1	A simple method for equine kinematic gait event detection
2	Summary
3	Background: Previous studies have validated methods for determining kinematic gait events using
4	threshold-based methods, however a simple method is yet to be identified that can be successfully
5	applied to all equine gaitswalk, trot and canter.
6	<b>Objectives</b> : To develop a simple kinematic method to identify the timing of hoof-on, peak vertical
7	force and hoof-off, which can be applied to <del>all equine gaits<u>walk</u>, trot and canter</del> .
8	Study Design: The horses ( $n=3$ ) were ridden in walk, trot and canter down a runway with four force
9	plates arranged linearly. Three-dimensional forces were recorded at a sampling rate of 960 Hz and
10	were synchronised with a ten-camera motion analysis system sampling at 120 Hz.
11	Methods: Events identified from the vertical ground reaction force (GRFz) data were hoof-on
12	(GRFz>50N), peak vertical force (GRFz <sub>peak</sub> ) and hoof-off (GRFz<50N). Kinematic identification of hoof-
13	on and hoof-off events was based on sagittal planar angles of the fore and hindlimbs. Peak
14	metacarpophalangeal/metatarsophalangeal (MCP/MTP) joint extension was used Two kinematic
15	methods were used to assess the time of GRFz <sub>peak</sub> _: a vertical orientation of the third
16	metacarpal/metatarsal (MCIII/MTIII) and peak extension of the
17	metacarpophalangeal/metatarsophalangeal (MCP/MTP) joint. The accuracy (mean) and precision
18	(SD) of the time difference between the kinetic and kinematic events were calculated for the fore and
19	hindlimbs at each gait.
20	<b>Results</b> : Hoof-off was determined with better accuracy ( <u>range:</u> -3.9 <u>4</u> <b>35</b> to 8.33 <del>3</del> ms) and precision
21	(5.43 to 11.39ms) than hoof-on across all gaits. Peak MCP <u>angle (5.83 to 19.65 ms) was a more precise</u>
22	/MTP angle (-0.298 to -62.5ms) was a more accurate representation of GRFz <sub>peak</sub> -than peak MTP angle
23	(11.49 to 67.75 ms)than MCP/MTP inclination (-217.593 to 54.018ms).
24	Main Limitations: The sample size was small and, therefore, further validation is required. The

25 proposed method was tested on one surface.

26 Conclusions: A simple kinematic method of detecting hoof-on, hoof-off and GRFz<sub>peak</sub> has been 27 identifiedis here proposed for all gaitswalk, trot and canter. Further work should focus on validating 28 the methodology in a larger number of horses and extending the method for use on surfaces with 29 varying compliance.

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#### 31 Introduction

32 Equine biomechanical studies rely heavily on determination of gait events and subsequent stride cycles for the accurate analysis of kinematic and kinetic variables [1]. However, a standardised, 33 evidence-based method to objectively determine gait events using motion capture data is yet to be 34 35 defined under for over ground, ridden conditionsfield conditions-[2,3]. Previous studies reported that 36 limb force and timing of initial hoof impact can be difficult to identify using kinematic data, with force plates being widely accepted as the "gold standard" for identifying hoof contact (hoof-on) and lift off 37 38 (hoof-off) [2,4,5]. Force plates are, however, rarely used outside laboratory conditionsin field conditions, so a reliable kinematic method of defining the time of hoof-on, hoof-off and peak vertical 39 40 force (GRFz<sub>peak</sub>) in field studies would be useful [2,6].

Previous validations of kinematic gait events against force data have reported high accuracy and precision [2,3,6,7,8,9]. Most of these studies use hoof markers for event detection but precise visual determination of hoof contact and lift off are difficult, especially on compliant surfaces [2, 10]. The objective was to use force data to evaluate a straightforward kinematic method to identify the time of hoof-on, hoof-off and GRFz<sub>peak</sub>, which can be universally applied to all limbs of the ridden horse in walk, trot and canter.

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## 48 Methods

49 Horses

Three Lusitano stallions (height at withers: 1.61–1.65m; mass: 535.5 - 585kg) trained to advanced level
dressage were ridden by their usual trainer (mass: 65 kg). The horses were assessed by a veterinarian
to be sound at walk and trot on a straight line.

### 53 Data Acquisition

54 Retro-reflective 3D markers were applied to the left and right side of the horse (Figure 1). A static trial 55 of each horse standing square and at least 6 successful walk, trot and canter trials were recorded. The 56 horses were ridden in walk ( $1.66 \pm 0.22 \text{ m/s}$ ), trot ( $2.44 \pm 0.25 \text{ m/s}$ ) and canter ( $2.95 \pm 0.69 \text{ m/s}$ ) down a runway with a poured rubber surface. Speed was measured using the first derivative of a marker on 57 58 the sacrum in the direction of motion. Kinematic data were captured at 120 Hz with a ten-camera 59 motion analysis system (Eagle cameras, Motion Analysis Corp.; Cortex 1.1.4.368, Motion Analysis 60 Corp.) and synchronised kinetic data with four force plates arranged linearly along a runway (Bertec 61 Corporation, USA) at 960 Hz.

### 62 Data Processing

Kinematic and kinetic data were analysed using Visual 3D (C-Motion Inc.). Kinematic data were interpolated (maximum gap 10 frames) and then filtered with a low pass zero lag 4<sup>th</sup> order Butterworth digital filter (cut off frequency of 10 Hz). The same filter was also applied to the kinetic data with a cut off frequency of 100 Hz in accordance with [11]. The timing of hoof impact, lift off and peak vertical force was calculated using GRF and kinematic data.

### 68 Gait event detection using GRF data

Footfalls were rejected if the hoof was not entirely on the force platform or if another hoof was in contact with the same force platform simultaneously. The vertical ground reaction force (GRFz) data were used to detect the time of hoof-on (GRFz>50N), peak vertical force (GRFz<sub>peak</sub>) and hoof-off (GRFz<50N).</p>

73 Gait event detection using kinematic data

74	To determine the kinematic hoof-on and hoof-off events for the forelimbs, a sagittal plane angle was	
75	computed using the following markers: 1) centre of rotation of the MCP joint; 2) centre of rotation of	
76	the distal interphalangeal (DIP) joint; 3) the lateral epicondyle of the humerus (Figure 1a). The	
77	hindlimb events for hoof-on and hoof-off were also identified by creating a sagittal plane angle, using	
78	the following markers: 1) centre of rotation of the MTP joint; 2) the talus representing the centre of	
79	rotation of the tarsal joint; 3) the hind DIP joint (Figure 1b). Planar angle-time curves were plotted for	
80	the fore and hindlimbs. A threshold of 0 degrees was used to define events when the two segments	
81	were aligned, with hoof-on <del>(O degrees) being coinciding with descent through O degrees and hoof-off</del>	
82	on ascent through 0 degrees.followed by extension of the MCP/MTP joint, and hoof off (0 degrees)	
83	being followed by flexion of the MCP/MTP joint. The time of GRFz <sub>peak</sub> was identified with the kinematic	
84	data using maximum MCP and MTP joint extension, where maximal MCP extension has previously	
85	shown a strong correlation with peak vertical force [12].	
86 87 88 89 90	Figure 1a) The sagittal plane angle used to identify hoof-on and hoof-off events for the forelimbs; 1) MCP joint; 2) fore DIP joint; 3) lateral epicondyle of the humerus. The MCIII was created using markers on the proximal end of metacarpal IV and MCP joint. The MCP joint was created using the MCIII and fore pastern segment, which was made using the centre of rotation of the MCP joint and fore DIP joint markers. Figure 1b) The sagittal plane angle used to create identify hoof-on and hoof-off events for the hindlimbe: 11 MTB joint; 2) talus; 2) hind DIP	
92 93 94	joint. The MTIII segment was created using the talus and MTP joint markers. The MTP joint was created using the MTIII and hind pastern segment, which was made using the centre of rotation of the MTP joint and hind DIP joint markers.	
95	The time of GRFzmat was identified with the kinematic data using two methods. The first method	
97	identified a vertical orientation of the MCIII and MTIII segments in the sagittal plane, which has	
98	previously been used in the forelimbs [12, 13]. The second method used maximum MCP and MTP joint	
99	angle, where maximal MCP extension has previously shown a strong correlation with peak vertical	
100	force [13].	
101	Gait event timings were derived using the GRF and kinematic methods. The accuracy and precision of	

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- the kinematic gait events at representing the GRF events were calculated for the fore and hindlimbs 102

103 at each gait in accordance with [3]. Accuracy is defined as the mean difference between kinematic

104 and GRF events (bias) and precision as the standard deviation (SD) of the mean difference (accuracy)

105 [3]. The smallest difference was considered the best accuracy and precision.

106 <u>Results</u>

107 A total of 227 stance phases (walk: 113; trot: 80; canter: 34) were analysed across all subjects. 108 Accuracy and precision of the kinematic gait events for all gaits and individual limbs (Table 1) showed that hoof-off was identified more accurately than hoof-on, as shown by a much smaller deviation from 109 the GRF event (Figure 2). Accuracy (difference in timings closer to zero) and precision (smaller 110 111 standard deviation of the difference in timings) were higher for hoof-on in canter compared to walk 112 and trot. Accuracy for hoof-off was highest at trot, but precision was highest at walk. The time of GRFz<sub>peak</sub> corresponded well with maximal MCP/MTP extension. but not with vertical inclination of MCIII/MTIII. 113 114 Table 1: The accuracy (mean) and precision (standard deviation) between events detected kinematically and 115 using ground reaction force data for forelimbs and hindlimbs of all horses at each gait. Canter was categorised further into leading (Le) and trailing (Tr) limbs. Positive values indicate that the kinematic event occurred before 116 117 the GRF event and vice versa for negative values. Negative values for stance duration indicate that the kinematic 118 method generates a longer timing. 119 120 121 122 123 124 125 Figure 2: The accuracy and precision of the kinematic gait events for fore and hindlimbs on a GRF trace at walk, 126 trot and canter. The solid black lines on each graph represent the GRF events at hoof-on (GRFz>50N), GRFz<sub>peak</sub> 127 and hoof-off (GRFz<50N) from left to right respectively. The dotted lines represent the events identified using 128 the kinematic methods; from left to right: hoof-on, peak MCP/MTP extension and hoof-off. The shaded areas 129 represent the precision of each kinematic event. The canter data from the leading and trailing limbs has been

130 grouped for the purpose of this graphical representation.

# 132 Discussion

This study evaluated a kinematic method for determining the timing of hoof-on, GRFz<sub>peak</sub> and hoof-off events in walk, trot and canter. The method is simple, can be applied to two dimensional or three dimensional kinematic data and can be used under most field conditions, provided the coronary band is visible. The hoof-off event was detected with better accuracy and precision than hoof-on, which was generally within one to two frames of the GRF event. The timing of GRFz<sub>peak</sub> <u>also</u>\_corresponded closely with maximal MCP/MTP extension-<u>but not with verticality of MCIII/MTIII</u>.

Hoof orientation during impact was not taken into account for this study. The hoof sole has been observed to be completely flat on the ground within several milliseconds of initial impact [1413], which suggests that the effect of hoof orientation on impact timing should be minimal. The distal interphalangeal joint markers are also at the centre of rotation, which therefore should make the detection method less sensitive to hoof orientation on landing. <u>The horses in this study were also</u> <u>tested during collected canter and further work is required to investigate the accuracy and precision</u> of the kinematic detection methods in horses travelling at faster velocities.

146 Precision as low as 2 ms or less than one frame of data has been reported [9] for hoof-on at walk and trot using a velocity threshold method, which appears to be the most accurate to date. A greater 147 148 sample of footfalls were analysed (360-800 hoof-on events for walk and trot in a straight line), 149 however it is important to note that differences were calculated by averaging the within-horse mean 150 values, which will lower the overall differences between footfalls [9]. Nevertheless, the hoof-off 151 kinematic detection method reported here demonstrated better accuracy at trot in the hind limbs 152 than the methods used by [9]. The hoof-off event at trot was comparable to some of the methods 153 described by [3], however the detection methods used appear to be more complex to administer 154 execute in comparison to this study.

Some methods [3,7,9] are also dependent on velocity thresholds. Surface properties can influence
 parameters such as hoof landing velocity [10], which may affect the repeatability of these methods if

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used on compliant surfaces. Forelimb landing angle is affected by surface stiffness [10], which
suggests that the angles used to calculate the kinematic events during this study may also be affected
by the surface properties. Surface effects are not well documented [3], so pilot work is recommended
when before testing on compliant surfaces [9].

161 Peak vertical force Mid-stance is commonly identified in research because it is associated with the risk 162 of musculoskeletal injuries and can be used during lameness assessments [14]. The ability to calculate 163 the timing of this in the absence of force data could constitute a useful tool when quantifying the 164 entire kinematic profile of a horse during such assessments.the peak forces experienced during 165 support can be associated with generating a risk factor for injury [15]. In this study, peak MCP was 166 167 correlation between MCP joint angle (49.4% stance) and GRF (47.7% stance) was found during in vitro 168 loading [12]. In contrast, [1615] suggested that maximal fetlock extension and peak force in the 169 forelimbs during trot occur more independently. \_A delay in fetlock extension has been observed 170 during trot- in the forelimbs of ridden horses [17] where it was proposed that the dynamic effect of 171 the rider may have a greater influence after mid-stance when the horse's centre of gravity is rising 172 [16], which. This could may explain why peak MCP and MTP extension occurred these events were 173 was after GRFzpeak synchronized in the present study. It was proposed that the dynamic effect of the 174 rider may have a greater influence after mid-stance when the horse's centre of gravity is rising [17], 175 which could explain the delay in the kinematic mid-stance event. Previous studies have used MCIII 176 inclination to represent the transition between braking and propulsive longitudinal forces in the 177 forelimbs [12] but the data presented here shows that peak MCP extension is a more appropriate 178 method of identifying the time of peak force. This can be further supported by [18] where the change 179 in longitudinal force in the forelimbs at walk occurred after the vertical orientation of the MCIII and 180 coincided with peak MCP extension.

181 Conclusions

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182 A simple method of detecting force gait events using kinematic data has been identified for all gaitsridden

183 walk, trot and canter-of the ridden horse. Further work must focus on validation using a greater sample size to establish

- 184 the effect of a larger population of horses on the accuracy and precision of the detection methods
- 185 under a number of differentvariety of ridden and un-ridden conditions.
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#### 187 **References**

- 188 [1] Leach, D. (1993) Recommended terminology for researchers in locomotion and biomechanics of 189 quadrupedal animals. Cells Tissues Organs, 146 (2-3), 130-136.
- 190 [2] Hobbs, S. J., Orlande, O., Edmundson, C. J., Northrop, A. J. and Martin, J. H. (2010) Development of
- 191 a method to identify foot strike on an arena surface: application to jump landing. Comparative Exercise Physiology, 7 (1), 19-25. doi:10.1017/S1755254010000097 192
- 193 [3] Boye, J. K., Thomsen, M. H., Pfau, T. and Olsen, E. (2014) Accuracy and precision of gait events 194 derived from motion capture in horses during walk and trot. Journal of Biomechanics, 47 (5), 1220-4. 195 doi: 10.1016/j.jbiomech.2013.12.018.
- 196 [4] Schamhardt, H. C. and Merkens, H. W. (1994) Objective determination of ground contact of equine 197 limbs at the walk and trot: comparison between ground reaction forces, accelerometer data and 198 kinematics. Equine vet. J. Suppl., 17, 75-79.
- [5] Witte, T. H., Knill, K. and Wilson, A. M. (2004) Determination of peak vertical ground reaction force 199 200 from duty factor in the horse (equus caballus). The Journal of Experimental Biology, 207, 3639-3648.
- 201 [6] Olsen, E., Andersen, P. H. and Pfau, T. (2012) Accuracy and precision of equine gait event detection 202 during walking with limb and trunk mounted inertial sensors. Sensors, 12, 8145-8156.
- 203 doi:10.3390/s120608145 204
- [7] Peham, C., Scheidl, M. and Licka T. (1999) Limb locomotion speed distribution analysis as a new 205 method for stance phase detection. Journal of Biomechanics. 32, 1119-1124.
- 206 [8] Galisteo, A. M., Garrido-Castro, J. L., Miró, F., Plaza, C. and Medina-Carnicer, R. (2010) Assessment 207 of a method to determine the stride phases in trotting horses from video sequences under field 208 conditions. Vet. Med. Austria, 97, 65-79.
- 209 [9] Starke and Clayton (2015), A universal approach to determine footfall timings from kinematics of 210 a single foot marker in hoofed animals. PeerJ, 3,e783. DOI 10.7717/peerj.783
- 211 [10] Burn, J. F. and Usmar, S. J. (2005) Hoof landing velocity is related to track surface properties in 212 trotting horses. Equine and Comparative Exercise Physiology, 2 (1), 37-41. 213 doi.org/10.1079/ECP200542
- 214 [11] Hobbs, S. J. and Clayton, H. M. (2013) Sagittal plane ground reaction forces, centre of pressure 215 and centre of mass in trotting horses. The Veterinary Journal, 198, e14-e19. 216 doi.org/10.1016/j.tvjl.2013.09.027
- 217 [12] Drevemo, S., Dalin, G., Fredricson, I and Hjertén, G. (1980) Equine Locomotion: 1. The analysis of
- 218 linear and temporal stride characteristics of trotting standardbreds. Equine Vet Journal, 12 (2), 60-65.
- 219 [1413] Merkens, H. W. and Schamhardt, H. C. (1994) Relationships between ground reaction force 220 patterns and kinematics in the walking and trotting horse. Equine Veterinary Journal, 26, (17) 67-70.
- 221 DOI: 10.1111/j.2042-3306.1994.tb04877.x
- 222 [14] Merkens, H. W. and Schamhardt, H. C. (1988) Evaluation of equine locomotion during different
- 223 degrees of experimentally induced lameness I: Lameness model and quantification of ground reaction
- 224 force patterns of the limbs. Equine Veterinary Journal, 20 (S6) 99-106. DOI: 10.1111/j.2042-3306.1988.tb04655.x
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227	events in equine locomotion. Equine and Comparative Exercise Physiology, 1 (2), A1- A30.
228	001.0rg/10.10/9/ECEP200419 [1716]Clayton H. M. Lanovaz, L.L. Schambardt H. C. & Wessum P. V. (1999). The effects of a rider's
230	mass on ground reaction forces and fetlock kinematics at the trot. Equine Veterinary Journal, <b>31</b> (S30),
231	218-221.
232	[18] Hodson, E., Clayton, H. M. and Lanovaz, J. L. (2000) The forelimb in walking horses: 1. Kinematics
233	and ground reaction forces. Equine Veterinary Journal, <b>32</b> (4), 287-294.
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