

§35. Symmetry of Reversal of Swirling Flow
Based on Variational Approach with the
Aid of Helicity

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Based on the variational approach, the reversal of the swirling flow has been described by the equation

$$\mathbf{\Omega} = -\frac{1}{\lambda} \nabla \times \mathbf{\Omega}, \quad (1)$$

where $\mathbf{\Omega}$ is the vorticity of the flow. An axisymmetric solution was obtained, and a reversal of axial flow was demonstrated. In order to relax the axisymmetric condition, we write

$$\mathbf{U} = (U_r(r, \theta), U_\theta(r, \theta), U_z(r, \theta)), \quad (2)$$

$$\mathbf{\Omega} = (\Omega_r(r, \theta), \Omega_\theta(r, \theta), \Omega_z(r, \theta)). \quad (3)$$

From the vorticity equation (1), we have a general solution as

$$\Omega_z = \Omega_z^{(c)} J_0(\lambda r) + \sum_{n=1}^{\infty} (\Omega_{zn}^{(c)} \cos n\theta + \Omega_{zn}^{(s)} \sin n\theta) J_n(\lambda r) \quad (4)$$

$$\Omega_\theta = -\Omega_z^{(c)} J_1(\lambda r) + \frac{1}{\lambda} \sum_{n=1}^{\infty} (\Omega_{zn}^{(c)} \cos n\theta + \Omega_{zn}^{(s)} \sin n\theta) \frac{d}{dr} J_n(\lambda r) \quad (5)$$

$$\Omega_r = \frac{1}{\lambda} \sum_{n=1}^{\infty} (n\Omega_{zn}^{(c)} \sin n\theta - n\Omega_{zn}^{(s)} \cos n\theta) \frac{J_n(\lambda r)}{r} \quad (6)$$

where $\Omega_{zn}^{(c)}$ and $\Omega_{zn}^{(s)}$ are numerical coefficients. The flow velocity \mathbf{U} may be expressed as

$$U_z = U^{(N)} - \frac{1}{\lambda} \Omega_z^{(c)} J_0(\lambda r) - \frac{1}{\lambda} \sum_{n=1}^{\infty} (\Omega_{zn}^{(c)} \cos n\theta + \Omega_{zn}^{(s)} \sin n\theta) J_n(\lambda r) \quad (7)$$

$$U_\theta = \frac{\Omega_z^{(c)}}{\lambda} J_1(\lambda r) - \frac{1}{\lambda^2} \sum_{n=1}^{\infty} (\Omega_{zn}^{(c)} \cos n\theta + \Omega_{zn}^{(s)} \sin n\theta) \frac{d}{dr} J_n(\lambda r) \quad (8)$$

$$U_r = -\frac{1}{\lambda^2} \sum_{n=1}^{\infty} (n\Omega_{zn}^{(c)} \sin n\theta - n\Omega_{zn}^{(s)} \cos n\theta) \frac{J_n(\lambda r)}{r} \quad (9)$$

In order to simply see effects of nonaxisymmetric components, we retain the lowest-order component as

$$\Omega_{zn}^{(c)} = \Omega_{z1}^{(c)} \delta_{n1}, \quad \Omega_{zn}^{(s)} = 0. \quad (10)$$

The present solution is not valid in the near-wall region, as is noted in the main text. In the calculation of dissipation the integral

$$\Phi = \int_V \left(\frac{\partial U_j}{\partial x_i} \right)^2 dV$$

is used, and the helicity is given as $\Psi = \int_V \mathbf{U} \cdot \mathbf{\Omega} dV$.

We limit the volume integral to the range $r \leq r_M$ per unit length of a cylinder. After a lengthy mathematical manipulation, we have

$$\Phi = 2\pi \Omega_z^{(c)2} r_M^2 J_0(\lambda r_M)^2 + \pi \Omega_{z1}^{(c)2} \left\{ r_M^2 J_0(\lambda r_M)^2 + 2\lambda^{-2} (1 - J_0(\lambda r_M)^2) \right\} \quad (11)$$

$$\Psi = \pi (2\Omega_z^{(c)2} + \Omega_{z1}^{(c)2}) r_M^2 \lambda^{-1} J_0(\lambda r_M)^2. \quad (12)$$

From Eqs.(11) and (12), Φ is rewritten as

$$\Phi = \lambda \Psi + 2\pi \Omega_{z1}^{(c)2} \lambda^{-2} (1 - J_0(\lambda r_M)^2). \quad (13)$$

From the eigenvalue condition $J_1(\lambda r_M) = 0$, we have

$$J_0(\lambda r_M) = -0.36. \quad (14)$$

In Eq. (13), the second term is positive from Eq. (14). This fact indicates that the minimum- Φ state under the constraint of fixed Ψ is realized for

$$\Omega_{z1}^{(c)} = 0. \quad (15)$$

That is, the axisymmetric condition is given as the minimum state of Φ .

Reference

Akira Yoshizawa, Nobumitsu Yokoi, Shoiti Nisizima, Sanae-I. Itoh, Kimitaka Itoh: NIFS-680 (2001)