Seismic Volcanic Risk Assessment Puna Geothermal Prospect Area Hawaii

by

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for the

Seismic Risk Assessment

and

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Committee interest

Volcanic Risk Assessment

prepared for Thermal Power Company Dillingham AMFAC



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1.0 EXECUTIVE SUMMARY

1.1 Introduction

This report summarizes the geologic, volcanologic, and seismologic data that relate to evaluation of the Seismic-Volcanic Risk Assessment (SVRA) for the Puna Geothermal Prospect (PGP) of the Lower East Rift Zone (LERZ) on the volcano, Kilauea, Hawaii. The basis for the assessment sections is developed in detail in the Geology Section (3.0), with the volcanic and seismic assessments discussed in Sections 4.0 and 5.0, respectively.

The Volcanic Risk Assessment leads to conclusions that the hazards and risk from volcanic activity and associated fissuring and faulting are high and diverse, but the risk to engineered structures and installations can be mitigated by proper procedures in siting and design. Recommendations are made as to the methods and factors that should be considered for mitigation. The Seismic Risk Assessment demonstrates that the hazard and risk from ground motion is of three general sources: frequent low magnitude volcanic earthquakes with epicenters near the site, infrequent earthquakes of deep focus, low to moderate magnitudes and generally from Kilauea, and tectonic earthquakes of about 6.5 to 7.2 magnitude from the Hilina fault zone with epicenters at distances of from 20 to 50 km (12 to 30 mi).

1.2 Volcanic Risk Assessment

The Puna Geothermal Project is sited in one of the most active eruptive centers of one of the most rapidly growing volcances in the world. Important eruptions of lava have affected the area in 1750, 1790, 1840, 1955, and 1960.

Evidence from the log of the HGP-A well indicates that, on a

long term basis, an individual site is over-run by lava about once every 900 years, but on a shorter time scale, the frequency is strongly influenced by topography; low areas are covered by flows much more frequently than high areas.

Although eruptions are frequent, they are also quite regular in their behavior and can be predicted with a much higher degree of certainty than is possible in other volcanic regions of the world. Large explosions of ash or pumice are highly unlikely; almost certainly, future eruptions will be like earlier ones, i.e. voluminous discharges of very fluid lava preceded or accompanied by earthquakes and surface deformation.

Future eruptions will be preceded by volcanic and seismic activity in the summit region and by extension and faulting of the ground surface near the site of the eruptive outbreak. They will be accompanied by numerous earthquakes and will form new fissures, avoiding previously active vents in favor of new ground. Fissures will almost certainly be located within the well-defined boundaries of the rift zone. Vents outside that zone are highly unlikely. Fountaining to heights of three or four hundered meters will surrounding region cover the with scoriaceous material, but ejection of explosive debris rarely has a serious effect beyond a few hundred meters from the vent.

The principal volcanic hazards to facilities sited in the East Puna zone are surface rupture, ground motion, and inundation by lava. By comparison, all other hazards are relatively minor. These hazards can be greatly reduced by a modest amount of planning and consideration of a few simple precautions.

If at all possible, permanent installations should not be

constructed in low areas where lava is likely to be channeled. Old cinder cones and other areas of relatively high ground are unlikely to be over-run within the next four or five decades. Diversion barriers, if well situated and properly constructed, can deflect lava into an alternative course, but they are ineffective as dams opposing the flow of lava directly.

By orienting buildings and other permanent structures with their shortest dimensions parallel to the axis of the rift, the longest effects of ground deformation and surface rupture can be materially reduced.

Close coordination with the Hawaiian Volcano Observatory and the Hawaiian Institute of Geophysics will help ensure timely warnings of impending eruptions.

1.3 Seismic Risk Assessment

The maximum earthquake that is probable for the next 40 year period is an assumed tectonic earthquake from the Hilina fault zone, with an estimated magnitude of 6.75 and an epicentral distance of 25 km (15 miles). An earthquake of this magnitude would have a mean peak horizontal acceleration of about 0.25 g, a mean peak horizontal velocity of 25 cm/sec, and mean peak horizontal displacement of 10 cm, with a duration of more than 0.05 g motion for about 15 to 25 seconds. This strength and duration of motion, is the strongest motion to be expected from a 100 year earthquake of about Ms = 7.2, and is within the range that can be readily mitigated by appropriate design.

The two earthquake hazards that may consitute a risk to future engineering structures and installations are primarily the strong ground motion from tectonic earthquakes, and to a minor

amount, landsliding, slumping or other secondary ground failures of steep slopes near the epicenter of earthquakes of above 5 magnitude. Surface faulting may occur in the site area in response to volcanic related activity, as is discussed in the volcanic risk assessment section of the report. Other seismic hazards and risks, including liquefaction, tsunamis and seiches are considered to be unimportant for this siting area.

2.0 INTRODUCTION

2.1 Purpose of Study

The goal of this report is to provide a seismic-volcanic risk assessment (SVRA) for the Puna Geothermal Prospect (PGP) located within the Lower East Rift Zone (ERZ) of Kilauea volcano, on the island of Hawaii (Fig. 2.1). The assessment is for the general siting area and is not intended to apply to any sitespecific domain within the general prospect area.

2.2 Scope of Work and Quality of Data Base

The scope of our work includes a preliminary study of available geologic literature, aerial photographs, maps, historical records, and limited bore hole data. The aerial photographs were used to assist in the field review of the siting areas and to search for faults and fissures near the site. Reports on the geology, seismology, tectonic, and volcanic settings are used to prepare this evaluation of the general volcanic and seismic hazards and risk to engineering structures. The site visits included a review of the faults, eruptive vents and other linear structures defined on the aerial photographs or shown on geologic maps of the area. These visits also permitted discussions with seismologists and geologists at the Hawaiian Volcano Observatory (HVO) and the Hawaiian Institute of Geophysics (HIG). This report integrates the catalogs of eruptions and earthquakes and the newer instrumental seismologic data of the latest listings of the National Oceanic and Atmospheric Administration (NOAA) hypocenter data file for worldwide earthquakes, and the HVO summaries of seismic data (Appendices A, B, and C). The above



Figure 2.1. Map of major volcanoes, volcanic rift zones and faults on the island of Hawaii (from Macdonald and Abbott, 1970).

elements of the program are synthesized to provide a general evaluation of the maximum possible and maximum probable volcanic eruptions and earthquakes for structures of an assumed 40 year life-span. The general assessment for volcanic and seismic hazards is adequate for evaluation of the broad siting area, but risk assessment for specific structures or sites within the area are not included in the scope of this report.

This project was proposed and completed in the following stages:

- A. Literature search, fault and lineament analysis of the aerial photographs supplied by Thermal Power Company.
- B. Preliminary data collection and discussions with personnel of the HIG and HVO by George Bergantz and his preparation of a preliminary draft of this report.
- C. Field Study by Mr. George Bergantz in June 1981, and by Dr. D. Burton Slemmons, Alexander R. McBirney, and Brian H. Baker in August 1981.
- D. Preparation of the draft report.
- E. Review and revision of draft report and final submission of the report.

The data base for the seismic risk assessment varies greatly in quality and scope, with poor documentation for early historic earthquake activity, and variable quality and accuracy of cataloging in the National Oceanic and Atmospheric Administration (NOAA) earthquake hypocenter data file of Appendix A. The HVO summaries since about 1962 are good and the data for the period 1975 to 1979 are excellent for most of the region.

2.3 Abbreviations

Abbreviations that are used in this report include the following:

ERZ, East Rift Zone

HIG, Hawaiian Institute of Geophysics

HGP, Hawaiian Geothermal Prospect

HVO, Hawaiian Volcano Observatory

LERZ, Lower East Rift Zone, between about 800 ft elevation and sea level

NOAA, National Oceanic and Atmospheric Administration

PGP, Puna Geothermal Project

SRZ, Southwest Rift Zone

3.0 GEOLOGY

3.1 Regional Geologic Setting

Kilauea is the southern-most of a chain of immense basaltic shield volcanoes extending northwestward across the north central Pacific. This chain has grown southeastward with time, so that the volcanoes are progressively older toward the northwest. Kilauea, the youngest and most active volcano of the chain, has grown to its present height of 1247 meters above sea level (nearly 6 kilometers above the sea floor) in a remarkably short period of about 500,000 years.

The chain has been described as the results of mid-plate volcanism, with northwestward movement of the Pacific plate over a "hot spot" or magmatic source, to form a series of islands and seamounts that vary in age and location from oldest at the northern end of the Emperor Seamount Chain, to the youngest on the south end of Hawaii in the Hawaiian Ridge segment of the chain (fig. 3.1 and 3.2). The potassium-argon dating of lava from these islands and seamounts (fig. 3.2) show a southeast migration of volcanism with time, with a mean migration rate of 11.0 cm/yr (Dalrymple and others, 1973). The volcanoes on the island of Hawaii conform to this general pattern with the northern vol-(Kohala and Mauna Kea) showing older ages and deeper canoes dissection by erosion than the two southern, actively growing volcanoes, Mauna Loa and Kilauea which have prolific historic and neohistoric volcanic activity.

The five major volcanoes of Hawaii (pls. 1 and 2, and fig. 2.1) are built from flows and pyroclastic debris from central



Eigure 3.1. Chains of seamounts and volcanic islands in the Pacific Ocean (from Williams and McBirney, 1979).



Figure 3.2. Relations of potassium-argon ages of lavas from the Hawaiian-Emperor chain north from Kilauea at the southeast end of the chain (from Williams and McBirney, 1979; and after Dalrymple and others, 1973).

conduits and rift zones. Cleaving these volcanic centers are radial rift zones which intersect at the central dome volcano, and which are the sites of, and passageways for, the bulk of the eruptive materials (Stearns, 1946). Mauna Loa and Kilauea are the southern-most major volcanoes of the island and of the chain. Both have many historic flows from their summits and northeasttrending rift zones.

Rocks in the vicinity of the Puna District and adjacent districts are typically aa and, less commonly, pahoehoe flows of olivine-bearing tholeiitic basalt and associated pyroclastic and hyaloclastic deposits (Stearns and Macdonald, 1946; Macdonald and Abbot, 1970). Three time-stratigraphic units are recognized, the Hilina Volcanic Series, the Pahala ash and the Puna Volcanic Series (fig. 3.3). The bulk of the older Hilina Volcanic Series is related to eruptive events from the Kilauea caldera with magmatic communication at moderate crustal depths inferred to connect with adjoining rifts (fig. 3.4). The Puna Volcanic Series include lavas that appear to have been differentiated from source magmas of the central conduit at Kilauea (Stearns and Macdonald, 1946).

3.2 Structural Features of Kilauea

Kilauea Volcano (fig. 3.5) can be divided into six structural zones (modified from the scheme of Swanson and others, 1976):

1. The summit area includes the caldera and two large pit-craters and has been the site of numerous eruptions and repeated surface deformation over the main reservoir of magma.



Figure 3.3. Geologic column for the main rock units on the island of Hawaii. All units have ages of less than 1,000,000 years; Recent extends to approximately 10,000 years ago (from Macdonald and Abbott, 1970).



Figure 3.4.

 Inferred subsurface geologic structure of the East Rift Zone of Kilauea based on seismic refraction and gravity data (form Furumoto, 1978).



EXPLANATION .



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Figure 3.5. Structural subdivisions of Kilauea Volcano and locations of triangulation stations shown in Figure 4.5. Boundaries of subdivisions are gradational in most places (Swanson and others, 1976). C.

2. The Chain-of-Craters zone (fig. 3.6) comprises a SEtrending belt of small satellite sheilds and pit craters. This is cut by ENE-trending fissures and merges into the East Rift Zone.

3. The ENE-trending East Rift Zone (ERZ) consists of small shields, pit craters, fissures, and faults. It is 3 to 5 km wide, extends 45 km from Mauna Ulu to Cape Kumakahi, and continues as a submarine ridge another 70 km to the northeast.

4. The Koae fault system of 20 km length is a 3 km wide zone of normal faults cutting the upper south flank of Kilauea. It is the direct structural continuation of the ERZ and links the East and Southwest Rift Zones.

5. The Southwest Rift Zone (SRZ) of about 20 km length is a less active counterpart of the East Rift Zone.

6. The Hilina fault zone of about 50 km length cuts the lower, southern flank of the Kilauea shield.

The SRZ and ERZ, together with the summit area and the Chain of Craters zone comprise the eruptive zone of Kilauea, whereas the Koae and Hilina fault systems are fracture zones from which little or no lava has been issued.

3.3 Crustal Structure of Kilauea and the East Rift Zone

In order to understand the nature of volcanic and seismic activity of Kilauea, it is helpful to review briefly the structure and evolution of the volcano and the mechanisms governing its behavior.

Seismic data indicate that the crust under Kilauea consists of 9 kilometers of volcanic rocks resting on 5 to 6 kilometers of older oceanic crust and a mantle composed of rocks with the



Figure 3.6. Map of Kilauea and the adjacent part of Maona Loa Volcanoes showing the summit caldera and the southwest and south-east rift zones, and the Koae and Hilina fault systems on the south flank. The Chain of Craters sector of the East Rift Zone extends from Halemaumau to Mauna Ulu (Swanson and others, 1976).

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seismic properties of serpentinized peridotite (Crosson and Koyanagi, 1979). The top of the mantle under the island is depressed by the great weight of the volcanoes from its normal depth of 10 km to about 14 km below sea-level.

Seismic refraction, gravity and seismic velocity surveys of the lower ERZ have shown (fig. 3.5, 3.7 and 3.8) a shallow surface layer of low and varied seismic velocities corresponding to young porous volcanic rocks (Vp = 2.5 to 3.0 km/sec), overlying a water-saturated zone extending to a depth of 1.8 km below sealevel. From 1.8 to 5 km, velocities average 5.25 km/sec, with a zone of higher velocity (about 7.0 km/sec) corresponding to a presumed dike complex along the ERZ (Broyles and others, 1979). Their gravity data indicate that the high-density zone of dikes is 12 km to 17 km wide, in contrast to the 4 km width of the ERZ. Part of the zone of high density lies to the north of the ERZ, supporting the suggestion (Swanson and others, 1976) that the ERZ has migrated to the south as the volcano has grown.

Seismicity in the ERZ is concentrated at depths of less than 10 km and has been related to lateral movement of magma from the summit region into a reservoir complex under the ERZ (Koyanagi and others, 1981). Swarms of shallow earthquakes commonly precede eruptions in the upper part of the ERZ, but near Puu Honaula (in the lower ERZ) shallow earthquake swarms have occurred without surface deformation or eruption, and these are thought to result from local movement in a magmatic storage zone isolated from the remainder of the rift (Koyanagi and others, 1974 and 1981).

3.4 Characteristics of Volcanism of Kilauea



Schematic cross section showing idealized crustal Figure 3.7 structure of Hawaiian Volcano (based largely on Kilauea). Numbers indicate P-wave velocity in km/sec (hill, 1969).



Figure 3.8 Hypothetical cross section through the island of Hawaii (SW to NE) showing principal features of structure as suggested by the seismic velocity interpretations of Crosson and Koyanagi (1979). Velocities are meant to denote averages for the crust and upper mantle. Small open circles are representative of earthquake depth distribution beneath Kilauea volcano (from Crosson and Koyanagi, 1979).

Because of the frequency of eruptions and many detailed studies carried out by the Hawaiian Volcano Observatory, the activity of Kilauea is more clearly understood than that of any other volcano. Techniques for monitoring and forecasting eruptions have reached a highly sophisticated and successful level of development.

While it is generally true that volcanism has a variety of forms and no two eruptions are exactly identical, Hawaiian activity is more regular than that of other types of volcanoes. The characteristics of the eruptive activity of Kilauea during its present mature stage of evolution have been well defined.

Eruptions are centered in two general regions, the summit caldera and the rift zones. In general, summit eruptions have a more localized effect, because they tend to be confined to depressions that restrict the flow of lava to a relatively small area. In recent years, however, activity in the summit region has shifted to the vicinity of the new eruptive center around Mauna Ulu, a short distance south of the caldera. Flows from this area have moved down the south flank of the volcano, but have no effect on the lower ERZ. Their significance for our present purposes is in the close connection between activity at the summit and eruptions farther down the rift zones.

Eruptions on the flanks of Kilauea are frequently linked with earlier activity in the summit region. The magma feeding flows discharged from the lower ERZ has been shown to come from a reservoir much higher in the volcanic structure. Swelling of the summit region is commonly observed before an outbreak on the

flanks, and monitoring of this swelling provides a means of anticipating when the volcano is charged with magma at a high level and is capable of erupting. In all the eruptions for which good data are available, earthquakes and tumescence have been recorded around the caldera, and regardless of whether or not these subsurface events were followed by an eruption at the summit, outbreaks on the rift rarely occur except after notable swelling of the upper parts of the volcano.

Many, but by no means all eruptions have been preceded by broadly distributed deep earthquakes followed by more localized seismic activity at a shallow level beneath the immediate region of the impending eruption. In some instances there may be little deep-focussed seismicity and only shallow localized earthquakes. While many of the earthquakes are small, they are recorded in large numbers by the seismic network operated by the U.S. Geological Survey for many days or weeks prior to the outbreak of magma at the surface. For this reason, it is highly unlikely that a major eruption will come as a surprise. It will be preceded by swelling, tilting, and extensive seismic activity well before any lava is discharged.

The chemical and physical character of the magma at Kileaua is also very consistent. It is a very fluid tholeiitic basalt that commonly contains conspicuous crystals of olivine and, more rarely, plagioclase. Apart from minor variations in some of its components, mainly trace elements and concentrations of olivine crystals, it can be expected to vary little for many decades to come. It is normally erupted at temperatures between 1150 and 1200 degrees centigrade and has a low viscosity (in the range of

300 to 1000 poises). Its density ranges widely according to the proportion of gas bubbles but the interiors of flows can reach density of 2.7 grams per cubic centimeter.

Lava is generally of the pahoehoe type near the vent but commonly changes to the clinkery as type as it flows downslope and cools. Some eruptions, such as that of 1790, produced lavas that were almost exclusively pahoehoe, whereas others, such as that of 1955, have been dominantly as. There is no simple way of anticipating which type of lava will be erupted in a particular location.

Eruptions usually break out relatively quietly at one or two points on the rift and quickly spread along a well defined fissure for distances of a few hundred meters to as much as several kilometers. The initial eruptive phase is characterized by spectacular fire-fountaining, which quickly increases in height and intensity. It normally lasts for a period of hours, days, or, more rarely, weeks. Along most of the eruptive fissure, the products of these early stages are incandescent bombs, spatter, and fine glassy filaments known as "Pele's hair". Ash is usually subordinate to coarser material, and scoriaceous cinders may accumulate to thicknesses of many meters around a centralized vent that persists in activity for several days or weeks.

Close to the coast, particularly in the area of Kapoho where the ground water table is shallow and rocks are very permeable, water may enter the upper levels of the fissure and greatly augment the explosivity of the eruption. When this occurs, the ejecta are more voluminous and tend to be gray ash, quenched glass, and blocky lithic debris. Regardless of the mode of erup-

tion, however, the deposits are confined to an area close to the vent and seldom accumulate to depths of more than a few meters at distances of more than half a kilometer. Violent explosions hurled large blocks several hundred meters during the steamblast eruption at the summit of Kilauea in 1790 and 1924, but large events of this kind have been uncommon in historic times and have been confined to the summit area.

Subsidence may occur either as linear troughs or as cylindrical collapse pits up to one or two hundred meters in diameter. These latter features are more typical of the upper parts of the rift where magma has been drained by intrusions or eruptions at a lower elevation. But the connection between subsidence and eruptions may not be an obvious one. In 1924, for example, the area of Kapoho subsided several feet even though no surface eruption was observed. It is thought that magma drained into a submarine section of the rift zone and may have erupted below sea level.

Lava flows begin to emerge concurrent with or very soon after the initial episode of fire fountaining. They seldom pour from the entire width of the fissure, except in the earliest stages. More typically, the eruptive vent quickly becomes localized in a short section of the rift. Lava is often discharged at rates of two to five million cubic meters per hour and commonly flows reach lengths of the order of ten kilometers, widths of two or three hundred meters, and thicknesses of about four meters, but these dimensions vary within wide limits. The widths and thicknesses of flows depend mainly on the steepness of the slope and on how much of the fissure is active at a particular time. As the lava moves away from the source, its width may either increase or decrease depending on the local topography. Flows on the south side of the rift tend to become narrower where the slope steepens, and in many cases well-defined channels only a few meters wide develop after the first broad front of the flow has passed. The velocity of flow varies directly with the slope angle and rate of discharge and inversely with the viscosity and width. Velocities as high as 40 miles per hour have been measured in narrow steep channels of pahoehoe lava.

Upon reaching the sea, lava may interact with the water to produce a spray of quenched granular basaltic glass, and if fed by a well-defined and rapidly flowing channel, a flow may develop a littoral cone that can grow to the size of a moderately large cinder cone. Again, the area affected by this explosive activity is confined to the immediate area of the point at which the flow enters the sea.

Taking the volcano as a whole, at least 50 eruptions have been recorded since Europeans first visited the islands, but it is only since 1912, when the Hawaiian Volcano Observatory was established, that reliable records have been available. Table 3.1 lists 46 eruptions and a number of suspected intrusive events that have occurred in this period of 69 years or an average of one every 1.5 years. Of these, 19 occurred in the ERZ and only two, those of 1955 and 1960, affected the East Puna District.

Klein (in press) recently examined this record and found that the timing of eruptions had no detectable periodicity. He observed that subsequent eruptions were independent of the date of the previous eruption. He has, however, found a number of fairly regular (or at least non-random) relationships. These can

TABLE 3.1

Kilauea Eruptions (1918-1979) and intrusions (1959-1980).

5	STARTING	DURATION	1 1000	TIONI					
E.	DATE	(4)	TYPE	TION*	6	DAYS SINCE	DAYS SINCE	ERUPTED	DEFLATION
ā			Sunare	I	ENT	LAST	LAST	VOLUME	I (TILT AT HVO,
1	2/23/18	14	SCHALL	ER	SWR	ERUPTION	INTRUSION	(100m))	IN MICRORADS)
2	2/7/19	294			-		-	.2	
1 3	12/21/19	221	-	-		349	-	27	-
4	3/18/21	7	P	=	5	1 317	-	49	-
5	. 5/28/22	.2	-		-	433	-		-
6	8/25/23	1 1.	-			1 420		1 1	-
7	. 5/10/24	17		-	=	424	-	.1	- :
8	7/19/24	11	E	-		1 70		ASH	-
9	7/7/27	1 13	E			1093	_		
10	2/20/29	1 2	E			594	·	2.3	-
11	7/25/29	4	E	i		155		1.3	-
12	11/19/30	19	E			487		2.0	_
13	12/23/31	14	E			199			-
14	9/6/34	33	E	i		288	_	8	-
15	6/27/52	136	E	1 1		6504	_	51	
16	5/31/54	3	E			703	_	7	
*17	2/28/55	88		E		273	-	95	-
18	11/14/59	36	E	I		1720		40	-45
*19	1/13/60	36		E	-	60	60	119	-300
20	2/24/61	1	E	1		408	408		1 (2
21	3/3/61	22	E	1-1		1 7	7		-6
22	7/10/61	7	E	- 1		129	129	13	-8
•23	9/22/61	4		3 1		74	74	2.5	-166
24	12/7/62	3		E	1	441	441	.3	-13
	5/9/63	1 1	-	- 1	L	1 -	153	-	-32
	7/1/63	2		I	1 1	1 -	53		-20
25	8/21/63	. 3		E	1	257	51	.8	-11
*26	10/5/63	2		E		45	45	8	-79
*27	3/5/65	11		E		517	517	18	-84
2.0	8/25/65	1	I	I	-		173		1 +8
28	12/24/65	2		E	-	294	121	.8	-45
= 29	11/5/67	251	E	1-		681	681	84	-11
30	8/22/68	5		E		291	291	.01	-54
22	2/22/62	16		E		46	46	7	-60
+22	2/22/09	/		E		138	138	17	-46
~	3/24/09	8/5		EP		91	91	185	-24
1	1/22/70			I			163		-6
	2/2/70		1				80		-6
1	4/5/70	8		I	I	-	12		-4
·* •	5/15/70	2			L	-	61		-9
i	6/11/71	2					40		-8
34	8/14/71	1			L		392		-4 .
35	9/24/71.	ŝ	5. 7	-	(=)	012	64	10	-16 -
	12/24/71	6	6		(2)	41	41	8	+12
*36	2/4/72	455		FD		111	91	126	-3
37	5/5/73	1		E		133	42	125	-2
38	5/7/73	187		50		430	458		-23
	6/9/73	1		T			12 .	2.5	(2
39	11/10/73	30		F		197	154	1	-0
40	12/12/73	222		50		1 12	134	10	-14
	3/24/74	1		II		52	102	50	-2

TABLE 3.1. Continued.

VENT	STARTING DATE	DURATION (d)	LOCATIONI &			DAYS SINCE	DAYS SINCE	ERUPTED VOLUME	1 DEFLATION I(TILT AT HVO.
			SUMMIT	I ER	SWR	ERUPTION	INTRUSION	(106 ² 3)	IN MICRORADS)
41	.7/19/74	3	E	-		219	1 117	1 10	-17
42	9/19/74	1 1	IE	1		62	67	1 11	+25
*43	12/31/74	1 1	1	i	E	1 103	103	1 15	-155
*44	1 11/29/75	1 . 1	IE	(1)	1	1 333	333	.2	1 -221
	6/21/76	1 . 1	1	II	1-	1 -	205	-	1 -7 .
	7/14/76	1 1	1	ii	1	1 -	23		-7
	2/8/77	1 1	1	11	1	I - '	209	1	-6
45	9/12/77	1 20		E	1	653	216	40	-109
	5/29/79	1 1		II	i	-	624		-3
	8/12/79	1 1	1	II	1	i	1 75		-2
46	1 11/16/79	1 1	1	IE	i	795	96	1 .4	-8
	3/2/80	1 1	1	it	i	-	1 107		-3
	1 3/10/80	1 1	1	I I	i	i –	1 8	i	-16
	8/27/80	1 1	1	i T	i		1 170	1	-7
	10/22/80	1 1		İT	1	-	56		-2
	11/2/80	1 1	1	i î	i	i –	1 11	i	-6

Location codes: Summit, Kilauea summit caldera or its margin; ER, east rift zone; SWR, southwest rift zone; Event codes: E, eruption; I, intrusion with no surface lava; EP, major phase of Mauna Ulu eruption of 1969-74. Data are complete through November 1980.

*Largest eruptions: volume exceeds 70 x 106m3, or deflation exceeds 70 microradians.

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be briefly summarized as follows.

1. Large-volume eruptions tend to be followed by longer reposes, which are interpreted as the time required for the shallow magma reservoirs refill to the extent that another eruption is possible.

2. The mean repose time between eruptions has been 282 days. Long periods of repose lasting several years are correlated with periods when Mauna Loa is active. The short repose times of a few days are probably due to brief physical obstructions that interupt an eruption that would otherwise be continuous. Intermediate repose time appear to be of random duration and cannot be correlated with any known phenomenon.

3. Summit and flank eruptions are often paired with flank eruptions following a summit eruption rather than vice versa, but the pattern is far from regular, and the time of the last summit eruption cannot be used to forecast the next flank eruption. Moreover, long sequences of summit eruptions have continued without a flank eruption. Conversely, long runs of flank eruption rarely occur without an intervening summit eruption.

3.5 Rift Zones

Rift zones radiate from calderas of historically active Hawaiian volcanoes and are sites of most of the eruptive and seismic activity. The rifts are defined by broad zones of linear grabens, fissures, aligned cinder cones, spatter cones, pit craters and associated earthquake foci and geophysical anomalies. Subsurface data and exposure by erosion of the older underlying volcanic foundations on other Hawaiian islands to the north show the rifts to be composed of multiple, narrow dikes of basalt, generally with steep dips. They generally show continuity to the summit calderas or their deeper, central magmatic sources.

The PGP (fig. 3.3 and 3.6) is on the ERZ of the eastern flank of Kilauea. The volcanic geology of the ERZ has been studied in detail by Holcomb, (1981). Most of this east flank is covered with lavas of no more than a few tens of thousands of years age, with most of its surface less than one thousand years old. The ERZ originates near the summit of Kilauea as a southeasterly trending alignment of vents, craters, and small calderas (figs. 3.3, 3.6, and 3.9). About 5 km south of Kilauea it joins the eastern end of the Kaoe fault zone where it changes in trend to a nearly straight ENE zone that passes through the PGP and continues offshore (Furumoto and Kovach, 1979).

The zone is a very straight topographic high, with а plateau-like character, that appears to be defined by the width of the zone of fissures. The ERZ extends at least 60-80 km ENE (Suyenaga and other, 1978) to the coastline, and the submarine topography indicate ENE extension of several tens of kilometers beyond. The extensional features in the zone, such as normal faults, linear cracks and fissures, and tilted fault blocks, delineate a zone of about 5 km width at the HGP-A well site. The volcanic eruptions on the zone are tabulated (tbl. 3.1) and are described in Section 4.0 of this report. They have been accompanied by seismic activity as is discussed in Section 4.0 and 5.0 and listed in Appendices A, B and C. All, or at least most, of the earthquake activity of the ERZ is directly associated with the volcanic activity. The nearest tectonic activity is along the



Figure 3.9. Structural map of the Lower East Rift (after Holcomb, 1981). Arrows denote the direction of flowage.

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Hilina fault zone, a few kilometers south of and sub-parallel to the rift.

The instrumentation for earthquake studies of the ERZ was poor before about 1960. Since 1960 improvements in the seismologic network have provided good data. Koyanagi and others (1981) document a major improvement in ability to assess the seismicity of this zone in about 1976, although the eastern part of the Puna district has not been fully instrumented. The most recent major eruptions on the ERZ near the PGP were in 1955 and 1960. Furumoto (1978) has modeled the subsurface geologic structure of the ERZ at the PGP, using on seismic refraction and gravity data (fig. 3.5).

The relationship between the ERZ and the central summit caldera has been reviewed by Koyanagi and others (1981). They state:

From seismic and tilt data, Eaton (1962) developed a structural model of Kilauea where magma traced to nearly 60 km depth rises to fill a small storage system a few kilometers beneath the summit. His data further indicated that magma is transported laterally through shallow rift zones to feed eruptions along these linear fissure systems.

The mechanics of magmatic movement in the rift zones were later studied in detail by Fiske and Jackson (1972). The laboratory experiments they conducted using gelatin models demonstrated how stresses from magmatic pressures could create extensive swarms of thin magma-transporting dikes within the rift zones. Also studied in their investigation was how the orientation of shallow rift zones could be influenced by gravitational loading of existing volcanic masses.

Koyanagi and others (1972) described the asymmetric distribution of crustal earthquakes along the East Rift Zone to support the concept that stresses generated by magmatic intrusions are relieved on the seaward, free slopes of the volcano: the north flank is buttressed against the massive Mauna Loa volcano and

remains stable and relatively immobile. Epicenter maps prepared in summary bulletins from HVO since 1962, such as in Koyanagi and others, 1978a, 1978b, 1978c, show the high concentration of crustal earthquakes on the seaward slopes of Kilauea, particularly in 1975-77 during the intensive aftershock activity following a 7.2-magnitude earthquake on November 29, 1975 (see fig. 3.10 of this report). The aftershocks clustered in the south flank along an elongate zone that extended from the southwest rift eastward to about Puu Honuaula on the east rift. The areas north of the east rift, as well as east of Puu Honuaula are contrastingly aseismic. Swanson and others (1976) verified the crustal instability and showed the trend of southward movement of Kilauea's south flank with detailed deformation surveys. They contend that magma forcefully intrudes the rift zones by forming many thin and near vertical dikes. The intrusion forces the wallrocks apart normal to the direction of intrusion ultimately causing the seaward displacement of the south flank.

Zablocki (in Keller and others, 1977) summarized these concepts by putting into perspective his findings from geoelectric surveys of the East Rift Zone, with particular emphasis in the lower part of the subaerial rift southeast of the Pahoa in an area of known microearthquake localization. He described a positive thermal anomaly elongated transverse to the major axis of the rift zone at a place that corresponds to an apparent left-lateral offset of the principal volcanic features that define the surface of the rift zone. He suggested that the buttressing effect of Mauna Loa north of the rift lessens with increasing distance away to the east, and eastward from Puulena the more symmetrical topography and deformation pattern accordingly indicate symmetry in the distribution of stress normal to the rift zone. Such changes in the stress field may cause structural offsets to develop in the rift and may cause magma fed laterally from the summit to accumulate, forming secondary storage zones.

Furumoto (1978), using seismic and gravity data and information gathered from the geothermal well, proposed a crustal model for the geothermal area (see fig. 3.5 of this report). He described the core of the rift as a broad zone that extends downward from a depth of 4 km. This hot zone is overlain by a 2 km thick dike swarm.

The Southwest Rift Zone (SRZ) is similar to the ERZ, and currently is the focus of frequent earthquakes activity, major tilting and probable magmatic movement. This zone appears to be



Figure 3.10. Locations of $M_A \ge 3.0$ earthquakes with focal depth of 0-20 km at Kilauea from December 1975 to December 1977. The Quality of location for most of the events plotted are less than 2 km in standard errors of epicenter (upper plot) and depth (lower plot). A-A' and B-B' are center lines for cross-sectional hypocenter plots prepared in the following figure 4b (Koyanagi and others, 1981).
narrower than the ERZ and does not extend as far offshore. (fig. 3.3 and 3.6). Forceful injection of dikes does not appear to initiate earthquakes of larger size (Swanson and others, 1976), but, like the ERZ, may be associated with frequent and, at times, rhythmic earthquakes. Eruptions from this zone are less frequent than in the ERZ and the total volume of historically erupted material is much smaller.

Historic eruptions, with associated earthquake activity at Kilauea and on its rift systems is summarized in Table 3.1. Sixteen of forty-nine eruptions (about 33 percent) are associated with the ERZ. Many eruptions were preceded within five years by deeper focus upper mantle to shallow-focus crustal earthquakes associated with magmatic movement in the summit region of Kilauea.

3.6 Fault Zones

3.6.1. General Comments

Four prominent fault zones are identified on the island of Hawaii, and in order of increasing distance from the site (fig. 3.3 and pls. 1 and 2) are:

A. Hilina fault zone,

B. Koae fault zone,

C. Hanuapo-Kaoiki fault zone, and

D. Kealakekua-Kholo fault zone.

The Hilina fault zone is the most significant zone to the PGP, because of both its proximity, and its high magnitude earthquakes. The Koae fault zone has a short length and historically has only low-magnitude earthquakes. This zone is located just south of Kilauea. The Hanuapo-Kaoiki fault zone at the base of the southeast flank of Mauna Loa and the northwest flank of Kilauea may be an inactive, or less active, antecedent structure to the Hilina fault zone (fig. 3.3 and pls. 1 and 2) and shows little or no historic earthquake activity. The Kealakekua-Kholo fault zone is a subarcuate zone along the western edge of the island.

3.6.2 Hilina Fault Zone

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The Hilina fault zone is a branching, complex normal fault zone with an arcuate surface expression trending east-west across the southern flank of Kilauea (fig. 3.3). The zone extends offshore from both its eastern and western ends, and this offshore extent is not well defined. From aftershock distribution following the 1975 earthquake and the tsunami source parameters, the zone appears to have a large offshore extent (Swanson and others, 1976). This fault zone has south-facing, sub-parallel and <u>en echelon</u> fault scarps of up to 500 m height in late Quaternary basalts. The fault morphology of the Hilina fault zone is characterized by block failures that are suggestive of slumping or landsliding. Lavas at the base of the scarp have dips that are rotated landward. This rotation is similar to that observed on blocks affected by landsliding.

This fault has two large historic earthquakes, the 1868 earthquake of poorly known magnitude, about 7.5 to 8.0 as inferred from intensity (Tilling and others, 1976), and the Ms = 7.2 earthquake of 1975. The tsunami effects of the 1868 earthquake were greater than that of the 1975 earthquake. The 1868 earthquake is assigned an estimated magnitude of Ms = 7.75 + 0.25.

The Hilina fault zone appears to be a gravity controlled fault that is affected by dilation from intrusive activity and associated pressure effects by magmas of the south flank of Kilauea and the ERZ. Various workers (Fiske and Kinoshita, 1969; Koyanagi and others, 1972; Swanson and others, 1976) propose that the stress regime and the geodetic deformation is affected by progressive instrusion of dikes and dilation of the ERZ. Failure during the 1975 earthquake by southeastward sliding or thrusting led to an observed geodetic decrease in elevation and southeastward movement of the land area and the companion uplift at the toe of the transported block to cause the tsunami (fig. 3.11). The direction of displacement (fig. 3.12) is in agreement with the maximum stress axis determined from the focal mechanism of the earthquakes (Swanson and others, 1976). During the 1975 deformation, there were associated swarms of earthquakes and ground cracking on the ERZ.

Geodetic data from stations on the north and south sides of the Hilina fault system shows displacements in the same direction but of different magnitudes, with both elongation and shortening of lines across the fault. Surveys of lines across the fault zone in 1970 prove that shortening does occur (Swanson and others, 1976), moreover, the net strain across the zone since 1914 shows overall shortening.

Leveling surveys across the south flank of Kilauea between 1958 and 1971 shows that the north side of the Hilina fault system has been uplifted relative to the south coast by 1.8 to 2.1 m.

The Hilina fault system has long been interpreted as a



Figure 3.11. Inverse refraction diagram to obtain tsunami generation area showing area of landward subsidence and offshore uplift (from Furumoto and Kovach, 1979).



Figure 3.12.

 Map of south flank of Kilauea on the island of Hawaii showing slip directions. Arrow lengths linearly indicate dip of slip vector with 9 km being horizontal and 0 km vertical (from Crosson and Endo, 1981).

gravity fault zone, the analogy being made with large landslides (Stearns and Macdonald, 1946; Moore and Krivoy, 1964), but this interpretation conflicts with the data suggesting historical horizontal shortening across the system, uplift of its northern side, and southward tilt of the fault blocks. Macdonald (1956) later abandoned the 'landslide' hypothesis, and suggested that tumescence in the summit and rift zones causes near vertical faults with the inland side upthrown.

Study of the focal mechanism of the November, 1975, Kalapana earthquake at the east end of the Hilina fault system led Ando (1979) to propose a near-horizontal slip-plane at a depth of 10 km, with southward movement of the southern flank of Kilauea owing to magma injection of the ERZ. Study of the aftershocks by Crosson and Endo (1981) confirmed a sub-horizontal slip-plane and SSE directed slip vectors, and emphasized the role of a weak horizontal (low velocity) layer at a depth of 10 km on which the south flank of the Kilauea shield is supposed to slide southwards in response to magmatic injection in the rift zone. This model is preferable to the 'landslide' models (Swanson and others, 1976), in that it provides for the accumulation of compressive stresses and vertical uplift of the zone between the Hilina fault system and the ERZ during phases of magmatic injection, and subsequent stress release by southward sliding on a weak layer at or below the base of the volcanic pile.

The available data suggest that the faulting at depth does not break cleanly to the surface, but is distributed or compensated by broad subsidence on the land area, with gently dipping listric faults that extend along the hyaloclastic deposits at

depth and dip SE at between 4° and 10° . Furumoto and Kovach (1979) suggest that the interface is on the ancient sea floor, with the toe of the block moving as a thrust at a depth of 5 to 7 km. These models are in general agreement with the geomorphic, seismologic, geodetic and tsunami data.

3.6.3. Koae Fault Zone

The Koae fault zone defines the northern edge of the mobile south flank of Kilauea (Swanson and others, 1976), as shown in Figure 3.3 and Plates 1 and 2. This fault zone spans the gap between the southwest and ERZ and trends EW a few kilometers south of Kilauea caldera. This fault zone consists of a pattern of <u>en echelon</u> cracks and normal faults with north-facing scarps that are usually less than 5 m high. During initial stages of eruptions or ground-cracking events on the East or Southward rift zones, the Koae fault zone has many more earthquakes from seismic swarms than does the Hilina fault zone (Swanson and others, 1976). Swanson and others (1976) indicate that the Koae fault zone is not generally the site for eruptions, but is more of a "tear away zone" as the result of dilation due to magma intrusion into the neighboring SRZ and ERZ.

3.6.4. Hanuapo-Kaoiki Fault Zone

The Hauapo-Kaoiki fault zone follows the SE boundary of Mauna Loa (fig. 3.3), and is of uncertain activity. No historic flows or eruptions have occurred along this zone and it is not characterized by well defined seismic activity, although some earthquake epicenters are on, or near, this zone. This zone is farther from the siting area than the Hilina fault zone and is of shorter exposed length and presumably of lower seismic potential. No maximum magnitudes are assigned to this fault zone.

3.6.5. Kealakekua-Kholo Fault Zone

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This zone has an acurate pattern that is similar to the Hilina fault zone on the south flank of Kilauea, and may have a similar gravitational relation to the actively growing western flank of Mauna Loa. The length is poorly defined, because much of the fault zone is offshore. The Ms = 6.25 earthquake of 1950 is the maximum historic earthquake for this fault zone.

4.0 VOLCANIC-RISK ASSESSMENT OF THE PUNA DISTRICT

4.1 Volcanic and Structural Features of Lower East Rift Zone4.1.1 Structure

For the purpose of this report, the Lower East Rift Zone (LERZ) is the sector ENE of Puu Kaliu (elevation 800 ft or 200 m above sea level) to sea level. Topographically, the zone runs along the crest of a broad ridge 3 km wide, from which gentle slopes descend to the NE and steeper slopes to the SE. Structural and volcanic features consist of faults and open fissures, some without lava and others with aligned spatter cones and ramparts of agglutinate. Faults and fissures are remarkably linear and parallel along a trend of N 55-60 E for distances of up to 10 km (fig. 3.9). Cinder cones and small lava shields (with and without craters), steep-sided tuff rings with deep craters resulting from phreatic eruptions, and broad expanses of lava are scattered along the central part of the rift zone.

The distribution of faults in the lower ERZ (fig. 3.9) suggests a concentration in the Kapoho area, and a scarcity in the PuuKaliu - Kiapu area. Numerous faults have been mapped in the middle part of the ERZ (west of the area shown in fig. 3.9), especially on its northern side (Holcomb, 1981). The scarcity of faults in the western side of the map is because they have been buried under the extensive lavas of the 1790 and 1840 eruptions.

<u>4.1.1.1 Fissures</u> The 3 km-wide zone of fissures and faults coincides with a zone of eruptive vents. No vents have been identified outside the zone on the flanks of the ridge. There is

abundant evidence of vent alignment along fissures, but there is no example of vents that were fed from faults, and this indicates that the mechanisms of fissuring and faulting are different. Since the surface rocks of the LERZ are mostly less than 500 years old, the structural features are well preserved and commonest in the oldest lavas that have escaped innundation during more recent eruptions. The oldest identifiable fissure in the LERZ fed a chain of small shields, spatter cones, and cinder cones along the 3 km long Puu Kii-Halemahina alignment, which is thought to be 300 to 500 years old by Holcomb (1981), but is thought to be more than 750 years old by R. J. Moore (personal communication, 1981). This fissure is centrally located in the LERZ and flows from it descended the LERZ to sea level east of Kapoho.

The next youngest activity was from the Puu Honaula fissure located immediately south of the Puu Kii zone. Three cinder cones, were built on low lava shields along this fissure. Another fissure close to the south edge of the LERZ was also active and both are dated at 500 to 750 years B.P. (R. J. Moore, pers. comm.).

Very extensive lavas of the eruptive phase of 1750 issued from fissures along much of the length of the ERZ. Just west of the LERZ long fissures from this eruption follow the northern and southern edges of the rift zone (fig. 3.9), and the flows flooded much of the crest and SE flank.

A 9 km fissure at the northern extremity of the ERZ opened during 1840 (fig. 3.9) and discharged lava about one mile down the NE flank. The volume of this flow totalled about 281,000 cubic yards and covered an area of 6.6 square miles. An addi-

tional discharge of lava is believed to have come from vents below sea level.

The fissures formed during the 1955 eruption are short and are off-set <u>en echelon</u> to the left toward to NE. In the middle part of the ERZ the main fissure is at the southern margin of the zone; to the ENE it steps toward the center of the rift. A gap of about 2 miles separates the two offset sections, and the HGP-A well is sited near the NNE end of this gap.

The 1960 eruptions took place from a short fissure near the NE end of LERZ, near the center of the Kapoho graben (right side of fig. 3.9). The 1977 flank eruptions occurred in the middle part of the ERZ, to the WSW of LERZ, on a single fissure near the center of the zone.

Historic fissures have formed immediately prior to eruptions, and developed by rapid growth of cracks to widths of up to 30 cm in a few hours, during swarms of microearthquakes. Fissures rarely exceed 1 meter in width and extend laterally at rates of up to 100 meters per hour. For each eruptive episode they have developed in different places within the width of the ERZ, and no case of regeneration of a pre-existing fissure is known. Each phase of fissuring and eruption typically occurs along a single linear fissure system. During one eruption, that of 1750, there may have been simultaneous eruption from parallel fissures, but this is very exceptional. The fissures represent the result of surface dilation and tensile fracture of rock due to dike injection at depth. The mechanism by which they are formed is summarized in a later section (Section 4.2.4.3). <u>4.1.1.2 Faults</u> Zones of parallel normal faults of small displacement occur throughout the ERZ and are best developed within the northern part of the middle rift zone and in the Kapoho area of the LERZ (fig. 3.9). The displacement pattern gives rise to step-faults downthrown to the NW and SE. Along the southern edge of the LERZ there is a predominence of minor faults downthrown to the SE.

The ERZ faults show displacements of only a few meters, even where they cut the oldest rocks, and they are remarkably linear, with no tendency to curve or branch. In these respects they differ markedly from faults of the Koae and Hilina fault systems, which are long systems of curving and branching faults with large displacements (up to 500 meters) that evolved over long periods of time. The ERZ faults and the systems cutting the south flank of Kilauea are not only spatially separate but show contrasts of form and history reflecting their distinctly different origins.

Faulting in the LERZ normally occurs during or immediately before an eruption in the same part of the rift. Examples are the eruptions of 1955 and 1960. In 1924, however, strong faulting was observed in the LERZ without an observed eruption of lava (Jaggar and Finch, 1924). Many earthquakes were felt at Kapoho on April 21, 1924, and the next day a fissure 15 feet wide opened across the coast road. Vertical displacement reached 8 to 12 feet. Near Kukii a graben block 20 feet wide sank 6 feet, and numerous cracks up to 3 feet wide developed nearby. This episode is thought to have been due to flow of magma into the lower ERZ, because it was accompanied by rapid drainage of the Halemaumau pit crater. The occurrence of earthquakes in the submarine part

of the ERZ during the same period suggests that an eruption below sea level may have drained magma from the ERZ.

4.1.2 Examples of Recent Flank Eruptions

<u>4.1.2.1</u> 1955 East Puna Eruption (Macdonald and Eaton, <u>1964</u>): After a repose of 273 days, Kilauea began to erupt on the morning of February 28 from a new fissure on the southwest slope of Puu Honaula, 24.5 miles ENE of Kilauea caldera (fig. 4.1). The outbreak was preceded for several months by earthquakes, which gradually increased in number to several hundred a day just before the eruption. Discharge of lava continued at the initial vents for only 28 hours and on March 1 was replaced by mild phreatic explosions and clouds of steam.

On March 2, a new series of earthquakes accompanied the formation of fault scarps and opening of fissures 2 miles farther northeast, and at 1415 hours lava broke out on the fissures. Through the next 2 days the eruptive fissures gradually extended another 2 miles NE, to the outskirts of Kapoho village. Lava fountains at the main vents reached a height of at least 800 feet, and flows from them covered approximately 1,100 acres. Activity in that area stopped on March 6.

On March 6 a new series of earthquakes commenced, originating in the area 2 to 12 miles southwest of the initial outbreak, and a new outbreak in that area was predicted. On March 12 lava broke out in that region, and between then and March 27 a series of new vents developed along the rift zone for 4 miles to the southwest. Three lava flows from these vents entered the ocean.

Activity ceased on April 7 but resumed weakly on April 24



Figure 4.1. Map of the eastern part of the Puna District, Island of Hawaii, showing the vents and lava flows of the 1955 eruption of Kilauea Volcano (Macdonald, 1959).

and gradually increased until a strong resurgence occurred on May 16. New flows covered the upper parts of earlier flows, and some new area, including one village. The eruption ended abruptly on May 26.

The volume of erupted material was approximately 141 million cubic yards. The flows covered an area of about 3,900 acres, of which 1,100 acres was under cultivation. Approximately 6.3 miles (10 km) of public road and many miles of cane-field road were buried, and 21 houses were destroyed. There were no human casualties.

The erupted lavas were basalts, becoming slightly more mafic as the eruption progressed. The temperature of lava as it was erupted was approximately 1,100 degrees centigrade.

Tilt records at the Pahoa seismograph station (north of the ERZ), and remeasurement of a triangulation network, showed that northward tilt began two days before the start of the 1955 eruption, and occurred again before the second and major eruptive phase. This suggests that dilation of the ERZ took place before and during the ground fissuring and shallow microseismic activity that immediately preceded the eruption. Ground deformation consisted of a general uplift of the LERZ of at least 0.4 m, accompanied by a 0.3 - 0.4 m subsidence of the zone adjacent to active fissures. Horizontal displacements were normal to the LERZ and ranged from 0.2 to 1.6 m. During the easterly extension of the fissure a pre-existing fault NW of Kapoho was rejuvenated, with a new displacement of 1.6 m (SE side down).

4.1.2.2 1960 Kapoho Eruption (Richter and others, 1970): On

the evening of November 14, 1959, after a quiet period of nearly five years, Kilauea Volcano renewed activity with an eruption in Kilauea Iki, a collapse crater adjacent to the main caldera. The eruption consisted of 17 separate eruptive phases, which ranged in duration from one week to less than two hours. At the cessation of activity on December 20, 1959, Kilauea Iki Crater held 50 million cubic yards of lava in a lake 335 feet deep.

After the summit eruption, shallow earthquake hypocenters migrated out along the ERZ and rose from 2 km to very shallow depths. On 13 January, an intense series of earthquakes near Kapoho was accompanied by subsidence of a graben bounded by two parallel faults trending N 60 E (fig. 4.2). The southern boundary fault running through the village of Kapoho had been active in 1924, when a maximum of 3.8 meters displacement was measured, and again in 1955 when minor displacement was observed at the west end of Kapoho. By the end of the day displacement reached a maximum of about 1.1 meters and the total length of the fault measured about 2.7 km. Similar movement on the northern fault (near the town of Koae; see fig. 4.2) reached a maximum displacement of 4 feet (1.3 meters) and a length of 3.04 km. At 1935 hours an eruption broke out along a 320 meter fissure somewhat north of the center of the graben and parallel to the boundary faults. No lava emerged from the faults. Fountaining up to heights of 100 meters was soon accompanied by a discharge of lava, mainly from the east end of the fissure. The fissure reached a maximum length of 370 meters around 2130 hours at which time activity began to concentrate in the central part of the fissure, and the rate of discharge of lava continued to increase.



Figure 4.2 Map showing the eruptive fissure of the 1960 eruption (Richter and others, 1970) in the Kapoho area of the Lower East Rift Zone, and the active faults of the Kapoho graben. The maximum extent of the lava field, and isopachs of the pumice blanket are also shown. The 1960 lavas were unusually thick see cross-section B-B' (inset).

4.1.2.3 The 1977 eruption (Moore and others, 1980; Dzurisin and others, 1980): Kilauea volcano began to erupt on September 13, 1977, after a 21.5-month period of quiescence. The eruption was preceded by four intrusive events during 1976 and early 1977. Motion of magma was reflected in deflation of the summit area, migration of shallow earthquakes into the upper and middle ERZ, extensional deformation across the Koae fault, and inflation of the ERZ. Harmonic tremor in the upper and central ERZ and rapid deflation of the summit area occurred for 22 hours before the outbreak of surface activity.

On the first night, spatter ramparts formed along a discontinuous, <u>en echelon</u>, 5.5 km-long fissure system (fig. 4.3) that trends N 70 degrees E between two prehistoric cones, Kalalua and Puu Kauka. Activity soon became concentrated at a central vent that erupted sporadically until September 23 and extruded flows that moved a maximum distance of 2.5 km to the east. On September 18, new spatter ramparts began forming west of Kalalua, extending to 7 km the length of the new vent system. A vent near the center of this latest fissure became the focus of sustained fountaining and continued to extrude spatter and short flows intermittently until September 20.

The most voluminous phase of the eruption began late on September 25. A discontinuous spatter rampart formed on a 700 m long segment near the center of the new, 7 km-long fissure system; within 24 hours activity became concentrated at the east end of this segment. One flow from the 35 m-high cone that formed at this site moved rapidly southeast and eventually reached an area 10 km from the vent and 700 m from the nearest house in the

Sea water appears to have entered the east end of the fissure about this time, because dark ash-laden steam began to be discharged from the east end of the fissure.

During the next 37 days of virtually uninterrupted activity, 160 million cubic yards of lava, covering about 2,500 acres, were erupted (fig. 4.2). The lava was at first confined to the graben and flowed down the northern side until it reached the sea around 800 hours on the 15th. After the 19th the lava began to over-top the margins of the graben and spread to both the north and south. An effort was made to restrict the southward flow by a series of three successive artificial barriers, but all of these were eventually overrun. Nearly all the lava was of the aa type; the main exceptions were channels within the central interior of the flow and small toes that from time to time broke out from the advancing front or through the base of barriers.

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A cinder cone at the main eruptive vent grew to a height of about 64 meters and discharged fountains of incandescent scoria to heights of 300 meters above the vent. The small villages of Kapoho and Koae, a United States Coast Guard station, and a number of residences along the coast were destroyed.

Almost concurrent with the beginning of the flank eruption, the summit area of Kilauea rapidly deflated as magma moved from beneath the summit into the rift zone to the flank eruption. Culmination of the summit subsidence occurred on February 7, 1960, when the floor of Halemaumau – a deep crater in Kilauea caldera – collapsed because of the withdrawal of the still-fluid core of the 1942 lava lake. Two smaller collapses on March 9 and March 11 in Halemaumau marked the end of the eruption.



Figure 4.3. Map showing eruptive products and active structures of the 1977 eruption in the middle East Rift Zone (Moore and others, 1980).

evacuated village of Kalapana.

An estimated total volume of 35 million cubic meters was produced during the 18-day eruption. Samples from active vents and flows are differentiated quartz-normative tholeiitic basalt, similar in composition to lavas erupted from Kilauea in 1955 and 1962. Plagioclase is the only significant phenocryst; augite, minor olivine, and rare orthopyroxene and opaque oxides accompany it as microphenocrysts. Sulfide globules occur in fresh glass and as inclusions in phenocrysts in early 1977 lavas; their absence in chemically-similar basalt from the later phases of the eruption suggests that more extensive intratelluric degassing occurred as the eruption proceeded. Bulk composition of lava varies somewhat during the eruption, but the last basalt produced also is differentiated, suggesting that magma withdrawn from the summit reservoir during the rapid deflation had not yet been erupted.

4.1.3 Frequency of Eruptions in the East Puna District

Considering only the lower ERZ, the average frequency of lava flows for the 231 years of recorded activity has been one eruption per 46 years. Because the spacing of eruptions is so irregular and the historic record contains only a small number of such events, this average has little meaning in terms of the probability of an eruption in a given period of time. Moreover, the frequency of lava flows at an individual site within this zone is much lower than that of the zone as a whole.

4.1.4 Deformation Associated with ERZ Eruptive Phases A wealth of data suggests that the Kilauea magmatic system consists of a vertical holding reservoir 2 to 5 km beneath the summit caldera. This reservoir is periodically fed by primary magma from depths of about 65 km, which usually causes inflation of the summit region and numerous shallow earthquakes owing to failure of the volcano superstructure. Inflation may be followed by summit eruptions, or by deflation accompanied by migration of seismic activity as a result of lateral movement of magma into a rift zone at depths of 3-5 km. Upward movement of magma under the rift zone (probably displacement of magma remaining from previous injections) causes tensile failure and dike injection accompanied by shallow earthquakes, dilation and uplift of the rift zone. As dikes ascend, fissures extend to the surface and widen rapidly, begin to emit fumes, and often emit lava fountains along their central parts. The fissures extend laterally at rates of up to 100 meters per hour.

The sequence of events during a typical ERZ eruption starts with shallow earthquake swarms of decreasing focal depth, followed by dilation of the active zone, formation of fissures, faulting and/or rejuvenation of nearby pre-existing faults, followed by eruption. The premonitory seismic and dilational phases may last as little as two days, and fissuring followed by eruption may occur in a few hours. This sequence may be repeated as a fissure extends laterally, or as successive phases of magmatic injection take place during a protracted eruption.

Seismicity of the rift zones is concentrated in a zone 8 km wide under the rift zones and immediately to the south. Hypocenters are concentrated at depths of 5 to 10 km (fig. 4.4), with a very sharp decrease in the number of earthquakes at focal



Figure 4.4. Earthquake hypocenters plotted within 10-km wide sections centered on lines A-A' and B-B' oriented normal to the rift zone as shown in Figure 3.10. Earthquakes of all magnitudes and with standard errors in epicenter and depth less than 2.5 km are included. Hypocenters for earthquakes in 1976 are marked with open circles and those in 1977 are indicated by black dots. The column of progressively shallow earthquakes immediately south of the axis of the rift in the middle East Rift Zone in section B-B' mainly occurred about the time of the September 1977 mid-east rift eruption (Koyanagi and others, 1981).

depths greater than 10 km (fig. 3.10). Earthquake epicenters cluster along the ERZ during the early period of an eruption, but are dispersed in the area of the Hilina fault system during the middle and later periods (Swanson and others, 1976). The north flank of the ERZ is strikingly aseismic, and the seismicity is strongly asymmetrical in a north-south direction, showing the tectonic instability is concentrated in the ERZ, within its south flank, and at depths of less than 10 km within the lower part of the volcanic superstructure and above the depressed top of the prevolcanic oceanic crust. Seismic sections across the ERZ (fig. 4.4) show that hypocenters define a diffuse zone dipping at about 45 deg. to the SSE (Koyanagi and others, 1981).

4.1.4.1 Horizontal Displacements in the ERZ: Horizontal displacements across the ERZ and the south flank of Kilauea have been obtained from triangulation surveys in 1896, 1914, 1949, 1958, and 1961, and from geodimeter trilateration surveys in 1970 and 1971 (Swanson and others, 1976). The observed displacements are large and systematic: displacement vectors are normal to the trend of the ERZ, and displacements are associated in time and space with fissuring and eruptive events (figs. 4.5A and B). During the 1955 eruption the Puu Kaliu and Puu Honaula stations north of the fissure were displaced north relative to stations far to the north (fig. 4.6). Stations to the south of eruptive fissures and on the south coast show larger SSE displacements (fig. 4.5; B, D, E and F). In a few cases horizontal displacements can be related to specific events in the ERZ: During the 1955 eruption there was 210 cm of extension near Puu Honaula, and in 1969 a 2 km wide zone west of Alae Crater in the upper ERZ



Figure 4.5. Horizontal displacements of trilateration stations for various periods during the years 1896 - 1970. Base stations for the determination of displacement vectors (arrows) are underlined (Swanson and others, 1976).



Figure 4.6.

Vertical displacement and topographic profiles across Lower East Rift Zone and eastern part of south flank between 1921, 1958, and 1973. Datum is 1958 elevation of BM 359.3. Inset shows location of bench marks, leveling route (dashed line), line of topographic profile (light solid line), and generalized eruptive fissures for 1955 eruption (heavier solid lines). Displacement data are projected onto line of topographic profile. Contour interval on inset map is 100 m (Swanson and others, 1976). extended 105 cm. These extensions are of the same magnitude as the aggregate width of observed fissures, showing that the fissures, and to a much lesser degree the faults, are responsible for most of the strain. The evidence suggests that the dilations of the ERZ immediately preceding eruptive events, are accompanied by surface fissuring, which result in relative horizontal displacements of the order of 1-2 meters.

<u>4.1.4.2</u> Vertical Displacements in the ERZ: Surveys of benchmarks along the Pahoa-Kalapana highway were made in 1921, 1958, 1969, and 1973. These indicate 0.2 m of uplift of the ERZ during 1921-1958 (fig. 4.6), and a progressive uplift of 0.3 m during 1958-1973 (fig. 4.7A). These uplifts are broadly sinusoidal in shape and are centered 0.5 to 1.5 km south of the axis of the ERZ. The 1958-1973 displacement profiles show development of a narrow graben at an elevation of 270 m (840 feet) on the south flank of the middle ERZ, but this cannot be identified with any mapped structure.

Another levelling line extends along the Pahoa-Pohoiki highway, which passes the HGP-A well site (fig. 4.7B). This shows progressive development of a 0.12 m subsidence with its axis close to the line of 1955 fissures, which has been interpreted as due to thermal contraction following the 1955 eruption (Swanson and others, 1976). We prefer to interpret this subsidence as due to residual elastic extensional strain, or to withdrawal of magma from the deeper parts of the 1955 dike system.

Data on vertical displacement therefore suggest that the south flank of Kilauea has been increasingly uplifted toward the ERZ and Koae fault system, with a maximum displacement within or



Figure 4.7.

Vertical displacement and topographic profiles across Lower East Rift Zone of Kilauea between 1958 and 1973. (A) Profiles between BM YY80 (Pahoa) and BM10 (Kalapana); (B) Profiles between BM YY80 and BM YY174 (Pa hoiki). Datum is 1958 elevation of BM YY80. Inset maps show locations of leveling route, key bench marks, and line of topographic profile. Displacement data are projected onto line of topographic profile. Contour interval of inset maps is 150 m (Swanson and others, 1976). just south of the rift zone. Records of tilt near the ERZ show that phases of uplift correlate with periods of shallow seismicity that precede or accompany intrusive and/or eruptive events.

4.1.4.3 Mechanical Models of ERZ Deformation: The curvature of the Kilauea rift zones, their parallelism to the strike of the southeast flank of Mauna Loa, and the asymmetry of structure across the volcano have been attributed to the gravitational loading of the Kilauea volcanic pile on the flank of Mauna Loa. The north flank of the volcano is buttressed, whereas the south flank is free to move SSE in response to dilations caused by magma injections in the rift zones (fig. 4.8) The injections into the rift zone occur during the filling of the high level magma reservoir beneath the summit, and are a result of the ascent of magma to the surface and the tumescence of the summit region. This creates a hydraulic head in the magma column adequate to cause lateral injection of magma into the still molten roots of the rift zone. Increased magmatic pressure then results in lateral and upward injection of dikes.

The deformation that accompanies upward injection of a dike has been analyzed theoretically (Koide and Bhattacharji, 1975a and b; Dieterich and Decker, 1975; Pollard and Holzhausen, 1979), and excellent observations of such deformation have been made in Iceland (Bjornsson and others, 1979). When the fluid pressure at the top of a dike exceeds the least horizontal stress in the adjacent rock, tensile failure can occur at the apex of the dike, and a fissure can propagate upward in a plane normal to the least principal stress in the rock. Under a ridge such as the ERZ the plane of tensile failure would be steep and located below the



Figure 4.8.

Crustal structure models across the summit region (A-A'), East Rift Zone (B-B'), and the submarine part of the Lower East Rift Zone (C-C'), showing the relation between injection into the rift zone and faulting in the Hilina fault system according to the "landslide" model (Swanson and others, 1976). axis of the ridge (Fiske and Jackson, 1972). The rate of upward propagation of the crack depends on the magmatic pressure and on the speed with which magma can rise. At any instant during ascent the region between the apex of the dike and the free surface consists of two parts: A far field in which horizontal compressive stress is increased, and slight upward deformation of the surface occurs, and a near field of conical cross-section above the dike in which horizontal stresses are decreased and the surface subsides. Between these two regions there are two surfaces of maximum shearing stress that are potential fault surfaces. Thus the surface deformation above an ascending dike, when it has reached 100 - 200 m below the surface, consists of a broad, slight uplift, with a narrow central depression cut by a fissure. On each side of the fissure normal faults of smalldisplacement may develop to form a graben, or pre-existing faults may be re-activated.

The width of the zone that is affected by faulting during a dike injection episode is determined by several unpredictable factors, such as the number of dikes and their widths (the total horizontal strain), the depth of the top of the dikes, their attitude, the presence of pre-existing planes of weakness, and the cohesive shear strength of the rocks (Koide and Bhattacharji, 1975a and b; Dietrich and Decker, 1975). The graben that formed during the 1977 eruption was only 100 m wide, whereas the Kapoho graben that subsided during the 1960 eruption was 900 m wide. Leveling along the Pahoa-Kalapana road between 1958 and 1964 indicated subsidence of a sharply defined zone 600 m wide, presumably during the 1960 eruption further to the northeast.

This was probably the effect of a dike that failed to reach the surface, and the subsidence was located to the south of the projection of the 1960 fissure, which led Dietrich and Decker (1975) to propose that the dike dipped to the south.

At present the ground deformation data for a LERZ eruptive event are not adequate for predicting the distribution of faulting, but the zone of faulting is not likely to be more than 1 km wide, and commonly will be much narrower than this. During intrusion events faulting may occur without fissuring, and the fault zone is likely to be on the south side of the ERZ. During fissuring and eruption events faulting may occur a few hundred meters on either side of the fissure. In either case vertical displacements of 1 to 2 meters are to be expected, with a maximum of 4 meters, and fault movement will occur during a period of a few hours to a few days immediately before an eruption.

When magma finally reaches the surface the axial zone of subsidence with its marginal faults becomes stabilized and uplifted. When dikes are not vertical the surface deformation is asymmetrical, with greater uplift over the hanging wall of the dike (Dieterich and Decker, 1975). The asymmetry of the vertical displacement profiles across the ERZ led Dietrich and Decker (1975) to suggest that the dikes dip SSE at 45 degrees, and this dip is similar to that of the zone of earthquake hypocenters under the ERZ (see fig. 4.4). Swanson and others, (1976) prefer a vertical dip for the dikes, but the attitude of the dikes remains unknown.

The factors that determine whether a summit inflation will be followed by magma flow into the rift zones, and whether such a



flow would result in a flank intrusion or eruption, are impossible to evaluate with our present knowledge. Similarly it is not possible to predict where in the rift zone an eruption is likely to occur.

4.2 The Puu Honaula Area

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4.2.1 Outline of the Geology and Structure

The following summary, and the accompanying geological map (fig. 4.9) are based on detailed maps by Holcomb (1981), and on the unpublished map of the Kapoho quadrangle by R.J. Moore. We have made slight modifications as a result of our own photogeological interpretation and a brief visit to the area.

The area lies across the upper part of the Lower East Rift Zone (LERZ), which is a broad shallow ridge between sea level and 800 feet elevation. In the western part of the area the top of the ridge is a shallow trough-like depression bordered by higher ground formed by the Puu Kaliu vent-fissure zone to the south, and by fissure zones of the 1790 and 1840 eruptions to the north. Further east the rift zone has a central low ridge composed of small shields and cones of the Puu Kii and Puu Honaula fissure zones. The southeast slope of the rift zone south of Puulena is unusually steep, and a lava mantled fault scarp is inferred to underlie this slope.

The oldest rocks are the cinder and spatter cones of Kiapu, which underlie a lithic tuff dated at 1,000 years before present (R.J. Moore, pers. comm., 1981). Small cones southwest of Puulena and at Puu Pilau may be of similar age.

The Puulena crater walls expose thin lava flows that are



Figure 4.9. Geological map of the Puu Honaula area, East Puna Hawaii (modification of map of Holcomb, 1981, by B. Baker using field studies, photogeology, and pers. comm. with R. Moore). capped by a lithic tuff dated at 1,000 years before present (YBP) and represent a small shield built on fissures along which deep pit craters developed, probably during a phase of magma withdrawal.

; In the northeast, an alignment of small low shields, spatter cones, and cinder cones marks the line of the Puu Kii eruptive fissure. Holcomb (1981) estimated the age of these rocks at 350-500 YBP, whereas R.J. Moore (pers. comm., 1981) reports they are older than the Puu Honaula vents to the south, which he dates at 500-750 YBP.

The most extensive lavas are those of the 1790 eruption, which flooded a large portion of the crest of the ERZ. In the northwest of the area these flows were derived from a fissure system higher up the rift zone, but in the south they were erupted from a fissure zone extending from the southwest corner of the area past the northern flank of Puulena. These flows ponded around Kiapu and almost covered the Puulena shield.

The northwest portion of the area consists of flows from the 1840 fissure, which lies at the northern edge of the middle ERZ, to the west of the area. These flows descended the northeast flank of the rift zone.

The most recent lavas were erupted in 1955 from a discontinuous en echelon fissure south and east of Puu Honaula. They are of limited extent and thickness in the mapped area (fig. 4.9).

The steep southern flank of the Puulena craters is believed to represent a buried normal fault downthrown to the southeast (Holcomb, 1981). A localized normal fault cuts the south side of the Puu Honaula cinder cones. The western end of the southern

fault of the Kapoho graben ends at the eastern boundary of the area, at the junction of the Puu Kii and 1955 flows. The last two faults are downthrown to the southeast less than 2 meters.

4.2.2 Frequency of Eruptions

It is difficult to estimate the average frequency of flows accumulating in a vertical sequence at a given site in the Puu Honaula area because there is no dated horizon in the prehistoric lavas. A crude estimate can be obtained from the measured depth of the interface between submarine and subaerial lavas in the HGP-A well. This horizon was logged at a depth of 1750 feet (533 m) or 1175 feet (358 m) below present sea level. The rate of subsidence measured by tide gauges is about 4.1 mm per year. If this rate is assumed for the area of the HGP-A bore hole, the age of the first subaerial lava would be approximately 87,313 YBP. Assuming an average thickness of 18.3 feet for individual lava flows above this level, an average frequency of one flow per 898 years is obtained for the site of HGP-A well. This estimate may be too low, as some data suggest the rate of subsidence in the LERZ is greater than that of the coast line at Hilo, but this factor cannot be determined from the presently available data. Conversly, if some of the section of HGP-A well is made up of sills injected between lava flows, the frequency of surface flows would be correspondingly less.

Within the Puu Honaula area (fig. 3.9), an area of about 20 square kilometers, there have been at least 6 periods of eruptive activity in the last 1,000 years, with an average recurrence interval of 166 years. Three events have occurred in the last 191 years for a recurrence interval of 64 years. In the entire LERZ,
4 major eruptions have occurred in 191 years, with an average recurrence of 48 years. This is a low level of activity compared to the ERZ as a whole, for which Klein (in press) lists 20 extrusive and 19 intrusive events since 1918, with an average recurrence interval of 3 years for each type of event. We estimate that a conservative recurrence interval of 40 years applies to the Puu Honaula area.

4.3 Volcanic Hazards

4.3.1 Introduction

A survey of the volcanic hazards of the island of Hawaii by the U.S. Geological Survey (Mullineau and Peterson, 1974) concludes that lava flows and volcanic related ground rupture to be the main hazards to property in the East Rift Zone (ERZ). We consider the probabilities for occurrence of these hazards to be the highest for any region on the island (and possibly in the world). Other hazards such as falling rock fragments, volcanic fumes, earthquakes, and tsunamis are much less serious.

4.3.2 Surface Deformation

Surface deformation in the LERZ consists of periodic uplift and horizontal extension, accompanied by fissuring and possibly normal faulting. All the evidence suggests that such deformation takes place before eruptions, or before renewed eruptions during lengthy periods of activity. Relatively slight deformation also occurs during periods of intrusive activity.

The broad arching, uplift, and tilting that accompanies extrusive events is not of sufficient magnitude or rate to constitute a hazard to property. The significant deformation hazards

are fissuring and faulting.

Within the area mapped (fig. 4.9) there are 16 individual fissure systems, and others may lie buried under lava flows. These have formed during a minimum of 6 eruptive episodes during the last 1,000 years in a zone 3 km wide extending from Pawaii Crater to the Lava Tree State Park.

The majority of fissuring events have formed lines of <u>en</u> <u>echelon</u> fissures, and development of paralled fissures is rare. Therefore we adopt a conservative model of formation of a single fissure 1 m wide every 40 years. The area affected by such a fissure would be 5,000 square meters, which is about 0.002 per cent of the area of the LERZ in Figure 4.9. There appears to be no control for the location of new fissures, which randomly form anywhere in the active zone. The risk to property is therefore a function of the frequency of fissuring (1 in 40 years), the average width of a fissure (1m), the width of the zone liable to fissuring (3,000 m), and the dimensions of the engineered structure at risk in a directional normal to the rift zone. The probability of a fissure intersecting a structure during a period of 40 years (the effective life of a plant) is shown in Table 4.2.

The risk of damage is proportional to the dimensions, shape, and orientation of the structure under consideration. For extensive structures, such as steam pipelines, that must cross some part of the rift zone the risk of damage is considerable, unless the structure is specially designed to accomodate large displacements. For smaller structures, such as generating plants, the risk is less, but the cost of damage may be greater.

TABLE 4.2

Dimensions of engineered structures versus probability of damage for a 40 year period in the LERZ.

Horizontal dimension of structure in direction normal to rift zone (ft)	Probability (per cent) of damage in a 40 year period
3,000	100
500	17
100	3
50	2

4.3.3 Hazards from Eruptions of Lava

The risk of an installation being destroyed by lava is the highest of all potential risks in the Puu Honaula area, because for a single eruptive event, the surface area affected is greater than the surface area affected by a fissuring and/or faulting event. Two types of risks from lava flows can be distinguished; (1) those associated with lava from an eruptive vent directly under or adjacent to the site and, (2) those due to lava flows coming from a more distant source.

Eruptive vents that have been active in the recent past are of three types. In the opening stages of an eruption, they are linear fissures that discharge fountains of incandescent spatter and scoria. With time these become more localized and discharge flows of lava. Cinder cones may form where there is prolonged ejection of pyroclastic material. Finally, in those areas where ground water is abundant or where sea water has access to the fissure system, steam blast eruptions may eject lithic debris, including blocks a foot or more in diameter. The effective radius of the effects of explosive discharge from these three types is essentially the same. They are unlikely to have a serious effect beyond a distance of a kilometer.

The fact that no eruptive vents have been found outside the boundaries of the LERZ makes it unlikely that one will occur there in the future, but this possibility cannot be completely discounted. Within the rift zone, most eruptions have been on the south side. It has been suggested the rift zone is moving southeastward (Swanson and others, 1976), but the evidence for this interpretation is not conclusive. There is convincing evidence, however, that new vents rarely coincide with old ones, and by this reasoning, one of the safest siting areas in the rift zone may be on an old cinder cone.

From these relations we conclude that the danger from a new eruptive vent is lowest outside the northern or southern boundaries of the rift zone. Within the rift zone, there is a marginally lower risk at a site situated on an older vent, especially within the northern half of the rift zone. These risks must be weighed against the practical disadvantages of increasing the distances steam must be transmitted.

The risk of a site being overrun by lava from a vent outside its immediate vicinity is largely a function of topography. Low areas into which lava is likely to be channeled have the highest risk, and elevated ground or areas in the lee of hills standing between the site and possible sources would have a much lower risk. Ground with a high slope angle will be covered by thinner flows than flat ground or depressions into which lava could be ponded, but flow velocities on these slopes here would be higher.

Figure 4.10 assesses the level of risk in the study area from lava flows as highest, intermediate, and lowest, using the principles of risk assessment outlined in this section. These are intended as general guidelines, and should be examined on a site-specific basis following the final selection of a site for installation of permanent structures.

Average thickness and rate of advance of lava flows may also be crudely calculated. Neglecting the eruption below sea level in 1884 and another event of a similar nature in 1924, five eruptions have occurred at elevations below 1,000 feet. Lava flows



Figure 4.10. Map showing relative risk of lava flow incursions. Arrows show likely directions of flow of lavas in future eruptions. The most likely paths of flow are shown with thick arrows. Pl marks areas with least risk of lava incursion and P6 marks areas of intermediate risk. Unshaded areas are those of greatest risk.

from eruptions, such as that of 1977, which occurred at higher elevations would not affect a site in the Pahoa district.

An average thickness of 18.3 feet (5.6 m) can be calculated from the total volumes and areas of the five historic flows. This average is strongly affected by the exceptional thickness of the lava of 1960, which averaged 36.7 feet (11.2 m) because it accumulated in a depression on a very gentle slope. Flows on steeper slopes average about 12 feet (3.6 m) in thickness. Thickness also varies from place to place according to the local topography and rate of discharge. It is greatest where ponding occurs or narrow constrictions limit the flow and cause the lava to form thicker flows in an upstream direction.

It must also be stressed that the thicknesses of lavas are greater during active flow than they are after forward motion is arrested. This is especially apparent in fluid pahoehoe flows on moderate to steep slopes. At a given point in the lava stream, the thickness normally diminishes as the flow spreads downslope and drains lava from higher elevations. This effect is dramatically illustrated at Lava Forest Park, where tree molds stand two or three meters above the final surface. Therefore, it should be anticipated that, for pahoehoe flows, transient thicknesses may be as much as twice the observed final thicknesses of about 12 feet (3.6 m). The exact magnitude of this difference will depend on the viscosity, rate of discharge, gradient and course of the flow, and the local topographic variations. Because of these factors, thickness of a flow cannot be predicted, but thicknesses of 30 feet or more can be attained at certain points during the course of an eruption.

Rates of advance of flow fronts are governed by the slope angle, viscosity of the lava, and rate of discharge at the vent. During historic eruptions, measured rates have ranged from as much as a few hundred feet per hour to as little as a few feet per day. In the East Puna District, rates of advance are much slower than on higher segments of the rift where slope angles are greater. During a prolonged eruption, it is common for the flow front to advance in one area for a day or two, and then shift to another front before returning to the earlier front, so that with time, advance may be highly sporadic for any particular portion of the front.

4.3.4 Alleviating Volcanic Hazards

<u>4.3.4.1 Monitoring:</u> Volcanic eruptions in the LERZ have an abundance of premonitory phenomena that make it possible to foresee a coming eruption for several days or weeks. This allows adequate warning time to evacuate personnel and portable equipment. For this reason, hazards to persons working in the area, and hazards to portable equipment, are not as serious as hazards to fixed facilities.

The methods currently in use to monitor the LERZ and to forecast eruptions and their accompanying deformation employ seismographic records, tiltmeter readings, resurvey of trilateration networks, and geodimeter measurements. These methods are applied by the staff of the Hawaiian Volcano Observatory (HVO) operated by the U.S. Geological Survey. Members of the staff of the Hawaiian Institute of Geophysics have established a geodimeter network around the existing geothermal well (HGP-A) to monitor ground deformation resulting from extraction of geothermal

fluids. The seismographs provide continuous records, whereas the tiltmeters and geodetic techniques provide data at infrequent intervals. Currently the HVO staff re-levels the trilateration stations twice a year and measure tilt two or three times a year. Geodimeter measurements have not been made since 1978.

Seismological techniques are the most effective methods of forecasting impending events in the ERZ, and the HVO network appears adequate for monitoring seismic activity. In the event that large-scale geothermal development takes place in East Puna, consultation with the staff of HVO should be accomplished to determine whether additional seismographs would be needed to improve the capacity to monitor shallow, very low magnitude activity. There is probably no advantage to be gained from installation of additional tiltmeters, but it is desirable to maintain the present HIG geodimeter network, to allow ground deformation in the area of any future geothermal plant to be monitored, especially during nearby extrusive or intrusive events. This would serve to locate zones of potential fissuring and faulting during any activity that may occur in the future. Such data are important for design considerations before construction of permanent installations in the area of the geothermal development.

Apart from these preliminary data bearing on the design and siting criteria of new facilities, the basic objectives of monitoring seismic activity and ground deformation should be to provide warnings of possible eruptions or ground rupture to allow time for precautionary measures. Frequent remeasurement of a geodometer network, particularly before and after swarms of earthquakes in the LERZ, would provide more detailed information on the location of tectonically active zones that are likely to be affected by an eruptive event.

<u>4.3.4.2 Site Selection</u>: By judicious site selection and design, it is also possible to greatly reduce the probability of inordinate losses to permanent facilities by taking advantage of topographic relief. For future development in the Puu Honaula area the question of selection of one or more sites for generating plants will become increasingly important. Figure 4.10 shows areas within a radius of one kilometer of the HPG-A well and proposed drilling sites to the north and east which are prime targets for future plant site locations.

Current knowledge of eruptive processes provides no basis for long term predictions of the locations where future eruptions are likely within the ERZ, but as historic eruptions have been more common on the south side, an outbreak in that part of the zone is more probable.

Topography is the controlling factor determining the risk of lava incursion on a selected site. The area at greatest risk within 1 km at HGP-A well or proposed wells is the shallow depression bounded by the Kaniahiku ridge to the north, and the Puu Kaliu - Kahuwai Kiapu - Puu Honaula - Puu Kii line to the south (fig. 4.11). Lavas originating within this area and in the ERZ up to 4 km west of the area are likely to be channeled down into this depression as indicated by the heavy arrows in fig. 4.11. Ponding of lavas on the nearly level ground immediately northwest and southwest of Kiapu could result in overflow between Kiapu and the HGP-A site. This would result in the flow of lava down the southeast flank of the rift (heavy arrows in fig. 4.11). Lavas originating in the northern part of the area would flow to the northeast, and those erupted south of the Puu Honaula ridge would flow to the southeast.

Areas of reduced risk from lava flows are primarily hills and, secondarily ridges, that rise at least 40 feet above the pathways of flows and are not within areas subject to ponding. Such areas are shown on fig. 4.11 and are graded from P1 (having the lowest risk) to P6 (intermediate risk). Unshaded areas have the highest risk.

The southeast flank of Puulena Crater (P6) is protected by the north rim of Kuhawai Crater, and by the Puulena Crater itself, which, if it were filled by lava, would overflow its eastern end. This site is located close to a buried fault (fig. 4.9) and is too distant from the geothermal area. This site has the advantage of being close to the edge of the southern (but most active) side of the LERZ.

Kiapu Hill (P5) rises 60 feet above the surrounding plain but lies in the path of any lava erupted in the southern third of the rift zone. The NE-trending Kaniahiku ridge (P4) rises 20 to 60 feet above the surrounding area, and, according to Holcomb (1981), is formed by 17th century lavas cut by normal faults. No evidence of faulting was found in a photogeological interpretation of this area. The ridge provides well protected sites close to a paved highway, but may not be feasible because of distance from the HGP.

We have selected five sites strictly on the basis of risk from lava flows, with little regard for distance from the geothermal area. The safest of these (A in fig. 4.10) is in the saddle between Puu Honaula and the next cone to the northeast, at an elevation of 660 feet. The site is 90 feet above the low ground to the north.

The second site (B) is 350 m south-southeast of the summit of Puu Honaula at an elevation of 650 feet, 45 feet above the low ground 800 m to the west. The site is on a shallow ridge 850 m from HGP-A.

The third site (C) is on the Kaniahiku ridge 310 m southwest of the Pahoa highway at an elevation of 700 feet. This site is 60 feet above the low ground on each side of the ridge. The ridge is shown as a zone of short normal faults by Holcomb (1981), but photogeologic methods do not confirm the existence of these faults. Should this site be seriously considered, the question of the existence of these faults should be investigated by trenching. The site is 2000 m from HGP-A.

A fourth site (D) is on Kiapu, an old spatter and cinder cone, at an elevation of 700 feet, 50 feet above the western base of the hill. A disadvantage of this site is that it lies in the path of flows that could descend from a considerable area higher in the ERZ, but it is unlikely that these flows would be thicker than 50 feet. Site D is 530 m southwest of HGP-A.

The last site (E) is on a low, horseshoe shaped ridge of old spatter immediately northwest of Puu Pilau, at an elevation of 630 feet. It is somewhat restricted in size (200 by 50 m) and is only about 30 feet above the level of ground to the west. The northwest side of the low cone on which the site is situated is partly protected by a ridge of boulders dozed from cultivated

fields. The ridge served as a diversion barrier during the 1955 eruption and could be enlarged in height and width to provide added protection. Site E is 550 m from HGP-A.

While site A is undoubtedly the safest of the ones we have listed, based on the listed criteria, there is little to choose between sites B and C, which are slightly less secure, and between sites D and E, which we consider more exposed.

4.3.4.3 Diversion Barriers: Efforts to influence the directions and rates of advance of lava flows have, for the most part, been unsuccessful in Hawaii, but elsewhere, particularly at Mt. Etna in Sicily, they have been more effective. During the 1960 eruption near Kapoho, large-scale efforts were made to construct barriers along the south side of the graben, and although in some instances they delayed the advance for a few hours or at most a day or two, all were eventually overrun.

Barriers fail either by being bodily pushed ahead of the flow or by penetration of their base by fluid injections. The high density and mass of thick basaltic flows, even when moving slowly, exerts such a large force against any obstacle in its path that it can simply force it ahead or aside. The bulk density of basaltic lava (about 2.7 grams per cubic centimeter) is considerably greater than that of the fragmented, scoriaceous rock and cinders used in hastily constructed barriers. To be effective, barriers of loose material would have to be wide and much higher than the anticipated level of encroaching lava flows.

If a flow can be diverted into an open channel, especially one having a smooth floor and steep gradient, the barrier does not receive the full force of the flow and may survive. This

principle accounts for the success of barriers at Mt. Etna. Owing to the steeper and more irregular topography on that volcano, it is easier to divert flows from one channel to another. In addition, the lavas of Etna, being more viscous, are less likely to penetrate the base of the barrier.

A well anchored barrier constructed of dense material, such as concrete, may be capable of protecting a narrow front at a given locality if the force of the flow can be diverted into a channel of lower resistance. In general, pahoehoe flows have a lower viscosity and can flow around obstacles, such as trees or small cones, more readily than aa lavas, but when ponded they also have a greater capacity for flowing beneath a light structure resting on the surface. The important principle governing the success of barriers is to deflect the flow into a more favorable course rather than attempting to oppose it directly.

4.3.4.4. Design Considerations: Of the various structures associated with a geothermal project – steam wells, pipelines, power plant, and associated facilities – wells and pipelines must be sited in accordance with relatively inflexible geological requirements, whereas more freedom is possible in placing the remaining facilities. It has been shown that the risk of lava flows is mainly a function of topography, and the risk of surface displacement is mainly a function of the dimensions and orientation of a structure across the trend of the ERZ.

The safety of pipelines, power lines, and large buildings can be enhanced by observing certain general guidelines.

1. Long linear structures within the ERZ may be subjected to horizontal ground displacements of at least 2 meters in a

direction N 30 W (normal to the rift axis) and up to 4 meters in a vertical direction. Pipelines, powerlines, and their supports can be constructed with sufficient vertical and horizontal compliance to withstand this magnitude of ground deformation.

2. Under favorable conditions diversion barriers may be capable of diverting lavas but are of little use as dams to oppose a flow directly. Short barriers on the north side of site B, the southwest side of site C, the west side of site D, and the northwest and northeast sides of site E would enhance the security of these sites.

3. To minimize the probability of failure by surface deformation, fixed facilities entailing relatively high costs, such as generating and auxiliary plants, should have a minimum dimension transverse to the trend of the LERZ (N 60 E). These facilities should, where possible, be built to withstand ground deformation of the magnitude indicated above (see 1).

4. It would be desirable to design roofs of buildings capable of shedding scoriaceous pyroclastic debris or supporting the load of a 1-meter layer of ash or cinders having a bulk density of 2 grams per cubic centimeter. 5.0 SEISMIC RISK ASSESSMENT OF THE PUNA DISTRICT, HAWAII

5.1 Introduction

5.1.1 Purpose of Study

This part of our study evaluates the earthquake hazard and general risk to future facilities for the Puna Geothermal Prospect (PGP) in the Puna District of Hawaii. Section 5.0 only considers ruptures of tectonic origin. Volcanic related fissures and faults are considered in Section 4.0.

5.1.2 Approach

Current state-of-the-art methods call for the detection, delineation, and definition of the character of seismogenic faults of a region to prepare an assessment of the location and faulting potential of active tectonic faults, and to evaluate the potential strong ground motion that could affect engineering structures at the site (Slemmons, 1977; and Glass and Slemmons, 1978). The usual methods of assessment include consideration of:

- A. Seismicity and source mechanisms of regional earthquakes.
- B. Geomorphic expression for fault rate of activity and fault slip type.
- C. Geologic assessment of stratigraphic and soil-stratigraphic evidence for fault activity.
- D. Assignment of maximum or maximum credible, and maximum probable earthquakes for the province and each seismogenic fault effecting the study area, with an estimation of future earthquake frequency and expected attenuated ground motion at the engineering site.

Review of aerial photographs, consideration of the youthful

and active historic and geologic record and the nature of the historic earthquake activity, support the classification of faults and fissures into two, very different, categories:

- Volcanic faults, fissures, and rifts, including the fractures of the East Rift Zone and the Southwest Rift Zone, along nearly straight volcanic alignments.
- Tectonic faults of the Hilina and Kealaekua-Kaholo fault type, with dipping fault planes and common arcuate traces.

These two types provide the source of most shallow-focus earthquakes, the former associated with magmatic movements, as discussed in Sections 3 and 4 of this report, and the latter with higher magnitude tectonic earthquakes.

5.1.3. Terminology

The following terms are defined for use in this report:

The <u>maximum</u> or <u>maximum</u> <u>credible</u> <u>earthquake</u> is defined as the severest earthquake that is believed to be possible at the site, or to be generated by a fault, as determined by geological and/or seismological evidence. The maximum earthquake for a site has a ground motion that is based on one or more assumed future earthquake sources or source areas, with the motion attenuated to the site as a function of the distance from the source to the site.

The <u>maximum probable earthquake</u> is the strongest earthquake that is likely to provide motion at a given site or area, for a specified period of time, generally assumed to be the life expectancy of an engineered structure. This is approximately 40 years for the purpose of this study.

5.2 Regional Seismicity

The regional seismicity of the island of Hawaii is high compared with many tectonically active regions of the world, and appears to be related mainly, or solely, to volcanic activity and processes. The seismic activity is generally very low along the old Emperor segment north of the island chain and along the northern, old part of the Hawaiian chain (fig. 3.1). Most of the activity is concentrated at the southern, currently active, end of this zone of "hot spot" volcanoes. No known major fault zones affect the chain in terms of major active tectonic plate boundaries.

The record of seismicity, particularly for low magnitude earthquakes is not well documented for the entire historic record and there is no unified catalog of earthquakes available. The main sources of information for earthquake hypocenters are:

- 1. The NOAA earthquake hypocenter data file (app. A),
- The Gutenberg and Richter (1954) catalog of pre-1951 data for moderate to high magnitude earthquakes, and

3. The HVO summary reports of regional seismicity.

These data bases all have significant deficiencies in quality and sensitivity of earthquake detection and location that change with time. The post-1960 NOAA file has many duplicate listings for the 100 mile (160 km) radius of HGP (see app. A). The epicentral map prepared from the data of Appendix A (fig. 5.1 and pls. 1 and 2) show a broad pattern of earthquake epicenters for earthquakes of more than about 25 km hypocentral depth, with a denser cluster near the deep central conduits of Kilauea and Mauna Loa; the



Figure 5.1 Earthquakes of greater than magnitude 3 within a 100 mile (160 km) radius of the Puna Geothermal Project. Many of these events are plotted twice because of duplication in the NOAA file - see Explanation for Appendicies A, B, and C.

epicentral pattern for earthquakes of less than 25 km focal depth show concentrated activity along and near the ERZ, SRZ, the rift zones of Mauna Loa, and along the Hilina fault zone and its offshore southeastern extension.

Two patterns are apparent on the epicentral map of deeper focus earthquakes (pl. 1):

- A clustering along the deep conduits of Mauna Loa and Kilauea, where pulses of new magma from the upper mantle are accompanied by earthquake activity, and
- 2. A broad pattern around the edges of the island of Hawaii, where crustal loading from the recent loading by rapid volcanic growth is believed to cause upper mantle tectonic adjustments, although mechanisms of these deep earthquakes is not well understood (Unger and Ward, 1979).

The maximum magnitude for earthquakes of more than about 25 km depth is about 7 for the west flank of the volcano (August 21, 1951) and 6.2 for the east flank of the volcano (April 26, 1973). These deeper focus earthquakes have caused less damage than shallower focus earthquakes of similar magnitude (Nielsen and others, 1977). The likelihood of future activity of this type near the site is considered by us to be low, with only two earthquakes of above 6 magnitude within the 31,400 sq mi area centered on the site for a 30 year period. Adjustments of this type should be more common to the north of the site, since the volcanic heights of Mauna Loa and Mauna Kea are greater and the volume of eruptive material is greater than in the Kilauea-East Rift Zone sector of the island.

Earthquakes of less than about 25 km focal depth are localized along the central conduits, but also have narrow and concentrated clustering along the active volcanic rifts. In addition a broad zone of distributed, very shallow focus earthquakes are described for zones of magmatic movement as has been summarized by Koyanagi and other (1981). The relationship of the ERZ to the Hilina fault zone is described in Section 2.0 and Section 5.3.

5.3 Seismicity of Faults near the Puna Geothermal Prospect

5.3.1 Hilina Fault Zone

The historic record shows a high rate of activity along the Hilina fault zone, with a large earthquake, perhaps of 7.5 to 8 magnitude in 1868 and a Ms = 7.2 earthquake in 1975. This zone shows a long history of small earthquakes as suggested by the earthquake catalog (app. A, B and C and pls. 1 and 2), and the activity shown in pre-1975 epicentral plots. The activity from 1963 to 1969 is shown in Figure 5.2 with volcanic related epicenters along the ERZ and epicenters on and near the Hilina fault zone. The epicenter map of all earthquakes for 1976 and 1977 (fig. 5.3) shows the earthquake activity in Hawaii, including the epicentral and aftershock area for the 1975 Kalapana earthquake, with a dense distribution of earthquakes to the south of the ERZ and the offshore zone of submarine uplift and tsunami generation (fig. 3.11). The focal mechanisms of earthquakes of this zone are compatible with a southeastward movement (figs. 3.11 and 3.12) of a block bounded on the northwest by the surface trace of the Hilina fault and extending into the offshore region (Fitch and Kinoshita, 1969; Furumoto and Kovach, 1979; Crosson and Endo,



Figure 5.2. Compilation of earthquake epicenters from short seismic swarm: that are associated with magmatic processes from 1963 to 1969. Earthquakes selected are of magnitude 2.0 and greater, and depths less than 15 km. The epicenters were plotted according to two time categories in which they occurred. Earthquakes during the initial stages of activity were concentrated near the outbreak area along the Koae faults and the ERZ. Earthquakes during the middle and late stages scattered far to the south toward the Hilina fault zone (Koyanagi and others, 1972). Note the close spatial association of the earthquakes associated with the eruption (solid dots) with the ERZ.



Figure 5.3. Epicenter plots presented in Hawaiian Volcano Observatory Summaries 76 and 77 for 1976 (A) and 1977 (B) showing the concentration of earthquakes in the south flank of Kilauea (from Koyanagi and others, 1981).

1981); Crosson and Endo (1981) show (fig. 3.12) vectors for displacements in this block. Wyss and others (1981) show that precursors to the Kalapana earthquake may have included aseismic stress drop by fault creep in the area indicated in fig. 5.4. Wyss (in press) also indicates that this event may represent three earthquakes of mb = 6.5 in close temporary association, to give the higher Ms value of 7.2.

The average seismic moment for the Kalapana earthquake (Ms = 7.2) was 1.2×10^{27} dyn cm, with an inferred stress drop of 12 bars (Furumoto and Kovach, 1979). These calculations, the geologic and tsunami relations for this earthquake, and the aftershock data suggest rupture of a large percentage of the total fault surface. The size of the faulted surface for the 1868 earthquake is unknown, but it does not appear likely that it could have been much greater than for the 1975 earthquake. The possibly larger magnitude (Ms greater than about 7.5) may be from a larger average displacement on a similar fault surface area, or more multiple events in a very short time period.

5.3.2 Koae Fault Zone

The Koae fault zone has frequent earthquake activity and appears to be related to combined tectonic and volcanic activity. The maximum volcanic earthquake is about 5.5 magnitude, which is approximately the maximum noted for volcanic related activity on any of the rift zones. Earthquake epicenters from this fault zone are more than 45 km from the site. When ground motion is attenuated, they are not likely to result in damaging motion at the HGP site.



Figure 5.4. Map of the rupture area of the Kalapana earthquake of 1975 in relation to the distribution of crustal anomalies. The one month aftershock zone is shown. The rupture area was estimated by Ando (1979) and is indicated by the rectangle. Squares indicate triangulation benchmarks, small dots show foreshock locations, the medium size dot marks the location of the M = 5.0 foreshock and the large dot indicates the epicenter of the magnitude 7.2 main shock (Wyss and others, 1981). 5.3.3 Honuapo-Kaoiki Fault Zone.

This zone has no known evidence for youthful or current activity. It may represent an older, ancestral Hilina fault zone type of feature. The zone is near some epicenters (pl. 1), but its current activity is uncertain. The 35 km distance of this fault zone from the PGP eliminates the need to consider it as an important source of damaging ground motion at PGP.

5.3.4 Kealakekua-Kaholo Fault Zone

This zone is near the source of the 1950 earthquake of Ms = 6.25. The zone is a system of arcuate to linear patterns of fractures similar to the Hilina fault zone. Earthquakes of more than Ms = 6.25 are possible, perhaps with a maximum of about 7.0. If the poorly known character of this structure is assumed to be similar to the Hilina fault zone, the 110 km distance from PGP eliminates the need to consider this fault zone as an important source of damaging ground motion at PGP.

5.4 East Rift Zone

The general geological and geophysical setting of the ERZ is discussed in Sections 3 and 4. The recent high quality data on seismicity and focal depths show frequent, low magnitude earthquakes of volcanic origin for this zone (figs. 3.10 and 5.3). Koyanagi (pers. comm., 1981) believes that the lack of deeper foci events on the ERZ is due to doming effects from intrusions on the ERZ which cause the high number of events and shallow area of activity. These data show a high level of volcanic activity related to uplift from magmatic injection, with modification from aftershocks of the 1975 earthquake. The depth profile of these aftershocks is suggestive of a possible southwest dip of a fault plane or rift zone (fig. 4.4).

The maximum magnitude for volcanic-related activity on the ERZ is about 5, based on the maximum historic earthquake. The historic record suggests that earthquakes of about Ms = 5 to 5.5 could occur at PGP. Planning for seismic design at this site should, for conservatism, assume that earthquakes of up to this magnitude range could occur during a 40 year time interval. This upper bound magnitude value may be limited by the high frequency of volcanic activity along the ERZ limiting the amount of stress and strain accumulation on this zone, and the frequent relief of such accumulations.

5.5 Earthquake Magnitude and Ground Motion

5.5.1 East Rift Zone

The strongest historic earthquakes on the ERZ are of volcanic origin, and for the NOAA hypocenter data file (app. A) of the last 20 years, indicate a maximum earthquake of about Ms = 5. The high frequency of volcanic activity suggests that relief of stress and strain on faults and dikes may occur every few years. Since the magnitude 5 earthquakes that have been recently observed may not represent the long-term maximum, we recommend that a higher maximum earthquake magnitude of 5.5 be assumed for the PGP, with an epicentral distance of from 0 to 10 km. High acceleration, displacement and velocity may occur at the site, but with only a few high frequency cycles of short duration. Motion of this type is not likely to cause structural damage to engineered structures. The following are the estimated ground motion parameters, defined by data on figs. 5.4 to 5.7.

- A. Mean Peak Horizontal Acceleration: The mean peak horizontal acceleration is 0.2 to 1 g (fig. 5.5).
- B. Mean Peak Horizontal Velocity: The mean peak horizontal velocity is 10 to 100 cm/sec (fig. 5.6).
- C. Mean Peak Horizontal Displacement: The mean peak horizontal displacement is 5 to 15 cm (fig. 5.7).
- D. Duration: The duration of ground motion greater than 0.05 g is 5 to 12 seconds (fig. 5.8).
- 5.5.2 Hilina Fault Zone

The relief of stress and strain by the 1972 earthquake, which ruptured most of the known length of the Hilina fault zone, is likely to mark the start of a new seismic cycle of accumulating stress and strain. Residual strain on possible unruptured parts of this fault zone, or aftershocks appear to have a potential for generating earthquakes of about Ms = 6.5. The gradual increase in strain could lead to another 7.2 magnitude earthquake in approximately 100 years. We estimate the earthquake potential to gradually increase during the next 100 years from Ms = 6.5 to Ms = 7.2 and assume for planning purposes that the maximum credible earthquake for the next 40 year period is about Ms = 6.75 for the PGP area.

The distance from PGP to the epicenter of a potential earthquake on the Hilina fault zone is difficult to determine from the present geologic and seismologic data base. Future specific design of vital engineered structures may need a special assessment of this problem. Alternative methods of measuring the length include the following:



Figure 5.5.

Peak horizontal acceleration recorded at base of small structures versus distance to the slipped fault for three magnitude ranges. Center line, mean regression line. Outer pair of lines represent 95 percent prediction interval; inner pair, 70 percent prediction interval. Length of lines represent distance interval considered in regression analysis. Uncertainty in distance is inversely related to symbol size. The lower right figure shows a comparison of the 70 percent prediction intervals for the three magnitude ranges (from Boore and others, 1981).

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C





Peak horizontal velocity. See Figure 5. for explanation of symbols and curves. Dashed curves the lower right figure for Magnitude 7.1 to 7.2 emphasize uncertainty in slope (from Boore and others, 1981).



Figure 5.7. Peak horizontal displacement. See Figure 5. for explanation of symbols and curves (from Boore and others (1981).



Figure 5.8. Near field duration of ground motion with acceleration greater than or equal to 0.05 g from historic earthquakes (Chang and Krinitzsky, 1977).

- 0
- From PGP to the nearest point on the surface trace of the Hilina fault, about 20 km.
- From PGP to the nearest potential hypocenter to the southwest on the bottom of the tectonically active block, about 25 to 30 km.
- From PGP to the center of energy release, about 40 to 50 km.

For conservative planning purposes, the nearest hypocenter for a large magnitude tectonic earthquake on this fault zone can be assumed at 25 km from PGP.

The estimated ground motion at PGP, is assumed to be an earthquake of about 6.75 magnitude for the next 40 year time period, with a source earthquake distance of 25 km. This provides the following estimate of ground motion:

A. <u>Mean Peak Horizontal Acceleration</u>: The estimated mean peak horizontal acceleration from figure 5.4 is about 0.15 for M = 6.0-6.4 and 0.4 for M = 7.1-7.6. The peak acceleration from fig. 5.9 is about 0.16 for an earthquake of about 6.6 magnitude and 0.28 for 7.6 magnitude. These values are consistent with the recorded 0.22 g for the Ms = 7.2 earthquake in 1975, at Hilo with an epicentral distance of 43 km (Rojahn and Morrill, 1977). These data lead to an estimate of a mean peak horizontal acceleration of 0.25 g for the next 40 year period at the site.

B. <u>Mean Peak Horizontal Velocity</u>: The estimated mean peak horizontal velocity from fig. 5.5 is about 15 cm/sec for M =6.4 and 35 cm/sec for an earthquake of M = 7.1-7.2. These data lead to an estimate of mean peak horizontal velocity of 25 cm/sec for the next 40 year period at the site.



C. <u>Mean Peak Horizontal Displacement</u>: The estimated mean peak horizontal displacement from fig. 5.6 is about 5 cm for M =6.4 and 15 cm for M = 7.1-7.2. The relative displacement was 3.4 cm at Hilo for the Ms = 7.2 earthquake in 1975, at an epicentral distance of 43 km (Rojahn and Morrill, 1977). These data lead to our estimate of mean peak horizontal displacement of 10 cm for the next 40 year period at the site.

5.6 Seismic Hazards at the Puna Geothermal Prospect

The main earthquake hazards are, in a general decreasing order of risk:

- 1. Ground motion
- 2. Landslides, slumps, and other secondary ground failures
- 3. Liquefaction
- 4. Surface faulting
- 5. Tsunamis and seiches

The principal hazard for the PGP is from strong ground motion from tectonic and volcanic related earthquakes. Tectonic earthquakes and their probable ground motions at the site are discussed in Section 5.4. Earthquakes caused by magmatic movements, although of high frequency and closer sources, have lower magnitudes and are expected to result in only minor damage and other effects (see Section 4.0).

Landslides, slumps and other gravity failures induced by strong earthquake motion are likely to affect the siting area. Liquefaction and tsunami effects are not important in the siting area, which is well above sea level and is generally devoid of materials that are susceptible to liquefaction. Surface faulting in the siting area is considered in Section 4.0.

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SOURCE CODES

CGS	-	Coast and Geodetic Survey
ERL	-	Environmental Research Laboratories
G-R	-	Gutenberg and Richter, 1954
GS	-	U.S. Geological Survey, Denver, CO, U.S.A.
HVO	-	Hawaiian Volcano Observatory, Hawaii National Park, HI, U.S.A.
ISS	-	International Seismological Summary, Kew, England, U.K.
NOS	-	National Ocean Survey
USE	-	United States Earthquakes

TIME

Date and Origin time in Universal (Greenwich) Time. (Note: Many earthquakes from HVO given in Hawaiian Standard Time in Appendix A, and duplicated with data from other sources in Greenwich Time. Those events in Appendix A preceeded by a (•) are duplicated because of this use of two time zones in the NOAA listing. Those events in Appendix A preceeded by a (•) are duplicated in Appendix B. These two types of duplications are omitted from the data in use in this report).

AUTHORITY (follows origin time)

H - Parameters of hypocenter supplied by the USGS Hawaiian Volcano Observatory

MAGNITUDES

For source, see source codes above. Under surface wave, SH = Horizontal components used.

INTENSITY

Maximum in Modified Mercalli (MM) scale or converted to MM scale.

PHENOMENA

D	Diastrophism	-F, surface faulting; -U, uplift/subsidence;
		-D, faulting and uplift/subsidence
Т	Tsunami	-t, tsunami generated; -Q, possible tsunami
S	Seiche	-S, seiche; -Q, possible seiche
V	Volcanism	-V, earthquake associated with volcanism
N	Non-tectonic	-C, coal bump or rockburst in coal mine; -E, explosion, accidental, controlled, or suspected explosion; -I, collapse; -L, lights or other such visual phenomena seen; -M, meteoritic source; -R, rockburst
0	Waves Generated	-A, acoustic wave; -G, gravity wave, -B, both A and G; -T, T-wave

REGION NUMBER (RN)

Geographic region number as described in Flinn, Engdahl, and Hill, 1974

CULTURAL EFFECTS (CE)

C - casualties

- D damage
- F felt

QUALITY/NUMBER OF STATIONS (Q/S)

Quality indicators are usually on an A, B, C, or D basis (A-very accurate; B-good; C-fair; D-poor). When used in combination for deep shocks, these represent the accuracy of (in order) epicenter, origin time, and depth.

MARSDEN/DEGREE SQUARE (MAR DG)

Numbering system dividing the world into 10° squares (MAR) and 1° subsquares (DG).

DISTANCE (DIST)

The distance in kilometers between the earthquake location and the designated point for radius searches.

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SARTHQUAKE DATA FILE

DR. D.B. SECHMONS UNIVERSITY OF NEVADA

160-KM RADTUS OF 19.467N.. 155-823W.

81/07/17. 14.55.45.

A-3

FRENTED SUTFUT WILL BE DISF CSED TO THE EDIS SITE LINE FRINTER

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3-3	1 9 41	5) :	25	: 7	++	31 .:	19.5CCN	155.5C(W	× 8			E.CCFAS			VII		613	0		(52	95	41.
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-1417/17.

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260	1962	::	. :	5 :	9 35	21.31	19.217M	155.2178	:05				3. HINL	FVD			613 1			152 9	2	13.
JSE.	1762	3	5)	9 .	7 43	16.51	19.4 1	155.4176	005				3.5 CML	1 00			613 1			052 9	2	49.
155	1 :: 64]:	5 i		. 34	55.34	1 19.4171	155.26EW	03.1.				. 4. 3 3HL	HVO			613 F			1.52 9	2	63.
252	. : 62	5	2	+ 1	3 34	55.75	19.4 N	1 55.4:75	105				3.7.ML	FA0			£13 F			652 9	5	49.
155	1 - 62	0	1 :	4 .	4 4.	4: . 31	19.25 N	155.6314	CC 5				3.5(HL	FVO			613 1			(52 9	5	36.

31/ 37/17.

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SJIICE	YE AR	Mü	DA	+ 6	14	SEC	LAT	LONG	DEPTH (KM)	PODY	MAGNI SURF	ITUDES- OTHER	LOCAL	•	INT	PHENOM	RN	CE	0/S	AAM	DG	DIST (KM)
" I YO!	CATES	A	FOS	SIL	LE	DUFLIC	ATE			,												
USE	1962	27	14	17	37	53.14	19.747N	155.637W	C1 0				.4.CCML	F VO			613	F		C52	95	40.
USE	1962	27	24	.9	52	41.1H	19.442N	155.987W	005				.4. 50ML	F VO			613	F		052	55	11.
JSC	1162	17	31	12	40	41.24	19.425V	155.0008	005				3.50ML	нуо			613	F		052	95	93.
USE	1 162	CT	31	15	24	15.61	19.333N	155.0824	035				3.70ML	HVO			613	F		052	95	P5.
USE	1962	CE	11	19	30	16.5H	19.: ELN	155.533W	100				CCKL	FVO			613	F		C52	95	49.
USE	1 -67	34	13	11	50	41.94	19.303N	155.195W	900				.4.66ML	F V0			613	F		C52	95	74.
USE	1 352	39	16	11	5è	HC . 52	19.35N	155 . 142W	900				4. 10ML	FV0			613	F		052	95	91.
USE	1 162	:9	11		11	15.11	19.1331	155.115W	003				3.6CML	HVO			613	F		252	95	83.
USE	1962	19	11	17	22	49.11	19.477N	155.233W	603				3.77ML	HVO			613	F		052	95	68.
USE	1962	67	11	:1	25	27.51	19.4774	155.233W	664				3.6CML	F VO			613	F		(52	95	61.
USE	1462	53	23	50	22	37.31	19. JF3N	155.0769	212				3.7CML	F VO			613	F		652	95	55.
JSE	1 :02	: 7	25	23	22	51.44	19.252N	155.503%	336				3.56ML	HVO			613	F		052	95	46.
USE	1962	1.	19	10	43	29.50	19.668N	156.1:39	012				3. 6 0ML	FV0			613	F		C52	96	32.
USE	1:42	1:	3:	23	3:	5: . ()	19.147N	155.550%	:(3				3.7:ML	HA0			613	F		:52	95	46.
364	1 7 6 2	11	2:	:1	3-	55.2F	26.2:14	155.19:4	C12				·3.7[ML	F VO			é13	F		TFF	(5	55.
JSE	: -:	11	12	.5	10	2:.7+	19.5534	155.7634	205				4.1CML	F VO			<i>É</i> 13	F		252	95	15.
JSE	: .42	1 2	14	· e	21	31.74	:9.2224	155.3534	1) *				3.5"ML	HV0			613	F		952	95	£2.
532	61	12	. 4	7	50	1: . 71	19.4".N	155.42-50	13"				3.7.ML	FV0			613	F		052	95	63.
132	1462	:2	21	::	14	11.11	14.3"EN	155.013%	1 3 3				• 4 • 1 CML	FVG			613	F		052	95	.86.
155	: 122	12	3:	13	47	14 !	· · · · · ·	155. 5069	023			*	•4.(:ML	F V0			£13	F		152	95	41.
JSC	1.43	11	14	: 5	3.4	44. 1+	10.1.11	1.22.31.21	11.0				. 4. 30ML	F VO			613	F		012	95	£
132	- "m3	21	30	.1	41	66.24	19.4 1N	155.2554	63.1.				• 4.20ML	PVO			613	F		125	95	63.
155	1943	. 3	13		57	25.31	10.4.3N	165.500W	115				3.50ML	FVO			613	•		152	35	41.
r ¥ - +	1943	: 5	22	2:	r .	40 .5t	1341N	155.131%	c12				3.8(ML	FVO			513	1		152	95	10.
725 .	1-43	33	23	.6	31	51.81	19.753N	155.5634	212				-4.50ML	FVO			612	r		226	95	147
- 4 P	1 24.5	11	25	. 11	1.	35	20.75 N	155.7334	135				3. 91 HL	HVU			513			150		141.
- * ,	: 1413	- 1	1.		: 5	57. 31	2 · . 174	155.7114	336				3.7.4L	FVO			613	-		100		1.5
155	: ++5	1	1 3	12	21	3	14.7451	155. 164	cer				J. HIML	FVO			613	F		150	95	45.
152	: 5	.'-	.)7	. !	25	.11.	19.14	155.5514	ce :				- 4.21ML	FVU			613	6		652	95	40.
JSE	1 1055	3:	- 4	- 21	7	=1.7-	19.417M	155.2744	153				3. 10PL	FVO			613	F		052	95	79.
JSE	1.45	-	11	12	43	57.54	17.2258	155.16.4	103				J. FOUL	HV0			613	-		052	96	4.5
132	1.20	- 1	11	- 14	11	14.75	1.3601	155.7250	303				J. SUML	FVU			413	-	112	152	Q.F.	47.
Cus	1 - 61	- 1	24	: 1	4 "	18.46	19.1.1	155.5.1.1	110	•••••1MB			7 6 ***	L VO			618	5	110	25.2	95	51.
05.	47.5		13		24	3	14.4.34	110.4.19					S C INL	E VO			613	F		65.2	96	16-
- 4 3	: 16)		15			11.00	19.4-51	100. 1400					3. 6. MI	EVO			613	F		252	95	
JSL		:			11	27.35		155.54CW	365				3. 3.1.1				613	F	C11	052	65	= 0.
5		: ;	21	1.	17	24.1	1 N	156	COS		1.0		3.5(3)	F VO			613	F		(52	95	51.
132		• ;		- 1	27	24 45	17 4 1	155 4114	1.16				3. 5 MI	L VG			613	F		652	55	
10.5	1 14.3			- 6	2.	11 74	M	155.1764					3.7141	E VO			613	F		25.2	95	62.
127			1.5			47.16	13.1744	155. 930	1.7.0				3.6(11)	FV0			613	F		052	95	51.
132	1 . 6 3		- 1		34	18.5	17.4.1 1	155.5764	115	·5.3048							613	F	\$19	052	95	41.
122		:	21		24	47. 1	19.4(.1)	165.4319	Cr5				3.1(11	F VO			613	F		152	95	51.
	1 2	î	24		25	26.56	17.4155	155.4514	205				3. SOML	t vo			611	F		C52	95	51.
135	1 . 6'	;	50			54. 14	17.4.1	155.4112	025				3.8.ML	HVD			613	F		052	95	51.
45.	1-44	i			:3	54.71	14.4.EN	155.4016	11				3.5CML	HV0			613	F		352	95	51.
PV i	1:23	: 1	14		7 7 1	25.41	20.1654	155.45.08	C1 2				3.75ML	FVO			613	F		1 3 3 3	(5	1 %.
USE	17:03	11	1 -	. : :	5 51	26.51	14.4:14	155.215%	.33)				3. EOML	FV0			613	F		052	95	63.
USE	1	11	3	1 .4	: : :	50	14.335N	155.1304	JCP				3.6.ML	HVO			613	F		052	95	FC.
JSE	: 204	11		1 1	:5	25.3+	17.3' 14	155.225W	31.6				3.70ML	FV0			ь13	F	600	652	95	71.
												-										

11/:7/1-.

FAGE

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SAJACE YE	AR M	2 0 1	HR	M	SEC	LAT	LONG	DEFTH		MAGN	ITUDES-			INT	FFENOM	RN	CE	Q/S	MAP	DG	DIST
AN LUDICY	176 4	0.00	1101	- 0		TE		(Kri)	BUDT	SURF	UTHER	LUCAL			0101.00						
15: 19	44 7	2 2!	CI	31	44.54	26.7°CN	155.1334	(12				. 4. 3(ML	FV0			613	F		113	(5	137.
USE 14	54 3	3 1.	16	5.4	36.01	19.275N	155.1624	00.9				3.6 (ML	t VO			613	F		652	95	76.
155 19.	.64 1	3 15		4.5	Sa . 411	19.292N	155.3574	31.1				3.70ML	FVO			613	F		352	95	85.
155 14	5.4 .	4 .11	12	21	55.15	19.4.51	155.4174	033				3.90ML	HVO			613	F		052	95	49.
11SF 14	6. 0	6 54	15	34	31.94	19.447.	155.2104	(45 .				. 4.03ML	H VO			613	F		C52	95	63.
157 19	64 2	6 . 4	21	22	31.001	19.72CN	155.0174	100				3. ECML	FV0 .			613	F		(52	95	15.
151 14	ot 1	6 36	22	1.	57.51	19.630%	155.4184	308				. 4.10ML	F VO			613	F		652	95	52.
JSE 1 3	64 3	7 11	2:	43	34.54	19.3134	155.115W	205				.4.50ML	HVO			613	F		052	55	82.
USE 11	64]	7 17	23	1.	56.41	19.5924	155.5874	213				. 4.53ML	FV0			613	F		652	95	49.
USE 19	r4 i	7 29	:4	(5	51.21	19.425#	155.2664	(25				3.5(ML	1-VO			613	F		052	95	65.
JSE 17.	64)	1 33	20	36	CL . 71	19.19EN	155.55EW	135				3.5CML	1-VO	,		613	F		(52	95	45.
235 17	£4 ;	5 13	16	27	35.4	19.50.1	155.4004	J1 1	• 4.10MB			* 4.5UML	FVO			613	F	014	052	95	51.
JSE 1-1	64 :	8 26	15	31	45.54	21.2331	156.1504	212				- 4 . 4 UML	HVO			613	F		JBE	63	90.
JSE 1 1	64 v	1 :1	:6	5 7	13.54	14.4521	154.4254	205		,		3.7 ML	FV0			613	F		652	94	160.
, USE :4	: 4a	- :4	. >	?	:2.1	14.4425	154.9378	((3)				3.8 (ML	H-VO			613	F		CE 2	54	99 .
352 1 .	6+)	1 1 -	17	2.2	29.11	: 1.1:5N	165.1150	225				. 4. SCML	I VO			613	F		(52	95	12.
115 : 1.	e. 4 . 3	1 : 1	12	- 7	56. IF	10.0-04	155.1222	905				3.6:ML	F VO			613	F		652	95	12.
7/3 13	£4 :	- 11	1.		4 ? . ! +	1 . 7 · N	: "E . 0174	31.*				• 5. 5: ML	hVO			613	F		252	86	111.
135 13	** 1	. 15	2	2 .	17.21	19.33 1	165.0954					3.70ML	FVO			613	F		652	55	24.
JSE 15.	44 1	: 24	·. •	: '	12 +t+	19.111	165.4134	131.				3.CCML	FVO			615	-		152	93.	11.
USE 14	** 1	. 27	: 2	2.2	6 . F	1 . 4 . 2 .	15.2.24					3.7LML	FVO			613	F		150	75	
USL : .	2+ 1	5 13		21	4 11	19.4.18	155.7850	23.2.*				• 4. 7 ML	F VO			013	-		0602	73	63.
13E 13	24 1	2 13	·.4	31	45.35	19.4.38	155.2.59	. 3.7				3.5.JAL	HVU			613	e		052	75	62.
13E 15	54 :	3 .3	::		1: • FH	19.4.28	155.285W	.3				• 4 • 0CML	FVU			ELS	-		652	75	23.
125 14	· E = 1	2 1.	11		4 t		155.2134	117				· D.LUML	FVO			513	5		152	55	13.
USE 1-	c4 1	2 1 4		s .	17+	14.30EN	155.92+4	- 9 5				J.C.ML	FVU			613	-		353	65	. 1
132 1-	· · · ·	1 +1	14	- 7	42.41	1	155.41.34	113				3.7.11	F VO			613	-		256	36	.70.
F 44 1 4	•	1 14	LF .		2	10 7/ - N	1.0.4.424	12.				3.8/41	F VO			613	F		(5.2	46	67.
152 14			-1		13.25	12.1624		112				3.7:41	E VO			613	F		152	GE	= 6 -
351 I.F	6: 1	- 11		4.	3:. 11	1	100.0.04	113				J. S. MI	HVO			613	5		352	FE.	1:3.
				11.	2	10	110. 174	305				A A COVI	EV0			613	F		1.52	95	73.
0.52 14		3	**	12	12.1	1 1 1 1	150	6113				5. 7(M)	EV0			613	F		652	95	£1.
152				24	13.15	13 3334	153.7.28					4.6081	E VO			613			162	95	45.
031 17	2 2	2 24	11		27 44	1	155					3. 70MI	HVO			613	F		05.2	95	69.
J	e	4 1 1		27	3 7	10 7 1	156 . 1365					3.5 ML	EVO ·			613	F		652	96	33.
		5 16		57	47.41	10,1371:	166.4461	res			•	3.5(ML	EV0			613	F		052	55	48.
134 13		5 75	•.		2	15.10° N	166.1.10					3.6731	F VO			(13	F		(52	95	12.
152				•			· FS 1131	17=				3.5.91	EV.			613	F		052	95	59.
J			••		3	0 717N	154 5 11					3.6.11	HVO			614.	F		CEF	26	153.
		7	*:			10 11 1	1.6	· ·				3. 6 . MI	b VO			613			652	95	6 .
0.52		,			14 34	15 3364	155					. 4. 3 CMI	E VO			613	F		15.2	95	42.
	2				14	14. 364	165 1776	207				3. 7. MI	F VO			613	F		652	55	91.
127 17	C			2 3	17.14	19.95.1	1+5.1574	120				3.6.41	HVO			613	F		352	55.	75-
135 14	4. 1		11	1.	17.15	9.33 M	156,1614	1.1.2				3. 5.11	EV0			613	F		(52	95	77-
0.02	•••••	1 25		31	35.31	16 1174	155.1534	115				3.5(ML	EV0			613	F		552	95	78-
126 1-	L	3 11	4		57.14	19.4431	166 3334	532				3.1 (M)	+ VO			613	F		652	95	59.
112 13		4 72	11		A	16.215.0	155. 634	90.5				3.7 CMI	FVO			613	F		052	95	90.
105 14	44 1	1	10	14	50.44	19.35 M	155.3284	.31				3.92ML	HVO			613	F		652	95	÷ 9.
115 14	163 1		12	1.	17.7+	9.774N	14.44.4	41				3. HCML	F VO			613	F		C52	94	115.

£1/17/17.

FACE

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SOURCE	YEAR	NU	DA	на	MPI	SEC	LAT	LONG	DEFT	80DY	MAGN	ITUDES-	LOCAL		I fi T MAX	FFENOK	RN	CE	c/s	MAR	G DIST
	ICATES		POS	SIR	IF		ATE			0001	001.1	011 211									
CUS	1965	12	26	:9	15	37.3	19.4:CN	155.2CCW	003	+4 . 3CMR -							613	F	C11	C52 5	95 72
USE	13.60	31	CE	23	43	57.3H	19.43PN	155.478%	034				3.50HL	t VO			613	F		C52 9	42
USE	1760	31	19	12	44	11.24	17.405N	155.3284	013				. 4. CCML	FV0			613	F		052 9	5 58.
USE	1965	51	23	30	C1	37.44	14.3971	155.5588	613				.4.15ML	FV0			613	F		052 5	5 35
FiD	1960	:1	22	.7	62	26.9	19.465N	155.1788	613				3.80ML	HVO			613	F		052 9	95 0.
USE	1965	. 2 2	13	:5	56	16.31	19.372N	155.31CW	030				3.7(ML	F VO			613	F		(52 9	61
HVG	1765	32	22	11	5-	55.3	19.645N	155.670W	333				3.70ML	F VO			613	F		C52 5	
JSE	1960	03	11	50	31	11	19.4121	155.453W	31 2		× *		. 4. 6 0ML	HVO			613	F		052 5	95 45.
- Y J	1ºco	23	13	18	0:	23.3	10.753N	155.7674	028				3.70ML	HVO			613	F		652 5	35 37
USE	1960	63	15	:0	64	53.Ft	:9.3171	155.4424	152				.4.1JML	HVO		×	613	F		652 9	49.
USE	1065	33	: 5	CC.	43	\$2.7t	19.377N	155.3.CW	C32				3.5CML	F VO			613	F		[52 9	5 E2
USE	1905	35	27	11	15	46. 31	19.215N	155.060W	04 3				3.7CML	FV0			613	F		052 9	95 91
HWS	1 165	36	12	27	21	25.9	19.352N	155.7524					3.50ML	HVO			613	F		052 9	15 15
USE	1965	31	01	:5	24	24.54	19.325N	155.405.	013 .				3.71ML	HV0			613	F		652 9	5 47.
USE	1965	:1	31	. 2	5ł	2 31	19.4170	155.426 .	:::				-4.3(ML	FV0			613	F		252 9	45.
USE	1 165	3.	17	·€	57	37.1+	1 . 4 : . 4	1043%	23				3.7:ML	1 VO			£13	F		C52 5	4 103
132	: : 6:	15	15	12	15	41.2:1	15.4: IN	154.21FC	23.3				3.5 ML	FVO			613	F		652 5	101.
JSE	1460	23	19	- 2	2:	43.20	13.1 34	155.1 AV	:30				3.5.ML	FVO			613	F		052 5	15 E.1.
JSE	1965	: 1	\$ 5	!ć	.3 ;	5	13.4434	155.417%	121	• 4 . 7 CMP			• 4 • 5 PML	нур			613	F		152 5	15 4P
3 î L	1 7 5 6	: 1	21	22	: *	21+	13.4714	155.4112	225				3.5.ML	FVO			613	•		LOK	5 . 49
350	: 100	:.	: 3	15	47	17.21	1 5 751:	115.2-28	:25				3.5.ML	F A 9			613	F		652 9	5 63
USE	:	1.	51	. 4	9-1	21.54	19.32.N	155.4674	5. 3				. 4. 5. ML	HVO			613	F		552 5	
447	1960	11	::		+2	32 . 2	19.5 1.11	: 53 . 3 . 3 .	30 3				- 3.8 CML	FVD	۷.		613	F		052 5	5 4.
JOE	1-65	11	17	:5	17	() . : F	: 4 . 1	164.6339					3.51ML	F VO			613	F		152 5	106.
USE	1-600	11	27	21	5+	-b1.ft	19.2.54	155.2304	י בנ				3.6.34L	F VO			613	F		1:2 5	5 71.
11.1	: 7.60	11	12	:5	4 5	11.1	: - + 75.N	155.6734	693				3.7.ML	FVO			613	F		152 5	5 1.
- +	1. 6.	13	13	15	41	15	19.2564	: 56 3 .	- n a				3.0 ML	HVO			613	F		052 9	46 48.
JSE	1 6.	1.	24	: 1	.:	3	1	155.117%	1.0			1	3.5:ML	HV0			613	F		652 9	5 11
JSE	1-57	51	11	:3	:4	21.51	16.1.15.1	116.3.6.8	C 5 5				3. CIML	FVO			613	F		152 5	5 E1
USE	1 167	11	:1	. 5	13	19.6F	19.3354	155.3334	327				3.5 PL	FVO			613	F		952 9	5 21.
C.5	1-6?		5 : 5	. 1	37	41. "+	19.543N	155. 929	3:5	14.6CMR			. 4.55ML	HVO			613	F	542	052 5	5 F4
C 3 3	10.1	4:	4	:5	3.	33.35	19.374N	155.4531	076	•4 • 4 3 M B			. 4.5 UML	FVO			613	-	036	052 5	15 46
USE	1 - 07	21	2 3	: 5	47	21.41	19.41 FN	165.4(1%	CC 7				3.4(ML	FVO			613	F		352 9	5 11
JSE	1-47	: 6	13	2 .	33	1 41	21 11 4	155.267%	\$27				3.15ML	IVO			613	1	,		5 124
JSE	1 1007	30	, : 4	13	5,	55.74	19.7160	155.3844	655				3.6.ML	FVD			E13			052 5	5 12
JSE	1.27	3.	24	:7	4.7	15.5-	13.266N	155.5621	206				3.2 ML	HVG			613	F		152 5	5 55
332	1 = 67	i		. 8	31	54.11	19.341 N	1-5-2154	(2				3.11ML	FAD			613	r		152 5	5 640
• 213	1 167	1	.);	:-	11	41.2	1	142.1109	537	• 4 • 2 CMP							. 613		(12	102 3	
352	1 1417		· · -		1.5	4 1.	14.45.5	150.2.2%	1350				-4-5.ML	FVU			613	r		002 0	
155	· 'o'	,	. 13		1 +	: 1. 3+	12.366%	155.1154	v. c.				3.5.ML	HVO			613	P		152 5	
JSE	.76		1 12	:2	51	1	14.3P3N	150.425.	5-0				• 4 • 1 JML	FVO			613	r		102 7	10 48
USE	: 357	¢	11	. 3	14	17.4+	19.5°2N	155.215%	(2)				3.CCML	FV0			613	1		652 5	5 630
JSE	1 - 07	3	1 12	- 2	24	23.ct	19.4-14	155.617W	112				J.ZLML	FVU			613	-		102 5	220
USE	1-67	3	22	- 1	34	27.).4	14.351N	155.4158	0.7.8				3.2.ML	FVO			613	-		012 1	5 50
13 -	1 101	6:	0 14	.5	5.	Ca.cr	13.2181	155.5-54	1.1		•		3 . 3 ML	PVO			613	F		102 5	42
1135	:947	51	:5	15	11	51.24	19.7150	155.269%	(26				3.2CML	FVU			613	F		052 9	5 65
135	: 767	51	15		2 !	32 . 1 +	19.3478	155.3142	123				. 4. CCML	FVO			61.5	-		152 9	5 76
356	1 +57	3.	: 10		41	2:.71	19.9530	155.3EFW	2.9 e				3.9.ML	F V0			615	F		152 9	5 /9.
.J 3 E	157	3	1 1 9	31	13	22.41	13.3954	155.3529	01.5				3.20ML	HV0			613	F		652 9	5 79.
USE	1001	-	: : 9	.2	-7	36.44	10.0124	155.5244	C3 4				3 . 30ML	FVO			613	F		252 0	5 12.

E1/:7/17.

FAGE

S	SURCE	YEAR	.ec	DA	+	1 11	SEC	LA	LG	DEFT		NAGNITUDES			INT	FFENOM	RN	CE	6/5	MAR	DG	CIST
			•							(< < >)	BODY	SURF OTHER	LOCAL		MAX	DISANO						(KM)
**	A IPD	ICATES	A	FOS	STH	LE	DUFLIC	ATE		10.00								-				50
	USE	1967	55	24	LE	(2	51.31	19.15CN	155.518 8	CCF		1	3.40ML	HVO			613	F .		052	93	720
	JSE	1967	55	27	17	45	19.21	19.3°2N	1:5-2164	CCF			3.5CML	FVQ			613	r		152	70	12.
	JSE	1 1.67)5	51	17	36	23.51	19.315N	155.416W	009			3.20ML	F VO			613	•		152	95	52.
	USE	1451	10	17	10		52.11	19.352N	155.267W	039			3. 3CML	HVO			613			052	73	DE.
	USE	1967	33	37		11	05.91	19.2551	155.3018	63C			3.1CML	H 40	2		613			052	75	16
	CSS	1967	63	CE	12	22	29.9	19.3CCN	155.6CEW	(17	•4.1CMB		•				613		014	052	73	33.
**2	2 JSE	1967	04	35	13	22	32.51	14.4171	155.2154	C1 3			• 4 • [[613	5		05 2	95	51
	USE	1367	29	23	10	31	23.51	19.2-34	155.3679	310		*	J. DSML	PVU			613	F		052	95	76.
	USE	1-61	34	20	22	2 37	25.41	19.1711	155.1646	140			3.4041	HV0			613	F		652	95	70.
	JSE	1721	94	28	1.	1 1 1	1 20.14	19.4034	100.114	620			3.2CML	FV0		2	613	F		052	65	43.
	051	1961	1-	10		4.3	St	19.7830	155.48.54	200		•	3.7041	L VO			613	F		152	95	44.
	USE	1	1,1	1 3 3	1	5 51	32.11	13.514	155.3510	632			3-0041	E VO			613	F		052	95	68.
	USE			20	11	1 1 4	37 9	13.3544	165 6524	21.0		3.20		1 10			613	F		652	55	67.
	132	1 4 5 7	11	- 1			F. th	19.4" N	1-5.3-14	:25	•		3.1681	HVO			613	F		652	95	£4.
	127	1 1 . 7					1	15.4 TI N	1 65 . 21 54	110			3.4 [ML	h VO			613	F		(52	55	63.
	158	1 -+ 7	1.			·	14.61	10.15 4	155.4162	615			3.2CHL	t VO			615	F		(52	95	51.
	1.	1 167	11	5.	10	2.	4	14.11.1	155. 31 31	200			3.3 JML	1-VO			613	F		552	95	ć4.
	110	1.27	: 2	1.	12	1 4	12.51	19.3/14	155.1.24	21.2			3.1 1HL	HVO			613	F		652	95	73.
	JSE	116:	12	6 9	2.	1 7	.2.21	11.41-1	1:5.4:44	40.5			3.10ML	FV0			613	F		652	55	.4 5.
	1155	: +++	1:	10	4	1.	15. 71	15.1164	150.335%	1:1			3. C[ML	1- V O			613	F		(52	95	65.
	132	1 - 6:	31	: 5	11	1 1	47.71	19.3331	155.1334	310			3.CCML	t vo			513	F		C 5.2	95	16.
	USE	1 44.2	41	: 1	1 15		11.11	1 1 71	155.2074	34 5			3.50ML	F VO			613	F		652	95	56.
	JSE	1 2000	11	25		43	44.51	19.1514	155. 194	A C C			3.7.3ML	HVO .			613	F		652	95	92.
	USE	1 561	.2	12		5.3.3	14.61	19.1344	155.1144	:19			3.5CML	FV0			613	F		6.5	95	F1-
	USE	11.6.	32	15	::	7	+7. ft	19.35.14	155.3.24	5 34			3.1(ML	F VO			613	t		C52	95	ti.
	JSE	: -4::	34	34	1		11.11	: 3: 3N	155.4574	3:5			3.7(ML	FVG			613	F		352	95	46.
	JSE	. '0:	24	1.	11		24	14.3-51	155.264	27			3.75ML	NVG			£13	F		152	9F	£
	300	1964	:4	15	20	3.	25.5+	19.2253	155.417%	31 5			3.00ML	HV0			613	F		652	95	54.
	'JSC	1551	:4	2 -	· . f	::	42.11	10.146N	155 . DEEN	129			3.2(ML	FVG			613	F		(52	55	65.
	USE	::	14	26	14	1 28	59.31	15.76EN	155.285%	531.			• 4.5(ML	F VO			613	F		C52	95	64.
	USE	1	34	2:	::	: 3:	2511	1-4-21	:55.4358	338			3.4 3ML	F V0			£13	F		552	95	47.
	JSE	1 7 65	25	23	21	42	34.51	19.4:7N	155.261 W	003			3.70ML	HVO			613	F		052	95	65.
	USE	: 9 42	15	::	:1	1 17	25.41	19.3354	155.1179	e 0 0			3.1CML	rv0			613	F		625	95	E2.
	JSE	1 76:	94	13	::	? 7	EF . 91	19.3-58	155.215W	635			3.CCML	1 10			£13	F		C 5 2	55	64.
	JSE	1 40-	0.5	: :	1 14	3=	1: . 1	13.4:14	155.2-44	105			3. SUML	PVO			613	F		52	95	63.
	JSC	1 . 5 =	. 17	12	20	5	96.3	2N	1-517%	37 F		3.40				÷	613	F	,	CAE	65	63.
	135	1 700 1	: 7	1.	1 1	1 4 3	19.21	13.317N	115.41.4	-13			3.5.3ML	FVO			613	ŗ		-52	35	120
	735	1		2.	• •		24.51	1	155.1555	11:			3.3(PL	FVO			613			152	95	***
	135	1.401	1	S.			1	1	10.004	0.14			J. JCHL	FVC			613	-		052	90	67
	155	• " • · · · · ·	37	5.		5:	44.11	14.35.10	125.1.14	619			J. TIML	HVU		,	615	r		222	70	C.3.
	JSE	1 104	-5	33		. 54	37.21	14.5550	155.1.2%	J1 'G	• 4 • 9548	1 60	• 4 • 9 [ML	FVU			613	F	022	052	95	23.
	JSE	1460					55.41	19.1 523	155.9168	14:0		3.20					613	F	-11	. 52	90	43.
	15:	:		1.	1	: 31	10.0	17.7.14	100.0039	0.3		3.10	•.				611	5		26.2	55	10
	145	1 100	00		4	1 2:		1	100. 11 30	1100-			1 7081	440			617	5	116	052	0.5	17.
	052	1762	15	15	11		12.41	19	166 2134	(16			3. 2041	E VO			613	F	.110	052	95	6.0
	050	1.1.61				1 1 4	17 /1	14 1674	165 1631	0.04			A. ICHI	F V0			613	F		552	06	71
	135	1 10	10	-			1 4- Di	17.0.34	155.414	220			3. SOME	E VO			613	ć		CET	56	11.
	352	1 1 6 2	10	2 .		20	5. 11	16 1.31	1-5 (11)				3. 00HL	HVO			613	F		36.2	55	51.0 A 1
	11771	7.	1.				20.0-		1-3-5-14	0	E	LGE 6	Jesunt				444			0.56		

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SOURCE	YE AR	MU	DA	FF	RMY	SEC	LAT	LGNG	DEFT (KY)	BODY	MAGN SURF	ITUDES- OTFER	LOCAL	• .	INT MAX	DISYNO	RN	CE	0/5	MAR	DG	CIST (KN)
V 1:10	ICATES	A	POS	SIE	BLE	DUFLIC.	ATE											1.20				
USE	1955	33	22	14	4 :9	56.04	19.367N	155.233W	CC 4				3.00ML	HAO			613	F.		052	95	69.
JSE	1961	29	03	::	: 58	23.41	19.35CN	155.4504	CCF				3.1[ML	FVO.			613	F		C52	95	47.
USE	1750	39	35	16	6 12	45.7+	19.952N	:55.365₩	960				3.2CML	F VO			613	F		C52	95	75.
JSE	19.60	24	JB	21	5 13	44.3H	19.435N	155.2684	020				3.7CHL	HVO			613	F		C 5 2	95	64.
USE	1 166	:0	24	34	+ 11	53.3	20.1671	155.2.14	308	(91		4.19	•			2	613	F		688	05	78.
USE	1461	10	26		: 47	19.91	19.152N	155.5014	333				3.70ML	HVO			613	F		052	95	53.
USE	1 761	11	10	20	21	45.41	19.4:1N	155.4144	C C 7				3.3CML	F VO			613	F		[52	95	42.
USE	1450	11	14	15	3 52	59.11	19.217N	154.9668	007				. 4. 30ML	FV0			613	F		252	94	100.
USE	19.64	11	20		6 43	21.14	19.3:41	155.3:04	333				3.70ML	HYO			613	F		252	95	62.
USE	1965	12	17	13	2 33	23.5H	19.3194	155.200W	C1C				. 4. 7 JML	FV0			613	F	C37	052	95	73.
USE	1961	12	20	it	1 15	11.11	19.333N	155.1(2%	611				3.5CML	HV0			613	F		352	95	23.
135	19:64	11	16	23	3 25	.1.21	19.5184	155.2174	615				3.6CML	F VO			613	F		552	95	72.
USE	1.4:59	31	15	27	7 37	26.01	19.715N	155.5.24	029				3.86HL	FV0			613	F		652	95	53.
335	1 - 5 -	11	22	1.	5 55	26.20	19.367N	155.4854					3.2 3ML	HVO		*.	613	F		952	55	43.
155	19.5	č 1	21	17	7 14	37.11	19.41.1	155.4124	123				· 3.2[ML	HVO			613			652	55	51.
1.12	1 67	12	17	. :		61.11	19.2714	155.3564	:45				3.5CML	+ VO			613	F		(52	95	63.
135	1.00	,			.7	Sanat	19.35 34	152.3834	13 3				3.5 ML	HVC .			613	F		452	95	54.
155	1 10.4		: 9			43+	4.134N	155.1505	.1 7				3.3:4L	HVO			613	F		052	95	76.
USE	: 101	12	1.			4 24	19.1334	155.1338	011	.4.5.115			.4.1C%L	HVO			613	F	118	252	95	£ 6 .
JSÉ	1961		17			"sont	19.471N	15.164	(1)				3.3[ML	FV0			613	F		652	95	. 72.
235	1-61		2:	11	14	1 1	10.414M	156.1254	613	3.9CMF			3.5CML	I VO			613		(13	652	96	61 .
155	14.64				7 15	36 . 14	19.3.20	155.4.16	1.1				3.7.ML	hVO			613	i		:52	55	54.
JSE	1107	13	11		3	41.96	19.4:34	155.433%	COF				3.70ML	HVO			613	F		052	55	47.
137		13	: 5		4 1 5	1	11.5141	155.4144	(35			3.60					613	F		652	85	58.
135	1 755 3	15	11	: :	3 34	37.61	12.11-1	155.2699	627				3.5CML	t VO			613	F		652	95	65.
15-	1464	1.	11	21	11	11 . 2"	12.2174	155.452%	9:5				3.73ML	FV0			613	F		252	55	53.
150	161	.4	14	-	1 2	-7	19.1758	155.435%	176				3.4 2ML	HVO	·		613	F		052	95	47.
JSE	3.05	4		14	4 4 :	24.14	19.4 21	: 55 . 4514	11.0				3.20ML	FV0			613	F		152	95	46.
USE	: 36 .	. 5				13.11	10.4141	155.6194	111				3.7CML	FV0			613	F		(52	95	21.
195	1	1.4	1 1		1 15	27.61	13. 1r6V	155. 698	111	· 4.93MB			. 5. 30ML	E VO			613	F	[49	C52	55	16.
155	1303	1.4	1 :	14	4	43.90	19.3.11	155. 1174	31 ?				3.16ML	FVO			613	F		052	95	53.
JSE	1	. 24.	17		4 34	46 . 17	17.9154	.55 85%	47				3.00ML	HVC			613	F	(9)	052	95	56.
135	1962		17		2 12	51.4+	11.235N	155.4174	634				3.60ML	F VO			613	F		252	95	55.
USE	: - 6 +	25	23	1	3 . 7	21.11	19. 341	155.6348	C12				3.ECML	FV0			613	F		(52	95	1(1.
JSE	1 261		25		5 54	57.21	17.3144	155.1184	3.15				3.80ML	t VO			613	F		652	95	12.
Jaz	1 + 5-	55	35	1 :	5 43	15.11	11.3154	155.533W	15 0				3.70ML	FV0			613	F	8	052	95	36.
435	:	• =	20		4 .1	44.71	19.3344	155.111W	264				3.3(HL	FV0			613	F		(± 2	95	11.
JSE	1	35	27	: :	- 1 -	2 +	1 1	155.264%	:1 6				3.3.ML	F VO			613	F		652	95	63.
135	1.200		13		5 33	61.14	19.133N	1:5.1194	:11				3.36ML	FV0			613	F		652	95	٤1.
13E	1461	2.5	. 4		3 3 2	51.31	19.3 11	: 55 . 2 . 1 %	.17				3.71KL	FV0			613	F		252	95	74.
435	1563	24	: 5		43	41.34	19.1171	155.211.	107				3.7 CML	FVO			613	F		C52	95	72.
15.7	1.64		16	10	9 41	45.91	0.4 1 M	155.45.18	211				. 4. 4 (ML	FV0			613	F		(52	95	46.
215	13.57	10	2.5		1 55	3100	17.4. 14	155.26EN	11 2	+4 30MB			. 4. 2. ML	FV0			613	;	012	652	55	53.
JSE	1=61)0	17	1	1 41	26.24	17.2678	155.1834	-11 "				.4.0:ML	HVO			613	F		C52	95	77.
135	1941	0.0	17		4	53.1H	17.9 45N	155 . 1.2 W	261				3.4:ML	rvo			613	F		052	95	97.
135	1 7 6 9	:5	:1	1.		4 41	19.3511	155.0508	007				3.BCML	F VO			613	F		(52	95	11.
USE	1:51	:1	13	:	6 57	30.61	17.5-24	155.2:04	0.5				3. CCML	+ VO			613	F		(52	95	73.
JSE	1 - 4.2	37	1 35	21	1 37	24.24	19.3254	155.3514	332				3. 50ML	HV0			613	F		652	95	56.
321	1201	17	13	:	1 22	22.14	19.2 .11	155.5654	330				. 4.23ML	HV0			613	F		\$52	95	44.
U52	1763	::	2"	14	4 47	11.1	19.3150	155.9(2%	(1(3.60					613	F		652	95	9.
11/37/1	7.										AGE	7										

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SIJ	SCE Y	EAR	:13	AC	FR	-11	SEC	LAT	LONG	DEPTH		MA G!	ITUDE	S			INT	PHENOM	RN	CE	Q/S	MAR	DG	DIST
										(KM)	BODY	SURF	OTH	ER	LOCAL		NAX	DISANO						(KM)
	11010	ATES	AF	05	518	LE	DUFLIC	ATE		,														
L	ISE 1	969	93	07	34	42	17.2	19.685N	156.0354	304			3.50		,				613	F	•	C52.	96	29.
J	SE 1	+art	19	13	19	42	20.44	19.3331	155.416W	C31-				- 1	4.30ML	H NO			613	F		052	95	51-
	SE 1	467	13	11	22	11	67.2	20.3334	155.0509	005		×	3.00						613	F		683	05	136-
	ISE 1	961	1:	14	22	55	31.94	19.369N	155. 1674	00 9		-		1	. 4 . COML	HVO			613	F		052	95	26.
· .	ISE 1	969	12	22	13	26	30.51	19.36FN	155.384W	C11					3.3CML	F VO			613	F		652	95	53.
	ISE 1	1953	11	35	15	21	24.64	19.059%	155.3514	900					3.6CML	F VO			613	F		C52	95	79.
	155 1	fait	11	1:	15	12	12.211	19.144N	155.5ilW	306					.4.50ML	HAO			613	F		052	95	52.
-	SE 1	367	11	11	37	23	25.71	19.4521	155.3534	213					3.13ML	HVO			613	F		052	55	12.
i	13: 1	1969	11	23	ic	: 5	44.64	19.5511	155.083W	117					3.6CML	HAO			613	F		052	95	84.
L	ISE :	969	1:	23	23	34	16.51	10.1134	155.516W	C32					3.2CML	FVO			613	1		152	95	F. L.
	ISE 1	ton?	11	24	19	12	22.9	19.6F5N	156.0514	035.			•4.50						613	-		052	76	20.
1	ISE 1	1967	12	11	6.9	55	23.31	19.9-53	155.334	009				٠.	3. SCML	HVO			613	5		052	73	17.
L	ISE 1	1-6-	12	(7	25	34	20.94	19.3338	155-1JCW	510					3.10ML	FVO			613	2		652	95	76
2	ISE 1	1463	12	25		34	34.1+	13.5 N	155.135%	625					3.2(ML	FVO			613	-		152	73	60.
	192 1	1.6 .	12	3:	13	23	25.71	13.301N	155.2639	232					3 3 EML	F VO			613	5		DE 2	93	70
	13 - 1	. 9 ,	1?	32		23	44	13.117N	155.735%	310					4.13ML	FV0			613	r c		25.2	95	10.
-	195 :	1.00	1-		14	1	52.74	14.5551	155.4654	-1					Jobunt	nyu			613	r		152	95	26
- 1	• • • • •	47.			12		52.5	14.416.4	1-5.+354						5.5 ML	FVO			613	F		152	95	31.
•	132 1			14	64		32		120.0011						3. 3 MI	FV0			613			052	95	1 4 -
	17	7.			1.2			1	11201014	31.1					3.1 ML	HVC			613			65.2	95	\$2.
-			::		.5	7(17.32.7%	100+1174						3.6 41	EV0			6:3			052	55	12.
			1.	- 7	10		10 1L	10 5101	166 . 1 6U	1.1.4					3. J CML	E VO			613	F		052	95	86.
•			13		• .	17			155.1639						3.3 MI	F VO			613	2		(5 2	95	3.
		577	12				11.2	·	155.6752	11					3.4 141	HVO		F	613			652	95	44.
		- 7	12	14	6		A	17.4 14	165.1.79	22					3.1 ML	HV0		Ē	613			C52	95	£1.
		37.					21	2 1 . 3 - 7 ::		121					3.1CML	F-VO			613	F		352	95	62.
			. ,	16		· · ·	4.1.	13.1144	1 35 . 47 79						3.4 ML	I VO		ε	613			652	55	44.
	15. 1	- 7			1.		51.30	17.144N	15.4672	238					3.5CML	F VO			613	F		352	95	46.
•		371	. 7	17			35	11.3174	155.1524	:25					3.3 ML	HVG		Ε	613			252	95	67.
Ð	15= 1	1.7"		1.5		. 47	35.74	12.3570	: 55 . 267%	227					3.40ML	FV0			613	F		652	95	65.
	1.	- 7:	: 7	2.5	:6		41	19.4131	:54 . 193W	102					3.4 ML	FV0			613			(52	94	114.
	¥3 1	19.7	23	2 :	16	54	2:.8	16.9671	156.1444	145					3.4 ML	F VO			613			052	16	64.
i i	173 :	: . 7.	.3	32	:4	33	:7.2	: 1. 5 : 3 %	154.9354	141					3.9 ML	FVG			613			052	94	99.
	13 1	1.7.	.3	32	1-3	3.	11.5	:4.372"	155.2749	13 *					3. 3 ML	FV0		E	613			052	95	65.
6	:55 1	- 7	:3	:3	::	5:	:2.7	21.6:24	155.5515	C: 0			.4.03						613	F		SFB	05	71.
	× 3 :	= 7:	: 5	: "	11		::.4	: 4.4 = 6.4	104.16:4	:01					3.1 ML	FV0			613			(52	94	1(7.
		- 7 .	: 3	1 -	. :	21	41	11.37 1	155. 461	· · ·				0	4.3 ML	t vo			613			152	95	68.
0	13 5 1	- 7	. :	: 0	11	23	5 71	11.3654	185. 114	517					.4.10ML	FVO			613	F		:52	95	22.
1	152 1	2 11	. 3	1 1	:1	4 :	2: .:+	19.134N	155.2614	C31					3.0CML	rv0			613	F	-	(52	95	66.
	11 1	1 - 7:	: 4	30	. 2	1.	26.4	19.5:11	156.257%	224.					4.C ML	FVO		E	£13			1:5	55	66.
	ISE :	7 !	11	5:	12	35	26.71	. 9 . 51 N	155.0514	32 **					.4.30ML	F VO			6:3	F		652	95	66.
	173 1	197.	.5	5:	2:	3.		19.33:5	155. 56W	JGH					3.7 ML	HVO			613			652	95	88.
0	JSE 1	1 7.7.	14	11		5.	12.5H	19.514N	155.1558	337					3.85ML	FV0			613	F		652	55	69.
		- 7:	:4	¢ 1.	. 1	1!	11.1	19.3/44	155.155.	031					3.C ML	HV0			613			052	95	78 .
	-13 :	1 . 7.	24	12	. 7	1 1 5	43.1	19.4:21	155.4334	C1 7					4.2 ML	1 V O		E	613			C 5.2	95	48 -
•	ISE S	1 7 7 :	: +	12	19	1 1 1	+3.7+	19.3494	:55.4174	311					4.3.ML	HVO			613	F		052	95	50.
	11. 1	1 3.1.	:4	1.5	.:		4.2 . 4	19.41EN	155.423%	,00					3. 0 ML	hVO		Ε	613			652	55	48.
	143	1 2.1:	. 4	. 4	::	7	:7.5	19.4 -3N	155.134:	021					3.5 ML	FV0		ε	613			352	95	68.
	-V: 1	197:	:4	1 4	::	. 51	25.1	19.681N	: 0 . : 674	:37					3.1 ML	F VO			613			052	56	52.
-1/	1/11											FAGE	ŧ											

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SJURCE	YEAR	NJ	AC	FR	41	SEC	LA	L'' G	DEPT		MA GN	ITUDES-			INT	FHENOM	RN	CE	0/S	MAR	DG	DIST
									(KM)	RODT	SURF	UIFER	LUCAL		TA A	012440						the s
*** 1 10	ICA ILS	A	105	513	1.1	ET AL	12	166 0741	20.4				3 (())	L VÓ			613	F			06	68.
O USE	1975	54	14	21	31	31.45	17.4514	100.2048	024				3.0 HI	F VO			613			096	05	71.
443	1915	34	15	-4	20	31.9	23+035N	155.5712	011				J.U ML	P V0			613			0000	05	
EV.	19.71	40	16	UE	20	33.5	19.335N	155.245%	029				J. O ML	HVO			613			052	73	60
. JSE	197:	24	15	12	25	33.55	19.3(2N	155.250%	228				3.20ML	PVU			613	•		352	73	07.
+47	197:	24	17	12	12	13.2	19.55EN	155 . E 90W	664	*e			••• C ML	FVU			013	-		102	93	10.
O USE	1971	34	17	22	12	13.5	19.514N	155.9168	C1)		•	4.10		1			EIS	r		052	22	1.
CAL	19.11	34	19	30	30	318	10.273N	155.427	027				3.0 ML	HV0			613	-		052	95	52.
S JSE	197;	.4	19	15	3.	3:.31	19.251N	155.418W	026				3.20ML	HVO			613	F		052	95	54.
-VJ	1 9 1	(+	24	2:	20	15.0	20.241 N	156.375¥	C17				3.2 ML	HVO		-	613			DEB	66	101.
FA7	1977	24	. 5	:2	25	:7.0	19.417N	155.425W	663				3.1 ML	rv0		ε	613			(52	95	48.
H43	197)	14	20	15	53	52.0	19.471N	154.63EW	0 3 2				3.7 ML	F VO			613	100		C 5 2	94	131.
O JSE	1 7.7)	14	29	31	23	25.3H	19.4254	154.902W	202				3.5 GML	HVO			613	F		\$52	94	103.
443	1973	64	5)	.5	32	14.1	14.335N	155.0982	926				3.1 ML	HVO			613			052	95	E4.
FV3	197:	. +	3.8	.0	: 7	21.1	14.171 N	155.CE1W	(11	•			3.6 ML	FVO			613			C52	95	65.
● JSE	1911	14	: :	10	37	11.6+	19.1471	155.1119	-11				·3.9CML	F VO			613	F		C52	95	\$1.
113	: -1:	34	3:	21	:3	33 . 7	: C . 2 _ 7N	145.3434	237		2		3.8 ML	HVO			613			052	95	58.
- 1 -	. 17:	.5	:1		÷ .	57.8	21 51 1	: 55 . 4 6 3 4	1.14				3.6 ML	HVC			613			26 5	C 5	65.
🌒 Jati	191.	Ċ	< 1	11		Fa*5	21.652N	155.3534	334			3.73 .	10 0 Ker				613	F		098	65	65.
JiL	197.	£ ",	: 2	: 1	4.*	22.24	19.41.41	155 144	C17				3.CCML	F VO			6:3	F		[52	55	63.
11:	: • 7:		23		30	15.2	3N	142.4 64	34				3.1 ML	FV0			613			366	05	76.
- V . 1	7 !	1	10		21	2.00	13.11.4	115.2-14	170				3.1 ML	HVO			613			252	95	69.
• JS:	1	: 5		10	21	31 . 34	10.30CN	155.250	5.6				3.20ML	1-V0			613	F		952	95	69.
F A 3	: 17:	:5	17	. 5	3.	53.6	19.3.DN	15551%	122				• 4. (ML	F VO			613			152	95	٤٤.
O JSE	1 - 1:	いい	1 3	10	3.	53.2+	19.16PM	155, 524	200				• 4.1CML	F VO			613	F		C52	95	٤٤.
1VC	1511	33	13	15	12	57.4	19.415N	155.426%	:34				3.2 ML	F VO		E	613			052	95	4E.
2 2 L \varTheta	124.	- 3	1.4	1	12	57.11	19.3:44	155.4171	; . C		1.2		3.26ML	FA0			613	F		052	95	53.
- 20	: . 7	03	14	11	1 ?	21.1	13.11-11	115.71 94	(11				3.3 ML	F V0			613			052	95	20.
-1.	: 11.	35	15	2	+ 5	15.1	17.4414	155.1149	105				3.4 ML	I VO			615			C.5.2	55	f
24.4	1911	10	1 5	- 5	55	51	19.5×2N	1:3.2474	500				3.1 ML	F VO		E	613			252	95	£7.
r ¥ J	1.47.	3=	: 5	15	52	15.2	19.3:34	155.741%	303				3.3 ML	HVO		E	613			252	95	c 8 -
443	1925	25	15	11	34	2 7	19.335N	155.129W	1:1				3.8 ML	FVO			613			652	95	71.
🔮 USE	: 77:	: 5	15	15	55	57.91	19.35EN	155.2344	654				3.2(NL	F VO			613	F		(52	55	69.
- 7 1	1 4 7:	30	15	23	50	4	18.395N	155.146%	363				3.4 ML	F VO		E	613			C52	95	67.
9 JSE	1 - 7 :	13	.16	_ 9	57	43+	19.145N	155.234%	025			•	3.6CML	HVO			613	F		052	95	69.
FN 3	1 97:	15	11	12	36	31 . 3	12.734N	154.743%	567				3.0 ML	F VO			613			652	94	123.
+ * -	177.	: 5	: 9	:5	: 5	33.7	19.395N	115.4524	6:1				3.0 ML	FVO		E	613			(52	95	46.
- 5.1	: = .7 :	10	25	1.	57	12.2	19.275N	155.5124	015				3.1 ML	F VO			613			C52	95	22.
714	197.	35	26	17	46	34.3	17.355N	115.1571	200				3.3 ML	HVO			613			352	95	77.
r ¥)	1	::	20	22	51	15.3	19.4174	.1.5 43.	21.0				3.6 1:L	FV0			613			:52	95	46.
rv:	1 - 7.	: >	50	13	17	41.4	:9.917%	154.(11.	131'				3.1 ML	F VO			613	ι,	~	652	94	137.
- 7 .3	1971	1.6	15		3,	46.5	19.42.N	155.4'64	312				3.4 ML	+ VO			613			(52	95	50.
140	: - 7.	:5	19	23	13	5:	:9.2174	155.5.44	.11 3				3.0 ML	HV0		Έ	613			652	95	42.
410	: 4.75	26	11	11	22	22.5	19.30.1	155.2844	333				3.6 ML	HYO		E	613			052	95	63.
• USE	: . 1:	(5	11	21	22	22.4+	19. 1664	155.2694	(31				3.6CML	FVO		_	613	F		252	95	65.
• • • •	: - 7:	56	15	. 5	11	56	19.3414	155.1224	6:1				5.1 ML	FVO			613	21		552	95	11.
- 40	1973	35	17	14	57	32.2	19.13FN	1:5.4121	: 19				3.3 ML	F VO		E	613			652	95	51.
- 4.5	2021	it	17	:1	44	4	19.5.5N	145.779:	204				3.2 ML	HVO		Ē	613			052	95	12.
9 JSE	1 57	Je	16	. 4	57	51.6+	19.516N	155.4012	039				. 3.4 (ML	FV0		-	613	F		652	95	5.5
CY-	: 97:	: 5	1-	: 4	44	27.1	25 .1 361	154.9534	507				3.7 ML	1.40			613			CHR	CA	116
t V .	: 57:	26	20	ĉé	r 4	:1.4	19.364%	155.0109	C13				3.0 ML	FVO			613			152	95	15.
21/07/1	· ·									1	FAGE	9										

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SJURCE	YEAR	MO	DA	⊢R	MN	SEC	LAT	LONG	DEFTH		M	AGN	ITUDES-	1.004		INT P	HENOM	RN	CE	Q/S	MAR	DG	DIST
ANN TADE	CA		120		FI		ATE			8001	30	N.F	UTALK	LUCKL									
44.3	1971	16	22	12	36	42.0	19-3-71	155.4624	0.39					. 4.3 ML	HVO		Ε	613		•	052	95	45.
- 4.3	1971	17	14	21	41	12.9	19.3774	155.3634	30.8					3.2 ML	HVO			613			052	95	86.
- 44.3	1 3 7:	17	1	21	57	12.8	19.41AN	155 724	01 3					3.1 ML	HVO			613			652	95	85.
USE	. 47.	: 7	11	-7	4.	13.51	19.364N	155. 664	611					3.2(ML	F VO			613	F		(52	95	66.
- 41	1971	17	11	12	3.2	\$1.5	19-392N	155.2774	331					3.1 ML	+ VO		ε	613			C52	95	64.
- 4.3	19:73		15	14	12	20.3	17.346N	155.1284	000					3.4 ML	F VO			613			652	95	80.
. 185	14.1:		16	12	10	19.61	19.3173	155.1/14	006					3.50ML	HVO			613	F		052	95	£4.
EV 3	157	27	3:	16	15	56.5	26-1:4N	155.4034	038					3.8 ML	FV0			613			890	05	٤7.
- A USE	1 4.7.	17	21	12	15	51.11	10.914N	155.4104	(11		3			3.8 (ML	FVO			613	F		(52	95	77.
	1 473	36	13	12	12	55.5	2J. 458 N	156. 35%	CIA					3.1 ML	F YO			613			611	63	61.
HVU	1 4.71	26	37	1.)	23	07.7	20.036N	155.3334	308					3.8 ML	HVO			613			66.8	65	86.
n ¥ .)	1301	22	07	17	46	35.9	20.071N	155.3289	658			21		3.1 ML	HVO			613			088	05	89.
O USE	1 77:	28	: 7	20	23	Ct . 54	19.90CN	155.3+14	017					3.70ML	HVO			613	F		652	95	72.
+ 4 3	147:	51	16	. 7	41	54 . :	19.4.7%	154.79ak	C41		•			. 4.2 ML	FV0			£13			(52	94	114.
O JSE	1571	36	16	:7	41	53.1+	19.4:51	154.7554	351.		×.			. 4.4CML	F VO			613	F		(52	54	115.
-1.1	: 47.	· · ·	17	1.5	2 -		19-353N	155.2724	-32					3.5 ML	F VO			613			052	95	65.
3 Jat	: + 7:	1)	18	. 7	21	C 5H	: 2. 111 1	155.2164	:32					3.5CML	F VO			613	F		C 5 2	95	67.
112	: 57.	: 1	3.2	17		22.4	14.4163	115.3348	0:0					3.1 ML	FV0			613			652	95	11.
F73	197:	· ·	3 !	. f	b:	:5.4	: . 7 . 411	155.6653	.12					3.3 ML	F AO			613			C 5 2	95	37.
172	: - 7:	(a	. 7	:7	3 +	53.1	12.1.7%	115.4 64	144					3.6 ML	HVO			613			052	٤5	153.
- V -	: " 7	. 1	15	:1	5:	11.5	10.0 3.41	156.4264	515					3.4 ML	HV0			£13			052	96	60.
F +)	1971	0.2	14	11	48	23.2.	19. c 72N	150.677%	123					3.2 ML	HV0			613			552	9E	87.
-73	19.71	. 9	17	2.0	. ?	17.2	19.4:11	155.447%	211					· 3.2 HL	1 10		E	613			C52	95	46.
FV G	1 - 7.	.4	2	1.	2 :	17.7	19.9777	155.0140	127					3.5 ML	HVO			613			C 5 2	56	58.
- 43	1 4.70		21	•:	25	30	19.344%	155.2:19	013					. 4.5 ML	F VO			613			352	95	73.
O	137	: :	2:	11	14	34 . 11	1+.733N	15.2668	(1:					. 4.5 CML	HV0			613	F		052	95	7:.
- 71	1 - 7 1	: 1	2:	22		247	1 7 N	155.2534	100					3.1 ML	FVO			613			(5 2	55	65.
11 -	: - 7		15	.:	1 .	14.5	12.74. N	1.6.5.54	171					3.6 ML	FV0			613			552	56	+2+
- Y J	1921	٦.	26	14	57	17.5	16.435V	155.4628	110					3.4 ML	HVO		E	613			052	95	440
● J3E	1-7:	24	27	10	. 7	17.11	10.416N	115.4564	(1)					3.4 CML	HV0			613	F		052	95	46.
360	1 5 7.	1:	. ?	:0	17	=t . 9t	19.352N	155.2144	632					3.CCML	FVC			613	F		(52	95	64.
- 73	1 137 -	1:	15	. 5	13	15.1	14.345N	:55.1354	207					3.2 ML	F VO			613			052	95	79.
360 🔴	: 571	1:	. 5	14	13	.14.5-	19.35 N	155.117W	554					3.30ML	HVO			613	F		052	95	٤1.
- 4 -	: 37.	1.	. 3	***	4	1: .1.	14.51 .N	165.2488	224					3.3 ML	HV0		ε	613			052	95	ć7.
O JSE	1 - 1:	11	: 3	11	4:	11.it	19.45-11	155.235%	C27					3.3CML	rv0			613	F		052	5 5	68.
143	1 7.7 .	11	14	.1	32	42	19.4221	155.5479	612					3.5 ML	FVO			613			(52	55	35.
440	1 1 7 3	: .	17	15	25	45.0	19.341 N	155.2571	113		•			3.1 ML	F VO			613			652	95	56.
3 . 1	1 5 1 1	1 .	25		1 1	55	10.13.1	155.2475	135.					. 4.2 ML	HVO			.613			C52	95	62.
🕒 J J 🗧	1 9.75	11	22	. :	3 ?	52.++	. 7 . 3 . N	155.234%	63E .					4.20ML	FV0 .			613	F		:52	55	73.
t V .	: > 1:	:.	2 1	: 7	47	11.5	17.5534	:56.417%	((7					.4.C ML	F V0			613			152	96	57.
• U3E	1971	1 -	2)	17	47	5.6	17.5174	156.4331	110				4.00					613	F		C52	56	51.
IV J	:91:	11	5 %	15	5.	:5.2	14.3.4N	155.110W	209					5.1 ML	HV0			613			052	95	82.
O JSE	157	1:	51	.4	5.	57.4-	19.2644	:55.0:34	00.5					3.2CML	HVO			613	F		052	95	ê7.
	1 7 7:	11	: 7	22	41	::.1	19.5 -33N	156.1124	:31					3. C ML	F V 0			613			(52	96	52.
- * -	1 : 7:	11	11	17	12	41.6	19.2134	155.34EW	336					3.7 ML	F V0			613			652	95	62.
● JSE	1 . 7 .	11	12	.3	12	4:. ++	19.2. N	155.3344	637					3.70ML	FV0			613	F		052	95	٤5.
- 13	1973	11	:2	19	46	15.1	19.94:N	155.7024	378					. 4.3 ML	HAO			613			052	95	56.
r 13	1 - 7.	1:	14	19	57	21.7	: 9.9"2"	155.7724	128					3.1 ML	hV0			613			052	55	55.
+ 1 -	1 - 7.	1:	12	21	55	::.3	20.111 N	155.1114	:21					3.2 ML	FVO			613			333	(5	73.
O USE	197)	11	13	31	45	15.6	2 +41	155 344	020			•	4.30					613	F		CEE	65	69.
-1/:7/1											PACE		10										

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SOUR	CE YEAR	MO	0 0 4	FR	4.7	SEC	LAT	LONG	DEFTH	BODY	MAGN	ITUDES	LOCAL		1 N T MA3	FFENCH	RN	CE	Q/S	MAR	DG	DIST (KM)
I	NDICATE	S A	POS	SIPL		UPLIC	ATE															
	() 1971	11	16	44	92	52.1	19.346N	155.1194	900				3.4 ML	HVO			613			052	95	£1.
F V	13 197	11	16	14	23	52.2	19.7HEN	156.3654	008	· ·			3.1 ML	HVO			613			052	96	62.
	F 197	11	16	14	. 2	51.6F	19.333N	155-1014	665				3.3CML	FV0			613	F		(52	95	13.
	1 1971	11	1.6	16	37	50 . 3	19.555N	155.7654	301				3.4 ML	F VO			613			C52	95	46.
. 15	F 1971	11	1.5	16	17	-7.9	19.867N	155.7684	100			3.40					613	F		052	95	46.
	1) 1071		22	12	0.2	11.2	19.115.9	154 1961	00.4				3.0 MI	HVO			613			052	96	45.
	10 107			16	4.5	10.0	10 2371	155 3640	011				3.2 MI	HVO			613			052	95	60.
	13 19.00	1 1		-1		Ar . 7	19.224 N	165.3620	201				3.2 ML	EVO			613			(52	95	62.
	5 1570		15	-1		31 11	19 2324	1.5. 1620	122				3. 3041	E VO			613	F		052	95	63.
	13 1371	1 1	1 1 5		14	31 5	13.1151	155.7.00	312				3.0 ML	HVO			613	•		052	55	43.
	10 1-75	1 1	15	17	5.3	15.2	19.4 114	156.6254	011				3.9 ML	HVO		F	613			052	95	26.
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	5 157		11		2.	10. Ja	19.3641	155.3664				2	3-6CML	by0		-	613	F		052	55	55.
	1 1971	1				22.6	14.6054	156.2414	25				·3.6 ML	HVO			613			652	96	30.
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	1 1 3 7	1 2	7			4	TM	165.4F1V	613				3.3 ML	HVO			613			652	95	65.
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i + 2 i + 3 i + 4 i + 3 i + 4 i + 3 i + 4 i + 3 i + 4 <td< td=""><td></td><td>1971</td><td>34</td><td>25</td><td>17</td><td>12</td><td>57.4</td><td>19.339N</td><td>155-1754</td><td>010</td><td>,</td><td></td><td></td><td>3.0 8</td><td>L HV</td><td>0</td><td></td><td></td><td>613</td><td></td><td></td><td>052</td><td>95</td><td>76.</td></td<>		1971	34	25	17	12	57.4	19.339N	155-1754	010	,			3.0 8	L HV	0			613			052	95	76.
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n vol 1 y viz i i i i i i i i i i i i i i i i i i i	GVF	19.71	34	12	33	14	39.9	14.34?N	155.136V	010				3.2 M	L HV	0		E	613			652	95	79.
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v_{v_0} 1971 $C7$ 22 11.6 $14.249V$ $155.012V$ 215 3.7 HL VO 613 $C52$ 95 61.4 v_{v_0} 1671 33 03 03 03 156 $19.422A$ $155.354V$ 111 3.6 HL VO E 613 $C52$ 95 51.4 v_{v_0} 1671 37 35 154 $41.9.653$ $156.24V$ 111 3.6 HL VO E 613 $C52$ 95 51.4 v_{v_0} 1671 17 154 44.5 $11.9.376V$ $155.283V$ 22 3.0 ML HVO E 613 $C52$ 95 63.4 v_{v_0} 1.971 17 $15.44.49$ $14.65V$ $19.212V$ $155.283V$ 22 3.0 ML HVO E 613 $C52$ 95 63.4 v_{v_0} 1.971 07 $10.44.45V$ $19.212V$ $155.274V$ 170 4.22 ML HVO E 613 $C52$ 95 71.4 v_{v_0} 1.971 07 112.43 22.62 $19.445V$ $155.467V$ 170 3.5 ML HVO 613 052.95 41.4 v_{v_0} 1.71 17.55 $19.45V$ $155.467V$ 171 3.5 ML HVO 613 052.95 41.4 v_{v_0} 1.771 17.52 2.21 $1.55.767V$ 2.23 3.4 H HVO	FVJ	: 57:	:5	27	24	57	11 .1	21.1751	156.9144	(11				3.4 M	LHV	0			613			830	06	128.
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+/J1	- 20	1971	52	13	12	15	47.4	19.6551	156.2400	111				3.C M	L HVO	D			613			152	96	29.
FV51971C7C9C119.2124155.9214C1C3.4 ML FV0E613C52.95711.31971377.216.45.914.65.4749374.4.2 ML FV0613C52.96271.41971371214.45.914.65.4749374.4.2 ML FV0613C52.96271.41971371214.45.914.65.474932.93.0 ML FV0613C52.95411.414.7127171331.721.1980153.456.423.13.1 ML FV0613C52.95421.414.71272527.559.4719.64.91155.464.23.13.1 ML FV0E613C52.95421.414.7127.2522.1526.719.364.155.76.729.93.5 ML FV0E613C52.95461.419.7127.2522.1526.719.364.155.76.729.33.4 ML FV0E613052.9561.419.7127.2522.1526.719.364.155.76.729.33.4 ML FV0E613052.9561.419.7127.2524.1756.227.44.20.155.76.723.33.5 ML FV0E613052.9561.419.7117.3111.35.97.74.155.76.723.33.6 ML FV0E613052.9561.419.7117.1715.17.	- 10	1	-1	\$ 4	- 4 4	45	1:.3	10.3.94	155.213%	1:5				3.0 M	LHV	0		£	613			052	55	63.
- 13 1 471 27272.1514.654146.644171.44.2 ML FV0613C529621 13 19110711141422.619.1554155.47941293.0 ML FV0613C529541 13 1071172122.4171531.721.1594155.4794154.3.5 ML FV0613C529542.+ 12 10711724171531.721.1594155.4274C13.5 ML FV0613C529542.+ 12 10711724171519.4451155.4274C13.1 ML FV0613C529542.+ 12 10711727221519.4514155.4274C13.5 ML FV0613C529544.+ 12 107117272223.127115.754223.12743.5 ML FV0613C529567.+ 12 1071172723.319.5441155.25445143.0 ML FV06130529567.+ 12 1071172723.415.757415.915.919.544415.75715.75715.75715.75715.757+ 12 15711715.319.5444155.767425.43.7 ML FV0613052956.+ 12 157115.319.5444155.767425.7 </td <td>F V 3</td> <td>1 7 71</td> <td>: 7</td> <td>: 5</td> <td>12</td> <td>1 '2</td> <td>44.5</td> <td>19.1124</td> <td>155.221W</td> <td>(1)</td> <td></td> <td></td> <td></td> <td>3.4 M</td> <td>L FVG</td> <td>D</td> <td></td> <td>ε</td> <td>613</td> <td></td> <td></td> <td>05.2</td> <td>55</td> <td>71.</td>	F V 3	1 7 71	: 7	: 5	12	1 '2	44.5	19.1124	155.221W	(1)				3.4 M	L FVG	D		ε	613			05.2	55	71.
473 1371 07 11 12 43 22.8 19.1650 155.2794 50.9 $5.376L$ VO 613 052 95 42.9 470 1071 07 14 17 15 51.74 155.7434 156.7344 116 3.5 ML HVO 613 052 95 42.95 470 1071 07 14 17 15 51.774 153.74544 311 3.5 ML HVO 613 052 95 42.95 470 1671 07 26 15 19.4647 155.7674 017 3.1 ML HVO 613 052 95 44.95 470 1671 17 26 15 19.4647 155.7674 016 3.1 ML HVO 613 052 95 44.95 470 1671 17 25 20.1674 155.7674 028 3.5 ML HVO 613 052 95 44.95 470 1971 17 23.2 20.1274 155.7674 028 3.6 ML HVO E 613 052 95 64.95 470 1971 17 23.3 19.5444 155.7674 028 3.6 ML HVO E 613 052 95 64.95 470 1671 $16.7756.5$ 16.4648 105.96664 102 3.7 ML HVO E 613 052	- 17	1 7:	:1	37	2.	15	44.9	14.6544	155. 1644	1.:.				• 4 • 2 M	LIV	0			613			C 5 2	96	2. •
$-\sqrt{3}$ $1-\sqrt{2}$ 37 22 12 34 $1-34$ <td>713</td> <td>1911</td> <td>)7</td> <td>11</td> <td>1</td> <td>د 4</td> <td>22.5</td> <td>19.155N</td> <td>155.6794</td> <td>200</td> <td></td> <td></td> <td></td> <td>3. 3 M</td> <td>L HVO</td> <td>D</td> <td></td> <td></td> <td>613</td> <td></td> <td></td> <td>652</td> <td>95</td> <td>41.</td>	713	1911)7	11	1	د 4	22.5	19.155N	155.6794	200				3. 3 M	L HVO	D			613			652	95	41.
+72 1371 27 17 31.7 21.199 153.4254 31.7 31.11 51.62 17.199 153.427 117 3.1 11 117 31.11 17.193 113.29 11.17 11.195 11		17:	51	22		1-	3 2	19.0454	155./34%	-16				3.5 M	L HVO	0			613			052	95	42.
FVG 1-71 C* C	-13	1 7 71	:1	2.4	17	- 3	51.7	21.193N	153.2564	-31				3.1 M	LFV	5		-	613			048	15	×1.
FV3 147. 37 24 23 14 34.7 14.3540 155.16.4 054 3.5 HL FV0 613 612 74 HV2 1371 17 29 14 17 23.2 23.1074 155.7624 323 3.4 HL FV0 613 613 652 95 67. HV3 1971 17 51 11 37 53.3 19.5040 155.2014 3015 3.0 HL HV0 613 052 95 67. HV3 1971 16 11 16 12 23.3 19.5040 155.2014 3015 3.0 HL HV0 613 052 95 67. HV3 1971 16 11 16 12 23.3 19.5040 155.4700 010 3.1 HL FV0 613 052 95 67. HV3 1971 16 11 36 43.3 19.5040 155.4700 010 3.7 HL FV0 613 052 95 67. HV3 1971 19.9344 37 36.9 20.14430 155.7770 010 3.7 HL FV0 613 052 95 71. HV3 1971 19.934 34 37 36.9 155.7778 125.7 4.0 ML HV0 613 064 05 74. HV3 1971 19.9 44 11 35 45.0F 21 1.01 155.7670 21.0 3.6 ML HV0 613 052 95 76. HV3 1971 14 14 15 45.0F 21 1.01 155.7770 20.0 3.4 ML HV0 613 052 95 76. <td>1 8 3</td> <td>- 71</td> <td></td> <td>26</td> <td>15</td> <td>+</td> <td></td> <td>19.441 1</td> <td>155.4276</td> <td>11</td> <td></td> <td></td> <td></td> <td>3.1 M</td> <td></td> <td></td> <td></td> <td>L</td> <td>613</td> <td></td> <td></td> <td>(52</td> <td>53</td> <td>420</td>	1 8 3	- 71		26	15	+		19.441 1	155.4276	11				3.1 M				L	613			(52	53	420
1972 1972	FA9	: - 7.	17	25	22	1	34.1	14.355N	155					3.5 M		2		÷	0			652	7:	200
AVJ 147 155 19 147 147 150 19 19 19 19 19 19 19 19 19 19 19 19 19 19 19 15 19 10 10	145	1 - 11	-1	27	11	17	23.2	20.1274	155.7824	12.2				3.4 6				E	613			052	0:	
FV3 1971 11 11 11 12 23.3 1970 14 1971 14 17 165.9 167 16	- 43		- 1	31	**	51	21	17.5244	100.2044	013			<u>*</u>	3.7 4				5	613			052	95	010
+V3 1-11 C C C C C C C C C C C C C C C C C C C	140	1971		1		- 7	52.03	17.014N	1.5. 67/1					3,1 4		, ,		r.	613			111	15	110
PV0 1971 14 15.4 15.4 15.5 15.5 16.6 17.1 16.1 16.2 17.1 16.1 16.2 16.1 16.2 17.1 16.1 16.2 16.1 16.2 17.1 16.1 16.2 17.1 16.1 16.2 16.2 17.1 16.1 16.2 16.2 17.1 16.1 16.2 16.2 17.1 16.1 16.3 06.2 05.7 76. PV0 1971 16.1 16.2 16.3 17.2 17.2 17.1 16.1 16.3 05.2 95 76. PV0 1971 16.1 16.1 19.5 17.2 17.2 3.4 11.4 16.3 05.2 95 76. PV0 1971 16.1 16.3 19.5 17.2 16.3 16.3 05.2 95 76. PV0 1971 16.1 16.3 19.5 19.5 16.3 16.3 05.2 95 76. PV0 1971 16.1 16.3 16.3 16.3 05.2 95	r V)	1 - 11			**		15 1	19.1194	155.2211	.1.2				3.7 4	F LAC	0		F	613			055	45	71.
• ERL 1771 28 34 11 55 45.0H 20.115H 155.900W 217 • 4.0 2ML HV0 613 F 014 068 05 71. • PV0 1971 18 10 06 12 25.6 19.300N 155.172H 003 ar/3 147, 39 11 21 55 41.5 19.530N 155.470W J71 BAGE 12 • 4.0 2ML HV0 613 F 014 068 05 71.	- 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4	1 4 7	17	0.5		14	43.3	20.1431	165.717L	.25.				• 4.0 M	L HV			2	613			DEP	05	76.
FV0 1971 1810 10 25.6 19.305N 155.172H CC3 3.6 ML HV0 613 052 95 76. m/3 147. 1911 21.65 41.5 10.536N 155.450V J71 3.4 ML HV0 613 052 95 45. E1/07/17. PAGE 12 12 12 12 12 12	B 231				11	16	45.11	2.11.1	155 . 5.09					• 4 • J *M	LHV	2			613	F	614	6.20	25	71.
A/3 147 36 11 21 55 41.5 19.536N 165.466W J71 3.4 ML HVO 613 052 95 45. E1/67/17. PAGE 12	EV.	1 5 11		11		1 2	26 .5	19.35FN	155 . 1724	((3				3.C M	LEV	5			613	· ·		352	95	76-
£1/27/17. PAGE 12	2/1	7	js	11	21		41.5	17.5.161	155	171				3.4 M	L HVO	0			613			052	95	45.
	11/57/1	7.									I	PAGE	12			2.5								81

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SJURCE	YEAR	MO	DA	FR 4	N	\$EC	а. 2	LAT	LCNG	DEF TH	+ -	BODY	MAGN SURF	ITUDES- OTHER	 L 0	CAL	*	INT MAX	FFENOM	RN	CE	e/s	MAR	DG	DIST (KM)
*** I :.D	ICARES	AF	255	SIBLE	0	UPLICA	ATE				ı								2.1						
PA0	19.71	CE	15	15 3	i i	CE .7	19.	362N	155.2678	035.	1:			-	. 4.8	ML	HVO		E	613			052	95	72.
FVG	19.71	il.	15	22 1	ε .	37.3	19.	314N	155.218₩	C1C				•	3.2	ML	FVO			613	•	PCT	152	95	64.
O EVL	1931	0.4	15	11 3	5	10. 31	19.	3678	155.253W	125.	• 4	. 50M3			3.0	MI	HVO			613			052	95	37.
	1 9.71	13	25	15 1	3	43.4	20.	256N	155.3739	1.17			4 I		3-2	ML	HVO			613			088	05	98.
EV.	1571	69	r7	19 =		(7.5	19.	3 1 7 N	155.2214	(10			1		3.7	ML	HVO		ε	613			652	95	71.
F V J	1971	63	10	2: 5	à .	46	19.	933N	156.4374	122					3.2	ML	F VO			613			652	96	78 .
CVH	1 9.71		19	15 3	3	46 . 3	19.	234N	155.576W	009					3.0	ML	F V0		ε	613			052	95	41.
r¥J	1 5:71	27	22	11 4	6	31.3	15.	7 55 N	155.314₩	u1 3					3.2	ML	HVO			613		•	052	85	ç
CVM	19:31	10	24	23 5	3	33 . 1	19.	345N	155.2298	P 2 0		1		· · ·	3.4	ML	HVO			613			052	95	70.
FAD	1971	69	25	13 3	9	3:.5	19.	425N	155.4194	CCE		;			3.0	ML	H VO			613			152	73	47.
FV3	1971	34	25	22 4	1	54.4	19.	301N	155.426%						3.3	MI	F VO		E F	613			052	95	. 51.
140	1 5.71	1.7	26	-2 -	0		13.	2521	155. 1560	1035					3.0	MI	HVO			613			652	95	66.
- 43	15:71	64	20	-6 -		54.44		3.3 .N	155.4118	6.3.8					. 3.3	ML	H VO		ε	613			652	95	56.
	1 9 71	• •	1.7	51 2		25.0	10.	: 41 N	1-5.345%	105					3.1	ML	FV0			£13			(52	95	£ 3 .
+V)	1 77:	1.	12	22 1	7	35.3	19.	379 N	155.4254	61 5					3.1	ML	F VO		£	613			C 5 2	95	49.
480	1 9 11	2 1	34	4 4		2: . 4	·: ".	1421	1-5. 43W	128					3.5	×L.	FVO			613			352	96	45.
n V J	7:	1 :	11	23 .	4	14.5	19.	= 35 N	155.254%	511				•	3.1	ML	nv0			613			652	85	69.
F ¥ 3	1 9 71	1:	15	:1 4	it	53.7	1	054N	155.250%	613					3.0	ML	FVO			613			052	85	. 27.
+ V -	: 97:	1.	13	: 8 4		11.5	11.	J. I.W	115.0239	C14					3.5	ML	FVO			613			152	10	15 4
r V G	1 71	11	16	-4 3			2	DITA	155.165W	007					3.0	NI NI	FVU			613			652	95	62.
400	17.71	11	14	14 4		61 3		51411	155 1634	0.9.4					3.1	MI	5 V O			613			052	85	EE.
FV I	1 . 71	11	25	15 5		11.4	. r.	THN	153.312.	666			4		3.0	ML	FV0			£13			6 9 3	65	F3.
r 43	1 5 71	11		23 4	2	54 . 3	20.	4 1 N	1:6.734%	(11					3.1	HL	FVO			613			111	66	116.
- 11	: 97:	11	11	25 4		17.5	12.	1431	155.9734	52 F			8		3.0	ML	F VO		E	613			C 5 2	95	16.
41.	1 - 7:	1 2	1:	- 4		7	17.	3.34	: 55. 225.	611					3.6	ML	HVO		E	613			652	55	71.
C V M	1 2.71	12		:4 4	1	11.2	19.	1 52 N	155.7318	124					3.4	KL	rv0		ε	613			652	95	69.
F ¥ 3	1 - 71	12	:7	.7 5	5	19.7	19.	501N	155.6924	133					3.0	ML	h VO			613			152	95	22.
+ 4 -	1 - 71	12	:1	12 1	7	50.4	19.	141N	155.11CW	00-		24			3.3	ML	FVO			613			152	95	49.
11 10	1	12	10	.2	2		10	1000	100.4238	31.3					. 4. 3	MI	HVO			613			152	95	82.
	1 5.71	17	14		=	33.1	19.	3.4.14	155.793.	1.1.9					3.3	ML	F 70		F	613			552	95	53.
	197	12		. 5 -	ē,	17.5	1 .	1433	155.3194	(34					3.2	ML	1 10		E	613			(52	95	60.
- 4.3	1 . 71	12	15		5	37	: 9.	4154	155.478%	209				2	3.2	ML	t vo		ε	613			(52	95	43.
LVF	19.11	12	14	.2 5	57	2 7	16.	7 N	155.272 .	61 ?					3.2	ML	FV0			613			052	85	131.
- 2 1	1 5.71	: >	14	.9 1	ē	35.0	18.	\$121	155.244	0.00					3.0	ML	HVO			613			552	85	96.
- 3)	1 - 7:	12	:8	.4 :		11	14 .	1 - 34	155.523.	615					3.1	ML	+ V0			613			(52	53	91.
- V)	1 2 71	12	1 1	1 . 1	5	Sc. F	14.	-+14	155.3114	; , ,	3				3.9	ML	1 10			613	••		(52	15	90.
440	1971	12	19	11 -	1	34 . 4	18.	77 1	155.3031	225					3.4	ML	FVO			613			052	25	92.
740	1 + 71	12	5)	.51 1	-	23.4	14.	7378	155.2719	C11					3.1	ML	HVO			613			052	65	162.
+ V 3	1971	12	2.5	-1 4	. 5	1:	13.	TATH	155.3.7%	101					3.0	ML	E VO			613			152	100	166
F A 3	1971	12					16	916.	155-5178	113					3.4	MI	L VO			613			152	15	79.
- 6 3	1 7 71	12	21			53.1	16	2 - 281	165.3029	(12					3. 2	MI	HVO			613			252	ES	61.
	3 71	12	10				1.5	TOTH	155.3.64	318					3.2	ML	FYO			613			052	85	96.
EV.	:971	12	2 -	: .	.3	17.9	16	5 72N	155.3261	(43.					. 4.0	ML	FV0			613			052	85	115.
+ + 3	1 9.71	12	23	22 1	i	42.4	11.	1 62N	156.1334	C12			•		3.6	ML	FVO			613			(52	15	19.
47)	19.7:	12	21	.7 3	7	44.5	10.	- 34 N	155.325%	213					3.1	ML	F VO			613			052	٤5	91.
81/37/1	7.											P	AGE	13											

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SOURCE	YEAN	KO	04	FR	MN	SEC	LAT	LCLG	O LPTH	800X	Mi . (NI	TUDES-		0.041	•	· •	INT	FHENOM	RN	CE	G/S	MAR	DG	DIST
*** I'D	104 15 5	AF	055	TRL	= (UFLIC	ATE	1	NA P	0001	3000		011 24			-									
by J	1971	12	21	:9	34	311.2	19.864N	155.3090	009					3.	4 MI	L HV	0			613			052	85	90.
HYO	1 9 71	12	21	19	51	31.9	18.8311	155.3194	013					3.	0 MI	LHV	0			613			052	85	92.
EY)	1 9.71	12	21	10	43	51.5	15 -1 41N	155-3054	C12					3.	2 MI	LHV	0			613			052	85	92.
by 3	1 9.71	12	21	14	17	22.7	16.113N	155.3174	012					3.	0 MI	LFV	0			613			C52	15	94.
ava	1 9:71	12	22	14	40	56.1	18.634N	155.2568	ū41					3.	2 MI	LHV	0		8	613			052	85	106.
440	1 5.71	12	23	. 4	33	34.5	19-655N	155.2714	229					3.	4 MI	LHV	0			613			052	85	110-
4YD	1 971	12	23	23	24	16.5	19.25JN	155.3388	007					3.	0 MI	LHV	0 .			613			052	95	62.
FV3	1 6 71	12	23	22	52	16.7	18 .8 48 N	155.325W	(13		4		3	. 4.	C MI	L. FV	0			613			652	85	
FV3	1 9.71	12	24	52	20	56.5	18.772N	155.2854	611					3.	9 MI	LFV	0			613			C52	15	e9.
LVH	1 5.71	12	24	50	39	37.1	15.925N	155.2964	300			×.		3.	1 MI	LHV	0			613			352	85	54.
C V n	1971	12	24	15	11	13.1	19.191N	155.3664	009					. 4.	0 MI	L HV	0			613			052	95	63.
CVF	1 71	12	2 +	17	3 1	12.5	19.197N	155.3574	803					. 4.	1 MI	L HV	0			613			052	95	63.
F V J	1 9.71	12	24	19	54	44.4	19.1921	155.35LW	100.					3.	2 MI	LFV	0			613			(52	95	63.
- v 0	1 - 71	12	24	25	47	31.9	13.145N	155.1:64	309					3.	1 MI	LIV	C			613			[52	95	Et .
1V2	1 5 7:	12	25	12	34	13.4	19.1371	155.1504	21.3					3.	S MI	L FV	0			613			052	95	76.
HV)	15.71	12	20	.1	1 +	.1.7	19.24-1	155.364%						• 4.	1 MI	LHV	0			613			252	95	6G.
F V)	1 2 71	12	24	. 2	: -	36.5	10.234N	155.3654	664				2	3 -	4 MI	LFV	0			613			652	95	6 C -
rvu	1 9 71	12	26	11	24	:7 + 1	19.212N	1-5-315%	651					- 4.	C MI	LFV	0			613			152	55	f 3.
- 43	1 9 71	12	25	12	25		14.1.28	145.2574	-10					3.	4 MI	LIV	0			613			C 5 2	55	63.
rvu	1 - 71	12	24	14	11	44.3	19.244N	155.2622	0 ° 8					3.	5 MI	LHV	0			613			652	55	66.
- 4 3	1 1.71	. 15	2 1	10	- 4	4:	:9 N	116.3134	·) 7					3.	1 21	LFV	0			613			052	95	62.
FVJ	1 = 11	13	26	10	17	35.4	19.275N	155.3344	(("					3.	4 ML	LFV	0			613			052	95	61.
r V 3	: 971	12	2€	:4	34	55.9	19.241 8	155. 1619	172						5 ML		0			613			152	95	t. C .
(71	1 7 7:	1 ?	30	21	31	2 4	19.2541	155.3549	. 3 6					3.	6 MI	LFV	0			613			052	95	21.
-11	1 9.71	12	24	21	40	46.2	10.2364	155.3494	138					3.	6 MI	LHV	0			613			652	95	61.
441	1 = 7 :	12	20	22	5.	44.9	19.2194	155.3574	1. 6					3.	C ML	LFV	0			615			152	25	£1.
-1.9	1 - 7:	: 2	?ć	25	55	43.6	19.224M	155.3395	217					3.	5 ML	LHV	G ·			613			352	95	£3.
r V J	1 - 71	12	21	17	22	51 .1-	19.2194	195.1564	202					3.	4 MI	LVV	0			613			652	95	£ 2 .
HV0	1 7.11	12	27	15	25	47.3	19.245 4	155.2164	106					3.	U MI	LFV	C C		E	613			-52	35	50.
- 4.3	1 9 7:	12	27	15	11	52.3	19.2578	155.3729	001					• 4•	/ ML	LHV	0			613			052	75	59.
-42	19.71	12	21	16	- 5	11.6	19.25.2N	155.3546	002					3.	5 ML		0			613			152	95	5/.
FVU	1-11	12	27	17		24.5	19.2674	150.5134	111								0		L	613			152	95	
- 40	71	12	27	18	57	51.4	11.5461	105.1319	J12					3.	4 14		0		5	613			152	10	
ry3		12	21	10	13	21.4	14.LIBN	150.CEIW						3.			0		E.	613			252	25	57.
ny J	1 3.71	12	21	19	2	22.0	13 3454	122.2416	111					3.	7 11		0			413			-52	65	60.
F73	1 2 71	12	24		53	11.7	13.3361	155 1731	60.6						6 341		0			613			(52	55	66
- 2)			14	: 7		2.0.3	- 4 - 2 - 2 .	155.4444							2 141		0			613			052	95	69.
	7.		5.4	•;				155.47.55						. 4.	1 1	L HV	0			613			352	95	5.9.
	- 7	1.	22		4.2	62.3	14.0461	1 F.S. 4 F.B.	- 16					. 4.	6 21	L HV	0			613		-	052	55	66.
- 23	1 . 71	12		::	44	2= . 1	19.230N	155.3660	119					3.	C MI	LFV	ō			613			(52	95	66.
440	19.7	12	3.3		11		13.2 44	155.1659	000					3.	5 11	L hV	0		•	613			£52	55	63.
540	1 9.7:	12	23		17	34.4	4.2324	155.3619	069					3.	2 11	LHV	0			613			352	95	61.
HV3	1 - 71	13	29	1.	23	11.6	19.4374	:55.346%	012					3.	1 ML	LHV	0			613			052	85	93.
EV 3	1 . 1.	12	31	42	3.7	22.1	11.1474	155.3442	(11					3.	5 ML	LHV	0			613			C52	25	F 5.
F73	1 - 72	11	2 -	. 6	12	24.7	11.93"1	155.1951	(31					3 .	3 ML	LIV	0			613			(52	15	94.
HVJ	1972	.1	17	14	47	30.3	19.0.5N	155.2974	:10					3.	7 81	LHV	0			613			652	85	96.
JV.	1972	.1	13	- 6	44	15.3	14.5 46N	155.3:74	65.9					3.	1 ML	LHV	0			613			352	25	¢1.
7/2	1 5 72	C1	13	13	57	3	10.0 3+N	155.3.34	211					. 4 .	3 ML	L FV	0			613			052	85	93.
+ > 0	: - 72	21	13	2 '	\$7	51 .1	LE.FORN	155.2574	£ 2 3					3.	C ML	LFV	0			613			(52	85	÷4.
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SOJACE Y	EAR	NO DA FR MI	520	LAT	LONG	OEPTH (KM)	BODY	MAGN SURF	ITUDES -	LGCA	L	•	INT	FHENDA	RN	CE Q/S	MAR	DG	CIST (KH)
INDIC	ATES	A FOSSIBLE	DUFLIC	ATE															
HYJ 1	9.72	01 18 16 13	43.5	19.459N	155.464₩	009				3 . C . M	L FVO			£	613		C52	95	42.
140 1	512	\$1 19 18 11	23.9	18.901N	155.127₩	051				3.1 M	L HVO				613		052	85	101.
HVO 1	5.72	01 19 20 37	23.7	19.2124	155.2834	012				3.6 M	L HVO				613		052	85	56.
FVJ 1	+72	01 21 11 42	41.9	18.767N	155.2934	012				3.0 M	L HVO				613		052	85	99.
FY0 1	9.72	01 25 12 14	59.2	18.771N	155.256₩	C 0 7	£.			3.C M	L FVO	10			613		[52	15	100.
443 1	9.72	\$1 20 13 35	32.8	18.247N	155.3061	32 3				3.0 M	LIVO				613		052	85	92.
HVD 1	9.72	21 21 .9 26	21.7	16.926N	:55.2984	û13				3.9 M	L HVO				613		052	85	94.
HVO 1	972	31 22 12 4.	19.3	19.24CN	155.393%	209				3.1 M	L HVO				613		652	95	57.
FV3 1	9 72	61 22 15 46	21.4	16 .78 3N	155.2599	CC7				3.0 M	L HVO				613		652	85	103.
FV3 1	572	31 23 27 65	45.6	20.312N	155.93CW	648				3.1 M	L FVO				613		CEE	٤5	93.
FV3 1	922	01 23 19 23	17.8	18.F45N	155.289₩	013				3.3 M	L FAO				613		652	15	53.
- VJ 1	9 72	3: 27 15 21	43.7	16.791N	155.2574	307				3.2 M	L HVO				613		952	85	130.
440 1	4.72	01 29 52 14	49.7	19.321N	155.2934	011				• 4 . 0 M	L FVO				613		052	85	96.
FA7 1	971	c1 30 05 51	42.3	19.779N	156.1234	225				3.0 M	L FVO				613		052	96	38.
FV5 1	4 72	52 12 15 53	21.0	19.2171	115.643W	C12				·3.3 M	LFVO			5	613		652	90	21.
F,VG 1	+ 12	C2 14 16 15	55.4	1.34EN	155.492W	51 .				302 1	LFVU			E.	613		152	15	
7 4 3 1	- 12	C? 16 11 14	4.4	18.00	110.100W	112				3.5 M	LIVO			5	613		152	06	4.9
- va i	. 7 72	.2 1/ 15 1/	20.0	13-21	155.4230	211				1 M	LEVO			E	613			66	91.
440 1		-2 10 14-07	41	14.4.1.171	153.2404	010				3.3 M	L HVO				613		446	25	75.
- 40 I	2 7 7 2	0 10 11 Ju		14.35 aM	156.6359	619				3.1 M	L FVO			F	613		252	55	48.
	071	22 26 22 16		19.63.1	1 5.4664	-1 -				3.2 M	L FVO			-	613		(52	56	63.
	413	.2 31 11	51.3	19.3171	1-5.2732					3.9 M	LEVO				613		052	85	57.
-42		3 74 75 43	37. 3	19.3551	155.7 34	34				3.8 M	L FVO			*	613		052	55	52.
- 43 1	472	(2 11 1: 1-	(5.)	11 . 7 N	155.3204	[13				3.0 M	L HVO				613		652	85	92.
+ + + +	- 71	62 28 22 47	17.5	19.257N	155.5238	203				3. C M	L FVO			ε	613		(52	95	44.
-12 1	774	12 29 12 1.	21.4	15.1940	156.525%	211				. 4.9 M	L + VO				613		C 5 2	96	Éł.
-10 1	5.1.	12 24 12 55	52.1	14.2" SN	156.4034	74				3.4 M	L HVO				613		952	96	56.
O THE .	7.7.2	62 29 22 63	21.91	14.26.50	156 . 5 33W	515	.4.9"MB			. 4.9 M	L HVO				613 F	033	C 5 2	96	71.
1 6 4 7	-72	15 21 23 32	:9.2	19.3/24	156.4111	633				3.4 M	L FVO				613		(52	96	57.
HVJ 1	572	35 33 32 32	53.1	:0.24=1	156.287%	°4 2				3.7 M	LIVO				613		C 5 2	96	49.
- 1V 2 :	972	33 33 68 .1	12.7	16.7771	155.3474	0:3				3.9 M	L FVO				613		652	85	92.
-43 :	5.12	5 34 J: J7		18.775N	155.3544	126				3.2 M	L FVO				613		652	85	95.
F13 1	971	13 28 17 11	26.7	11.752N	155.296%	((7				3.3 M	L HVO				613		052	85	100.
FVJ :	572	3 :9 .3 11	52 . 3	16 . E 32 N	155.316W	013				3.4 M	L FVO				613		(52	15	90.
-10 1	77:	13 13 .3 13	13.3	19.3334	152.1314	906				3.6 M	L 1 NO				613		\$52	95	15.
- Y	+ 72	23 11 15 32	1: • 2	20.175N	155.1904	041				3.1 M	L HVO				613		56 E	05	79.
- VJ :	7.	13 2 1 24 32	26.3	10.3454	::2.1000	264				3. J M	L HVO				613		652	95	73.
-V.) 1	-7.	13 19 11 19	C1 . 4	11 .: "~N	155.3014	:1:				3.4 M	LIVO				613		052	65	8 A .
rii 1	1972	13 3 14 11	21.2	11.4644	155.5141	:22				3.8 M	LFVO			-	613		152	50	11.
143 1	1972	.5 31 15 24	34.9	19.35.4	155.2759	201				• 4.1 1	LFVO			L	615		652	22	16.
- (V -	9.72	13 31 15.55	FF . 9	19.36: N	155					3.1 M	LHVO			Ł	613		652	95	23.
1 C.V.P	1972	1 -5	43.2	19.514N	155.2474	035		8		3.0 M	L FVO			۶	613		152	95	60
FVJ 1	1 7 72	24 JE .8 22	15.3	19 1 194	192.1918					3. 7 4				2	613		152	95	64.
100 1	- 12		55 0	12 76. 4	100+2044	229				3. G M	L HVO	X			613		152	65	161-
	. 77	4 11 23 23	47.9	10.0521	165. 1240	225				3.0 M	LEVO				613		052	85	87-
	1 3 72	14 15 1 AT	12.5	16 . 5 921	156. 3644	C1.5				3.6 4	LHVO				613		652	25	69-
571	1 17 1	14 15 .2 14	21.3	19.1331	155 .: 21 4	010				3.3 M	LIVO				613		C52	95	11.
441 1	1 = 1)	14 17 20 1.	2: 3	1 977N	155.2264	01.5				3.2 M	L FVO				613		052	85	16.
				2															

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Invi Invi Dool John Office Dool John Office Dool John Dool Dool John Dool Dool John Dool Dool Dool John Dool Dool John John	SJURCE	FAR	40	DA	+ R	MN	SEC	L	AT .	LONG	DEFTH	+ -		MAGN	ITUDE	S		 C A 1			INT	FH	ENOM	RN C	ε	Q/S	MAR	DG	CIST
Internal	INDI	CATES		205	SIRI	F	UPLIC	ATE			(1.5)		8001	SUKF	011	LK		LAL				01	5 110						
i y 2 i y 2 <td< td=""><td>HVJ</td><td>1972</td><td>34</td><td>19</td><td>1.0</td><td>16</td><td>40.0</td><td>14.9</td><td>8 SN</td><td>155.6438</td><td>342.</td><td></td><td></td><td></td><td></td><td></td><td>. 4.0</td><td>ML</td><td>HVO</td><td></td><td></td><td></td><td></td><td>613</td><td></td><td></td><td>C52</td><td>85</td><td>E 0 .</td></td<>	HVJ	1972	34	19	1.0	16	40.0	14.9	8 SN	155.6438	342.						. 4.0	ML	HVO					613			C52	85	E 0 .
i y 1 i y 2 i y 2 i y 2 i y 3 <th< td=""><td>EV0</td><td>1 372</td><td>C4</td><td>21</td><td>11</td><td>20</td><td>59.5</td><td>18.8</td><td>+ 2N</td><td>155.319W</td><td>010</td><td></td><td></td><td></td><td></td><td></td><td>3.0</td><td>ML</td><td>HYO</td><td></td><td></td><td></td><td></td><td>613</td><td></td><td></td><td>052</td><td>85</td><td>68.</td></th<>	EV0	1 372	C4	21	11	20	59.5	18.8	+ 2N	155.319W	010						3.0	ML	HYO					613			052	85	68.
iv30 19.2 24 29 19 39 195 3149 014 3.0 RL V0 613 652 65 67. iv30 1972 66 20 02 77 031 30 RL V0 613 652 65 77. iv31 1972 65 14 65 77. 3.2 RL V0 613 652 65 77. iv31 1972 65 11 13 65.5 6112 3.5 RL V0 613 652 76 77. iv31 1972 66 11 13 62.5 77. 3.5 RL V0 613 652 76 77. iv31 1972 66 21 12.5 10.6 3.6 RL V0 613 652 75 76. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77. 77	FV3	: 971	24	26	67	15	15.1	11.9	: 5N	155.3104	C1 C						3.0	ML	F VO					613			[52	15	\$6.
1922 192 192 192 192 192 192 193 192 193 192 194 193 192 194	h V O	15.72	24	29	19	19	53.7	18.9	22N	155.3189	218						3.0	ML	t VO					613			052	15	85.
1972 35 14 25 25 25 25 25 25 25 25 25 25 25 25 27 3.2 H HV0 613 652 95 64. HV3 1972 25 27 35 14 15 155 154 155 154	CVE	19.72	üä	32	37	39	54.2	19.4	SSN	155.2478	031						3.0	ML	FVO				ε	613			052	95	67.
r+32 r+32 r+3 r+3 <td< td=""><td>473</td><td>1972</td><td>35</td><td>14</td><td>::6</td><td>2:</td><td>06.3</td><td>21.0</td><td>274</td><td>157.2544</td><td>151</td><td></td><td></td><td></td><td></td><td></td><td>3.3</td><td>ML</td><td>FV0</td><td></td><td></td><td></td><td></td><td>613</td><td></td><td></td><td>683</td><td>07</td><td>141.</td></td<>	473	1972	35	14	::6	2:	06.3	21.0	274	157.2544	151						3.3	ML	FV0					613			683	07	141.
ry3 j j j j j j j j j j j j j j j j j j j	FY3	19.72	65	15	14	:5	35.7	19.5	27N	155.2724	627						3.2	ML	HVO				Ε	613			052	95	64.
n*0 142 15 27 12 26 12 26 12 26 12 26 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 22 12 23 <	F ¥ 3	1 972	(5	16	22	27	14.0	19.3	57N	155.1514	COF		2				3.0	ML	FV0	, i				613			[52	95	٤7.
n*0 19.2	hyJ	1 7.72	15	27	12	36	11.4	15.9	7411	155.3154)12						3.5	ML	F VO					613			C52	85	77.
n vo j. j2 j1 j2	CV n	1 9.72	ιŝ	32	19	22	12.2	19.2	21 N	156.5244	046						3.2	ML	HVO					613			052	96	73.
FY3 1973 1973 1973 1974	n V D	1972	20	11	:3	34	52.3	1=.3	-5N	155.126N	369						3.1	ML	FV0				ε	613			052	95	80.
r y 11 9722 62 62 62 719 - 6 2 03 - 7 H19 - 6 2 05 - 7 H7 - 7 H7 - 7 H1 - 7 H </td <td>FV2</td> <td>1 7.72</td> <td>:5</td> <td>21</td> <td>11</td> <td>35</td> <td>25.5</td> <td>:9.3</td> <td>5711</td> <td>155.0294</td> <td>619</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>3.6</td> <td>ML</td> <td>hV0</td> <td></td> <td></td> <td></td> <td></td> <td>613</td> <td></td> <td></td> <td>052</td> <td>95</td> <td>90.</td>	FV2	1 7.72	:5	21	11	35	25.5	:9.3	5711	155.0294	619						3.6	ML	hV0					613			052	95	90.
1_{12} 1_{12} 1_{2} <td>r V J</td> <td>1972</td> <td>26</td> <td>24</td> <td>:9</td> <td>:3</td> <td>5" .1</td> <td>10.4</td> <td>671</td> <td>155.3+1W</td> <td>COF</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>3.0</td> <td>ML</td> <td>FVO</td> <td></td> <td></td> <td></td> <td>ε</td> <td>613</td> <td></td> <td></td> <td>(52</td> <td>95</td> <td>53.</td>	r V J	1972	26	24	:9	:3	5" .1	10.4	671	155.3+1W	COF						3.0	ML	FVO				ε	613			(52	95	53.
AY 1 1632 32 24 12 10 17.4 14.144 15.1600 32 3.0 ML MV0 613 652 95 71. FW0 172 77 12 27 11 44.1 14.1741 155.1710 (16 3.3 ML MV0 613 652 95 53. FW0 172 77 12 27 11 44.1 15.1741 155.1710 (26 3.3 ML MV0 613 652 95 53. FW0 172 77 14 14.5 15.1741 155.1710 (26 3.3 ML MV0 613 652 95 51. FW0 172 77 14 14.5 15.1741 155.1710 (26 3.3 ML MV0 613 652 95 51. FW1 172 77 14 14.5 14.3741 156.3460 '35. 3.4 ML MV0 613 652 95 51. FW1 172 77 15.1717 14.4741 155.320.111 3.2 ML MV0 613 652 95 65. FW1 172.7 17 15.771 14.4741 155.320.121 3.2 ML MV0 613 652 95 65. FW1 172.7 15.771 14.4741 14.4441 155.320.121 3.2 ML MV0 613 652 95 65. FW1	110	1 + 72	35	25	JD	19	57.c	19.3	794	155.4414	109						3.2	ML	FV0				E	613			052	95	47.
n y 1 172 17 12 12 14 14 15 11	LVh	1 4 7 2	35	23	12	1	17.4	19.0	4412	155.1868	.32						3.0	ML	HVO					613			252	95	71.
F V0 1 72 77 12 77 12 77 12 77 12 77 12 17 14 16 57 16 16 15 12 17 16 15 12 17 16 15 12 17 16 15 12 17 16 16 35 17 16 16 35 17 16 16 35 17 16 16 35 16 16 35 17 16 17 16 16 35 17 16 17 16 17 16 17 16 17 16 17 17 12 17 12 17 16 17 16 17 16 17 16 16 17 16 17 17 16 17 17 17 16 17	- × -	17.74	.7	.3	:2	35	2	1	374	155.114	155						3.0	ML	FV0					613			052	95	1:0.
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	-15	1 72	17	14	. 9	1.0	57.5	19.1	1 8 31	155.3214	236 .						4 . 4	ML	F VO					613			(52	95	76.
r_{43} r_{42} r_{72} r_{71} r_{72} r_{72} r_{73} r_{74} r_{74		: 1.7 :	:7	14	11.	5.	31.7	1	N	154.0004	:4 ?						3.3	ML	HVO					613			052	94	126.
$r_{V_{1}}$ $1_{V_{2}}$ $(r_{1}$ r_{2} $(r_{1}$ r_{2} $(r_{1}$ r_{2} $(r_{1}$ r_{2} $(r_{1}$ $(r_{2}$ $(r_{1}$ $(r_{2}$ $(r_$	- 13	: 1.7 :	.7		22	5	:3.6	:9.3	1.N	156.344%	136						3.4	ML	HVO					613			052	96	51.
ev31.72c? 1.72.11.7.31.27.771.67.771.61.723.3. ML FV06.13C.526.56.3ev31.4.27.13.5. 7.17.7.61.5.9.711.5.2.523.13.1ML FV06.13C.526.56.13ev31.4.27.11.5.7.7.61.5.9.711.5.2.521.13.1ML FV06.13C.526.56.13ev31.4.27.11.4.31.4.1.21.5.5.7.520.163.1ML FV06.13C.526.56.7ev31.4.27.11.4.1.11.5.5.7.520.163.1ML FV06.13C.526.56.7ev31.4.27.17.4.31.4.4.21.5.5.7.520.163.1ML FV06.130.526.56.7ev31.4.27.17.4.31.4.4.21.5.7.520.163.1ML FV06.130.526.56.7ev31.7.2<	EV)	: 472	r 7	17	2:	17	23.3	11 . 3	141	156.2134	(1)		·				3.2	ML	FV0					613			652	85	٤7.
$r_{V2} = 15.72$ $i7 = 15 - 3.17$ $i7 = 0.74$ $i5.3 - 9 = 13.62 (n = 15.5) (2 V = 22)3.1 = M = VO613 = 652 = 85 = 83.r_{V3} = 5.72i7 = 14 - 53 - 7 = 5.5119 + 9 + 9 + 10 = 155 - 265 = 21 = 3.2 M = VO613 = 652 = 85 = 83.r_{V3} = 172 = 27 + 12 - 12 = 13 = 37 = 13 = 14 + 129 = 155 - 265 = 21 = 3.1 M = VO613 = 652 = 85 = 83.r_{V3} = 172 = 27 + 12 = 17 = 12 = 33 = 33 = 3.1 = 14 + 129 = 155 - 265 = 21 = 3.1 M = VO613 = 652 = 85 = 83.r_{V3} = 1.72 = 27 = 27 = 23 = 23 = 33 = 3.1 = 2.74 + 125 - 24.52 = 137.3.1 M = VO613 = 652 = 95 = 67.r_{V2} = 1.72 = 27 = 27 = 27 = 123 = 23 = 2.74 + 125 - 224 = 37.3.1 M = VO613 = 613 = 652 = 95r_{V2} = 1.72 = 27 = 27 = 27 = 123 = 27.41 = 155 - 224 = 37.3.1 M = HVO613 = 652 = 95 = 57.r_{V2} = 1.72 = 27 = 27 = 27 = 123 = 129.74 + 125 - 224 = 37.3.1 M = HVO613 = 652 = 95 = 57.r_{V3} = 1.72 = 27 = 27 = 27 = 129 = 129.11 = 10.4 - 20.1159.393.110.3.2 M = HVO613 = 652 = 95 = 72.r_{V3} = 1.72 = 17 = 129 = 129.11 = 19.4 - 20.1159.393.110.3.0 M = HVOE = 613 = 652 = 95 = 72.r_{V3} = 1.72 = 27 = 15 = 13 = 31 = 1.4 + 3.53.1155 = 2.04 = 013 = 4.4 + 00094.5 (M = VO)E = 613 = 652 = 95 = 72.r_{V4} = 1.72 = 2 = 123 = 12.4 + 12.5 - 244 = 11.4 + 20.113 = 4.4 + 00094.5 (M = HVO)E = 613 = 652 = 95 = 72.r_{V4} = 1.72 = 2 = 12 = 12.4 + 12.5 - 244 = 11.4 + 20.113 = 4.4 + 14.1 = 2.2 + 2.4 + 12.5 - 24.5 = 11.4 = 1.4 + 2.4 + 12.5 - 24.5 = 11.4 = 1.4 + 2.4 + 12.5 - 24.5 = 11.4 = 1.4 + 2.4 + 12.5 - 24.5 = 11.4 = 1.4 + 2.4 + 12.5 - 24.5 = 11.4 = 1.4 + 2.4 + 12.5 - 24.5 = 11.4 = 1.4 + 2.4 + 12.5$	r ¥ .	1) 12	27	17	22	11	17,3	1c	174	155.2164	513						3.3	ML	F 40					613			\$52	15	19.
v_{12} $1-7_{12}$ v_{13} $1-7_{14}$ v_{13} v_{14} v	111	19.12	17	15	21	17	17.0	15.9	314	155.3314	011						3.1	ML	rv0					613			652	85	£3.
$4 \cdot y_1 = 1 \cdot y_1$ $17 \cdot y_1 = 1 \cdot y_1 +	-43	14.72	. 7	13	. 5	23	39	13.2	SeN	155.310%	:21						3.0	ML	HYO					613	-		652	85	•0.
h = 3 1 = 12 C7 14 = 3 14 = 14 < 14 < 14 < 14 < 14 < 14 < 14 <	-VV	: - 7_	:7	1.6	: 7	. 7	55.1	19.9	14 N	155.232%	J1 E						3.2	۳L	FV0					613			052	85	65.
n_{13} $1+12$ 27 21 17 3_{12} 165 126 31 3.1 11 $14V0$ E 613 052 95 67 -472 17 25 25 35 5 27 1155 172 17 12 123 25 25 35 21 27 1155 123 124 1155 1155 1164 1164 1165 1164 <td< td=""><td>1 3</td><td>1 = 72</td><td>\$ 7</td><td>11</td><td>· •</td><td>14</td><td>11 .:</td><td>11 .1</td><td>121</td><td>155.3158</td><td>C C P</td><td></td><td></td><td></td><td></td><td></td><td>3.1</td><td>ML</td><td>F VO</td><td></td><td></td><td></td><td></td><td>613</td><td></td><td></td><td>(52</td><td>15</td><td>1 5.</td></td<>	1 3	1 = 72	\$ 7	11	· •	14	11 .:	11 .1	121	155.3158	C C P						3.1	ML	F VO					613			(52	15	1 5.
4, 1, 4, 7, 2, 7, 2, 2, 3, 3, 2, 3, 3, 3, 2, 1, 3, 4, 1, 5, 5, 30, 1, 30, 10, 10, 10, 10, 10, 10, 10, 10, 10, 1	11)	: 412	:"	43	17	34	: . 5	17.4	524	155.245%	231						3.1	ML	FVO		2		ε	613			C52	95	67.
$+\sqrt{0}$ $, 72$ 17 124 73.6 $21.7.4$ $156.4.6.4$ $156.4.6.4$ 37 3.1 HL $HV0$ 613 613 66.6 69.7 $+V3$ 1672 27 37 74 16.4 $19.4.64$ $156.4.64$ 233 3.6 RL $HV0$ 613 652 95 $53.$ $+V3$ 19.72 27 29 17.1 19.4420 $155.4.644$ 233 3.6 RL $HV0$ 613 052 95 $74.$ $+V3$ 1472 12 29 17.1 19.4420 $155.4.644$ 106.4 3.0 HL $HV0$ 613 052 95 $72.$ $+V3$ 1472 19 29.17 $11.9.4420$ $155.4.644$ 106.4 3.0 HL $HV0$ 613 052 95 $72.$ $+V3$ 1472 29 17.1 $14.3.56.164$ $106.414.40409$ $4.6.604$ 4.1 HL 40.613 052 95 $72.$ $+1.412$ $19.32.414$ $19.4440.4155.1644.110.094.1HLHV061305265.62.+1.41219.32.316.6.21.9.144.1155.71.44.1155.71.44.1155.71.44.1155.71.44.1155.71.44.1155.71.44.1155.71.44.1155.71.44.1155.71.44.1155.71.44.1155.71.44.1155.71.45.114.1165.71.44.1155.71.44.1155.71.45.114.1165.71.44.1155.71.45.114.1165.71.44.1155.71.45.114.1165.71.44.1155.71.45.114.1165.71.44.1155.71.45.114.114.1165.71.44.1155.71.45.114.114.1165.71.44.1155.71.45.114.114.1165.71.44.1155.71.45.114.114.1165.71.44.1155.71.45.114.114.1165.71.44.1155.71.45.114.11$	- 7 .	1 7.	. 7	25	25	33	33.5	: 1. 7	446	155.1300	-3P						3.0	ML	HVO					613			366	35	۶7.
FY3 $1,72$ $C7$ $3C$ 71 42 $193,1241$ $185,163,110$ $3.C$ RL $FV0$ 613 052 95 $15,$ FV3 1772 $2e$ 25 17 49 $164,1231$ $155,4669,231$ 119 $3.c$ RL $FV0$ E 613 052 95 $74.$ $4V3$ 1472 $1e$ 25 $10,3420$ $155,4669,231$ 119 $3.c$ RL $FV0$ E 613 052 95 $74.$ $4V3$ 1472 12 25 $113,31$ $13,440$ $155,5662,374$ 316 $3.c$ RL $FV0$ E 613 052 95 $72.$ $14,2$ 1472 $135,313$ $13,440$ $155,762,104$ $(11,340)$ 4.5000 4.5000 E 613 052 95 $72.$ $14,2$ 1472 $135,313$ $134,470,155,1134$ $155,2104,013$ 4.44000 4.5000 4.5000 E 613 052 $85.$ $72.$ $14,2$ $1472,233,311,16,213,3400,155,1134,030154,300,1143.1MLFV061305285.66.14,2147,230,123,114,14,370,114,155,174,0103.1MLFV061305285.66.14,21,142,172,17,114,15,170,110,150,174,110,157,170,110$	440	. 172	.1	29	:7	21	23.5	2 : . 2	7 . 3	155 521	.37					•	3.1	ML	HVO					613			CPS	05	89.
F $\sqrt{3}$ 1 $\sqrt{72}$ 2 $\frac{3}{2}$ 3 $\frac{1}{3}$ 1 $\frac{6}{2}$ <td>EV 3</td> <td>: 772</td> <td>67</td> <td>30</td> <td>11</td> <td>4 :</td> <td>59.9</td> <td>19.3</td> <td>2611</td> <td>155.1(36</td> <td>:10</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>3.0</td> <td>5L</td> <td>FV0</td> <td></td> <td></td> <td></td> <td></td> <td>613</td> <td></td> <td></td> <td>052</td> <td>95</td> <td>15.</td>	EV 3	: 772	67	30	11	4 :	59.9	19.3	2611	155.1(36	:10						3.0	5L	FV0					613			052	95	15.
4 V31 $3/2$ 1 $6/2$ 2 $5/2$ 2 18 2 7.1 1 $9/4$ $19/4$ $3.93/4$ 3.2 H/VO 613 052 95 $74.$ 4 V3 1472 $C1$ 27 15 13.1 31.6 $19/4$ 155.6964 309 3.0 ML HVO E 613 052 95 $72.$ 1772 27 5 11 31.2 $16/4.187$ $155.7.644$ $C10$ $4.40M3$ $4.5CML$ HVO E 613 $C52$ 95 $72.$ $1/2$ $19/72$ 37 15 11.31 23.44 $19.344M$ $155.7.644$ $C10$ $4.40M3$ $4.5CML$ HVO E 613 $C52$ 95 $72.$ $1/2$ $19/72$ 37 15 13.41 $15.3214H$ $14.55.7.644$ 010 $4.40M3$ $4.5CML$ HVO 613 $C52$ 95 $72.$ $1/2$ $19/72$ 19 15 $15.214H$ $155.7.644$ 014 $3.1ML$ HVO 613 052 85 $65.$ $1/2$ $19/72$ 19 $15.3714H$ $155.7.714H$ 015 $3.70M0$ $4.6ML$ HVO 613 052 85 $61.$ $10/2$ 13.7 $14.952.7714H$ $155.7714H$ $15.7714H$ $3.70M0$ $4.6ML$ HVO 613 052 85 $61.$ 11.17 17.4 37 $13.6414H$ $155.7714H$ $15.7714H$ $3.70M0$ $4.6ML$ HVO 613 052	+ 13	1071	29	33	17	43	16.4	19.1	12 M	155.4654	:33						3.0	HL.	1 10				ε	613			(52	95	53.
$4\sqrt{3}$ 1472 27 17 11 $15\sqrt{4}$ $19\sqrt{4}\sqrt{4}$ $155\sqrt{6}\sqrt{6}\sqrt{5}\sqrt{6}$ $3\sqrt{6}$ $3\sqrt{6}$ $4\sqrt{6}$ $3\sqrt{6}$ $4\sqrt{6}$ $16\sqrt{6}$ 295 20 $1\sqrt{3}$ 1972 27 15 11 $31\sqrt{6}\sqrt{6}\sqrt{6}\sqrt{10}$ $15\sqrt{6}\sqrt{6}\sqrt{10}\sqrt{6}\sqrt{10}$ $5\sqrt{6}\sqrt{10}\sqrt{6}\sqrt{10}\sqrt{6}\sqrt{10}$ $6\sqrt{10}\sqrt{6}\sqrt{10}\sqrt{6}\sqrt{10}\sqrt{6}\sqrt{10}\sqrt{10}\sqrt{10}$ $1\sqrt{3}$ $19\sqrt{2}\sqrt{10}\sqrt{10}\sqrt{10}\sqrt{10}\sqrt{10}\sqrt{10}\sqrt{10}10$	453	1 2 22	.c.	25	.2	15	27.1	19.3	4 2 N	155.3934	110						3.2	ML	FV0					613			052	95	74.
V_3 1472 C_7 C_5 C_1 S_1 S_1 S_1 S_2 C_7 S_2 <t< td=""><td>4 V -3</td><td>1 + 72</td><td>21</td><td>33</td><td>17</td><td>1:</td><td>13.9</td><td>17.4</td><td>-4 N</td><td>155.6968</td><td>20.4</td><td></td><td></td><td></td><td></td><td></td><td>3.0</td><td>ML</td><td>HA0</td><td></td><td></td><td></td><td>٤</td><td>613</td><td></td><td></td><td>052</td><td>95</td><td>20.</td></t<>	4 V -3	1 + 72	21	33	17	1:	13.9	17.4	-4 N	155.6968	20.4						3.0	ML	HA0				٤	613			052	95	20.
$ \begin{array}{c} \begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 $	ナイノ	1 9 72	24	:5	:1	3:	33.6	19.2	1.2.11	155.7.68	210						. 5.1	ML	F VO				ε	613	3		52	95	72.
$1/2$ $14/72$ 14^3 15^3 16^3 $16^$	🕒 EPL	1 4:15	39	15	11	51	23.41	19.3	33N	155.2104	c13	.4	• 4 0 M B				4.5	CML	F VO					613 F		C 23	C52	55	73.
-7.2 19.72 39 36 13 12 14 165 124 114 165 124 114 165 124 114 165 124 114	11-	172	19	15	23	+1	2	19.3	4 4 11	155.1134	034						• 4 • 1	ML	FV0				£	613			C52	55	62.
e_{12} 1.472 1.472 $1.4 + 1.2$ $1.4 + 1.5 + 1.4 + 1.6$ $1.4 + 1.5 + 1.7 + 1.6$ $1.4 + 1.5 + 1.7 + 1.6$ $1.4 + 1.5 + 1.7 + 1.6$ $1.4 + 1.5 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1.7 + 1.6$ $1.4 + 1.7 + 1.6 + 1$	- 4 C	1 7.72	36	15	. 3	52	:3.9	1	- 4 V	152.1354	114						3.1	ML	HVO					613			052	85	22.
• 1 1	- + C	: • • •	54	10	. 4	12	11.1	11	- N	155.7174	(13					÷	3.4	ML	FVO					613			052	25	e6.
a_{15} 13_{17} 14_{5} 17_{17} 14_{5} 17_{17} 31_{5} 3.1 ML FV0 613 052 15 27_{17} 17_{17} a_{17} 13_{17} 14_{17}	• 1 i L		C	-	- 4	+1				115.1176	C1 C	5	.7:XG				4.0	CPL	FVO		•			613 F		663	152	55	11.
FV. $13/2$ 24 37 4 37 155 340 11 3.0 ML 100 613 052 85 91 473 $13/2$ 23 37 16 54 13.9 $19.994N$ $155.316V$ $(12$ 3.0 ML HVO 613 052 85 91 $-VG$ 1472 (277) 11 21 55.2 16.16 1052 85 91 $-VG$ 1472 (277) 122 29 3.1 $11.916N$ $155.416V$ 3.2 3.2 ML HVO 613 052 85 91 $-VG$ 1472 19 122 29 3.1 $11.916N$ $155.416V$ 112 3.6 ML HVO 613 052 85 $44.$ $-VG$ 1472 19 13 13.41 (1.1) $19.412N$ $155.468N$ 111 3.3 ML HVO E 613 052 85 $44.$ $-VG$ 1472 19 13.13 $4.102N$ $155.468N$ 111 3.3 ML HVO E 613 052 95 $44.$ $-VG$ 1472 19 13.15 $50.264.2$ $15.411N$ $155.468N$ 100 3.1 ML $4VO$ 613 052 96 $30.$ $-VG$ 1472 19 13.15 $50.264.2$ $15.411N$ $155.463N$ 000 3.0 ML $1VO$ 613 052.95 $11.$	-13	1 1.17		: 7	. 1	47	.5.0	1:	17N	145.2719	61.5						3.1	ML	F VO					613		-	:52	15	11.
475 632 2337 16554 13.69 14.944 155.3169 122 3.6 ML HVO 613 052 85 $91.$ -906 14.72 (277) $12.695.2$ 14.463 155.4159 (233) 3.2 ML HVO 613 052 85 $79.$ $+906$ 14.72 (277) 12.29 37.5 14.452 3.6 ML HVO 613 052 85 $79.$ -973 14.72 12.74 35.6 13.11 $14.612N$ $155.464N$ 212 3.6 ML HVO 613 052 85 $44.$ -973 14.72 19 $13.34.1$ 11.11 $19.412N$ $155.434N$ 311 3.6 ML HVO 613 052.95 $44.$ -973 14.72 16.2 $15.411N$ $155.447N$ 314 3.6 ML 470 613 052.95 $47.$ 91.472 13.41 $15.412N$ $155.447N$	FV.	:)./2	- 1	37	. Ŧ	37	10.5	15.3	1.91	155.3.6%	211						3.0	ML	HVO	•				613			052	85	-2-
-VG 1472 C9 C7 11 24 55.2 14.472 C3 3.2 ML HVO 613 052 55 79. +VG 1472 C9 C9 <td< td=""><td>-12</td><td>- 25</td><td>5.3</td><td>37</td><td>. E</td><td>.54</td><td>13.0</td><td>1</td><td>4 + N</td><td>155.3169</td><td>112</td><td></td><td></td><td></td><td></td><td></td><td>3.0</td><td>ML</td><td>HVO</td><td></td><td></td><td></td><td></td><td>613</td><td></td><td></td><td>652</td><td>85</td><td>91.</td></td<>	-12	- 25	5.3	37	. E	.54	13.0	1	4 + N	155.3169	112						3.0	ML	HVO					613			652	85	91.
FV0 1772 C4 C9 22 53 C4 C12 3+0 ML FV0 613 C52 F5 F2 HV3 1472 C4 17 17 17 17 12 24 32 44 613 C52 F5 F4 HV3 1472 C4 13 17 11 155 F6 610 C52 95 F4 HV3 1472 C4 13 13 10 14 3+0 ML HV0 E 613 C52 95 44+ HV3 1472 C4 12 16 5+45.4 211 3+0 ML HV0 E 613 C52 95 47+ HV3 1472 C4 12 16	- 43	1 - 33	()	: 7	:1	21	35.2	11.1	FAN	155.415%	C33	· ·					3.2	ML	HVO					613			052	25	19.
-773 1 + 72 1 + 1 + 22 47 52.49 14.1F1N 155.546 010 3.3 ML FV0 E 613 C52 95 44. -740 1972 19 15 13 12.41 19.412N 155.442KN 011 3.0 ML HV0 E 613 C52 95 44. -740 1972 03 16 12.51 19.74N 156.415W CCF 3.1 ML HV0 613 052 96 30. -740 1972 13 16 50 26.42 19.411N 155.442N CC9 3.4 ML FV0 E 613 C52 95 47. 1470 1972 13 16 50 26.42 19.441N 155.442N CC9 3.4 ML FV0 613 052 95 47. 1472 13 16 15 15.42N 155.43N 00.9 3.6 ML FV0 613 052 95 11. 4V0 1972 13 16 15 15<.367A	- 10	1 - 72	C.3	: 9	22	39	3.1	11.9	16N	155 - 184W	112						3.0	ML	FVO					613			652	2.5	
-7.0 1.472 39 15 15 16 12.11 14.412.N 155.455.857.8 11 3.0 ML MV0 E 613 052.95 47. r 0 1472 0.7 16 2.0 15.46 19.774.N 156.471.9V CF 3.1 ML HV0 613 052.96 30. r 0 1972 19 13 15.50 26.42 15.447.9V CCP 3.4 ML HV0 E 613 052.95 47. r 0 1972 33 2.6 16 16.26.3 19.495.N 155.447.9V 20.9 3.6 ML HV0 E 613 052.95 47. r 0 1972 13 16 16.52.357.4 15.9 3.2 ML HV0 613 086.05 P4. r 1972 13 16 52.367.4 15.9 3.2 ML HV0 613 086.05 P4.	-43	1 - 12	- 1	11	25	4?	36 . 4	19.1	FIN	155.5-64	110						3.3	ML	FVO				E	615			652	95	44.
F 0 1477 04 16 20 05 146 1474 156 000 541 M L FV0 613 052 96 304 540 1772 19 13 16 36 2642 194411 155 4403 009 344 ML EV0 613 052 95 474 4V3 1973 33 26 16 16 2643 19445N 155 430 009 340 ML EV0 613 052 95 114 4V3 1972 13 16 35 21 2749 23 346N 155 3677 37P 342 ML EV0 613 086 05 844	- 19	1 4 72	19	13	:3	4 -	1.1		121	155.43EN	211						3.0	ML	HVU				Ł	613			152	35	4/.
FAG 1972 19 10 10 10 10	r J	1 4 12		10	21	1.5	1.0	14.1	4 14	156.115W	200						3.1	mL.	1.40					613			052	76	30.
IV0 IV0 <td>- 10</td> <td>1972</td> <td>14</td> <td>14</td> <td>11</td> <td>20</td> <td>20.2</td> <td>17.4</td> <td></td> <td>170.44.9</td> <td>240</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>3.4</td> <td>CL.</td> <td>F VO</td> <td></td> <td></td> <td></td> <td>c</td> <td>(13</td> <td></td> <td></td> <td>052</td> <td>95</td> <td>*/*</td>	- 10	1972	14	14	11	20	20.2	17.4		170.44.9	240						3.4	CL.	F VO				c	(13			052	95	*/*
TWO 1772 17 JE WE CE 214T 23495518 175 STR 175 STR 180 512 HE NU BIS USB 5 644	143	1972	11	25	- 6	10	27.0	1	· · · N	155 1436	100						3.0	ML	HVO					613			092	95	11.
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	• V I	DICATES	A	FOS	SIB	LE	DUPLIC	ATE															
	FV0	1972	10	27	64	37	24.0	19.35"N	155.113W	603				3.1 HL	FV0			613			052	95	82.
	ty3	1972	11	62	17	25	32.6	19.562N	156.4654	C12	,			3.3 ML	F VO			613			C52	96	65.
	-VJ	1972	11	04	11	52	51.7	19.732N	156.1034	041				3.9 HL	F VO			613			652	96	35.
	1 HYJ	1972	11	17	:9	28	34.2	19.345%	155.1214	009				3.1				613			052	55	81.
	2 . 10	1902	11	17	19	29	34.0	19.318.4	155.118W	830				3.8	•			613			052	95	81.
	FV3	1 972	11	11	(5	53	35.0	19.205N	155.6098	((?)				3.2 ML	HV0		ε	613			052	95	41.
	FV0	15.72	11	19	17	47	31 . 2	16.192N	155.7:14	100				3.1 ML	FV0 .		ε	613			(52	95	36.
	TVD	1912	11	17	17	19	53.2	19.281N	155.025W	C41				3.7 ML	FV0			613			052	95	92.
	HVJ	1972	11	12	18	15	22.0	19.398N	155.676%	613			, alt	3.1 ML	HVO		ε	613			052	95	52.
	440	16.72	11	2)	:9	24	51.3	17.4434	155.3934	01 3				3.2 ML	HVO		ε	613			052	95	51.
	FVJ	19.72	13	: :1	13	51	11 .1	20.023N	155.5158	100				3.C HL	F YO			613			GBP	05	69.
	+ 10	1972	1:	34	14	55	11.5	19.155N	155.275W	034				3.2 ML	I VO		ε	613			(52	95	65.
	113	1972	12	. 37	1)	25	25.5	10.4451	155.4628	639				3.0 ML	HV0		E	613			052	95	44.
	+10	1 5.72	13	16	4	34	51.3	19.1990	155.613%	6)9				3.1 ML	HVO .		ε	613			052	95	41.
	+,15.	19.72	1 3	11	:2	2?	36 . :	19.7214	154.0694	:52				3.0 ML	H VO			613			052	94	100.
	+ 13	1972	14	2:	17	32	59.1	19.1711	155.7:16	669				3.3 ML	FVO		3	613			(52	95	21.
	~ 1 3	1 9 7 2	12	21	21	15	47.5	26.179N	155.0192	250				3.1 ML	F VO			613			CFE	[5	72.
	-43	1 - 72	12	21	22	+ 2	13.5	17.475N	115.052W	013				3.2 ML	HVO			613			652	55	7.
	r V 3	7-	:2	21	.2	14	51.6	13.4 11	155.9664	637 .				. 5.2 ML	FVO			613			352	95	17.
	rV0	: +7:	12	23	. ?	11	F0.4	19.575N	1-6.116*	(5)		1		3.2 ML	FVO			613		-	652	96	22.
	E E A L	1 37_	13	5 3 3	• *	. 4	1	19.517N	:	:45 .	• • • • (!!!	3		• 4.9CML	FVO			613	F	(4(652	95	17.
4	ERL	: 172	1.	5 33		4 1	15.11	19 7N	156. 359	\$ 45 .				• 4.50ML	FVO			£13		008	052	96	1 /.
	783	1972	1.	24	1.	43	-5.9	19.5-11	1:5.674	039 .				. 4.7 ML	HVO		÷ .	613			052	55	17.
	-10	1 3 72	12	25	22	- 4	12.3	19.5.3N	145.971 4	33 9				3.4 ML	F VC			613			652	95	18.
	- 10	1 4.73	03	2	2	3.	11-1	19.11.24	155.5742	100				3.6 ML	F AO		£	613			(52	55	45.
	- Y .	1 7.75	v i	1 33	.6	11	12.5	19.2.34	156.0164	235			*	3.1 ML	+ VO			613			(52	96	40.
	74.	1 4 75	3	4	. 5	22	42	2. • 3 · · N	155 .: 212	030				3.1 ML	FVO			613			JEE	05	103.
	- 1 -	1 . 12	6.1	31	1.	31	3	17.6-EN	156414	:45				5.3 ML	HVO		-	£13			052	56	26.
	+1.5	1 2 7 *	. 1	1 13	11	3.		14.3190	15575000	(("				3.7 ML	HV0		E	613			052	95	18.
	-10	175	33	14	.16	11	42.7	13. 32.34	155.563W	50.9				3-1 ML	EVO .			613			652	95	67.
	177	1 7.13	-	1 1 4	. 0	43	15.9	19.787N	155.554	009				3.2 ML	PVG		-	613			652	55	67.
	- V -	1 - 75	2	1 1 9	· a	4 2	-6.5	19.3701	155.4146	130				3.5 ML	HVO		٤	613			052	95	-0.
	r v 3	1 9.73	¢ i	1 22	:3	11	-3-3	14.425N	155.62EW	c1.0				3.1 ML	FVD	e	E	515			052	55	58.
	r ¥ 3	1 - 73	-	1 22	11	57	44.5	19.5278	155.6262	C1C				3.3 ML	FVD		5	613			(52	95	58.
	r 4 u	1971	-	24	14	55	10.5	19.1741	155.690W	951				3.1 ML	FVO		E	613			152	32	58.
	n (-	1975	-	2 11	2.	2.7	44.5	23.244	155.2434	034.				3.5 ML	HVO			613			UE E	15	22.
	- V 3	1775	ε.	12	11	. 23	33.5	14.44.54	1:5 . 1/2 .	0.14				3+0 ML	FVC		-	613			652	93	12.
	+ *	1 7 7 5			• •	1 3	****	19.11.141	1					J.L ML	FVU		L	613			102	93	49.
	r4)	1 2 75		12	14	45		14.525 V	1-5.3424	321				3.4 ML	1 40			613			152	70	
	14.	1-75	4.	11	-1	21	5 ?	21.12.244	115.9523	1.6.				3.3 ML	FVJ			613			162	10	90.
	- 4 -	- 13	3	2 1 '	1.	4.3	41.4	1.0.5144	150.5.38	1.1 1				3.9 ML	HVU		·	013			332	73	10.
	FVU	1 - 13	-	: : 9	15	11	1 = • 4	17.3211	155.1289	513				3.0 ML	FV0		-	613			052	95	16.
	F V 3	19.15	-	14	LC	25	11.7	19.637N	155.7914	C11				3.1 ML	FVD		E	613			152	95	21.
	443	1 - 75	-	22	22	10	1	19.5574	120.4154	111				3.4 PL	r vu			613			102	70	57.
	110	17.15	1:	: 23	-1	41	52.2	14 • 256 N	125.2550	126.				• 4.0 ML	100			613			652	35	26.
	44.3	75	1.	25	13	44	.7.5	20.0 .31	155.3.51	119				3.5 ML	FVO			613			000	05	14.
	F V)	1513	0	2 24	- 2	34	22.2	2(.17cN	156.065W	(20				3.4 ML	FVO		-	613			VEE	66	e1.
	r v)	1 - 73		ir	11	4.7	45.3	19.4/11	1-5.45.00	CIC				• 4.C ML	FVO		E	613			152	95	45.
	- V 3	1 973	3	5 ??	-6	51	45.7	14.31"N	155.221W	610				3.4 ML	F VO		E	613			052	95	71.
	-43	: 3.73	2.	5 07	17	. 52	45.6	13-64	155.224	010				3.2 ML	1140		E	613			052	32	11.
	11511	- / .										PALIF											

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Saure	F YELD	Ma	0.4	L.P.	M M	SEC		LCNG	DEETH		PAGNI	TUDES				INT	FFENOM	RN	CE	Q/S	MAR	CG	DIST
20141	C ILMA		0.4		4.4	CLU		Leno	(KM)	BODY	SURF	OTHER	LOO	CAL	•	MAX	DISVNO						(KM)
**¥ 13	DICATES		ens	SIB	IF I	DIPLIC	ATE							-									
FV.	1471	63	OF	17	54	6.11	19-355N	155.1098	611				3.1	ML	HVO		ε	613			052	95	82.
F.V.	1 1971		T1	13	13	15.1	19-5171	156.3524	613				3.0	ML	FV0			613			[52	96	50.
	1 1 2 73	18	1 4	17	14	56 3	20 1 :41	155.6290	025				3.1	ML	+ VO			613				15	76.
	1673	0.3	1.	10	23		16 1654	156.5019	011				3.0	ML	HVO			613			052	95	12.
	1 1073	0.3	15	14	51	44.9	19 37N	155.5214	046				3.3	ML	HVO			613			052	95	39.
	1273	23	15	22	14	:7.1	19. CALN	156.2664	(61				3.1	ML	HVO			613			052	96	62.
	1 1 1 7 3	67	22	14	19	ci . 2	19.4:40	166.4160	001				3.0	MI	FVO .		E	613			(52	95	49.
	1 1 2 2 2	- 2	22	10	5.	45.5	19.75 M	156.7560	012				3.5	MI	FVO		Ē	613			C52	95	34.
	1 1201	10	20	16	13	FT .5	14.3191	155.7960	610				3.1	ML	HVO		Ē	613			052	95	19.
	1 1573	54	10	11	12	47.1	13. 3CH M	155.4761	C11				3.0	ML	FV0		-	613			052	95	51.
	1971	r 4	15		59	31.9	19.331N	155.1234	P 11				4.3	ML	FV0			613			052	95	81.
	1973	0.4	1.4	14	20	57.5	19.1411	155.1664	CCF				3.0	ML	FVO		•	613			C52	95	13.
- 4	1971	04	1 4	13	41	44.5	19.1931	156.1644	666				3.5	ML	h VO			613			052	96	.2.
- 4	1973	14	• 6	12	51	15.9	1= .7355	155 . 13RV	.068				3.1	ML	HVO			613			052	95	79.
	1 -: 73	.4	• ,	.7	.7	61.76	10.9.7N	154.6679	03.20	4.20MB			4.71	ML	FV0			613	F	219	252	54	139.
- 4		1			16	23.1	- 9 . 1 C4N	155.6164	612				3.9	ML	F VO			613			152	95	52-
: 2	1 - 73	34	24	16	1.	21.44	4.=174	155.7330	847 .				4.20	ML	t VO			613	F	C16	(52	95	53.
	1975	14	2		4.4	47.5	19.7.7N	155.171.	: 36				3.2	ML	FVD			613			652	95	79.
- 7	7'		26	24	51	17.7	13.3421	155	.56				3.1	ML	HVO			613			052	95	96.
- 1) : - 7!	-		17	2-	1:.3	19.413N	155.14AW	037				3.4	ML	FV0			613			052	95	52.
r ¥	1	:4	24	: 7	4.0	15.3	10.471N	155	[31				3.1	ML	F VO			613			(52	95	112.
5.3	1 2 7 3	14	26	2.1	26	24.31	19.7334	155.1009	.55.	.6. UPMR	6.1MS6	. 30FAS .	6.20	ML	4 VO	VIII		613	С	243	\$52	95	\$7.
11	: =.75	14	26	25	53	32.5	19.544N	155.6714	613				4.0	ML	FV0			613			552	95	61.
- 7	1 : 7:75	64	4 3	12	:1	56.5	19.73*.8	155.1238	542				3.4	ML	HV0			613			052	95	95 .
+ 4	1 1 7.75	: •	28	13	15	45.7	19.015N	155. CELW	(36				3.2	ML	F VO			613			¢52	95	163.
÷ v	1 - 73	:4	14	22	5:	11 . :	19.931N	155.1544	(15				3.0	ML	F VO			613			652	95	92.
- V	19.75	64	3:	14	26	56.2	26.0064	155.2484	607				3.0	ML	F VO			613			335	C 5	96.
- V	1 1.75	35	21	:5	14	97.6	12.2371	155.1154	643				3.1	PL	HVO		-	613			052	95	96.
~ V	6 12.73	JĴ	: 5	.4	5.	2:.7	19.3971	155.2364	001				3.2	ML	r vo		E	613			652	95	68.
- 1	: 1975	: 5	: 5	1:	11	3: • €	1=.5[4M	155.2454	(()				3.0	ML	FVO			613			652	95	07.
: 1	2 19.75	25	::	1.	11	24.2	19.9:24	155.2750	643				3.1	ML	FVO			613			(52	95	>1.
-1	175	15	15	13	11	14.5	14.3734	155.234%	000				3.4	ML	HV0		2	613			052	75	50.
-1 -1	0 15:15		15	4 -	41	22.1	19.374N	155.2344	610				3.2	HL.	HV0		5	613			052	75	56.
F 4	0 1972			11	21	43.9	19.3703	100.236W					3.3	MI	E VO		L	613			(52	95	66
F V	1 1772	10		-1		5 7	10 1.LN	155 3414					3.0	MI	F V0			413			050	95	65
17	1 1 7 7 3	100		14	3.	22	10 0	155 1100	17				3.7	141	HVO		-	613			1.5.2	95	97.
		• 2			1.2	4.7	19.1411	1-5.7770					3.1	MI	EV0			613			052	95	65.
			. 4		. 7	1	16.9190	115.1454	144				3.3	ML	F VO			613			652	29	-2.
	- 7 4		. 7	: 7		17.1	15.3134	155.1614	24.1				3.4	ML	t VO			613			052	95	90.
1 V	15 15	14	36		54	15 . 5	19 174	155.2254	212				3.2	ML	HVO			613			ũ52	95	60.
n V	1 15.73	.5	17		32	10.1	19.6754	155.1:14	036				3.1	ML	HVO			613			052	95	94.
- V	0 1:75	15	11	17	4.	17.5	19.176N	155.4544	636				3.1	ML	FV0			613			052	95	55.
r ¥	\$ 1975	:5	12	. 5	12	1:.9	19.903N	155.2236	C11				3.3	ML	FVO			613			(52	95	76.
- 4	2 : . 73	:=	12	13	5:	11.5	19.9543	155.276%	013				3.4	ML	E VO			613			C52	55	14.
11	5 1923	35	15	22	5:	37.5	19.447%	150.8758	(:0				3.0	ML	FV3			613			C52	95	2.
4:	3 15.45	:5	16	1 :	12	14.4	20.5544	155.5444	:34				3.0	ML	hV0			613			683	65	116.
۳V	6 1975	15	19	63	12	24.1	1= .724N	155.2(10	(39				3.2	ML	H VO			613			052	95	r 8 .
r (2 1975	55	1 4	19	11	21.9	19.3514	155.2466	(27				3.2	ML	F VO		ε	613			\$52	55	68.
r V	1975	25	27	15	22	61.4	19.456N	155.2824	\$16				3.4	ML.	t vo			613			652	95	63.
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SOURCE	YEAR	P.O	CA	+#	MN	SEC	LAT	LONG	CEFTH		MA (GN 1	TUDES-		CAL			PHENON	RN	CE	0/5	MAR	DG	DIST
TNOT	CATES		120	TEI		DUFLIC	ATE		1.41	8001	3000		VIILA	20	CAL			 						
n¥J	1 7.73	35	29	23	15	18.6	19.4291	155.480W	309					3.0	ML	HVO	÷	Ε	613			052	95	42.
d V O	19.75	25	34	20	43	23.2	19.9491	155.1878	037					3.2	ML	HVO			613			052	95	90.
FY0	1933	26	C 1	13	44	11.4	19.9:31	155.1(14	(13					3.4	ML	HVO			613			052	95	95.
HVU	1 + 23	26	12	11	15	43.7	19.2230	1 155 . C95W	600					3.0	ML	F VO			613			652	95	17.
TVU	1 9:73	GE	34	13	36	10.2	19.5161	1 155.169%	244					3.2	ML	HV0			613			052	95	77.
-43	1 9:73	50	29	20	33	22.3	19.158	1 155.5C9W	009					3.0	ML	HVO		E	613			052	95	42.
HVJ	1973	C S	(5	23	33	23.9	19.3190	155.2254	013					3.2	ML	HVO		1	613			652	95	71.
FV3	1973	io	1:	19	36	27.2	19.3631	1 155 . 321 W	C31					3.0	ML	F VO		E	613			(52	95	59.
-va :	1973	Jé	19	11	10	23.2	19.537	1 155.6998	209					3.0	ML	F VO		E	613			C52	95	21.
HVU	19.13	36	10	11	39	55.3	19.572	155.613W	613					3.0	ML	FVO		· E	613			052	95	31.
n¥ D	1973	ũ6	23	17	12	50.7	19.3411	155.116W	609					3.4	ML	HVO		E	613			C52	95	61.
FVC	19.73	:5	21	14	26	1.61	19.2851	1 155.264W	01 3					• 4 • 1	ML	HVO		ε	613			052	95	68.
- VC	19.75	Jà	22	15	44	12.7	19.5241	1 156.2354	108					3.0	ML	1 AO			613			C52	96	41.
- 7.	1 575	36	22	32	\$7	5.7	1557	1 155.5988	r44					3.2	ML	HVO			613			\$52	96	76.
440,	1 5.73	- 5	24	::	5 =	: 7.2	13.675	1 156.2421	01 3					3.0	ML	HV0			613			052	96	44.
- 12	: - 73	26	24	12	• :	25.2	:3.3721	1 155.307W	139					3.3	ML	F VO			613			C 5 2	95	82.
r V .	1 5 7 5	: 5	: -	23	21	20.00	20.1911	1 155.1629	674					3.7	ML	FVO			613			(11	16	11.
17.2	1 = 73	: 7	11	21	::	25.4	13.224	1 155.3100	010					3.2	ML	FVO			613			052	95	120
-1)	1 - 72	:7	- 1	24	- 2	51.3	14.263	155.222	013					3.6	ML	HVO			613			052	95	6 7
r V)	1975	: 7	1.4	- 3	21	27.04	11.42	115.112N	146				×.	3.6	AL	FVU			613			152	05	03.
• 1 -	1 - 72	. 1	. 4	. t	2.	2	1	1 100 - 126 4	125					3.7	ML	F VO			615			152	LE	65 .
- / /	1	1	1 -	: 4	11	4.1.6		156 4754						3.0	MI	HVO			613			052	96	48.
- 13	1 - 12	- 1			45	21.42	14.200							3 3	MI	EVG			613			OFF	65	77.
	. 7 4 2		**		4.5	14 4	10 3411	1 165 5750	117					3.6	MI	HV0			613			652	95	64.
	1 2 97	::	17		34	61.3	10.64 -	1 156.1964	- 26					3.2	MI	F VO			613			(52	56	24.
			14	:,			12.15.	1 155 4/ 64						3.6	MI	FVO			613			952	95	77.
					17	13.1	19.317	1 165 6 2	C1 C					2.5	ML	HVO			613			252	96	76.
	1 6 71	.,	7		11	51.1	19.3-70	1 1 56 . 416U	611					3.0	ML	FVO			613			:52	95	51.
		17	23		: 7	15.9	16.0061	1 155.2600						3.1	PL	FV0			613			052	15	51.
- 14	1 - 73		11		11	23.3	17.3431	1 165.2110	21.0					3.2	ML	hVO			613			052	95	73.
- Y 3	. 4.73		. 1	32	2.3	45	19.0741	155.4-64	235					3 . 1	ML	HVO			613			052	95	73.
- 40	1 475	-,	15	(I	4 .	31.4	20.015	1 155.2440	672					3.6	ML	HVO			613			CPE	06	79.
	475	1.	:1	13	1 -	4.5	19.365	1 155.4534	:35					3.6	HL	+ VO			613			\$52	95	69.
170	: = 73	32	11		45	:1.7	19.367	155.2538	21.0					3.2	ML	FVO		•	613			052	95	67.
- V 2	71		14	23	49	4 6	19.413	155.4624	.1 3					3.2	ML	HVO		Ε	613			952	55	44.
7:)	: + 13		15	22	:4	16.1	19.922	155.1504	.4 1					3.0	ML	FV0			613			052	95	68.
	: : 7 1	: +	1 -	17		15.00	2 . 214	1 175.741W	019					3.3	ML	+ VO			613			686	05	84.
-10	: > 75	3.1	27	:2		4: .:	19.203	114.5774	:4 4					3.2	ML	I VO			615			C52	94	131.
1 .	: ? 7 *	1 1	3 7	11	4 -,	53.5	17.402	1 155. 1:2%	210					3.0	ML	F VO			613			352	95	3.
r 7 3	. 9.73	33	3.	13	0	25.7	17.= 321	1 155 37%	330					3.2	ML	HVO			613			052	55	97.
-13	: 5.75	0.2	: 3	. 4	: 5	17.3	19.735	1 156 294	110					3.3	HL	FV0			613			C52	96	34.
- ¥ J	1 9 73	33	16	:4	17	45	19.11:	1 156. 164	C11					3.2	ML	F VO			613			C 52	96	42.
143	1 7 7 5	5.	14		27	11.1	19.215	155.572%	059					3.3	ML	F VO		E	613			352	95	41.
- 43	1 - 73	23	14	17	11	51.5	19.2-6	1 155.3665	- 39					3.1	KL	HVO		ε	613			052	95	50.
- ¥ -	1 3 13	23	15	23	49	17.3	19.377	1 155.266%	232					3.9	ML	FV0		E	613			052	95	65.
O 'S	: 571	:9	1.	: 9	. 7	11 . ++	17.113	1 155.21 3%	[27	3.7CMB				3.7	CML	F VO			613		(20	652	95	63.
1.1.1	1 7.73	33	1 9	12	27	21.0	14.2.1	155.5489	001					3.6	ML	F 40		E	613			C 5 2	95	46.
CVr	13.75	:+	19	: 7	22	30.0	19.046	1 155.5934	:13					3.0	ML	FV0			613			052	55	52.
-43	1 4 75) =	21	.3	57	21.7	10.243	: 155.417W	216					3.6	ML	HVG		ε	613			052	95	29.
11/(7/17										F	FAGE	19	9											

.

								1.4 1.5										
SOURCE	YEAK	C CN	AH	RHI	SEC	LAT	LONG	D [F T}	MI .GN	ITUDES			INT	FFENOM	RN	CE Q/S	MAR UG	DIST
								(KM) BODY	SURF	OTHER	LOCAL		MAX	DISANO				
*** 1:.D	ICARES	A FO	SSI	ELE	OUFLIC	ATE	5 X							-				
F A 3	1973	C9 2	9 :	4 4:	42.5	19.422N	155.412W	009			3.C ML	FVO		Ł	613	•	152 95	21.
.140	19:73	11 9	1 3	6 43	05.6	25.109N	155.917W	231			3.9 ML	HAO			615		088 05	12.
rva	1983	1: 0	2 0	6 51	12.5	20.21EN	155.41 CW				3.4 ML	HAO			613		058 05	94.
+ 1 3	1975	1: :	2 :	7 11	14.4	20.222N	155.4794	C C 7			3.2 ML	FVO		1	613		111 13	94.
-43	1973	13 3	4 :	7 53	2:.3	19.155N	155.1194	018			3.1 ML	1 10			613		652 95	11.
- V O	1 973	1) 2	8 1	? 17	42.4	19.3431	155.138%	600			3.3 ML	нур		-	613		052 95	19.
CVF.	19.75	1))	9 J	1 53	45.3	19.333N	155.2644	331 -		•	4.7 ML	HV0		ε	613		052 95	66.
FA0	19.73	1: 5	9 1	2 (1	12.2	19.332N	155.272	(32 •		•	4.3 ML	HAO		E	513		052 95	
0 35	1 9.75	1) 0	9 1	1 53	45.31	19.333N	155.2634	027 4 . 8 3M	IB .	٠.	5. CCML	HV0			613	F 048	052 95	65.
• 55	1973	1; 0	9 1	2 31	65.6H	19.333N	155.2534	227 4 . 80M	B		4.5CML	HVO	1		613	F 022	052 95	65.
e A H	1903	13 1	3 .	6 11	12.1	20.£16N	156 . 269%	013			4-3 ML	HVO			613		088 06	116.
GS	1 9.75	1: 1	5 1	6 11	12.91	26.625N	155.915W	CC2 .4.30M	18		4.4 CML	HVO			613	025	188 05	129.
- V J	19.73	13 1	4 1	1 42	28.8	13.7641	155.7974	C12			3.0 ML	FVO			613		152 95	54.
UVI.	19.75	1. 1	5 2	2 47	20.5	22.5259	156.0814	.)3.1			5.1 ML	FVO	1		515		SEE UD	e1.
-*3	1 9.73	1. 1	6 -	5 4.	4:.5	14.5.24N	155.1238	34 3			5.3 ML	HVO			613		052 95	94.
+ V.2	1 - 75	1. 1		6 53	5 1	1 i - r N	155.163%	237			3.0 ML	HVO			613		032 95	27.
+43	1973	1. 1	1 :	2 1:	41	10.1576	150.1521	C21			3./ ML	FVO		E C	613		152 95	01.
HV 3	1 9 75	1 2	1 1	4 14	31.4	19.351N	155.418%	-19			3.4 ML	FVO		£	613		252 95	-1.
-73	1 9:15	1. 2	4 :	2 32	43.3	1 N	155.4214	97.6 120			3.4 ML	HVO		F	613		652 85	60.
403	15	1 4	0 .	1 33	1.4.1		120.11			•	4.3 P.L	E VO		L	617		652 65	47
FVG		11 .	3 :	1 1	4: . !	14.3	155.4434			•	4. C ML	F VO			617		611 15	115.
F73	1	11 1	: -		F	2	165 4171	4.0		•	3.9.141	HVO			613 1	F 013	65F 35	106-
• 15			: :			10 1271	1.5.7.7.				3.3.91	EVG		· F	613		652 55	1.8.
	. 2.13	1: 2		4 23	31 7	11 . 36 M	165.2610	* 4 F			3.5 ML	E VO		L.	613		652 65	6.6.
÷ • •		11 5		7 5-	14.3	19.5.1	155. 2224	517			3.1 ML	FVO			613		(52 95	71.
- 1 3		• • • •		3 11	40.00	17.4 31	155.4431	. 3.6			3.2 ML	FVO			613		052 95	46.
- 3 ,	16:14	1: 3		1 17	13	19.4*11	155.4+34	10.9			3.1 ML	HVO		E	613		052 95	52.
- 4.)	: = 35	12 3	4	. 1.	27.6	10.0441	1:0.5534	24 .		•	3.0 ML	H-VO			£13		52 85	66.
- 5 3	1 3 15	12 1	3 .	4 2:	55.9	19.3674	155.2931	C . 4 .			4.7 ML	F VO			613		C52 95	63.
0 35	19.21	12 1	3 1	4 2=	56.11	19.357N	155.2028	031 4 . 4 0M	8	· •	4. OCML	FV0			613	F C28	052 95	£3.
n/3	1 - 73	12 1	4 1	0 45	41.1	19.515N	155.726W	30.9			3.6 ML	HVO			613		652 95	71.
4VD	1 3.73	12 1	7 3	3 :7	47.9	12.7621	:55.5514	33 9			3.4 ML	400			613		052 85	EE.
- 40	: 974	:1 :	1 .	ó 5"	\$1.7	10.4:3N	155.4424	660			3.6 ML	FVO			613		352 95	47.
nvü	147+	01 3	12 .	6 27	51.7	17.242N	1-5.4764	011			3.5 ML	ł vo		E	613		052 95	49.
0 35	19.14	5: .	1 1	0 27	51.6H	13.23 N	155.4600	21.9			3. EIML	F VO	III		613		052 95	51.
EV-	1 1 74	C1 6	5 1	5 17	15.1	19.504N	154.5279	-12			3.1 ML	HA0			613		C52 94	97.
r V 3	1974	:: :	٤.	4 : +	43.6	19.376 A	1*E.023W	515			3.4 ML	F VO			613		(52 95	71.
0 55	1974	01 3	- 1	4 34	43.51	10.3114	155.0000				3.7 (ML	F VG	111	-	613		652 95	72.
115	12.14	22 -	3	7 47	· 4	: 4 . 71!	155. 1028	211			3.2 ML	FVO		ε	613	••	052 95	1.
743	1 - 7+	21 1	2 /		34.1	19.3334	155.123%		25	•	4.7 ML	FVO		E,	613		652 95	21.
ê i S	1974	C1 1	2 1	5 :4	33.94	19.343N	155. 341	C:7 .4.90M	18	•	4 . 7 CML	F VO	111	-	613	45	652 95	50.
- 43	1 7 7 4	C1 1	3 1	- 40	27.5	19.493N	155.74:W	C1C			3. 5 ML	FVO		Ł	613		(52 95	15.
- 1)	1 - 7-	51 1	5 1	4 33	1 * • 9	17.5738	110.44114	013 ,			3.5 ML	HVU		-	613		152 95	43.
- 10	1 - 1 -	(1 1	5 2	4 60	40.5	19.115N	155.6/19	153 4		•	4.2 ML	HVU		Ł	615		052 95	46.
	- 73		£ .	1	40.51	19.78.1	155.6120				4.41ML	F VU	111	r	613		102 95	*D +
- 7.3	14.74	01 1	-	5 1-	47.4	**• 3~ JN	1.0.4524	- 14			Jeu HL	E VO		L	413		(5) 05	
115	1 3 14	11		3 20	61.0	14.03.4	100. 0%	000			3 2 ML	E VO			613		652 65	100-
	1 7 1 1			2 31	-G. 6	19.1714	15.1361	119			3.6 MI	HVO			613		052 95	79.
	1.2.11	** 4							LAGE	21								• ~ •

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SJIRCE	YEAR	мэ	DA	14	44	SEC	LAT	LGNG	DEPT	н -		MAGN	ITUDE	S			INT	FHENOM	RN	CE	0/S	MAR	DG	DIST
**N TID	CATES	A 1	os	151	E (DUFLIC	ATE		(())		8001	3011	VIII	LIN	LUCAL			0131.00						
- ¥)	1 974	31	31	14	15	34.3	19-426N	155.4228	190						3.3 ML	I VO			613			C52	95	49.
440	1 574	21	51	21	15	49.1	19.252N	156.1684	061						3.3 ML	hVO			613			052	96	38.
- 4 -	1974	22	14	13	15	54.6	19.559N	155.916W	600						4.2 ML	HVO			613			052	95	11-
E WO	1 - 74	52	6.9	19	16	15.2	19.542N	155.9208	010						3.1 ML	HVO			613			052	95	9.
2: 0	1 9 74	:2	15	-4	16	54."H	19.54CN	155.9CCW	100	. 4	.1CMB				4.3CHL	FV0	٧		613	F	25	(52	95	٤.
	1974	0.0	35	16	-1	25.0	19.1560	155.6824	676						3.1 ML	I VO		E	613			C52	95	40.
. 12	19.74	3.3	15	16	:1	27.44	19-15JN	155.6734	003						3.70ML	+VO	III		613			052	55	42.
- 40	1 3.74	32	16	0.4	39	24.5	19.597N	156.2328	325						3.4 ML	HYO			613			032	96	39.
	1974	52	C.E	14	37	25.CH	19.507N	156.000.	(3(3.5 CML	HVQ	III		613	F	23	052	96	26.
EV.	: = 7+	22	CE	21	56	39.5	19.513N	155.265W	C2 4						3.1 ML	F VO			613			(52	95	65.
	1374	32	55	11	55	39.51	19.4 901	155.2604	024					•	3.30ML	F VO	III		613			052	95	65.
CVD.	1924	22	16	13	47	16.)	19.291N	155.3104	v31						3.2 ML	HVO		ε	613			052	95	63.
rya	1974	[2	23	12	54	12.2	19.976N	155.4828	034						3.4 ML	hV0			613			052	85	69.
r V J	: 774	22	:2	:0	53	27.3	19.337N	155 . 2 2 %	013						3.C ML	FV0			613			:52	95.	73.
- ¥3	1 7.74	23	05	: :		12.3	10.474N	155 . E 7 F W	11 "						3.1 ML	+ VO		E	613			(52	95	1.
441	1 = 7+	15	:7		27	32.7	20N	:55.3464	335						3.3 ML	FVO			613			096	05	87.
IV.	1 5 74	15	; a	15	13	52.1	21.197N	115.444%	122						3.3 ML	FV0			613			098	65	83.
FJJ	: - 1-	: 5	• •	. 1	1.	3: . !	19.906N	155.1661	((e						3.2 ML	F VO			613			652	96	53.
- / 2	1 - 7 -	: 5	1 5	22	5:	34.6	19.175N	154.40 11	243						3.2 ML	F A0			613		•	(52	64	1[4.
11.	117-	15	2)	1.	10	3:.5	10.413M	155.4376	21:						3.1 ML	HV0			613			252	95	47.
- 25	1 7.7+	: 5	23	25	53	56 . 1	14.2754	155.1300	206						3.2 ML	HVO			613			C 5 2	95	75.
ê is	1 - 7-	:3	24	14	31	17.7+	19.24CN	1-5.10.4	217						3.5 CML	PAD.	111		613			652	95	75.
- 43	: 474	:3	27	22	51	54.2	11 . 752N	155.5531	639						3.6 ML	F VO			613			(52	65	67.
o 35	: + 74	35	25	:ĉ	5:	51.41	16.91.4	165.540%	142 4					•	4. [[ML	F VO	III		613			C 5 2	15	72.
1VU	1971	14	14	11	4.7	15.3	10.373V	155.2754	:27						3.5 ML	1.00		2402	613			C52	95	64.
6 33	1574	24	24	:1	42	15.50	19.5001	155.2735	r.2 ·	•					4.0CML	rv0	III		613			652	95	65.
rd:	1 7 74	: -	7.4	16	2)	:4.5	11 .1 -2N	155.3414	(15						3.C ML	F VO			613			052	85	86.
- 1 -	1 . 7.	34	64	. ł	• :	22.2	: 9.21 GA	155 . 1254	221						3.3 ML	FVO		E	613			(52	95	23.
nV:	1 7 7 +		22	22	:1	52.3	19.417N	155.4284	332						3.6 ML	F VO		E	613			C52	95	41.
- 7 3	1 9.7+	54	23	. !	44	23.7	19.14 .N	155.5944	211						3.0 ML	HVO		Ę	613			C 5 2	95	47.
-10	19.14	34	24	31	45	51.4	13.5.15N	155.2400	209						3.0 ML	FVO			613			652	95	70.
FVC	1574	6.11	25	:2	5 c	23.2	19.519N	155.2244	(1)						3.1 ML	r vo			613			052	95	/1.
🔹 🦻	1 3:74	34	25	12	24	5f . 1H	10.320N	155.22.9W	00 P					••	4. UCML	F VO	111		613			052	95	71.
111	1 9 7 4	34	37	.5	43	46 2	19.3F2N	155. 451	3:5			8			3.1 ML	нур			615			652	95	89.
	1574	24	3 -	12	.14	51.4	19.79 N	155.156%	135						3.1 ML	FVO			613			052	95	24.
35	1 7 7 .	64	3.	12	44	11.4F	19.35CN	165.1108	000						3.2(ML	FVO	111		615			152	55	12.
0 35	1 7 74	3 - +	3.	12	4 3	4:.21	19.369N	155.CECM	205						3.3CML	I VO	111		615			(52	75	25.
11-	197+	١٢.	1 :	-1	10	14.7	19.2341	155.1+2%	315						3.3 ML	100			613			652	95	10.
	: 1.1-	20	2.5	•	17	25.0	19.2001	165.2609	-14					•	4.2 ML	HVO			613	-		032	95	
😧 55	19.14	65	0.5	1.	17	23.01	19.34:1	15teletek	:13	• 4	.4 MB			•	4.51ML	FVU	111		613	r	2.4	152	.5	E/.
F ¥ 3	1974	::	: 6	2:	45	31.6	19.1.7N	154.1166	\$31	8					5.5 ML	FVU			613			152	94	112.
~ V 1	1 9 74	25	- 2	23	5	07.1	1-464N	155.5098	265					•	4.0 ML	FVO		E	613			652	95	244
EV3	19.7+	:0	19	: 4	. + 7	25.9	19.472N	155.5260	0.00						3. 2 ML	HVO		E	613			052	32	51.
- V 3	1014	د د	15	- ċ	÷.	:1.5	19.435N	155.6139	004						3.2 ML	FVO			613			052	35	28.
+43	1574	: 5	1 %	:2	40	31.1	5: . 34 34	155.4994	133						3.1 ML	FVO			615			OFF	15	127.
F V 3	: 97+	:5	15		23	19.1	22.574N	155.5124	0.7						3.4 ML	FVO			615			111	15	127.
-145	107.	15	17	:3	54	45.4	19.7431	155.7628	013						3.4 ML	PVO		E	615			052	20	55.
- ¥)	197+	35	22	. 2	35	2 . 3	23.4651	155.617	:32						3.1 ML	HVO		-	613			056	05	114.
FV3	1 - 7 -	::	23	13	11	34.5	13.342N	155.7674	C1 5						3.6 ML	HVO		E	613			052	22	10.
r ¥ J	1974	:5	23	14	17	:7.5	19.2190	155.1228	C1 C				~ 1		2+1 ML	FVU			613			1.25	77	52.
el/17/1	7.										f	AGE	21											

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SOURCE	YEAN	:40	DA	FR	4.1	SEC	LAT	LGNG	DEFTH		MAGN	ITUDE	s			 INT	FFENOM	RN	CE	0/5	MAR	DG	DIST
	CARCE								(KM)	BODT	SURF	UTP	LK	LUCAL			013140						
	LA.T.S	05	053	19	19	55 A	19.217N	155.3674	008		7			3-1 81	F VO			613			052	95	61.
140	1 7114	25	24	17		33.4	19 2261	155. 1400	304					3.7 MI	HVO			613		•	052	95	60.
nyu	1 3 74	13	29	23	10	10.0	19.2271	155. 6050	334					3.6 MI	HVO			613			668	05	77.
440	19.14	12		13	30	62	10 1701	155 6690	036					3. C ML	HV0			613			652	95	96.
	1 2 14		23	12	~ 7	*0 1	19.435 M	155 4414	CC 9				-	4.1 MI	F VO		E	613			(52	95	46.
FVJ	1574	05	13	24	12	10 11	19.42CM	155.4360	0.3.8					4.1341	HVO	TIT	-	613			052	95	46.
	1 2 174	10	10	10	14	20 1	19 295N	155 2224	107				•	5. 4 ML	HVO		E	613			652	95	72.
FVJ	1 2 73	10	17	17	50	A1 7	19.9111	155 7600	129					3.2 MI	HVO		-	613			052	95	÷1.
- W O	1 9 74	10	10		15	42.4	19.3791	155.4190	(10					A.F. ML	HV0		-	613			052	95	50.
440	1 - 72	15	19		11	13.9	19.3124	155.4350	677					3.6 ML	+ VO		· E	613		•	C52	95	46.
44.	19.74	115	19	15	22	13.7	19.164N	155.4224	0.0.9					3.6 ML	FVO		-	613			052	95	49.
44.7	19:74	16	19		17	51.6	19.174N	155.4194	109					3.1 ML	HVO		£	613			052	95	50.
	14:24	60	19	15	.5	42.4H	19.34CN	155.4108	008	.5.10MB				4.9 CML	FVO	v		613	D	58	C52	95	52.
6 35	1979	60	19	15	11	13.5+	19.35.N	155.42CW	615		•			3. E C ML	FV0	III		613			(52	95	56.
0 35	1 - 7 -	:4	1 3	15	13	33.64	17.35 W	155.4104	537	•				3.7 CML	F VO	III		613			(52	95	51.
17.1	1 - 1+	12	1.5	31		53.3	19.3754	155.4361	9)					3.1 ML	HVO		E	613			352	95	48.
- V 3	19.74	. 5	21	21	5.	24.5	19.1371	155.2124	2.29					4.3 ML	HVO			613			052	95	72.
a .s	1 2 74	51	21	1.5	5.	31 .41	19.13"N	155.214%	0.17	.4.35MB				4 . 4 CML	1-10	111		£13	F	20	652	95	12.
	1914		22	21	51	17.6	19.1.3N	155.1214	(1)					3.1 ML	1 10		E	613			(52	95	72.
- 43	1 = 74	15	2 7	12	44	43.4	: 4154	155.262%	. 22					3.0 ML	1 VO		E	613			652	95	63.
35	1 9 7+		2 8	-1	4 4	42.34	14.41 N	155.J.J.W	231					3.10ML	HVC	III		613			652	95	63.
- 45	1 = .7 +	37	10	. 2	51	3 7	10.4141	155.3 169	.17					3.2 ML	FA0			613			0.5	95	:2.
-10	1 9.74	57	C 🗧	14	42	35.0	1 712N	155.(234	[32					3.1 ML	HVO			615			052	95	
÷ 5	:74	57	15	- 3	17	17.0+	1=.47.4	155.4409	628					3.2CML	FVO	111		613			152	95	46.
CVF	1 - 7 -	27	12	15	32	59.1	14.4051	155.72P d	5.10					3.5 ML	FV0		E	EIS			052	42	16.
9 35	1 4.7+	07	13	,1	15	#4.JF	N	155.73.1	¢ 13					3.6.ML	HVO	111		613			1.52	20	10.
-	197.	:1	13	it:	37	43.6	19.56 1	155.2564	31 5					3.1 ML	FVC			613			652	95	61.
🕘 55	1 174	:7	13	16	37	46.51	19. 16 N	155.250%	201					3.4(ML	FVO	111	-	613			152	77	11
244	1 - 7 -	27	15	24	4 ?	14.5	17.4561	1:5.5-74	025					3. 4 HL	F VO		L	613			152	65	66.
-42	1 7.7+	27	13	11	22	-3.3	17.5-14	155.1576	J J 4					3.4 ML	hv0	* * *		613			(52	66	150.
25	A 7.14	11	19	14	23	44.31	18.241 1	100.2919	008					3 COMI	E VO	111		613			552	95	67.
22	1974		17	15		12.1	10.111	100 . 2 CL #	-16					3.2 MI	F VO			613			(52	95	51.
	1 7 1 4			- 13	**	12 21	17.01.20	165 5560	(1)					3.7.1	F VO	TTT		613			:52	95	67.
	1 7 14	. 7	17	12	- 4	44.34	19.4.1	155.56 1	126 -					A. OCML	HVO	TIT		613			052	95	50.
	1 . 7.	17	21	16	7	4 A	10.345N	165. 144	.30					3.4 ML	FVO		E	613			652	95	71.
49.15		.,	2.2	*	1.7	41.51	17.3520	155.0114	:31					3.9 CML	FV0	111	-	613			652	95	72.
- × .	4 74	.,	21	: 1	4	33.1	13.4271	155 . 5974	223					3.2 ML	t vo		ε	613			052	95	30.
				1	14	(1	150.4164	115					3.4 ML	+ VU			613			(52	95	63.
74.4		.1	24	Ξ,		13.2	19.1141	155 . 1=2						3. 0 ML	HVO		E	613			:52	95	64.
	- = .7 +	67	34	. 4	13	12.54	19.374N	155.2018	514					3.90ML	FV0	111		613			152	95	64.
+ 4 3	1 4 7 4	:7		.7	14	11 . 1	: 7.3.71	154.1114	:31					3.5 HL	FV0			613			152	54	112.
- 43	1 5.74	65	2.	:6	. 5	14.1	19.5.44	155.671%	:00					3.1 ML	F VO		E	613			C 5 2	95	23.
	: +1+	65	20	. 1	12	54.4	14.3754	155.3-6%						4.2 ML	HVO		ε	613			052	55	61.
25	7 .	13	16	. 6	44	36.3+	15.47 W	155.6704	355					3.4.ML	FV0	III		613			652	95	22.
21	1214	:1	: 8	: 1	1.2	57.5H	19.35.1	155.3CCW	(27 .	4.2CMB				4.3CML	F V0	III		613	F	27	052	95	62.
14.	: 17.	24	39	15	2:	15.7	19.921N	155.7114	C41					3.0 ML	FVO			613			(52	95	91.
18.3	157+	. 5	12	:1	30	23.6	19.391N	150.4441	986					3.5 ML	FVO			613			C 5 2	95	46.
0 35	19.74	. 9	12	21	26	21.54	14.57.N	155.43:4	358	9				3. E OML	HVO	111		613			652	95	49.
- 43	: + 7+	6 -	13	23	22	55.7	: 4324	155. c. o.	624					3.6 ML	FV0		ε	613			052	55	29.
111:2/1	7.									F	AGE	22											

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SUJRCE	YEAR	80	DA	MR	MN	SEC	LAT	LCLG	DEPT	+	MA GN	ITUDES-				INT	FEROM	PN CE	G/S	MAR	DG	DIST
	CATES		203	sta	F		ATE		(KM)	BODY	SURF	OTHER	LOCAL			MAX	DISANO	,				
	1 5.74	25	13	22	45	17.3	19.4311	155.6010	C.0. A				3-1 ML	- FYO			F	613		(52	95	36.
- W3	1674	0.0	14	13	27	07.2	19.465	1 155 6274	604				3-0 ML	E VO			-	613		C52	95	27.
24.5	1 3 74	16	14	21		29.4	19.297	156.3390	620				3-1 ML	EV0			(#)	613		05.2	96	51.
44.1	1 6 70	0.2	17			16.3	19.6031	155 6704	207				3.1 MI	HVO			F	613		052	95	23.
- 42	1 9 74	00		22	6.2	21.3	19 1 641	1 154 1114	(24				3.6 ML	H VO			-	613		052	96	44.
FVU	1714	24			52	20 11	16 7301	156 1700	610		· .		3.6 (MI	LVO		111		613		152	3.0	47.
	19.14		14		52	2Lelr	19.770	156 1768	604				J . CUML	FV0				613		652	66	15.
443	1 7164	56	10	14	11	23.1	19.5191	155.0724	206		\$		3.1 HL	7 40	1.00	* * *		613		052	95	12.
35	19:14	23	21	15	25	23.40	19.3331	155.75.W	006				3.3041	HV0				613		652	55	71.
	1 7.64		20	ie	10	51 01	19.3140	155.2218	CDC				3 O ML	F VO				613		652	95	72.
	1914		24	14	13	16 6	10 110	155.2218	667	~			3.7 JHL	F VO		111		613		152	95	62.
- 40	1	20	2.7	21	10	10.0	19 171	155.3109	210				5.5 HL	HVO				613		652	95	72.
	1 7:14	0.2	24	7	4.0	40 75	10 111	1 166 3120	010				- 4 - 6 GML	HVO		111		613 F	34	052	95	72.
- 33	1 3 7	1.3	20		47	11 2	19 173	1 165 . 5470	225	••••••			3.1 MI	HVO				613	34	652	95	76
	1 2 7 7 7		15	**		1. 21	19 3921	155.170	510				A 3CHI	F VO		111.		613		052	95	5.
	1 5 74	10	1.2		- 0	47 7	10	1 166 5744	126				T. T MI	+ 10			5	613		152	55	61.
F 4 - 0	1 2 74	13	17	***	3.1	37 . 14:	19.7:00	1.2.1.1.1	116			1	3.5.11	E VO		TIT	-	613		152	5.	51.
	1 7 84		-			13. 4	16.4.11	105.6370	- 10				3.5 ML	EVO				613		-5,5	95	47.
					-	25.2	19.4571	1 155.1134	613	•			3.6 ML	HVD			F	613		052	95	75.
	1 4 74	: a		3.	:;	1 . 7	25 .1 5 14	1 . 55 . 5251	621				S.I ML	FVO			-	613		CEE	15	15.
2: 0		44	5.	.6		4 1. 71	34.14.15	115.5534	147				3. 9 0ML	F VO		III		613		611	(5	15.
- V.	1 . 1 .	1-		. 1	4.	24.7	19.573	155.5184	511				3.3 ML	HVO				613		552	95	41.
- 43	1	1	19		37	55.1	1= . 17:1	155.4634	210				3. U ML	FV0				613		652	95	43.
+ 7.3	1 - 1-	1 .	11	22	LE	34.1	19.417	155.5174	(22				3.1 ML	HVO				613		C52	95	63.
r V u	1774	1)	11	17	-	41.1	11.451	1 155.4104	:35				3.C ML	F VO				613		(52	15	71.
14,	1 7 14	1 ;	15	1	3.	15.4	10.4371	1 155.4984	117				3.5 ML	FVO				613		652	95	40.
- 1 -	1 3 2 4	: 1	16	14	16	12.4	19.191	1 155.3734	.26				3.0 ML	HVO				613		C52	95	64.
- 7-5	. 174	13	1 =	14	4.2	4:.2	15.019	11.6.5711	. 23				3.2 AL	FVC		. N.		613		552	56	66.
C 25	1974	1.	1 -	: 1	31	15.31	19.42:1	1 155.49(%	133				. 4. C (ML	r VO		III		613		652	95	41.
- 14	1974	17	17	1.5	17	11.4	19.717	154.9400	603				3.3 ML	t VO				613		C52	94	163.
HVC	1 . 1.	ز 1	24	U.D	14	54.7	19.57.1	: ::5.477%	310				3.2 ML	FV0		1		613		652	95	44.
	: +7+	1)	2=	13	2:	\$7.3	19.331/	1 :55.1890	210				3.4 ML	HVO				613		052	95	74.
• 3S	1974	10	26	23	2:	17.14	19.33:1	1 165 . 191W	6:9				3.70ML	HVO		III		613		052	95	74.
+ ¥ 3	1 9 74	1.	27	:2	: 2	34.8	19.523	1 155.6638	033				3.1 ML	FVO			E	613		(52	95	24.
- 43	1 4 74	13	29	18	57	32.3	19.41.1	1 155.4224	209				3.4 ML	F VO			ε	613		(52	95	45.
0 35	2974	1.	51	. 4	57	3.º.2H	19.39"	1 1:5.41	326				3.7CML	FVO		III		613		652	95	£ C .
- 12	: 7 -	13	32	12	1.	43 . 3	17.372	1 155.5.2%	211				3.2 ML	FV0				613		652	95	41.
r V e	: 474	17	51	::	.1	41 . 1	14.3:41	1 :25.1448	::0				3.5 ML	r vo				6:3		352	°5	÷9.
r7)	1 - 74	1 :	31	1	4 ?	22.1	19.100	1 155 424	0.0				3.7 ML	1 10				613		652	95	٤5.
🔮 u S	1 7.74	13	3:	2.	11	4 ··H	19.171	155. 1402	225				• 4.UCML	F VO		III		613	•-	652	55	85.
55	1 2.74	1,	31	2.	45	22.1+	19.35	1 155 701	176				3. EGML	HVO		111		613		052	55	66.
CVF	17 +	11	\$1	- 3	42	28.4	10.234	1 145.7714	JC4				3.0 ML	h VO				613		052	95	16.
r V J	: 67-	11	29	14	46	12.7	19.340	1 155.1346	((9				3.C ML	F VO			E	613		(52	95	79.
0 35	1924	11	13	: 4	45	:5.71	19.372	1 155 . 14 34	207				3,2CML	F VO		111		613		C52	95	79.
145	1.414	11	13	-1	5.	14.7	10.415	155.425W	010				• 4.2 ML	FVO				613		C52	55	48.
0 55	1 4.74		12	11	53	4.71	10.4 1	155.4100	006				• 4.1.ML	HVO		111	-	613		352	95	50.
-VC	: 77-	11	12	15	54	14.5	19.4221	155.2054	601				3.1 ML	HVO			E	613		052	45	63.
GS GS	. 9 74	11	13	. 4		:4.11	14211	155.2100	213				3.5(ML	FVO		111		613		(52	35	63.
- 7)	1 2 1 4	11	13	22	2 -	22.05	20.2-11	155.1364	032				3.0 ML	VU				613		5 5 3	15	74.
. Y I.	1 1.64	11		1-4	1.1	01.0	T. * * 4 C];	1122.4740	02.2		105		3.3 ML	F V0				613		625	62	10.

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A-25

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INT FFENOM RN CE G/S MAR DG DIST LONG DEFTH -----MAGNITUDES-----SJURCE YEAR MO DA HR MN SEC LAT (KM) BODY SURF OTHER LOCAL MAX DTSYNO (KH) 613 052 96 613 052 95 111 613 052 95 613 052 95 111 613 052 95 111 613 F 26 052 95 E 613 050 00 ... I DICATES A FOSSIBLE DUPLICATE 5.0. NVO 1924 11 16 J5 12 39.2 19.212N 156.3644 031 3.4 ML HV0 3.6 ML HVO 3.6 CML HVO 3.6 CML HVO

 NY3
 1424
 11
 16
 J5
 254.2
 19.212N
 155.6544
 051

 NY0
 1924
 11
 16
 17
 5C
 23.6
 19.552N
 155.6564
 CCF

 0
 35
 1974
 11
 16
 12
 41.21
 19.19CN
 156.22CN
 CIF

 HV0
 1974
 11
 21
 14
 14.6
 19.357N
 155.311W
 031.*

 • 35
 1974
 11
 22
 J7
 49
 14.7H
 19.340N
 155.317W
 929 * 3.90MB

 +V0
 1974
 11
 36
 23.57
 17.435N
 155.418W
 036

 24. 47.

 III
 613 F
 26
 052 95

 IL
 HV0
 E
 613 052 95

 IL
 HV0
 E
 613 052 95

 IL
 HV0
 E
 613 052 95

 L
 HV0
 E
 613 052 95

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 613 052 95

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 E
 613 052 95

 HV0
 III
 613 052 95 5

 HV0
 IIII
 613 052 95 5

 HV0
 IIII
 613 052 95 • 4.4 ML HVO • 4.50ML HVO • 5.5 ML HVO 61. 61.

 1904
 11
 30
 03
 54
 23+7
 14+435N
 155+414M
 096
 55 ML
 FV0

 FV0
 1974
 11
 35
 C4
 (7)
 37.9
 19.485N
 155-376V
 CCF
 3.6 ML
 HV0

 HV0
 1974
 11
 35
 04
 34
 64.6
 19.425N
 155-451M
 CC6
 3.6 ML
 HV0

 HV0
 1974
 11
 35
 34
 64.9
 19.456N
 155.451M
 CC6
 3.6 ML
 HV0

 HV0
 1974
 11
 30
 44
 65.9
 19.456N
 155.423M
 039
 3.4 ML
 HV0

 HV0
 1974
 11
 30
 64
 24+1
 19.456N
 155.423M
 039
 3.0 ML
 HV0

 HV0
 1974
 11
 30
 66
 24+1
 19.456N
 155.423M
 036
 3.0 ML
 HV0

 HV0
 1974
 11
 30
 66
 24+1
 19.425N
 155.423M
 036
 3.1 ML
 HV0

 HV0
 1974
 11
 30
 . . 5.3 FML 1 VO ● 13 1-74 11 5. 15 54 23.4F 14.4179 155.4.8F F37 .5.10MP 5.5MS 3.60ML HV0 3.40ML HV0 • 35 1074 11 5. 14 97 37.78 10.473N 185.361W CLA ● 35 1474 11 SC 14 45 54.1H 19.44"N 155.34CH CCP 3.5 ML + VO EV. 1974 11 30 18 28 39.0 19.419N 165.4218 012 3.3 ML + VO - 1 1 1 1 1 5, 25 14 52.2 19.46 1 155.493W 007 3.1 ML HVO n/) .774 12 31 .3 52 54.2 19.39"N 155.443W 008 3.1 ML HVO 3.3 ML HVO HV) 1974 12 01 18 59 11.1 19.419N 155.434V 339 0.1 ML FV0 3.3 ML FV0 3.1 ML FV0 3.1 ML FV0 5.4 ML FV0 4.1 ML FV0 3.3 NL FV0 4.3 CML FV0 3.5 ML FV0 Fr. 197- 12 22 12 41 32.6 19.032N 155.515% (40 FT. 1974 12 13 14 47 41.7 19.447N 155.3978 CC9 TYT :574 12 17 12 15 44.2 17.4200 155.6278 003 473 1974 11 7 .7 33 50.5 19.424N 165.4148 313 FV1 1-1- 11 17 15 1+ 27.9 19.477N 155.447W CC? 12 18 11 20 52.5 19.7134 156.1664 129 143 1674 12 38 61 14 27.68 19.4734 155.4438 328 1 + 14 6 35 1-1- 12 39 .6 44 31.4 19.4530 155.4010 025 3.5 ML HVO rVJ -V. .474 12 14 12 39 13.5 19.366N 155.4254 010 3.2 (ML HV0 3.4 ML HV0 @ 55 1974 12 15 16 4- 31.44 19.426M 155.31CH CC7 -. J 1474 12 14 .6 42 17.1 19.437N 155.613W CC4 3.1 ML HV0 14. 1974 12 11 13 37 75.4 19.42 N 155.528W 270 3.1 HL HV0 -41 1414 12 11 .2 32 25.6 19.4754 155.6198 262 -VC 1-7+ 17 11 07 21 54+4 .4+4414 155+4178 03P 3.C ML HVO 3.ECML HVO (52 95 32. (52 95 34. 052 95 84. 052 95 84. 052 95 84. 052 95 49. 052 95 29. 052 95 30. • 75 1+74 12 11 14 34 THATE 14.45FN 185.52CH 201 3. 3CHL + VO 35 117. 12 11 13 45 54.78 19.4334 155.5602 106 3.6 ML H 40 -4, 1474 12 12 CH 11 18.2 19.365N 155..51N 018 613 613 0 15 157+ 12 12 14 -1 13.1H 19.16:N 155.110W 006 3. SUML HVO III

 3.6 ML FV0
 613

 3.7 ML FV0
 613

 3.1 ML FV0
 E

 3.1 ML FV0
 E

 3.1 ML FV0
 E

 4.7 ML FV0
 E

 613
 E

 -V) 1474 12 14 10 11,10.4 19.4138 155.4228 (C9 3.7 ML + VO -V) 197- 12 14 .5 52 24.2 19.475N 155.6.34 CC3 -/0 147- 12 15 .6 5. 08.7 19.4 12N 155.431W 010 -10 1474 12 15 14 17 10.4 19.4644 155.5578 031 652 95 29. -V. 1974 12 15 13 53 47.5 19.475N 155.601W 002 · 4. FCML FVO III
 • 4+ECML FV0
 III
 613 F
 32 C52 95

 • 4+E ML FV0
 613
 052 95

 3+1 ML HV0
 E
 613
 652 95
 0 03 157- 12 15 2: 53 47.4F 13.4534 155.593% 934 ... 30MB 31. 171 1974 12 16 23 17 23.6 13.4 7N 165.432L CO9 48.

N

47.

FAGE 24

-/1 14.7- 12 15 23 33 34.9 19.4 3N 155.4378 668

11/27/11.

SOURCE	YEAR	MO	0 A	FR	411	SEC	LA	LG	[EF]		MAGN	ITUDES-			INT	FFENOM	RN	CE	6/5	MAR DG	DIST
						in the second			(KM)	BODY	S UR F	OTHER	LOCAL		MAX	DISANO					(KM)
••A 1001	CATES	A	Pas	S 191	.E (DUFLIC	ATE										(18			062.05	4.8
FVU	1 9.74	12	16	:9		55.1	19.417N	155.429	66.9				3.8 ML	HVU		e.	613	5	61	652 55	49.
S : Q	1 9 74	12	16	:9	17	29.41	14.34CN	155.42CW	100	• 5 • COMB			• 4.9CML	FVO			613	r	01	(52 75	47.
G G S	19.24	12	16	.19	30	35.71	14.3908	155.4200	CCR				3.70ML	FVU	111		613			052 95	29.
EA -	19.74	12	16	10	23	24.0	19.425N	1:5.6074	004				3.2 HL	HVO		L	613			652 55	49.
O 65	19.14	12	16	14	23	92.04	19.4201	155.4204	009				3.9UML	FV0	111	F	613			C52 95	45.
E A D	1914	12	17	16	- 4	15.2	14.3520	155.4658	100				3.2 ML	140		-	613			152 95	64
141	19.74	12	14	22	3.	52.6	14.42.N	105.2738	116				3.1 HL			۶	613			052 95	45.
HV3	14.74	12	21	54	It	14.0	14.345N	155.9468	210				* 4+1 ML	F V 0			613			552 95	28.
87.3	1994	12	21	10	17	41.4	19.4490	105.614%	333				5.0 HL	H VO			613			052 95	47.
• 65	19.14	12		10	10		19.3654	155.4434	105				- 4-20ML	FY0		· F	613			(52 95	51.
FVU	19.14	12			45	35 1	13 3214	155 4190	009				3.0 ML	E VO		Ē	613			C52 95	51.
- 20	1 3.74	12	23		59	45.4	17.3214	155. 1120	209			•	3.1 ML	HVO		-	613			C52 95	66.
- '' '	1 3.14	1 2			17	43.3	19.3494	155.2510	031				. 4.6 ML	HVO			613			052 95	64.
EV.	1 - 7-	12		1 3	1.4	44.9	17.356N	155.0851	032	•			304 ML	FV0		E	613			052 95	64.
	1 - 74	1 .	34	. 7	47		17.4718	1	28	. 4. 50MB			. 4.70ML	F VD	111		613	F	39	C52 95	65.
	1 3.74	: 2	25		12	21.1	19.2201	155.3004	336				. 4.2 HL	FV0			613			052 95	67.
- 1.4	1.74	12	14	• .	. 7	1 6	19.2274	155.2544	30.8				3.P ML	FVO			613			052 95	67.
F 4 9	. 17-	12	20	1	24	14.5	19.2254	155.1154	3 3 3				. 4.3 ML	HVO			613			052 95	66.
r V .	: + 7.4	12	2.8	5.	÷ ÷	19.5	:9.2:7N	155.3114	135				5.4 ML	FVO			613			(52 95	66.
0 33	1 74	12	25		13	2++	1 ? 'N	155.20:0	115		•		. 4.35ML	F VO	III		613			\$52 95	£t.
35	1 4 7 4	12	2 4	. 4	17	11.2:1	17.231	155.29:4	:135				• 4.10ML	HVO	III		613			652 95	67.
is	1 - 74	12	20		.4	14.11	19.22:N	156.3064	:(5				. 4.43ML	F VO	111		513			052 95	67.
- * ,	: 174	12	25	22	: 1	48.4	20.1524	154.126	1(5				3.2 ML	FVO			613			CEE C4	134.
- 4-4	: > 7 -	12	2 :	17	- 2	39.0	19.753N	15619	: 36				3.7 ML	F VO			613			052 96	35.
· ·	1 .7+	12	27	: -	- 4	17.3	11.1. FN	155.387	24 5				3.0 ML	HVO			613			CEE C5	EE.
	1 .7 -	12	25	: 7	24	23.0	19.3431	155.1674	338				3.9 ML	FVO		E	613			052 95	£7.
4 18	1 - 14	12	33	. 3	: 2	41.11	19.7411	156.1500	: (4				3.9.ML	HV0	111		613			652 96	35.
0.10	1 . 1 -	13	2.9	15	24	23.51	19.35 N	1:5. "4:4	(27				• 4.2CML	FVO	111		613			152 95	
- + .)	197+	13	24	57	34	15.2	19.5130	155 . 172	.012				3.4 ML	FVO			613			052 85	117.
- 1 3	1974	12	1,	10	35	57.5	19.345N	155.4(5%	(1)				3.2 ML	FVO		5	613			052 95	21.
- / -	1 - 7+	12	3.0	11	39	:2.5	14.4 41.9	110.61/4					3.2 ML	F VO		5	613			152 95	£ 4 .
nd -	1914	12	24	11	22	11.4	14.3424	100.2844	0.51			*	3.7 ML	HVO		F	613			152 9F	4.5.
	19.14	12	3.	12	51	44.5	10 12 1	155 29	10.4				- 4-10ML	EV0	111	-	613			052 55	65.
	1 . 7		31		22	10.51	19 47 1	155.611.	117	•			3.60ML	F VO	111		613			052 95	50.
•		14	3.			5	9.317N	1FF . 116.					3.2 21	FVO		E	613			(52 95	59.
	7 .	1 3	31		2 .	27.11	15.3019	165.31 1	. 5				3.4 CML	F VO	111	-	613			(52 95	E4.
		17	31	· .	÷ .	F 111	4.76 N	155.43 1	121				3.5.ML	F VO	111		613			652 95	49.
- /	- 7 .	12	51		1.4	3.2	19.2-64	155.267	1.16				3.0 FL	FV0		ε	613			.052 95	58.
F73	1 4 74	12	31	: 2	25	29.5	19.311 1	155.368 4	(15				3.2 ML	hV0		E	613			652 95	56.
+ 1 -	1) 7 .	12	3:	12	4:	41 . 2	19.3 14	155.364 4	005				. 5.5 ML	FVO		ε	613			C52 95	57.
- 7.5	1 5 74	12	31	13	16	45.4	19.27EN	155.3654	207				3.0 ML	F VO		ε	613			652 95	51.
r1)	1 7 74	12	31	: 5	56	37.7	19.34.1	155.1344	114				3.5 ML	HVO			613			052 95	59.
743	1 + 7 +	12	3:	:+	30	22.1	19.3.224	155.172%	015				3.4 ML	FV0		ε	613			052 95	56.
- V)	197+	12	31	:4	4 7	15.0	19.2704	155.3674	((6				• 4.1 ML	FV0		£	613			052 95	58.
- 13	1974	12	11	14	5.9	14.3	19.2734	155.1614	£ 0 0				3.6 ML	FVO			613			(52 95	59.
n V J	1 = 7+	12	31	13	2:	5:.5	17 94	155.1074	535	e.			• 4.4 HL	FV0			613			052 95	88.
-13	: 974	:2	31	: 5	51	17.2	13.30%	155.3314	371				3.3 ML	HVO		Ε	613			052 95	60.
- V -	1 = 7+	12	31	16	4-	19.4		155.3Fx	004				3.1 ML	HVO		ε	613			652 95	59.
=1/)7/1	7.										AGE	25									

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						1200			LONG	NEDTH		MAGN	TUDES-		-		INT	PHENOM	RN	CE	Q/S	MAR	60	DIST
SJURCE	YEAR	Mu	AC	FR	MN	SEC		L • I	LONG	(KM)	BODY	SURF	OTHER	LOCAL	-		MAX	DISAND						
			Ensi	RIA		HEL TC.	ATE											F	613			052	95	55.
AN INI	1074	12	31	17	10	53.4	19	.311N	155.3818	004				3.2 M	L 1.40			Ē	613			052	95	56.
- V J	1274	12	31	19	:2	17.4	19	.20JN	155.378W	005				3.2 M				- F	513			052	95	55.
- 23	1 37-	12	31	19	12	21.3	19	.312N	155.3794	120				3.1 0	HVO		111	-	613			052	95	60.
	1 4 74	12	31	19	30	5= .2h	19	.31CN	155.3338	305				3.200	L				613			(52	95	55.
	1974	12	31	19	51	8:.9	19	.21CN	155.3971	C C 7				J. 4 2 M	L L VO			Ε	613			C 5 2	95	55.
- 11)	19.74	12	31	2 .	4 1	55.4	19	.303N	155.3864	034			. *	3. 4 M	HVO				613			052	95	59.
LAL	1 7.7+	12	31	2.1	53	25.0	19	.262N	155.3594	207				3.4 4	HVO	· · ·		ε	613			052	95	55.
440	1974	12	31	21	24	43.5	19	-272N	155.4324	396				. 4.3 M	L HVO				613			052	95	57.
HY3	1 7 7 4	12	51	-1	41	54.3	19	.263N	155.362%	004				3. 6 (%	L FVO		III		613			(52	95	57.
0 35	19.74	12	31	53	14	22.81	19	-291 N	155.36LW	103				3.26%	LIVO		III		613	_	-	152	70	57.
35	1974	13	31	22	25	29.11	14	. 36 JN	15. 16.04		.5.5 MB	5. MS		: 5.364	L HVO		1		613	D	19	052	95	59.
35	1974	13	31	22	4.	4/.55	17	2714	155.360%	006				3.06M	L HVO		III		613			152	95	EC.
O 35	1774	1.	31		0	13.50		- 34 TN	155.3364	613				3.504	L FVO		111	5	613			(52	95	53.
🙆 + S	1 9 14	1.				1- 6	1 4	.236 N	155.435W	135				3.5 M	LIVO				613			052	95	65.
- / >	1 - 15	11		- 1	112	:7.3	19	.175 N	156.144.	÷.• .				- 4.1 M	L FVO				613	F	15	052	95	65.
44.4	1 - 75		11	1	1 23	50.9-	: 0	-1:37	155.4.3%	470	• 4 . 0 h M B			. 4.20				E	613			552	55	65.
**2 FY3	1 9 7 9		: : 1		29	17.0	: "	. 26 AN	165.3644	125				3.0 4	I F VO			ε	613			652	95	54.
-1)	1975	31	31	- 1	55	47.2	17	.2 %N	1-5.4.34	005				4.1 M	L HVO			٤	613			052	95	56.
	1470	j.			2 2	18.1	19	• 275 M	156.3686	367				. 4.6 1	L HVO				613			052	95	62.
	: 375	1	1 11		2 +1	11.9	19		165.355%	1.6				3.5 8	L HVO				613			052	95	540
- 43	13.75	5	1 11		3 :5	45.9		1	105.4164	015	*			3.3 1	L FVO			E	613			152	95	56.
r V J	1970	-	1 21		3 44	16.3	1 3		155.3510	16.4				3.4 H	L FVO				613			052	95	53.
r V 1	1975	3	1 11	-	4 5:			1. 1625		032				3.1 1	IL FVO				613			652	QE	58.
Π¥	1975	3	1 11		4 4 5	17.1		41	155.345%	. 31				3.4 1	IL HVO				613			032	95	62.
	1 1 1 1 2	-				14.7	1 7		1 155.354.	133				3.1 1	IL FVO				6:3			652	95	£2.
- V -	1.75	2	1 .1			1.1.1	10	.::7!	1 155 . 15 15	227				3.3 1	IL FVO				613			352	95	53.
	1 - 7 -	3	1 1	1 2	6 1	5 12.7	1	9.2375	1 155.4112	. 031				0.21					613	F	17	C52	95	64.
	1975	3	1)	1	0 1	\$ 54.31	+ 1	1.3: 1'	155.3000	1 305	. 4.5LME			3.0.5	I FVO				613			652	95	56.
	1 197.	3	1 2	1 2	6 4	1 45.3	1 .	9.2491	1 155.3756	: 107				4-1()	IL HVO				613	F	14	052	55	54.
	1975	:	1 3	1 (7 4	55.0	+ 1	9.375	1 155.400	1 265	. 4.21M			3.3 1	IL EVO			E	613			C 5 2	95	57.
-1	1975	2	1 0	1 0	7 54	44.5	1	9.2721	1 155.354	0.05				3.1	IL HVO				613			052	95	60.
- 1	1975	:	1 2	1 0	7 2	51.0	1	3.2.3	115.350	1 6.35				3.5	AL HYO				613			052	95	27.
V	1 13:75	3	1 2	1 3	9 1	35.4			166 A(5)	1 116				. 4.3	PL PVO				613			552	95	56.
+ 7	5 1775	c	1 5	1 -	9 4	45.1	-	0.7.1	1 166.371	013				3.6	ML FVO			-	513			152	65	70.
r V	J 197:		1 .		5 8	1 47.7	. :	9.319	1 155 . 232	11				5.4	HL HVO			L	613			652	SE	55.
-4	0 1773		1 1	1 1		44.4	ĩ	4.277	N 156.410	10.0			,	. 4.4	ML HVO			. "	413	F	19	052	95	19.
	1 19 12			1 1		2 :7.:	F 1	9.25.	N 155.400	6 6 17		3		- 4.4(ML F C				613		.,	C 52	95	63.
• • >	1 1 1 7 6		1 1	; ;	1 2	54.5	1	9.113	N 155.363	N CC 8				- 4 - 1	IL FVO				613	F	43	052	55	59.
	1473			1 1	2 4	1 11.3	+ 1	7.211	N 155.400	¥ 005	.4.70M	3		• 5.10	ML FVU				613	F	27	052	95	45.
	1 5 7-		11 3	1 1	3 1		• 1	9	N 155.500	4 910	G .4.50M	3							613	F	37	652	95	32.
22	7-		1 1	1 1	3 2	1 54.5	. 1	9.475	N 155.580	1 212	G .5.13M	e • 5 • 3M	2	3.6					613	5		(5)	95	56.
**1 * 2) : 17-		1 0	1 :	3 4	4 27.8	:	9.134	N 155.366	N CC3		0		• • • • • •					613	F	20	(52	95	56.
	197		1 3	1 1	13 4	4 36.J	* i	9.271	N 155.854	4.110	C . 4.70M	3		3.1	ML HVO				613	5		052	2 95	57.
	3 197:	5	1 3	1 1	4 1	- 55.6	1	9.351	N 155-356	4 103				3.7	ML HVO			٤	613	5		052	95	71.
	1 19.7:		1 3	1 1	15 3	5 18.9	9 I	9.295	N 155.234	0 31 C				3.1	ML HVO				613	5		05:	2 95	59.
FV	J 197:	: 1	:: :	1 1	16 3	1 41.5	5 1	3.247	N 100.3/1	N 035				3.0	ML FVO				613	5		(5)	? 95	15.
÷ •	J 197:	5	1	: !	17 2	3 41 .1	1 1		W 100+114	with		FAGE	26											
c1/27	/17.																							

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SJURCE	YEAR	06	DA	۲R	MN.	SEC	LAT	LONG	DEPT	۲	MA GN I	TUDE	s		• •	INT	PENOM	RN	CE	Q/S	MAP	DG	DIST
					_				(KM)	BODY	SURF	OTH	ER	LOCAL	•	MAX	DISVNO						((()
1 1.40	ICARES	A	FOS	5181	LE	DUFLIC	ATE		DOF				•	A . 20MI	L VO			613	F	22	052	Q.C	F 9.
0 05	1935	01	11	1,	40	43. JF	19.2300	155.4004	205	A. 5.140			. *	A. 30ML	HVO	•		613	F	16	052	95	59.
	1 3 7 4	31	31	~ ~	10	55 0	19.2004	155.34000	000				•	S-A MI	HVO			613	•		052	95	63.
- V J	1075	61	C 1	21	17	53.7	19.301N	155.4174	CC2					3.1 ML	h VO			613			052	95	53.
- 20	19.75	01	01	21	37	20.4	19.4739	155.4614	C1 C					3.6 ML	F VO		E	613			(52	95	44.
440	1975	11	21	23	26	54.1	19.234N	155.3594	206					4.2 HL	HVO		-	613			052	95	51.
- 4.3	1975	01	11	23	56	51.1	19.2951	155 . 26AW	010					3.7 ML	HVO		ε	613			052	95	67.
HVO	1 1 75	c1	:2	12	39	09.7	19.201N	155.3998	011	4				3.6 ML	HV0			613			052	95	59.
+ 4.0	19.75	01	22	C3	27	43.1	19.217N	155.317W	000					5.0 ML	F VO			613			(52	95	59.
r V J	1975	21	32	.3	39	53.4	19.125 N	155.374W	C10					3.6 ML	+ VO			613			C52	95	62.
HVO	1920	31	32	23	41	47.6	19.267N	155.405W	008		•			3.4 ML	HV0			613			052	95	55.
GVH	19.75	21	32	33	43	(7.9	19.311V	155.3934	006					3.0 ML	HVO		ε	613			052	95	54.
F 40	1975	C 1	ί2	i 4	i.t	23 . 1	1ª . 277N	155.4100	039					3.4 HL	HV0		ε	613			052	95	54.
F 7 3	1975	:1	:2	64	26	47.2	19.234N	155.3198	C1 0					3.2 ML	. FV0			613			(52	95	56.
C. D	1975	31	32	29	27	5F . "H	19.2" IN	155.400%	1 23	• 4 • 0MB			•	4.1CML	. FVO			613	F	12	052	95	59.
410	: 7.75	11	.2	12	1 +	F 9	10.104V	155.37 JV	207			· .		3.1 HL	HV0		-	613			052	95	. 62.
FV3	1 9 75	c 1	:2	12	44	:2.5	19.7630	155.4.21	105					3.0 ML	. HVO	×	-	613			652	95	54.
r V J	1975	31	: 2	11	1	47.7	4.141	155.2928	000			×		3.1 ML	FV0		Ł	613	-		152	95	24.
35	1 7.75	01	12	13	27	45. 1	14.2.	155.4.39	005	• 4 • 5 UM5	4.2 % 5			5.11ML				613	r	31	652	90	57.
-/3	19.75	51	12	1=	9.1	35.5	19.1.10	155.5734		•				3.3 ML			6	613			152	95	. 02.
443	1 4:15	-1		10	44	13+3	12 4271	105 (744						3.6 11	EVO		2	613			(52	95	26.
- 4 3	1 - 15				5.2	14	16.315M	155 304	0.05					3.2 ML	F VO			613			152	55	5.4.
	1 7 7 3	31	12	20	11	10.0	12.2764	155.3500	0.09				•	3.0 ML	FV0		-	613			052	95	62.
-11	7.	21	13	-1	4.7	52.4	19.17 N	155.3459	513					3.9 11	HVO			613			152	95	62.
4.1.1	1 4 75	61	: 3			10.3	19.745N	155 . 1774	234					3.2 ML	FV0			613			052	95	52.
	: . 75	21			11	****	19.2108	1 - 5 . 4 - 7%	033					3.4 ML	FV0			613			(52	95	57.
- 3 3	1 77-	21	13	5	15	16.7	19.1724	155.7514	:10					3 . 1 ML	+ VO			613			652	95	62.
- 13	19.75)1	53	27	37	4	19.2:41	15.3624	210		,		•	4.9 ML	HVO			613			052	95	62.
4 V J	1975	.1	23	57	43	43.2	17 . 2 3e N	155.2934	30.3					3.2 ML	. HVO			613			052	95	57.
F V 7	:975 .	:1	C 3	(+	1:	42.4	19.244N	155.391W	603					3.4 ML	. HVO	•		613			C52	95	57.
+ 43	1 75	31	23	11	14	44 + 1	19.2171	155.3134	C1 C					3.5 ML	. FVO		-	613			(52	95	59.
41)	1 9 7 2	11	33	- 1	: 1	35+3	13.31.51	155.3754	010					3.3 ML	. HVO		Ε	613			C 5 2	95	57.
- 1.	1475	31	33	12	27	19.5	19.341N	155.37PW	336					3.5 ML	. HVO			613			052	95	58.
- 40	1 3:75	-1	12	11	17	28.7	14.2.74	155.3696						3.8 ML				613			152	73	57.
+13	1 473	- 1	1.5		2.	51 . 7	10.241 N	155.3719	110					3.1 ML	. FV0		F	613			(52	95	56.
	1 7 7:			1.	20	1	14.3214	170.120%						3.5 MI	EVO		с.	613			15.2	96	60
	1	- 1		::	11		10 14 31	155 46 31	001					3-0 ML	HVO			617			252	95	5.5.
- / .							10 20.11	155.7160	616					3.7 MI	EV0			613			652	95	26.
	1 . 7 7 .				2.		10.14.34	155.714	010	. A. 7CMB				501 112				613	F	19	(52	95	36.
- 33	75	11			10	52.0	16.3101	155.1254						4.4 ML	+ VO		' E	613			52	95	
- 11	1 2 1 -	21	11	3.4		51.5	19.197N	156.2234	314				•	3.1 ML	HVJ		-	613			052	96	52.
	: 3.75	11	14		15	2- 1	19.3411	155 . 3 SEW	1105					3.7 ML	HYO			613			652	95	58.
- 70	1 5 75	c 1	64	: 1	4 .	1: .7	10.239M	1-5. 1+1W	624					3.1 ML	FV0			613			652	95	58.
. 35	1 1.75	21	64	. 6	30	52.31	19.31:1	155.11 (1	100	. 4.3CM3				4.5CML	+ 10			613	F	16	(52	95	84.
4/2	19.75	51	34	15	32	25.5	19 .241N	155.371%	31 3					3.7 ML	. FV0			613			052	95	59.
- 14	1 4.75	21	14	15	32	:5.2	19.240 N	155.373W	617					5.0 ML	HV0			613			652	95	59.
-17	: 5.75	11	14	10	42	13.1	19.279N	155.38:4	337					5.1 ML	. HVO		E	513			052	95	57.
+ 4 -	1 . 75	21	34	ie	1.	31.6	19.2224	155.3154	CC5					3.4 ML	. FVO			513			(52	95	59.
=1/37/1	7.									. F	AGE 2	7											

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SOURC	EYEAR	MJ	DA	-	R MI	ti S	EC	LAT	CNG	DEPTH	• -		MAGN	ITUD	ES-					INT	FHENDH	RN	30	Q/S	MA	DG	DIST
			1.05			0.0		ATE		(KM)		8001	SURF	01	FER	20	CAL				013440						
	1975	21	0.0		6 1	3 1	H.2	19.232N	155.3660	207						3.5	5. MI	- VO				613	· ·		052	95	60.
	1 4 75		2.0	1	4 2	2 5	6.0	19.256N	155.3624	0.09						3.1	ML	HVO	3		5	613			C52	95	56.
440	1995	C1		1	5 2	4 5	3.9	19.256N	155-34PW	305						3.2	ML	HVO			-	613			052	95	61.
EV.C	1975	01		:	6 5		6.6	19.224N	155.3754	116						3.0	ML	F VO				613	:+		(52	95	60.
HVO	19.75	21	24	:	7 2	5 3	2.0	19.1951	155.3640	006				×		3.0	ML	F VQ				613			C52	95	62.
44.3	1975	11		;	9 2		3.1	19.276N	155.4164	609						3. 9	ML	FVO				613			052	95	56.
440	1 3.75		25		6 4	6 3	9.6	19.227N	155.3654	0.06						4.1	ML	HVO				613			952	95	56.
25	1975	C 1			1 3	2 1	6.9.	19.51 TN	155.6554	31 0 G	• 5	.12MB	5.3MS						r.			613	F	43	052	95	21.
F V U	1975	C1	C 5	1	1 1		1.3	19.2 "FN	155.3948	005						3.0	ML	FV0			ε	613			(52	95	55.
r VG	19.75	31	36	1	7 4	7 .	2.9	19.277N	155.4018	613						4.5	ML	F VO			ε	613			052	95	55.
140	1935	31	37		3 5:	1 4:	5 . 1	19.285N	155.4654	005						3 . 1	ML	HVO			ε	613			352	95	54.
G 35	1 9.73	31	ũ I		3 4	7 0	3. JH	19.3.JN	155.420W	005	• 4	. 4 9MB		•.		. 4.4	OML	hVO				613	F	20	052	95	54.
FV2	19.75	\$1	:7	2	3 31	2	7.2	19.45CN	155.592W	600						3.4	ML	HVO				613			052	95	30.
+ 13	1975	21	21	2	5 5	2 5	:.2	19.25"N	1=5.343W	4 2 D						. 4.1	ML	F VO				613			652	95	61.
- 43	19:15	31	33		c 1	5 3	1.3	12.244N	155.5404	316						3.5	ML	F VO				613			\$52	95	62.
7.13	1 . 7:	11	17		5 1	4 5	4.0	19.2421	165.3300	:41						3.1	ML	HVO				613			\$52	95	62.
- 10	: 9:75	51	17	1	3 .	4 .	7.1	: 3.5434	155.3041	115						3.3	ML	FV0			E	613		÷	C52	95	54.
+13	: 775	21	31	i	7 3	4 E	4.1	10.1.54	155.5711	:31						3.2	ML	1-10			E	613			\$52	95	48.
-15	197:	- 2	15	:	1 1	1 2	·	13.4334	155.2414	0.28						3.1	ML	1 VO				613			C52	55	61.
745	1 4:15	15	37	· .	4 7	4 4	+.5	19.974.4	156.3344	01:						3.1	ML	FVU			-	613			352	76	74.
-1.	191:	12	33	•	c 4	5 E	2.4	19.2448	155.5450	200						3.6	ML	HVO			E	613			052	45	43.
443	19.05	12	12	: :	: 3	5 2	7.4	19.545N	156.2438	215						3.1	ML	FVO				613			552	75	45.
- 4 3	1973	- 7	14	1	5 4	2 4	2.1	14.3751	155.(56W							3.4	mL.	F VU				613			052	75	30
- V J	197:	23	20		4 4	. 4	4.9	19.4.DV	1-2.6.34	013						3.0		F VO			E	613			052	QE	52.
	1 - 1-	11	21		1 1	. 4	1.2	10.1704	153.1.1 W	3.4						3.4	NI NI	hv0			-	613			052	GE	620
- 1)	151	14	- 4	•	2 1		1	19437LN	ITP. FIN	034						3.1		F VO			-	613			152	65	50.
F 7 5	1.7	• -		-	5 4	1 2		19.00110	.70.8134							3.1	MI	L VC			F	613			152	95	24.
C J .	12.75				7 .		1 0	10.5 44	LACOUNT ACL							3.1	MI	E VO			5	613			652	9.	25-
14.5	1 2 12		• •		1 4		3 7	13	155.6511					14		3.0	MI	HVO			F	613			152	95	24.
	1 2 75		1.0		r 1.		2.1	19.4.20	155.473.	31.1						4-1	MI	E-VO				613			052	95	43.
	1 75		16		6 1	0 2	6.4	· 9 . 4424	166 . 60 TU	61.5					•	3.2	ML	I VO				613			652	95	46.
	1.47.		1.4		7 5	- 5		19.435N	155.6121	0.14						3.2	MI	EVO			F	613			652	95	28.
- 4 - 4	1 3 75		1 -	, ,	1 5	5 4	3.1	1-417W	165.6139	334						3.1	ML	HVO				613			052	95	22.
- 11	1 1 7 5	5 3	1.6		1 5	7 =		19.456N	155.2444	523						3.1	ML	FV0				613			052	95	67.
+ V *	1 + 7=		17	1	5 11	1 3	4 . 1	19.5.04	145.6694	616						3.2	ML	F VO	•		ε	613			(52	95	23.
- 71	1 . 7=			. 1	4 4		. 5	19.4:14	: 55 . 6371	177						3.2	ML	t VO			ε	613			C52	95	26.
	1	• •	Ξ.		1 .		5.1	12.4371	155.7724	21.1						3. 3	ML	FVD			E	613			052	95	12.
- V.:	4.25	1.1		-	3 2		2.0	14.5 1.4	155.6514	1.5						3.1	ML	+ VO			2	613			352	95	25.
- 4.3	7-		22		: 4	1	5.7	19.41 24	115.1724	1:5						3.1	ML	FV0			E	613			052	95	3.
FV	: 775	0 1	23		1 5	5 5	7.1	19.1424	155.1174	609						3.0	ML	t vo			ε	613			C52	95	£1.
LAL	1 +75	6 5	24	. 1	2. 2.	6 7	7.7	19.454N	155.5914	601						4.4	ML	F VO			E	613			052	95	31.
171	19.75	0	20	1	0 1	5 2	3.1	19.4041	155.5074	031						3.3	ML	HVO			Ε	613			052	95	36.
443	1975	63	21	. 1	0 4	7 5	3.6	19.4151	155.6:34	253						3.2	ML	FV0			ε	613			052	95	30.
+ V 3	: 475			: :	7 4	3 4	0.0	19.416%	155.6649	[[7]						3.0	ML	FVC			ε	613			(52	95	23.
172	: 9.75	34		1	- 1	7 5	3.5	19.5 N	155.6634	077						3 . 1	ML	FV0			Ε	613			052	95	23.
440	1 3.70	64	34	1	3 .	- 5	5.7	19.3214	155.229%	611						3.9	ML	HV0				613		× .	052	95	72.
FV3	1975	54	: 4	. :	5 1	5 1	7.4	19.32CN	155.2278	(1)						3.5	ML	F 40				613			052	95	71.
+ 1 -	: 97:	64	0.5		2 :		3.2	19.271 1	155.311W	C C 7						5.0	ML	FVO			E	613			(52	95	57.
-13	1975	34	1.	1	(2	4 0	4.9	10.2771	155.3248	336						3.5	ML	+ VC			E	613			C 5 2	95	56.

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A-30

SJURCE	YE AR	но	01	1 F F	:1N	SEC	LAT	LONC	DEPTH	BODY	MAGN SURF	ITUDES -	LO	CAL		INT MAX	FFENOM	RN	CE	Q/S	MAR	DG	DIST (KM)
INDI	CATES	A	ens	STH	IF I	DUFLIC	ATE																
	19:75	04	15	11	56	56.3	19-28AN	155.3774	a07				3.8	ML	HVO		E	613			052	95	57.
AVD	9.75	14	16	12	15	55.4	19. 12N	155.2224	31.0				3.8	ML	HVO			613			052	95	71.
	1 2 75	6.4	27	r .	24	55.3	19.4141	155 . 6124					3.9	MI	EVO			613			052	95	30.
F V U	1075		37	10	ic	20.3	10 2754	155 3611	010			A)	3.0	MI	L VO		F	613			652	95	69.
	1743	34	37	29		67.0	10 305N	LEE JEAU	04.0				3.0	MI	H VO		-	613			052	85	76-
nvo	1943	34			32	10.0	10.9951	100.0044	04,0				3.0	MI	HVO		F	613			652	95	25.
440	1713	94	13	LD	24	10.9	19-442N	100.6074					3.0	PIL.	HVO		L .	613			052	95	79
HAD	14:25	64	10	14	17	41.2	19.341N	155.1344	010				3.3	TL.	HV0		5	613			152	95	79
FYG	1 - 15	64	11	.0	22	24.9	19. SEN	100.1448	LIL .				3.5	nL.	FVU		L	613			150	0.5	27
445	1 9:75	04	15	23	24	11.2	19.4:31	155.6264	205				3.1	nL	1 40		-	013			152	75	210
UVF	: 5.15	34	17	16	53	22.5	14.531N	155.5624	CCA				3.1	ML	PVU		· E	613			052	73	29.
440	1 1.75	14	17	23	23	14.7	15.3524	155.221W	516				3.5	ML	HVO		-	613			052	75	120
HV3	19.15	C +	18	CC	57	11.6	19.490N	.53.679W	013				3.3	ML	FVO		Ł	613			052	93	19.
n V 3	1 - 75	64	1 2	- 3	22	24.0	19.309N	155.2234	010				3.7	ML	1 10			613			652	22	/1.
443	14.15	34	15	11	11	29.6	19.503N	155.8168	:13				3.2	ML	FVO			613			152	22	26.
24.3	19.15	74	: -	13	3:		16°-316M	156.7482	r46				3.3	ML	HVO		-	613			052	69	110.
HVC	1 - 7 1	:4	14	14	15	.4.1	19.5311	:55.6E44	: [9				3.0	ML	FVO		E	613			252	95	24.
- V	1 4 75	14	18	24	2.0	55.4	19.4 14 N	155.12%	((4				3.0	ML	FVO			613			652	55	29.
r ¥ 3	14.75	34	2.	15	17	3	14.126 N	155.7744	007				3.3	I.F	F VO			611			152	95	41.
- V L	1 - 75	34	21	1:	-3	50.4	19.2414	155.5050	212				3.0	ML	F VO			613			052	55	38.
n V C	1 : 75	.+	24	.4	4 .7	15.9	19.3643	165.3 18	: : .				3.0	P.L	FVO			£13			552	25	.57.
EN J	1975	: 4	32	. 7	::	21.4	19.0164	115.41.31	:: 1				3.1	ML	F VO		_	E13			552	95	24.
-10	1 .75	34	5.	1.9	35	35.1	19.4+24	1.2.4.14	321				3.3	ML	F VC		E	613			152	95	27.
UAL C	1915	24	- 7	25	41	33.0	21 4N	155.5741	[14				.3.2	ML	F V0			613			SEE	65	14.
110	1 - 75	÷4	27	22	.4	53.3	17.4424	155.6369	103				3.0	мL	HVO		£	613			652	95	29.
44.3	19.10	94	23	- 1	14	21.1	19.446%	152.6212	323				3.2	ML	F VO		. E	613			052	45	31.
+ V 0	1 , 12	:4	33	:1	41	r7.5	19.4(2)	155.27EH	015				3.4	ML	F VD			613			152	95	£4.
141	1 4.75	1.9	3	19	5.3	12.0	19.376 N	155.483%	230				5.3	ML	I VO			613			C52	95	43.
14.4	1 4 7.	11 **	3.	. ú	4.7	e	1 - 475M	153.5569	123				3.5	ML	HV0		E	613			352	95	31.
	1 9 75	5	<1	21	14	24.1	16 .: 451	155.7288	159			×	3.0	ML	HVO			E13			\$52	85	1: 9.
+ VG	1 3 75	25	(5	21	۲ż	36.5	17.434N	155.657.	024				3.2	ML	FV0			613			022	95	29.
r V 0	1975	:5	: 5	22	55	11 . 3	10.4334	155.6019	((3				3.0	ML	FVO		E	613			(52	95	36.
	1475	35	37	17	5?	30.5	19.0134	156.7.28	211				3.7	ML	I VO			613			652	96	54.
445	1975)5	17	2:	3 :	15.5	19.4741	155.5924	001				3.5	ML	F VO		•	613			052	55	20.
430	19.75	:5	1)	:4	33	51.9	10.3384	155.1264	213				• 4.5	ML	F V O		E	613			652	•5	£1.
HV0	19.75	65	11	: 4	12	12.1	19.5.35N	155.0046	001				3 . 0	ML	HV0		£	613			652	95	24.
+ 10	1 175	65	11	19	44	31.5	19.4614	155.6318	C 2 3				3.4	ML	F VO			613			(52	55	26.
- 4 -	1 3 7.5	35	14	. 3	4 1:	51.3	19.5924	155.5584	521				3.0	ML	1 VO		ε	613			C 5 2	95	56.
- 43	: 11.	3.5	: -	10	÷ 3	5 . a	19.4248	165.6116	3				3.0	HL	1100			613			ú52	95	30.
- 40	. > 7>	55	: 3	11	5:	17.4	19.4354	165.5482	551				3.1	ML	FV0		ε	£13			652	9 5	36.
FVJ	1 7 7:	15	18	18	25	46.5	. G . 4 32M	:55.6150	113				3.3	×ι	FV0			613	•*		652	55	25.
- 80	197:	35	17	.5	13	15.4	12.428N	155.61EW	334				3.5	RL	+ V0		E	613			052	95	28.
- 44	: 5.73	:5	19	19	4 3	27.3	19.4404	:55.5974	611				3.0	ML	HVO		E	613			C52	95	30.
HVO	: 1.7:	15	21	12	32	56.2	20.3121	155.6134	523				. 4.7	ML	FV0			613			CRE	05	58.
FVU	1 9 73	:5	22	64	45	15.4	19.37EN	155.4696	111				3.2	ML	HVO		£	613			652	95	45.
45	1975	:5	23	58	3.7	51 .71	20.302N	155.6474	(22	• 4 . 4 MB			4.7	CML.	F VO			613	F	22	133	(5	96.
HVG	19.15	15	34	:2	:4	45.3	17.4151	155.4164	011				3.5	ML	FV0		ε	613			052	95	49.
CVE	1 4.75	15	25	:5	13	37.3	17.664N	156. 134	22P	Χ			3.0	ML	HVO			£13			C 5 2	96	26.
445	1935	(5	- 7	11	5 2	54.6	17.465N	155.5528	020				3.1	ML	FV0		E	613			652	95	31.
FV3	1975	:5	27	.6	40	41.9	19.4191	155.6781	663				3.6	ML	FVO		E	613			152	95	29.
HVJ	1 77=	35	29	12	1 +	14.1	19.37FM	155. 111	029				3.9	ML	F VO		Ε	613			C52	95	15.
51/07/1	·.									F	AGE	29											

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A-31

SUJRCE	YEAR	CN,	101	۲	8 .1	" S	E C	LAT	LONG	DEPTH			MAG	NITU	JDES-				IN	TF	HENOM	RN	CE	0/5	MAR	DG	DIST
										(KM)	800	YC	SURF	(DTFER	L	OCAL	•	MA	¥ 0	TSVNO						(KM)
INDI	CATES		FOS	SI	BLE	DU	FLIC	ATE											-								
C V H	1 9:25	15	31	1	2 4	ú 3	5.1	13.374N	155.4648	007						3.	0 ML	FVO				613			052	95	45.
HVU	19.15	35	30	2	2 4	5 3	7.1	19.454N	155.6064	003						3.	2 ML	HYD				613			052	95	29.
FV0	:975	63	C 1	2	2 5	7 5	7.5	19.451 N	155.593W	CC 4						3.	2 ML	HVO			ε	613			C52	95	30.
+ Yu	1975	65	22	2	5 1	: 1	4.5	19.37CN	155.4658	305						3.	3 ML	FV0				613			(52	95	45.
- 43	1975	36	12	i	9 5	A 3	7.3	19.457N	155.6004	201						3.	1 ML	E VO			. Ε	613			(52	95	36.
- 4.3	1 9.75	25		1	1 1	G 4	6.2	19.4810	155. 5704	201						3.	1 HL	HVO				613			652	95	32.
HVD	1905	15	15	•	- 1	1 0	3.1	19.316N	155.2154	016						3.	6 ML	HVO				613			052	95	18.
F 40	1975	- :	67		6 -	2 1	1.7	10.574N	155.4468	111						3.	1 ML	h VO				613			052	95	46.
EV.)	1 9 75	16	67		1 5	1 6	7.6	19.196N	155 . 6584	215						3.	6 ML	FV0		-	E	613			(52	95	42.
	19.75	36	2.2	-	3 3	2 2	9.3	17.3431	155.1334	010	× :					3.	4 ML	HVO				613			052	95	£ C .
- V.I	1975	36	11		2 5	1 1	1.6	19.4341	155 . 6:94	194		1.0				3.	2 ML	HVO			ε	613			052	95	25.
	1 4.7 .	25	11	1	5 1	6 4	4.7	19.4371	155.6194	004						3.	2 ML	HVO			-	613			252	95	26.
- W.5	1 3 73	16		:	7 5	4 1	2.3	15.131 N	155.1004	156						3.	C ML	HVO				613			652	95	20.
FVJ	1 3 7 6 3		1.7	;				16.452N	166.6750							3.	C ML	FVO			ε	613			C 5 2	95	32.
	1			:			1 6	19.6.49	166.6644	67	•					5.	2 ML	HVO				613			052	95	24.
	174.5				2,		1	16 4:26	165.6154							3.	5 MI	HVO			F	613			: 5.2	95	29.
	1 1 75			ï				19.4541	165.48.4	61.0						3.	5 ML	EV0			-	613			052	55	42.
					2 1	3 4		* 0	155.6:44	6:3						3.	2 ML	+ VO			ε	613			(52	95	26.
- /)	1 4 75	. 7	1:	1		1 .1	5.7		14.4630							3.	O ML	F VO			~	613			C52	94	166.
			1.2			2 4		12.3.74		537						3.	2 ML	FV0				613			652	85	EE.
			10		•			10 100M	165.4716	136						3.	a ML	HVO				613			052	85	tt.
- 9.4	75	~ 7		;				19.1714	155.3:74							4.	2 ML	+V0				613			652	95	
	1975	17	2.4	-				19.476N	155.3171	631						3.	4 ML	FVO				613			(52	95	61.
4 - 5	1 2 3 4		12	-	1 .		1 -	10.1614	155.315.4	126 4							2 141	EV0				613	F	20	652	55	61.
• • • •			15	;	1 1	: ;		14.4314	155./404	115	r.						3 ML	HVO				613			652	95	26.
	1 . 7 .	1.			5 1	3 1	5.2	9.4611	165.1111	6.0 -						4 .	2 ML	FYD				613			052	95	26.
	1			*-		2 1		13.4174	144. 5664	27.5						3.	C MI	HV0				613			:52	95	34 -
	1 1 1 1			•	4 -	. ;		16.4.74	165.4 140	201						4 -	3.CMI	+ VG				61 1		5	(52	55	29.
	1		1	1		3 3		16.4 (24)	165.6704	204						4 .	4.241	F VO				613		5	652	95	26.
	1 3 76	14	10	;		3 2	5	13. 616 1	166.446.	112						3.	2 ML	HVO			F.	613			652	95	46.
F 4 C	1 3 75		14	2	2 4			19.5420	155.4150	601						3.	C 31	+ VO			•	613			152	95	42.
	1975	17	17	-	5 3	2 4	2.7	19.4 39M	166.4234	116						3.	6 ML	HVO			E	613			052	95	45.
- 1/ -	1 3 72	17	1.7			1 2	7.6	10. = 141	155.4601	256						3.	1 ML	HVO			F	613			652	55	44.
	1 2 1 2	- 7	17	'		1 2	2.1	19.6 SEN	155.6613							3.	6 ML	EVO			-	613			652	55	45.
	19.15		- 7	ĩ		7 4		14.5614	155.4020	103						4.	7 ML	F VO				613			(52	95	42.
	1 2 74		37	:		0 4	2 24	16	155 4520	() 7						3.	6 CMI	E VO				613		10	152	95	45.
				:				16 5114	1 5.4.21	2.18						3.	SAMI	HVO				613		6	652	95	45.
	1 - 13			:		5 6		10 3 10.1	165.41.38	235						4.	2 MI	EVO			F	613			652	95	45.
	1.0.7.			;	5	7 4		12.04.1	155 . 4751	000						3.	2 MI	E VO			F	613			152	95	44.
143			. ,	-				13	155 4631	195						3.	5 MI	1 4.3			F	613			-= 2	Q.F.	45
	1 2 7 2			-				15-21	165 3614	106						3.	3 11	E VO			F	613		**	052	95	45
147			11	-	- 2	3 4	1.1	1 7 4 D 2 D M	100.4614								6 41	LVO			Ē.	613			152	66	45.
-43	. 4.13	11	31	-	2 2		1.1	19.54 .4	100.4619							3.	0 111				5	613			CES	95	
r V 3	15 15	61	1	5	3 3	5 2		19.5.5N	150.4724							3.	3 CHL	H VO			L	617		17	DE 2	95	
• 55	1415	-1	3.		. +	1 9		14.51.44	1-5.4789	091	-3.9	n B					JUIL	L VO			5	417			16.5	06	4.5.
	14:15	37	: 4	~	1 5	: 4	• 5	19.536N	1:5.4654	005						3.	JEL	P VU			-	613			052	75	
-1)	14.15	(7	25	÷	1 (a i	• 7	19.53.N	155.4732	001						5.	6 ML	- 40			5	613			052	30	43.
- K)	:975	67	: 1	:	4 :	6 3	1.4	19.532N	155.4574	266							1 ML	FVO			L	613			132	22	45.
S	1 7:75	07	15		4 5	- 5	2.2	19.526N	150.462%	209					5	4.	ZOML	F V0			-	613		19	652	95	45.
-43	19.30	17	16	:	4 5	2 1	·.e	14.533N	155.4670	307						3.	C ML	HVO			E	613			052	95	44.
- 73	15.75	27	36		6 3	- 0	۰.٢	19.5324	155.4734	366						3.	3 ML	F VO			E	613			652	55	43.
11/27/1	7.											F	AGE	30													

SJURCE	YEAR	MO	10	84	MM	SEC	LA	LG	(KM)	BODY	MAGN SURF	ITUDES-	LOCAL		INT	FFENOM	RN	CE	Q/S	MAR	DG	CIST (K4)
++N IND	CARES	4 1	:05	SIR	LE	DUPLIC	ATE															
141	1975	CT.	38	12	56	35.2	19.525N	155.4748	3 3 3				3.3 ML	. PV0		E	613			652	95	43.
G 35	1 9 75	37	39	:1	39	07.5H	19.517N	155.4654	037		4		3.90ML	+ VO			613		6	C52	95	44.
440	1975	37	38	29	57	12.7	19.535N	155.4654	107				3.9 ML	FVO		1 E	613		1.5	052	95	44.
HVD	17.15	37	12	21	0.9	21.4	19.53JN	155.4764	606		8		3.2 ML	HVO		ε	613			052	95	44.
EV3	1975	67	11	23	33	41.4	19.54CN	155.4624	((5				3.0 ML	HVO		E	613			052	95	45.
F VG	1 9.75	.7	: 9	.3	49	27.6	19.536N	155.4654	100				3.4 MI	HVO		E	613			(52	95	44.
EV0	1 1.75	37	19	. 5	47	47.7	19. F43N	155.4664	009				3.9 MI	F VO		Ē	613			C52	95	44.
HYO	1975	27	19		57	49.6	19.541N	155 . 4714	606				3-1 MI	нуо		, Ē	613			652	95	44.
. 35	1975	67	24		37	12.64	19.5170	155.4564	056				. A. 10MI	HV0		-	613		12	052	95	45.
ENG.	1975	57	19	:7	. 4	34.0	19.53 N	155.4639	100		!		3.0 MI	HVO		F	613			052	95	44.
F V 3	1975	-7	6.9	1	AC	DT. 6	19.5314	155.4704	CCA				- A-5 MI	- FV0		-	613		÷ •	(52	95	44.
	1 4.75	07	14	11		23.0	19.542N	165 469U	0.17	· ·			3.4 41	+ VO		F	613			652	95	45.
	1 476	17	13	1.1	0.7	27 54	13 6134	155 4424	207				3. 4 001	HVO		-	613		11	052	95	
	1 3 75	07	12	15		42.75	12.5154	155 462W	217				- A. 30MI	HVO			613		12	65.2	95	
0.03	1 3 75	67	-0	1.	41	12 . IF	C SCTN	155 4654	667				A. SCHL	HVO			613	F	10	052	95	44.
	1 2 75		:	10		26.4	10 5201	1.1.46.34	200				3 1 MI	- NO		5	413	•	10	152	95	
r, /	1 7 7 2	1.1	. 7	•		10.01	10 2721	110.4624	100				3.1 41	- FVO		5	613		÷	152	75	- 3.
	1.9.4	- 1	14	- 5		50.5	150-1	100.4/10	SUE				3.0	. F VO		-	6.3			652	75	42
			1.	- 4	1.		19.2451	100+1104					3.4 ML				617			25.2	25	
	1 6 75	• ;			-	20.00	1 3 6 . 14	156 517.					3 6 34			F	613			(52	95	31
		: ;				50 -	13 . 6. 4	1 5	23.1				3.7 41	. FV0		-	613			16.2	95	64.
							1	150.1014					5 0 1 ML				(13			26.9	15	
	1 9.4.2						13 6 7 7 1	155 4 19	12 3				3 0 40	HVO		F	613			000	95	30.
	1 2 4 2		31	*3	21	2.1 7	13 41-14	155.0.0	. 1				3.5 11				613			150	95	7.
- 13	1 7 15					20 5	17.44.2.14	103.7424	210		•		3. C MI			5	613			153	95	15
F ¥ 3	17/7	- *				10.7	10 2674	100.1204	111				3 5 61			L	613			652	0F	65
					36	11.7	10 0714	100.0-01					3 2 2	HVO			613			65 2	95	67
- 2.3	1 - 12		1		2:	2.7 • 1	10 0 7 7 1	1.0.0-04					3 . J FiL			5	613			152	95	56 .
	1 7 1 1 1	1.	1.1			67 1	10	155.2433	617			1	3.0 41			L	613			652	64	24
1.1.2	1 4 1		11				12.444	1 0.1211	676				3.7 ML	1.40		-	(13			(52	6.5	2
P 7 -		14	- 4		42		14.2874	100-2109	135				3.6 ML	FVO		£	613			152	95	
.175		11	16	1	4	:1.6	** · / · / ·	155.2452	316				S.C ML	FVU		-	613		1	052	10	11.3.
- 4 -	1975	1:	21	- 1	34	44	14.44-51	152.4/48	010				• 4. U FiL	HYU		L	613			052	93	43.
- 4 -	14.15	-	21	15	44	31.4	2	155+1240	-15				- 3+0 ML	FVU			613			052	63	95.
	1 4 17			- 4		21.05	14	175.1351	133				J.L ML	FVU			615			052	76	36.
147	1575		01		41		18.00 1	155+1434	134				3.0 ML	FVU			613			152	10	93.
116	1912	3.3		12	: •	20.02	18.4.64	100.7528	512			. '	3.1 ML	FVU			613			052	25	91.
-7:	1					4 . 5	18.4031	1-234	614				3.5 ML	HVU			613			052	53	93.
- / /	- 17.	- *	55		2.14	10.4	1 P 74 N	155.0514	211				3.5 ML	FVO			613			052	85	93.
* ¥ G	1975	1.4	\$7	L É.	1.	*	16 . 315N	155.7475	111				3. (ML	F VO			613			252	85	91.
r 7.5	1 - 7-		1.	• 2	34	1:.5	19.33.11	155.1434	13.9				3.6 ML	FVO			613	54	**	C52	95	7.
145	1=1:	7.9	1:	. 4	43	50.5	15.3324	155.7616	212				3.1 ML	FVO		-	613			052	85	127.
- ¥ -	19:7:	Ç.a	10	13	21	- 5 • •	15.3514	155.4953	242				3.1 ML	- HVO		E	613			052	95	46.
F43	1 9 75	()	10	13	12	10.3	19.341N	155.1114	(("				3.0 ML	HVO		-	613			052	95	82.
rV)	1 9 15		1 4	:4	54	21.6	1 - 2424	105.535W	(1)				3.1 ML	FVO		E	613			652	55	44.
- 4.2	: 3.75	64	21	14	46	35.2	19.3371	155.2.HW	214				3.2 ML	F VO		Ε,	613			652	95	72.
-40	19.75	34	4 2	.2	ic	.7.1	19.395N	155.4354	060				3-4 ML	HVO			613			052	95	46.
F 4 3	1975	: 9	- 5	¢1	3 3	56.2	14.251 N	155.451W	[4]				3.C ML	F VO		ε	613			052	95	46.
FVU	1 7 7 5	33	¿ C	- 1'	34	13.7	18.9+74	115.2714	015				3.9 ML	FVO			613			652	15	83.
715	1975	13	33	- 4	23	35.4	13.246 N	155.656W	911				3.0 %L	L NO		E	613			652	95	30.
713	1975	15	- 1	31	₹4	3.0.0	19.2104	166.2254	-1 C				3.7 ML	HVO			613			052	95	71.

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SJURCE	YEAR	мо см	DAI	FR MN	SEC	LAT	LONG	DEFT			MAG	NI	TUDES			•	INT	FFENOM	RN	CE	Q/S	MAR	DG	CIST (KM)
ANY LUDI	CARES		220	TAIF	30611	ATE			bu		5000		011 21											
EV.	19.15	10	12	14 17	47.9	16 .445N	156.7244	(73						3.6	S ML	HVO			613		• •	052	86	144.
+ YG	1975	10 1	11	11 15	38 . 5	19.271 N	155.359%	100						3.	A ML	FVO		3	613			[52	95	55.
nvo	1975	1.3	1.1	13 22	14.5	19.497N	155.8F6W	017						3.1	ML 0	FVO		E	613			652	95	3.
HYU	19:15	10	13	16 17	37.1	19.282N	156.2054	343						3.3	2 ML	HYO			613			052	96	55.
HYD	19:35	13	19	01 95	46.5	19.142N	155.5584	231						3.5	5 ML	hVO		E	613			052	95	50.
hVO	1975	IC :	22	12 39	13.9	19.7694	155.3876	(17						3.1	G ML	HVO	·	ε	613			052	95	62.
EV4	19:75	13 .	22	16 53	54-9	11.9234	155.29CW	\$12		× '				3.1	L ML	FVO			613			652	15	17.
CVI:	19:75	13 :	26	23 31	47.5	19.32:1	155.4724	01 0					K	3	3 ML	HVO			613			052	95	46.
FYD	19.75	14 1	27	19 23	37.8	18.916N	155.2788	21 3						3.1	2 ML	HVO			613			052	85	28.
GVH	19.75	12	27	19 3:	52.9	19.315N	155.223W	210						3-	7 ML	HVO			613			652	23	11.
rv3	1975	IC .	30	17 47	34.9	18.919N	155.217W	[21						3.1	I ML	HVD		6	613			652	60	27.
r40	1975	1)	31	34 50	53.E	19.20CN	155.642W	600						3.1	ML	FVO		L	613			152	95	96
AVD	19.75	11	31	15 22	24.7	18.931N	155.3944	012						3.4		FVU			613			052	85	88.
H A O	1975	11	15	13 5:	31.2	16.9944	155.2554	016	·					3.1		L VO		5	613			352	55	61.
- 4 -	1 9:75	11		12 25	21 .2	17.34.8	155.5124	13.						4 4 6 6		F VO		Ľ	613			(52	95	62.
r 4 0	1979	11		- 22	11	10.3114	155.0114	13.1							MI	t vo			613			(52	95	62.
N Y 2	1940	1.	. 0	1	50.0	4 19.4 N	165.3050	174.4	-4 - 4	MA				. 4.	SCAL	E VO			613	F	26	352	95	61.
. 15	1 7 7 2	11		• • • • •	12.1	17.4.1	165.3050	125 4						. 4.(ML	HVO			613	F	15	052	95	61.
	1.97.	11	12	14 -	67.0	19.4	155.3108	:25 .		•				. 4.1	ICML	H VO			613	F	14	052	95	61.
	1		. 7		14.4	14.465N	155.276%	621						3.1	2 ML	FVO			613			(52	95	64.
nV.	: 5.35	11	15	14 5.	36.5	19.2=4 N	155 728	:13						3.6	5 ML	t VO			615			652	95	19.
475	1575	11	19	14 23	4=.5	15.94FN	155.507%	:54						3	5 ML	FV0		÷	613			352	63	66.
-43	1975	11	11	11 24	3	19.359N	155.136%	919						. 4	S ML	HVO			613			352	95	90.
• JS	1 - 75	11	11	11 2.	21.7	- 19.4.13N	155	437						. 4.1	UCML	FV0			613	F	13	052	95	53.
	: 97"	11	11	:	12.3	19.35-1	155.2594	C1 .						3.	1 ML	FAC			613			(52	55	66.
241	1 , 7:	11	13	23 23	*4.9	19.5464	155. 162	100						3.	7 ML	+ VO			613			\$52	95	87.
177	1911	11	14	1 2	1 13.7	14.34 N	155.3418	532						3.	Y YL	FVO		E	613			052	95	= =
: ٧ -	1575	11	14	.1 53	4: . 7	19.001N	1:5.4104	(35						3.3	2 ML	F VO			613			152	95	65.
483	1 5 25	11	1+	37 5:	43.7	19. 14 EN	155.566W	33 H						5.	ML	FVO			613			052	13	51.
- V -	1975	11	15	12 5	21.2	19.320N	155.0249	311						• 4•	4 ML	HVO		5	613			052	90	44
- 4.7	1 9.75	11	15	13 :.	32.2	1 3 / E N	115.1834							3.		FVU HVO		5	613			052	95	23.
rV J	1975	11	20.	15 41	44.2	14.5524	155.5139							3.0		F V0		2	613			C52	55	64.
r V G	1975	11	25	-1 4	14.5	10.4.11	100.2 4%	614						3.0	2 MI	E VO			613			052	95	62.
riv J	1-12	11	21		12.4	10.000	100.271%							3.1	MI	LVO			613			068	36	1.5.
H+ G	19.75	-+		1 3	44.6	10 1101	181 0700	100						3.1		EV0			613			052	95	16.
₩¥)	1113	11	21	10 1.	4.49	17.51.14	11007724									EVO			613			552	96	75.
r V i	1 - 1 -	11	2.4		•	1 - 1 4 4 4	100.200								7 11	F VO			613			052	95	1
-1 V -5	1915	11	-			1.1.1.1	155 1761							4.	3 141	HVO		F	613			952	95	85.
- 10	1 2 1 1	11	27	- 4	12.00	17.34.4	166 3230	(15						3.1	6 MI	FVO		-	613			052	95	66.
HVS	14.75	11	27		2.42	1 . 2 7 7 4	154 0C51	613						3.		E VO		•	613			\$52	94	94.
F V	1 3 7 3	11	2 2		24.4	19.36 1	154.9210	0.00						3 - 1	MI	F VO			613			C52	94	101.
- 40	1 7 73	11	22	.9 1	52.9	19.3574	153.35 14	623						3.1	ML	HV0			613			352	95	56.
	11.76	11	23	4 6	13.1	19.3461	155 . 1525	610						3.1	8 ML	HVO			613			052	95	76.
	1 4 75		20	.4 .	34.9	. 7. 24 KN	155.3769	2.14						3.	D ML	HVO			613			052	95	59.
	67-	11	24	1.	45.5	19.391N	155.(540	116						3.	7 ML	F VO			613			252	95	87.
	1 - 7-	11	24	1:1	\$ 23.4	19.25-1	155.3314	DOE						3	S ML	+ VO		ε	613			C 5 2	95	61.
340	1970	11	24	1) :	3 35.2	19.354N	155.2594	01.1						3.	7 ML	F VO		£	613			052	95	66.
- VD	. 9.75	11	29	:1 3	19.6	19.235N	154. 31%	96 ?						3	ML ML	HVO			613			652	94	103.
11/17/1	7.									P	AGE	3	2											

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STIRCE	YE AR	HO	24	н	R 44	SEC	LAT	LONG	DEFT			MAGN	ITUDES					INT	FHENOM	RM	I CE	Q/S	MAR	DG	DIST
								*	(KM)	BOI	DY	SURF	OTHER	LC	CAL		•	MAX	DISYNC)					(KM)
INDI	CARES	A	FDS	SSI	BLE	DUPLI	CATE																		
.FVO	19.75	11	29	1	(45	5 (1.0	19.322N	155.345W	CC1					3 . 3	5 ML	HVO				613	6		052	95	59.
443	1 9.75	11	25	1	1 01	09.1	19.322N	155.1158	CCF					3.5	5 ML	+ VO			ε	613			C52	95	82.
4V3	1975	11	25	7 1	1 00	58.7	19.128N	154.8454	019					3.1) HL	HV0				613	5		052	94	116.
- > >	1935	11	29	1	1 38	17.3	19.435N	155.4454	526					3.4	A ML	HV0			ε	613	5		052	95	46.
CVF	1 1 7 3	11	29	1	1 51	38.7	19.345N	154.9791	r 0 1					3.0	ML	HV0				613			052	94	96.
HV0	1975	11	2 9	1 :	2 :5	5 52.9	19.374N	155.CCEW	(12					3.2	2 ML	F VO				613	i		052	95	92.
FVJ	1975	11	25) 1	2 2:	27.5	19.267N	155.3664	366			1		3.4	HL.	. F 40				613			C52	95	58+
CVn	1 7.73	11	2 9	9 1	2 2.	27.3	19.279N	155.365W	007			•		3	S ML	. HVO				613			652	95	58.
n V J	1525	11	2		2 25	12.9	19.3291	155.3434	123					3.1	L ML	HV0			E	613	5		052	95	59.
447	19.35	11	29		2 4:	54.2	19.345N	155.0494	308		,			3.1	ML	FV0				613			952	95	82.
FA3	19.75	11	20	9 1	3 29	23.1	19.181N	155.2024	C1 C					3.:	ML	FV0				613		107	152	93	23.
35	19.75	11	2 *	9 1	5 35	40.5	P 19.350N	155. 539	13 9	. 2 . 1	MB	5.185		•						613	F	1.41	652	75	66
4VO	1975.	11	2 9	1	4 12	59.7	19.4.4N	154.3744	507					3.	L ML	. FVU				613			052	79	67
-15	. 9 17	11	2		4 14	33.5	19.5556	155.7624	114					5					L	613			152	55	8.
F 4 3	197:	11		1	4 4.	47.1	1	100. 220			ND	7 140	7 20646		L PL	FVU				613		215	152	95	91.
	1573		-		4 4	4.4	13 2714	150. 244	0.05		nc	1.113	I CUTAS		MI	L VO		·		613		~	552	95	
- 4 3	1 . 1 .	11	2		21		17.7725	1.5. 1724						3.0	NI NI	HVO			F	613			35.2	95	££.
- 4 3	1 - 1 -	4 4	-			5 47.01 E. 2	10.1311	165 3601						3	MI	HVO			-	613			652	95	57.
- 2.0	7 .	11	5				19.3160	155.0152	166					3.	ML	HVO				613			352	95	52.
	1 . 7 3					:7.1	14.37HM		201					4 . (S ML	F VO				613			(52	95	91.
	1 .	11	5	1 1		2 2 4 5	17.41.4	155.41.34	1,9					3.5	ML	FV0			Ε	613			652	95	51.
-15	19.75	11	20		6 44	57.3	19.4/54	155.3558	202					3 . 1	ML	HVO				613			052	95	67.
773	: 575	11	2.		1 1	· · · · · ·	19.3214	155.1183	: 18					3.5	5 ML	HVO			*	613			052	95	83.
+ 13	: 97:	11	2) :	7 3	22.4	141CN	155.0031.	504					3.4	ML.	FV0				613	i		052	95	92.
r V J	147-	11	2 .	, ;	7 4	11.2	19.3.74	154.014%	:06					3 . 5	HL	+ 10				613			C52	94	54.
-11	1 ; 7)	11	2	; ;	1 1	1	13.197N	154 . 1 . 5 . 4	:16					3.1	T ML	FV0				613			052	54	94.
28	:515	11	2		. 4	5 fa.c	F 19.1.175	155.2159	; 1 2	.4.9	MS			4.6	SIML	HVO				613		19	052	95	75
- v 3	1975	1:	2	•	1 5	: fé . 3	19.4351	155.1194	100					3 . 9	PL	FV0				613			052	95	£1.
r 7 3	1 . 7 :	11			1 56	: !! .5	17.175N	154.111.	::7					3.8	ML	. F VO				613	i		(52	94	105.
- 73	1970	11	. 2	; 1	9 1	21.0	19.5571	155.1524	331					3.1	ML	. F VO			2	613			C52	95	72.
140	1 1 75	11	2	+ 1	1 1	1 :1.5	19.4724	:55.4134	226					3 . 1	L ML	HV0			ε	613			052	95	45.
-7)	: 9.75	11	30	9 1	9 1	23.2	19.1274	155.2254	500					3.3	5 ML	FV0				613			052	95	75.
143	: + 75	11	2	9 :	9 3	31.5	19.2.34	155.315%	((4					3	ML	. HVO			-	613			052	95	59.
143	1575	11	2	4 3	11	27.3	19.4224	155.374 4	112					4.	ML	FVO			E	613			152	93	54.
-15	: 975	11	2	1 4	4	. 51.6	17.2 %N	155.1760	202					2	D ML	FVO				613			152	75	61.
••1 -75	19.75	11	2		1 .	14.1	19.3345	170.0104	-1-7					3.1						413			052	95	61.
	1 1 4 2	::					10 3 77.	153.201A						3.1	- MI	h VO			F	613			652	95	63.
F						1 23.1	12.1-6 1	114.1654	er 5					3.0	MI	FVO			-	613			:52	94	117.
	1 3 75		2		11		13.4 61	154.5160	105					3.1	MI	FV0				613			052	94	102.
113	1575					7 . 7	19.4371	155.4 24	619					3.1	ML	HVO				613			052	95	50.
- 4 3	1 - 75					31.7	19.1461	165.1539	300					3.	ML	FY0				613			052	95	78.
	1975	1	3		3 1	\$ 23.0	19.3-64	155.1314	619					3.1	ML	HVO				613			052	95	79.
	1912		5		3 2	27.1	17.426 0	154.9094	209					3.5	5 ML	+ 10				613			C 5 2	94	112.
-12	14.75	1	5		+ 4		19.3-31	155.5185	30			1		3.0	NL O	HVO	· .		E	613			652	95	91.
443	19.15	11	5)	5 1	1 2 7	19.369N	155.0614	226					3.4	ML	HYO			E	613			652	95	87.
+ V J	: 475	1	3	: .	5 45	24.5	19.554N	155.164W	CC7					3.0	ML	FV0			E	613			(52	95	87.
- 13	1975	1	3		7 9:	47.4	:9.334N	155.3346	909					3.0	ML	I VO			E	613			C52	95	59.
185	1 - 15	12	3		7 2	7 22.3	19.336 N	155.1114	337					3.	E KL	FV0			£	613			052	95	82.
111.11	7										P	AGE	33												

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SOURCE YEAR	MJ DA FR MN SEC	LAT LONG	DEFTH	BODY	MAGNI SURF	TUDES	LOCAL	•,	INT MAX	FFENOM	RN	CE Q/S	MAR DG	(KM)
INDICANTS	A FOSSIBLE DUPLI	CATE												
HVJ 19:25	11 33 39 49 37.9	19.3931 154.9634	306				3.1 ML	HVO			613	•	052 94	70.
HV0 1975	11 3: 10 64 45.1	19.453N 154.864W	C09				3.1 ML	- HVO			613		052 94	107.
FVJ 1975	11 3: 10 3: 54.0	19.561N 155.255W	CIC				3.2 ML				613		152 75 052 94	99.
HVJ 19.25	11 30 13 47 14-2	19.35LN 154.945W	000				3.6 MI				613		052 95	72.
440 1975	11 50 14 55 50.9	19.403N 155.0595	0.31				3.2 ML	HVO		£	613		052 55	87.
HU 1975	11 30 17 26 24.4	19-363N 155-081W	1001				3.5 ML	HYO		Ē	613		052 95	65.
EV.) 19.25	11 30 19 21 09.5	19.357N 155.254W	C1 C		i.		3.2 ML	FVO		-	613		C52 95	67.
HVJ 13.25	11 32 29 57 14.3	19.3778 155.0538	006				3.7 ML	HVO		Ε	613		652 95	88.
111 19.75	11 30 02 45 42.1	19.331N 155.059h	005				3.7 ML	HV0			613		052 95	£8.
440 19.75	11 33 22 51 01.8	19.365N 155.120W	008				3.0 ML	HVO			613		052 95	61.
FV0 1975	12 01 26 41 35.5	19.407N 155.051W	0.00				3.1 ML	- HVO			613		052 95	87.
aV) 1975	12 51 52 51 54.5	19.4211 154.9674	006				3.1 ML	- HVO	1		613		052 94	95.
nyu 1975	12 31 4 31 19.4	19.331N 155.125W	001	•			3.1 ML	HVO			613		052 55	81.
4/0 19.75	12 31 .7 of u2	19.35 1 154.6779	000				3-1 ML	- FVO		5	613		052 94	96.
FV : - 75	12 .1 .1 24 23.5	19.1768 105.101W	117				3.4			Ľ	613	*	(52 95	43.
FA1 1412	12 11 21 51 25.3	16.8110 144.3794	111				3.7 21	HYO			613		652 94	95.
74 157	12 11 12 13 13 14.2	19.3618 165.1244	1.10				3.3 HL	HVO			613		052 95	80.
H10 117-	12 11 16 27 35	19.3014 154.9915	137				3.0 ML	FV0			613		C52 94	54.
- V.a. 1975	12 11 11 13 14.4	19.3471 155.1158	100				3.5 ML	F VO			613		(52 95	61.
-10 13.13	11 12 2 15 41	19.362N 165.255W	209				3.6 141	. FVO			613		C52 95	67.
-VJ 1975	12 42 .5 43 55.3	19.454N 154.872W	719				3.1 ML	. HVO			613		052 94	106.
-11. 1.7.24	12 .2 .5 21 29.0	1ª.2:2N 155.197	399				3.0 ML	. FV0		•	613		622 95	75.
-VO 1975	12 02 17 14 15.3	19.311N 155.347w	.04				3.3 ML	F VO		E	613		052 95	55.
r/0 1975	12 02 10 11 19+3	19.3754 155	117				3.2 ML	. FVO			613		(52 95	91.
113 111	12 32 11 12 45.4	17.3558 154.9934	i u a				5.1 ML	F VO		-	513		652 94	94.
-1. 1·1º	12 12 14 21 15.5	19.314N 155.353V					5.2 ML	. HVO		Ł	613		102 90	540
110 20.20	12 12 .6 . 22.6	19.2744 155.2234					3. 5 11				613		(52 95	56
140 1975	12 12 22 32 45.4	19.3211 154.4434	110				3.3 MI	. FV0			613		652 95	59.
-Ve 1-75	12 33 72 10 35.2	19.211N 100.34/5	31.3	•			3.5 ML	- FVO			613		052 95	52.
110 112	12 13 13 1 17.7	4 19 375V 154 643U	-01 -				4.1031	hvo			613	7	052 94	95.
EV.1 1575	12 13 15 10 36.6	19.50 N 165.130	C1C				3 . F ML	FY0			613		052 95	4.
FVJ 1975	12 13 15 31 11.1	19.3948 154 .9151	126				4.2 ML	. FVO			613		(52 94	94.
35 1975	12 23 .5 27 56.6	H 19.342N 155.005V	205				3.66ML	+ Y0			613	9	052 95	15.
25 14.75	12 33 .4 43 53.41	- 19.315N 155.337W	SIA		•		3.1 GML	HV0			613	10	052 95	60.
-41 :3.7-	12 13 11 23 .3	14.1: N 155.1 64	113				3.1 PL	- FVO			613		(52 95	69.
F80 1972	12 03 11 11 44.5	19.1+71 155. 441	LC+				3.C ML	FV0			613		052 95	89.
-14 127:	12 33 11 1 . 23.0	19.351N 154.913.	115				4 . C ML	. F V O			613		C52 94	95.
37 41 LAN	12 13 12 33 46.6	19.34:N 155.342W	035				3.1 ML	. FVO		E	613		652 95	56.
-1) :+15	12 -3 12.51 23.3	19.1728 155.0290	217				4.2 ML	. HVO			613		C52 95	90.
FV0 1975	12 03 13 12 4+.3	19.249N 155.413N	212				3.0 ML				613		052 95	55.
FVJ 197:	12 13 17 41 26.5	10 1101 104 - 712	126				J E ML			F	613		C52 94	76.
nV0 1375	12 14 2. 27 50.4	1". 132H 113. JE24					3.2 ML	- FV0		5	613		052 95	69
441 1949	10 10 20 40 04+0	13.3090 154.411	115				3.8 MI	FV0		L	613		052 54	95.
F/2 1975	12 [4 .1 13 [1.3	19.379N 154.911	600				4.C ML	FVO			613		052 94	59.
141 1915	12 94 31 41 35.7	19.532N 155.2 CV	012				3.C ML	+ VO			613		(52 95	73.
140 197	12 34 17 34 2.4	19.344N 155.3451	105				3.3 ML	F VO			613		052 95	56.
				D	105 3	•								

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SJURCE	YEAR	MO	DA	+ R	4:4	SEC	LAT	LCNG	DEFTH		MAGN	ITUDE	ES				INT	PHENOM	RN	CE	Q/S	MAR	DG	DIST
									(KM)	BODY	SURF	OTH	ER	LOC	AL	•	MAX	DISANO						(KM)
*** INDI	CARES	AF	05	SIBI	LE	DUFLIC	SATE										×	÷						
n V J	1975	12	14	10	35	11.3	19.394%	154.9508	005					3.5	ML	HVO			613			052	94	98. /
FV0	19.75	12	04	11	19	41.8	17.36CN	155.2804	207					3.7	ML	HV0			613	÷.		052	95	25.
+ 4 3	1975	12	64	11	39	1:.1	19.350N	154 .9634	6 3 3					3.5	ML	FV0			613			(52	94	97.
nV J	19.75	12	04	14	21	32.8	19.4411	154.8674	009	·.				3.7	ML	F YO			613			C 5 2	54	166.
CVE	19.75	12	04	17	32	17.3	19.353N	155.3784	900					3.6	ML	HVO	•	E	613			052	95	85.
HVJ	19.75	12	34	21	46	31.3	19.379N	155.1:34	608					3.1	ML	HVO			613			052	95	82.
EV9	1975	12	: 4	21	56	54.3	19.366N	155.0034	006					3.1	ML	HVO			613			652	95	93.
+ Vu	1 5 75	12	25	10	:9	11.5	19.3671	155.252W	C1 .			8		3.3	ML	FVO			613			(52	95	67.
LAN	19.75	12	35	12	20	47.2	19.5511	155.122W	009					3.1	ML	H VO			613			052	95	81.
P / 0	15175	12	15	10	11	55.2	19.259N	155.3554	009				247	3.8	ML	HVO		E	613			052	95	59.
CVF	19.75	12	63	11	37	59.1	19.397N	154.5934	007					3.0	ML	FVO			613			052	94	95.
+ 40	1975	12	60	23	5:	26.3	19.335N	155.291W	006					3.1	ML	FV0			613			C 5 2	95	64.
- VO	19.75	12	36	13	17	40.4	17.379N	155.0314	007					3.1	ML	F A0		~	613			C 5 2	95	90.
IV.	1 4.75	12	15	19	1 %	10.1	19.337N	155.1224	91 0		1			3.0	HL	r 10		E	613			352	95	81.
-V-	14.70	12	17	. 3	47	20.9	19.3611	155.2588	013					3.3	ML	HVO			613			052	95	66.
- 4 -	1 475	12	:7	: ?		22.5	19.2750	155.2(28	CC6					3.3	ML	F 40			613			(52	95	74.
- 1:	: 5 75	12	37	17	5:	43.3	19.4464	:54.9241	235					3.0	ML	1 10		,	615			252	94	111.
475	: 70	13	3 =	: 1	- 1	33.4	19.4.21	15.:40%	15 b					3.2	ML	F V0		-	615			202	95	11.
770	1 9.75	12	13	.2	24	51+1	19.3124	155.347%	.13					3.2	ML	HVO		E	613			152	97	179.
- 4 3	: - 75	12	28	, F	35	52.5		1-4.141.	136					3.0	ML.	FVU			(11			152	06	1970
r V ~	: 975	12	C.F.	• •	11		14.755N	155.0149	(14					3.4	ML	F VO		F	613			652	95	19.
	1975	12	35	11	1:	54.6	19.3725	155.120	194					3.0	MI	HIO		-	613			052	95	82.
n i J	19.15	12	13	12		43.1	10.3334	100.115%	1.1.2					3.2	ML	EV0			613			052	95	£1.
- 4.7	1 3 12	12	t d	14	1	51	17.0000	100 1124	11.7					3.2	MI	E VO		F	613			(52	95	62.
F V 3	1 1 1 2	12		22		40.07	10 4714	165 (272	10.6					3.6	ML	+ VO		Ē	613			652	95	16.
F 23	17 /2	12	1.7		3.	1.3+1	10.1214	1.5. 1674	310					3.2	MI	F VO		-	613			052	95	£7.
183		12	3.2				13.7 (EN	1=5.347"	0.6					3.6	ML	HVO		E	613			652	95	59
- 4.4	1 9 71	1		:1	11	1.3	13.3.74	155.1114	SUP					4.4	ML	HVD		-	613			052	95	٤1.
- 43	1 4 7 -	12	19	13	10	57.7	19.3447	166.1058	C1 C					3.0	ML	t VO		ε	613			652	95	12.
443	1 7 73	1 2	14	13	34	37.3	19.3451	155.1164	611					3.0	ML	FV0		E	613			352	95	15.
	1975	12	: 9	13	50	54.5	13.3614	155.1278	100					4.3	ML	HVO			613			352	95	F 6 .
H Y G	: 9 75	12	1.	11	14	37.0	19. 4 .5 %	155.42.3%	911					3.1	ML	HVO			613			652	95	53.
+ 13	1 3 75	12	1:	::	3 :	3: .7	19.35:N	155.1998	C1 C					3.4	ML	F VO		· E	613			(52	95	13.
443	1 3.73	12	1 1	15	43	10.9	19.334N	155.2611	310					4.0	ML	1 10			613			C 5 2	55	73.
HV.)	1475	12	11	* 3	÷ *	11.3	14.551N	15575W	500					3.1	ML	FV0		ε	613			652	95	66.
440	1 1.23	1?	11	. 5	41	13.1	19.2651	155.1199	100					3.2	ML	HVO			613			652	95	£1.
F ¥	1 7 7-	12	11	:2	25	F	19.341 N	152.0574	150					3.4	ML	FVO			613			625	55	67.
11	1 170	12	11	13	11	43.1	10.357N	155.1624	227					3.3	ML	1 VO		ε	613			(52	95	17.
CV n	1 1.	15	12	:5	۲.,	0.00	19.3534	155.1360	2.30				•	4.9	ML	FV0			613		••	052	95	75.
-15	1975	12	12	16	5:	\$7.7	19.375N	155. 1432	217					3.2	ML	HVO		E	613			652	95	29.
- 1 4 4	1515	12	13		. 53	36 . 3	19.37-N	155.153W	SOH				•	4 - 1	ML	HVO		ε	613			052	95	67.
-13	14.75	12	: 3	11	17	43.0	19.117N	154.5326	((7					5.4	ML	H VO			613			052	94	149.
- 13	1975	12	14	1.	4 :	40.3	19.344N	1-5.1(94	969					3.4	ML	1 40		5	613			052	73	620
1¥3	197:	12	14	11	47	77.4	17.3051	155.2528	0]9					3.0	ML.	HVU		-	613			152	10	67.
- 4 5	19.15	12	14	14	, G	27.2	19.3121	155.24FW	110	1				3.5	ML.	HVU LVO		Ł	613			152	94	57.
FA3	1915	12	15	14	3.4	11.8	14.395N	124.969%		1				3.1	HI.	L VO			613			(52	65	76.
140	1975	12	16		43	17.2	19.416N	119.1154	1176					3.4	ML	1 10		Ľ	611			152	GA	166.
HV3	1973	12	17		4	20.0	19.4458	165 1120	000					3.1	41	E VO			613			152	95	£1.
170		12	Γ,	10	42	0	1	100.1100	0		AGE	14		3.1					013				1.1	
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INT FRENOM RN CE Q/S MAR DG DIST SOURCE YEAR NO DA FR MN SEC . MA> DTSVNO (KH) (KM) BODY SURF OTHER LOCAL ... INDICATES A POSSIBLE DUPLICATE 613 052 95 67. HV3 19:13 12 17 09 54 30-2 19.363N 155.256W 009 3.8 ML HVO 613 652 95 43. 3.8 ML + YO 12 19 19 13 43.4 19.431N 155.473W C10 HV0 1975 E 613 (52 95 59. 3.1 ML +V0 FV3 1975 12 19 16 42 22.4 19.3CEN 155.346W CC9 652 95 3.1 ML HV0 E 613 64. 197) 197) 12 19 18 04 16.3 19.434N 155.276W 017 052 95 E 613 .93 3.0 ML HVO E 613 613 E 613 613 E 613 613 E 613 613 613 613 613 12 20 14 14 57.3 19.359N 155.046W 009 0 k n 1975 652 55 50. 12 20 23 30 44.5 19.381N 155.329W 007 3.4 ML HV0 4VD 19.15 052 95 59. 3.1 ML HV0 12 21 17 45 39.6 19.24CN 155.353W 610 HVG 1 9 75 3.6 ML + VO (52 95 £ C . 12 23 J3 50 55.8. 19.342N 155.129N C1C + VJ 1975 3.4 ML HVO 3.1 ML HVO 3.0 ML HVO 12 23 04 04 13.6 19.35°N 155.0418 008 052 95 19. 4V0 1975 12 23 16 19 33.3 19.3C2N 155.:734 609 052 95 65. rVJ 1975 3.0 ML FV0 3.4 ML HV0 3.6 ML FV0 052 55 52. LAH 12 23 39 58 37.4 19.211N 155.4728 311 1 1.75 052 95 52. 19.211N 155.47CW C1C hV0 1 9.75 12 23 13 12 51.1 (52 95 £1. 19.42EN 155.29EW C13 12 23 16 41 47.1 LAF 19.75 C52 95 3.6 ML + VO 51. HVJ 1475 12 23 16 47 06.1 14.426N 155.3*14 013 -3.7 ML HVO 613 052 95 81. 12 23 18 41 47.1 19.365N 155.1159 009 -45 197-3.1 ML FVO 3.5 ML FVO 3.1 ML FVO 3.2 ML FVO 3.1 ML FVO 3.1 ML FVO 613 252 95 1.65. · +V3 19.1: 1" 24 .. ++ 34.9 19.357N 155.077W 200 E 613 +Y) 1875 13 24 14 31 19.4 19.274N 155.2004 C10 (52 95 74. 615 C52 94 1.475 12 24 10 43 45.6 19.4358 154.5278 531 613 99. - V 1 052 95 12 25 11 26 40.2 19.3429 165.7542 010 £7. 1V -1 E 613 152 95 -Y. : 17 12 26 . 4 3: 2:.4 15.4529 165.0318 011 . 6. E 613 352 95 11 16 19 27 18.4 19.3428 155.1.78 (15 3.5 ML +V0 82. + 43 197 613 (52 95 17 26 13 32 54.2 19.3718 155. 164 200 3.7 ML HV0 84. EVE 1275 3.2 ML + VO 613 12 26 25 53 57.2 19.3658 155.2559 310 052 95 67. +Vi) 1175 613 . 4.2 ML FVO 052 95 53. 12 25 22 55 24.9 17.9418 155.6128 339 14. 1175 3.7 ML + 40 613 052 55 57. 243 1915 12 27 32 52.4 19.2878 155.3698 .10 E 613 652 95 FV: 1975 12 27 .7.15 30.3 19.3710 155.105% (CE 3.9 ML HVO 73. 12 27 CE 55 24.04 20.0 ... 156. ... 10 C30 . 613 F 11 DEE CE .. 4.1[ML + VO 61. 0.35 1975 3.1 ML FV0 5 613 12 17 15 51 3... 19.3324 155.1114 354 652 95 £2. 613
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 110 1-7: C52 95 -V: 1975 12 27 16 5 02.2 19.4349 155.4 68 209 3.1 ML HVO 50. 19.377N 155.1.24 639 3.6 ML HVO 552 95 ć2. 113 19.75 12 33 3 2 41.0 3.6 ML HVO 3.[ML FVO 3.2 ML FVO (52 95 64. 17 31 .1 47 41.7 19.51 N 155.273# (26 + 43 1515 652 95 19. 12 31 .9 34 14.3 19.3622 155.2409 007 ndi 1975 3.6 ML +V0 352 85 110. 01 51 JE 32 48.1 15.835% 155.176% 017 143 15.7-. 4.7 ML HVO 052 15 124. 11 11 .4 54 19.9 13.674N 155.147K (55. 473 1975 052 95 EVO 1975 (1 (1 15 56 47.3 19.3628 155.7518 (() 3.5 ML + VO 57. 3.4 ML + VO (52 95 72. +V. 1976 21 25 23 17 44.6 19.526N 115.212W CC7 052 95 EV0 1976 01 05 . 43 37.6 19.3129 155.3469 005 3.C HL FVO 54. 3.2 ML HV0 652 94 -1- 1-1-11 24 12 34 52.1 13.4659 164.2641 109 154-3.7 ML + VO 480 1.475 21 37 ... 16 33.4 19.2118 165.2444 216 652 95 59. 613 .-+13 177- .1 07 11 44 55.5 19.4554 154.1174 000 .3.1 ML HVO (52 94 134. 3.1 ML FV0 3.3 ML FV0 C52 95 31 37 1: 35 07.9 19.3714 155.1958 218 613 13. FY3 1:72 613 31 38 .2 22 53.4 19.754N 156. 42W 3CA C52 96 40. 4VJ 14.75 3.0 ML HVC 4.2 ML HVO E 613 C52 95 110 :5170 21 10 14 "7 04.5 19.5468 155.110% 009 c2. 613 952 95 +13 :1.70 11 11 14 15 40.2 19.5134 155.270W 024 64. . 3. 3CML EVO 35 1476 21 11 22 26 15.00 CO. 240N 155.572W C10 613 F 16 666 65 72. . 4.1[ML + VO ● 55 1776 11 12 JC 25 39.3F 19.3009 155.309 0374 *4.5 MB 4.2MS 613 F 27 52 95 64. 613 . - 0 1975 J1 12 13 44 32.9 19.365N 105.1119 009 3. J ML HVO 052 95 P2. 4V0 1476 01 12 23 55 21.8 19.553N 155.1154 009 3.2 ML HVD E 613 652 95 81. 3.2 ML + VO 613 252 95 ENG 1976 21 14 CF 13 27.6 19.7708 155.1098 CC9 62. -Y. 1475 21 15 12 41 45.5 17.4(7) 155.743% (14 . 4.4 ML 1 VO 613 652 95 62. FAGE 36 -1/17/17.

SJURCE	YE AR	NO DA FR	MN SEC	LAT	LONG	DEFTH	800		MAGN	ITUDES		LOCAL			INT MA>	FHENOM	RN	CE	¢/s	MAR DG	CIST (KM)
*** 15D	ICATES	A FOSSIF	IE DUEL	ICATE																	
-IVJ	1926	11 15 12	59 26.	1 19.411N	155.2938	016					1	4.5. ML	FVO				613			052 95	62.
6 65	1 976	11 15 22	59 24.	GF 19.300N	155.3004	930.	.4.8	MB				4.50ML	HVO				613	F	54	052 95	64.
EV0	1670	(1 16 19	29 13.	19.375N	155.1(9)	611						3.7 ML	HV0	12			613			052 95	82.
	1976	01 16 20	22 (3.	9 19.355N	154.9944	([2]						3.2 ML	FV0				613			152 94	94.
	1975	01 17 35	29 13.	01 19.30CN	155.100%	005						3.50ML	F VO				613	F	14	C52 95	٤٩.
EVH	19.75	31 15 .4	49 22.	4 19.362N	155.2554	610						3.6 ML	HVO				613		~	052 95	67.
HVD	1976	31 18 14	25 10.	9 19-363N	155.1174	009						3.6 ML	FVO				613			052 95	81.
EV0	1 3.76	C1 16 14	13 37.	+ 19.361N	155.1274	667						3.6 ML	HVO				613			052 95	٤٥.
FV.3	1575	.1 11 23	57 46.	5 19.3754	155.1994	201						3.6 ML	FV0				613			(52 95	13.
HYG	1975	11 21 15	22 17.	7 19.365N	155.112W	308						3.0 ML	+V0				613			(52 95	£2.
LAF	1975	11 21 11	41 21.	2 19.367N	155.1208	008						4.1 ML	HVO				613			052 95	£1-
	1975	11 23 62	47 4.	1 19.361N	155.0936	609						3.7 KL	HVO			£	613			152 95	٤5.
EV 2	1970	\$1 23 18	21 14.	1 19.364N	155.132W	613			ć.			3.2 ML	HV0				613			052 95	79.
F V G	1975	31 26 16	55 51 .	7 19.4111	154.5:14	100						3.C ML	F VO				613			(52 94	102.
144	1 4.7:	01 27 25	15 51.	4 13.173N	155.1:3.	603						3.6 ML	HV0			5	613			252 95	13.
713	1 175	61 27 22	2 2 t 2º.	2 15.335N	155.1119	300					-	4.0 ML	HVO			ε	613			052 95	£2.
443	. 970	31 29 32	17 24.	3 19 .: "3N	155.626:	01 0						3.0 ML	HV0			ε	613			352 95	41.
- 43	: 9.7 :	21 24 65	11 54.	2 13.14+N	155.1014	: [9						3.2 ML	F VO			E	613			252 95	£2.
H 4 5	: . 7.	21 27 1	1 1	5 19.4794	154.4941	209						4.7 ML	F VO				613			652 94	54.
🕘 , S	1975	71 25 2	17 52.	1 19.4 .5	155.1.04	005	• 4 • 5	MB				4.5 CML	F VO				613	F	27	552 95	53.
- +)	1 3 7 5	31 31 14	2. 12.	51 19.4-44	155.3764	100	•					3.1 ML	HAO				£13			052 95	53.
F A .3	1475	21 31 2.	17 27.	19.169N	155. F1W	356						3.3 ML	F VO				613			352 95	85.
r 7 0	1970	62 23 10	42 13.	5 19.17EN	155.1998	CC 9						3.4 ML	FAO				613			[52 55	13.
r V 3	:57:	02 33 2	50 55.	5 19.261N	155.2531	010						3.5 ML	F VO				613			652 95	57.
-143	1 2.75	15 12 1	1 4 - 04.	5 19.357N	155.1356	1:30						3.1 ML	FVO				613			052 95	19.
-VJ	. 9.7 :	12 :5 :0	9 1÷ 1/.	7 19.3414	155.119%	029						3.2 ML	FVO			E	613			152 95	E1.
EV O	157-	2 (7 2.	148 12.	3 19.3318	155.124%	(()						3.2 ML	F VO			E	613			652 95	£1.
- 4 -	15 15	12 11 -0	11 24.	2 19.141N	1:5	667						3.2 ML	FVO			E	613			152 95	
- ¥ .,	1.70	u2 13 f	49 51.	4 13.503N	155.4628	C11						3.6 ML	HVO				613			052 95	10.
~ ¥ 3	197-	U2 23 1	° 51 14.	9 2. AIUN	156.1224	232.					•	5.1 ML	FVU				613	~		000 06	107.
🌒 ມລິ	1973	C2 21 24	51 13.	E 20.276N	156.267%	(33%).	• 4 • 9	MB	4 . [MS			5.CUML	H VO		v		613	r	48	150 05	92.
r 7)	: 9.75	C2 23 C9	45 13.	5 19.5L.N	155.7544	(14						3.2 ML	FVU				613			152 75	67.
.110	1975	J2 24 1	5 5- 14.	2 17.5758	155.1110	201						4.2 ML	FVU			5	613			052 95	65
- 4 -	1973	32 24 14	4 4 2 32.	6 14.5763	155. 214	6.4						3.2 11	L VO			5	613			(52 95	60.
C V P	12.13	J2 24 1	- 1- 3	5 19.102N	155.1334	139						3.1 HL	F VO				613			(52 95	6.2
F A 3	14:7:	22 25 1.	42 2	4 14.5721	195	114						3.9 66	F VO				413			(52 95	12.
- VC	197-	12 26 7	33 25.	4 19.174N	155.1 60	U.S.P						3 . 3 ML	F VO			r.	413			552 95	F 2 .
772	1 - 75	. 27 1	41 14.	8 19+52*N	100.110	14						3.6 HI	HNO			E	613			550 55	91.
- Y .		13 . 6 1.	2 23 .4.	1 10 7 4	100. 336							3.1 M	EV0			F	611			352 95	73.
- 4 3		13 . 7 .	05 34	1 1945.1V	100+2 5%	125						3.7 MI	E VO			-	613		•*	(52 95	£1.
r V 3				0 10.000	152 5500	0.0.2						3.1 11	E VO				611			211 25	72.
- Y)	1910	05 1. 2	41 14.	a 10 3/74	100.002W	510						3.1 ML	HVO				613			152 95	66-
- V J	1 4 70		4 12 42.	2 17.35 N	154 1464	- 13						3.3 MI	EVO				613			652 94	129-
- 43	1 7.15	13 12 2	1 1. 1/.	4 16. 654	155.5100	(1)						3.5 MI	E VO				613			(52 95	54.
F V O	1070			1 12	166 3540	012						3.6 41	+ VO				613			(52 95	40-
- 4 3	121	61 19 1	3 24 10	1 10.1FAM	155.7579	006						3.9 ML	H-VO			F	613			052 95	87.
110	1042	11 17 1	1 1 1 10	4 19 UIN	165.1.00	109						3.1 ML	HVD			5	613			C52 95	62-
	147-	11 21 1	G TI TT	5 19.3714	165. 2540	01 9						3.3 MI	EV0			-	613			652 95	67-
- V-	1 . 7	11 21 0	31 54	6 19.3171	155.1444	0.19						3.2 ML	EV0				613			052 95	79.
			5 51 640	1 1 1 2 2 1 1		1.11		D	ICE	17											

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SOURCE YEAR	MO DA FR MA SEC	LAT LONG	DEFTH	ODY SURF	ITUDES	LOCAL	•	INT MA3	FFENOM	RN	9 33	/s	MARC	DIST
**N INDICAXES	A POSSIBLE DUPLIC	ATE												
NVJ 1935	93 22 20 43 26.9	19.364N 155.184	W 309			3.3 ML	HVO		- Ε	613			052 9	15 84.
FVG 19.75	63 22 21 19 55.7	19.341N 155.111	W 010			3.1 ML	HVO		£	613	1.21		052 9	15 82.
HVJ 1935	03 23 15 66 63.2	19.3149 155.356	W CC9			3.7 ML	FV0			613			C52 9	15 63.
HV0 19.75	03 29 25 09 52.0	19.364N 155.253	W 010			3.7 ML	+ VO			613			052 9	15 67.
HVJ 1975	03 29 38 31 29.8	19.491N 155.251	W 613			3.0 ML	HA0			613			052 9	15 66.
HVJ 1976	03 32 14 52 10.3	19.334N 155.122	w 010			3.4 ML	HA0		E	613			052 9	15 81.
FV0 1936	C4 C2 LE 14 56.5	19.344N 155.10	A (CA		**	4.6 ML	HV0		Ł	613			652 9	13 22.
FAD 1842	24 22 29 14 11.7	19.443N 155.44	w CC7	×.		3.4 ML	FVU			613			102 7	23.
nV0 1926	64 32 19 55 33.3	19.331N 155.216	M 906			3.6 ML	FVG			613	. *	2.4	052 5	10 /1.
GS 1946	64 32 18 14 26.CH	17.4.3N 155.100	1 805 .4.5	5 MB	*	4.50ML	HVO	۷	5	613 1		29	052 7	
HVJ 19175	04 03 01 45 42.2	10.395N 155.224	¥ 004			3.0 ML	FVU		Ľ	613			052 5	5 72-
FV0 19.75	C+ C6 C3 12 52.1	14.143N 155.2L				3.1 MI	L VO			613			152 0	15 72.
FVJ 1975	04 58 11 54 22.2	15 140 N 150	4 115			3.4 ML	EV0		F	613			052 5	25 17.
470 1975	04 11 17 30 4*•2	10 11-N 165 1F	1 100	•		30 ML	HVO		E	613			C52 9	5 57.
NV0 1745	34 12 37 25 22.5	19.6-18 100.00	1. 1.16			3.3 ML	h VG		-	613			C52 9	94 105.
-10,1746		19.317N 155.254	L ()(3.5 ML	HVO			613			652 9	5 67.
100 197	14 20 11 12 13 46.5	13,7568 155.	1 352 -			4.6 ML	F VO			613			652 8	119.
A 45 1975	10 30 a 18 30.40	18.9-5N 155.17	0		•	3. 9 (ML	HVO			613 1	F	15	052 8	5 92.
	F4 22 14 54 14.9	19.5250 165.31	4 112			3.4 HL	FV0			613			152 9	es.
FA: 157:	14 3. 18 57 11.0	19.51CN 155.344	W (1)			3.4 ML	F VO		ε	613			(52 9	95 E9.
CV3 1776	34 23 12 24 53.6	14.1654 155.11				4.2 ML	I VO		ε	613			C52 9	15 84.
143 1920	04 26 21 44 41.5	19.346N 155.2F	N 835			3.1 ML	HVO			613			652 9	15 É3.
-10 1476	15 31 18 52 54.3	19.3 74 155.35	¥ 657			3.2 ML	HVO		Έ	£13			052 9	95 54.
rva 1470	15 12 26 41 57.4	19.115N 155.521	2 33 2			3.3 ML	F VO			613			(52 9	15 - 4.
17: 197:	3- 37 .6 14 43.4	17.35 PN 155.12.	V 31"		•	3.4 ML	F VC			613			C52 9	15 79.
-75 1916	25 11 .8 77 .4.5	19.37EN 15575	12 20 F			3.5 ML	HVO		ε	613			652 9	15 85.
-+.1 :4.70	12 12 15 55 11.6	19.3394 165.19	+ 304			3.7 ML	HV0		-	613			052 9	15 74.
F10 1975	15 14 19 13 42.2	19.20CN 155.5C	7 010			3.1 ML	FVO		Ē	613			152 9	15 44.
-13 2-7-	55 17 .1 45 26.1	14.330N 155.27	W C15 ,			3.5 ML	1 10		E	613			152 7	5 73
1/0 1976	00 17 20 54 44.2	19.324N 155.14	6 010			3.0 ML	PV0			613			652 5	15 17.
-10 1976	15 17 21 44 19.0	19.34"N 155.37	W 107			3.1 ML	HV0		5	613			162 6	5 81.
443 1975	15 11 16 16 41.3	19.329N 155.12	W (39			3.5 P.L	FV0		5	613	/		152 6	5 86.
+ + + 1 + 10	11 19 17 12 11.5	19.52.9 100.12				3.1 MI	F VO		L	613			:52 9	5 15.
-40 1975	JE 21 14 34 44.0	14.3614 166.1	U 11			3.2 MI	HV0		F	613			152 9	5 83.
103 1775		1G 3. IN 155. 55	0 211			3.7 ML	нур		-	613			052 9	5 67.
423 1975	24 23 17 31 2 .2	19.341N 155.114				4.3 ML	FV0		E	613			152 5	5 82.
47. 147.	74 25 22 33 27.5	13.+731 155.41	1. 10			J.1 ML	FVO			613			652 9	5 50.
110 12.76	16 26 12 41.5	19.354N 155.05	11 1:19			3.3 ML	HVO		٤	613			652 9	15 E4.
443 1975	10 31 .6 27 21.1	20.246N 155.60	N 332		•	3.6 ML	HV0			613			086 0	,5 ć7.
FV0 1575	Ch 31 18 32 10.0	21.264N 155.77	4 663			4.1 ML	HV0			613			088 0	5 50.
- 43 1975	35 31 24,53 52.7	20.1478 155.11.	W C29 .			3.C ML	1 10			613			CFF C	5 76.
173 1975	35 31 69 55 52.3	20.1141 155.86	¥ 525			3.) ML	F VO			613			C68 0	5 73.
-VJ 19.7:	35 31 15 15 16.4	19.669N 155.04	4 172			3.3 ML	HVO			613			052 9	5 91.
HVU 1975	Ce C4 22 51 51.3	19.3591 155.11	4 359			4.1 ML	F V O			613			652 9	5 61.
+43 : 774	16 16 .3 45 14.9	19.3721 155.27	w C1C			3.1 HL	F VO		E	613			152 9	5 66.
rva 1973	JE 37 10 39 37.6	19.319N 155.26	W 531			3.5 ML	1 VO		E	613			052 9	5 67.
140 1575	30 10 10 15 23.9	19.335N 155.12	H 304			3.3 ML	F VO		٤	613			652 5	5 E1.
-15 1835	Se 10 22 15 35.2	19.55'N 155.142	4 910			3.2 ML	HVU			613			052 9	5 /9.

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E1/:7/17.

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CONCE	VEAR	MC	10	h	R M:1	1EC		LAT	LONG	DEFTH			-MAGN	OTHE	2 10	CAL	•	MAX	DTSV	0 /						(KM)
SUGACE										(KM)	BOD	Y	SURF	UTINE												
AAN 180	TEATES	Δ	POS	SI	BLE	DUFLIC	ATE			 1.577 AP 1447 					3-1	ML	HVO				513			052	95	60.
EVO	19:76	66	12	1	2 42	15.5	19.	3 3 E N	155.1344	000		8			3.0	ML	FY0				513			[52	95	19.
E VO	1976	26	13	1	4 21	41.0	10.	3 3 7 N	155.1371	009		÷.			3.2	ML	+ VO			Ε (513			C52	95	63.
HVG	1 - 76	36	14	1	4 17	15.2	19.	4 3 4 N	155.2641	604					3.4	ML	HVO				613			052	95	92.
- 40	1976	26	15	:	5 13	32.5	19.	457N	155.4805	010					3 . 4	ML	HVO		1	1	613			052	95	23.
- 110	14.16	36	16	3	9 17	15.9	19.	364N	155.9815	1 308			Х о	×.	3.4	ML	HVO				613			652	95	23.
	1576	66	11	1	2 ::	11.5	17.	375N	155.101:	1221					3.1	MI	FVO				613			C 5 2	95	61.
- 40	1 3 75	0.6	23	Ĵ	1 25	11.3	19.	3921	155.251	1 205					3.1	MI	F VO			£	613			052	95	41.
44.3	1 370	16	21	2	3 38	23.0	19.	1914	155.547	1 211					3.1	MI	HVO			5	613			652	95	/1.
- 11	1976	26	21	1	8 16	27.2	19.	369N	155.215	1 035					3.4	MI	HVO			0	613			052	95	79.
HYD	19.30		2:	1	9 33	34.1	19.	371N	155.210	1 006					3.1	ML	HVO			ε	613			052	95	71.
- 40	19.76	26	21	1	9 36	29.9	19.	Set N	155.216	1.006					3.1	ML	1 VO				613			652	95	76.
- 41	197-	36	21	2	5 80	34.7	17.	372N	155.221	CC5					3.1	> MI	HVO		ć.	E	613			052	95	24.
- 44.4	1 9.76	0.4	21	2	0 13	12.0	12.	3334	155. 184	1 30 4					3 . (ML	FVO				613			052	95	E1.
= ()	1 4.70);	2	2	1 27	29.2	17.	1-51	155.247	N 013					3.	HL	h VO				613			652	94	109.
	7.	C	21	2	3 5:	31.1	:9.	475N	154.846	N 201					3	ML	FYO			ε	613			(52	95	tt.
	1 5 7 5	٠.	12		3 . 4	1 34.6	19.	3774	:55.241	V 20 *					3.	ML	L HVJ				613			652	95	E
- 1	: 17,	1.			1 1	10.3	17.	3 * 4 N	: 5. 243	V 395					3.1	6 ML	L HVO				613			652	95	/3.
- 11	1 7.70	. د	, 2.	- 1	7 4	1 53.7	19.	3304	155.146	V 30 4					3.	2 11	L HVO				613			UB B	66	67.
445	1 - 10	3	5 24			- 51.00	200	12:1	156.141	4 142				e.	3.	2 ML	L FVO				613			1111	05	16.
+ 7 1	: 47.	2	. !		6 :	7 47.3		2321	155.014						3.	1 ML	LIVO			ε	613			152	55	67.
HVI	1 27-	3	7 1	υ.	1 +	43.0	· · ·	4.17	1-5. 11	1 1.00					3.	2 ML	L FVO				615			052	45	82.
1 V r	1975	J	7 2	ć i	.5 4	= 45 . 3	19.		100.000						3.	2 11	L HVO			ε	613			052	65	70.
- 1 1	1970	1	1 1	9 1	17 3	2 12.7	12.	.34 N	155.112						3.	0 41	L HVO				613			(52	9.5	75.
FV3	1570	C	7 1	: :	:1 5	: 24.1	10	-3+2N	155. 27						3.	2 11	LIVO				615			152	95	67.
F 4 3	1775	0	7 1	1	23 2	· 17 !	:9		155.223						3.	0 11	LIVO				613			05.2	65	54-
- 1)	1 176	5	7 1	2	:2 4	5 35.2	1.	.: · 5 N	170.246	R 107					3.	1 MI	L HYO				613			052	05	6.8.
-i	: - 7:	3	7 1	5	16 4	. 55.7	* 3	.17-1	1.5.4.						3.	5 MI	L FV0				613			052	95	71.
- V 3	10.70	3	1 1	4	. :	5 . 2 . 4	14	. : - 71	105.042	4 100					• 3.	1 14	L FVO			E	613			952	95	61.
+ ¥ 3	1476	:	7 1	4	14 1	4 38 +1	: 4	. 2 78	100.414						3.	3 MI	LIVO			ε	615			150	90	4.5.
- 13	: 9.76	3	7 1	5	5	4 57.1	13	.3el	1 1 2 5 2 8	W 205					3.	2 M	L FYO			-	615			052	55	£1.
743	1976	U	11	5	.1 1	1 29.4	14	• 1 / 2 0	100.244	14 119					3.	4 M	L HVO			E	613			(52	95	80.
- V)	1 - 76	3	7 1	r	23 3	1 25.6	1.1	. 531"	1 100.12						3.	C M	L FVO			ε	613			152	95	15.
= V D	: - 70	- J	7 1	5	. 5	1 16.1		. 5 5 21	1 100 147	W 229	٠				. 3 .	7 M	L FVO	•		Ł	613			652	95	67.
+ 12	: 474	i	7 ĉ	2	. 4 4	: 5: •:			100.007	W 615					3.	2 M	L IVO				613			0.6.2	53	79.
- 7 1	1 75	1	7 2		21 4	. 45.4	17		155.L44	11 010					3.	7 M	L HVO			-	613			55.5	95	41.
	1575		7 2	3	: 4 3	r 11.1	1 1:	.1.34	1 1 66 65	00 015					3.	4 M	L FVO			L	613			352	95	£7.
- * -	: 775		7 2	4		14.	1 17	• 2 f 2							3.	3 M	L FVO			~	613			(5)	95	15.
F V 1	1970		7 2	4	- · ·		. 1"			24 669					4.	C M	IL FVO			L	(13			652	95	Et.
+ / .	157-		7 2	. 7	.7	4 66			1 1 55. 34						3.	EM	IL FVO				613		-	353	95	51.
17.	: 4.7-		7 2	. 7	2: 3	1 12.	1	. 5 . 2	1 165 10	50 115					3.	5 M	IL FVO			~	613			35	95	£2.
	7:		17 2			5 17.1		• 3 - 5	1.5.11	11 111					3.	18 M	IL HVO			Ł	613			15	95	73.
5 V) 177:	- 1	. 1 .	sc	1.5			. 24	1 155.0						3.	CM	IL FVO				613			(5)	95	67.
rV.	75				23	14.	6 10	1	1 166. 74	65 375					3.	1 4	IL FVO			F	413			65	2 95	65.
- V () 197:	-	17 .	1		24.	1 10	4 .5	N 155.24	4: 135					3.	3 M	L HVO			5	613			05	2 95	68.
۷۲	197-	7	11 3	5 1	15	51 31.	1 12	1.57	N 155.24	24 9.2					3.	U M	ML HVO			C.	613			05	2 95	E 4 .
- 4	3 197:	•		1	**	1 17	5 10		N 155-16	EV CCF					3.	4 M	ML FVO				613			(5	2 95	67.
F V -	3 197:	5	18 1			10 10	- 10	1.1.1	1 155.24	4 626					3.	6 M	ML IVO				613			05	2 95	67.
• -1) 197	-	1.5	11	16	17 11	4 10		1 155.25	21 310					3.	2 1	ML HVD			F	613			05	2 95	72.
	- 1	2			- 5	3 17	1 1:	1.397	1 165-21	34 858	2			12.74	3.	ů ľ	ML FVU			-	010					
- V	1.7.1	S					• •						PAGE	39												

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SJURCE	YEAR	мо	DA	ŀR	4.1	SEC	LAT	LONG	DEFTH	BODY	MAGN	ITUDES	LOCA	- L		INT MAX	FFENOM	RN	CE	Q/S	MAP	DG	DISI"
ISDI	CATES	AF	oss	191	5 0	UFLIC	ATE																
HV0	19.76	33	C 3	(5	23	31.9	19.442N	154.8954	603				3.0 M	LHV	0			613	-9		052	94	104.
HVJ	1 436	05	36	23	35	55.4	19.379N	155.093W	-1 33				3.2 M	LFY	0			613			C52	95	£3.
n v D	19.75	U.P	37	31	31	45.4	19.355N	155.J45W	007				3.3 M	LHV	0		ε	613			\$52	95	٤9.
	19.75	0A	37	11	42	19.3	19.323N	155.2COW	209				3.1 M	L HV	0		ε	613			052	95	73.
440	1925	6.8	63	13	63	33.5	19.39 N	155.2444	005		*		3.4 K	LHV	0			613			652	95	67.
+ 43	1976	10	10	19	: 3	47.6	19.32CN	155 . 222W	C10				3.5 M	LFV	0			613			(52	95	71.
TV 3	1910	38	14	: 7	21	52.4	19.357N	155.1354	906				3.2 M	LIV	0			613			652	95	79.
aVJ	1970	36	19	15	37	44.5	15.973N	155.378W	032			•	3.1 M	LHV	0			613			052	85	76.
HYD	1930	58	26	33	13	43.6	19.363N	155.2 11	010				3.6 M	LHV	0			613			052	95	63 .
FVJ	1975	35	28	18	59	55.5	19.355N	155.2236	C10				3.C M	LFV	0			613			052	95	70.
r V D	1976	35	31	1.1	41	36.5	19.3"UN	155.495%	610		5 al 1		4.C M	LFV	• •			613			C 5 2	95	41.
1VJ	19.70	Ja	31	:4	33	36.5	19.332N	155.1174	209				3.4 M	LHV	0		ε	613			052	95	82.
c V n	1 7126	:9	32	13	21	26.8	19.353N	155.:534	208				3.5 M	LHV	0	•	E	613			652	95	88.
1 V G	15.75	¢ e	: 3	1	16	55.9	19.31 N	155.177%	004	•			3.1 14	LHV	0		ε	613			052	95	75.
+ 43	1 176	19	: 3	-2	23	41.4	19.462N	154.1554	221				3.5 M	LFV	0		-	613			(52	94	108.
14.2	1 270	34	14	: 3	1.	5+.2	1.0.2.14	155.0724	517				3.9 M	L FV	0		ε	613			652	55	6:.
443	975	33	24	23	3.5	26	19.3835	155.997.	:4 ^				3.1 M	LFV	0			613			052	95	15.
***	1 - 7.2	: 9	5.5	٠ŕ	:4	: 9	1 1:3N	1.2.144	(1)				3.2 M	LHV	0		ť.	613			652	95	1.6.
r V J	1575	: 1		14	54	2 7	19. TON	155.7154	C12				3.C M	LFV	0			613			152	95	32.
- V _	1170	3.1	: 4	- 5	44	15.2	: 3 . 4 4 1 1	154.0.44	968				3.5 M	LFV	0		-	613			152	34	165.
n / 3	: -7.	J	÷٠	14	1 1	1: • 4	14.2544	192.5654	0.05				3.6 M	LHV	0		•.	613			052	75	LL.
-12	: 17-	15	- T		24	4 • T	19.3734	1:5.9:10	000				3.0 4	LFV	0		5	613			652	95	15
+ 4 3	1 2 75	: 9	: 7	55	: 1	12.03	14.57 N	1:5.0798	CC				2.0 4		0			(13			652	95	50
- V D	1977	39	35	- 4		25.5	14.3.5N	155.3478	010				3.2 5		0		E F	613			052	C.C.	570
LA P	19.70	. 4	19	22	14	1: . /	19.4528	150.5734	010				3.0 1		0		L.	613			(52	85	105.
5 V Q	1 7 7 -	24	11	. 3	20	11.6	16 . 1 1 D N	155.2264	.se				3 6 4		0		5	613			352	05	86.
FA7	1 275	(4	11		4	····	14.11.11	1-2-114					3.6.4		0		-	613			162	96	66.
r 7	1 7 75		15		::		17.5* 58	102. 14%				,	2 3 4		0		F	613			152	95	12.
nV J	1115		21	22	-	44.1	17.2454	1-2.10-4	())				3.3.4	I HV	õ		-	613			052	95	6.2
	1 4.7%	24	45		34	20.07	14.4424	150.28 14	01.0				3 7 4	L	0			613			052	95	71.
FV.	1 7.75	64	20		A 7	-3.4	19.1200	100.21%	010				3.3 M	LEV	0		F	613			(52	95	54.
1 4 1	1 7 14				51		10 4334	155 1011	100				3. 4 M		0		F	613			(52	95	11.
- 40	17.17	11	22	::	22		10.3324	199.1214	(1-				3.1 M	LEV	0			613			552	95	80.
140	.) / 3	11		11	12	40.0	1 2 3 7 4	155 1000	110				3.0 M	I HV	0		F	613			652	95	62.
				10	1.	50	1 3 8 TE V	166 1161	600				3.8 M	I HV	0		F	613			052	95	62.
- 40	1715	1.	13	. 0	24	T	10 17:1	100.1100	10				3.5 4	I IV	0		-	613			152	95	15.
	1 4 7 5	11	12		12	3	10.4701	166.0000	2.7.9				3. 5. M	LEV	0			613			552	55	64.
		: '	• ;	- 3	1.1		· · · · · · · · ·	55 7761	13.2				3. 5 M	L HV	0			613			652	95	65.
		: :				22 1	17	166 14 10	: 27				3.3 M	I FV	0			613			652	95	10.
					1. 1	51	10.1151	165.1100	119				3.2 M	I FV	ñ ·			613			152	95	£1.
- V .	. 7 / 2			1.	4.1		15 1/9 N	155 10.11	1.6				3.4 14	1 + 1	0		F	613			652	95	74.
	1 3 74	11	32		• 1	25.3	19.7511	155 1560	216			3	3.5 M	LHV	0		Ē	613			052	95	28.
	1 3 75	1	24	7	17	23.4	19.1.24	155.0630	31.0				3.3 M	LHV	0		-	613			052	95	67.
	1675		(2	11		46.4	16.311 4	155.2241	11:				3.7 M	LHV	0			613			052	95	71.
	7.			14	14	16.1	9. 175N	155 41	114				3.3 M	LEV	0		Ε	613			(52	95	83.
	7-	11	14			46.7	19.3514	155.1114	300				3.0 M	LHV	0		-	613			(52	55	12.
- 11	1 3 7.	11	10	21	4	47.3	19.191N	155.4179	21.2				3.3 M	LHV	0			613			052	95	49.
		: 1	13	15	33	13.4	17.5434	155694	CJA				3.8 4	LHV	0		ε	613			052	95	£6.
F 7 0	1 7 7:	11	: (1.1	1 1	15.5	19.545N	155.1968	C1C	,			3.1 M	LHV	0			613			652	95	73.

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SJURCE	YEAN	80	DA	FR	Mti	SEC	LAT	LONG	DEPTH (KM)	во	0 Y	MAGN SURF	ITUDES OTFE	 R	LOCAL	-	.•	I	NT	PHENOM	RN CE	c/s	HA; I	Dû	DIST (KM)
APY IVD	ICATES	A	FOS	SIB	LE	DUFLIC	ATE																		
r V J	19.76	11	12	16	54	46.5	19.356N	155.0414	007						3.5 M	LF	VO				613		C52	95	19
-IV J	1910	11	12	2ú	07	21.5	19.944N	155.6004	311				•		3.5 M	LF	VO .		.7	-	613		052	73	61.
- HVU	19.75	11	13	11	14	03.4	19.366N	155.185W	604			,			3.7 MI		0				613		052	95	64
FV3	14:10	11	14	14	14	23.1	19.4250	155.2758	015						3.6 4		10				613		(52	95	15
FVJ	1975	11	16		20	33.4	19.510	100.110	005						3.7 N		0			F	613		052	95	68.
- 40	17.10	11	1 1	00	21	40.0	19 30CN	155.2620	014						3.0 41		vo ·			-	613		052	95	63
44.7	575	11	24	14	1 2	15.0	23.1/SN	155.9354	917						3.0 MI	LHY	võ				613		696	65	78
EV3	1970	11	24	:0	15	51.5	19.4 (4N	155.2658	C G 4						3 . 1 MI	LH	VO				613		052	95	65
	19.75	11	3:	17	40	17.1	19.3241	155.1908	000						3.3 MI	LH	O			E	613		[52	95	74
	19.75	11	3 3	18	16	45.3	19.322N	155.1889	010						3.0 MI	LH	cv			- E	613		C52	95	75
UAL	1970	12	31	34	44	17.5	19.361N	155.2544	j]7						3.1 HI	LH	VO -				613		052	95	67
-1 V D	1975	12	14	÷3	5.	53.3	19.334N	155.136%	600						3.0 MI	LH	0				613		652	95	PO
r V J	1 7 7 3	12	56	15	26	51 . 1	19.3594	155.127%	((9						3.6 MI	LF	VO				613		352	95	10.
+ V.J	147-	12	27	:4	÷ .	17.1	1-4:5N	155.2559	C15						3 . C MI		0				613		152	95	e2.
17.1	1975	12	it	- 1	4 1	17.5	14.3:5N	1=5.444.1	226						3.4 1		0				613		152	95	63
- V	1-1-	12	34	1.	31	4	14.5004	155.2079	515						2. U MI		0			۶	613		:53	55	63
- 4 3	1 . 7 .	12	13	: 1	21	4 1	19.1331	155.1150	111					10	3.2 MI		10			F	613		(52	55	\$ 2
F 13	1 1 1 3	12	1.		1		19.376.21	- 55. 17.	20.0						4.6 MI		vo			Ē	613		252	95	12
		• •	1.0				10.1774	155.1181		5.0	MS				4 . 8 "MI	LH	vo	٧		-	613 F	45	\$52	95	£1.
1/2	1 47-	12	35	.7	11	14.9	19.67.N	:56 . : 46%	116						3.3 MI	LH	0				613		152	56	21.
E ¥ 3	1975	12	27	:4	15	21.5	19.394%	155.246%	005						3.3 MI	Lh	vo				613		352	55	67.
- 41	: . 77	12	27	. 5	24	27.5	19.3241	155.2762	613						3.1 MI	LH	V O			E	613		C52	55	65.
17:	1 7 10	12	27	12	:3	54.1	19.1318	155.6340	51 3						3.1 MI	LF	0			ε	613		352	95	42.
C 13	1 4 7 3	12	27	:4	15	2 6+	17.3554	155.2474	315						3.3681	LFI	0				613 F	7	652	55	67.
+13	1 4 7	12	_: 1	19	37	:4.9	19.3204	155.2538	(1)						3.2 MI	LH	0			E	613		652	95	73.
	: 97-	12	2 .	:9	24	26 . 4	19.3.11N	115.2424	CC5						3. C MI	LF	0				613		(52	95	£ł.
-1)	1 97.	15	3 .	30	47	41.5	18.4531	155.3354	512						3.6 11		cv			_	613		C52	15	126
111	1-73	12	3.	.4	1.3	51.6	19.325N	155 . E6W	31 3						3.0 MI	LH	VO			E	613	-	352	95	66
	- 17	-1	22	14	26	35.30	19.3404	155.1204	0.3.4						3 . 7 LMI						613 F	5	152	95	- 1.
13	19.11	- 1				13.20	19.39(1	100.2714	115						5-6:MI		0				613 F	5	652	95	50
22	1 - 77		1 3			63 34	19.411	155.29.0	016						3. 90M	L H	0				613 F	10	052	95	43
25	1 4.77	51	1.4	23	26	42.5H	19.30JN	155.1066	610	· A . 2	MB				4.60MI	L H	vo	IV			613 F	21	452	55	84
	1 9.77	01		::	40	11 . 7H	19.34CN	155.2000	((5	4.1	MC				4 . C [MI	LH	vo				613 F	14	(52	95	73.
. 35	1 9 17	02	34	11	20	53.01	19.4 1CN	155.1004	535	1.5	MB				4.500	LH	vo	۷			613 F	25	C 5 2	95	12.
23	1 4 77	: ; 2	3 4	14	25	11.74	2 .11 N	155.4714	011						3.70M	Lr	0				613 F	12	CFE	65	24.
23	· · 77	15	<u>ہ</u> د	1 1 1	2:	10.51	19.3134	155.5174	15 1						4 . 1 (MI	LH	VG				613 F	18	052	95	39.
1 75	1 . 77	34	2 !	-4	4 7	23+	2 N	155.3334	015						4.5CM	LH	vo				613 F	- 22	666	C٤	13.
.5	1917	26	74	.9	4 -	14.74	19.3471	15 534	00 9	4.8	MB				4 . 8 CMI	LF	0	۷			613 F	52	252	95	85.
- 55	1 9 17	37	15	17	59	42.01	19.425N	155.453	C1 7						4 . 1 CMI	L H	0				613 F	12	C 5 2	95	45.
2 c 👪	1977	13	51	.7	54	21 . 3H	14.34CN	155.2224	31,					1	4 . 1 JMI	L PI	. 0			.*.	613 F	18	352	55	71.
33	1 5 77	- 1	11	:5	14	12.11	19.522N	155.145%							2.9191		0				613 1	15	152	95	14.
	1 3 11	15	1	12	17	13.4+	19.3271	155 455	31.3						L GONI						613 P	19	252	70	11
	1 - 1/	10	3.	1 24	40	17.14	19.3674	155.3179	F						4.50M		0				613	25	25.2	95	4.0
	19.17	5.3				16.64	19.750	155.7670							4 - C [MI		0				613 E	12	1.52	GE	P.C.
2: 8	1 + 77	19	10	4	~ ;	45.31	19.16 N	155 . 1179	005						4 . 1 CM	LH	0				613 F	13	(52	95	11.
35	: 9 17	39	23	112	1-	44.11	19.3673	155. 514	010						4 . 1 CMI	LH	0				613 F	11	352	95	66.
411- 11	-											ACE	4.1												

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S	JURCE	YEAR	20	01	19	2 4	I SE	c	LAT	LCNG	DEFT	+		MAGNI	TUDES	1.0	C 41		INT	PHENOM	RN	CE	G/S	MAR	DG	DIST (KM)
							0.00					DU	01	1 SONT	UTTER	20				0101.10						
	A LAUL	LANES	20	10	510		2 00	210,	IO ETEN	155 1444	120					3.6	OMI	HVO			613	F	10	052	95	.99
	30	1 5183	15	20			3 77	74	12 31 M	155.2234	510					3.4	OMI	HVO	TV		613	F	12	052	95	71.
		1 3 71	15	6.0			1 20		19.5151	155 16 14	614					3.2	CMI	EV0	T V		613	F	17	052	35	79.
	33	1 7.00	LD				6 14	• 11	14.00011	100.100%	C1 5					3.4	CMI	L VO	TV		613	F	9	152	15	77.
	12	1 2.75	U G	13		4			10 3454	100.4074	115					3.1	CMI	HVO	TV		613	F	11	652	95	86.
	17	1	00	13		2 2	4 111	• 211	19.34.4	100.0004	030						ONIL	1.40			613		12	052	65	71.
		19.75	16	21	1.	1 2	1 99	•1H	14.3234	155.2218	111					3.4	CHI	1.40			613		29	1.6.2		60
	35	13.16	(0	23	11	1 4	1 59	•6H	14.325N	125.7564	.11	.4.9	MB			4.2	CHL	FVO	:		613	-		153	95	
	12	1 7 11	67	C 1	15	- 1	1 15	• 5	19.32CN	155.12LW	"					3.9	CHL	FVO	1		(13	Ē		152	65	
	35	19.76	25	31	23	3 3	7 21	•41	19.010N	155.4818	12.5	. 4 . 5	МĤ		. :	4.0	LML	FVO	14		613	2	15	652	75	00.
	35	19.75	39	15	2	3 2	6 46	914	19.33°N	155.22eV	310					3.1	UNL	HVO	1.4		613	r.	15	052	75	20.
*	35	19.13	3.9	12	. 6	6 1	6 36	• 1 P	14.3384	155.1100	610					4+1	UML	FVU			013	5	10	052	35	02.
74	33	1 9:75	11	23	11	5 1	5 1:	91	19.2331	155.55CW	C11					9.2	CML	FVO	1.4		613	5	15	052	95	43.
Ē.	33	1911	12	14	: 4	• :	2 44	• *	19.22CN	155.22CW	C1 C					4.1	CML	FVO	1.4		613	r	11	152	93	11.
÷*)	15	1 3.48	12	27	i.	- 4	1 50	r	14.351N	155.2179	613	4.6	мR			4.3	SML	FVU	1.4		615	r.	42	052	33	11.
	25	1 9 7 9	22	14	-		2 51	• 1 ·	13.14.14	155.0 19						4. (IML	FVO	111		613	r	15	552	95	
8	39	: . 7	- 3	3 5-	-	۰,	7 .	. 24	13.715N	162.5465	3	× 5 • 0	MA	- 4 - 3 MS		4.1	JAL	FVO	v		013	-	27	052	75	E
	28	7 .	. 5	1.	1	5 3	2 I I	• 5t	19.331N	155.1100	1 2	14.8	Nº 13		•	4.6	LML	HVO			613	F	13	152	95	260
	3.5	1 , 7 ;	- 3	1:	1 3	1	• •		17.201N	155.200.	11					3.6	CML	FVO			613	r		352	93	C 4 .
25	ذ ذ	1 - 7 -	13	7.5	ŧ	. 4	. 5		22+1 47 M	122	12	۰.6	MI			4.5	LAL	FVJ	v		613	r	11		15	11.
	25	1 1 7		- :	1	7 5		• 'F	2 2574	155.4214	\$	4.4	Md		-	9.4	LML	I VO			613	-	17	28.8	LS	56.
	13	1 - 7 -	17	3 =	1.	, :	+1	. 7.4	19.755 N	155.3744	2 .					3.6	LAL	FVO	111		613		13	052	32	29.
	13	1613	7	27	. 1		5 .1	.ft	19.307N	152.1318						3.5	CML	FVO	1 V		613	1		152	55	
	35	1 - 7-	:7	31	1.	3 3	1 51	.41	19.445%	155.4334	1.2	. 4.5	M 8			4.3	JHL	F VO	IV		613	F	12	C52	55	47.
1	15	1 + 7 +	19	14	1.	2 5	: 43	. 24	21.4174	156.2538	25	: 4 - 1	Mē			4 • 5	OML	F VO	v		613	F	15	166	06	156.
	13	: 9.13		: 0	23	3 1	4 15	. 4 !-	14.3771	155.454.	11	,				3.9	JML	F VO			613	F	11	552	95	46.
5	35	1 - 77	5.0	22	1	7 5		· +	17.1471	155.72%	-	5.7	MB	- 4.8MS		5.5	OWL	F VO	v		613	F	142	052	95	FE.
1	13	1974		12		2 ?	n ::	. 41	19. 4484	155 . : 31 %	9	4.8	MR			4.3	CML	F VO	IV		613	۴	٤	(55	55	19.
2	5.5	141.	1,3	27	15	5 1	. 45	.51	14.3761	155.121%	10	4.7	43			4.4	OML	F VO	v		613	F	23	C . 2	95	11.
17	13	: 9 75	11	1 4	1	7 3	1 13	1.31	12.9:4V	115.1918	14					4.[CHL	1-10	IV		613	F	9	u52	95	47.
12	33	1971	15	31			j 11	. 71	19.114%	155.343W	1	4.1	MP			4.2	CML	F VO	IV		613	F	12	(52	96	£7.
	. 5	: 37.	12	16		1 3	2 27	1.20	19.4 .1	155.4714	11					4.0	CML	FV0	IV		613	F	10	252	95	44.
	33	: 171	1.2	: 4		3 4	4 : 3	5.11	10.414%	155.4.4%	11				4	4.1	OML	HVG	IV		613	F	8	052	95	50.
	33	1 7 5 :	(1	2 6	- 1	1 2	4 4	5h	19.3121	155.5418	527					4.6	OML	HVO			613	F	11	052	95	40.
	15	: 71		: 2		. 3	1 23		19.712N	156.1954	CICG				-,	4.2	CML	r VO			613		18	(52	96	110.
	25	15.21	33	12	::	2 5	7 4.3	. 71	14.3991	155.2368	652	.4.6	MB			4.3	CML	FVO			613	F	21	(52	95	69.
	14	1 2 2 1		:5		÷ ,	7 31	1.71	:9.234 N	155.5624	311				1-	4.0	SML	HVO			613	F	9	052	95	44.
	:5	: - : :		2 1	(·	+ :	1 37	. "	19.1413	155.2144	633 .					3.9	CML	FVO			613		11	652	95	64.
		1.58.		1 -		. 4		.11	19.1730	:55.1.94	(1)					4 . 3	CML	F VO			613	F	9	152	95	\$2.
			2.2	14	,	1 .	7 1-	. 71	: 1.36.38	155.42.24	91 1					4.1	UML	HV0			613	F	14	052	95	50.
	23	: 9 - :	.1	2 .	11	4		. ".4	9.6.1N	150.1491	225					4.0	OML	HVO			613	F	. 8	(52	96	32.
	10	145		22		7 -	. 1.	. 71-	: 2.366.9	155.1134	101					4.0	SML	FV0			613	F	8	C52	95	61.
	14		10	3-			3 12		19.4. CN	155.2164	(2)					4.1	CML	HV0			613	F	9	052	95	72-
		198	11	24		1 3	1 62	1. 71	19. 16 10	155.1504	209					4.2	OML	t VO			613	F	10	(52	95	Et.
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NUMBER OF FITS 2093 NUMBER OF SUSPECTED DUPLICATES

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FREE ARED BY THE NATIONAL SECRETSICAL AND SOLAR-TERFESTRIAL DATA CENTER

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Appendix B. Earthquakes with M_L greater than or equal to 4.0 from January 1, 1977, through December 31, 1979.

3

SOURCE	YEAR	MO	DA	HR	MN	SEC	LAT	LONG	DEPTH (' <m)< th=""><th>MAGNITUDE (M_L)</th></m)<>	MAGNITUDE (M _L)
нуо	1977	01	14	13	26	42.38	19.33	155.12	9.93	4.6
HVO	1977	01	23	10	49	01.84	19.34	155.20	8.78	4.0
HVO	1977	01	29	22	48	49.72	19.36	155.08	9.07	4.1
HVO	1977	02	03	15	20	49.70	19.35	155.08	9.87	4.5
HVO	1977	03	09	00	29	17.40	19.42	155.50	44.21	4.0
HVO	1977	04	20	18	49	23.01	19.94	155.31	10.47	5.0
HVO	1977	04	22	09	44	00.12	19.32	155.26	10.10	4.0
HVO	1977	06	05	23	42	18.92	19.36	155.08	9.31	5.1
HVO	1977	07	05	07	59	42.03	19.44	155.45	11.89	4.1
HVO	1977	08	07	21	54	20.32	19.33	155.22	10.29	4.1
HVO	1977	08	13	12	24	28.46	20.16	155.61	4.61	4.1
HVO	1977	08	19	08	19	13.34	19.33	155.12	10.15	4.2
HVO	1977	09	07	13	51	06.71	19.38	155.32	31.26	4.5
IIVO	1977	09	15	18	50	05.45	19.34	155.06	9.30	4.0
HVO	1977	09	19	09	01	45.11	19.36	155.13	8.77	4.0
HVO	1977	10	09	14	38	51.90	19.40	155.25	24.90	4.0
HVO	1978	04	07	16	43	43.29	19.87	155.13	39.27	4.0
HVO	1978	06	23	01	47	58.56	19.32	155.26	10.51	4.4
HVO	1978	07	01	09	18	13.27	19.31	155.11	7.97	4.2
HVO	1978	08	31	13	07	20.97	18.98	155.49	38.51	4.3
HVO	1978	09	11	20	16	06.11	19.33	155.11	9.60	4.1
HVO	1978	11	23	03	16	15.88	19.24	155.55	11.40	4.2
HVO	1978	12	14	04	12	45.04	19.31	155.22	10.49	4.1
HVO	1978	12	27	00	40	55.83	19.34	155.22	9.93	4.3
HVO	1979	03	06	05	07	58.54	19.52	155.27	27.43	4.7
HVO	1979	03	10	03	55	14.65	19.33	155.11	9.57	4.5
HVO	1979	03	21	20	46	59.79	20.10	155.84	16.22	4.5
HVO	1979	03	27	21	30	09.80	20.09	155.83	12.31	4.9
HVO	1979	07	31	03	30	51.28	19.47	155.43	11.65	4.3
HVO	1979	08	14	02	51	42.19	20.81	156.29	24.48	4.5
HVO	1979	09	21	21	59	37.62	19.35	155.07	9.19	5.5
HVO	1979	09	21	23	29	12.34	19.35	155.04	9.21	4.3
HVO	1979	09	27	05	35	45.49	19.33	155.12	10.05	4.3

B-1

Appendi	x B.	Page 2	2.							
SOURCE	YEAR	МО	DA	HR	MN	SEC	LAT	LONG	DEPTH (km)	MAGNITUDE (M _L)
HVO HVO HVO	1979 1979 1979	10 10 12	14 30 13	07 19 17	37 35 44	$16.92 \\ 11.68 \\ 03.08$	19.91 19.88 19.41	155.18 156.34 155.41	40.57 00.02 11.44	4.0 4.2 4.0

EXPLANATION FOR REFERENCE COLUMN IN APPENDIX C.

BSSA - Bulletin of the Seismological Society of America

- G-R, 1954 Gutenberg, B., and Richter, C.F., 1954, <u>Seismicity</u> of the Earth and Associated Phenomena, 2d ed., Princeton Univ. Press, Princeton, N.J., 310 p.
- Richter, 1958, <u>Elementary Seismology</u>, W.H. Freeman and Co., San Francisco, 768 p.
- EQHUS U.S. Department of Commerce, NOAA, Records of the Honolulu Observatory, Honolulu, Hawaii.
- HVO L&S U.S. Geological Survey, <u>Hawaiian Volcano Observatory</u> Summary (previously the Volcano Letters and published by the National Park Service), Hawaii Volcano Observatory, Hawaii.
- Monthly Weather Review U.S. Weather Bureau. The general reference to this source is sufficient because earthquakes are described in the issue for the month in which they occured, with few exceptions. Earthquake reports are very complete for the period 1915 to June, 1924.
- ISS, Kew Kew Observatory, <u>International Seismological Summary</u>, 1913 - 1963, Kew, England. This report became the <u>Bulletin of the International Seismological Centre</u> in 1964 and was printed through 1965 at Edinburgh, Scotland.
- USEQ <u>United States Earthquakes</u>. Annual publication of the U.S. Department of Commerce, Coast and Geodetic Survey from 1928 through 1968, the NOAA National Ocean Survey for 1969, and the NOAA Environmental Data Service, 1970.

Note: All times listed by NOAA, 1973 are Hawaiian Standard Time.

YEAR	DATE	TIME	AREA	LAT	LONG	FELT AREA	MAX INT	MAG.	REFERENCES	
1834	2/19		Island of						BSSA v.2, 1912	
			Hawaii							
1838	2/12			10 0	155 5		 V			
1868	4/2	±10:00	S. COast of	19.0	155.5		Λ		BSSA v. 4. 1914	
			Inawall						G-R, 1954	
	- C.								Richter, 1958	
1909	3/13		Island of						EQHUS	
	10/17		Hawaii							
1912	10/15	12.08	Hawall Kilauga arga				V		HVO LES	
1913	10/25	01:28	Kilauea area				v			
1918	11/2	00:03	Mauna Loa				VII			
									ISS, Kew	
									Monthly Weather	
1010	1/28	17.53	Hawaii				V			
1919	8/26	02:34	Island of				v		HVO LES	
1010	0,20		Hawaii							
1919	9/14	17:50	Kilauea				VII		ISS, Kew	
									HVO LES	
1923	1/14	02:58	Island of						ISS, Kew	
1023	2/0	21.11	nawa11							
1923	12/14	06:04	- 11							
1923	12/25	19:16	Hawaii							
1924	8/20	06:50	Island of							
	- 10		Hawaii							
1925	7/8	06:15								
1926	2/28	27.03								
1920	4/22	25.05	Mauna Loa							
1926	6/9	10:05	Island of							
			Hawaii							
1927	3/20	05:22	11							
1927	8/3	10:12								5
1929	9/28	07:40	Hilo, Hawaii				VII		USEQ	2
									I	

Appendix C. Earthquakes of intensity V or greater in NOAA (1973) not listed in Appendix A or B.

YEAR	DATE	TIME	AREA	LAT	LONG	FELT AREA	MAX INT	MAG.	REFERENCES	
1930	5/20	19:22	Hualalai area				V		USEQ	
1930	5/25	20:47	Kilauea				V			
1931	1/30	00:08	Wajohinu				V			
1933	12/2	06:30	Hilo				VI			
1934	5/10	10:39	near Hakalau	19.6	155.4		V		u - 2016 - 101	
1935	1/2	07:17	Kilauea	19.4	155.3		V			
1935	6/28	09:30	Mauna Loa	19.6	155.2		V			
1935	9/30	23:06	11	19.4	155.7		ν.		π	
1935	10/1	00:28	· · ·	19.6	155.4		V			
1935	11/21	01:41		19.5	155.5		V			
1936	4/15	08:57	Kilauea	19.4	155.2		V		"	
1938	2/17	02:48	Mauna Loa	19.6	155.4		V		"	
1939	5/15	10:58	Kilauea	19.4	155.1		V		"	
1939	5/23	14:44	Kilauea	19.5	155.4		V			
1939	5/24	13:29	"	19.4	155.2		V			
1939	5/31	21:21		19.6	155.2		V		"	
1939	6/12	01:41	Kau Desert,				v		"	
			Hawaii							
1939	7/14	04:21	Kilauea	19.3	155.1		V			
1940	9/1	22:45	N. of Island	21.0	155.3		V		"	
			of Hawaii						G-R, 1954	
1941	11/6	10:11	near Waimea				V		USEQ	
1941	11/18	03:26	"				V			
1941	11/22	21:53					V			
1943	11/10	16:52	southern				VI			
			Hawaii							
1944	11/12	05:26	SW of				V			
			Halemaumau							
1945	3/4	00:00	Mauna Loa				V			
1945	5/19	01:48					V			
1945	9/19	05:33	Saddle area,				V			
1.1			Hawaii							
1947	3/19	23:06	Island of				V			
1017	0/70	04.04	Hawall				V		· 11	
1947	9/30	04:04	Maura Las				V			
1949	2/20	15:54	Mauna Loa				V			
1949	5/2	05:02					v		ω	
						······				

Appendix C. Earthquakes of intensity V or greater in NOAA (1973) not listed in Appendix A or B.

YEAR DATE TIME AREA LAT LONG FELT AREA MAX 1XT MAG. REFERENCES 1950 3/25 05:43 Mauna Loa V USEQ 1951 9/16 01:43 Kaoiki fault 19.2 155.5 V " 1952 2/1 10:16 near Kauman V " " 1952 3/17 17:58 off coast of 19.1 155.0 V " " 1952 7/12 13:55 Kona; Hawaii V " " " " 155.5 V " " " " 155.5 V " " " " 155.5 V " " " 1 1 1 1 1										
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	YEAR	DATE	TIME	AREA	LAT	LONG	FELT AREA	MAX INT	MAG.	REFERENCES
1951 9/16 01:43 Kaoiki fault 19.2 155.5 V " 1951 11/8 09:34 Mauna Loa 19.2 155.5 VI " 1952 2/2 01:16 near Kaumana V " 1952 2/12 13:53 Kona, Hawaii V " 1952 7/12 13:53 Kona, Hawaii V " " 1953 1/9 21:10 Mauna Loa 19.4 155.5 V " " 1953 1/15 02:05 " 155.5 V " " " " 155.5 VI " " " 19.5 155.5 VI " " " " " " 19.5 155.5 VI " " " " <td>1950</td> <td>3/25</td> <td>05:43</td> <td>Mauna Loa</td> <td></td> <td></td> <td></td> <td>V</td> <td></td> <td>USEQ</td>	1950	3/25	05:43	Mauna Loa				V		USEQ
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1951	9/16	01:43	Kaoiki fault	19.2	155.5		V		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1951	11/8	09:34	Mauna Loa	19.2	155.5		VI		"
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1952	2/2	01:16	near Kaumana				V		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	1952	3/17	17:58	off coast of	19.1	155.0		V		
1952 7/12 13:53 Kona, Hawaii V " 1953 1/9 21:10 Mauna Loa 19.4 155.5 V " 1953 1/15 02:05 " 19.3 155.4 V " 1953 1/15 02:05 " 19.3 155.4 V " " 1953 8/21 19:47 Hawaii V "		1.1.1.2.3		Hawaii						
1953 1/9 21:10 Mauna Loa 19.4 155.5 V " 1953 8/21 19:47 Hawaii V " 1953 8/21 19:47 Hawaii V " " 1955 8/21 16:02 " VI " " " 1955 8/7 07:18 off N coast 20.5 155.5 V " " 1955 8/14 02:28 Kileuca 19.5 155.5 V " " 1955 8/14 02:28 Kileuca 19.5 155.5 V " " 1955 5/13 21:54 off N coast 20.3 155.3 V " " " 1956 10/16 00:45 W of Hawaii 20 155.4 VI "	1952	7/12	13:53	Kona, Hawaii				V		
1953 1/15 02:105	1953	1/9	21:10	Mauna Loa	19.4	155.5		V		
1953 6/21 19:47 flawal1 20.57 155.5 VI " 1955 3/27 16:02 " VI " " 1955 3/27 16:02 " 19.5 155.5 VI " " 1955 3/7 04:24 " 19.5 155.5 V " " 1955 8/14 02:28 Kileuea 19.5 155.5 V " " 1955 10/26 16:56 near 19.5 155.5 V " " 1956 5/13 21:54 off N coast 20.3 155.3 V " " 1962 10/16 00:45 W of Hawaii 20 157 V " " BSSA v.56, 1966 1962 6/27 18:28 Kaoili fault 19.4 155.4 V	1953	1/15	02:05	Uavaii	19.5	155.4		V		н
1955 3/7 16:02 " 19.5 15.5 VI " 1955 4/1 04:24 " 19.5 155.0 V " " 1955 4/1 04:24 " 19.5 155.0 V " " 1955 8/7 07:18 off N coast 20.5 155.5 V " " " 1955 8/14 02:28 Kileuea 19.5 155.5 V " " " 1955 10/26 16:56 near 19.5 155.5 V " " " 1956 5/13 21:54 off N coast 20.3 155.3 V " <	1955	0/21	19:47	Kilouoo	20 52	155 5		VVI		н
1953 3/21 10:02 " 19.5 155.0 V " 1955 8/7 07:18 off N coast 20.5 155.5 V " " 1955 8/14 02:28 Kileuea 19.5 155.5 V " " 1955 10/26 16:56 near 19.5 155.5 V " " 1956 5/13 21:54 off Hawaii 20.3 155.3 V " " 1956 10/16 00:45 W of Hawaii 20 157 V " " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " " BSSA v.56, 1966 4 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " " BSSA v.56, 1966 4	1954	7/3	11:55	KITAUEA II	20.5:	100.0		VI		11
1955 8/7 07:18 off N coast of Hawaii 20.5 155.5 V " 1955 8/14 02:28 Kileuea 19.5 155.5 V " 1955 10/26 16:56 near 19.5 155.5 V " 1955 5/13 21:54 off N coast of Hawaii 20.3 155.3 V " 1956 5/13 21:54 off N coast of Hawaii 20.3 155.3 V " " 1952 6/27 18:28 Kaoili fault 20 157 V " " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " BSSA v.56, 1966 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " BSSA v.56, 1966 1964 1964 1964 1966 1966 1966 196	1955	A/1	04.24		19 5	155 0		VII		н
1955 8/14 02:28 Kileuea 19.5 155.5 " 1955 10/26 16:56 near 19.5 155.5 V " 1956 5/13 21:54 off N coast 0.3 155.3 V " 1956 5/13 21:54 off N coast 0.3 155.3 V " 1956 10/16 00:45 W of Hawaii 20 157 V " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " BSSA v.56, 1966 VI " BSSA v.56, 1966	1955	8/7	07:18	off N coast	20.5	155.5		v		
1955 8/14 02:28 Kileuea 19.5 155.5 V " 1955 10/26 16:56 near 19.5 155.5 V " 1956 5/13 21:54 off N coast of Hawaii 20.3 155.3 V " 1956 10/16 00:45 W of Hawaii 20 157 V " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " 1962 6/27 18:28 kaoili fault 19.4 155.4 VI " BSSA v.56, 1966 VI " BSSA v.56, 1966 " U U U U	1000			of Hawaii						
1955 10/26 16:56 near 19.5 155.5 V " 1956 5/13 21:54 off N coast off Awaii 20.3 155.3 V " 1956 10/16 00:45 W of Hawaii 20 157 V " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " BSSA v.56, 1966 VI " BSSA v.56, 1966 U	1955	8/14	02:28	Kileuea	19.5	155.5				
1956 5/13 21:54 off N coast of Hawaii 1962 20.3 155.3 V " 1956 10/16 00:45 W of Hawaii Naoili fault 20 157 V " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " BSSA v.56, 1966	1955	10/26	16:56	near	19.5	155.5		V		
1956 5/13 21:54 off N coast of Hawaii 20.3 155.3 V " 1956 10/16 00:45 W of Hawaii 20 157 V " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " 1964 18:28 Kaoili fault 19.4 155.4 VI " BSSA v.56, 1966				Makauweoweo						
1956 10/16 00:45 W of Hawaii 20 157 V " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " BSSA v.56, 1966 VI VI "	1956	5/13	21:54	off N coast	20.3	155.3		V		11
1956 10/16 00:45 W of Hawaii 20 157 V " 1962 6/27 18:28 Kaoili fault 19.4 155.4 VI " BSSA v.56, 1966 Image: state stat				of Hawaii						
1962 6/27 18:28 Kaoili fault 19.4 155.4 VI BSSA v.56, 1966	1956	10/16	00:45	W of Hawall	20	157		V		
BSSA V.50, 1900	1962	6/27	18:28	Kaoili fault	19.4	155.4		V 1		RCCA - F6 1066
										BSSA V.50, 1900
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Appendix C. Earthquakes of intensity V or greater in NOAA (1973) not listed in Appendix A or B.

SEISMIC VOLCANIC RISK ASSESSMENT, PUNA GEOTHERMAL PROSPECT AREA, HAWAII

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David B. Slemmons, George W. Bergantz,

Robert A. Whitney P.O. Box 8877 University Station

Reno, Nevada 89507

for the

SEISMIC RISK ASSESSMENT

and

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for the

VOLCANIC RISK ASSESSMENT

prepared for

THERMAL POWER COMPANY DILLINGHAM AMFAC

October 1981

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PLATES

(in pocket)

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- Plate 2. Epicenter map of earthquakes of $M_L \ge 4.0$ from 1929 to 1980 with focal depths less than about 25 km.

1.0 EXECUTIVE SUMMARY

1.1 Introduction

This report summarizes the geologic, volcanologic, and seismologic data that relate to evaluation of the Seismic-Volcanic Risk Assessment (SVRA) for the Puna Geothermal Prospect (PGP) of the Lower East Rift Zone (LERZ) on the volcano, Kilauea, Hawaii. The basis for the assessment sections is developed in detail in the Geology Section (3.0), with the volcanic and seismic assessments discussed in Sections 4.0 and 5.0, respectively.

The Volcanic Risk Assessment leads to conclusions that the hazards and risk from volcanic activity and associated fissuring and faulting are high and diverse, but the risk to engineered structures and installations can be mitigated by proper procedures in siting and design. Recommendations are made as to the methods and factors that should be considered for mitigation. The Seismic Risk Assessment demonstrates that the hazard and risk from ground motion is of three general sources: frequent low magnitude volcanic earthquakes with epicenters near the site, infrequent earthquakes of deep focus, low to moderate magnitudes and generally from Kilauea, and tectonic earthquakes of about 6.5 to 7.2 magnitude from the Hilina fault zone with epicenters at distances of from 20 to 50 km (12 to 30 mi).

1.2 Volcanic Risk Assessment

The Puna Geothermal Project is sited in one of the most active eruptive centers of one of the most rapidly growing volcanoes in the world. Important eruptions of lava have affected the area in 1750, 1790, 1840, 1955, and 1960.

Evidence from the log of the HGP-A well indicates that, on a

long term basis, an individual site is over-run by lava about once every 900 years, but on a shorter time scale, the frequency is strongly influenced by topography; low areas are covered by flows much more frequently than high areas.

Although eruptions are frequent, they are also quite regular in their behavior and can be predicted with a much higher degree of certainty than is possible in other volcanic regions of the world. Large explosions of ash or pumice are highly unlikely; almost certainly, future eruptions will be like earlier ones, i.e. voluminous discharges of very fluid lava preceded or accompanied by earthquakes and surface deformation.

Future eruptions will be preceded by volcanic and seismic activity in the summit region and by extension and faulting of the ground surface near the site of the eruptive outbreak. They will be accompanied by numerous earthquakes and will form new fissures, avoiding previously active vents in favor of new ground. Fissures will almost certainly be located within the well-defined boundaries of the rift zone. Vents outside that zone are highly unlikely. Fountaining to heights of three or four hundered meters will surrounding region cover the with scoriaceous material, but ejection of explosive debris rarely has a serious effect beyond a few hundred meters from the vent.

The principal volcanic hazards to facilities sited in the East Puna zone are surface rupture, ground motion, and inundation by lava. By comparison, all other hazards are relatively minor. These hazards can be greatly reduced by a modest amount of planning and consideration of a few simple precautions.

If at all possible, permanent installations should not be

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constructed in low areas where lava is likely to be channeled. Old cinder cones and other areas of relatively high ground are unlikely to be over-run within the next four or five decades. Diversion barriers, if well situated and properly constructed, can deflect lava into an alternative course, but they are ineffective as dams opposing the flow of lava directly.

By orienting buildings and other permanent structures with their shortest dimensions parallel to the axis of the rift, the longest effects of ground deformation and surface rupture can be materially reduced.

Close coordination with the Hawaiian Volcano Observatory and the Hawaiian Institute of Geophysics will help ensure timely warnings of impending eruptions.

1.3 Seismic Risk Assessment

The maximum earthquake that is probable for the next 40 year period is an assumed tectonic earthquake from the Hilina fault zone, with an estimated magnitude of 6.75 and an epicentral distance of 25 km (15 miles). An earthquake of this magnitude would have a mean peak horizontal acceleration of about 0.25 g, a mean peak horizontal velocity of 25 cm/sec, and mean peak horizontal displacement of 10 cm, with a duration of more than 0.05 g motion for about 15 to 25 seconds. This strength and duration of motion, is the strongest motion to be expected from a 100 year earthquake of about Ms = 7.2, and is within the range that can be readily mitigated by appropriate design.

The two earthquake hazards that may consitute a risk to future engineering structures and installations are primarily the strong ground motion from tectonic earthquakes, and to a minor

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amount, landsliding, slumping or other secondary ground failures of steep slopes near the epicenter of earthquakes of above 5 magnitude. Surface faulting may occur in the site area in response to volcanic related activity, as is discussed in the volcanic risk assessment section of the report. Other seismic hazards and risks, including liquefaction, tsunamis and seiches are considered to be unimportant for this siting area.