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**Parametric Study on the Heating Values of Product gas via Steam  
Gasification of Palm Waste using CaO as Sorbent Material**

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**Abstract.** The abundance of oil palm waste in Malaysia is a good candidate to be used as a feedstock for syngas and hydrogen production. Biomass steam gasification is one of the promising methods for syngas production. This work focuses on the steam gasification with in-situ CO<sub>2</sub> capture using CaO as absorbent materials for hydrogen production from palm oil empty fruit bunch (EFB). Three parameters (temperature, steam/biomass ratio and sorbent/biomass ratio) has been studied on the lower heating value (LHV) and higher heating value (HHV) of the gas produce. The results show that the current study gives higher value of LHV at lower temperature of 823 K. The higher value of LHV is obtained due to the lower concentration of CO<sub>2</sub> caused by using CaO as sorbent material. Furthermore, CaO materials enhanced the concentration of concentration of the CO, H<sub>2</sub> and CH<sub>4</sub> in the gas product.

## Introduction

Due to the energy crisis and environmental issues mainly evoked by the use of fossil fuels as primary energy source, syngas and hydrogen ( $H_2$ ) has the potential to become a significant form of energy in the future as it is relatively cleaner than fossil fuels. Several alternatives and renewable sources are under considerable interest to be used for production of syngas and  $H_2$ , including biomass. The usage of biomass for syngas production is an attractive approach to be explored in Malaysia due to its abundance. Being the world largest producer of palm oil [1], the availability of empty fruit bunch (EFB) provides excellent feedstock for syngas and  $H_2$  production [1]. Syngas can be produced via a few methods: thermochemical processes (i.e. pyrolysis and gasification) or biological processes (i.e. biophotolysis and fermentation) [2]. Between the two thermochemical methods, Balat [3] reported that syngas and  $H_2$  production via gasification process is more economical than pyrolysis due to lower production cost. For gasification, the conversion of biomass into gaseous product can be enhanced by processing at high temperature and using gasifying agent such as air, pure steam, air-steam or oxygen-steam mixtures. Reported literature studies showed that when pure steam is used as the gasification agent, higher  $H_2$  content in the gas product can be obtained economically [4, 5]. Furthermore, the purity of  $H_2$  in a steam gasification process can be increased when it is coupled with  $CO_2$  adsorption material. Several performance indicators have been identified in the literature to study the gasification process for syngas and  $H_2$  production (gasification efficiency, thermodynamic efficiency, lower heating value, higher heating value, carbon conversion efficiency etc). Many researchers have identified that lower heating value (LHV) and higher heating value (HHV) are very important performance indicators to investigate the effect of parameters on the gas product from biomass gasification using different biomass as feed stock [6-12].

The performance of biomass gasification process is affected by at least five factors, namely, temperature, steam/biomass ratio, pressure, space time and bed composition. In the gasification process coupled with  $CO_2$  adsorption material, the sorbent/biomass ratio also has been identified as a factor affecting the gasification performance. In this work, a modeling approach is used to

investigate the effects of these operation conditions on the performance indicators of the gasification process especially on the lower and higher heating values (LHV and HHV) of gas product.

## Experimental Approach

In this study, the biomass considered for H<sub>2</sub> production via the steam gasification process is oil palm empty fruit bunch (EFB). The molecular formula for EFB is C<sub>3.4</sub>H<sub>4.1</sub>O<sub>3.3</sub> (based on 1 kg of biomass) with the molecular weight of 97.7 kg/kg mole [13]. Several assumption have been considered for the modeling approach: CaO is present in the system at a constant mass ratio with respect to EFB fed, the reactions proceed isothermally and occur at constant pressure, i.e. 1 atm, the tar and ash formations in this process are negligible and the operating temperature range taken below the 1043 K, at which beyond this temperature, the calcination reaction favored [14].

The flowsheet development, modelling and simulation have been presented by authors in the earlier work [15, 16]. The pervious study focuses on the mathematical modeling of the simplified process design for hydrogen production from palm waste using MATLAB. The flowsheet includes steam generation, gasification and gas cleaning units. The flowsheet model was incorporated with the mass and energy balances. The developed model is used as a platform to investigate the effects of process parameters: temperature, steam/biomass ratio and sorbent/biomass ratio on the hydrogen production and efficiency using MATLAB [15]. The effectiveness of the biomass gasification process is evaluated in terms of heating values of the gas product i.e. lower heating value (LHV) and higher heating value (HHV). LHV (MJ/Nm<sup>3</sup>) and HHV (MJ/Nm<sup>3</sup>) of the gas product are calculated using the Eq.1 and 2, respectively.

$$LHV = (30 \times CO + 25.7 \times H_2 + 85.4 \times CH_4) \times 0.0042 \quad (1)$$

$$HHV = (H_2 \times 30.52 + CO \times 30.18 + CH_4 \times 95) \times 4.1868 \quad (2)$$

where H<sub>2</sub>, CO and CH<sub>4</sub> are the mole percentage of those components in the gas product.

## Results and Discussion

The effect of temperature on the LHV and HHV is profiled in Fig. 1. It is observed that by increasing the temperature within the range of 823-1023 K, both LHV and HHV decrease. The heating values of the gas product are highly dependent on the CH<sub>4</sub>, CO and H<sub>2</sub> contents [17-19]. With increasing temperature, the H<sub>2</sub> and CO<sub>2</sub> amounts increase whereas the amount of CH<sub>4</sub> and CO contents decrease leading to the decreasing of LHV and HHV of the gas product due to the water gas shift and methane reforming reactions.

Similar trends of LHV and HHV changes with increasing temperature have been reported by other researchers in their work on catalytic steam gasification [10, 20] and steam gasification with CO<sub>2</sub> capture [9, 11, 21]. The effect of steam/biomass ratio on LHV and HHV is shown in the Fig. 1. It is observed that both LHV and HHV slightly decreased when increasing the steam/biomass ratio. The value of LHV and HHV changes due to the variation in the gas composition of the gas product. By increasing the steam/biomass ratio H<sub>2</sub> increases while CH<sub>4</sub> and CO amounts decreases as reported in the previous work [15, 16]. Excess of steam not only makes the water gas shift reaction faster but also moves forward to char gasification and methane reforming reaction, which produced more gases along with H<sub>2</sub>. Therefore, LHV and HHV decrease when increasing steam/biomass ratio but the effect is less significant compared to when increasing the temperature (Fig. 1). Similar trends of LHV and HHV have been reported by other researchers in their work investigating the effect of increasing steam/biomass ratio for catalytic steam gasification of biomass [9, 10, 20] and steam gasification [4, 5, 22]. In addition, the effect of sorbent/biomass ratio on LHV and HHV is plotted in Fig. 2. It is observed that when increasing sorbent/biomass ratio, both LHV and HHV increase. LHV and HHV depend on the composition of H<sub>2</sub>, CO and CH<sub>4</sub> in the gas product as mentioned before, LHV and HHV increase when increasing the sorbent/biomass ratio due to increase of H<sub>2</sub>, CO and CH<sub>4</sub> amounts in the gas product. Similar trends for increase of HHV and LHV by using CaO material is observed by Xu *et al.* [23] and Mahishi *et al.* [24], respectively. Table 1 shows the comparison of LHV between the current study and those reported by other works on biomass gasification for hydrogen production.

It is observed that the current study gives higher value of LHV at lower temperature (823 K) compared to others due to the CaO using as sorbent material.

## **Conclusion**

Current study presented the steam gasification with in-situ CO<sub>2</sub> capture using CaO as absorbent materials for hydrogen production from palm oil empty fruit bunch (EFB). Three parameters (temperature, steam/biomass ratio and sorbent/biomass ratio) has been investigated on the lower heating value (LHV) and higher heating value (HHV) of gas product. The results showed that the current study gives higher value of LHV at lower temperature of 823 K. The higher value of LHV is obtained due to the lower concentration of CO<sub>2</sub> caused by using CaO as sorbent material. Furthermore, CaO materials enhanced the concentration of concentration of the CO, H<sub>2</sub> and CH<sub>4</sub> in the gas product.

## **References**

- [1] S. Sumathi, S.P. Chai, A.R. Mohamed, Utilization of oil palm as a source of renewable energy in Malaysia, *Renewable and Sustainable Energy Reviews*. 12 (2008) 2404-2421.
- [2] M. Ni, D.Y.C. Leung, M.K.H. Leung, K. Sumathy, An overview of hydrogen production from biomass, *Fuel Processing Technology*. 87 (2006) 461-472.
- [3] M. Balat, Hydrogen-Rich Gas Production from Biomass via Pyrolysis and Gasification Processes and Effects of Catalyst on Hydrogen Yield, *Energy Sources, Part A, Recovery, Utilization, and Environmental Effects*. 30 (2008) 552 - 564.
- [4] J. Gil, J. Corella, M.P. Aznar, M.A. Caballero, Biomass gasification in atmospheric and bubbling fluidized bed, Effect of the type of gasifying agent on the product distribution, *Biomass and Bioenergy*. 17 (1999) 389-403.
- [5] C. Franco, F. Pinto, I. Gulyurtlu, I. Cabrita, The study of reactions influencing the biomass steam gasification process, *Fuel*. 82 (2003) 835-842.

- [6] M.A.A. Mohammed, A. Salmiaton, W.A.K.G.W. Azlina, M.S.M. Amran, Gasification of empty fruit bunch for hydrogen rich fuel gas production, *Journal of Applied Sciences*. In-Press (2011)
- [7] M. He, Z. Hu, B. Xiao, J. Li, X. Guo, S. Luo, Hydrogen-rich gas from catalytic steam gasification of municipal solid waste (MSW), Influence of catalyst and temperature on yield and product composition, *International Journal of Hydrogen Energy*. 34 (2009) 195-203.
- [8] N. Gao, A. Li, C. Quan, F. Gao, Hydrogen-rich gas production from biomass steam gasification in an updraft fixed-bed gasifier combined with a porous ceramic reformer, *International Journal of Hydrogen Energy*. 33 (2008) 5430-5438.
- [9] C. Pfeifer, R. Rauch, and H. Hofbauer, In-Bed Catalytic Tar Reduction in a Dual Fluidized Bed Biomass Steam Gasifier, *Industrial & Engineering Chemistry Research*. 43 (2004) 1634-1640.
- [10] J. Li, Y. Yin, X. Zhang, J. Liu, R. Yan, Hydrogen-rich gas production by steam gasification of palm oil wastes over supported tri-metallic catalyst, *International Journal of Hydrogen Energy*. 34 (2009) 9108-9115.
- [11] N. Howaniec, A. Smoliński, Steam gasification of energy crops of high cultivation potential in Poland to hydrogen-rich gas, *International Journal of Hydrogen Energy*. 36 (2011) 2038-2043.
- [12] P. Weerachanchai, M. Horio, C. Tangsathitkulchai, Effects of gasifying conditions and bed materials on fluidized bed steam gasification of wood biomass, *Bioresource Technology*. 100 (2009) 1419-1427.
- [13] K. Laohalidanond, J. Heil, C. Wirtgen, The production of synthetic diesel from biomass, *KMITL Sci. Tech. J.* 6 (2006) 35-45.
- [14] L. Han, Q. Wang, Y. Yang, C. Yu, M. Fang, Z. Luo, Hydrogen production via CaO sorption enhanced anaerobic gasification of sawdust in a bubbling fluidized bed, *International Journal of Hydrogen Energy*. 36 (2011) 4820-4829.

- [15] A. Inayat, M. M. Ahmad, M. I. A. Mutalib, S. Yusup, Process modeling for parametric study on oil palm empty fruit bunch steam gasification for hydrogen production, *Fuel Processing Technology*. 93 (2012) 26-34.
- [16] A. Inayat, M.M. Ahmad, M.I.A. Mutalib, S. Yusup, Flowsheet development and modeling of hydrogen production from Empty Fruit Bunch via steam gasification, *Chemical Engineering Transactions*. 21 (2010) 427-432.
- [17] M.A.A. Mohammed, A. Salmiaton, W.A.K.G.W. Azlina, M.S.M. Amran, Gasification of Empty Fruit Bunch for Hydrogen Rich Fuel Gas Production, in 3rd International Conference on Chemical & Bioprocess Engineering, Kota Kinabalu, Malaysia. (2009) 1292-1297.
- [18] V. Skoulou, A. Swiderski, W. Yang, A. Zabaniotou, Process characteristics and products of olive kernel high temperature steam gasification (HTSG), *Bioresource Technology*. 100 (2009) 2444-2451.
- [19] P. Lahijani, Z.A. Zainal, Gasification of palm empty fruit bunch in a bubbling fluidized bed: A performance and agglomeration study, *Bioresource Technology*. 102 (2011) 2068-2076.
- [20] P. Ji, W. Feng, B. Chen, Comprehensive Simulation of an Intensified Process for H<sub>2</sub> Production from Steam Gasification of Biomass, *Industrial & Engineering Chemistry Research*. 48 (2009) 3909-3920.
- [21] T. Pröll, H. Hofbauer, H<sub>2</sub> rich syngas by selective CO<sub>2</sub> removal from biomass gasification in a dual fluidized bed system, Process modelling approach, *Fuel Processing Technology*. 89 (2008) 1207-1217.
- [22] K. Umeki, K. Yamamoto, T. Namioka, K. Yoshikawa, High temperature steam-only gasification of woody biomass, *Applied Energy*. 87 (2010) 791-798.
- [23] G. Xu, T. Murakami, T. Suda, S. Kusama, T. Fujimori, Distinctive Effects of CaO Additive on Atmospheric Gasification of Biomass at Different Temperatures, *Industrial & Engineering Chemistry Research*. 44 (2005) 5864-5868.

[24] M.R. Mahishi, M.S. Sadrameli, S. Vijayaraghavan, D.Y. Goswami, A Novel Approach to Enhance the Hydrogen Yield of Biomass Gasification Using CO<sub>2</sub> Sorbent, *Journal of Engineering for Gas Turbines and Power*. 130 (2008) 011501.

[25] M.A.A. Mohammed, A. Salmiaton, W.A.K.G. Wan Azlina, M.S. Mohammad Amran, A. Fakhru'l-Razi, Air gasification of empty fruit bunch for hydrogen-rich gas production in a fluidized-bed reactor, *Energy Conversion and Management*. 52 (2011) 1555-1561.

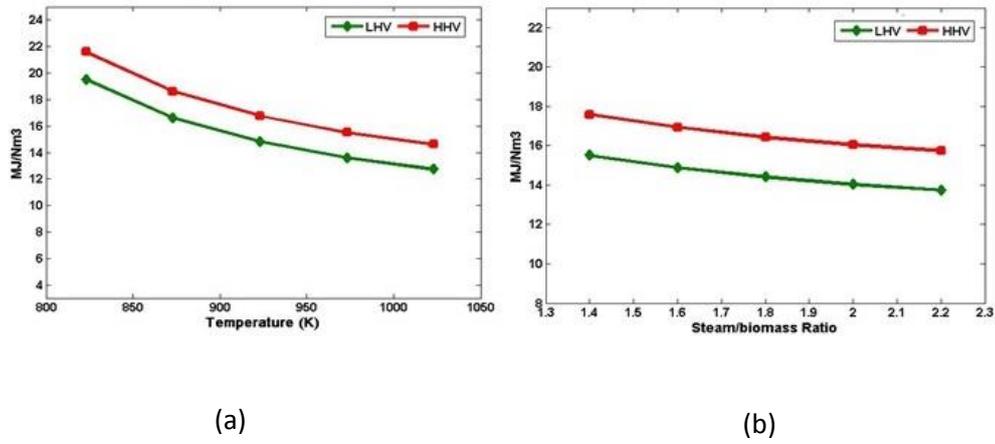


Fig. 1: (a) Effect of temperature on lower heating value and higher heating value of gas product. (Steam/biomass ratio=1.8, Sorbent/biomass ratio=0.9); (b) Effect of steam/biomass ratio on lower heating value and higher heating value of gas product. (T=973 K, Sorbent/biomass ratio=1.0).

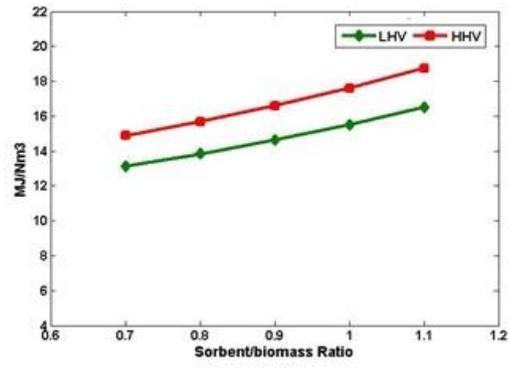


Fig. 2: Effect of sorbent/biomass ratio on lower heating value and higher heating value of gas product. (T=973 K, Steam/biomass ratio=1.4).

Table 1: Comparison of for LHV based on biomass gasification.

| Gasification Process | Biomass               | T (K) | LHV<br>MJ/Nm <sup>3</sup> | Reference     |
|----------------------|-----------------------|-------|---------------------------|---------------|
| Air                  | EFB                   | 1123  | 12.84                     | [25]          |
| Steam-Catalyst       | Municipal Solid Waste | 973   | 14.44                     | [7]           |
| Steam-Catalyst       | Pine Sawdust          | 1123  | 12.67                     | [8]           |
| Steam-Catalyst       | Oil Palm Waste        | 1023  | 11.26                     | [10]          |
| Steam-CaO            | Larch                 | 1023  | 15.48                     | [12]          |
| Steam-CaO-Catalyst   | EFB                   | 823   | 20.20                     | Current Study |