

# Bidirectional Boost/Buck Quadratic Converter for Distributed Generation Systems with Electrochemical Storage Systems

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**Abstract**—The increasing number of distributed generation systems using renewable and non-conventional energy sources show the trend of future generation systems. Most of these systems require power electronic converters as an interface between the DC voltage buses and electrochemical storage systems. Such storage systems, like batteries or supercapacitors, usually need bidirectional DC-DC converters to allow their charge or discharge according with necessary operation conditions. In this paper, a non-isolated bidirectional Buck-Boost converter with high voltage gain for electrochemical storage devices used in distributed generation systems is presented. To achieve high voltage gain ratios, the proposed topology presents quadratic characteristics in both step-down (Buck) and step-up (Boost) operation modes. In addition to the wide conversion range, it presents continuous input and output current, reduced charging/discharging ripple and simple control circuitry. All these features allow the energy exchange smoothly and continuously resulting in a longer durability of storage devices. The principle of the operation of the proposed converter in both operation modes, as well as their theoretical analysis will be discussed. The performance of this bidirectional power converter is confirmed through simulation and experimental results.

**Keywords**— *bidirectional DC/DC converter, Boost and Buck quadratic converter, distributed generation systems.*

## I. INTRODUCTION

The investment in renewable and sustainable energy sources is continuously increasing. According with data available from 2015 the global new investment in renewable energy and fuels climbed to a record USD 285.9 billion [1]. Furthermore, a significant interest over the last years about losses over long transmission and distribution lines, reduction of installation costs and voltage regulation problems have encouraged the development of distributed generation systems based on photovoltaic panels (PV), fuel cells (FC), wind turbine, micro-turbines, etc., allowing small-scale generation located near to the customers rather than remote locations [2, 3]. Also remarkable is the increasing number of other applications (telecommunications systems, hybrid electric vehicles, aviation, uninterruptible power supplies, etc.) using non-conventional energy sources [4-8]. Undesirably the floating nature of most renewable energy sources makes them unsuitable for standalone operation as the sole power source. For instance, hydrogen and hydrocarbon fuel cells contain high electrochemical energy but usually require back-up power at starting conditions [9, 10]. The most common solution to overcome this problem is to use energy storage devices such as batteries or supercapacitor in addition to the renewable energy source to compensate for these fluctuations and maintain a smooth and continuous power flow to the load [11]. Bidirectional DC-DC converter plays an important role in such applications, allowing energy exchange

between storage devices and the rest of the system. Besides the adaptation to different voltage levels these converters will also control the charge or discharge of storage devices according with required operating condition. Several bidirectional DC-DC converters based on isolated and non-isolated topologies have been presented in literature for this purpose [12-17]. Most of isolated topologies need a transformer and a high number of switching devices which increases the cost and the switching losses, in addition to more complicated control schemes [18-21]. Non-isolated topologies are mainly based on the conventional Buck-Boost and Cuk configurations which are fairly simple and easy to control [22-25]. However, in many applications the high gain requirements are such that the conventional DC-DC converter operates with extremely duty-cycle operation which may result in reverse-recovery problem and causes not only low efficiency but also creates electromagnetic interference (EMI) problems [13]. To extend the voltage gain ratio, several DC-DC converters with magnetic coupling techniques have been proposed, notwithstanding some disadvantages such as pulsating bus voltage remain and complex control schemes [26, 27].

In this paper, a non-isolated bidirectional Buck-Boost quadratic converter is proposed. This solution is suitable for distributed generation systems where conventional converters are inadequate for high-frequency applications and where the specified range of input voltages and the specified range of output voltages call for an extremely large range of conversion ratios. This converter with quadratic DC conversion ratio offer a significantly wider conversion range, continuous input and output current, reduced charging/discharging ripple and also simple control circuitry.

## II. BIDIRECTIONAL BOOST/BUCK QUADRATIC CONVERTER

One of the most known topologies with wide voltage range is the Boost quadratic converter. As can be seen by Fig. 1, this topology is characterized by the use of two inductors, one intermediate capacitor, three diodes and a single power switch.

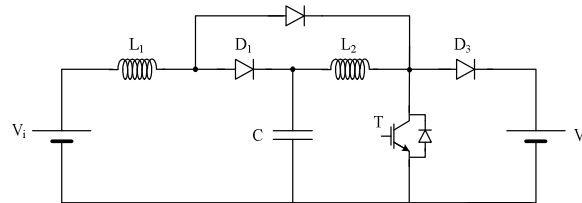


Fig. 1. Classical quadratic Boost converter.

In order to overcome the limitation of the unidirectional power flow of the Boost quadratic converter it is proposed a new bidirectional power converter. Fig. 2 shows the power topology of this converter. As presented in this figure, the power circuit does not require more passive components (inductors and capacitor) than the required by the classical Boost quadratic converter. It is also characterized by a static voltage gain with a quadratic function for both Boost and Buck operating modes.

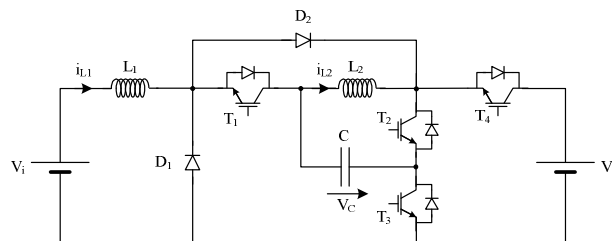


Fig. 2. Proposed bidirectional Boost/Buck quadratic converter.

In order to analyze the proposed bidirectional dc/dc converter will be assumed steady state operation, continuous conduction mode (CCM) and ideal components. As described, the proposed power converter allows for two distinct modes of operation: discharging and charging of the storage system.

### III. OPERATION OF THE POWER CONVERTER

In the discharging mode the converter operates as a Boost converter, transferring the energy from the storage system to the load. In this mode two of the transistors ( $T_1$  and  $T_4$ ) are always in the OFF state and the transistor  $T_3$  is always in the ON state. This mode is also characterized by two equivalent circuits during one switching cycle ( $T_s$ ), as described below:

First equivalent circuit (Fig. 3 a)): This circuit is obtained when the transistor  $T_2$  is in the ON state (during the time interval of  $\delta T_s$ ). In this state the inductors  $L_1$  and  $L_2$  will be charged since the currents in these inductors will increase linearly. The energy stored in the capacitor  $C$  is transferred to the inductor  $L_2$ .

Second equivalent circuit (Fig. 3 b)): This circuit is related with the transistor  $T_2$  in OFF state (during the time interval of  $(1-\delta)T_s$ ). This state is characterized by the discharge of the inductors  $L_1$  and  $L_2$ . During this time interval the currents in these inductors will decrease linearly. The energy that was stored in the previous state is now transferred to the capacitor  $C$  and to the load:

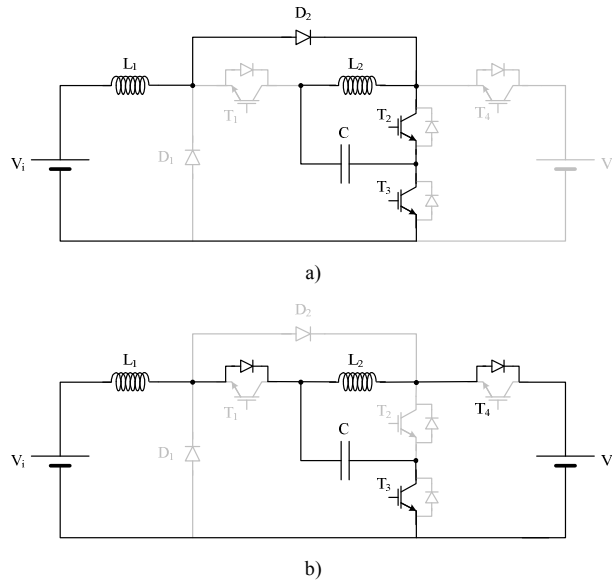


Fig. 3. Equivalent circuits during one switching period for the discharge mode of the storage system.

From the analysis of these two operating stages is possible to obtain the voltage gain of this converter in discharge mode and in CCM. Thus, considering that the average voltages in the inductors in the two operating stages are equal, the following relationships are obtained

$$\delta V_i + (1 - \delta)(V_i - V_C) = 0 \quad (1)$$

$$\delta V_C + (1 - \delta)(V_C - V_o) = 0 \quad (2)$$

From the partial voltage gains that are obtained from the previous equations, the input to output voltage gain in this discharge mode is given by:

$$\frac{V_o}{V_i} = \frac{1}{(1-\delta)^2} \quad (3)$$

The operation of the converter in charging mode is characterized by the energy transfer from the load to the storage energy system. In this mode of operation the converter operates as a Buck converter. As in the previous operation mode in this case only a single transistor controls the output voltage through commutation. Thus, the transistors  $T_2$  and  $T_3$  are always in the OFF state. The transistor  $T_4$  could be always in the ON state or can commutate at the same time with transistor  $T_1$  (additional switching losses). From the analysis of this operating in CCM is possible to verify that during one switching cycle there are two equivalent circuits, as following described:

First equivalent circuit (Fig. 4 a)): This first equivalent circuit is related with the on-time (time interval of  $\delta T_s$ ) of transistor  $T_1$ . During this time period the currents in inductors  $L_1$  and  $L_2$  will increase in absolute value. Capacitor  $C$  will discharge since its energy will be transferred to inductor  $L_1$ .

Second equivalent circuit (Fig. 4 b)): The obtained circuit associated to the complementary time (time interval of  $(1-\delta)T_s$ ) is related with the transistor  $T_1$  in OFF state. In this state the currents in the inductors  $L_1$  and  $L_2$  will decrease in absolute value. The energy that was stored in those inductors will be transferred to the capacitor  $C$  and to the load (storage system).

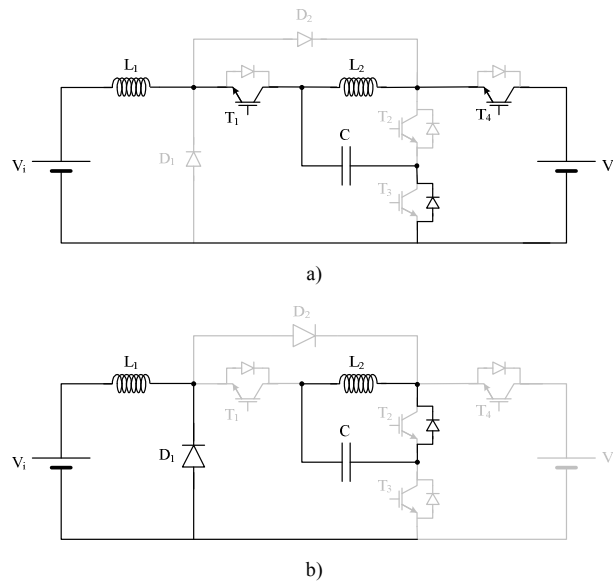


Fig. 4. Equivalent circuits during one switching period for the charge mode of the storage system

The relationship between the output and input voltage of the converter in discharge mode in CCM can be obtained from the analysis of the equivalent circuits presented in Fig. 4. Thus, according to these circuits and considering that the sums of the average voltages in the inductors during one switching cycle are equal to zero, the next relationships are obtained:

$$\delta (V_C - V_i) - (1-\delta) V_i = 0 \quad (4)$$

$$\delta (V_C - V_o) + (1-\delta) V_C = 0 \quad (5)$$

The input voltage gain of this converter in discharge mode will therefore be given by the partial voltage gains that can be obtained from the previous equations, as follows:

$$\frac{V_o}{V_i} = \delta^2 \quad (6)$$

#### IV. SIMULATION RESULTS

The operation modes of the proposed bidirectional Boost/Buck quadratic converter were verified through numerical simulations. These simulations were performed using the Matlab/Simulink program. The converter operation was verified at  $V_i = 24\text{V}$  (battery voltage),  $V_o = 200\text{V}$ ,  $L_1 = 1\text{ mH}$ ,  $L_2 = 2\text{ mH}$ ,  $C = 150\text{ }\mu\text{F}$  and switching frequency  $f_s = 14\text{ kHz}$ .

In the discharge mode it is considered the voltage of the storage as the input and the  $V_o$  as the output voltage. Figures 5, 6 and 7 show the obtained simulated results for the converter, operating in discharging mode (quadratic Boost) and CCM. These results were obtained for a duty cycle of 0,66. In Fig. 5 is possible to verify the input voltage (1), capacitor voltage (2) and output voltage (3). The high gain of the power converter is confirmed by this result. Figs. 6 and 7 show the inductor currents  $i_{L1}$  and  $i_{L2}$  and the voltage at the terminals of transistors  $T_1$  and  $T_2$ . From these figures is possible to confirm the continuous inductor current operation. The ripple current in both inductors are also similar in magnitude.

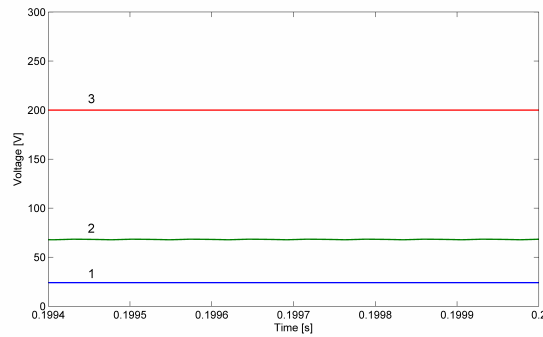


Fig. 5. Discharging mode. Simulation waveforms of the: 1 – input voltage  $V_i$ , 2 - capacitor voltage  $V_c$  and 3 - output voltage  $V_o$ .

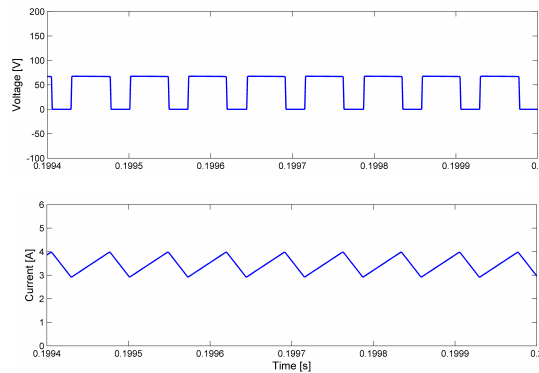


Fig. 6. Discharging mode. Simulation waveforms of the transistor  $T_1$  voltage ( $V_{T1}$ ) and inductor  $L_1$  current ( $i_{L1}$ ).

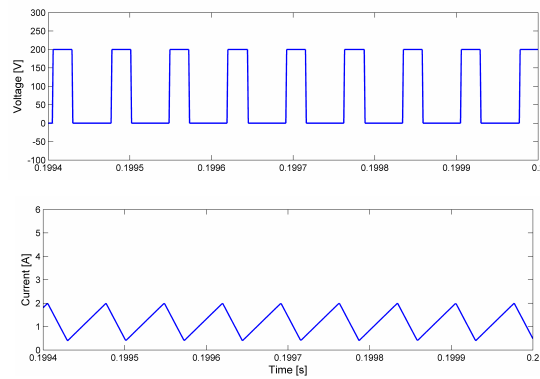


Fig. 7. Discharging mode. Simulation waveforms of the transistor  $T_2$  voltage ( $V_{T2}$ ) and inductor  $L_2$  current ( $i_{L2}$ ).

The operation in charged mode (quadratic Buck) was also confirmed through the simulations. Figs 8-10 show the obtained simulated results in this mode of operation for a duty cycle of 0,35. The input voltage (1), capacitor voltage (2) and output voltage (3) are presented in Fig. 8. As expected, in this case the output voltage (storage system) is much lower than the input voltage. The inductor currents  $i_{L1}$  and  $i_{L2}$  and the voltage at the terminals of transistors  $T_1$  ( $V_{T1}$ ) and  $T_2$  ( $V_{T2}$ ) are presented in Figs. 9 and 10. From these figures is possible to confirm the continuous inductor current. Even in this mode the ripple current in both inductors are still similar in magnitude.

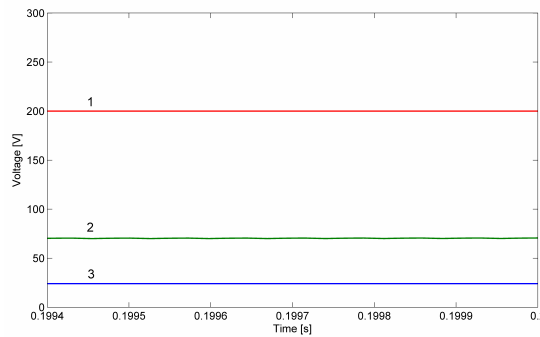


Fig. 8. Charging mode. Simulation waveforms of the: 1 – input voltage  $V_o$ , 2 - capacitor voltage  $V_c$  and 3 - output voltage  $V_i$ .

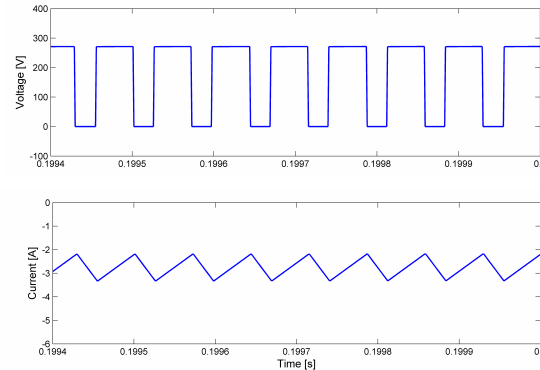


Fig. 9. Charging mode. Simulation waveforms of the transistor  $T_1$  ( $V_{T1}$ ) voltage and inductor  $L_1$  current ( $i_{L1}$ ).

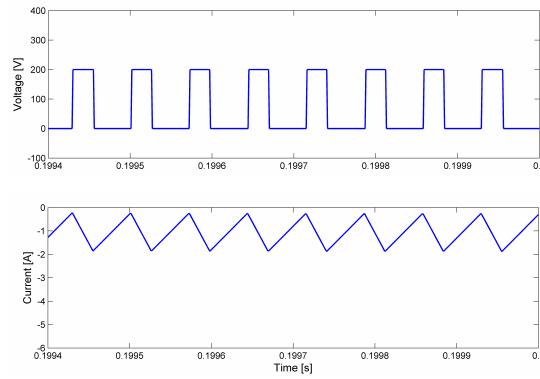


Fig. 10. Charging mode. Simulation waveforms of the transistor  $T_2$  voltage ( $V_{T2}$ ) and inductor  $L_2$  current ( $i_{L2}$ ).

## V. EXPERIMENTAL RESULTS

A prototype of the proposed converter was built to validate the theoretical considerations and obtained simulation results. The circuit parameters of the experimental prototype are the same as those used for simulation. As made for the simulation the prototype was verified in the discharging mode ( $V_i=24V \rightarrow V_o=200V$ ) and charging mode ( $V_o=200V \rightarrow V_i=24V$ ) power flow.

The waveforms obtained from the experimental prototype in discharging power flow mode (quadratic Boost) are presented in Figs. 11, 12 and 13. All these results were obtained for a duty cycle of 0,67. From Fig. 11 is possible to confirm that the input voltage (1), capacitor voltage (2) and output voltage (3) are in agreement with the expected. This figure also confirms the high gain of the power converter. Figs. 12 and 13 show the inductor currents  $i_{L1}$  and  $i_{L2}$  and the voltage at the terminals of transistors  $T_1$  ( $V_{T1}$ ) and  $T_2$  ( $V_{T2}$ ). Through these figures is possible to confirm the expected continuous inductor current operation. They also show that the ripple current in both inductors are also similar in magnitude.

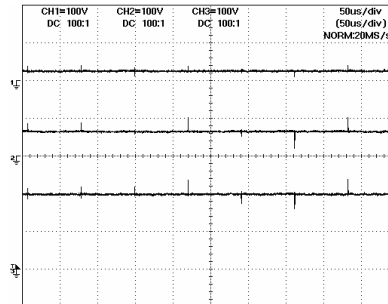


Fig. 11. Discharging mode. Experimental waveforms of the: Ch1 – input voltage  $V_i$ , Ch2 - capacitor voltage  $V_c$  and Ch3 - output voltage  $V_o$ .

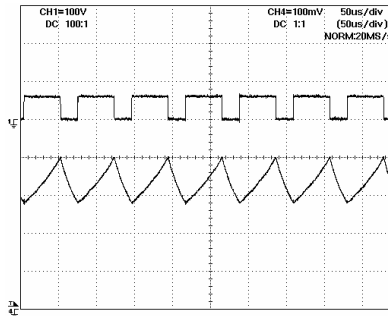


Fig. 12. Discharging mode. Experimental waveforms of the: Ch1 – transistor  $T_1$  voltage ( $V_{T1}$ ) and Ch4 – inductor  $L_1$  current ( $i_{L1}$ ).

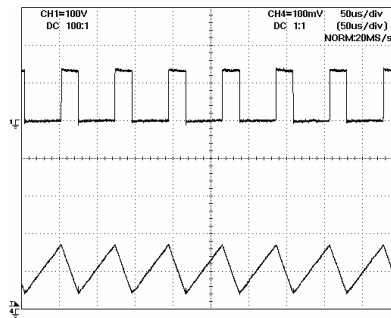


Fig. 13. Discharging mode. Experimental waveforms of the: Ch1 – transistor  $T_2$  voltage ( $V_{T2}$ ) and Ch4 – inductor  $L_2$  current ( $i_{L2}$ ).

Experimental tests with the laboratory prototype in charging mode (quadratic Buck) were also performed. The waveforms that were obtained in this mode with a duty cycle of 0,36 are presented in Figs. 14, 15 and 16. The input voltage, capacitor voltage and output voltage are presented in Fig. 8. These results are similar with the ones presented in the previous test. Regarding the experimental waveforms of inductor currents  $i_{L1}$  and  $i_{L2}$  and the voltage at the terminals of transistors  $T_1$  and  $T_2$  they are presented in Figs. 14 and 15. These figures show that the converter works in continuous conduction mode and that the ripple current in both inductors are similar in magnitude.

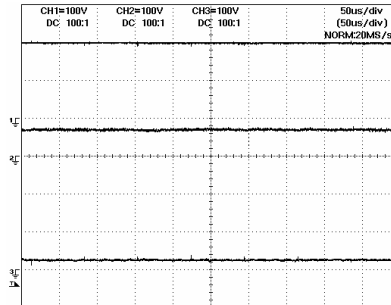


Fig. 14. Charging mode. Experimental waveforms of the: Ch1 – output voltage  $V_o$ , Ch2 - capacitor voltage  $V_c$  and Ch3 - input voltage  $V_i$ .

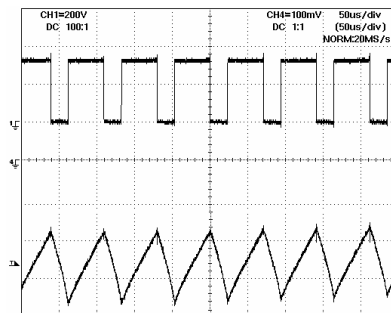


Fig. 15. Charging mode. Experimental waveforms of the: Ch1 – transistor  $T_1$  voltage ( $V_{T1}$ ) and Ch4 – inductor  $L_1$  current ( $i_{L1}$ ).



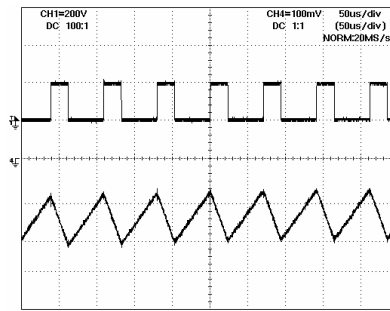


Fig. 16. Charging mode. Experimental waveforms of the: Ch1 – transistor  $T_2$  voltage ( $V_{T2}$ ) and Ch4 – inductor  $L_2$  current ( $i_{L2}$ ).

According to the figures presented in this section is possible to confirm that the experimental results are very similar with the obtained through numerical simulations.

## VI. CONCLUSIONS

A bidirectional DC-DC converter with Boost/Buck characteristics for electrochemical storage systems was proposed in this work. The proposed converter presents a Boost quadratic characteristic when the storage system is in discharge mode and Buck quadratic characteristic when the referred system is in charge mode. As a result, with this converter is possible to obtain higher and lower voltage gain with reduced duty ratios. Besides that, it presents continuous input and output current, reduced charging/discharging ripple and simple control circuitry. Due to these features, this non-isolated bidirectional Buck-Boost converter with high voltage gain is indicated for several applications, such as, electrochemical storage devices used in distributed generation systems. The performance of the proposed converter was tested and verified through simulations and with a laboratorial prototype. The obtained experimental results are in agreement with the simulation results, confirming the expected results for this topology.

## ACKNOWLEDGMENT

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