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Article

A Two-Temperature Open-Source CFD Model for Hypersonic Reacting Flows, Part Two: Multi-Dimensional Analysis [†]

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Abstract: *hy2Foam* is a newly-coded open-source two-temperature computational fluid dynamics (CFD) solver that has previously been validated for zero-dimensional test cases. It aims at (1) giving open-source access to a state-of-the-art hypersonic CFD solver to students and researchers; and (2) providing a foundation for a future hybrid CFD-DSMC (direct simulation Monte Carlo) code within the OpenFOAM framework. This paper focuses on the multi-dimensional verification of *hy2Foam* and firstly describes the different models implemented. In conjunction with employing the coupled vibration-dissociation-vibration (CVDV) chemistry–vibration model, novel use is made of the quantum-kinetic (QK) rates in a CFD solver. *hy2Foam* has been shown to produce results in good agreement with previously published data for a Mach 11 nitrogen flow over a blunted cone and with the *dsmcFoam* code for a Mach 20 cylinder flow for a binary reacting mixture. This latter case scenario provides a useful basis for other codes to compare against.

Keywords: hypersonics; computational fluid dynamics; two-temperature solver; OpenFOAM; verification; direct simulation Monte Carlo

1. Introduction

The Knudsen number, defined as the ratio of the mean free path of the gas particles to the characteristic length of the problem, is commonly employed to gauge the degree of rarefaction of a gas. During the entry of a planetary atmosphere at hypervelocities, a craft will traverse the full range of the Knudsen number, from the free-molecular regime down to the continuum regime. Practically, this translates into the need for different numerical techniques to resolve the flow-field past such hypersonic bodies.

The direct simulation Monte Carlo (DSMC) method developed by Bird [1] is a particle-based methodology that is particularly well-suited for computing high Knudsen number flows, typically above 0.05, while the conventional computational fluid dynamics (CFD) approach that solves the Navier–Stokes–Fourier (NSF) equations is generally adopted for the lower range, below 0.005. In between lies an intermediate zone where DSMC is computationally prohibitive and where

conventional CFD fails due to the presence of non-continuum regions within the flow-field. To extend the range of applicability of the NSF equations towards the continuum–transition regime, Park formulated the two-temperature CFD model [2], thus distinguishing the trans-rotational energy pool from the vibro-electronic energy pools and modelling the energy exchange processes via vibrational rate equations.

Open-source solvers dedicated to the study of the hypersonic regime are very scarce. Among such codes are *hy2Foam* and *dsmcFoam*. *hy2Foam* [3] is a new two-temperature CFD solver developed at the University of Strathclyde [4,5] within the framework of the open-source CFD platform OpenFOAM [6]. It aims at (1) giving open-source access to a state-of-the-art hypersonic CFD solver to students and researchers; and (2) providing a foundation for a future hybrid CFD-DSMC code [7].

For rarefied gas flow environments, OpenFOAM possesses a DSMC solver called *dsmcFoam* that has been developed and validated at the same University [8,9]. The two main features of *dsmcFoam* are that vibrational-translational post-collision energy redistribution is executed using a quantum version of the Larsen–Borgnakke procedure [8,10] and that chemical reactions are described by Quantum-Kinetic (QK) theory, as initially proposed by Bird [11].

The primary objective of this paper concerns the verification and validation of *hy2Foam* for multi-dimensional case scenarios. The secondary goal is the assessment, for a two-dimensional gas flow, of one of the conclusions formulated in [5], namely that the combination of a particular chemistry–vibration model with chemical rates derived from QK theory provides a satisfactory consistency between the CFD and DSMC codes.

2. Methodology

This section essentially describes the state-of-the-art numerical procedures that have been implemented in *hy2Foam* to solve hypervelocity flow-fields in near-thermal equilibrium.

2.1. Non-Equilibrium Navier–Stokes–Fourier Equations

The computation of transient hypersonic reacting flows in the continuum regime traditionally employs the non-equilibrium Navier–Stokes–Fourier (NSF) equations. These are shown below in flux–divergence form using a Cartesian coordinate system for a mixture composed of N_s species, including N_m molecules [12]:

$$\frac{\partial \mathcal{U}}{\partial t} + \frac{\partial (\mathcal{F}_{i,inv} - \mathcal{F}_{i,vis})}{\partial x_i} = \dot{\mathcal{W}}. \quad (1)$$

The vector of conserved quantities, \mathcal{U} , is defined as

$$\mathcal{U} = (\rho, \rho_s, \rho u, \rho v, \rho w, E_{ve,m}, E)^T, \quad s \in N_s, m \in N_m, \quad (2)$$

where u , v , and w are the components of the velocity vector. ρ is the mass density of the fluid and ρ_s is the partial density of species s . The flux vectors are split into inviscid and viscous contributions and are written as follows:

$$\mathcal{F}_{i,inv} = \begin{pmatrix} \rho u_i \\ \rho_s u_i \\ \rho u_i u + \delta_{i1} p \\ \rho u_i v + \delta_{i2} p \\ \rho u_i w + \delta_{i3} p \\ E_{ve,m} u_i \\ (E + p) u_i \end{pmatrix}, \quad (3)$$

$$\mathcal{F}_{i,vis} = \begin{pmatrix} 0 \\ -\mathcal{J}_{s,i} \\ \tau_{i1} \\ \tau_{i2} \\ \tau_{i3} \\ -q_{ve,i,m} - e_{ve,m} \mathcal{J}_{m,i} \\ \tau_{ij} w^j - q_{tr,i} - q_{ve,i} - \sum_{r \neq e} h_r \mathcal{J}_{r,i} \end{pmatrix}, \tag{4}$$

where the index i refers to one of the three dimensions of space and δ is the Kronecker delta. E and $E_{ve,m}$ represent, respectively, the total energy and the total vibro-electronic energy for molecule m . In the remainder of the article, the index tr denotes the trans-rotational energy mode, ve the vibro-electronic energy mode and e the electron energy mode. h_s is the enthalpy per unit mass of species s , while the pressure, p , is recovered from the partial pressures using Dalton’s law

$$p = \sum_{s \neq e} p_s + p_e = \sum_{s \neq e} (\rho_s R_s T_{tr}) + \rho_e R_e T_{ve,ref}, \tag{5}$$

where R_s is the specific gas constant. Finally, the electron temperature is set to the vibro-electronic temperature of a reference particle, $T_{ve,ref}$.

In Equation (4), τ_{ij} represent the components of the viscous stress tensor, which can be written as follows:

$$\tau_{ij} = \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) + (\lambda + \mu_b) \frac{\partial u_k}{\partial x_k} \delta_{ij}, \tag{6}$$

where μ is the shear viscosity, λ is the second viscosity coefficient, and μ_b is the bulk viscosity. This work assumes that Stokes’ hypothesis is valid, namely that $\mu_b = 0$ and that the shear and second viscosity are not independent quantities but given by the relation $\lambda = -\frac{2}{3} \mu$. In *hy2Foam*, the species shear viscosities can be considered as temperature-independent, or either set to follow Blottner’s formula [13] or a power law. The spatial components of the heat conduction vector are assumed to follow Fourier’s law

$$q_{tr,i} = \sum_s q_{tr,i,s} = \sum_s -\kappa_{tr,s} \frac{\partial T_{tr}}{\partial x_i} \quad \text{for } s \in N_s \setminus \{e\} \tag{7}$$

and

$$q_{ve,i} = \sum_s q_{ve,i,s} = \sum_s -\kappa_{ve,s} \frac{\partial T_{ve,s}}{\partial x_i} \quad \text{for } s \in N_s. \tag{8}$$

The thermal diffusivities $\kappa_{tr,s}$ and $\kappa_{ve,s}$ can be considered as temperature-independent, or set to follow Eucken’s formula [12,14]. Mixture quantities are recovered from species quantities using a mixing rule. The Wilke [15], Gupta [16], and Armaly and Sutton [17] mixing rules have been implemented, and the latter one is being used in this work, as recommended in the review of Palmer and Wright [18].

The diffusion fluxes, $\mathcal{J}_{s,i}$, are governed by Fick’s law with a correction term to ensure mass conservation [19]

$$\begin{aligned} \mathcal{J}_{s,i} &= \mathcal{I}_{s,i} - Y_s \sum_{r \neq e} I_{r,i} && \text{for } s, r \in N_s \setminus \{e\}, \\ &= \mathcal{M}_e \sum_{r \neq e} \frac{\mathcal{C}_r \times \mathcal{J}_{r,i}}{\mathcal{M}_r} && \text{otherwise,} \end{aligned} \tag{9}$$

with

$$\mathcal{I}_{s,i} = -\rho \mathcal{D}_s \frac{\partial Y_s}{\partial x_i}, \quad (10)$$

where Y is the mass-fraction and with the effective diffusion coefficient of species s in the mixture defined as [20]

$$\mathcal{D}_s = (1 - X_s) \left(\sum_{r \neq s} \frac{X_r}{\mathcal{D}_{s,r}} \right)^{-1} \quad \text{for } s, r \in N_s \setminus \{e\}, \quad (11)$$

in which X is the molar-fraction, \mathcal{C}_r represents the charge of species r and \mathcal{M} is the molecular weight. The binary diffusion coefficients, $\mathcal{D}_{s,r}$, are modelled using binary collision integrals $\Delta_{s,r}$ as [21]

$$\mathcal{D}_{s,r} = \frac{k_B T_{tr}}{p \Delta_{s,r}}. \quad (12)$$

Finally, the source term vector, \mathcal{W} , is written as

$$\mathcal{W} = \left(0, \dot{\omega}_s, 0, 0, 0, \dot{\omega}_{v,m}, 0 \right)^T, \quad (13)$$

where $\dot{\omega}_s$ is the net mass production of species s and $\dot{\omega}_{v,m}$, for $m \in N_m$, is defined as follows:

$$\begin{aligned} \dot{\omega}_{v,m} &= Q_{m,v-T} + Q_{m,v-V} + Q_{m,C-V} + Q_{m,e-V}, & \text{if the reference molecule for } e \text{ is not } m, \\ &= Q_{m,v-T} + Q_{m,v-V} + Q_{m,C-V} + Q_{m,e-V} + Q_{h-e} + Q_{e-i} + \mathbf{U} \cdot \nabla p_e & \text{otherwise,} \end{aligned} \quad (14)$$

where \mathbf{U} represents the velocity vector. The meaning of the different vibrational source terms that appear in Equation (14) is given in the subsequent paragraphs.

2.2. Energy Transfers

The decomposition of the total energy, E , as shown in Equation (15), allows the isolation of different energy pools, each of them being described by a specific temperature and exchanging energy with the other pools:

$$E = \frac{1}{2} \rho \sum_i u_i^2 + \sum_{s \neq e} E_{t,s} + \sum_{s \neq e} E_{r,s} + \sum_{s \neq e} E_{v,s} + \sum_{s \neq e} E_{el,s} + E_e + \sum_{s \neq e} \rho_s h_s^\circ. \quad (15)$$

In order of appearance in Equation (15) are the kinetic, translational (index t), rotational (r), vibrational (v), electronic (el), electron (e), and chemical energies. u_i are the spatial components of the velocity vector and h_s° is the standard enthalpy of formation of species s . The relationship between the total energy of a specific mode and the energy per unit mass of species s is given in Equation (16) for the electronic energy mode

$$E_{el} = \sum_{s \neq e} E_{el,s} = \sum_{s \neq e} \rho_s e_{el,s} \quad (16)$$

and the different energies per unit mass of species are detailed below for each mode:

$$e_t = \frac{3}{2} R_s T_{tr}, \quad (17)$$

$$e_r = R_s T_{tr}, \quad (18)$$

$$e_{v,s} = R_s \frac{\theta_{v,s}}{\exp\left(\frac{\theta_{v,s}}{T_{ve,s}}\right) - 1}, \quad (19)$$

$$e_e = R_e T_{ve,ref}, \quad (20)$$

$$e_{el,s} = R_s \frac{\sum_{i=1}^{\infty} g_{i,s} \theta_{el,i,s} \exp(-\theta_{el,i,s}/T_{ve,s})}{\sum_{i=0}^{\infty} g_{i,s} \exp(-\theta_{el,i,s}/T_{ve,s})}. \quad (21)$$

The simple harmonic oscillator model [11] is utilized for the vibrational mode, with $\theta_{v,s}$ being the characteristic vibrational temperature for species s . $\theta_{el,i,s}$ and $g_{i,s}$ are the characteristic electronic temperature and the degeneracy degree of a given electronic state i for species s , respectively. The two-temperature model formulation adopted in *hy2Foam* then consists in rewriting Equation (15) as follows:

$$E = \frac{1}{2}\rho \sum_i u_i^2 + E_{tr} + \sum_{s \neq e} E_{ve,s} + E_e + \sum_{s \neq e} \rho_s h_s^\circ \quad (22)$$

with

$$E_{tr} = E_t + E_r \quad (23)$$

and

$$E_{ve,s} = E_{v,s} + E_{el,s}. \quad (24)$$

The vibrational source terms introduced into the NSF equations in the preceding paragraph are now described in sequence. The energy exchange between the trans-rotational and the vibro–electronic energy modes (V–T), designated by $Q_{m,V-T}$, is dictated by the Landau–Teller equation [22] and may be written as

$$Q_{m,V-T} = \rho_m \frac{\partial e_{ve,m}(T_{ve,m})}{\partial t} = \rho_m \frac{e_{ve,m}(T_{tr}) - e_{ve,m}(T_{ve,m})}{\tau_{m,V-T}} \quad m \in N_m, \quad (25)$$

where $\tau_{m,V-T}$ is the molar-averaged V–T relaxation time. This former quantity is evaluated as the summation of the Millikan and White semi-empirical correlation [23] and Park's correction factor [2], and later denoted as MWP. It becomes

$$\tau_{m,V-T} = \frac{\sum_{s \neq e} X_s}{\sum_{s \neq e} X_s / \tau_{m-s,V-T}} \quad m \in N_m, \quad (26)$$

where X is the species molar-fraction and $\tau_{m-s,V-T}$ is the interspecies relaxation time expressed as

$$\tau_{m-s,V-T} = \frac{1}{p} \exp \left[A_{m,s} \left(T_{tr}^{-1/3} - B_{m,s} \right) - 18.42 \right] + \frac{1}{\bar{c}_m \sigma_{v,m} n_{m,s}} \quad \text{with } p \text{ in atm.} \quad (27)$$

For a given colliding pair (m, s) , the tabulated values of $A_{m,s}$ and $B_{m,s}$ used in this paper can be found in [4]. The collision-limited relaxation time introduced by Park [2] is a function of the average molecular speed, \bar{c}_m , the limited collision cross-section, $\sigma_{v,m}$, and the number density of the colliding pair, $n_{m,s}$.

The second V–T model tested in this work is the SSH theory named after Schwartz, Slawsky, and Herzfeld [24]. The coefficients of this latter model are taken from the work of Thivet [25] and a blended model is created with the MWP formulation for molecule-atom collisions.

Vibrational–vibrational (V–V) energy transfer is denoted by $Q_{m,V-V}$ and modelled according to the formulation given by Knab et al. [26,27], as described in [4]. In Equation (14), Q_{h-e} , $Q_{m,e-V}$, and Q_{e-i} stand for the energy exchange between free-electrons and heavy-particles, free-electrons and the vibrational mode, and the vibrational energy removal due to electron impact ionisation, respectively. They are assumed to be zero in this work. The term in $\mathbf{U} \cdot \nabla p_e$ represents an approximation to the work done on the electrons by the electric field induced by the electron pressure gradient [28]. Finally, the vibro-electronic energy added or removed by chemical reactions to species m , and represented by $Q_{m,C-V}$, is modelled either with the Park TTV model [2] or the coupled vibration-dissociation-vibration (CVDV) model in *hy2Foam* [4].

2.3. Departure from the Continuum Regime

The local gradient-length Knudsen number introduced by Boyd [29] is often used as a breakdown parameter in the literature (e.g., in [30–33]). For a local macroscopic flow quantity ϕ , it is written as

$$Kn_{GLL-\phi} = \frac{\lambda}{\phi} |\nabla \phi|, \quad (28)$$

where λ is the local mean free path of the gas molecules and ϕ can either be the gas density, the temperature, or the magnitude of the velocity vector $|\mathbf{U}|$ (or $\max(|\mathbf{U}|, a)$ in the denominator, where a is the speed of sound for low-speed regions [34]). The degree of local continuum breakdown is then evaluated as the maximum for all of the aforementioned flow quantities

$$Kn_{GLL} = \max(Kn_{GLL-\rho}, Kn_{GLL-T_{tr}}, Kn_{GLL-T_{ve}}, Kn_{GLL-|\mathbf{U}|}), \quad (29)$$

and the regions where the continuum assumption does not hold are identified when Kn_{GLL} exceeds a given breakdown value, Kn_{Br} , typically being taken equal to 0.05. This parameter is key in hybrid CFD-DSMC codes.

3. Results and Discussion

3.1. Mach 11.3 Blunted Cone

In this section, a non-reacting nitrogen flow past a blunted cone is examined at Mach 11.3. The case is composed of a 6.35 mm-radius nose followed by a flat plate forming a 25° angle with the free-stream flow direction and whose streamwise extension is 5 cm. The 2D axisymmetric mesh that has been employed is shown in Figure 1. The structured grid is aligned with the bow shock and consists of 600 by 200 cells. The first spacing at the wall surface is set to 2 μm by default and to 10 μm for comparison purposes.

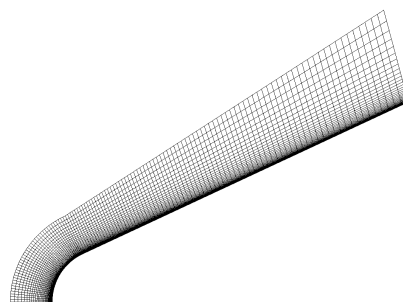


Figure 1. Mesh for the blunted cone (each 5th line is represented in each direction).

The initial conditions of this case scenario are given in Table 1. The free-stream velocity corresponding to a Mach number of 11.3 is 2764.5 m/s. The free-stream temperature and pressure are 144.4 K and 21.9 Pa, respectively. The wall is assumed to be isothermally heated to a temperature of 297.2 K. This simulation uses the MWP formulation for V–T energy exchange and the Blottner and Eucken formulas to compute transport properties. The variable hard sphere model is chosen for the calculation of the mean-free-path and the Knudsen number is computed using the streamwise extent of the cone as the characteristic length. The non-equilibrium boundary conditions employed at the cone surface are the first-order Smoluchowski temperature jump [35] and Maxwell velocity slip [36], with the accommodation coefficients being taken as equal to unity. The set-up for this case can be found in the Supplementary Materials.

The *hy2Foam* solver uses the numerics present in the official OpenFOAM application *rhoCentralFoam* [37], namely the KNP central-upwind schemes of Kurganov, Noelle and Petrova [38]. Hence, *hy2Foam* is first order accurate in time and second order accurate in space. Improving the numerics of the solver to better capture the near-wall region notably is an ongoing area of research. Convergence was achieved after 2.8 h of computations on the ARCHIE-WeSt (Academic and Research Computer Hosting Industry Enterprise in the West of Scotland) High Performance Computer [39]. The run used 24 Intel Xeon X5650 2.66 GHz cores (Santa Clara, CA, USA) with 48 GB RAM and 4xQDR Infiniband Interconnect computer-networking communications.

Table 1. Initial conditions for the Mach 11.3 blunted cone.

Quantity	Value	Unit
Free-stream velocity, U_∞	2764.5	m/s
Free-stream pressure, p_∞	21.9139	Pa
Free-stream density, ρ_∞	5.113×10^{-4}	kg/m ³
Free-stream temperature, T_∞	144.4	K
Free-stream mean-free-path, λ_∞	1.01×10^{-4}	m
Overall Knudsen number, Kn_{ov}	0.002	-
Wall temperature, T_w	297.2	K

This particular configuration has already been studied by Wang and Boyd [40], using the MONACO DSMC code and a Navier–Stokes CFD solver from the University of Michigan. The results from these simulations are reported in the subsequent graphs with the denomination *DSMC: MONACO* and *CFD: Michigan*. Moreover, experimental data is also shown in Figure 2d,f and correspond to the run 31 of the CUBRC (CUBRC Inc., Buffalo, NY, USA) experiments [41].

The emphasis is placed on stagnation line data and then on surface properties such as the pressure coefficient, C_p , friction coefficient, C_f , and Stanton number, St , respectively, given by

$$C_p = \frac{p - p_\infty}{0.5 \rho_\infty U_\infty^2}, \quad (30)$$

$$C_f = \frac{\tau}{0.5 \rho_\infty U_\infty^2}, \quad (31)$$

$$St = \frac{q}{0.5 \rho_\infty U_\infty^3}, \quad (32)$$

those essential aerothermodynamic quantities being shown in Figure 2d–f.

In Figure 2a–c, the pressure, temperature, and velocity stagnation line solutions given by the CFD code of Wang and Boyd are very similar to the ones produced by *hy2Foam*. It can be seen in Figure 2a that the vibrational mode is barely excited for this case scenario. The single-temperature model version of *hy2Foam* gave the same results. The small discrepancies concerning the shock stand-off distance can easily be explained by the difference in grid point density along the symmetry axis (indeed, the spatial extension of the domain normal to the body adopted here is about 40% larger than the one in [40]) and

by the use of a different viscosity model (the power law was used in [40]). As it is the case in most simulations of hypersonic flow-fields, the bow shock thickness given by the NSF equations is clearly under-predicted, as shown by the different DSMC profiles.

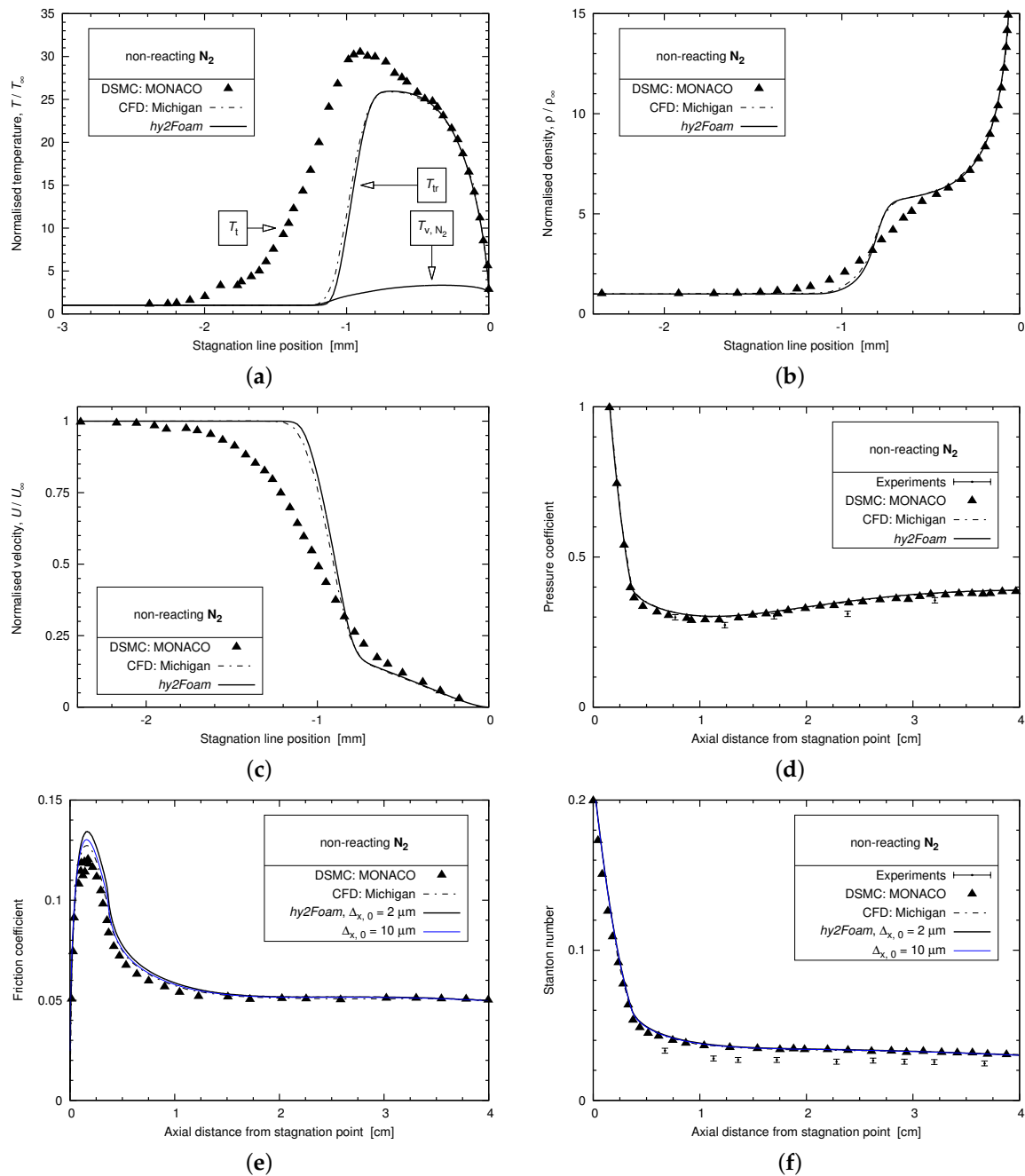


Figure 2. (a–c) Stagnation line profiles, and (d–f) surface quantities along the blunted cone; (a) normalised temperature; (b) normalised mass density; (c) normalised velocity; (d) pressure coefficient; (e) friction coefficient; (f) Stanton number.

Once again in Figure 2d–f, an excellent agreement is found between *hy2Foam* and the Michigan NSF solver as the profiles of the surface quantities are shown to be superimposed with a first spacing of 10 μm . If the mesh is further refined to 2 μm , a small decrease in the Stanton number is observed. In conclusion, it is thought that the mesh used in [40] had a first spacing close to 10 μm .

The variable hard sphere mean-free-path computed by *hy2Foam* in the wall vicinity is of the order of 2 μm . Good DSMC practice dictates that the mean-free-path to cell-size ratio should exceed one so one could argue that the DSMC mesh employed might not be fine enough near the wall to accurately capture the surface aerothermodynamic coefficients along the body, e.g., the peak amplitude of the skin-friction.

Finally, this case is a good illustration that a hypersonic simulation can now be carried out using open-source packages all the way from pre- to post-processing using Gmsh (version 2.11.0) [42] as a mesher, *hy2Foam* as a solver, Paraview [43] (version 4.1.0, Sandia Corporation, Albuquerque, NM, USA and Kitware Inc., Clifton Park, NY, USA) as a visualization utility, and Gnuplot [44] (version 5.0) as a grapher.

3.2. Mach 20 Cylinder

This section focuses on the hypersonic Mach 20 flow of nitrogen over a two-dimensional circular cylinder of radius $R = 1$ m. A symmetry plane exists about the $y = 0$ plane allowing the modelling solely of the upper half of the domain to be considered. The streamwise extent of the computational domain spans from -1.8 m to 5 m and the initial conditions are listed in Table 2.

A free-stream velocity of 6047 $\text{m}\cdot\text{s}^{-1}$ is applied with a free-stream pressure of 0.89 Pa and temperature $T_\infty = 220$ K. Such a temperature is high enough to result in a vibrationally-excited and chemically active flow-field. The cylinder wall is held at a uniform temperature of 1000 K. The overall Knudsen number of 0.0022 lies in the lower range of the continuum-transition regime; however, the gas locally may lie in the transition regime.

Table 2. Initial conditions for the Mach 20 cylinder.

Quantity	Value	Unit
Free-stream velocity, U_∞	6047	m/s
Free-stream pressure, p_∞	0.89	Pa
Free-stream density, ρ_∞	1.363×10^{-5}	kg/m^3
Free-stream temperature, T_∞	220	K
Free-stream mean-free-path, λ_∞	4.45×10^{-3}	m
Overall Knudsen number, Kn_{ov}	0.0022	-
Wall temperature, T_w	1000	K

The mesh used in this investigation is shown in Figure 3 and was constructed using Ansys ICEM (Integrated Computer Engineering and Manufacturing) CFD (Canonsburg, PA, USA) [45]. This mesh consists of 155,000 cells with the first cell spacing at the cylinder wall set to 2 microns. Both Maxwellian velocity slip and Smoluchowski temperature jump boundary conditions were applied at the walls with the accommodation coefficient equal to 1.

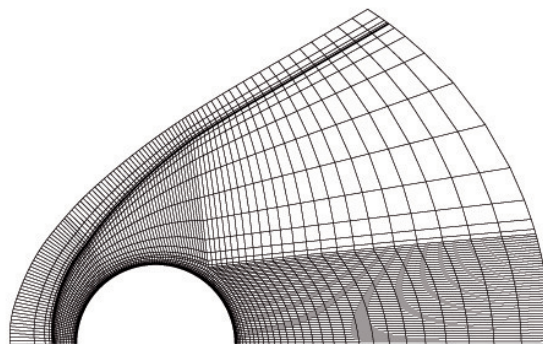


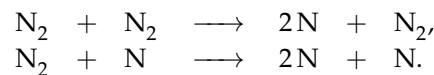
Figure 3. Mesh for the cylinder (each 5th line is represented in each direction).

For the shear viscosity and the thermal conductivity, the Blottner and Eucken formulae were applied, respectively, while the mixing rule employed was that of Armaly and Sutton. Both MWP and SSH formulations are successively used for V–T energy transfer for comparison purposes. The different set-ups are summarised in Table 3 together with a run identification number.

Table 3. Computational fluid dynamics (CFD) simulations performed.

Run Number	V–T Transfer	Electronic Mode	CV Model	Rates
1	MWP	no	CVDV	QK
2	SSH	no	CVDV	QK
3	MWP	no	Park TTv	Park

Two chemical reactions were also considered, these being the irreversible molecule–molecule and molecule–atom dissociation of nitrogen



The Arrhenius rate constants are shown in Table 4 in which the units of A and T_a are given in $\text{m}^3 \cdot \text{mol}^{-1} \cdot \text{s}^{-1}$ and Kelvin, respectively. They are derived from the QK theory [8] and Park’s rates for use in a two-temperature CFD solver [2].

Finally, two configurations associating a chemistry–vibration model with a set of chemical rates have been studied. The first one is called CVDV-QK and has been tested for zero-dimensional heat bath scenarios only [4]. The second configuration, subsequently named Park, is the one conventionally used in hypersonics and combines the Park TTv model with Park’s rates. The set-up for this case can be found in the Supplementary Materials.

Table 4. Parameters for the evaluation of the forward rate constant.

Reaction Rate	Reaction Colliding Partner	Arrhenius Law Constants		
		A	β	T_a
Quantum-Kinetics (QK)	N_2	2.47×10^{18}	−0.62	113,500
	N	6.02×10^{18}	−0.68	113,500
Park	N_2	7.0×10^{21}	−1.6	113,200
	N	3.0×10^{22}	−1.6	113,200

The DSMC configuration is provided in [5], and good DSMC practice was satisfied for both the mesh and time-step. In the DSMC mesh, a total of 5.5 million cells were employed, which were filled with over 80 million equivalent DSMC particles at steady-state. Non-reacting case scenarios were also executed in [5], and the analysis will not be repeated here, although some of the results will be reported in the following graphs and tables.

The departure from local thermodynamic equilibrium is shown in Figure 4a for the CFD run number 2 using the local gradient-length Knudsen number. Dark grey and black colours indicate Kn_{GLL} values beyond 0.05 and cover, as expected, the bow shock and the near-wake areas. Similar results were found for the other runs.

The Mach and trans-rotational temperature fields given by *hy2Foam* and *dsmcFoam* in Figure 4b,c compare well in the compression region, for $x < 0$. In the wake of the cylinder, however, T_{tr} is generally smaller using DSMC. Unlike the non-reacting simulation that demonstrated a good agreement for the vibrational temperature field in the compression area [5], the discrepancies in Figure 4d are much larger this time in the whole domain when compared with DSMC. This can be explained by the application of the QK theory to capture the chemistry–vibration coupling and the use of the quantum

Larsen–Borgnakke method in *dsmcFoam*, which promotes a quicker energy harmonisation in expansion regions (where $T_v > T_{tr}$) as reported in [4] using a zero-dimensional analysis. The Park combination used in run 1 is the instance that provides less accurate results with local vibrational temperatures above 10,000 K.

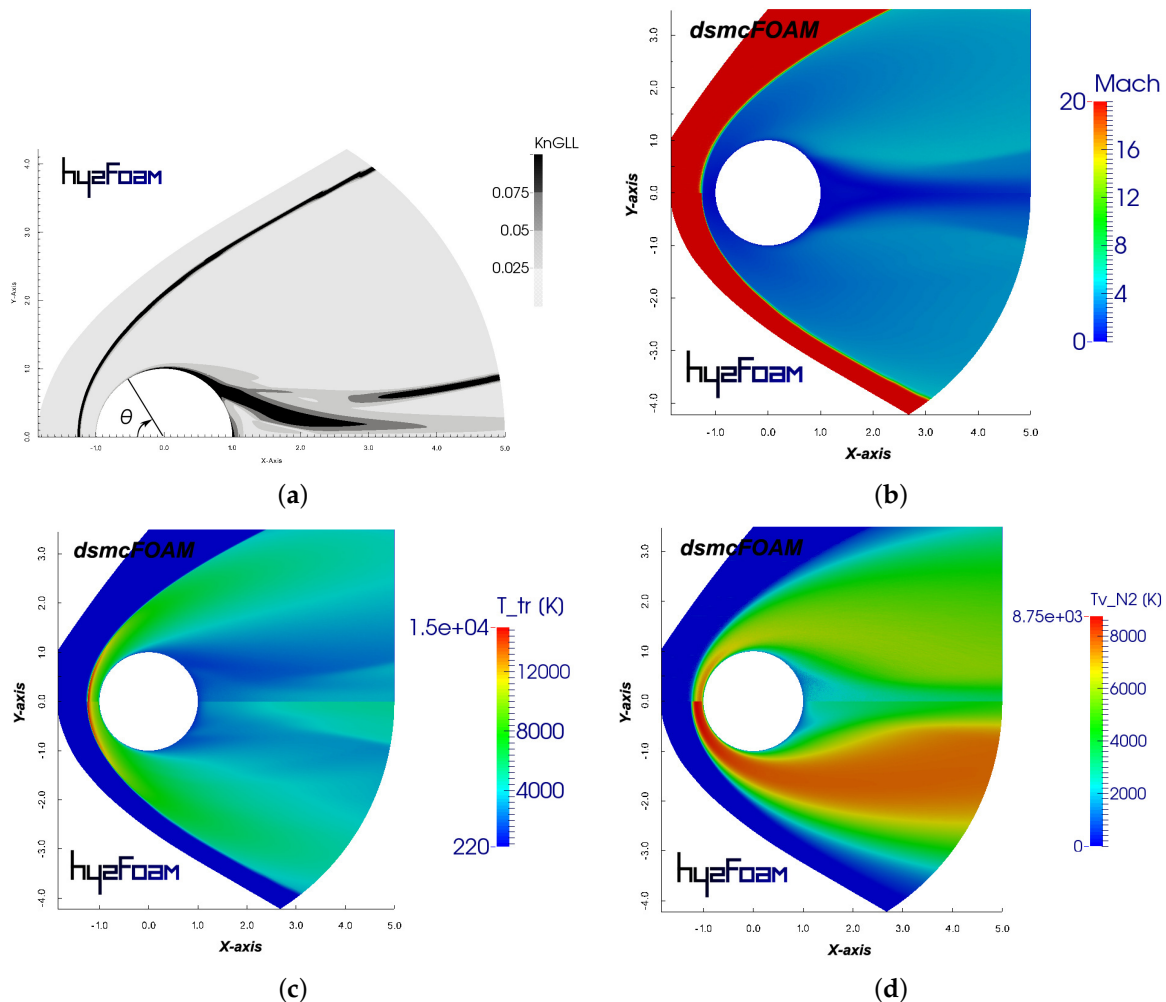


Figure 4. Computational fluid dynamics-direct simulation Monte Carlo (CFD-DSMC) flow-field comparisons for run number 2. In (b–d): the *dsmcFoam* solution is represented in the upper half and the *hy2Foam* solution in the lower half. (a) Local gradient-length Knudsen number; (b) Mach number; (c) trans-rotational temperature; and (d) vibrational temperature.

Figure 5a–c compares the stagnation line profiles of Mach number, temperature, and number density given by *hy2Foam* and *dsmcFoam*. It is normally evident that the bow shock is more diffuse when using the DSMC method compared with CFD. However, it is evident that the shock stand-off distances are almost identical using both solvers and are approximately equal to 0.25 m, which is about 5 cm closer to the body than for the non-reacting case [5]. The peak in trans-rotational temperature is correctly determined using the CVDV–QK combination for both runs 1 and 2 and is slightly over-predicted using the Park combination. As shown previously in Figure 4d, the trend in vibrational temperature shows a steeper increase across the shock wave. In Figure 5c, the evolution of the species number densities for all runs is in satisfactory agreement with *dsmcFoam* outside of the $Kn_{GLL} > 0.01$ band. The early production of atomic nitrogen within the shock is not captured in the CFD solver due to the slight difference in shock thickness prediction.

Surface properties of pressure coefficient, skin friction and heat transfer are shown in Figure 5d–f for both non-reacting (NR) and reacting simulations. There is a reasonable agreement between the CFD and DSMC solvers for C_p and C_f .

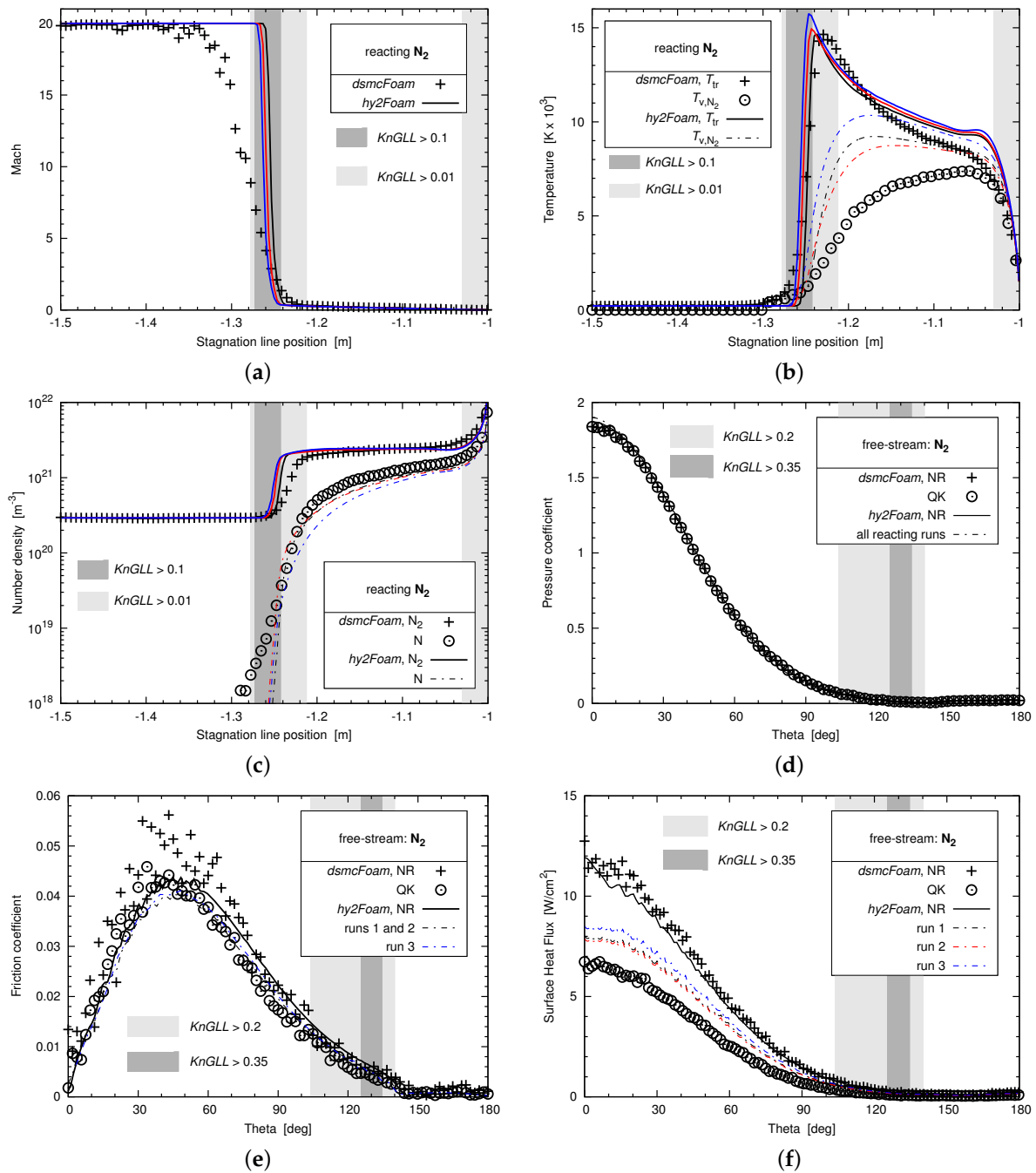


Figure 5. (a–c): Stagnation line profiles. CFD run 1: **black lines**, run 2: **red lines**, run 3: **blue lines**. (d–f): surface quantities around the cylinder. (a) Mach number; (b) temperature; (c) number density; (d) pressure coefficient; (e) skin-friction coefficient; (f) surface heat flux.

The drag coefficient for each simulation is provided in Table 5, and this coefficient estimated by *hy2Foam* represents less than 2% error when compared with *dsmcFoam*, and the reacting environment does not significantly affect its magnitude. In addition, the values of *hy2Foam* and *dsmcFoam* are reasonably close to the one predicted by the Newtonian theory that is 4/3. The integrated heat flux,

C_H , is however showing larger discrepancies between the two codes. There are several factors that could explain this observation: (1) a Kn_{GLL} number greater than 0.1 all around the cylinder; (2) a different treatment of the vibration-translational energy transfer between CFD and DSMC codes; and (3) the use of the KNP numerical schemes in *hy2Foam* that are known for being too dissipative in the near-wall region. It is also shown that the CVDV-QK association is producing a 27% larger integrated heat flux as compared with *dsmcFoam*, while the Park combination overpredicts C_H by 39%.

Table 5. Aerothermodynamic coefficients.

CFD Run Number	C_D		C_H (kW)	
	CFD	DSMC	CFD	DSMC
NR	1.3	1.286	106	115
1	1.302		81.0	
2	1.302	1.284	80.5	63.3
3	1.304		88.1	

C_D is the drag coefficient and C_H represents the integrated heat flux.

4. Conclusions

The newly-coded open-source two-temperature CFD solver *hy2Foam* has been extended to simulate hypersonic multi-dimensional case scenarios. *hy2Foam* has shown to perform as well as a Navier–Stokes CFD solver from the University of Michigan for a Mach 11 blunted cone, and to be in satisfactory agreement with the *dsmcFoam* code for a Mach 20 flow of a binary reacting mixture around a circular cylinder. For this latter case, the aerothermodynamic loads were better estimated using the novel CVDV-QK model combination rather than the conventional Park combination, when compared to the *dsmcFoam* code. This result reaffirms the predictions found using zero-dimensional cases in [4]. Finally, it is considered that the cylinder case scenario presented in this paper provides a useful basis for other codes to compare against.

Future work for the extension of *hy2Foam* will include the development of an 11-species plasma model for application in weakly-ionized flow environments. The discrepancies observed between the CFD and DSMC codes for Kn_{GLL} numbers outwith the continuum regime will motivate the development of an open-source hypersonic hybrid hydrodynamic-molecular gas flow solver using both the *dsmcFoam* and *hy2Foam* codes [7].

Supplementary Materials: The following are available online at www.mdpi.com/2226-4310/3/4/45/s1.

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