01	45	05.0	18.947N	155.073W	010				3.1	ML	FVO						67.
FVO	1972	08	17	04	37	00.5	18.230N	155.316W	011				3.0	ML	HVO						62.
FVO	1972	08	17	05	59	13.0	19.044N	155.316W	012				3.0	ML	HVO						91.
FVO	1972	08	17	11	01	05.2	18.183N	155.415W	033				3.2	ML	HVO						79.
FVO	1972	08	19	22	59	03.1	18.916N	155.314W	012				3.0	ML	FVO						68.
FVO	1972	08	19	22	42	32.4	19.181N	155.556W	010				3.3	ML	FVO	E					44.
FVO	1972	08	13	13	41	01.1	19.412N	155.436W	011				3.0	ML	HVO	E					47.
FVO	1972	08	16	20	03	10.6	19.744N	156.015W	006				3.1	ML	FVO						30.
FVO	1972	08	13	15	50	26.2	19.411N	155.440W	009				3.4	ML	FVO	E					47.
FVO	1972	08	26	16	10	20.3	19.485N	155.438W	009				3.0	ML	FVO						11.
FVO	1972	10	10	05	21	27.9	20.046N	155.357W	009				3.2	ML	HVO						64.

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LCNG	DEPTH (KM)	MAGNITUDES				INT MAX	PHENOM DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL								
**N INDICATES A POSSIBLE DUPLICATE																					
FVO	1972	10	27	04	37	24.0	19.350N	155.113W	009												
FVO	1972	11	02	17	25	32.6	19.562N	156.465W	012												
FVO	1972	11	04	11	52	01.7	19.702N	156.103W	041												
**1 FVO	1972	11	17	09	28	34.2	19.345N	155.121W	009												
**2 FVO	1972	11	17	09	29	34.0	19.338N	155.118W	008												
FVO	1972	11	18	05	53	35.0	19.205N	155.609W	009												
FVO	1972	11	19	17	47	31.0	19.192N	155.701W	008						E	613			052	95	41.
FVO	1972	11	19	17	39	53.2	19.281N	155.025W	041						E	613			052	95	36.
FVO	1972	11	19	18	05	02.0	19.388N	155.676W	010						E	613			052	95	52.
FVO	1972	11	23	09	04	51.8	19.443N	155.393W	010						E	613			052	95	51.
FVO	1972	12	01	13	59	11.1	20.023N	155.585W	008							613			08P	05	69.
FVO	1972	12	04	14	55	11.3	19.355N	155.375W	034						E	613			052	95	65.
FVO	1972	12	07	13	25	25.5	19.445N	155.462W	039						E	613			052	95	44.
FVO	1972	12	18	04	34	57.3	19.199N	155.613W	019						E	613			052	95	41.
FVO	1972	12	11	02	29	16.0	19.701N	156.069W	052							613			052	94	100.
FVO	1972	12	20	17	32	59.8	19.171N	155.701W	009						E	613			052	95	26.
FVO	1972	12	21	21	15	49.5	20.108N	155.819W	029							613			08E	05	72.
FVO	1972	12	21	02	42	33.5	19.475N	155.952W	010							613			052	95	7.
FVO	1972	12	23	09	04	51.6	19.611N	156.066W	037							613			052	95	17.
FVO	1972	12	23	08	11	59.4	19.605N	156.070W	050							613			052	96	22.
● ERL	1972	12	23	09	04	50.9	19.617N	156.063W	045		● 4.9CMB					613	F	(4C	052	95	17.
● ERL	1972	12	23	09	04	50.10	19.617N	156.063W	045							613		008	052	96	17.
FVO	1972	12	24	10	45	05.8	19.591N	155.967W	039							613			052	95	17.
FVO	1972	12	25	22	04	12.0	19.813N	155.971W	039							613			052	95	18.
FVO	1973	01	02	27	27	11.1	19.118N	155.574W	008						E	613			052	95	45.
FVO	1973	01	03	16	07	00.3	19.302N	156.316W	035							613			052	96	40.
FVO	1973	01	04	13	22	41.2	20.399N	155.891W	039							613			08E	05	103.
FVO	1973	01	16	17	51	57.5	19.605N	156.141W	045							613			052	96	26.
FVO	1973	01	13	11	31	00.0	19.319N	155.700W	009						E	613			052	95	18.
FVO	1973	01	14	04	31	49.7	19.983N	155.560W	009							613			052	95	67.
FVO	1973	01	14	06	49	15.9	19.987N	155.555W	009							613			052	95	67.
FVO	1973	01	19	09	49	56.3	19.379N	155.414W	009						E	613			052	95	50.
FVO	1973	01	22	13	10	03.8	19.906N	155.629W	010							613			052	95	58.
FVO	1973	01	22	13	47	44.5	19.927N	155.626W	010						E	613			052	95	58.
FVO	1973	01	24	18	33	16.5	19.174N	155.690W	008						E	613			052	95	34.
FVO	1973	02	11	01	26	44.5	20.014N	155.343W	008							613			08E	05	82.
FVO	1973	02	12	18	23	33.5	19.493N	155.772W	019							613			052	95	12.
FVO	1973	02	09	11	18	47.5	19.879N	155.463W	008						E	613			052	95	49.
FVO	1973	02	12	19	46	55.1	19.350N	155.342W	031							613			052	95	54.
FVO	1973	02	13	01	21	09.2	20.129N	155.862W	060							613			08E	05	96.
FVO	1973	02	17	19	49	47.9	19.514N	155.503W	009							613			052	95	10.
FVO	1973	02	19	10	11	05.4	19.301N	155.029W	010						E	613			052	95	70.
FVO	1973	02	19	16	26	11.7	19.637N	155.796W	011						E	613			052	95	21.
FVO	1973	02	22	22	16	10.9	19.567N	156.435W	011							613			052	96	59.
FVO	1973	02	23	07	47	52.2	19.356N	155.395W	026							613			052	95	58.
FVO	1973	02	25	13	44	07.5	20.011N	155.395W	019							613			08E	05	79.
FVO	1973	02	26	10	30	22.2	20.176N	156.065W	020							613			08E	06	81.
FVO	1973	03	06	18	49	45.9	19.471N	155.450W	010						E	613			052	95	45.
FVO	1973	03	07	26	51	45.7	19.310N	155.221W	010						E	613			052	95	71.
FVO	1973	03	07	17	52	43.6	19.315N	155.022W	010						E	613			052	95	71.

11/07/77.

SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LCNG	DEPT	-----MAGNITUDES-----				INT	FFENOM	RN	CE	Q/S	MAR	DG	DIST
										(KM)	BODY	SURF	OTHR								
**V INDICATES A POSSIBLE DUPLICATE																					
HVO	1973	03	08	17	54	00.6	19.395N	155.109W	009												
HVO	1973	03	11	13	49	15.1	19.517N	156.352W	013												
HVO	1973	03	13	17	36	56.2	20.134N	155.629W	025												
HVO	1973	03	14	19	29	01.5	19.395N	155.801W	011												
HVO	1973	03	15	14	51	44.9	19.537N	155.521W	046												
HVO	1973	03	15	22	16	17.1	19.046N	156.266W	061												
HVO	1973	03	23	14	39	08.2	19.414N	155.416W	009												
HVO	1973	03	26	09	56	45.5	19.753N	155.756W	012												
HVO	1973	04	02	18	12	53.5	19.319N	155.786W	010												
HVO	1973	04	09	04	41	47.1	19.388N	155.406W	011												
HVO	1973	04	15	00	59	38.9	19.331N	155.123W	009												
HVO	1973	04	16	14	29	57.8	19.343N	155.106W	008												
HVO	1973	04	18	13	41	44.3	19.193N	156.164W	066												
HVO	1973	04	19	12	51	05.9	19.335N	155.138W	008												
ERL	1973	04	23	07	07	53.7H	19.957N	154.667W	030	.4.20MR											
HVO	1973	04	24	06	16	23.1	19.894N	155.886W	012												
ERL	1973	04	24	15	16	21.8H	19.917N	155.733W	040	.4.20CHL											
HVO	1973	04	26	13	58	00.5	19.707N	155.171W	036												
HVO	1973	04	26	14	57	17.7	19.942N	155.078W	056												
HVO	1973	04	26	17	28	18.3	19.931N	155.149W	037												
HVO	1973	04	26	17	40	15.3	19.971N	155.169W	031												
ERL	1973	04	26	29	24	28.0H	19.933N	155.190W	058	.6.00MR	6.1MS6.39FAS		VIII								
HVO	1973	04	26	23	33	38.3	19.944N	155.601W	010												
HVO	1973	04	28	12	07	56.5	19.735N	155.123W	042												
HVO	1973	04	28	13	14	45.7	19.915N	155.081W	036												
HVO	1973	04	28	22	07	18.7	19.921N	155.154W	015												
HVO	1973	04	30	19	26	56.2	20.066N	155.049W	007												
HVO	1973	05	01	16	14	03.0	19.937N	155.115W	043												
HVO	1973	05	05	09	30	25.7	19.397N	155.236W	001												
HVO	1973	05	05	10	01	30.8	19.384N	155.245W	000												
HVO	1973	05	05	11	07	28.0	19.912N	155.075W	043												
HVO	1973	05	05	15	11	18.3	19.373N	155.238W	009												
HVO	1973	05	05	17	41	55.0	19.374N	155.239W	000												
HVO	1973	05	05	11	27	43.9	19.376N	155.236W	001												
HVO	1973	05	05	11	40	51.5	19.375N	155.241W	000												
HVO	1973	05	05	12	54	53.9	19.385N	155.241W	001												
HVO	1973	05	05	23	00	29.5	19.955N	155.118W	037												
HVO	1973	05	06	00	26	14.7	19.981N	155.077W	001												
HVO	1973	05	04	18	07	30.4	19.919N	155.149W	044												
HVO	1973	05	07	17	02	10.1	19.913N	155.161W	041												
HVO	1973	05	08	02	54	05.6	19.917N	155.220W	010												
HVO	1973	05	10	06	32	18.3	19.875N	155.111W	036												
HVO	1973	05	11	17	49	17.8	19.176N	155.454W	036												
HVO	1973	05	12	05	10	11.9	19.904N	155.123W	011												
HVO	1973	05	12	10	50	11.6	19.954N	155.070W	010												
HVO	1973	05	13	22	51	37.5	19.497N	155.075W	010												
HVO	1973	05	16	10	02	14.4	20.004N	155.048W	034												
HVO	1973	05	19	03	10	24.1	19.924N	155.201W	039												
HVO	1973	05	19	19	11	21.8	19.951N	155.246W	027												
HVO	1973	05	29	15	22	01.4	19.466N	155.262W	016												

81/07/17.

SOURCE YEAR	MO	DA	HR	MI	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES				INT PHENOM	RN	CE	Q/S	MAR DG	DIST (KM)	
									-----	-----	-----	-----							BODY
** V INDICATES A POSSIBLE DUPLICATE																			
HVO	1973	09	29	24	42.5	19.422N	155.412W	009											
HVO	1973	11	01	56	43	26.109N	155.917W	031											
HVO	1973	11	02	06	51	15.2	20.218N	155.481W	006										
HVO	1973	11	02	17	14	14.4	20.222N	155.479W	007										
HVO	1973	10	04	17	53	21.3	19.156N	155.119W	018										
HVO	1973	10	08	19	17	42.4	19.343N	155.138W	009										
HVO	1973	10	09	31	53	45.0	19.333N	155.264W	031										
HVO	1973	11	09	02	01	02.2	19.332N	155.272W	032										
● SS	1973	10	09	11	53	45.0H	19.333N	155.263W	027	4.80MB									
● SS	1973	10	09	12	01	00.6H	19.333N	155.263W	027	4.80MB									
HVO	1973	10	13	06	11	12.1	20.516N	156.769W	013										
● SS	1973	11	13	16	11	11.4H	20.620N	155.915W	002	4.30MB									
HVO	1973	10	14	11	42	28.8	19.764N	155.977W	012										
HVO	1973	10	15	22	47	29.5	20.226N	156.061W	020										
HVO	1973	11	16	26	40	41.3	19.820N	155.123W	040										
HVO	1973	11	17	26	53	29.8	19.470N	155.183W	037										
HVO	1973	11	18	02	31	49.8	19.767N	155.160W	021										
HVO	1973	11	21	18	09	33.9	19.331N	155.408W	010										
HVO	1973	11	24	06	33	45.0	19.508N	155.481W	026										
HVO	1973	11	26	07	33	19.7	19.215N	155.814W	009										
HVO	1973	11	03	11	10	41.7	19.330N	155.443W	000										
HVO	1973	11	10	23	33	58.2	20.144N	155.476W	020										
● SS	1973	11	11	09	04	59.1H	20.117N	155.417W	040										
HVO	1973	11	23	13	36	46.2	19.167N	155.717W	009										
HVO	1973	11	24	04	23	38.7	18.966N	155.551W	040										
HVO	1973	11	24	02	59	14.9	19.318N	155.282W	010										
HVO	1973	11	24	17	10	46.0	19.418N	155.443W	006										
HVO	1973	11	29	13	17	13.3	19.451N	155.263W	009										
HVO	1973	12	04	20	16	27.6	19.844N	155.553W	040										
HVO	1973	12	13	04	26	55.9	19.367N	155.293W	034										
● SS	1973	12	13	14	28	56.1H	19.357N	155.292W	033	4.40MB									
HVO	1973	12	14	16	46	41.3	19.315N	155.226W	009										
HVO	1973	12	17	23	17	47.9	18.962N	155.551W	038										
HVO	1974	01	01	06	50	01.7	19.403N	155.492W	009										
HVO	1974	01	02	06	27	51.7	19.242N	155.476W	011										
● SS	1974	01	02	06	27	51.6H	19.233N	155.480W	010										
HVO	1974	01	05	15	17	16.1	19.594N	154.987W	012										
HVO	1974	01	08	04	43	43.6	19.316N	155.225W	010										
● SS	1974	01	09	14	54	43.5H	19.311N	155.206W	009										
HVO	1974	01	09	17	47	50.4	19.417N	155.162W	011										
HVO	1974	01	12	06	24	34.1	19.337N	155.123W	009										
● SS	1974	01	12	16	24	35.9H	19.343N	155.134W	007	4.90MB									
HVO	1974	01	13	00	46	29.3	19.492N	155.740W	010										
HVO	1974	01	13	14	52	13.9	19.370N	155.493W	010										
HVO	1974	01	15	22	05	45.5	19.186N	155.601W	033										
● SS	1974	01	16	01	04	46.5H	19.780N	155.600W	036										
HVO	1974	01	17	15	18	42.4	19.350N	155.455W	009										
HVO	1974	01	19	13	06	17.7	19.350N	155.602W	006										
● SS	1974	01	20	09	27	51.2H	19.190N	155.690W	006										
HVO	1974	01	21	12	26	09.5	19.324N	155.138W	009										

81407/17.

SOURCE YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT MAX	PHENOM DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
									BODY	SURF	OTHER	LOCAL								
**N INDICATES A POSSIBLE DUPLICATE																				
HVO	1974	05	24	19	39	55.4	19.217N	155.367W	008					613				052	95	61.
HVO	1974	05	24	23	49	13.6	19.229N	155.369W	006					613				052	95	60.
HVO	1974	05	25	13	38	82.3	20.151N	155.405W	036					613				068	05	77.
HVO	1974	06	02	13	44	51.5	19.478N	155.069W	036					613				052	95	96.
HVO	1974	06	03	13	02	09.1	19.438N	155.441W	009					613	E			052	95	46.
SS	1974	06	03	23	02	09.1	19.420N	155.436W	008				III	613				052	95	41.
HVO	1974	06	14	19	33	24.3	19.295N	155.222W	007					613	E			052	95	72.
HVO	1974	06	10	23	59	41.7	19.911N	155.768W	029					613				052	95	51.
HVO	1974	06	19	05	05	42.4	19.378N	155.419W	010					613				052	95	50.
HVO	1974	06	19	08	11	13.9	19.312N	155.435W	007					613	E			052	95	41.
HVO	1974	06	19	05	33	03.7	19.384N	155.422W	009					613				052	95	49.
HVO	1974	06	19	15	07	51.6	19.374N	155.419W	009					613	E			052	95	50.
SS	1974	06	19	15	05	42.4	19.360N	155.400W	008	4.50MB			V	613	D	58		052	95	52.
SS	1974	06	19	15	11	13.5	19.350N	155.420W	005				III	613				052	95	50.
SS	1974	06	19	15	33	03.6	19.350N	155.410W	007				III	613				052	95	51.
HVO	1974	06	19	15	05	53.0	19.375N	155.436W	008					613	E			052	95	48.
HVO	1974	06	19	20	51	26.5	19.437N	155.212W	009					613				052	95	72.
SS	1974	06	21	05	51	27.4	19.330N	155.214W	007	4.30MB			III	613	F	20		052	95	72.
HVO	1974	06	22	01	51	17.6	19.433N	155.120W	010					613	E			052	95	72.
HVO	1974	06	27	15	44	43.4	19.415N	155.282W	002					613	E			052	95	63.
SS	1974	06	28	01	44	42.9	19.410N	155.270W	001					613				052	95	63.
HVO	1974	07	09	02	51	36.7	19.419N	155.310W	010					613				052	95	52.
HVO	1974	07	09	14	42	35.0	19.712N	155.025W	032					613				052	95	94.
SS	1974	07	12	03	17	17.6	19.470N	155.440W	008					613				052	95	46.
HVO	1974	07	12	15	32	53.1	19.465N	155.729W	049					613	E			052	95	16.
SS	1974	07	13	11	12	43.0	19.450N	155.731W	008					613				052	95	16.
HVO	1974	07	13	08	37	45.6	19.360N	155.256W	013					613				052	95	67.
SS	1974	07	13	16	37	46.5	19.350N	155.250W	007					613				052	95	68.
HVO	1974	07	13	20	43	12.8	19.458N	155.697W	003					613	E			052	95	30.
HVO	1974	07	13	11	20	33.5	19.340N	155.257W	004					613				052	95	66.
SS	1974	07	19	14	33	49.3	18.540N	155.290W	008					613				052	85	120.
SS	1974	07	19	15	00	02.7	19.210N	155.250W	001					613				052	95	67.
HVO	1974	07	19	16	41	41.2	19.610N	155.571W	015					613				052	95	50.
SS	1974	07	19	21	22	02.9	19.340N	155.250W	000					613				052	95	67.
SS	1974	07	19	22	41	40.0	19.870N	155.560W	026					613				052	95	50.
HVO	1974	07	21	19	17	51.4	19.346N	155.214W	032					613	E			052	95	71.
SS	1974	07	22	14	17	50.5	19.320N	155.210W	030					613				052	95	72.
HVO	1974	07	23	13	46	33.0	19.420N	155.597W	003					613	E			052	95	30.
HVO	1974	07	23	16	15	03.2	19.477N	155.276W	015					613				052	95	63.
HVO	1974	07	24	12	11	13.2	19.374N	155.410W	008					613	E			052	95	64.
SS	1974	07	24	04	13	02.5	19.330N	155.260W	014					613				052	95	64.
HVO	1974	07	27	17	04	11.1	19.397N	154.410W	031					613				052	94	112.
HVO	1974	08	07	16	05	14.1	19.540N	155.671W	009					613	E			052	95	23.
HVO	1974	08	09	11	12	04.4	19.375N	155.376W	009					613	E			052	95	61.
SS	1974	08	09	16	44	36.3	19.470N	155.670W	008					613				052	95	22.
SS	1974	08	18	11	13	59.5	19.340N	155.300W	027	4.20MB			III	613	F	27		052	95	62.
HVO	1974	08	19	15	21	15.7	19.400N	155.710W	041					613				052	95	91.
HVO	1974	08	12	11	26	27.6	19.300N	155.440W	008					613				052	95	46.
SS	1974	08	12	21	06	20.5	19.370N	155.430W	008					613				052	95	49.
HVO	1974	08	13	20	03	55.7	19.432N	155.616W	004					613	E			052	95	29.

11/17/77.

SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES	INT	FFROM	PN	CE	G/S	MAR	DG	DIST (KM)	

										BODY	SURF	OTHER	LOCAL	MAX	DTSVNO				
***V INDICATES A POSSIBLE DUPLICATE																			
FVJ	1974	08	13	22	45	30.3	19.431N	155.603W	004										3.1 ML FVO
FVJ	1974	09	14	13	27	07.2	19.465N	155.627W	006										3.0 ML FVO
FVJ	1974	09	16	21	59	29.6	19.297N	156.329W	038										3.1 ML FVO
FVJ	1974	08	17	23	04	16.3	19.523N	155.670W	007										3.1 ML FVO
FVJ	1974	08	17	22	52	21.3	19.804N	156.101W	024										3.6 ML FVO
● SS	1974	08	18	08	52	20.1F	19.790N	156.170W	039										3.8CML FVO
FVJ	1974	08	18	14	31	25.1	19.379N	155.072W	006										3.1 ML FVO
SS	1974	08	21	08	38	23.4H	19.553N	155.955W	006										3.30ML FVO
FVJ	1974	08	23	18	15	02.3	19.314N	155.221W	010										3.7 ML FVO
● SS	1974	08	24	04	15	01.9H	19.316N	155.220W	008										3.9JML FVO
FVJ	1974	08	25	12	22	18.6	19.339N	155.310W	007										3.3 ML FVO
FVJ	1974	08	27	21	49	40.8	19.333N	155.206W	010										4.5 ML FVO
● SS	1974	08	28	07	49	40.7H	19.333N	155.210W	007	4.80MB									4.60ML FVO
FVJ	1974	09	03	11	43	13.6	19.370N	155.563W	025										3.1 ML FVO
SS	1974	09	18	07	58	34.2H	19.395N	155.870W	010										3.3CML FVO
FVJ	1974	09	19	15	51	57.7	19.503N	155.504W	029										3.3 ML FVO
● SS	1974	09	21	01	31	37.3H	19.780N	155.830W	039										3.5CML FVO
FVJ	1974	09	24	21	17	13.8	19.411N	155.437W	009										3.5 ML FVO
FVJ	1974	09	25	02	20	25.2	19.507N	155.113W	009										3.6 ML FVO
FVJ	1974	09	25	27	16	51.2	20.181N	155.529W	028										3.8 ML FVO
● SS	1974	09	26	06	18	41.7H	20.181N	155.530W	042										3.90ML FVO
FVJ	1974	10	09	01	44	20.7	19.575N	155.508W	011										3.3 ML FVO
FVJ	1974	10	09	12	37	55.1	19.575N	155.463W	010										3.0 ML FVO
FVJ	1974	10	10	22	08	36.8	19.907N	155.997W	022										3.1 ML FVO
FVJ	1974	10	11	17	51	40.8	19.995N	155.480W	035										3.0 ML FVO
FVJ	1974	10	18	08	31	38.4	19.427N	155.498W	019										3.5 ML FVO
FVJ	1974	10	18	14	10	12.4	19.593N	155.973W	026										3.2 ML FVO
FVJ	1974	10	18	14	49	41.2	19.919N	156.871W	033										3.2 ML FVO
● SS	1974	10	18	18	38	05.3H	19.420N	155.490W	008										4.0CML FVO
FVJ	1974	10	17	18	17	33.4	19.717N	155.840W	009										3.3 ML FVO
FVJ	1974	10	24	06	19	54.7	19.577N	155.477W	010										3.2 ML FVO
FVJ	1974	10	28	13	23	07.3	19.331N	155.189W	010										3.4 ML FVO
● SS	1974	10	26	23	20	17.1H	19.330N	155.190W	009										3.70ML FVO
FVJ	1974	10	29	12	52	34.8	19.523N	155.863W	009										3.1 ML FVO
FVJ	1974	10	29	18	57	30.3	19.410N	155.422W	009										3.4 ML FVO
● SS	1974	10	31	14	57	39.2H	19.397N	155.410W	009										3.7CML FVO
FVJ	1974	10	31	18	17	43.8	19.372N	155.612W	011										3.2 ML FVO
FVJ	1974	10	31	18	31	41.8	19.364N	155.644W	009										3.5 ML FVO
FVJ	1974	10	31	18	48	02.1	19.365N	155.648W	009										3.7 ML FVO
● SS	1974	10	31	21	01	41.9H	19.373N	155.650W	025										4.0CML FVO
● SS	1974	10	31	21	45	02.1H	19.367N	155.670W	026										3.80ML FVO
FVJ	1974	11	01	13	42	29.4	19.594N	155.771W	004										3.0 ML FVO
FVJ	1974	11	09	04	46	18.7	19.360N	155.134W	009										3.0 ML FVO
● SS	1974	11	09	14	45	15.7H	19.370N	155.140W	007										3.20ML FVO
FVJ	1974	11	10	01	58	14.7	19.415N	155.425W	010										4.2 ML FVO
● SS	1974	11	10	11	53	14.7H	19.407N	155.410W	008										4.1ML FVO
FVJ	1974	11	10	18	59	04.3	19.422N	155.285W	001										3.1 ML FVO
● SS	1974	11	13	14	57	04.1H	19.420N	155.280W	002										3.5CML FVO
FVJ	1974	11	13	22	59	22.5	20.251N	155.636W	022										3.0 ML FVO
FVJ	1974	11	15	09	19	01.5	19.460N	155.479W	035										3.3 ML FVO

197711

STATION	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES BODY SURF OTHER LOCAL	INT MAX	PHENOM DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)	
..V	INDICATES																		
A	POSSIBLE DUPLICATE																		
HVO	1974	11	16	05	12	39.2	19.212N	156.364W	031										58.
HVO	1974	11	16	07	50	23.8	19.502N	155.656W	008										24.
GS	1974	11	16	15	12	41.3F	19.190N	156.220W	01F		III								47.
HVO	1974	11	21	21	49	14.6	19.337N	155.311W	031										61.
GS	1974	11	22	07	49	14.7H	19.340N	155.317W	029	3.90MB		III	F	26					61.
HVO	1974	11	30	03	54	23.7	19.435N	155.418W	006			E	613						49.
HVO	1974	11	30	04	07	37.9	19.415N	155.376W	008				613						53.
HVO	1974	11	30	04	34	04.6	19.400N	155.451W	006			E	613						46.
HVO	1974	11	30	04	46	54.8	19.456N	155.403W	009			E	613						50.
HVO	1974	11	30	04	55	35.5	19.415N	155.428W	008			E	613						48.
HVO	1974	11	30	06	02	44.1	19.434N	155.436W	008			E	613						47.
HVO	1974	11	30	06	11	14.6	19.416N	155.425W	009				613						48.
HVO	1974	11	30	06	40	27.8	19.384N	155.429W	009				613						48.
HVO	1974	11	30	06	47	20.1	19.379N	155.478W	006			E	613						43.
HVO	1974	11	30	07	18	20.5	19.481N	155.497W	005			E	613						52.
HVO	1974	11	30	08	00	37.4	19.417N	155.494W	006				613						51.
HVO	1974	11	30	13	17	43.0	19.377N	155.430W	009				613						41.
GS	1974	11	30	13	34	33.4F	19.417N	155.438W	007	5.10MP	5.5MS		75						51.
GS	1974	11	30	14	37	37.7H	19.430N	155.360W	009			III							55.
GS	1974	11	30	14	49	54.8H	19.447N	155.350W	008			III							53.
HVO	1974	11	30	14	01	53.0	19.419N	155.420W	012				613						49.
HVO	1974	11	30	14	05	00.2	19.481N	155.493W	007			E	613						50.
HVO	1974	12	01	03	52	54.2	19.380N	155.443W	008			E	613						47.
HVO	1974	12	01	18	59	11.1	19.410N	155.434W	009				613						47.
HVO	1974	12	02	12	46	32.6	19.030N	155.605W	040				613						62.
HVO	1974	12	03	14	47	40.7	19.447N	155.397W	009				613						51.
HVO	1974	12	07	12	13	44.2	19.400N	155.627W	003				613						27.
HVO	1974	12	07	17	33	09.5	19.404N	155.414W	010				613						49.
HVO	1974	12	07	18	14	27.9	19.477N	155.447W	009				613						46.
HVO	1974	12	08	01	28	52.5	19.713N	156.160W	029				613						101.
GS	1974	12	08	01	14	27.8F	19.400N	155.440W	008		III								47.
HVO	1974	12	08	06	44	01.9	19.453N	155.481W	005			E	613						50.
HVO	1974	12	08	12	39	13.5	19.366N	155.425W	010			E	613						49.
GS	1974	12	08	16	40	31.9F	19.420N	155.310W	007		III								53.
HVO	1974	12	08	06	42	17.1	19.437N	155.633W	004				613						28.
HVO	1974	12	11	01	39	05.4	19.400N	155.589W	010			E	613						49.
HVO	1974	12	11	02	32	25.6	19.439N	155.619W	002				613						28.
HVO	1974	12	11	07	27	54.4	19.440N	155.417W	009				613						49.
GS	1974	12	11	08	14	30.1F	19.400N	155.520W	001			III							38.
GS	1974	12	11	13	45	52.7F	19.430N	155.600W	006			III							74.
HVO	1974	12	12	04	11	18.0	19.365N	155.591W	008			E	613						64.
GS	1974	12	12	14	01	13.1F	19.460N	155.110W	006			III							62.
HVO	1974	12	14	00	11	10.4	19.410N	155.422W	009				613						49.
HVO	1974	12	14	06	50	24.2	19.435N	155.643W	003				613						29.
HVO	1974	12	16	06	39	08.7	19.410N	155.431W	010			E	613						48.
HVO	1974	12	16	14	17	06.4	19.464N	155.597W	011			E	613						30.
HVO	1974	12	16	14	53	47.9	19.475N	155.001W	072			E	613						29.
GS	1974	12	16	21	53	47.4F	19.450N	155.590W	074	3.30MB		III	F	32					31.
HVO	1974	12	16	23	17	01.6	19.417N	155.432W	009				613						48.
HVO	1974	12	16	23	33	30.8	19.435N	155.437W	009			E	613						47.

11/07/11

SOURCE YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES			INT PHENOM MAX DTSVNO	RN	CE	Q/S	MAR DG	DIST (KM)	
									BODY	SURF	OTHER							LOCAL
**N INDICATES A POSSIBLE DUPLICATE																		
HVO	1974	12	31	17	10	53.4	19.311N	155.361W	004									3.2 ML FVO
HVO	1974	12	31	19	02	17.4	19.293N	155.378W	005									3.2 ML FVO
HVO	1974	12	31	19	12	21.3	19.312N	155.379W	007									3.1 ML HVO
HVO	1974	12	31	19	30	55.2H	19.310N	155.333W	005									3.20ML HVO
SS	1974	12	31	19	30	55.2H	19.310N	155.333W	005									3.4 ML FVO
FVO	1974	12	31	19	51	30.9	19.260N	155.397W	007									4.2 ML FVO
HVO	1974	12	31	21	43	55.4	19.300N	155.386W	004									3.4 ML HVO
HVO	1974	12	31	21	53	25.0	19.262N	155.359W	007									3.4 ML HVO
HVO	1974	12	31	21	24	43.5	19.272N	155.402L	006									3.4 ML HVO
HVO	1974	12	31	21	41	54.3	19.263N	155.362W	007									4.3 ML HVO
SS	1974	12	31	21	14	02.8H	19.290N	155.360W	006									3.0CML FVO
SS	1974	12	31	22	25	23.1H	19.300N	155.370W	003									3.2CML FVO
SS	1974	12	31	22	40	47.5H	19.290N	155.360W	100	5.5 MB	5. MS							5.3CML HVO
SS	1974	12	31	23	06	45.2H	19.272N	155.360W	006									3.0CML HVO
SS	1974	12	31	23	36	37.5H	19.340N	155.330W	006									3.5CML FVO
SS	1974	12	31	23	58	37.5H	19.238N	155.435W	005									3.5 ML FVO
HVO	1975	01	01	01	29	31.6	19.175N	155.349W	005									4.1 ML FVO
HVO	1975	01	01	01	02	07.3	19.175N	155.349W	005									4.20
HVO	1975	01	01	01	02	59.0H	19.175N	155.410W	047	4.0MB								3.2
HVO	1975	01	01	01	09	17.0	19.260N	155.364W	005									3.0 ML FVO
HVO	1975	01	01	01	55	40.6	19.276N	155.400W	005									3.0 ML FVO
HVO	1975	01	01	02	02	16.1	19.276N	155.368W	007									5.1 ML HVO
HVO	1975	01	01	02	41	10.9	19.014N	155.355W	006									4.6 ML HVO
HVO	1975	01	01	03	25	45.8	19.231N	155.373W	009									3.5 ML FVO
HVO	1975	01	01	03	44	16.3	19.247N	155.416W	008									3.3 ML FVO
HVO	1975	01	01	03	35	25.6	19.263N	155.400W	004									3.4 ML FVO
HVO	1975	01	01	04	48	21.5	19.250N	155.415W	002									3.1 ML FVO
HVO	1975	01	01	05	19	13.7	19.241N	155.385W	007									3.4 ML FVO
HVO	1975	01	01	05	50	16.2	19.275N	155.354W	008									3.1 ML FVO
HVO	1975	01	01	05	51	07.8	19.277N	155.351W	007									3.3 ML FVO
HVO	1975	01	01	06	03	07.7	19.237N	155.411W	021									3.2 ML FVO
SS	1975	01	01	06	43	54.0H	19.310N	155.300W	005	4.5MB								4.1CML HVO
HVO	1975	01	01	06	47	45.5	19.249N	155.375W	007									3.0 ML FVO
SS	1975	01	01	07	41	55.0H	19.370N	155.400W	005	4.2MB								4.1CML HVO
HVO	1975	01	01	07	54	44.5	19.272N	155.394W	005									3.3 ML FVO
HVO	1975	01	01	07	59	51.0	19.273N	155.386W	005									3.1 ML HVO
HVO	1975	01	01	09	11	35.4	19.241N	155.377W	009									3.5 ML HVO
HVO	1975	01	01	09	46	45.7	19.247N	155.405W	006									4.3 ML FVO
HVO	1975	01	01	10	27	05.0	19.200N	155.371W	003									3.6 ML FVO
HVO	1975	01	01	10	33	47.7	19.310N	155.352W	011									3.4 ML FVO
HVO	1975	01	01	10	46	44.4	19.277N	155.400W	009									4.4 ML HVO
SS	1975	01	01	11	02	07.0H	19.200N	155.400W	005	4.7MB								4.4CML FVO
HVO	1975	01	01	11	21	54.5	19.183N	155.363W	008									4.1 ML FVO
SS	1975	01	01	12	41	11.0H	19.200N	155.400W	005	4.7MB								5.1CML FVO
SS	1975	01	01	13	18	00.6H	19.300N	155.399W	010	4.5MB								3.0
SS	1975	01	01	13	28	54.5H	19.475N	155.380W	010	5.1MB	5.3HS							3.0
HVO	1975	01	01	13	44	23.8	19.334N	155.386W	003									3.0
SS	1975	01	01	13	44	36.1H	19.171N	155.384W	010	4.7MB								4.9C
HVO	1975	01	01	14	17	58.8	19.333N	155.386W	003									3.1 ML FVO
HVO	1975	01	01	15	35	18.9	19.295N	155.234W	010									3.7 ML HVO
HVO	1975	01	01	16	30	41.5	19.247N	155.371W	009									3.1 ML HVO
HVO	1975	01	01	17	23	41.1	19.177N	155.316W	007									3.0 ML FVO

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES				INT PHENOM MAX DTSVNO	RN	CE	Q/S	MAR DG	DIST (KMP)
										RODY	SURF	OTHER	LOCAL						
** I INDICATES A POSSIBLE DUPLICATE																			
GS	1975	01	01	17	46	45.01	19.230N	155.400W	005	4.90MB									
GS	1975	01	01	20	46	49.01	19.230N	155.400W	005	4.50MB									
HVO	1975	01	01	21	03	55.9	19.230N	155.348W	009										
HVO	1975	01	01	21	17	52.7	19.231N	155.407W	002										
HVO	1975	01	01	21	37	20.4	19.473N	155.461W	010										
HVO	1975	01	01	23	26	54.1	19.234N	155.389W	006										
HVO	1975	01	01	23	56	53.0	19.295N	155.268W	010										
HVO	1975	01	02	02	39	09.7	19.201N	155.399W	011										
HVO	1975	01	02	03	27	43.1	19.217N	155.387W	006										
HVO	1975	01	02	03	39	53.4	19.185N	155.374W	010										
HVO	1975	01	02	03	41	47.6	19.267N	155.405W	008										
HVO	1975	01	02	03	47	07.9	19.311N	155.393W	006										
HVO	1975	01	02	04	08	23.1	19.277N	155.410W	008										
HVO	1975	01	02	04	26	47.2	19.234N	155.349W	010										
GS	1975	01	02	07	07	54.04	19.271N	155.400W	001	4.0MB									
HVO	1975	01	02	12	14	54.9	19.194N	155.370W	009										
HVO	1975	01	02	12	44	02.5	19.303N	155.402W	005										
HVO	1975	01	02	13	18	47.7	19.314N	155.392W	006										
GS	1975	01	02	13	27	45.01	19.277N	155.410W	008	4.50MB	4.2MS								
HVO	1975	01	02	15	44	34.9	19.147N	155.370W	008										
HVO	1975	01	02	16	44	03.5	19.274N	155.394W	010										
HVO	1975	01	02	20	43	51.2	19.427N	155.636W	001										
HVO	1975	01	02	20	52	16.0	19.315N	155.366W	008										
HVO	1975	01	02	23	33	19.1	19.206N	155.350W	009										
HVO	1975	01	03	01	02	54.4	19.171N	155.345W	010										
HVO	1975	01	03	03	15	39.3	19.245N	155.377W	004										
HVO	1975	01	03	03	33	39.8	19.210N	155.407W	009										
HVO	1975	01	03	05	15	06.7	19.170N	155.381W	010										
HVO	1975	01	03	07	32	45.3	19.234N	155.362W	010										
HVO	1975	01	03	07	43	43.2	19.236N	155.393W	003										
HVO	1975	01	03	08	11	40.4	19.244N	155.391W	009										
HVO	1975	01	03	08	14	44.1	19.217N	155.383W	010										
HVO	1975	01	03	08	34	35.3	19.202N	155.375W	010										
HVO	1975	01	03	10	07	04.6	19.241N	155.378W	006										
HVO	1975	01	03	11	17	28.2	19.247N	155.368W	010										
HVO	1975	01	03	11	47	51.7	19.241N	155.371W	010										
HVO	1975	01	03	11	55	10.1	19.301N	155.355W	003										
HVO	1975	01	03	12	41	04.7	19.243N	155.372W	008										
HVO	1975	01	03	13	03	37.1	19.240N	155.363W	001										
HVO	1975	01	03	15	31	09.4	19.291N	155.349W	016										
GS	1975	01	03	17	32	44.14	19.142N	155.716W	010	4.70MB									
HVO	1975	01	03	20	05	52.4	19.338N	155.125W	009										
HVO	1975	01	03	20	59	01.5	19.122N	156.223W	014										
HVO	1975	01	04	02	15	28.1	19.241N	155.398W	005										
HVO	1975	01	04	03	40	12.7	19.239N	155.381W	004										
GS	1975	01	04	15	35	52.01	19.370N	155.100W	008	4.30MB									
HVO	1975	01	04	15	02	26.6	19.241N	155.371W	010										
HVO	1975	01	04	15	32	05.2	19.269N	155.373W	010										
HVO	1975	01	04	15	42	13.1	19.279N	155.380W	007										
HVO	1975	01	04	16	11	31.6	19.202N	155.345W	005										

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT F-PHENOM	RN	CE	Q/S	MAR	DG	DIST (KM)	
										BODY	SURF	OTHER	LOCAL	MAX	DTSVNO						
**V INDICATES A POSSIBLE DUPLICATE																					
HVO	1975	04	05	11	56	58.3	19.284N	155.377W	007												57.
HVO	1975	04	06	12	15	55.4	19.312N	155.222W	010												71.
HVO	1975	04	07	04	24	56.3	19.414N	155.602W	009												30.
HVO	1975	04	07	14	39	29.3	19.275N	155.261W	010						E	613					69.
HVO	1975	04	07	22	32	16.0	18.995N	155.354W	048												76.
HVO	1975	04	10	06	54	10.9	19.442N	155.607W	054						E	613					29.
HVO	1975	04	10	14	19	43.2	19.341N	155.139W	010												79.
HVO	1975	04	11	06	22	24.9	19.336N	155.144W	010						E	613					79.
HVO	1975	04	12	23	24	01.2	19.473N	155.626W	005												27.
HVO	1975	04	17	16	53	22.3	19.531N	155.562W	038						E	613					24.
HVO	1975	04	17	23	33	14.7	19.305N	155.221W	010												72.
HVO	1975	04	18	00	57	11.6	19.490N	155.609W	010						E	613					19.
HVO	1975	04	18	03	22	21.0	19.309N	155.223W	010												71.
HVO	1975	04	18	11	11	09.6	19.503N	155.616W	015												36.
HVO	1975	04	18	13	01	39.9	19.916N	156.748W	046												110.
HVO	1975	04	18	14	15	04.1	19.341N	155.604W	009						E	613					24.
HVO	1975	04	18	20	04	35.4	19.476N	155.612W	004												29.
HVO	1975	04	21	15	37	2.3	19.126N	155.704W	007						E	613					41.
HVO	1975	04	21	16	07	59.4	19.251N	155.505W	010												38.
HVO	1975	04	24	14	45	15.4	19.014N	155.3.10	000												57.
HVO	1975	04	24	17	11	21.4	19.016N	155.603W	007												24.
HVO	1975	04	24	19	05	36.1	19.400N	155.601W	001						E	613					29.
HVO	1975	04	27	20	41	33.0	20.064N	155.574W	014												74.
HVO	1975	04	27	22	04	53.8	19.442N	155.606W	003						E	613					29.
HVO	1975	04	29	11	14	21.1	19.446N	155.601W	003						E	613					30.
HVO	1975	04	30	01	41	07.5	19.408N	155.271W	015												64.
HVO	1975	04	30	19	23	10.0	19.390N	155.463W	009												43.
HVO	1975	04	31	16	42	20.0	19.475N	155.606W	003						E	613					31.
HVO	1975	05	01	21	14	04.1	19.045N	155.728W	059												159.
HVO	1975	05	05	21	14	30.5	19.434N	155.607W	004												29.
HVO	1975	05	05	02	55	14.3	19.433N	155.601W	003						E	613					30.
HVO	1975	05	07	17	52	36.3	19.013N	156.702W	011												94.
HVO	1975	05	07	21	33	04.5	19.474N	155.592W	001												30.
HVO	1975	05	11	14	32	51.9	19.338N	155.126W	019						E	613					61.
HVO	1975	05	11	04	12	02.6	19.535N	155.664W	007						E	613					24.
HVO	1975	05	11	14	44	38.2	19.461N	155.631W	003												26.
HVO	1975	05	14	03	16	51.8	19.390N	155.590W	021						E	613					56.
HVO	1975	05	14	16	53	57.8	19.434N	155.601W	003												30.
HVO	1975	05	15	11	51	37.4	19.434N	155.597W	001						E	613					30.
HVO	1975	05	18	18	23	45.0	19.430N	155.605W	003												29.
HVO	1975	05	19	16	13	10.4	19.428N	155.615W	004						E	613					28.
HVO	1975	05	19	18	49	27.3	19.449N	155.597W	001						E	613					30.
HVO	1975	05	21	22	32	06.2	20.012N	155.611W	003												58.
HVO	1975	05	22	04	46	05.4	19.378N	155.466W	007						E	613					45.
US	1975	05	23	01	30	58.7	20.302N	155.647W	022	4.4	MB				E	613	F	22			96.
HVO	1975	05	24	02	04	45.8	19.415N	155.416W	011						E	613					49.
HVO	1975	05	25	05	13	37.3	19.664N	156.013W	020												26.
HVO	1975	05	27	11	02	54.6	19.468N	155.562W	000						E	613					31.
HVO	1975	05	29	16	46	41.9	19.419N	155.608W	003						E	613					29.
HVO	1975	05	29	12	14	14.1	19.378N	155.361W	009						E	613					65.

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT MAX	PHENOM DTSVNO	RV	CE	Q/S	PAR	DG	DIST (KM)
										BODY	SURF	OTHR	LOCAL								
**4 INDICATES																					
A POSSIBLE DUPLICATE																					
HVO	1975	05	30	12	40	35.1	19.374N	155.464W	007												
HVO	1975	05	30	22	45	37.0	19.454N	155.606W	003												
HVO	1975	06	01	22	57	57.5	19.451N	155.593W	004												
HVO	1975	06	02	05	10	14.5	19.379N	155.465W	001												
HVO	1975	06	02	09	58	37.0	19.457N	155.600W	001												
HVO	1975	06	03	10	19	46.2	19.480N	155.579W	001												
HVO	1975	06	05	08	11	03.1	19.318N	155.615W	010												
HVO	1975	06	07	06	02	11.7	19.394N	155.446W	010												
HVO	1975	06	07	11	53	57.6	19.196N	155.608W	010												
HVO	1975	06	08	05	32	29.0	19.343N	155.133W	010												
HVO	1975	06	11	08	51	13.6	19.434N	155.609W	004												
HVO	1975	06	11	15	16	44.7	19.437N	155.619W	004												
HVO	1975	06	13	07	54	02.3	19.138N	155.100W	056												
HVO	1975	06	13	16	34	05.0	19.452N	155.578W	000												
HVO	1975	06	20	18	00	51.5	19.515N	155.654W	007												
HVO	1975	06	21	09	20	21.0	19.410N	155.615W	000												
HVO	1975	06	21	13	39	55.2	19.454N	155.480W	010												
HVO	1975	06	25	00	44	41.1	19.404N	155.614W	003												
HVO	1975	07	01	15	31	05.2	19.400N	155.460W	001												
HVO	1975	07	03	01	02	40.1	19.397N	155.470W	037												
HVO	1975	07	04	01	19	34.1	19.499N	155.471W	036												
HVO	1975	07	04	17	40	54.9	19.373N	155.317W	030												
HVO	1975	07	04	21	00	46.6	19.374N	155.317W	031												
SS	1975	07	05	03	40	56.1	19.353N	155.315W	028												
HVO	1975	07	05	23	18	17.6	19.401N	155.440W	010												
HVO	1975	07	05	25	09	45.2	19.469N	155.633W	007												
HVO	1975	07	06	01	23	06.3	19.407N	155.600W	009												
SS	1975	07	06	04	11	11.0	19.447N	155.603W	001												
SS	1975	07	06	04	25	45.4	19.430N	155.630W	004												
HVO	1975	07	06	16	59	22.5	19.518N	155.446W	002												
HVO	1975	07	06	23	48	56.1	19.542N	155.415W	001												
HVO	1975	07	07	05	39	42.7	19.539N	155.463W	006												
HVO	1975	07	07	09	11	27.6	19.539N	155.469W	006												
HVO	1975	07	07	03	23	22.1	19.536N	155.461W	007												
HVO	1975	07	07	14	47	42.5	19.540N	155.482W	003												
SS	1975	07	07	15	10	46.6	19.513N	155.452W	007												
SS	1975	07	07	15	25	22.0	19.513N	155.455W	008												
HVO	1975	07	07	16	33	00.3	19.533N	155.460W	005												
HVO	1975	07	07	19	07	36.3	19.544N	155.475W	006												
HVO	1975	07	07	20	30	36.2	19.542N	155.463W	005												
HVO	1975	07	07	22	33	41.1	19.539N	155.461W	006												
HVO	1975	07	07	22	50	01.7	19.541N	155.461W	009												
HVO	1975	07	07	23	33	28.0	19.535N	155.472W	007												
SS	1975	07	08	00	47	41.0	19.513N	155.478W	001												
HVO	1975	07	08	05	52	40.5	19.536N	155.465W	009												
HVO	1975	07	08	01	09	07.7	19.530N	155.473W	001												
HVO	1975	07	08	04	16	31.4	19.532N	155.457W	006												
SS	1975	07	08	04	55	52.2	19.526N	155.462W	009												
HVO	1975	07	08	04	59	10.8	19.535N	155.467W	007												
HVO	1975	07	08	06	31	00.9	19.532N	155.473W	006												

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SOURCE	YEAR	MO DA HR MN. SEC			LA	L	G	LEFT (KM)	-----MAGNITUDES-----				INT	F#ENOM MAX DTSVHO	RN	CE	Q/S	MAR	DG	DIST (KM)
		BODY							SURF		OTHER									
**N INDICATES A POSSIBLE DUPLICATE																				
FVJ	1975	07	08	18	56	35.2	19.525N	155.474W	008			3.3 ML FVO		E	613			052 95	43.	
SS	1975	07	08	11	09	07.5H	19.517N	155.465W	007			3.90ML FVO			613	6		052 95	44.	
FVO	1975	07	08	20	07	02.7	19.535N	155.465W	007			3.9 ML FVO		E	613			052 95	44.	
FVO	1975	07	18	21	09	21.4	19.530N	155.470W	006			3.2 ML FVO		E	613			052 95	44.	
FVO	1975	07	08	23	53	43.4	19.540N	155.462W	005			3.0 ML FVO		E	613			052 95	45.	
FVO	1975	07	09	13	49	27.6	19.536N	155.468W	007			3.4 ML FVO		E	613			052 95	44.	
FVO	1975	07	09	15	47	42.7	19.543N	155.466W	009			3.9 ML FVO		E	613			052 95	44.	
FVO	1975	07	09	15	57	48.6	19.541N	155.470W	006			3.1 ML FVO		E	613			052 95	44.	
SS	1975	07	09	16	07	02.6H	19.512N	155.458W	006			4.10ML FVO			613	12		052 95	45.	
FVO	1975	07	09	17	04	34.0	19.530N	155.463W	007			3.0 ML FVO		E	613			052 95	44.	
FVO	1975	07	09	18	40	03.5	19.531N	155.470W	008			4.5 ML FVO			613			052 95	44.	
FVO	1975	07	09	18	34	23.8	19.542N	155.458W	007			3.4 ML FVO		E	613			052 95	45.	
SS	1975	07	09	19	47	27.5H	19.512N	155.462W	007			3.60ML FVO			613	11		052 95	44.	
SS	1975	07	09	19	47	42.7H	19.515N	155.460W	007			4.30ML FVO			613	12		052 95	45.	
SS	1975	07	09	19	40	03.4H	19.507N	155.465W	007			4.50ML FVO			613	F	10	052 95	44.	
FVO	1975	07	09	19	30	06.1	19.530N	155.462W	006			3.1 ML FVO		E	613			052 95	45.	
FVO	1975	07	12	16	34	39.0	19.525N	155.471W	006			3.0 ML FVO		E	613			052 95	44.	
FVO	1975	07	15	11	19	59.0	19.466N	155.515W	009			3.4 ML FVO			613			052 95	82.	
FVO	1975	07	11	18	19	36.0	19.453N	155.535W	010			4.1 ML FVO			613			052 95	22.	
FVO	1975	07	15	19	58	44.7	19.460N	155.517W	017			3.0 ML FVO		E	613			052 95	31.	
FVO	1975	07	20	23	14	59.0	19.466N	155.560W	031			3.7 ML FVO			613			052 95	54.	
FVO	1975	07	19	13	59	14.9	19.529N	155.501W	023			3.1 ML FVO			613			060 05	96.	
FVO	1975	07	30	13	31	22.4	19.533N	155.510W	019			3.9 ML FVO		E	613			052 95	30.	
FVO	1975	07	31	11	44	04.3	19.450N	155.642W	012			3.2 ML FVO			613			052 95	7.	
FVO	1975	08	03	01	19	09.5	19.464N	155.735W	010			3.0 ML FVO		E	613			052 95	15.	
FVO	1975	08	05	17	38	34.7	19.367N	155.498W	008			3.2 ML FVO			613			052 95	55.	
FVO	1975	08	05	15	51	35.7	19.373N	155.543W	007			3.3 ML FVO			613			052 95	57.	
FVO	1975	08	08	18	57	51.7	19.370N	155.590W	007			3.0 ML FVO		E	613			052 95	56.	
FVO	1975	08	18	17	20	57.1	19.443N	155.720W	037			3.9 ML FVO			613			052 96	24.	
FVO	1975	08	24	17	48	31.0	19.387N	155.670W	035			3.6 ML FVO		E	613			052 95	64.	
FVO	1975	08	26	07	48	57.6	19.757N	155.645W	016			3.0 ML FVO			613			052 85	103.	
FVO	1975	08	27	17	34	44.0	19.449N	155.474W	010			4.0 ML FVO		E	613			052 95	43.	
FVO	1975	08	27	13	24	31.4	19.672N	155.620W	015			3.0 ML FVO			613			052 85	95.	
FVO	1975	08	29	02	01	00.6	19.753N	155.633W	033			3.0 ML FVO			613			052 96	36.	
FVO	1975	09	01	19	41	01.4	19.800N	155.643W	009			3.0 ML FVO			613			052 85	93.	
FVO	1975	09	11	10	39	26.2	19.826N	155.752W	012			3.1 ML FVO			613			052 85	91.	
FVO	1975	09	12	20	15	41.3	19.883N	155.653W	010			3.0 ML FVO			613			052 85	93.	
FVO	1975	09	13	13	14	16.4	19.874N	155.651W	011			3.0 ML FVO			613			052 85	93.	
FVO	1975	09	07	16	31	41.1	19.715N	155.747W	011			3.0 ML FVO			613			052 85	91.	
FVO	1975	09	11	13	34	13.5	19.830N	155.643W	009			3.6 ML FVO			613			052 95	7.	
FVO	1975	09	11	14	43	55.3	19.830N	155.761W	012			3.1 ML FVO			613			052 85	127.	
FVO	1975	09	16	13	34	15.1	19.861N	155.498W	042			3.1 ML FVO		E	613			052 95	46.	
FVO	1975	09	19	13	10	59.3	19.341N	155.611W	009			3.0 ML FVO			613			052 95	82.	
FVO	1975	09	19	19	24	20.0	19.342N	155.635W	010			3.1 ML FVO			613			052 95	44.	
FVO	1975	09	21	14	46	05.2	19.337N	155.628W	010			3.2 ML FVO		E	613			052 95	72.	
FVO	1975	09	22	12	10	07.1	19.396N	155.435W	009			3.4 ML FVO			613			052 95	46.	
FVO	1975	09	25	01	39	00.7	19.258N	155.498W	041			3.0 ML FVO		E	613			052 95	46.	
FVO	1975	09	26	10	35	30.7	19.987N	155.671W	015			3.9 ML FVO			613			052 95	83.	
FVO	1975	09	33	14	33	35.4	19.348N	155.656W	011			3.0 ML FVO		E	613			052 95	30.	
FVO	1975	10	01	31	34	39.6	19.319N	155.725W	010			3.7 ML FVO			613			052 95	71.	

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPT (KM)	-----MAGNITUDES-----				INT FENOM MAX DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
***V INDICATES A POSSIBLE DUPLICATE																				
FVO	1975	10	02	14	17	49.9	18.445N	156.724W	073											
FVO	1975	10	04	14	05	38.0	19.276N	155.399W	008											
FVO	1975	10	10	13	22	14.5	19.497N	155.666W	017											
FVO	1975	10	13	16	17	37.1	19.282N	156.205W	043											
FVO	1975	10	19	01	05	46.5	19.142N	155.588W	031											
FVO	1975	10	22	12	39	13.9	19.769N	155.387W	017											
FVO	1975	10	22	16	52	54.9	18.933N	155.290W	012											
FVO	1975	10	26	23	37	40.3	19.320N	155.472W	010											
FVO	1975	10	27	19	23	37.8	18.916N	155.278W	010											
FVO	1975	10	27	19	35	52.9	19.315N	155.223W	010											
FVO	1975	10	30	17	47	34.9	18.919N	155.287W	021											
FVO	1975	10	31	04	50	53.8	19.200N	155.642W	009											
FVO	1975	11	01	10	22	04.0	18.931N	155.294W	012											
FVO	1975	11	02	19	25	31.2	18.809N	155.285W	016											
FVO	1975	11	06	02	05	20.2	19.340N	155.312W	030											
FVO	1975	11	06	03	21	11.5	19.340N	155.311W	031											
FVO	1975	11	06	04	02	50.3	19.334N	155.312W	030											
SS	1975	11	06	12	10	23.0H	19.410N	155.300W	025											
SS	1975	11	06	13	21	19.0H	19.410N	155.300W	025											
SS	1975	11	06	14	02	57.0H	19.410N	155.300W	025											
FVO	1975	11	07	15	12	14.4	19.405N	155.276W	024											
FVO	1975	11	08	04	54	36.5	19.294N	155.670W	013											
FVO	1975	11	09	14	27	48.5	18.948N	155.507W	054											
FVO	1975	11	10	01	26	31.1	19.358N	155.336W	019											
SS	1975	11	10	11	24	21.7H	19.400N	155.280W	007											
FVO	1975	11	11	03	09	12.3	19.358N	155.280W	017											
FVO	1975	11	13	23	02	04.9	19.358N	155.280W	009											
FVO	1975	11	14	11	03	28.7	19.340N	155.341W	032											
FVO	1975	11	14	11	51	45.9	19.301N	155.410W	035											
FVO	1975	11	14	07	53	43.9	18.746N	155.586W	039											
FVO	1975	11	15	12	53	21.2	19.320N	155.224W	011											
FVO	1975	11	15	13	10	02.0	19.378N	155.163W	009											
FVO	1975	11	20	13	41	44.2	19.550N	155.613W	009											
FVO	1975	11	23	11	43	14.3	19.420N	155.274W	014											
FVO	1975	11	27	02	21	15.4	19.300N	155.271W	013											
FVO	1975	11	27	07	37	34.6	20.040N	156.492W	011											
FVO	1975	11	27	16	15	41.6	19.310N	155.472W	009											
FVO	1975	11	29	01	00	00.0	19.144N	155.286W	026											
FVO	1975	11	29	01	54	04.1	19.378N	155.187W	031											
FVO	1975	11	29	04	40	13.5	19.340N	155.179W	016											
FVO	1975	11	29	09	13	20.2	19.257N	155.263W	035											
FVO	1975	11	29	09	25	12.1	19.377N	154.995W	019											
FVO	1975	11	29	09	35	24.3	19.360N	154.924W	000											
FVO	1975	11	29	09	35	56.8	19.307N	155.350W	000											
FVO	1975	11	29	09	51	10.1	19.348N	155.152W	010											
FVO	1975	11	29	09	56	34.3	19.243N	155.376W	004											
FVO	1975	11	29	10	00	45.5	19.391N	155.054W	006											
FVO	1975	11	29	10	13	23.3	19.265N	155.331W	006											
FVO	1975	11	29	10	13	05.2	19.354N	155.250W	010											
FVO	1975	11	29	10	33	19.6	19.233N	154.310W	060											

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SOURCE	YEAR	MO	DA	HR	MM	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT	PHENOM	RM	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL								
**N INDICATES A POSSIBLE DUPLICATE																					
FVO	1975	11	29	10	45	11.0	19.322N	155.345W	001												59.
FVO	1975	11	29	11	01	09.1	19.322N	155.115W	006					E	613						12.
FVO	1975	11	29	11	09	58.7	19.128N	154.845W	019						613						116.
FVO	1975	11	29	11	38	17.9	19.435N	155.445W	026					E	613						46.
FVO	1975	11	29	11	51	38.7	19.345N	154.979W	031						613						96.
FVO	1975	11	29	12	05	51.9	19.374N	155.006W	012						613						92.
FVO	1975	11	29	12	22	27.5	19.267N	155.366W	008						613						58.
FVO	1975	11	29	12	24	27.0	19.279N	155.365W	007						613						56.
FVO	1975	11	29	12	29	12.9	19.329N	155.343W	003					E	613						59.
FVO	1975	11	29	12	40	54.2	19.398N	155.049W	008						613						88.
FVO	1975	11	29	13	29	23.1	19.061N	155.202W	010						613						83.
SS	1975	11	29	13	35	40.5P	19.360N	155.53W	009	*5.F MB	5.1MS				613	F	197				11.
FVO	1975	11	29	14	12	59.7	19.424N	154.974W	007						613						95.
FVO	1975	11	29	14	14	33.3	19.333N	155.062W	009					E	613						67.
FVO	1975	11	29	14	40	46.1	19.397N	155.122W	007						613						91.
SS	1975	11	29	14	47	41.4P	19.334N	155.104W	005	*6.C MB	7.1MS7.20FAS			I)	DT VL	613	C	211			91.
FVO	1975	11	29	15	17	03.5	19.370N	155.062W	005						613						11.
FVO	1975	11	29	15	29	48.7	19.345N	155.070W	007					E	613						86.
FVO	1975	11	29	15	30	54.3	19.331N	155.060W	009						613						57.
FVO	1975	11	29	15	31	51.0	19.316N	155.055W	006						613						92.
FVO	1975	11	29	16	07	07.1	19.378N	155.059W	001						613						91.
FVO	1975	11	29	16	24	24.3	19.414N	155.400W	009					E	613						51.
FVO	1975	11	29	16	45	57.3	19.445N	155.355W	008						613						67.
FVO	1975	11	29	17	33	40.9	19.321N	155.109W	008						613						83.
FVO	1975	11	29	17	37	22.9	19.410N	155.003W	004						613						92.
FVO	1975	11	29	17	45	18.2	19.377N	154.914W	006						613						94.
FVO	1975	11	29	18	17	51.7	19.397N	154.988W	006						613						94.
SS	1975	11	29	18	43	59.2P	19.147N	155.215W	012	*4.9 MB					613		19				70.
FVO	1975	11	29	18	50	56.3	19.433N	155.113W	008						613						61.
FVO	1975	11	29	18	58	26.5	19.375N	154.881W	007						613						105.
FVO	1975	11	29	19	05	21.0	19.357N	155.182W	006					E	613						71.
FVO	1975	11	29	19	17	21.5	19.470N	155.413W	026					E	613						49.
FVO	1975	11	29	19	17	23.2	19.107N	155.205W	009						613						75.
FVO	1975	11	29	19	30	31.5	19.203N	155.315W	004						613						59.
FVO	1975	11	29	20	15	27.3	19.425N	155.374W	010					E	613						54.
FVO	1975	11	29	20	40	51.6	19.296N	155.076W	002						613						17.
**1 FVO	1975	11	29	21	07	04.7	19.334N	155.316W	010						613						61.
**2 FVO	1975	11	29	21	09	13.5	19.279N	155.367W	007						613						61.
FVO	1975	11	29	21	54	33.9	19.377N	155.091W	007					E	613						13.
FVO	1975	11	29	22	01	26.1	19.346N	154.860W	005						613						107.
FVO	1975	11	29	23	42	59.1	19.445N	154.916W	005						613						102.
FVO	1975	11	30	00	13	47.7	19.437N	155.402W	009						613						50.
FVO	1975	11	30	03	01	31.7	19.346N	155.163W	009						613						78.
FVO	1975	11	30	03	13	03.0	19.356N	155.131W	009						613						79.
FVO	1975	11	30	03	28	27.1	19.428N	154.908W	009						613						102.
FVO	1975	11	30	04	41	04.5	19.343N	155.018W	006					E	613						91.
FVO	1975	11	30	05	09	20.7	19.369N	155.061W	006					E	613						87.
FVO	1975	11	30	05	45	24.6	19.354N	155.064W	007					E	613						87.
FVO	1975	11	30	07	00	47.4	19.354N	155.334W	009					E	613						59.
FVO	1975	11	30	07	27	22.0	19.356N	155.111W	007					E	613						62.

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT PHENOM MAX DTSVNO	RN	CE	Q/S	PAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
*** INDICATES A POSSIBLE DUPLICATE																				
HVO	1975	11	30	09	49	37.0	19.393N	154.960W	006											
HVO	1975	11	30	10	04	46.1	19.453N	154.864W	009											
FVJ	1975	11	30	10	32	54.0	19.361N	155.255W	010											
HVO	1975	11	30	10	47	14.5	19.360N	154.945W	003											
HVO	1975	11	30	14	08	38.9	19.332N	155.211W	008											
HVO	1975	11	30	14	10	11.0	19.403N	155.059W	001											
HVO	1975	11	30	17	20	24.4	19.363N	155.081W	004											
FVJ	1975	11	30	19	21	09.5	19.367N	155.254W	010											
HVO	1975	11	30	20	57	14.3	19.377N	155.050W	006											
HVO	1975	11	30	22	40	42.1	19.333N	155.059W	005											
HVO	1975	11	30	22	51	00.8	19.365N	155.120W	008											
FVJ	1975	12	01	10	41	35.5	19.407N	155.051W	000											
HVO	1975	12	01	02	31	54.3	19.407N	154.960W	006											
HVO	1975	12	01	04	31	19.4	19.331N	155.125W	001											
HVO	1975	12	01	07	06	26.2	19.360N	154.977W	008											
HVO	1975	12	01	08	24	27.6	19.275N	155.101W	007											
FVJ	1975	12	01	11	01	23.0	19.447N	155.477W	010											
HVO	1975	12	01	11	09	10.0	19.391N	154.979W	009											
HVO	1975	12	01	11	19	03.2	19.361N	155.104W	009											
FVJ	1975	12	01	16	37	7.5	19.398N	154.990W	001											
FVJ	1975	12	01	18	33	14.4	19.347N	155.115W	004											
HVO	1975	12	02	03	15	47.1	19.362N	155.055W	009											
HVO	1975	12	02	05	43	54.3	19.454N	154.872W	010											
HVO	1975	12	02	06	21	29.0	19.260N	155.197W	009											
HVO	1975	12	02	07	04	16.3	19.311N	155.147W	009											
FVJ	1975	12	02	08	11	14.3	19.375N	155.129W	007											
HVO	1975	12	02	11	14	46.4	19.365N	154.993W	009											
HVO	1975	12	02	14	01	14.5	19.314N	155.303W	006											
HVO	1975	12	02	16	07	22.6	19.374N	155.323W	007											
FVJ	1975	12	02	22	32	45.4	19.351N	154.743W	006											
HVO	1975	12	03	02	06	55.2	19.311N	155.347W	010											
HVO	1975	12	03	04	03	09.6	19.430N	155.390W	010											
SS	1975	12	03	05	07	17.74	19.375N	154.983W	001											
FVJ	1975	12	03	05	10	35.6	19.322N	155.170W	010											
FVJ	1975	12	03	05	31	01.0	19.394N	154.915W	006											
SS	1975	12	03	06	27	56.64	19.342N	155.065W	005											
SS	1975	12	03	06	43	53.34	19.315N	155.337W	008											
HVO	1975	12	03	07	03	13.0	19.310N	155.316W	010											
FVJ	1975	12	03	11	17	44.3	19.347N	155.444W	004											
HVO	1975	12	03	11	18	23.0	19.351N	154.943W	005											
HVO	1975	12	03	12	33	46.6	19.341N	155.342W	005											
HVO	1975	12	03	12	51	23.0	19.372N	155.029W	007											
HVO	1975	12	03	13	12	44.3	19.240N	155.410W	012											
FVJ	1975	12	03	17	46	26.6	19.395N	154.971W	006											
HVO	1975	12	03	21	27	56.3	19.332N	155.082W	004											
HVO	1975	12	03	21	43	54.0	19.315N	155.337W	009											
HVO	1975	12	04	01	04	03.2	19.399N	154.981W	005											
FVJ	1975	12	04	01	14	04.3	19.379N	154.931W	009											
FVJ	1975	12	04	01	41	33.7	19.332N	155.280W	009											
HVO	1975	12	04	07	33	37.4	19.344N	155.045W	005											

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SOURCE	YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT PHENOM MAX DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
*** INDICATES A POSSIBLE DUPLICATE																				
HVO	1975	12	04	10	35	11.3	19.394N	154.950W	005											98.
HVO	1975	12	04	11	19	46.8	19.366N	155.080W	007											85.
HVO	1975	12	04	11	39	10.1	19.350N	154.963W	006											97.
HVO	1975	12	04	14	21	52.8	19.441N	154.867W	009											100.
HVO	1975	12	04	17	32	17.3	19.353N	155.078W	008											85.
HVO	1975	12	04	21	04	31.3	19.378N	155.103W	008											82.
HVO	1975	12	04	21	56	54.3	19.366N	155.003W	006											93.
HVO	1975	12	05	10	09	06.5	19.367N	155.252W	010											67.
HVO	1975	12	05	12	20	47.2	19.361N	155.122W	008											81.
HVO	1975	12	05	19	11	55.2	19.289N	155.355W	009											59.
HVO	1975	12	06	01	37	59.1	19.397N	154.593W	007											95.
HVO	1975	12	06	03	50	26.3	19.335N	155.291W	006											64.
HVO	1975	12	06	13	13	48.4	19.379N	155.031W	007											90.
HVO	1975	12	06	19	10	09.0	19.337N	155.122W	010											81.
HVO	1975	12	07	03	47	20.4	19.361N	155.058W	010											66.
HVO	1975	12	07	12	19	00.5	19.275N	155.202W	006											74.
HVO	1975	12	07	17	53	45.3	19.445N	154.824W	008											111.
HVO	1975	12	08	11	00	33.4	19.473N	155.149W	028											77.
HVO	1975	12	08	12	24	51.1	19.313N	155.347W	010											59.
HVO	1975	12	08	18	35	52.6	19.477N	154.841W	028											109.
HVO	1975	12	08	19	00	54.1	19.355N	155.059W	014											66.
HVO	1975	12	08	19	00	39.6	19.372N	155.032W	008											89.
HVO	1975	12	08	19	00	43.7	19.333N	155.116W	005											82.
HVO	1975	12	08	19	07	31.0	19.365N	155.115W	010											81.
HVO	1975	12	08	22	00	45.7	19.334N	155.113W	009											82.
HVO	1975	12	09	02	54	13.1	19.371N	155.067W	006											86.
HVO	1975	12	09	07	00	00.1	19.361N	155.052W	010											67.
HVO	1975	12	09	09	32	41.3	19.345N	155.047W	009											59.
HVO	1975	12	09	10	10	01.3	19.317N	155.121W	008											81.
HVO	1975	12	09	13	10	52.9	19.349N	155.105W	010											82.
HVO	1975	12	09	13	34	37.0	19.346N	155.016W	011											15.
HVO	1975	12	09	13	50	54.5	19.361N	155.127W	009											80.
HVO	1975	12	10	11	14	37.0	19.365N	155.423W	011											50.
HVO	1975	12	10	11	30	30.7	19.350N	155.099W	010											83.
HVO	1975	12	10	15	42	16.9	19.334N	155.201W	010											73.
HVO	1975	12	11	03	57	11.3	19.351N	155.075W	009											86.
HVO	1975	12	11	05	41	19.1	19.365N	155.119W	009											81.
HVO	1975	12	11	10	20	50.6	19.391N	155.057W	009											67.
HVO	1975	12	11	13	10	43.1	19.397N	155.062W	007											87.
HVO	1975	12	12	05	30	04.5	19.353N	155.136W	009											79.
HVO	1975	12	12	06	51	07.7	19.375N	155.040W	007											89.
HVO	1975	12	13	01	01	56.3	19.377N	155.053W	008											87.
HVO	1975	12	13	11	17	43.0	19.377N	154.832W	007											149.
HVO	1975	12	14	01	40	00.8	19.344N	155.109W	009											82.
HVO	1975	12	14	11	47	07.4	19.365N	155.052W	009											67.
HVO	1975	12	14	14	09	27.2	19.312N	155.046W	010											59.
HVO	1975	12	15	14	20	00.8	19.393N	154.969W	007											56.
HVO	1975	12	16	05	43	17.2	19.416N	155.015W	007											70.
HVO	1975	12	17	01	40	25.8	19.445N	154.858W	008											108.
HVO	1975	12	17	05	45	54.5	19.363N	155.116W	009											81.

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	L (M)	DEPTH (KM)	-----MAGNITUDES-----				INT (MAX)	FENOM DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL								
**N INDICATES A POSSIBLE DUPLICATE																					
HVO	1975	12	17	09	54	30.2	19.363N	155.256W	009												
HVO	1975	12	19	09	13	43.4	19.430N	155.473W	010												
HVO	1975	12	19	16	42	22.4	19.306N	155.346W	009												
HVO	1975	12	19	18	04	16.3	19.434N	155.276W	017												
HVO	1975	12	20	14	14	57.3	19.359N	155.046W	009												
HVO	1975	12	20	23	30	44.5	19.381N	155.029W	007												
HVO	1975	12	21	17	45	39.6	19.290N	155.353W	010												
HVO	1975	12	23	13	50	55.6	19.342N	155.129W	010												
HVO	1975	12	23	04	04	13.6	19.359N	155.041W	008												
HVO	1975	12	23	06	19	33.3	19.392N	155.173W	009												
HVO	1975	12	23	09	58	37.4	19.211N	155.472W	011												
HVO	1975	12	23	13	12	51.1	19.211N	155.470W	010												
HVO	1975	12	23	16	41	42.1	19.406N	155.291W	013												
HVO	1975	12	23	16	47	06.1	19.406N	155.301W	013												
HVO	1975	12	23	18	41	47.1	19.365N	155.115W	009												
HVO	1975	12	24	00	44	34.4	19.357N	155.077W	009												
HVO	1975	12	24	04	31	39.4	19.275N	155.011W	010												
HVO	1975	12	24	10	43	45.6	19.435N	154.827W	008												
HVO	1975	12	25	11	26	48.2	19.342N	155.054W	010												
HVO	1975	12	26	04	31	21.4	19.452N	155.031W	011												
HVO	1975	12	26	09	27	18.4	19.342N	155.120W	016												
HVO	1975	12	26	13	30	54.2	19.371N	155.116W	009												
HVO	1975	12	26	20	53	57.2	19.365N	155.055W	010												
HVO	1975	12	26	22	05	24.9	17.941N	155.022W	039												
HVO	1975	12	27	02	32	52.4	19.287N	155.369W	013												
HVO	1975	12	27	07	19	31.3	19.371N	155.195W	008												
SS	1975	12	27	08	00	24.0	20.021N	156.303W	030												
HVO	1975	12	27	18	57	30.5	19.382N	155.111W	008												
HVO	1975	12	27	18	30	02.2	19.434N	155.476W	009												
HVO	1975	12	30	09	20	41.9	19.377N	155.120W	039												
HVO	1975	12	31	08	47	43.7	19.500N	155.273W	026												
HVO	1975	12	31	09	34	14.3	19.360N	155.040W	007												
HVO	1975	01	01	00	32	48.1	19.335N	155.176W	017												
HVO	1975	01	01	06	54	15.9	18.674N	155.147W	056												
HVO	1975	01	01	18	36	47.3	19.362N	155.051W	009												
HVO	1975	01	05	03	17	44.1	19.356N	155.012W	007												
HVO	1975	01	06	00	43	37.6	19.300N	155.346W	005												
HVO	1975	01	06	12	04	52.1	19.465N	154.754W	009												
HVO	1975	01	07	00	16	31.4	19.211N	155.044W	016												
HVO	1975	01	07	01	44	53.1	19.453N	154.817W	008												
HVO	1975	01	07	11	38	07.9	19.371N	155.195W	018												
HVO	1975	01	08	02	22	03.4	19.754N	156.142W	004												
HVO	1975	01	10	14	07	04.3	19.346N	155.110W	009												
HVO	1975	01	11	14	05	40.2	19.513N	155.073W	024												
SS	1975	01	11	22	26	15.0	20.021N	156.303W	010												
SS	1975	01	12	00	05	39.0	19.300N	155.300W	031												
HVO	1975	01	12	03	49	22.9	19.365N	155.111W	009												
HVO	1975	01	12	03	06	21.8	19.340N	155.115W	009												
HVO	1975	01	14	08	03	27.6	19.370N	155.109W	009												
HVO	1975	01	15	12	41	45.5	19.480N	155.043W	014												
										4.5 MR		4.2MS									
HVO	1975	01	12	03	49	22.9	19.365N	155.111W	009												
HVO	1975	01	12	03	06	21.8	19.340N	155.115W	009												
HVO	1975	01	14	08	03	27.6	19.370N	155.109W	009												
HVO	1975	01	15	12	41	45.5	19.480N	155.043W	014												

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SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES			INT (MA)	PHENOM DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTTER								
***N INDICATES A POSSIBLE DUPLICATE																				
HVO	1976	01	15	12	59	26.1	19.411N	155.293W	016											
GS	1976	01	15	22	59	24.0F	19.382N	155.300W	030	4.8 MB										
HVO	1976	01	16	19	29	13.8	19.375N	155.169W	008											
HVO	1976	01	16	20	00	03.9	19.355N	154.994W	002											
GS	1976	01	17	05	29	13.0F	19.360N	155.160W	005											
HVO	1976	01	18	04	49	28.4	19.362N	155.255W	010											
HVO	1976	01	18	14	05	10.9	19.363N	155.117W	009											
HVO	1976	01	18	14	13	37.9	19.361N	155.127W	007											
HVO	1976	01	18	23	57	46.5	19.375N	155.099W	007											
HVO	1976	01	21	05	22	17.7	19.365N	155.112W	008											
HVO	1976	01	21	11	41	21.2	19.367N	155.120W	008											
HVO	1976	01	23	02	47	46.1	19.361N	155.093W	009											
HVO	1976	01	23	08	20	14.1	19.364N	155.132W	009											
HVO	1976	01	26	18	55	51.7	19.410N	154.911W	007											
HVO	1976	01	27	05	35	51.4	19.373N	155.173W	009											
HVO	1976	01	27	22	26	29.2	19.355N	155.111W	009											
HVO	1976	01	29	02	07	24.3	19.393N	155.026W	010											
HVO	1976	01	29	05	07	54.2	19.344N	155.161W	009											
HVO	1976	01	29	10	15	56.5	19.370N	154.994W	009											
GS	1976	01	29	21	19	58.0F	19.410N	155.100W	005	4.5 MB										
HVO	1976	01	31	04	32	10.0	19.444N	155.376W	009											
HVO	1976	01	31	21	17	27.7	19.369N	155.151W	008											
HVO	1976	02	03	16	42	13.8	19.371N	155.189W	009											
HVO	1976	02	03	21	50	55.5	19.361N	155.253W	010											
HVO	1976	02	05	11	43	04.5	19.357N	155.135W	009											
HVO	1976	02	05	19	18	16.7	19.341N	155.119W	009											
HVO	1976	02	07	02	48	10.3	19.330N	155.124W	007											
HVO	1976	02	10	16	18	28.2	19.341N	155.154W	007											
HVO	1976	02	13	07	48	51.4	19.332N	155.162W	010											
HVO	1976	02	20	19	01	14.9	19.410N	156.120W	030											
GS	1976	02	21	05	51	13.8	20.280N	156.267W	033N	4.9 MB 4.0MS										
HVO	1976	02	23	09	45	13.5	19.361N	155.094W	009											
HVO	1976	02	24	05	51	14.2	19.371N	155.111W	009											
HVO	1976	02	24	14	43	30.6	19.346N	155.080W	008											
HVO	1976	02	24	19	18	31.6	19.352N	155.133W	009											
HVO	1976	02	25	13	48	20.4	19.370N	155.166W	009											
HVO	1976	02	28	03	55	28.9	19.374N	155.176W	009											
HVO	1976	03	01	19	41	54.9	19.354N	155.110W	009											
HVO	1976	03	06	12	23	14.4	19.360N	155.135W	006											
HVO	1976	03	07	07	40	14.1	19.361N	155.210W	010											
HVO	1976	03	07	16	25	34.6	19.361N	155.120W	007											
HVO	1976	03	10	21	41	14.2	20.077N	155.582W	026											
HVO	1976	03	11	24	02	40.2	19.360N	155.050W	010											
HVO	1976	03	12	21	17	17.3	19.371N	154.846W	009											
HVO	1976	03	13	08	16	16.4	19.345N	155.080W	011											
HVO	1976	03	13	20	20	01.8	19.324N	155.084W	012											
HVO	1976	03	19	13	24	30.3	19.356N	155.057W	009											
HVO	1976	03	23	13	13	19.9	19.331N	155.109W	009											
HVO	1976	03	21	09	31	33.5	19.371N	155.094W	010											
HVO	1976	03	21	20	31	24.6	19.337N	155.144W	008											

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SOURCE	YEAR	MO	DA	HR	MM	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT MAX	F-PHENOM DTSVNO	RN	CE	Q/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHR	LOCAL								
**N INDICATES A POSSIBLE DUPLICATE																					
HVO	1975	03	22	20	43	26.9	19.364N	155.084W	009												
HVO	1975	03	22	21	19	55.7	19.341N	155.111W	010												
HVO	1975	03	23	15	06	03.2	19.314N	155.306W	009												
HVO	1975	03	29	05	09	53.0	19.364N	155.253W	010												
HVO	1975	03	29	08	31	23.8	19.431N	155.257W	013												
HVO	1975	03	32	14	52	10.3	19.334N	155.122W	010												
HVO	1975	04	02	08	14	06.5	19.344N	155.100W	009												
HVO	1975	04	02	09	14	11.7	19.643N	155.899W	007												
HVO	1975	04	02	09	55	03.3	19.331N	155.216W	008												
GS	1975	04	02	18	14	06.0H	19.400N	155.100W	005	4.5 MB											
HVO	1975	04	03	01	43	42.2	19.345N	155.284W	004												
HVO	1975	04	06	03	12	52.1	19.343N	155.209W	009												
HVO	1975	04	08	10	54	22.2	19.141N	155.281W	005												
HVO	1975	04	11	15	35	43.2	19.348N	155.254W	005												
HVO	1975	04	12	07	25	23.5	19.316N	155.350W	009												
HVO	1975	04	14	22	01	34.1	19.451N	154.865W	008												
HVO	1975	04	20	17	11	13.1	19.372N	155.254W	010												
HVO	1975	04	21	18	13	24.5	19.755N	155.105W	050												
GS	1975	04	22	14	13	06.3	19.068N	155.172W	033N												
HVO	1975	04	22	15	54	34.9	19.025N	155.211W	012												
HVO	1975	04	24	11	33	01.0	19.310N	155.344W	010												
HVO	1975	04	23	12	24	54.8	19.165N	155.266W	009												
HVO	1975	04	26	21	44	41.5	19.348N	155.283W	005												
HVO	1975	05	01	18	52	04.9	19.377N	155.351W	007												
HVO	1975	05	10	20	43	57.4	19.115N	155.531W	060												
HVO	1975	05	12	06	14	43.4	19.340N	155.133W	017												
HVO	1975	05	13	03	07	04.5	19.308N	155.258W	008												
HVO	1975	05	12	05	05	11.6	19.355N	155.194W	005												
HVO	1975	05	14	09	13	42.2	19.200N	155.505W	010												
HVO	1975	05	17	01	45	26.1	19.330N	155.271W	010												
HVO	1975	05	17	03	54	44.2	19.329N	155.143W	010												
HVO	1975	05	17	21	36	19.0	19.340N	155.377W	007												
HVO	1975	05	14	06	16	41.3	19.325N	155.125W	009												
HVO	1975	05	19	17	12	05.5	19.310N	155.104W	009												
HVO	1975	05	21	14	39	45.0	19.353N	155.201W	011												
HVO	1975	05	21	12	53	05.6	19.351N	155.101W	009												
HVO	1975	05	22	18	52	04.4	19.351N	155.252W	011												
HVO	1975	05	23	17	31	21.2	19.341N	155.114W	009												
HVO	1975	05	25	02	33	07.0	19.473N	155.472W	009												
HVO	1975	05	28	12	00	45.5	19.344N	155.351W	008												
HVO	1975	05	31	06	07	21.1	20.246N	155.603W	032												
HVO	1975	05	31	08	32	10.0	20.244N	155.770W	003												
HVO	1975	05	31	08	53	53.7	20.147N	155.813W	029												
HVO	1975	05	31	09	55	53.3	20.114N	155.806W	025												
HVO	1975	05	31	15	15	16.4	19.649N	155.849W	002												
HVO	1975	06	04	22	53	51.3	19.359N	155.119W	009												
HVO	1975	06	06	03	45	14.9	19.322N	155.273W	010												
HVO	1975	06	07	10	39	37.6	19.319N	155.261W	031												
HVO	1975	06	10	09	15	03.9	19.335N	155.122W	008												
HVO	1975	06	10	22	05	02.2	19.336N	155.142W	010												

11/07/77.

SOURCE YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT MAX	FFENOP DTSVNO	RM	CE	G/S	MAR	DG	DIST (KM)
									BODY	SURF	OTHER	LOCAL								
**N INDICATES	A POSSIBLE DUPLICATE																			
FVO 1976	06	12	12	42	15.5	19.338N	155.134W	009												60.
FVO 1976	06	13	14	21	41.0	19.337N	155.137W	009												79.
FVO 1976	06	14	14	17	15.2	19.404N	155.264W	004				E								65.
FVO 1976	06	15	05	10	32.5	19.407N	155.460W	010												42.
FVO 1976	06	16	09	17	15.9	19.364N	155.081W	008												55.
FVO 1976	06	18	12	01	11.6	19.376N	155.101W	006												83.
FVO 1976	06	18	12	01	11.6	19.376N	155.101W	006												67.
FVO 1976	06	20	00	25	11.3	19.392N	155.251W	005				E								47.
FVO 1976	06	20	03	06	23.0	19.191N	155.547W	011												71.
FVO 1976	06	21	18	16	27.2	19.369N	155.215W	005												70.
FVO 1976	06	21	19	03	34.1	19.371N	155.219W	006				E								71.
FVO 1976	06	21	19	36	29.9	19.366N	155.216W	006												70.
FVO 1976	06	21	20	00	34.7	19.370N	155.221W	005												84.
FVO 1976	06	21	20	13	12.0	19.390N	155.184W	009				E								64.
FVO 1976	06	21	21	27	29.0	19.396N	155.247W	003												109.
FVO 1976	06	21	23	55	31.1	19.475N	154.840W	001				E								66.
FVO 1976	06	22	03	04	30.6	19.377N	155.241W	001												66.
FVO 1976	06	22	03	01	39.3	19.368N	155.243W	005												73.
FVO 1976	06	24	13	47	53.9	19.330N	155.188W	005												67.
FVO 1976	06	24	24	45	51.0	19.400N	155.341W	013												67.
FVO 1976	06	24	25	17	47.3	19.400N	155.341W	007				E								67.
FVO 1976	07	01	08	17	43.0	19.401N	155.341W	005												16.
FVO 1976	07	03	01	4	43.0	19.340N	155.055W	009												67.
FVO 1976	07	06	13	45	48.1	19.341N	155.112W	006				E								82.
FVO 1976	07	09	17	02	19.7	19.340N	155.120W	011												70.
FVO 1976	07	10	21	00	24.1	19.340N	155.120W	011												70.
FVO 1976	07	11	23	24	10.8	19.350N	155.223W	009												67.
FVO 1976	07	12	12	45	35.2	19.345N	155.246W	004												54.
FVO 1976	07	13	16	4	55.7	19.154N	155.481W	047												64.
FVO 1976	07	14	02	15	12.4	19.397N	155.241W	005												71.
FVO 1976	07	14	14	14	28.1	19.378N	155.213W	005				E								60.
FVO 1976	07	15	06	54	38.1	19.361N	155.121W	001												46.
FVO 1976	07	16	11	11	28.4	19.176N	155.044W	009				E								61.
FVO 1976	07	16	03	31	25.6	19.331N	155.127W	009												80.
FVO 1976	07	19	01	51	16.1	19.332N	155.187W	010				E								65.
FVO 1976	07	22	02	40	51.1	19.377N	155.17 W	009												67.
FVO 1976	07	22	01	43	45.4	19.396N	155.048W	005												79.
FVO 1976	07	23	19	32	17.1	19.334N	155.140W	010				E								41.
FVO 1976	07	24	02	20	14.7	19.283N	155.592W	010												27.
FVO 1976	07	24	03	4	31.0	19.408N	155.046W	005				E								65.
FVO 1976	07	27	17	14	26.9	19.311N	155.142W	009												61.
FVO 1976	07	27	21	57	12.7	19.392N	155.243W	005												51.
FVO 1976	07	28	16	3	19.6	19.396N	155.099W	010												62.
FVO 1976	07	30	05	02	41.7	19.347N	155.111W	009				E								73.
FVO 1976	07	31	03	19	14.1	19.331N	155.203W	009												67.
FVO 1976	07	31	05	00	24.0	19.191N	155.246W	005				E								65.
FVO 1976	07	31	16	51	36.1	19.405N	155.264W	005												68.
FVO 1976	07	31	11	01	33.5	19.387N	155.242W	002				E								64.
FVO 1976	08	01	15	01	17.5	19.364N	155.068W	001												67.
FVO 1976	08	01	16	35	12.0	19.392N	155.24 W	006												67.
FVO 1976	08	02	06	57	11.4	19.394N	155.252W	010				E								72.
FVO 1976	08	03	03	3	17.1	19.393N	155.210W	009												

SOURCE YEAR	MO	DA	HR	MIN	SEC	LAT	LONG	DEPTH (KM)	MAGNITUDES	INT PHENOM	RN	CE	G/S	MA: I DG	DIST (KM)

									BODY SURF OTHER LOCAL	MAX	DTSVNO				
***V INDICATES A POSSIBLE DUPLICATE															
HVO	1976	11	12	16	54	48.5	19.356N	155.241W	007						19.
HVO	1976	11	12	20	07	21.5	19.944N	155.600W	011						61.
HVO	1976	11	13	11	14	03.4	19.366N	155.385W	009						64.
HVO	1976	11	14	04	19	23.1	19.425N	155.275W	015						64.
HVO	1976	11	16	02	23	35.4	19.377N	155.378W	009						65.
HVO	1976	11	17	05	51	48.6	19.539N	155.236W	025						68.
HVO	1976	11	18	22	24	43.8	19.398N	155.282W	004						63.
HVO	1976	11	23	14	12	16.0	20.108N	155.835W	017						78.
HVO	1976	11	26	10	15	58.5	19.404N	155.265W	004						65.
HVO	1976	11	30	17	46	17.1	19.324N	155.190W	009						74.
HVO	1976	11	30	18	18	45.3	19.322N	155.186W	010						75.
HVO	1976	12	01	04	44	17.5	19.361N	155.254W	009						67.
HVO	1976	12	04	03	50	50.8	19.334N	155.136W	009						80.
HVO	1976	12	06	05	26	58.1	19.359N	155.127W	009						80.
HVO	1976	12	07	14	06	17.4	19.405N	155.295W	015						62.
HVO	1976	12	08	11	47	17.0	19.316N	155.444W	026						49.
HVO	1976	12	09	15	27	49.7	19.306N	155.387W	013						63.
HVO	1976	12	13	17	28	40.1	19.377N	155.124W	010						81.
HVO	1976	12	17	09	31	43.3	19.333N	155.115W	009						82.
HVO	1976	12	18	04	01	31.6	19.316N	155.117W	009						82.
HVO	1976	12	18	14	01	04.5	19.377N	155.118W	009						81.
HVO	1976	12	25	17	31	14.8	19.677N	156.146W	006						28.
HVO	1976	12	27	14	15	21.5	19.394N	155.246W	005						67.
HVO	1976	12	27	15	24	27.5	19.324N	155.276W	010						65.
HVO	1976	12	27	12	13	54.3	19.199N	155.634W	010						42.
HVO	1976	12	27	14	15	20.6	19.394N	155.247W	005						67.
HVO	1976	12	28	19	37	14.9	19.320N	155.293W	010						73.
HVO	1976	12	28	19	24	26.9	19.391N	155.242W	005						61.
HVO	1976	12	30	30	47	41.5	18.463N	155.335W	012						126.
HVO	1976	12	30	04	19	51.6	19.325N	155.286W	010						66.
HVO	1977	01	01	14	26	35.5	19.398N	155.120W	009						81.
HVO	1977	01	05	00	25	13.0	19.390N	155.250W	005						67.
HVO	1977	01	08	10	09	38.7	19.333N	155.133W	010						80.
HVO	1977	01	12	13	05	59.3	19.402N	155.290W	016						63.
HVO	1977	01	14	23	26	42.5	19.300N	155.106W	010						84.
HVO	1977	01	23	20	45	11.7	19.340N	155.200W	009						73.
HVO	1977	02	04	11	20	53.0	19.408N	155.100W	005						82.
HVO	1977	02	04	14	25	11.7	20.111N	155.470W	001						84.
HVO	1977	03	09	17	29	18.5	19.313N	155.517W	001						39.
HVO	1977	04	21	04	47	23.0	20.111N	155.333W	015						83.
HVO	1977	06	04	19	42	14.7	19.367N	155.283W	009						85.
HVO	1977	07	05	17	59	42.0	19.429N	155.453W	017						45.
HVO	1977	08	01	07	54	20.3	19.340N	155.222W	017						71.
HVO	1977	08	11	05	19	16.7	19.322N	155.195W	009						74.
HVO	1977	08	19	18	19	13.4	19.337N	155.192W	010						81.
HVO	1977	09	30	12	46	21.5	19.377N	155.455W	017						46.
HVO	1977	09	07	23	51	07.7	19.367N	155.317W	009						60.
HVO	1977	09	16	14	51	16.0	19.390N	155.267W	001						86.
HVO	1977	09	19	14	01	45.0	19.408N	155.117W	005						81.
HVO	1977	09	23	10	05	44.0	19.367N	155.507W	010						88.

#1/07/17.

SOURCE	YEAR	PO	DA	HR	MN	SEC	LAT	LONG	DEPTH (KM)	-----MAGNITUDES-----				INT PHENOM MAX DTSVNO	RN	CE	G/S	MAR	DG	DIST (KM)
										BODY	SURF	OTHER	LOCAL							
**N INDICATES	A POSSIBLE DUPLICATE																			
SS	1973	04	08	02	43	44.2H	19.635N	155.144W	029											
SS	1973	05	23	07	09	26.7H	19.310N	155.223W	010											
SS	1973	06	03	01	02	02.1H	19.667N	155.163W	014											
SS	1973	06	13	02	49	35.0H	19.300N	155.467W	015											
SS	1973	06	13	16	54	01.2H	19.340N	155.653W	006											
SS	1973	06	21	13	23	44.1H	19.323N	155.221W	010											
SS	1973	06	23	11	47	59.6H	19.323N	155.056W	011	4.9 MB										
SS	1973	07	01	19	18	13.3	19.320N	155.120W	00											
SS	1973	08	31	23	07	21.4H	19.010N	155.481W	025	4.5 MB										
SS	1973	09	05	23	26	46.9H	19.330N	155.226W	010											
SS	1973	09	12	06	16	06.1H	19.330N	155.110W	010											
SS	1973	11	23	13	15	15.9H	19.233N	155.950W	011											
SS	1973	12	14	14	12	44.9H	19.320N	155.220W	010											
SS	1973	12	27	12	41	56.3H	19.331N	155.217W	010	4.6 MB										
SS	1973	02	14	2	52	51.0H	19.340N	155.010W	0											
SS	1973	03	08	04	07	05.0H	19.315N	155.270W	020	4.5 MB	4.3 MS									
SS	1973	03	11	13	52	19.6H	19.331N	155.110W	010	4.8 MB										
SS	1973	03	11	14	14	56.5H	19.331N	155.090W	011											
SS	1973	03	22	06	43	59.4H	20.040N	155.010W	012	4.6 MB										
SS	1973	04	01	07	03	11.0H	20.057N	155.801W	09	4.4 MB										
SS	1973	07	08	19	03	41.7H	19.750N	155.974W	020											
SS	1973	07	07	11	06	33.6H	19.327N	155.131W	0											
SS	1973	07	31	13	33	51.4H	19.466N	155.433W	010	4.5 MB										
SS	1973	08	14	12	51	42.2H	20.017N	156.263W	025	4.1 MB										
SS	1973	08	16	23	04	19.4H	19.377N	155.454W	011											
SS	1973	09	12	07	59	37.8H	19.347N	155.072W	09	5.7 MB	4.8 MS									
SS	1973	09	22	02	20	12.4H	19.343N	155.038W	09	4.8 MB										
SS	1973	09	27	15	33	48.5H	19.326N	155.120W	010	4.7 MB										
SS	1973	10	14	17	07	17.9H	19.900N	155.131W	014											
SS	1973	10	31	05	35	11.7H	19.174N	155.243W	01	4.1 MB										
SS	1973	10	06	1	52	27.2H	19.400N	155.471W	011											
SS	1973	10	14	3	44	03.1H	19.414N	155.416W	011											
SS	1973	01	20	1	24	43.8H	19.310N	155.541W	027											
SS	1973	01	22	05	31	21.4H	19.710N	156.195W	010											
SS	1973	02	12	12	57	52.7H	19.399N	155.236W	002	4.6 MB										
SS	1973	05	15	09	07	37.7H	19.220N	155.992W	011											
SS	1973	05	23	04	11	33.7H	19.341N	155.214W	033											
SS	1973	07	10	05	40	35.1H	19.433N	155.179W	010											
SS	1973	08	14	07	27	15.7H	19.350N	155.400W	011											
SS	1973	08	20	16	00	21.0H	19.601N	156.149W	025											
SS	1973	10	22	07	43	19.7H	19.366N	155.113W	001											
SS	1973	10	31	02	23	14.0H	19.480N	155.210W	021											
SS	1973	11	23	11	31	55.7H	19.361N	155.350W	009											

NUMBER OF HITS 2393
NUMBER OF SUSPECTED DUPLICATES 6

PREPARED BY THE NATIONAL GEOLOGICAL AND SOLAR-TERRESTRIAL DATA CENTER

ENVIRONMENTAL DATA SERVICE-----NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION

Appendix B. Earthquakes with M_L greater than or equal to 4.0 from January 1, 1977,
through December 31, 1979.

SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (km)	MAGNITUDE (M_L)
HVO	1977	01	14	13	26	42.38	19.33	155.12	9.93	4.6
HVO	1977	01	23	10	49	01.84	19.34	155.20	8.78	4.0
HVO	1977	01	29	22	48	49.72	19.36	155.08	9.07	4.1
HVO	1977	02	03	15	20	49.70	19.35	155.08	9.87	4.5
HVO	1977	03	09	00	29	17.40	19.42	155.50	44.21	4.0
HVO	1977	04	20	18	49	23.01	19.94	155.31	10.47	5.0
HVO	1977	04	22	09	44	00.12	19.32	155.26	10.10	4.0
HVO	1977	06	05	23	42	18.92	19.36	155.08	9.31	5.1
HVO	1977	07	05	07	59	42.03	19.44	155.45	11.89	4.1
HVO	1977	08	07	21	54	20.32	19.33	155.22	10.29	4.1
HVO	1977	08	13	12	24	28.46	20.16	155.61	4.61	4.1
HVO	1977	08	19	08	19	13.34	19.33	155.12	10.15	4.2
HVO	1977	09	07	13	51	06.71	19.38	155.32	31.26	4.5
HVO	1977	09	15	18	50	05.45	19.34	155.06	9.30	4.0
HVO	1977	09	19	09	01	45.11	19.36	155.13	8.77	4.0
HVO	1977	10	09	14	38	51.90	19.40	155.25	24.90	4.0
HVO	1978	04	07	16	43	43.29	19.87	155.13	39.27	4.0
HVO	1978	06	23	01	47	58.56	19.32	155.26	10.51	4.4
HVO	1978	07	01	09	18	13.27	19.31	155.11	7.97	4.2
HVO	1978	08	31	13	07	20.97	18.98	155.49	38.51	4.3
HVO	1978	09	11	20	16	06.11	19.33	155.11	9.60	4.1
HVO	1978	11	23	03	16	15.88	19.24	155.55	11.40	4.2
HVO	1978	12	14	04	12	45.04	19.31	155.22	10.49	4.1
HVO	1978	12	27	00	40	55.83	19.34	155.22	9.93	4.3
HVO	1979	03	06	05	07	58.54	19.52	155.27	27.43	4.7
HVO	1979	03	10	03	55	14.65	19.33	155.11	9.57	4.5
HVO	1979	03	21	20	46	59.79	20.10	155.84	16.22	4.5
HVO	1979	03	27	21	30	09.80	20.09	155.83	12.31	4.9
HVO	1979	07	31	03	30	51.28	19.47	155.43	11.65	4.3
HVO	1979	08	14	02	51	42.19	20.81	156.29	24.48	4.5
HVO	1979	09	21	21	59	37.62	19.35	155.07	9.19	5.5
HVO	1979	09	21	23	29	12.34	19.35	155.04	9.21	4.3
HVO	1979	09	27	05	35	45.49	19.33	155.12	10.05	4.3

Appendix B. Page 2.

SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (km)	MAGNITUDE (M _L)
HVO	1979	10	14	07	37	16.92	19.91	155.18	40.57	4.0
HVO	1979	10	30	19	35	11.68	19.88	156.34	00.02	4.2
HVO	1979	12	13	17	44	03.08	19.41	155.41	11.44	4.0

EXPLANATION FOR REFERENCE COLUMN IN APPENDIX C.

BSSA - Bulletin of the Seismological Society of America

G-R, 1954 - Gutenberg, B., and Richter, C.F., 1954, Seismicity of the Earth and Associated Phenomena, 2d ed., Princeton Univ. Press, Princeton, N.J., 310 p.

Richter, 1958, Elementary Seismology, W.H. Freeman and Co., San Francisco, 768 p.

EQHUS - U.S. Department of Commerce, NOAA, Records of the Honolulu Observatory, Honolulu, Hawaii.

HVO L&S - U.S. Geological Survey, Hawaiian Volcano Observatory Summary (previously the Volcano Letters and published by the National Park Service), Hawaii Volcano Observatory, Hawaii.

Monthly Weather Review - U.S. Weather Bureau. The general reference to this source is sufficient because earthquakes are described in the issue for the month in which they occurred, with few exceptions. Earthquake reports are very complete for the period 1915 to June, 1924.

ISS, Kew - Kew Observatory, International Seismological Summary, 1913 - 1963, Kew, England. This report became the Bulletin of the International Seismological Centre in 1964 and was printed through 1965 at Edinburgh, Scotland.

USEQ - United States Earthquakes. Annual publication of the U.S. Department of Commerce, Coast and Geodetic Survey from 1928 through 1968, the NOAA National Ocean Survey for 1969, and the NOAA Environmental Data Service, 1970.

Note: All times listed by NOAA, 1973 are Hawaiian Standard Time.

YEAR	DATE	TIME	AREA	LAT	LONG	FELT AREA	MAX INT	MAG.	REFERENCES
1834	2/19	-----	Island of Hawaii	-----	-----	-----	-----	-----	BSSA v.2, 1912
1838	2/12	-----	"	-----	-----	-----	-----	-----	"
1868	4/2	±16:00	S. coast of Hawaii	19.0	155.5	-----	X	-----	" BSSA v.4, 1914 G-R, 1954 Richter, 1958 EQHUS
1909	3/13	-----	Island of Hawaii	-----	-----	-----	-----	-----	"
1912	10/13	-----	Hawaii	-----	-----	-----	-----	-----	"
1913	9/8	12:08	Kilauea area	-----	-----	-----	V	-----	HVO L&S
1913	10/25	01:28	Kilauea area	-----	-----	-----	V	-----	"
1918	11/2	00:03	Mauna Loa	-----	-----	-----	VII	-----	" ISS, Kew Monthly Weather Review
1919	1/28	17:53	Hawaii	-----	-----	-----	V	-----	"
1919	8/26	02:34	Island of Hawaii	-----	-----	-----	V	-----	HVO L&S
1919	9/14	17:50	Kilauea	-----	-----	-----	VII	-----	ISS, Kew HVO L&S
1923	1/14	02:58	Island of Hawaii	-----	-----	-----	-----	-----	ISS, Kew HVO L&S
1923	2/9	21:11	"	-----	-----	-----	-----	-----	"
1923	12/14	06:04	"	-----	-----	-----	-----	-----	"
1923	12/25	19:16	Hawaii	-----	-----	-----	-----	-----	"
1924	8/20	06:50	Island of Hawaii	-----	-----	-----	-----	-----	"
1925	7/8	06:15	"	-----	-----	-----	-----	-----	"
1926	2/28	07:11	"	-----	-----	-----	-----	-----	"
1926	3/19	23:03	"	-----	-----	-----	-----	-----	"
1926	4/22	05:02	Mauna Loa	-----	-----	-----	-----	-----	"
1926	6/9	10:05	Island of Hawaii	-----	-----	-----	-----	-----	"
1927	3/20	05:22	"	-----	-----	-----	-----	-----	"
1927	8/3	10:12	"	-----	-----	-----	-----	-----	"
1929	9/28	07:40	Hilo, Hawaii	-----	-----	-----	VII	-----	USEQ

Appendix C. Earthquakes of intensity V or greater in NOAA (1973) not listed in Appendix A or B.

YEAR	DATE	TIME	AREA	LAT	LONG	FELT AREA	MAX INT	MAG.	REFERENCES
1930	5/20	19:22	Hualalai area	----	----	----	V	----	USEQ
1930	5/25	20:47	Kilauea	----	----	----	V	----	"
1931	1/30	00:08	Waiohinu	----	----	----	V	----	"
1933	12/2	06:30	Hilo	----	----	----	VI	----	"
1934	5/10	10:39	near Hakalau	19.6	155.4	----	V	----	"
1935	1/2	07:17	Kilauea	19.4	155.3	----	V	----	"
1935	6/28	09:30	Mauna Loa	19.6	155.2	----	V	----	"
1935	9/30	23:06	"	19.4	155.7	----	V	----	"
1935	10/1	00:28	"	19.6	155.4	----	V	----	"
1935	11/21	01:41	"	19.5	155.5	----	V	----	"
1936	4/15	08:57	Kilauea	19.4	155.2	----	V	----	"
1938	2/17	02:48	Mauna Loa	19.6	155.4	----	V	----	"
1939	5/15	10:58	Kilauea	19.4	155.1	----	V	----	"
1939	5/23	14:44	Kilauea	19.5	155.4	----	V	----	"
1939	5/24	13:29	"	19.4	155.2	----	V	----	"
1939	5/31	21:21	"	19.6	155.2	----	V	----	"
1939	6/12	01:41	Kau Desert, Hawaii	----	----	----	V	----	"
1939	7/14	04:21	Kilauea	19.3	155.1	----	V	----	"
1940	9/1	22:45	N. of Island of Hawaii	21.0	155.3	----	V	----	" G-R, 1954
1941	11/6	10:11	near Waimea	----	----	----	V	----	USEQ
1941	11/18	03:26	"	----	----	----	V	----	"
1941	11/22	21:53	"	----	----	----	V	----	"
1943	11/10	16:52	southern Hawaii	----	----	----	VI	----	"
1944	11/12	05:26	SW of Halemaumau	----	----	----	V	----	"
1945	3/4	00:00	Mauna Loa	----	----	----	V	----	"
1945	5/19	01:48	"	----	----	----	V	----	"
1945	9/19	05:33	Saddle area, Hawaii	----	----	----	V	----	"
1947	3/19	23:06	Island of Hawaii	----	----	----	V	----	"
1947	9/30	04:04	"	----	----	----	V	----	"
1949	2/26	13:54	Mauna Loa	----	----	----	V	----	"
1949	5/2	05:02	"	----	----	----	V	----	"

Appendix C. Earthquakes of intensity V or greater in NOAA (1973) not listed in Appendix A or B.

YEAR	DATE	TIME	AREA	LAT	LONG	FELT AREA	MAX INT	MAG.	REFERENCES
1950	3/25	05:43	Mauna Loa	----	----	----	V	----	USEQ
1951	9/16	01:43	Kaoiki fault	19.2	155.5	----	V	----	"
1951	11/8	09:34	Mauna Loa	19.2	155.5	----	VI	----	"
1952	2/2	01:16	near Kaumana	----	----	----	V	----	"
1952	3/17	17:58	off coast of Hawaii	19.1	155.0	----	V	----	"
1952	7/12	13:53	Kona, Hawaii	----	----	----	V	----	"
1953	1/9	21:10	Mauna Loa	19.4	155.5	----	V	----	"
1953	1/15	02:05	"	19.3	155.4	----	V	----	"
1953	8/21	19:47	Hawaii	----	----	----	V	----	"
1954	7/3	11:53	Kilauea	20.5?	155.5	----	VI	----	"
1955	3/27	16:02	"	----	----	----	VII	----	"
1955	4/1	04:24	"	19.5	155.0	----	V	----	"
1955	8/7	07:18	off N coast of Hawaii	20.5	155.5	----	V	----	"
1955	8/14	02:28	Kileuea	19.5	155.5	----	----	----	"
1955	10/26	16:56	near Makauweoweo	19.5	155.5	----	V	----	"
1956	5/13	21:54	off N coast of Hawaii	20.3	155.3	----	V	----	"
1956	10/16	00:45	W of Hawaii	20	157	----	V	----	"
1962	6/27	18:28	Kaoili fault	19.4	155.4	----	VI	----	"
									BSSA v.56, 1966

Appendix C. Earthquakes of intensity V or greater in NOAA (1973) not listed in Appendix A or B.

SEISMIC VOLCANIC RISK ASSESSMENT,
PUNA GEOTHERMAL PROSPECT AREA, HAWAII

by

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VOLCANIC RISK ASSESSMENT

prepared for

THERMAL POWER COMPANY

DILLINGHAM

AMFAC

October 1981

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1.0 EXECUTIVE SUMMARY

1.1 Introduction

This report summarizes the geologic, volcanologic, and seismicologic data that relate to evaluation of the Seismic-Volcanic Risk Assessment (SVRA) for the Puna Geothermal Prospect (PGP) of the Lower East Rift Zone (LERZ) on the volcano, Kilauea, Hawaii. The basis for the assessment sections is developed in detail in the Geology Section (3.0), with the volcanic and seismic assessments discussed in Sections 4.0 and 5.0, respectively.

The Volcanic Risk Assessment leads to conclusions that the hazards and risk from volcanic activity and associated fissuring and faulting are high and diverse, but the risk to engineered structures and installations can be mitigated by proper procedures in siting and design. Recommendations are made as to the methods and factors that should be considered for mitigation. The Seismic Risk Assessment demonstrates that the hazard and risk from ground motion is of three general sources: frequent low magnitude volcanic earthquakes with epicenters near the site, infrequent earthquakes of deep focus, low to moderate magnitudes and generally from Kilauea, and tectonic earthquakes of about 6.5 to 7.2 magnitude from the Hilina fault zone with epicenters at distances of from 20 to 50 km (12 to 30 mi).

1.2 Volcanic Risk Assessment

The Puna Geothermal Project is sited in one of the most active eruptive centers of one of the most rapidly growing volcanoes in the world. Important eruptions of lava have affected the area in 1750, 1790, 1840, 1955, and 1960.

Evidence from the log of the HGP-A well indicates that, on a

long term basis, an individual site is over-run by lava about once every 900 years, but on a shorter time scale, the frequency is strongly influenced by topography; low areas are covered by flows much more frequently than high areas.

Although eruptions are frequent, they are also quite regular in their behavior and can be predicted with a much higher degree of certainty than is possible in other volcanic regions of the world. Large explosions of ash or pumice are highly unlikely; almost certainly, future eruptions will be like earlier ones, i.e. voluminous discharges of very fluid lava preceded or accompanied by earthquakes and surface deformation.

Future eruptions will be preceded by volcanic and seismic activity in the summit region and by extension and faulting of the ground surface near the site of the eruptive outbreak. They will be accompanied by numerous earthquakes and will form new fissures, avoiding previously active vents in favor of new ground. Fissures will almost certainly be located within the well-defined boundaries of the rift zone. Vents outside that zone are highly unlikely. Fountaining to heights of three or four hundred meters will cover the surrounding region with scoriaceous material, but ejection of explosive debris rarely has a serious effect beyond a few hundred meters from the vent.

The principal volcanic hazards to facilities sited in the East Puna zone are surface rupture, ground motion, and inundation by lava. By comparison, all other hazards are relatively minor. These hazards can be greatly reduced by a modest amount of planning and consideration of a few simple precautions.

If at all possible, permanent installations should not be

constructed in low areas where lava is likely to be channeled. Old cinder cones and other areas of relatively high ground are unlikely to be over-run within the next four or five decades. Diversion barriers, if well situated and properly constructed, can deflect lava into an alternative course, but they are ineffective as dams opposing the flow of lava directly.

By orienting buildings and other permanent structures with their shortest dimensions parallel to the axis of the rift, the longest effects of ground deformation and surface rupture can be materially reduced.

Close coordination with the Hawaiian Volcano Observatory and the Hawaiian Institute of Geophysics will help ensure timely warnings of impending eruptions.

1.3 Seismic Risk Assessment

The maximum earthquake that is probable for the next 40 year period is an assumed tectonic earthquake from the Hilina fault zone, with an estimated magnitude of 6.75 and an epicentral distance of 25 km (15 miles). An earthquake of this magnitude would have a mean peak horizontal acceleration of about 0.25 g, a mean peak horizontal velocity of 25 cm/sec, and mean peak horizontal displacement of 10 cm, with a duration of more than 0.05 g motion for about 15 to 25 seconds. This strength and duration of motion, is the strongest motion to be expected from a 100 year earthquake of about $M_s = 7.2$, and is within the range that can be readily mitigated by appropriate design.

The two earthquake hazards that may constitute a risk to future engineering structures and installations are primarily the strong ground motion from tectonic earthquakes, and to a minor

amount, landsliding, slumping or other secondary ground failures of steep slopes near the epicenter of earthquakes of above 5 magnitude. Surface faulting may occur in the site area in response to volcanic related activity, as is discussed in the volcanic risk assessment section of the report. Other seismic hazards and risks, including liquefaction, tsunamis and seiches are considered to be unimportant for this siting area.