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Use of High Strength Steel for Hydrogen Containment

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Use of High Strength Steel for Hydrogen Containment

Abstract

The research involves experiments on model lab heats of an ultra-high-strength steel (high C, low Ni) and a high-toughness, high-strength steel (high Ni, low C) to determine the limits of toughness as a function of yield strength, grain-boundary purity, and hydrogen fugacity. In addition, the existence and mechanism of brittle intergranular cracking in ideally pure steels is being investigated.

Comments

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Use of High Strength Steel for Hydrogen Containment

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Overview

The research involves experiments on model lab heats of an ultra-high-strength steel (high C, low Ni) and a high-toughness, high-strength steel (high Ni, low C) to determine the limits of toughness as a function of yield strength, grain-boundary purity, and hydrogen fugacity.

In addition, the existence and mechanism of brittle intergranular cracking in ideally pure steels is being investigated.



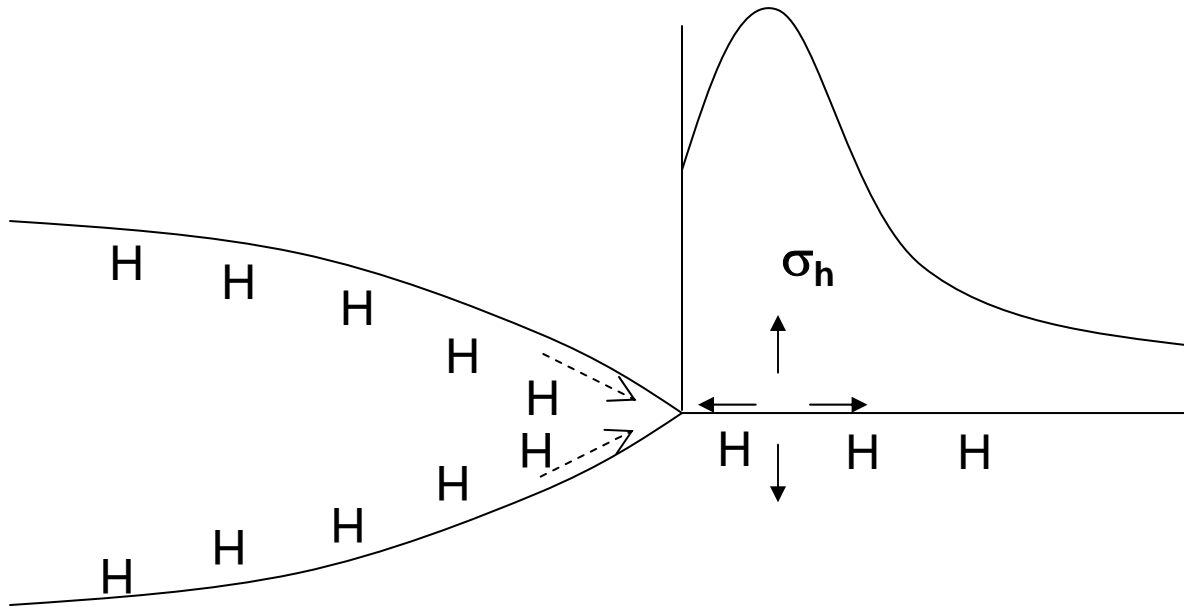
Advantage of steel for tanks and transport

- **Capable of high strength (low mass)**
- **Economical**

Challenge

- **Hydrogen-induced intergranular embrittlement**

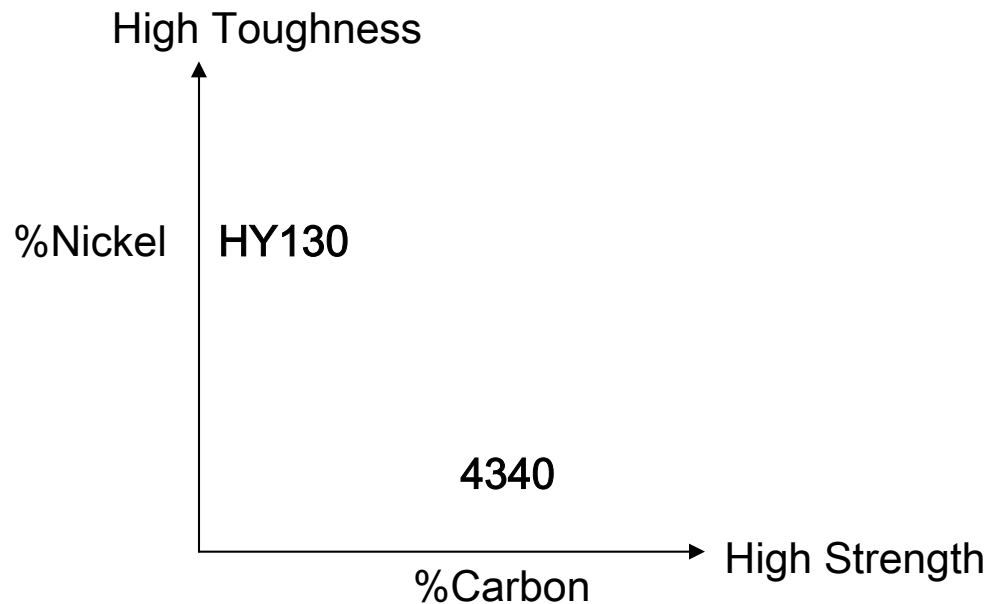
The mechanism



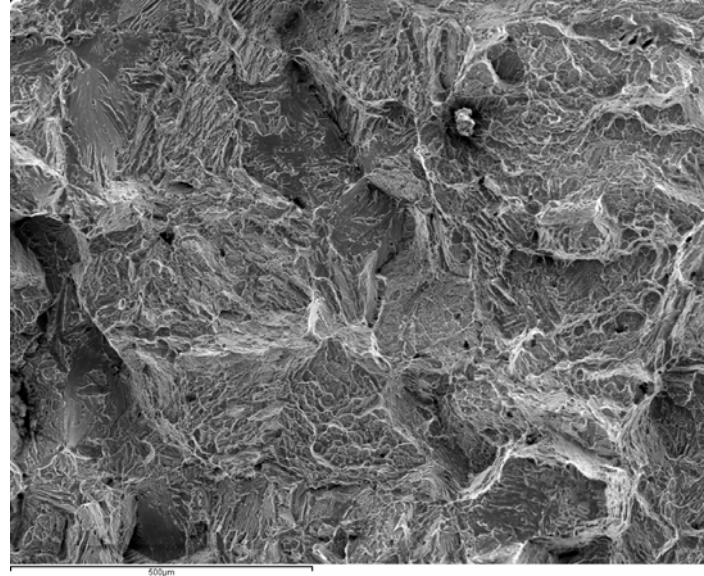
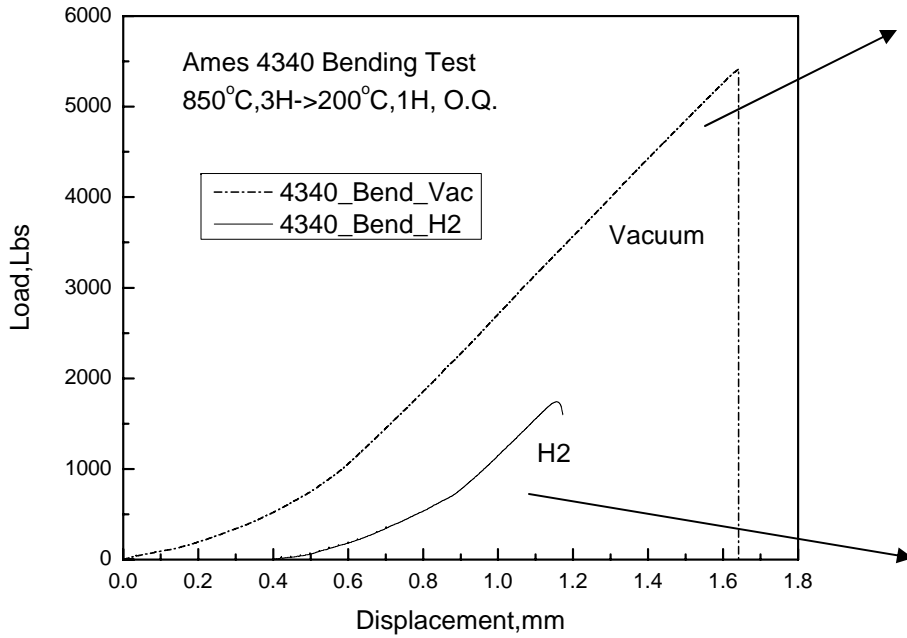
Sharp crack, Nanoscale cracking

Two kinds of steels

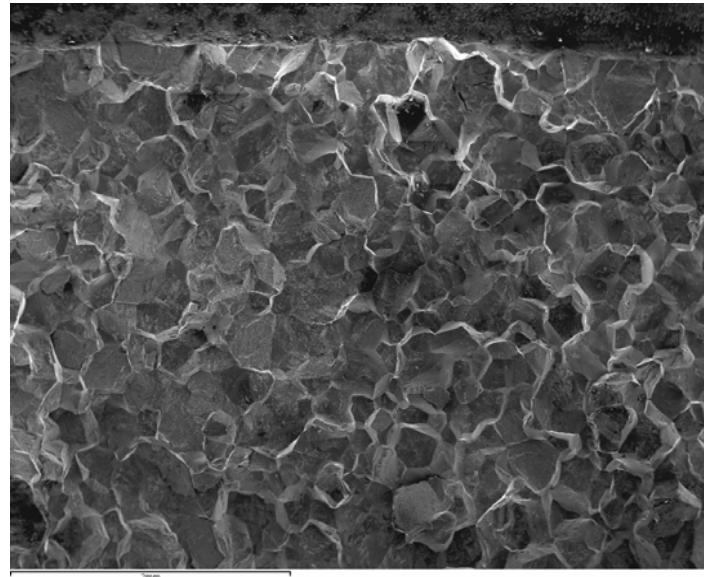
- Inherently High-Strength (4340)
- Inherently High-Toughness (HY130)

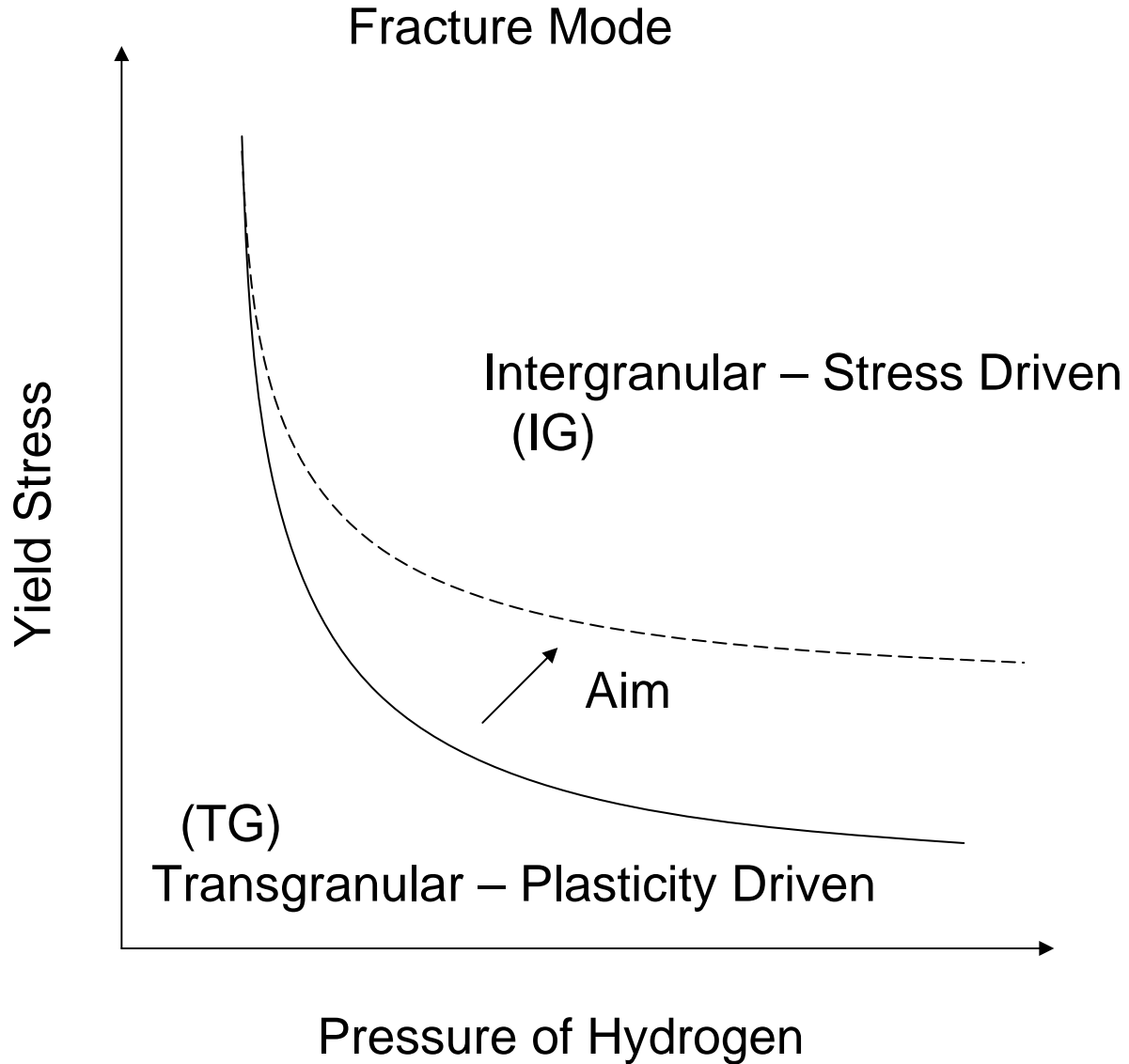
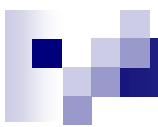


Intergranular (IG)



Transgranular (TG)







Three Controlling Parameters

- Fugacity of hydrogen
- Yield strength of the steel
- Grain-boundary purity (and microstructure?)

- These parameters control the fracture mode of intergranular (IG) and transgranular (TG)

Hydrogen concentration(C_0)
dissolved in lattice under hydrogen pressure (P)

$$C_0 = 0.00185 P^{1/2} \exp(-3440/T)$$

$$C_0 = 10^{-8} \text{ at.fr under } P = 1 \text{ atm.}$$

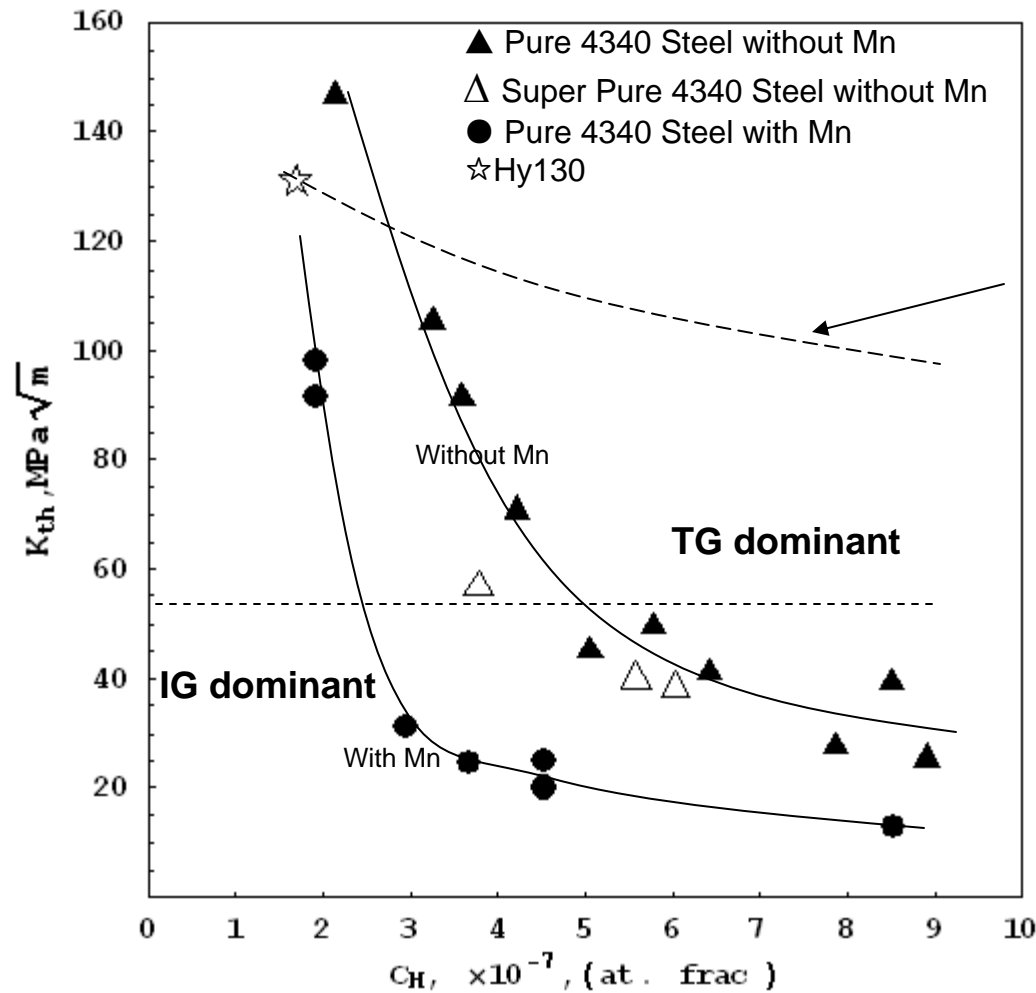
H concentration ahead of a crack tip under
hydrostatic tensile stress (σ_h)

$$C_H = C_0 \exp\left(\frac{\sigma_h V_m}{RT}\right)$$

- $\sigma_h = (\sigma_{11} + \sigma_{22} + \sigma_{33})/3 = 2.42 \sigma_y$
- molar volume of hydrogen in iron: $V_m = 2.1 \times 10^{-6} \text{ m}^3/\text{mole}$

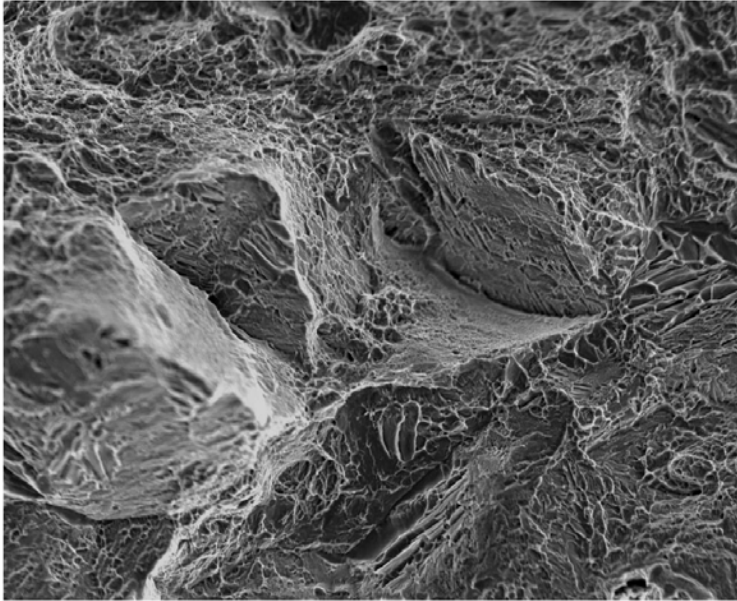
$$C_H = 10^{-6} \text{ at.fr under } \sigma_y = 1750 \text{ MPa } P_{H_2} = 1 \text{ atm}$$

Effect of Purity of High Strength Steel

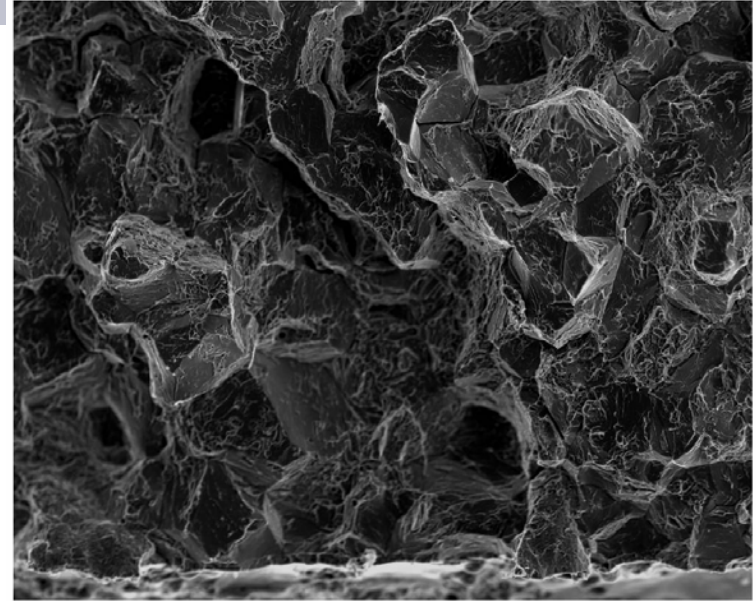


Is this possible?

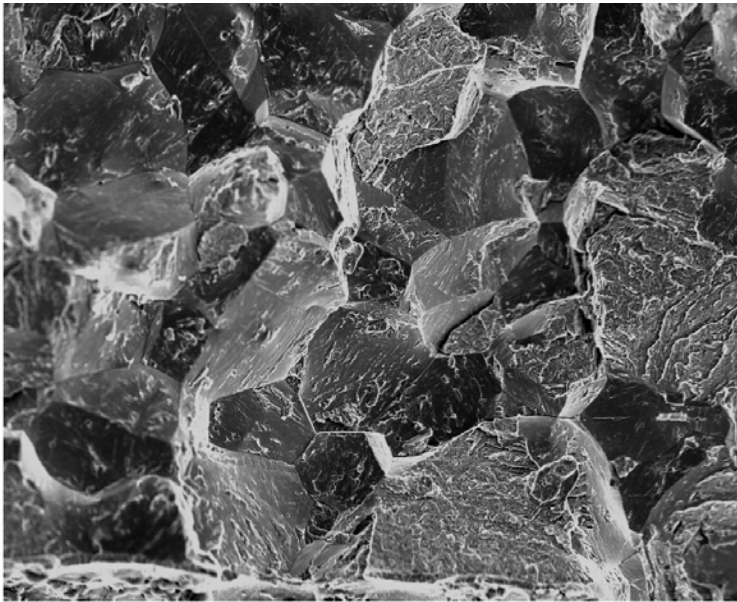
$$C_H = 0.00185 (P_{H_2})^{\frac{1}{2}} \text{Exp}\left(-\frac{Q_s}{RT}\right) \text{Exp}\left(\frac{2.42 \sigma_y V_m}{RT}\right)$$



100µm
V1, Homo ->860 C,1Hour in Vacuum -> 100C,1Hour in Vacuum, Bend test in Vacuum



200µm
A1, Homo ->860 C,1Hour in Vacuum -> 100C,1Hour in Vacuum, Bend test in Air



200µm
H1, Homo ->860 C,1Hour in Vacuum -> 100C,1Hour in Vacuum, Bend test in H2

Even ideally pure grain boundaries are cracked in hydrogen at high strength levels.



Summary and Future Work

- Under low hydrogen fugacity, hydrogen induced cracking (HIC) of ultra-high strength steels grows along grain boundaries regardless of the purity.
- High-strength/high-toughness steel shows excellent resistance to HIC under low hydrogen pressure.
- To determine the limit of hydrogen fugacity that can be tolerated for high-purity/high-strength steel.
- Understanding of underlying HIC mechanism of ultra-high-purity/high-strength steel without segregated impurities and precipitates

Acknowledgement

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