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1	Flow-induced Crystallization of Long Chain
2	Aliphatic Polyamides under a Complex Flow
3	Field: Inverted Anisotropic Structure and
4	Formation Mechanism
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## 12 Abstract

The present work deals with the flow-induced multiple orientations and crystallization structure of polymer melts under a complex flow field. This complex flow field is characteristic of the consistent coupling of extensional "pulse" and closely followed shear flow in a narrow channel. Utilizing an ingenious combination of an advanced micro-injection device and long chain aliphatic polyamides (LCPA), the flow-induced crystallization morphology was well preserved for ex-situ 19 synchrotron micro-focused wide angle X-ray scattering (µWAXS) as well as small angle X-ray scattering (SAXS). An inverted anisotropic crystallization structure was 20 21 observed in two directions: perpendicular and parallel to the flow direction (FD). The 22 novel anisotropic morphology implies the occurrence of wall slip and "global" 23 fountain flow under the complex flow field. The mechanism of structure formation is 24 elucidated in detail. The experimental results clearly indicate that the effect of extensional pulse on the polymer melt is restrained and further diminished due to 25 26 either the transverse tumble of fountain flow or the rapid retraction of stretched high 27 molecular weight tails. However, the residual shish-kebab structures in the core layer 28 of the far-end of channel suggest that the effect of extensional pulse should be 29 considered in the small-scaled geometries or under the high strain rate condition.

## 30 1. Introduction

31 Flow-induced crystallization (FIC) of polymer melts is a fundamental issue of 32 polymer physics. It is of clear theoretical significance, and very important in practical 33 applications. Developing specific flow condition by using delicate flow geometries is an important method through which the cause-effect relationship among 34 35 polymer-surface interactions, melt flow behavior and subsequent crystallization can be investigated. However, most studies of experimental protocols reported in these 36 literatures involve only shear [1-8] or extensional flow [9-13], rather than complex 37 flow field. The main reason might be perceived experimental difficulties and a lack of 38

39 correlation between molecular orientation and non-Newtonian flow behavior under 40 complex flow field. Although computer simulations provide many valuable 41 information of system on a macroscopic scale [14], i.e. flow pattern, viscosity, stress 42 profile, etc., there is still the need for probing the microscopic picture of flow 43 behavior under complex flow field as well as its effect on crystallization of polymers.

44 One of the most prominent industrial flow field is the consistent coupling of and closely following shear flow. For example, 45 extensional "pulse" in injection-moulding processes, polymer melts usually experience short-term 46 47 extensional effect caused by converging flow at the sprue entrance, then flow rapidly into the rather colder mould and solidify while subjected wall shear stress. Early 48 49 experiments suggested that the transient extensional effect is important during the 50 very early stage before the fully development of laminar shear flow [15]. Nevertheless, 51 most researchers tend to consider that the FIC in filling channel is dominated by shear 52 effect solely. While in some cases, the effect of so-called fountain flow, a two 53 dimensional flow restricted to a small region of the flow front, is also suggested 54 [16-18]. However, several phenomena in this widespread process have not been 55 sufficiently recognized. First, if one wants to reproduce the condition that polymer 56 experience during the industrial processes, how to deal with the non-isothermal nature 57 of those complex flow geometries, especially the temperature gradient between two 58 flow patterns, will become a very delicate task. Second, if converging flow is

59 generally referred to as a "strong" flow, which would generate considerable chain stretching conditions [19, 20], then why its contribution is not being valued. Indeed, 60 61 the relaxation of oriented or stretched polymer chains might not allow the effect of 62 extensional pulse to be observed in the final products. However, nowadays, the desire 63 for high productivity in the industry makes the strain rate of processing grow by leaps 64 and bounds. The effect of extensional pulse might not keep invisible anymore. Third, 65 as the demand of micro or sub-micro components is rising rapidly, it is very necessary to consider the potential deviation of flow behavior from the typical shear field in 66 67 those small-scaled geometries.

68 To explore the crystallization of polymer melt in the extensional-shear-coupled 69 flow filed, a simple case is studied in this work. Through a short entrance polymer 70 melts are jetted into a thin and straight-walled channel, and subsequently crystallize 71 under wall shear stress. An advanced micro-injection device was employed as a 72 protocol to introduce this complex flow field. By applying the sprue-less design, the 73 injection nozzle is in direct contact with a thin cavity. Flow visualization techniques 74 showed that the transient extensional pulse occurs as the converging flow at the 75 junction between the nozzle and the cavity, while the shear flow closely follows in the 76 rest part of cavity [22]. As the cavity size decreases, several effects are promoted to 77 help further understand FIC behavior under the complex flow field [21, 22]: (i) a 78 considerably high strain rates can be imposed to secure the strong chain stretching condition; (ii) the heat transfer becomes more efficient, thus an isothermal condition
can be applied on the shear pureion; (iii) converging flow and shear flow are strongly
coupled, since there is no room for radical free-surface flow (i.e. flow with zero
lateral-stress).

83 Another question is the applicable polymer system. To deal with the non-isothermal 84 condition, it is very important to use a polymer which can respond quickly to the processing history it experiences. To preserve the effect of flow condition, it should 85 also have rather slow relaxation dynamics. In addition, the chain stretching condition 86 87 of this polymer should be able to be quantitatively described. Based on those 88 considerations, long chain aliphatic polyamides (LCPA) are introduced. By 89 incorporating long alkane segments - typically more than ten methylene groups and 90 hence diluting the amide linkages, LCPA serve as the example of a polymer 91 possessing intrinsic flexibility and strong intermolecular interaction simultaneously 92 [23]. Generally, at temperatures well above the melting point, the hydrogen bonds 93 between the molecules of LCPA are weakened (both in terms of individual bond 94 strength and total number), which leads to the exhibition of flexibility. Rheological 95 models, such as the Doi-Edwards model, are applicable in this case. On the other side, 96 when LCPA are cooled back towards the melting point, the strong chain interaction 97 reconstructs again to affect the relaxation behavior and, most importantly, fasten 98 crystallization dynamics [24]. The efficient heat transfer of experimental protocols

99 and special feature of LCPA could result in well-recorded crystallization morphology. 100 Hence, it is possible and convenient to ex-situ probe the flow-induced hierarchical 101 crystallization structure. In this work, synchrotron micro-focused wide angle X-ray 102 scattering (µWAXS) as well as small-angle X-ray scattering (SAXS) were used. The 103 microscopic morphology can be spatially resolved directly using high-resolution scanning diffractometry of µWAXS [25, 26]. Those methods require little sample 104 preparation and thus diminish the risk of introducing artifacts [26, 27]. In combination 105 106 with vastly exiting information, FIC behavior under complex flow field can be 107 understand more thoroughly.

108 **2. Experimental** 

## 109 2.1 Materials and sample preparation

110 The additive-free PA1012 was produced from bio-fermenting sources (Shandong 111 Guangyin New Materials Co. Ltd, Zibo, China). The melting point was 189 °C 112 determined by differential scanning calorimeter with heating rate of 10 °C/min. The 113 melt flow index was 0.72 g/10min at 235 °C using 2.16 kg as loading. Since PA1012 114 has very similar molecular structure and physics properties to PA1212, the 115 weight-average molecular weight  $(\overline{M}_{w})$  of PA1012 was thus characterized by the empirical equation  $[\eta] = 6.54 \times 10^{-2} \overline{M}_{w}^{0.70}$  for polyamide 1212 as reference. The 116 molecular weight  $\overline{M}_{u}$  of PA1012 was 265 kg/mol, where the intrinsic viscosity ([ $\eta$ ]) 117

118 was 409.3 mL/g using m-cresol as the solvent. The molecular chain length of PA1012

119 with this  $\overline{M}_{w}$  is long enough to form ordering structures.

120 Fig. 1 shows how temperature exercises influence upon the relaxation behavior of 121 PA1012 melts. At short relaxation times, G(t) changes little in a broad temperature 122 range, which indicates the global configuration of the chain as well as stiffness of a 123 single chain is less affected at temperature above the melting temperature, T<sub>m</sub>. While at long times, G(t) is explored into the terminal relaxation regime above 230 °C but 124 125 into the plateau regime at 210 °C and 190 °C. The reconstruction and strength increase 126 of hydrogen bonding at lower temperature give rise to a sudden leap of physical 127 entanglement points leading to the slow relaxation dynamics of large motion units.



128

129 Fig. 1. Apparent stress relaxation modulus,  $G(t) = \sigma(t)/\gamma$ , plotted logarithmically 130 against time for PA1012 at different temperature. The value of strain  $\gamma$  is 10% for all 131 experiments.

The sprue-less micro-injection moulding device (Battenfeld Microsystem 50) was used to create the complex extensional-shear-coupled flow filed. The diameter of the nozzle was 5 mm. The dimension of followed straight-wall channel was  $20.0 \times 1.5 \times 0.5$  135  $mm^3$  (length direction (LD)  $\times$  width direction (WD)  $\times$  thickness direction (TD)). 136 Converging flow occurred at the junction between nozzle and cavity. Fig. 2 shows the 137 sample for ex-situ investigation and the sites of the flow types adapted from 138 computational fluid dynamics simulation result [22]. The color of sample represents 139 the time scale of arrival flow front. The cavity temperature was set as 80 °C attaining 140 balance between processability and slow relaxation dynamics. The injection rate was 141 100 mm/s. The whole mould filling process would be finished within sub-0.1s. This 142 short processing time scale suggests the mould filling procedure is ahead of the 143 complete solidification of PA1012 at the moulding temperature. The material was 144 melted at 270 °C initially by a rotating screw positioned at a 45° angle. It was pushed 145 by the screw in a very accurate metering chamber. Then, the injection piston jetted the 146 material through the barrel (270  $^{\circ}$ C) and the sprue-less nozzle (250  $^{\circ}$ C) into the cavity. 147 Highly repeatable process control and accurate material dosing were observed during 148 moulding by monitoring shot to shot variation of dosing performance and pressure 149 curves. PA1012 granules were kept in a vacuum oven at 80 °C for 24 h for drying 150 before preparation.

- 151 2.2 Mi
  - 2.2 Micro-focus wide angle X-ray scattering scanning



Fig. 2. Sample for ex-situ probing and the supposed site of the flow types. The scheme of experimental geometry shows the procedure of  $\mu$ WAXS scanning and resultant diffraction patterns (thumbnails). Insert: the actual plaque-shaped sample.

156 The X-ray source for diffractometry was BL15U, the hard X-ray micro-focused 157 beamline at SSRF (Shanghai Synchrotron Radiation Facility). Using a Si/Rh coated K-B mirror-pair, the beam was focused on the sample with a  $3\times3 \ \mu\text{m}^2$  beam size at 158 159 focal position. The sample was mounted on a three-axis motorized translation stage. A 160 standardized line scanning program with the X-ray beam perpendicular to the WD-LD 161 plane was carried out at three different equidistant positions (Fig. 2) marked as 'gate', 'center' and 'end' to investigate the crystal structure and orientation changes both 162 163 perpendicular and parallel to the flow direction (FD). The distance between the end 164 position and the far-end of sample was 100 µm. The step size between each adjacent 165 focus spot was 35 µm hence 43 individual diffraction patterns obained at Gate, Center

166 and End positions separately. Data was collected using a MARCCD detector with an 167 average pixel size of  $79 \times 79 \,\mu\text{m}^2$ . The photon energy was 18 KeV giving a wavelength 168 of 0.688 Å with the sample-to-detector distance of 206.3 mm. The exposure time was 169 1 s. Each diffraction pattern frame was denominated using the initials of scan position 170 plus the number of scan sequence at this position, i.e., frame 1 at gate position would 171 be G1, frame 2 at center position C2, frame 3 at end position E3, etc. Background reduction and automated batch-operation of µWAXS patterns were conducted using 172 173 the Fit2D software package. Self-designed Matlab programs were used to give pattern 174 visualization and plotting.

175 The phase content for internal comparison within the batches is presented as 176 crystallinity index ( $\chi_c$ ):

177 
$$\chi_{\rm c} = \frac{A_{\rm c}}{\sum A_{\rm c} + A_{\rm A}} \qquad (1)$$

178 where  $A_c$  is the integrated area of crystalline peaks belonging to a specific crystal 179 phase and  $A_A$  is the integrated area of amorphous halo.

180 The peak deconvolution was performed with the constraint conditions (see 181 **Supporting Information**) and these constraint conditions were necessary to 182 determine the center of amorphous halo and each reflection separately because the 183 amorphous halo and multiple phase signals were combined together in the origin 184 testing data. To fulfill the description of the whole orientation state, the approach 185 derived from Wu and Schultz's [28] was adopted to quantify the mesophase contents.

186 The percentage of the mesophase  $(P_{\text{meso}})$  can be calculated as:

187 
$$P_{\rm meso} = POP - \sum \chi_{\rm c} \qquad (2)$$

188 
$$POP = \frac{\int_{0}^{2\pi} [\int_{S} I(s,\phi) ds - I_{b}(\phi)] d\phi}{\int_{0}^{2\pi} \int_{S} I(s,\phi) ds d\phi}$$
(3)

189 where *POP* is the percentage of oriented phases; *s* is the scattering vector;  $\phi$  is the 190 azimuthal angle;  $I(s,\phi)$  is the background-corrected intensity from the diffraction 191 pattern;  $I_b(\phi)$  is the baseline of the azimuthal intensity profile resulted solely from the 192 integral over a domain *S* of  $I(s,\phi)$ , herein *S* is as the same scattering angular range as 193 the one used in calculating  $\chi_c$ .

To manifestly demonstrate the crystallization structure, as shown in Fig. 3, the xy-coordinate pattern is transformed to polar coordinates with the scattering angle ranging from 8.0 °to 11.4 °and the azimuthal angle from 0 to 360 °.



198 Fig. 3. Demonstration of the regions used for generating the polar coordinate pattern 199 from the xy-coordinate pattern. E and M represent the equatorial and meridian 200 direction, respectively. The definition of azimuthal angle are also shown.

#### 201 2.3 Small angle X-ray scattering

202 SAXS data at gate, center and end position were collected on the BL16B beamline 203 of SSRF. To mitigate against a resolution problem from simultaneous scattering from 204 two different highly oriented layers, the skin layer was blocked (sides) or cut away 205 (top/bottom) deliberately in the SAXS experiments. The focus spot size was  $0.3 \times 0.2$ mm<sup>2</sup>. A radiation wavelength of 1.24Å was applied with the data collected using the 206 207 same type of MARCCD detector as used for the BL15U experiment. Two different 208 sample-to-detector distances, 2074.7 mm and 5088.6 mm, were employed to explore 209 lamellae reflection and central diffuse scattering signal, respectively. The exposure 210 time was 60s and 20s, respectively. According to the reciprocal relationship in 211 scattering, the central diffuse scattering signal from fibrils or shishes would be much 212 larger and more intense in the case of long s-d distance. Thus, to avoid overexposure, 213 shorter exposure time was used for longer s-d distance. In addition, the high vacuum 214 optical path in BL16B ensures that the atmospheric scattering in both cases is greatly 215 eliminated. All SAXS patterns were corrected for background and X-ray fluctuation. 216 To obtain the 1D scattering profile,  $q=4\pi(\sin\theta)/\lambda$  was used, where q is the module of 217 scattering vector;  $\theta$  is one half the scattering angle;  $\lambda$  is the X-ray wavelength.

218 **3. Results and Discussion** 

## 219 *3.1 Determining flow regime of extensional pulse.*

The dimensionless group Weissenberg number (*Wi*) is used to rheology characterize the strength of extensional pulse due to converging flow. In the case of extensional flow at channel entry, two *Wi* related to two different time scale can be expressed as [19, 29]:

224 
$$Wi, \operatorname{rep} = \tau_{\operatorname{rep}} \ln \left[ \left( \frac{R_o}{R_c} \right)^2 \right] \left( \frac{4Q}{\pi R_c^3} \right) \quad (4)$$

225 
$$Wi, s = \tau_s \ln\left[\left(\frac{R_o}{R_c}\right)^2\right]\left(\frac{4Q}{\pi R_c^3}\right) \quad (5)$$

226 where  $\tau_{rep}$  is the reptation time;  $\tau_s$  is the time scale for faster chain retraction (Rouse 227 relaxation time);  $R_0$  is the radius of nozzle;  $R_c$  is the equivalent radius of cavity and 228 the  $R_{\rm C}$  of cavity is 0.455 mm calculated from Huebscher equation.; Q is the 229 volumetric flow rate. The largest reptation time for high molecular weight (HMW) tails,  $\tau_{rep}^{HMW}$ , is the proper choice for  $\tau_{rep}$  due to the crucial role of them in forming 230 231 oriented structure [9, 19, 30] and is estimated as 6s at 250 °C from the relaxation time 232 spectrum (see Supporting Information). According to Doi-Edwards theory [31], the relation between above two relaxation time is  $\tau_s = \tau_{rep}^{HMW}/3Z$ , where Z is the average 233 number of entanglements and  $Z = M_w/M_e$ . The molecular mass between 234 entanglements  $M_{\rm e}$ , calculated from  $M_{\rm e} = \rho RT / G_N^0$ , is 21.7 kg/mol for PA1012 at 250 235 °C, resulting in a Z value of 12. For the rheological description,  $\tau_{rep}$  and  $\tau_s$  are regarded 236 237 as orientation relaxation time and stretch relaxation time, respectively. In the flow 238 regime Wi,rep, Wi,s > 1, a strain rate greater than  $1/\tau_{rep}$  and  $1/\tau_{s}$  indicates the fast flow

239 condition. As a result, chain sections are strongly oriented and the chain conformation 240 becomes similar to that of the crystalline state. The calculated magnitude of Wi, rep is 241 about 5.43×10<sup>5</sup>. Such a large magnitude of  $W_{i}$ , rep guarantees the strong oriented 242 courter path of polymer chains. Moreover, the magnitude of  $W_{i,s}$  following from  $\tau_s$  is 243 considerably larger than 1  $(1.51 \times 10^4)$ , suggesting the polymer chain of HMW is 244 strongly stretched. Hence, the strong extensional flow at nozzle entrance and relative 245 low entanglement density ensure the sufficient stretch of the polymer chains or chain 246 sections to fulfil the formation of oriented nuclei. It is also noticed that the calculated 247 Z value is comparable to the simulation result  $Z \leq 10$  for which the G(t) shows no 248 sign of plateau regime [32]. This is reconciled with the rheology data at 250 °C and 249 thus confirms the reliability of calculation of Wi,s.

#### 250 *3.2 Analysis of crystallization structure*

Fig. 4a shows the first frame collected at the gate position (G1). This diffraction 251 252 pattern is similar to that found in highly oriented polyamide samples [33]. The major 253 difference between this pattern and the one of common highly oriented polyamide is 254 the distinguishable coexistence of  $\alpha$ -phase and  $\beta$ -phase crystals in the present case. 255 Two signals superposed at the inner layer  $(2\theta = 9.11)$  are contributed from the 256 diffraction of both  $\alpha 100$  and  $\beta 100$  planes. Another two signals emerging at outer layers ( $2\theta = 9.95$  ° and 10.43 °, respectively) can be indexed to  $\alpha 010/110$  and  $\beta 020/120$ 257 258 planes, respectively. Since the diffraction arcs are not fully separated, the  $\beta$ -phase is 259 inferred from the relatively greater outer arcing due to the presence of  $\beta 020/120$ 260 diffraction signals [35]. In addition, it can be observed that the reflection maximum

shifts about 7 degree from the equatorial.



262

**Fig. 4.** The wide angle X-ray reflection signals at (a) G1; (b) G2; (c) G3 and (d) G10 in polar coordinates. The graphics to the right represent the corresponding azimuthal intensity profiles. The colored arrows indicate the specific reflection. The  $\beta$ 020/120 profiles marked \* inevitably overlap with  $\alpha$ 010/110 profiles. Oriented  $\beta$ -phase can be observed from the peak around 180 °.

Next to the G1, G2 (Fig. 4b) shows that the  $\alpha 010/110$  planes superposed in G1 have separated into four off-equatorial and intensity-unequal arcs. This pattern formation

270	nevertheless results from, statistically, precessional rotation of uniaxial oriented
271	crystals. The peak position of $\alpha 010$ is split by $\pm 30^{\circ}$ and the $\alpha 110$ by $\pm 18^{\circ}$ about the
272	equator. Using the unit cell for $\alpha$ -phase of PA1012 reported by Jones <i>et al.</i> [36]
273	(a=0.459 nm, b=0.530 nm, c=2.98 nm, $\alpha$ =50°, $\beta$ =77°, $\gamma$ =64°), the ideal reciprocal
274	space angles in the X-ray diffraction patterns from lamellar-crystal mats (taken with
275	X-ray beam parallel to the lamellae surface) can be concluded as follows: the 100
276	should be split by $\pm 5^\circ$ , the 010 by $\pm 38^\circ$ and the 110 by $\pm 33^\circ$ about the either side of
277	equator. The implication of this difference, according to Dreyfuss and Keller's
278	observation in polyamide 66, 610 and 612, accounts for the partial randomization
279	around the a-axis [37]. Because the a-axis is the direction of hydrogen bond
280	progression corresponding with the fastest crystal growth, this pattern is favorably
281	consistent with the structure of $\alpha$ -phase crystals as the incomplete twisting chain-fold
282	lamellae [1, 38]. The separation of $\alpha 010/110$ reflections also makes the shadowed
283	$\beta$ 020/120 signals more apparent in G2. Although the $\alpha$ -phase crystals lose orientation
284	uniformity in at least in one direction, it seems that the orientation state of $\beta$ -phase
285	remains unchanged.

G3 (Fig. 4c) shows very different formations. Two strong peaks at the equatorial are characteristic of  $\beta$ -phases present in both G1 and G2. However, in G3, sharp peaks cannot be found either from the inner layer or from the outer layers, which indicates that there is no  $\beta$ -phase present at this location. Moreover, the disorientation of the

290  $\alpha$ -phase can be observed from the relative larger spreads, particularly along the  $\alpha 100$ 291 arcs. Comparing to X-ray diffraction patterns from lamellar-crystal mats, the intensity 292 differences of  $\alpha$ -phase signals (unequal arcs) also indicate the incomplete twisting of 293 lamellae.



294

Fig. 5. The wide angle X-ray reflection signals at (a) C22; (b) E22 and their intensity profiles. Colored arrows indicate the specific reflection. The  $\beta 020/120$  profiles marked \* have the same meaning with those in Fig. 4.

The  $\beta$ -phase crystals can be seen again at G8 located at about 245  $\mu$ m from the edge of the sample and is present up to G38, which is located at almost the same distance from the opposite edge. Between those two frames, the diffraction patterns clearly 301 present a superposition of arcs from the  $\alpha$ -phase and sharp equatorial reflections from 302 the  $\beta$ -phase, as presented in Fig. 4d, and indicates that while both  $\alpha$ -phase and 303  $\beta$ -phase crystals are uniaxial oriented the  $\beta$ -phase exhibits a more highly oriented 304 state.

305 Crystallization structure changes within the WD at the center and end positions 306 follow similar rules to those seen at the gate position. However, the strong meridian 307 signals found in around the centerline of above two positions, such as C22 and E22 308 (Fig. 5), are clear enough to indicate the evolution tendency of the flow field along the 309 FD. Since the azimuthal intensity distributions of the  $\alpha 100$  reflections and the  $\beta 100$ 310 reflections in samples C22 and E22 remain comparatively unchanged compared to G8, 311 the appearance of the meridian signals cannot be simply interpreted as the ensemble 312 rotation of crystals, but should be still considered as a consequence from a random 313 orientation about the a-axis [1]. If the X-ray is vertical to the fiber axis, a uniformly 314 twisting lamellae, which is equivalent to a completely random state around the a-axis, 315 would generate a pattern with  $\alpha 010$  reflections center on the meridian with spreads 316 decreasing towards the equatorial and the  $\alpha 110$  has the maxima between the meridian and equatorial with decreasing intensity to each direction [37]. Nevertheless the  $\alpha 100$ 317 318 reflection should be less affected by this twisting structure. Similar oriented and 319 twisting texture for  $\alpha$ -phase crystals of polyamides can be found in some spherulites 320 [34] and the transcrystallites growing epitaxially on fibers [39]. In addition, given that

β-phase crystals are highly oriented in both cases, the most possible morphology
represented by C22 and E22 is that α-phase crystals, in a complete twisting mode,
epitaxially grew on the long-range ordered β-phase crystals.

324 *3.3 Analysis of anisotropic structure* 

The so-called skin-core morphology, an anisotropy perpendicular to the FD, is a typical inhomogeneous structure resulted by different regimes of shear flow [19, 40]. Fig. 5 shows the normalized azimuthal intensity scans of different reflections at three positions. The profile data are plotted to a color scale image with full azimuthal angle as the x-axis and real-space scan position as the y-axis. On this basis, three distinct structural layers are identified.



Fig. 6. Normalized azimuthal intensity scans of different reflections (rows) at eachposition (columns). The rows from the top to the bottom represent the overlapped

334  $\alpha 100/\beta 100$  reflections (a, d, g), the  $\alpha 010/110$  reflections (b, e, h) and the  $\beta 020/120$ 335 reflections at gate position (c, f, i), respectively. The columns from the left to the right 336 represent the reflections at gate (a, b, c), center (d, e, f) and end position (g, h, i), 337 respectively. Note the unequal arcs (UA) and meridian signal (MS) emerging in the 338  $\alpha 010/110$  reflections at different positions. The reduction of color contrast along the 339 FD represents the decreasing of overall orientation.

340 The skin layer is the strongest oriented layer containing both  $\alpha$ -phase and  $\beta$ -phase 341 crystals. The skin layer was only found in the first and last one or two frames. As can 342 be inferred from the reflection maximum off-equatorial shifting, the crystals in this 343 layer show a rotational tilting inward toward the cavity center. The next layer, termed 344 "shell layer", features larger spreads in  $\alpha 100$  reflection (Fig. 6a-6c) and arcs with 345 different splitting distance in  $\alpha 010/110$  reflections (Fig. 6d-6f). This interesting texture 346 can be attributed to the disorientation and, more prominently, twisting lamellae of the 347  $\alpha$ -phase as mentioned above. Moreover, the most significant characterization of the 348 shell layer can be made by considering the deficiency of  $\beta 020/120$  signals (Fig. 6g-6i). 349 The thickening of the shell layer along the FD can be thus noticed. The core layer, 350 differing markedly from the conventional parts originated from pure shear flow, is 351 uniformly dominated by a highly oriented structure instead of the widely reported 352 large or deformed spherulites.

353 Another important but often neglected inhomogeneous structure is the structural 354 distribution along the FD. In our case, while the thickness of skin layers remain the 355 same, the reflection signals with both  $\alpha$ -phase and  $\beta$ -phase exhibit maxima on about 356  $\pm 7^{\circ}$ ,  $\pm 6^{\circ}$  and  $\pm 5^{\circ}$  to equatorial for the gate, center and end position, respectively. 357 This suggests a non-parallel and varying orientation direction with respect to the FD 358 as mentioned before. The shell layers increase in depth along the LD while core layer narrows down. For those two inner layers, an expected reduction of overall degree of 359 360 orientation at increasing distance from gate can be observed. However, as can be seen 361 from the shift of reflection maxima (highlighted by white dash dot lines in Fig. 6d-6e 362 and 6g-6h), the crystals of the two inner layers (especially for the shell layer), split by the centerline, tend to tilt outward toward the wall. Notably, this bending direction is 363 364 totally different from that of skin layer. The maximum tilt degree increases with distance from gate to end but decreases with the distance away from the component 365 366 surface.



368 Fig. 7. The crystallinity index as a function of scanning sequence at (a) gate, (b) 369 center, and (c) end. The crystallinity is identified as total  $(\alpha+\beta)$  CI.

370 The change of phase contents (Fig. 7) again suggests above two anisotropies. The 371 maximum crystallinity is always observed in the skin layer at each position but its 372 magnitude is less obvious at the gate position. The changes of  $\alpha$ -phase CI ( $\gamma_{\alpha}$ ) are 373 complicated. For the gate and the center position, the  $\chi_{\alpha}$  in the skin layer is lower than 374 that in the shell and core layers, but for the end position the results show the contrary 375 is true. The  $\beta$ -phase CI ( $\chi_{\beta}$ ) shows similar distribution through the WD at each position but dramatically decreases with distance from the gate towards the end. The 376 377 change of mesophase basically follows the trend of the  $\beta$ -phase, which indicates that 378 the  $\beta$ -phase were formed by crystallization of oriented melts and that relaxation of 379 orientation certainly occurs in the shell layer or in the location away from the nozzle 380 entrance. The sharp boundaries between skin-shell-core layers are contrasted by the abrupt changes of  $\chi_{\beta}$  and the percentage of mesophase. 381



382

**Fig. 8.** (a) The SAXS pattern collected at the center position. The spread lamellae reflection was highlighted by the blue dash dot lines. (b) 1D scattering profile of lamellae reflection with integration sector demonstrated by dark dot lines. To exclude

equatorial streak, regions were integrated from -65 °to -180 °. The cartoon portrays the
origin of lamellae reflection in SAXS patterns.

## 388 *3.4 Molecular origins of anisotropic structure*

389 The SAXS pattern collected at the center position (Fig. 8a) shows an azimuthally 390 narrow equatorial streak and meridian blob-like lamellae reflection. This pattern 391 generally indicates that the presence of oriented shish-kebab structure [27, 41, 42]. 392 Except for those two parts, a rather spread and weak lamellae reflection occurred at 393 larger q can be observed. Figure 8b shows the corresponding lamellae reflection 394 profiles were best fitted by two overlapping peaks. The sharp peak at smaller q is 395 from the lamellar stacks of kebabs [38, 42]. The weak peak belonging to the spread 396 lamellae reflection might be assigned to the "row structure"-those lamellae stacks 397 with smaller long periods and broader orientation distributions [1, 41].



398

**Fig. 9.** (a) From left to right, the SAXS patterns at gate, center and end, respectively.

400 (b)The average length of shish-kebabs (L) and integration breadth defining the 401 disorientation degree  $(B_{eq})$  is calculated using  $q^2 B_{\pi/2}^2(q) = 1/L^2 + q^2 B_{eq}^2$ , where 402  $B_{\pi/2}(q)$  the integration breadth along azimuthal scan at specific is scattering angle. 403 Since the beam size used in SAXS experiments is much larger than that in  $\mu$ WAXS, the SAXS patterns should contain aggregated information from different layers. The 404 405 crystallization morphology in the core layer is represented by shish-kebab structure. 406 This suggestion is based on two above observations: first, the  $\beta$ -phase crystals in the 407 core layer are oriented steadily parallel to the FD and form nuclei from strained melts, 408 which, in smaller structural levels, accords with the fibrous morphology of shish; 409 second, the kebabs themselves could be straight or twisted [38, 43] and possess some 410 degree of freedom to orient with the FD [5], which is only observed in  $\alpha$ -phase. It is 411 most possible that the shish backbone consists of  $\beta$ -phase, while continued growth of 412  $\alpha$ -phase forms kebab structures. Mechanically, this conclusion is reconciled when 413 consider the  $\beta$ -phase crystals adopt a less organized alternative sheet stacking 414 arrangement and thus kinetically promote the formation of shish nuclei from oriented 415 melt, while the  $\alpha$ -phase crystallize in all sheet stacking progressively, which 416 thermodynamically favors folded-chain lamellae. On the other side, for the shell layer, 417 it is prudent to relate the period system formed by incomplete twisting  $\alpha$ -phase 418 crystals to the so-called row structure. Considering the chains and lamellae normals of 419  $\alpha$ -phase crystals are non-parallel, the formation of row structure would be more 420 readily [1].

421 Since an unexpected core layer structure was observed, it's necessary to 422 quantitatively demonstrate changes of shish-kebab structure in the core layer along

423 the FD. A larger sample-to-detector distance was used to investigate such behavior. Fig. 9a shows the SAXS patterns collected at gate, center and end. The length scale 424 425 dimension and orientation state of the shish-kebabs are calculated by Ruland's streak 426 fitting method [43-45]. The results in Fig. 9b show that the average length of the 427 shish-kebabs (L) at the gate is around 250 nm but drastically decreases to only 26 nm 428 at the end position. The disorientation degree, represented by values of  $B_{eq}$ , gradually 429 increases along the FD. This observation suggests that the shish-kebabs are thin and 430 long-range ordered at the gate while discrete and less oriented one at the end. The 431 average length of shish-kebabs at the end is surprisingly small. However, it might 432 make sense in the case of polyamides. Due to the large decrease in free energy on 433 crystallization as a result of the hydrogen bonding, the long period and lamellae 434 thickness for polyamides is only about  $6 \sim 10$  nm and 4 nm, respectively. The value of 435 long period is significantly lower than that for polyethylene or polypropylene, which 436 is in the range 18 to 30 nm depending on crystallization condition. The apparent long 437 period at end position is about 10 nm. Morphologically, the scaffold feature of 438 shish-kebab can be satisfied. In fact, the value of 26 nm is very close to the recent 439 result in which the microshish in the initial stage of scaffold-network nuclei was about 440 30 nm [42]. Considering the shish-kebab structures in end position formed under the 441 extensive relaxation condition, the length value of shish would be reasonable.

442 In addition, two apparent phenomena should also be stressed. One is that the 443 equatorial scattering intensity of center streaks drops faster with distance away from 444 the nozzle entrance, which may be attributed to an increase in interference between 445 the weakly correlated discrete shishes arising from imperfect orientation as well as 446 limited length [46]. The other is that even though the long period of lamellae 447 reflection wouldn't change much, their scattering intensity decreases from gate to end. These two phenomena together indicate that the density of shish-kebabs in the core 448 layer decreases along the FD, which can be confirmed by the WAXS data. Although 449 450 the WAXS deconvolution results cannot fully represent the structural fraction of 451 larger structures, the relative variations indeed reflect the relaxation of long-range 452 order and loss in average orientation along the FD.



**454 Fig. 10.** Schematic illustrations of the crystallization morphology of the 455 skin-shell-core layer structure at different positions within the component. Blue and 456 green stacks represent α-phase crystals and β-phase crystals, respectively. The sheets 457 in β-phase stacks are parallel to lamellae normal while those in straight α-phase stacks 458 are not. The number inside indicate the position of layer border. The scale of lamellae 459 between each layer is not exactly the same.

460 These analyses declare the observation of novel anisotropic structures of PA1012 under the extensional-shear-coupled flow field Fig. 10 shows the schematic 461 illustration demonstrating the molecular origins of this skin-shell-core layer structure 462 463 and its evolution along the FD. Nearing the cavity wall, the crystals in the skin layer 464 show a fibrillar texture. The overall  $(\alpha+\beta)$  crystallinity index remains constant along 465 FD. High proportions of mesophase observed in this layer indicate a broad range of 466 high orientation states. Typically, the molecular chain or lamellae normal lie parallel 467 with the surface of the component in the skin layer and that skin layer will narrow 468 down from the gate to end [47]. However, the preferred oriented axis in this case may 469 bend inward to the inner parts at the gate position and become increasingly parallel to 470 cavity surface away from gate position. Moreover, the obvious thinning of the skin layer in common components originated from pure shear geometry cannot be 471 observed, instead, the orientation regularity of lamellae would further increase at the 472 473 far-end.

474 Finding no trace of  $\beta$ -phase, the next layer, the shell layer, can thus be recognized. The  $\alpha$ -phase crystals in the shell layer exhibit the so-called row structure. This texture 475 476 can be represented by the relative larger spreads of  $\alpha$ -phase reflections and the 477 specific splitting angle of the overlapped  $\alpha 010/110$  [39, 41]. Given the contrasts of 478 azimuthal intensity in this layer are still recognizable even at the end position, the 479 existence of isotropic spherulites is denied. The lowest mesophase contents are observed in the shell layer, which means a large number of stretched chains relaxed 480 481 here. Another notable aspect is that it is observed at the center and end of the 482 component, and that the preferred axis of row structures tends to tilt outward toward 483 the wall (in contrast to the case in the skin layer).

484 As discussed above, the core layer is characterized by the observation of 485 shish-kebab morphology. The shish is composed of  $\beta$ -phase crystals and, necessarily, 486 of mesophase [44, 48], while the  $\alpha$ -phase crystals fall into kebab structures and 487 change from untwisting to complete twisting. The µWAXS and SAXS data together 488 suggest the shish-kebab entities in the core layer shorten in length scale and increase 489 in distribution of orientation along the FD. The evolution of shish-kebabs from gate to 490 end is consistent with the previous investigation [49]: the lower flow rate generates a 491 lower shish density and would enhance the twisting growth of kebabs thereafter.

492 3.5 Analysis of crystallization dynamics under the complex flow filed

493 Although the reduction of overall orientation along the FD is expected, it is still 494 interesting to recognize two inverted anisotropic features compared to components 495 originated from pure shear flow geometry. (i) For the skin layer, thinning or loss of 496 orientation cannot be detected. The bending fibrils structure at the gate position 497 gradually becomes parallel to the cavity wall along the FD. Moreover, the orientation 498 regularity increases further at the far-end of the cavity. (ii) The intermediate layer (identified as "shell layer" in this case) is most often characterized by the fine-grained 499 500 morphology or the shish-kebabs corresponding to different flow or pulse rate rates. 501 While the core layer is isotropic or, at best, deformed spherulites either for macro or 502 micro components [19, 27, 47, 50, 51]. Some special technologies, such as oscillation 503 shear injection molding [50] and gas-assisted injection molding [52] may generate 504 thicker oriented layers, but the regularity that orientation degree consecutively 505 reduces from skin to core remains unchanged. However, a completely opposite is 506 observed in this case: the core layer is dominated by high level of orientation structure 507 whereas the shell layer is not.



509 Fig. 11. Schematic illustration of flow condition and its effect on polymer chain510 sections. (a) Extensional pulse resulting in stretched of HMW tails. (b) Solidified skin

511 is dragged to deform before any debonding occurs. At the end position, strong wall 512 slip results in huge increases in wall shear stress while at the gate position, weak slip 513 only brings about affine deformation. (c) The instantaneous flow geometry of fountain 514 flow in cavity and shear gradient based on previous studies [16-18, 53]. The active 515 area of transverse flow locates near the slip wall where the shear flow emerges. The 516 flow field is separated into two distinguished regions by the red dash lines: the 517 transverse tumble dominant region and retraction dominant region.

The unusual anisotropic crystallization morphology of PA1012 cannot be simply interpreted as the consequence of shear-induced crystallization in different flow regime. Due to the strong coupling between extensional flow and shear flow, the flow patterns deviated from pure shear flow. Most importantly, this deviation was recorded owing to the special combination of material and experimental protocol.

523 As discussed before, HMW tails of PA1012 were strongly stretched due to the 524 severe extension effect at the nozzle entrance (Fig. 11a). Once the melt entered into 525 the cavity, considering the mould temperature, 80 °C, which is close to the glass 526 transition temperature of PA1012, fast solidification (Fig. 11b) would occur at the 527 location near to the cavity wall [54]. However, crystallization was enhanced by the 528 strong stretched polymer chains and, as such, a highly oriented fibrils structure was 529 observed in the skin layer. In addition, because of the high adhesive energy provided 530 by polar amide group, polymer chain of PA1012 would stick to the cavity wall, which

will result in wall slip behavior [55, 56]. The unusual variation trend of the skin layer 531 532 can be attributed to a "strong-to-weak" wall slip effect [55]. Due to the wall slip effect, 533 the thin skin, with one side being adsorbed to the wall, was dragged by the 534 high-velocity flow elements in the center space of cavity. This effect resulted in 535 bending fibrils structure at the gate, which is much like the affine deformation of a 536 rubber network under an external shear field. A similar texture was observed in a 537 study on gas-assisted injection moulding processing in which the central fluid was 538 high pressure gas [52]. As for the end position, since the fluid elements at this 539 position entered the cavity earlier, a larger magnitude of flow velocity would generate 540 a more strong slip in consequence of debonding of polymer-wall interfacial region 541 [55]. Therefore, more regular and less rotationally tilted fibril crystals were observed. 542 Since the external characteristic lengths of geometries reduce enormously compared to the ideal condition, laminar flow would not fully develop after the rapidly 543 544 extensional pulse. The implication is that the flow behavior would be more close to a 545 "global" fountain flow. The fountain effect for polymer generates a localized 546 hydrodynamic phenomenon demonstrated by the complex two-dimensional flow (axial and transverse) [16, 57, 58]. Question on whether fountain flow influences the 547 548 molecular orientation still remains nowadays [59, 60]. Fig. 11c shows the 549 instantaneous flow profile of the fountain flow at the end and gate positions in which 550 fluid elements between the centerline and slip interface would decelerate in the

551 direction of flow and would acquire a transverse velocity spilling outward toward the 552 wall [16, 53, 57]. According to the chain behavior proposed by Chu et al [38, 61, 62], 553 this transverse velocity perpendicular to the flow could bring about hydrodynamic 554 drag forces and tumble effect to coil the stretched chains at an intermediate region 555 near to the wall, for which relaxation might be accelerated. It is most possible that the 556 fast relaxation caused by tumble effect lead to the formation of twisting row structure in the shell layer, since this kind of period structure is favored under intermediate 557 558 strain condition [1]. Referring to the thickness of shell layer, the transvers tumble 559 dominant regions are identified. As highlighted by the red dotted line, the maximum 560 transverse velocity located on the side nearing to slip wall and its active area would be largest at flow front [16, 57]. Considering that, it is convenient to understand the 561 562 sharp shell-core layer border. The higher and wider-area transverse flow at the flow front results in the thicker and less oriented shell layer at end position, and notably, 563 564 the larger tilt of crystals in the shell layer as well as part of the core layer at the far 565 end will be observed.

Although the magnitude of the transverse velocity is much smaller around the centerline, the stretch chains in this region would get through continuous retraction. However, in our case, reconstruction of hydrogen bonding between polymer chains slowed the retraction process of stretched HMW tails, which was enough for the development of shish nuclei in core layer. On the other side, the morphological 571 differences of kebab in core layer could clearly distinguish the different relaxation 572 degree along the FD [38, 49]. One should notice that, even though extensional pulse was sufficiently strong and PA 1012 solidified rapidly, a dramatic decrease of density 573 574 and length of shish at the center and end position could be observed. This suggests, 575 for most cases, the effect of extensional pulse on the polymer melt would be 576 restrained and further diminished along the FD. Hence, it is also very important to know that no observable trend of deformation and orientation phase in core layer 577 578 means zero-stress boundary in the centerline of cavity but does not necessarily mean 579 nothing happens there.

#### 580 **4. Conclusions**

581 A special combination of experimental protocols and polymer system was presented 582 for investigating the flow-induced crystallization of polymer melts under the complex 583 flow field. The line-scan collections of synchrotron µWAXS at three different 584 positions of final component provide a clue to comprehensively assess the 585 crystallization textures and flow behavior of polymer melts. The crystallization 586 structure, multiple orientation and phase contents together indicate a novel inverted 587 anisotropic structure: along the FD, a skin layer showing more regular and less 588 rotational tilted orientation at the far-end of the cavity; perpendicular to the flow, the 589 shell layer showing less oriented twisting row structures consisted of  $\alpha$ -phase crystals 590 only, while the core layer showing shish-kebabs for which the complete twisting

591  $\alpha$ -phase lamellae epitaxially growing on the  $\beta$ -phase shish. These textures were 592 confirmed by small-angle X-ray scattering. The inverted laver structure implies the 593 wall slip and a global fountain flow happened under the complex flow field. Certain 594 question was stressed on whether the fountain flow influences the molecular 595 orientation. The answer seems to be that the fountain flow itself would not enhance 596 the molecular orientation. On the contrary, if polymer chains are sufficiently extended, 597 the transverse tumble of fountain flow would speed up the retraction of oriented 598 chains in intermediate region between skin and core. The quantitative analysis on the 599 shish-kebabs in the core layer suggests the effect of extensional pulse should be valued in the small-scaled geometries or under the high strain rate condition. 600

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