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The probability of climatically derived seasonal surface runoff in southern Ontario.

C. V. Ramasastry
University of Windsor

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THE PROBABILITY OF CLIMATICALLY DERIVED SEASONAL
SURFACE RUNOFF IN SOUTHERN ONTARIO

by

C. V. Ramasastry

A Thesis
Submitted to the University of Windsor in
partial fulfillment of the requirements
of the degree of Master of Arts
Department of Geography

1976

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ABSTRACT

This thesis presents maps of the probability of climatically derived seasonal surface runoff in southern Ontario for the four seasons based on climatic data of temperature and precipitation from about forty-one climatic stations. The method, which is based on the Phillips modification to the Thornthwaite-Mather water balance model is discussed and tested in a small watershed, Duffin Creek. From the correlations obtained between measured runoff and runoff computed by means of the Thornthwaite-Mather and Phillips models, it was found that the Phillips model is a better estimator of runoff for southern Ontario.

The resulting runoff probability maps based on the Phillips model indicate that highest probable amount of runoff is likely to occur in the spring season. In all seasons, the maximum probable runoff is likely to occur in the areas to the east of Georgian Bay and Lake Huron.

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CHAPTER 1

1.1 Introduction

It is well known that runoff at a place varies from year to year and month to month. For agricultural and hydrological purposes it is desirable to know the variability of such runoff as well as its average amount. For any area, it is important to express runoff in terms of its probabilistic occurrence.

Precipitation probabilities which have been studied by many authors, are usually derived from measured data of precipitation. Similarly, it would be desirable to use actual measured values of runoff for constructing maps of runoff probability. However, this ideal is difficult to achieve. For example, in southern Ontario only twenty-four drainage basins have runoff records of more than 15 to 20 years duration. The climatological stations for the same period of record outnumber by three to one the number of hydrometric sites with comparable records. Besides being more numerous, climatological installations have the additional advantage of being more uniformly distributed and less subject to instrumental failure in their measurement. Thus, one of the classical techniques in hydrometeorology is the augmentation of short streamflow records by inter-

polation from climatological and hydrometeorological data. Where streamflow records are inadequate, estimates of runoff can be obtained by comparing precipitation with evaporation losses.

Studies of runoff are of importance for planning irrigational schemes, water resource management, water transportation and agricultural operations. Especially in Canada, which has about 10 per cent of the world's fresh water resources, water surplus, that amount of water that annually and seasonally runs off the surface of the land, and its time and probability of occurrence is of importance to industry and agriculture. At the present time in southern Ontario, information on runoff is desirable because of its importance to the pollution flowing from agricultural and forest lands into the boundary waters of the Great Lakes System. In addition, the province is one of the most densely populated and highly industrialized areas in Canada. Although it contains only 11 per cent of the total improved farmland, the area produces about 30 per cent of the total value of farm products, ranking first in agricultural production on a per unit basis. Approximately half of the fruit, two-thirds of the vegetables and over 40 per cent of Canadian dairy products come from this area.

The International Joint Commission of the United States and Canada has set up an International Reference Group on Great Lakes Pollution from Land Use Activities,

PLUARG. One of the tasks of this group (Task C) is to carry out intensive studies of a small number of representative watersheds, selected and conducted to permit some extrapolation of data to the entire Great Lakes basin and to relate contamination of the water quality, which may be found at river mouths on the Great Lakes, to specific land uses and practices. The present study is part of this task.

For the quantitative estimation of runoff the use of information collected from the hydrological network provides a new dimension for the climatologist. No longer are the studies on runoff limited to gauged networks or where streamflow records are numerous; however, climatological parameters in computing runoff have their own limitations, as these parameters cannot take into account all the factors that contribute to runoff. The present study makes use of climatological data in an effort to obtain information on seasonal runoff.

1.2 The problem and study area

Runoff probabilities on a seasonal basis are unknown in the southern Ontario region. In the present study, an attempt is made to construct maps of runoff probabilities for the four seasons. It is hoped such maps will be useful to resource planners, engineers involved in the construction of dams and water power

developments, both for domestic and industrial purposes, and to assess the amounts of pollutants entering into the Great Lakes System.

The study area for the present investigation is southern Ontario as defined by Brown (1968). The region is bounded by the Great Lakes on the south, west and north-west, and the Ottawa and St. Lawrence Rivers on the east. From the level plains bordering Lakes Erie and Huron, there is a gradual rise in elevation in a generally north-easterly direction to the Dundalk uplands. The crown of this upland stands about 300 meters above the lakes and terminates at the brow of the Blue Mountain section of the Niagara Escarpment, overlooking the lower lands to the east and Georgian Bay to the north.

1.3 Water holding capacity of soils

In order to compute the water balance at a place it is necessary to know information on the water holding capacity of the depth of soil for which the balance is to be computed. The Soil Association of Southern Ontario map (John, 1971) shows eight major divisions and sixty-eight minor ones in the region. Many of the southern Ontario soils have been grouped and reclassified by John (1971) according to Laboratory of Climatology system using the Thornthwaite-Mather (1957) water balance model. His classification shows five major types, fine sandy loam in

the northwest and toward the south, silt loam soils around the Dundalk uplands and part of Muskoka area, clay loam and clay type of soils on the bordering areas on the east and western portions of the region.

Soil and vegetation are the determining factors of the water holding capacity of soil at a place. Sandy soils hold less water per unit depth than clay soils. Based on the soil types and the land use patterns in southern Ontario earlier workers (Sanderson, 1966; John, 1971 and Phillips, 1975) used soil capacities ranging from 152mm. to 330mm.

1.4 Climatic conditions in southern Ontario

Climate varies considerably across the whole region because of the nature of the climatic controls and physiographic setting in the distribution of land and water bodies.

Precipitation

Brown (1968) reported the mean annual precipitation distribution in southern Ontario. The areas of highest precipitation are found at elevations of 360 to 420 meters on the slopes east of Lake Huron and Georgian Bay and receive 1020 millimeters. The average precipitation ranges from about 660 in the southwest (Essex County) to 1020 millimeters in the area west of Georgian Bay.

Snowfall in southern Ontario is one of the elements that affect the seasonal distribution of the runoff pattern. The frequency of shifting low pressure systems, cold arctic air masses in winter, and the extent of ice cover over the lakes are important controls in determining the amount of snow. In southern Ontario, snowfall accounts for about 30 per cent of total annual precipitation in the Leamington region (Brown, 1968). The mean annual snowfall in the region ranges from over 2790 millimeters in the Huron, Georgian Bay and Muskoka regions to less than 1220 millimeters near Hamilton and to about 890 millimeters in the Kent-Essex region.

Evapotranspiration and the water balance

The concept of potential evapotranspiration, the amount of water loss due to evaporation and transpiration from an extensive, closed homogeneous cover of vegetation that never suffers from a lack of water, was introduced to the climatic literature by Thornthwaite (1948) and subsequently used to define other water budget and moisture parameters.

Potential evapotranspiration, when expressed in terms of depth of water alone, is an index of both thermal efficiency and water needed for growth of plants. Average annual potential evapotranspiration and mean annual actual evapotranspiration for southern Ontario as reported by

Brown (1968) according to the 1948 system of Thornthwaite indicate that most of southern Ontario has an annual potential evapotranspiration of at least 530 millimeters with a maximum of about 660 millimeters over the Leamington region, while lowest values are found in the Dundalk upland and the Algonquin Park region.

Variations in actual evapotranspiration occur when soil moisture is depleted by evapotranspiration and subsequently replaced by precipitation. The soil supply is at potential rate only during periods of rain or irrigation; at other times it is less than potential rate. By assuming a soil moisture holding capacity, Thornthwaite obtained actual annual estimates of water used by crops from a simple accounting of evapotranspiration. The mean values of actual evapotranspiration in southern Ontario are about 530 millimeters and show regional variation. The highest value, 580 millimeters, is found just northwest of London.

In southern Ontario during the cool half-year precipitation greatly exceeds water need and, after the soil moisture has been recharged, moisture surplus occurs. During the periods of rain, rainfall replenishes soil moisture until the soil moisture holding capacity is reached. Precipitation in excess of that needed to saturate the soil is considered as a surplus which runs off and is available as surface runoff, or percolates to the water table. Much of the surplus water in southern

Ontario is deposited on the ground as snow and usually runoff does not take place in large quantities until the spring season. Table 1 illustrates the bookkeeping procedure for computing the monthly estimates of actual evapotranspiration and climatic water budget for Pickering, Ontario, as described by Thornthwaite and Mather (1955) and the details of the computational procedure may be obtained from "Instructions and Tables for Computing Potential Evapotranspiration and the Water Balance" (Thornthwaite and Mather, 1957).

Figure 1 indicates the water surplus map according to Sanderson and Phillips (1967). One can observe great differences in annual water surplus, from 150 millimeters in Essex County to more than 500 millimeters in the Algonquin Park uplands.

Month to month variation in runoff across southern Ontario can be seen in Figure 2, representative hydrographs based on hydrometric data (Surface Water Data) for Duffin Creek above Pickering and the Thames River at Ingersoll. The hydrographs indicate that highest runoff occurs during the winter and spring seasons (29 and 48% respectively) while summer and fall seasons have low runoff (11 and 12% respectively). Winter and spring runoff together account for about 74 per cent of the total annual runoff, while summer and fall amounts constitute for only 26 per cent.

The spatial variability of runoff is due to the

TABLE 1
CLIMATIC WATER BALANCE (THORNTHWAITE AND MATHER, 1955)
PICKERING, ONTARIO - 1970

	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Year
TEMP	-8.30	-6.10	0.80	7.10	11.20	18.20	20.60	20.70	16.10	10.90	5.30	-4.00	7.71
UNPE	0	0	0	1.0	1.8	3.0	3.3	3.5	2.5	1.8	0.7	0	
ADPE	0	0	0	34.0	67.3	117.0	128.0	128.0	79.2	50.5	18.5	0	622.5
PCPN	51.7	31.8	50.2	84.6	62.7	30.0	86.9	49.5	65.0	77.2	46.0	73.4	709.0
P-PE	51.7	31.8	50.2	50.6	-4.6	-87.0	-41.1	-78.5	-14.2	26.7	27.5	73.4	
APWL	0	0	0	0	-4.6	-91.6	-132.7	-211.2	-225.4	-138.6	-82.3	0	
STOR	251.1	282.9	152.4	152.4	148.2	83.6	64.0	38.1	34.8	61.5	89.0	158.2	
DST	0	0	0	0	-4.2	-64.6	-19.6	-25.9	-3.3	26.7	27.5	69.2	
AEV	0	0	0	34.0	68.9	94.6	106.5	75.4	68.3	50.5	18.5	0	514.7
DEF	0	0	0	0	0.4	22.4	21.5	52.6	10.9	0	0	0	107.8
SURP	0	0	180.7	50.6	0	0	0	0	0	0	0	0	231.3
ROFF	0.2	0.1	18.0	106.7	53.4	26.7	13.3	6.7	3.3	1.7	0.8	0.4	231.3

TEMP Monthly mean daily temperature °C
 UNPE Unadjusted potential evapotranspiration
 ADPE Adjusted potential evapotranspiration
 PCPN Precipitation in millimeters
 P-PE Precipitation minus potential evapotranspiration
 APWL Accumulated potential water loss
 STOR Storage
 DST Change in storage
 AEV Actual evapotranspiration
 DEF Water deficiency
 SURP Water surplus
 ROFF Runoff

All values except temperature are in millimeters.

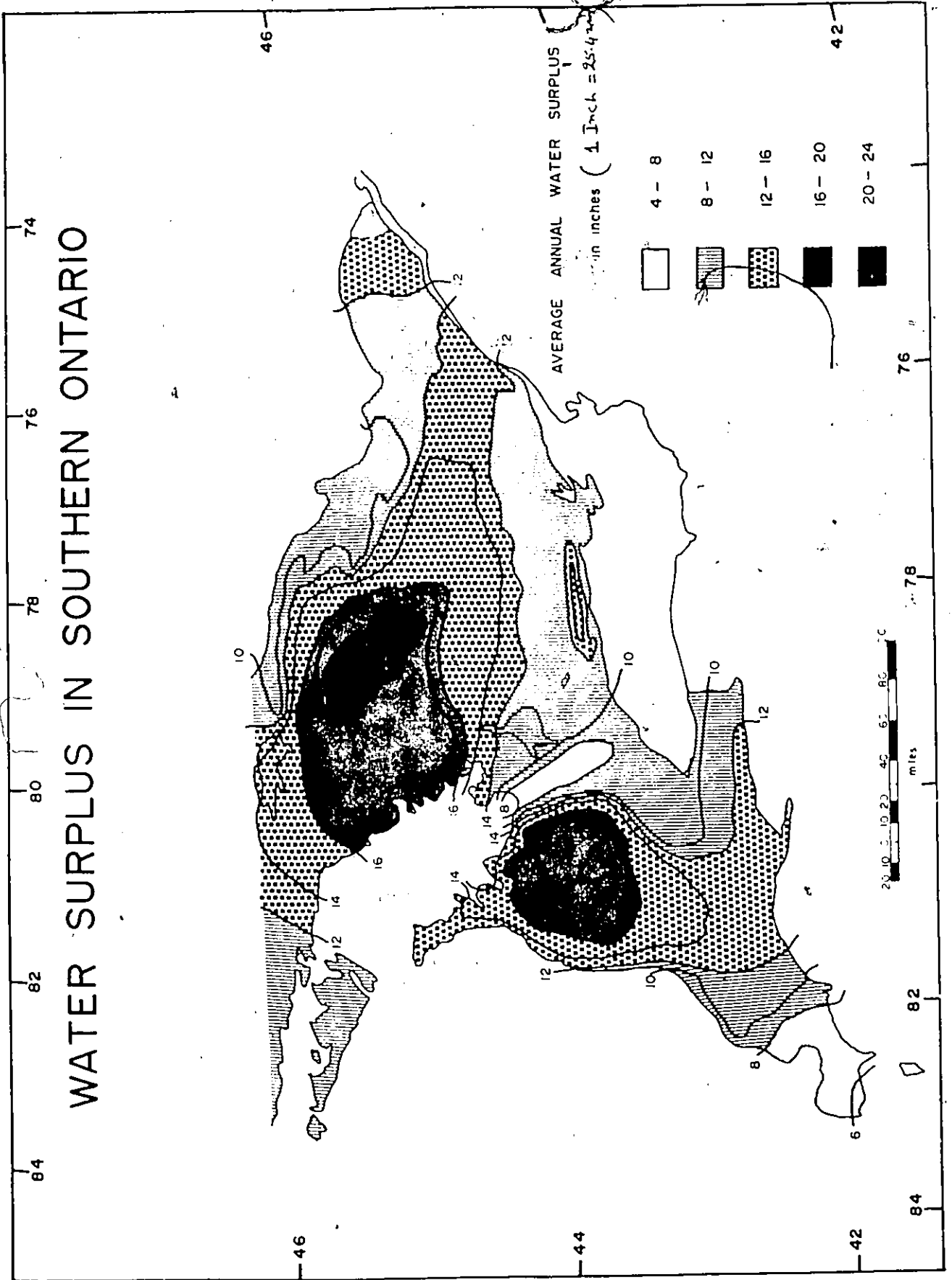


Figure 1

various factors such as climatic and physiographic controls. Only after the factors responsible for the seasonal fluctuation have been ascertained is it possible to design a suitable technique to compute runoff theoretically.

CHAPTER 2

2.1 Runoff theory

Ward (1967) defined runoff as "the gravity movement of water over the earth," and further stated that it is the amount which remains from precipitation when allowance is made for evapotranspiration and storage both above and under the ground surface. Runoff can be better understood from a comprehensive description of the hydrologic cycle in terms of three principal phases - precipitation, evaporation and runoff, both surface and subsurface. In the hydrologic cycle, water evaporates from the oceans and the land, and becomes a part of the atmosphere. The evaporated moisture is lifted and carried in the atmosphere until it precipitates to the earth, either on land or in the oceans. The precipitated water may be intercepted or transpired by plants, may run over the ground surface and into streams to oceans, or may infiltrate into the ground. Much of the intercepted and transpired water and some of the surface runoff returns to the air through the process of evaporation and transpiration. The infiltrated water may percolate downward to be temporarily stored as ground water which later flows out of rocks as springs or seeps into streams as runoff to oceans, or evaporates into the

atmosphere to complete the cycle.

Surface runoff is mainly derived from precipitation through three main component sources. First, runoff from rainfall, which is intermittent with its occurrence dependent entirely on the rate of rainfall being in excess of the loss rate due to evaporation, transpiration and percolation. Secondly, there is the snowmelt runoff from accumulated snowfall, which is an important source in colder climates. Lastly, there is a contribution to runoff from ground water storage and it is replenished by infiltration which constitutes a loss from the rainfall and snowmelt contributions to the runoff.

Climate and physiography are the important factors that influence the distribution of surface runoff. Under climate the parameters that influence runoff are precipitation, interception, evaporation and transpiration. Of these, probably the most important factor governing runoff is the precipitation - form and type, intensity and duration, time and areal distribution, frequency and storm movement and direction. In southern Ontario, during winter and spring months, precipitation in the form of snow poses problems. If temperatures are cold enough, the atmosphere supplies the moisture both for snowfall and for condensation of water vapour on the snow surface, while meteorological factors control the interchange of energy in the basin snowpack. During the snowmelt period, much water from the snow

surface will begin to move downward into the lower layers of the snowpack where, since temperatures are usually below the freezing point, refreezing of the meltwater will occur. Additional heat will be added to the snowpack both from the air above and from the ground below so that after a period the temperature of the entire pack will approach 0°C .

Meltwater continues to be absorbed by the snowpack until the liquid water-holding capacity of the pack is reached and the snow is defined as ripe. The density of the snowpack which has been increasing remains fairly constant after the water holding capacity is reached. Additional melt water now moves downward through the snow to the ground surface and, depending on the infiltration capacity of the soil and the rate of melting of the snow, the melt water will either a) enter soil and move through it, or b) form a slush layer at the surface that will both contribute to moisture infiltrating the soil surface, or to the overland runoff from the area.

Any attempt to estimate runoff theoretically, in particular in southern Ontario, must take into account the vital contribution of snowmelt to the spring and winter season runoff, or its potential for storage and subsequent appearance as runoff.

Generation of snowmelt at a point location in a snowpack is mainly due to thermodynamic processes, although travel of the melt water to another point in the pack

depends on physiographic (gradient, depth, etc.) and hydrodynamic (porosity, structure, storage, etc.) properties.

The important sources and processes influencing heat transfer to or from a snowpack are listed below:

Absorbed short wave (solar) radiation, R_s

Net long wave (terrestrial and atmospheric) radiation, R_b

Condensation (or vaporization) from the air, R_h

Heat content of rain water, H_r

Conduction of heat from ground, H_g

The melt water produced by the net transfer of heat from all sources to the snowpack may be obtained as

$$M = H / 80 B$$

where

M - water equivalent of snowmelt (Cms.),

H - algebraic sum of all heat contributions (cal/cm^2), and

B - thermal quality of the snowpack, defined as the ratio of heat required to melt a unit weight of snow to that of ice at 0°C (average from 0.95 to 0.97, for 3 to 5 per cent liquid water).

The constant 80 is the heat input in Cal/sq.cm required to produce one inch of water (25mm.) from ice at 0°C .

While the individual physical relations can be

utilized to determine the effect of different meteorological, ground and vegetation conditions on the snowmelt and consequent runoff at a point, they are hardly satisfactory to apply over a large area because of the myriad of complex factors involved.

The physiographic characteristics are the second major factor influencing surface runoff. These include a) geometric influences - size, shape, slope, orientation, elevation, stream density, b) physical factors such as land use, soil cover and type, topographical features, and c) channel characteristics such as storage capacity of the soil, discharge capability, bed slope, channel roughness, and braiding and meandering tendencies.

In the climatological studies of runoff, among the several physiographic factors that influence runoff, soil moisture storage is of importance. Soil moisture may be determined simply as a result of a bookkeeping procedure in which all precipitation occurring when the soil moisture content is below field capacity is treated as a moisture increment and moisture is lost from the soil only by evapotranspiration. Precipitation occurring when the soil is above field capacity is treated as surplus; some of it is lost as percolation to contribute to ground water storage to appear as springs and underground streams, some flows out as surface runoff. All of this surplus available for runoff in a particular month may not be lost in that month,

as some of the surplus water is often detained on the watersheds past the end of the month and will run off in succeeding months.

2.2 Methods of estimating runoff

The construction of runoff probability maps on a monthly or seasonal basis would be simple if the gauged values of runoff covered extensive areas with long periods of record or if a perfect technique to estimate runoff were available.

In recognition of the role of climatic parameters in runoff distribution, several attempts have been made in the past to develop simple annual yield expressions incorporating mean temperature and precipitation.

Theoretically, runoff at a place can be estimated from the water balance equation

$$R = (r + s) - (E + T + S_t + U)$$

where

R - Runoff from drainage area

r - Precipitation in the form of rainfall

s - Precipitation in the form of snowfall

E - Direct evaporation

T - Transpiration from plants and vegetation

S_t - Change in storage

U - All other factors (Underground flow, etc.).

In the above equation, only precipitation both in

the form of snow and rainfall can be measured accurately. If it is possible to estimate precisely evaporation, transpiration and all other factors, one can compute runoff at a place using the above relation. However, in actual practice, the limiting factors are the measurement of evaporation, transpiration and underground flow.

Realizing the above relationship between runoff, precipitation and evapotranspiration, several workers (Bruce and Rodgers, 1954; Carter, 1955; Morton and Rosenberg, 1959; Brunk, 1961; Bruce, 1962; Derecki, 1964; Sanderson, 1966 and 1971; Pentland, 1968, and Phillips, 1975) have attempted to calculate runoff from climatic data by energy budget and degree-day methods.

In recent years, climatic estimation of runoff gained new popularity after Thornthwaite (1948), who formulated a bookkeeping model as the basis of his climatic classification. Later it was modified by Thornthwaite and Mather (1955) to make it more meaningful under a wide range of soil and vegetation conditions. Table 1 illustrates the procedure for computing the monthly climatic water balance for Pickering, Ontario. The advantage of Thornthwaite's water balance model is its relative simplicity of computation requiring data only on air temperature, precipitation and latitude.

Muller (1966) used Thornthwaite's water balance model as one of the approaches in his study of the effect

of reforestation on water yield and computed the annual runoff from four small watersheds in the Allegheny Uplands of New York State for each year from 1935 to 1957. He reported that measured runoff tended to be greater than computed runoff at the beginning of the study when forests covered 20 to 50 per cent of the watersheds; measured runoff was less than computed in the latter years when forests covered 80 to 90 per cent of three watersheds.

Recently, Solomon (1967) calculated runoff both on an annual and long term basis, taking into account the difference between recorded precipitation and computed evaporation.

Mather, et. al. (1972) applied the climatic water budget bookkeeping technique in Delaware and New Jersey in the eastern United States to compute net flow figures for a 20-year period starting in 1949 and concluded that the calculated values of net flow are quite consistent with other available meteorologic and hydrologic information.

Many of the above studies employ the climatic bookkeeping approach either directly or with slight modification. Where studies of streamflow are based on the original Thornthwaite climatic water balance model, estimated streamflow values fluctuate markedly from measured values particularly in spring and winter months. This discrepancy between computed and measured values might be because

Thorntwaite, in his original scheme, has made no allowance to account for runoff resulting when precipitation occurs as snow when mean monthly temperature remains at or close to 0°C. Also, in the original model developed by Thorntwaite, no allowance was made for accounting for the effect due to convective summer storms. As a result of snow accumulation, runoff occurrence is from the delayed surplus which collects during spring and winter months. Furthermore, winter months have little flow and runoff is sufficiently delayed so as not to correspond with measured values in the spring.

Realizing the drawbacks in the Thorntwaite book-keeping model, Van Hylckama (1958) developed nomograms to account for direct runoff by planimentering the areas between runoff and base flow curves for each month. These amounts were then subtracted from precipitation amounts, to arrive at effective precipitation. He then applied the technique to the Delaware Valley basin, giving due weight to the occurrence of snow and the rate of snowmelt, the amount and nature of direct runoff from intense precipitation and the influence of local characteristics such as soil depth, average slope and stream density on the rate of runoff. Compared to the Thorntwaite model, the Van Hylckama modification to account for snow runoff to the original Thorntwaite water balance model is a significant advance with improved estimates in every season. However,

the difficulty in his system is in the additional computations making the system tedious to use.

Using Thornthwaite's climatic bookkeeping model, Sanderson (1966) evaluated each of the factors of the water budget for the Lake Erie basin for the period 1958 to 1963. Comparing these results with average conditions over the lake basin, she sought new understanding of the factors responsible for changing lake levels. During her investigations she suggested modification to the original climatic model in an attempt to arrive at a simple method for determining winter runoff based on two assumptions: a) that snowmelt runoff during the months with mean temperature -0.9°C need not be considered zero but modified by the number of days with maximum temperature greater than 0°C ; b) that runoff in the first month with mean temperature greater than 0.9°C be considered as 50 per cent of available water surplus. Employing these assumptions, Sanderson found a 0.99 correlation between measured and computed annual runoff for the Grand River basin.

In an unpublished B.A. thesis, Phillips (1967) used runoff records at seven drainage basins in southern Ontario for a ten year period to compare with the computed annual water surplus. Using only one station in each basin, he obtained a correlation coefficient of 0.86 between measured and computed annual runoff. One obvious drawback in the above two studies is that in dealing with snowmelt similar

weight is given to all days with the same mean temperatures. This might result in overestimation of the energy available for snowmelt in cold months and underestimation during the warm periods.

Using five different drainage basins in southern Ontario, John (1971) reported that the Thornthwaite water balance model overestimates runoff in the high runoff period (January to June), and underestimates it in the low runoff period (July to December) and further indicated the model yields good results when applied to large basins. His computed values of runoff based on three stations in the Duffin Creek basin overestimated runoff, with correlation of 0.75 for the January to June period while in the period July to December the underestimated values yielded 0.81 correlation. On an annual basis he obtained a high correlation of 0.90. The overestimation and underestimation during periods of high and low runoff periods may be because the Thornthwaite model uses only temperature in estimating evaporation. Basically, evaporation is a function of radiation rather than temperature and in most of southern Ontario, the amount of incoming insolation is highest during May, June and July, while air temperature reaches a maximum only in July and August. Also, although there could be days within a month with above or below freezing temperatures, the Thornthwaite model assumes no resulting runoff for a month when the average temperature

is below 0°C :

A heat related unit sometimes used in hydrometeorology to account for snowmelt is the degree-day, a unit expressing the amount of heat in terms of a twenty-four hour period. The degree-day or degree-hour values (temperature summation above a base temperature) can be correlated with runoff values. The approach is only a rough estimate as many other factors besides temperature influence snowmelt. Several workers have given values ranging from 1.27mm. to 5mm. of snowmelt per degree-day under conditions of continuous snow cover and with temperatures above freezing (Collins, 1934; Bruce, 1962).

Garstka, et. al. (1958) in their studies on snowmelt in Colorado, observed that a daily maximum temperature was a better reference point than mean, since a mean temperature of 0°C need not necessarily indicate that melting would not occur. Similarly, Collins (1934) attempted to forecast runoff based entirely upon degree days above freezing.

Generally, applications of the climatic bookkeeping approach for theoretical estimation of runoff have dealt with large areas and average conditions with emphasis on annual yields. For yields in specific years, Sanderson (1966) in southern Ontario and Mather (1969b) in Delaware, found correlations ranging from 0.90 to 0.99 between computed and measured runoff. However, when small areas or seasonal

or monthly time periods are considered, the results are less reliable.

In order to test the applicability of the Thornthwaite climatic bookkeeping approach for estimating runoff on a monthly and seasonal basis, the model has been applied to a small watershed in southern Ontario, Duffin Creek gauged at Pickering.

CHAPTER 3

3.1 The Duffin Creek watershed

The watershed, Duffin Creek (at Pickering) has an area of about 176 sq. kilometers and it is drained by natural water courses. This watershed was selected out of several small watersheds in the southern Ontario area after a careful examination of their climatic record of data, and based on the following criteria:

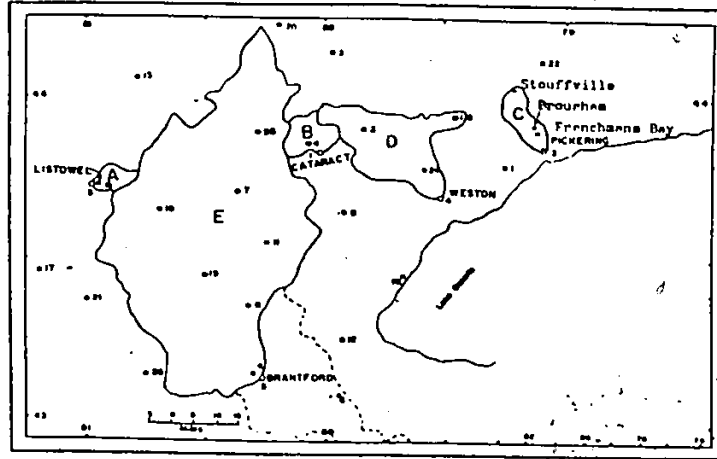
- a) the drainage water flow at the measuring site should be natural,
- b) watersheds selected should lie within southern Ontario and the period of record of gauged runoff should be continuous during the period of study, and
- c) the selected watershed should be nearly representative of the rest of southern Ontario. The representative characteristic of the selected watershed to the rest of southern Ontario has been established by comparison of the moisture index of Thornthwaite (1948), which represents both thermal and moisture

conditions at a place. According to Sanderson's (1950) moisture relationships in southern Ontario, most of the region falls within the fourth humid to first humid category, and the selected watershed at Pickering has a moisture index of 45.6 and can be classified as second humid, a characteristic which indicates a resemblance to the rest of southern Ontario. Figure 3 shows the location of the watershed and the locations of the meteorological stations used to test the model.

Elevations in the watershed generally increase northwards, reaching a height of about 360 meters in the extreme north, while the lowest elevations in the south are at 87 meters around Pickering. The watershed has a much varied topography which approximately resembles the rest of southern Ontario. The northern section is part of the Peel plain physiographic region and the extreme southern tip is also plain area.

The surface soils in the Duffin Creek watershed, like all those of southern Ontario, are the result of glacial action (Report on Flood Control and Water Conservation, 1962). In the northeast and south central parts of the basin, the prevailing soil is Fox grey-brown podzolic

LOCATION OF DRAINAGE BASINS, METEOROLOGICAL AND HYDROMETRIC STATIONS (after John, 1971.)



DUFFIN CREEK (ONTARIO)
ABOVE PICKERING
ELEVATIONS



Contour Interval = 100 Feet



- A MIDDLE MAITLAND RIVER (ONTARIO) ABOVE LISTOWEL
- B CREDIT RIVER (ONTARIO) ABOVE CATARACT
- C DUFFIN CREEK (ONTARIO) ABOVE PICKERING
- D HUMSER RIVER (ONTARIO) ABOVE WESTON
- E GRAND RIVER (ONTARIO) ABOVE BRANTFORD
- METEOROLOGICAL STATION
- HYDROMETRIC STATION

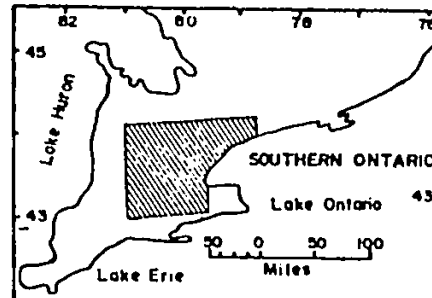


Figure 3

sandy loam. In the northeast it is coupled with the Guelph grey-brown podzolic sandy loam, while in the south it is coupled with the Granby dark grey gleisolic sandy loam on level stone-free topography.

The variation in the permeability of these soils is considerable. Pervious type of soils consisting of kame moraine, beach, boulder, and sand plain are prevalent in the upper and lower parts of the watershed and account for 36 per cent. Semipervious soils of drumlinized till plain soil type appear in the central part of the basin and constitute 44 per cent. About 20 per cent of the soil in the basin consists of bevelled till, plain and clay plain varieties and these impervious soils appear in the central and lower parts.

According to the land use maps prepared by the Canada Land Inventory, ARDA Branch (1968), there are nine different land use types in the watershed. Most of the natural vegetation within the study area has been destroyed for developing farms and land lying fallow. Approximately 13 per cent of the total area of the drainage basin is forested.

In order to compute the water balance for the watershed, it is necessary to have the following information: a) mean monthly air temperature, b) total monthly precipitation, and c) information on the water holding capacity of the depth of soil for which the balance is to

be computed.

Mean monthly air temperature and total monthly precipitation for each of the years from 1966 to 1973 at four climatic stations within the watershed, namely Brougham ($43^{\circ}55'N$, $79^{\circ}07'W$), Frenchmans Bay ($43^{\circ}49'N$, $79^{\circ}05'W$), Pickering ($43^{\circ}51'N$, $79^{\circ}03'W$), and Stouffville ($44^{\circ}00'N$, $79^{\circ}03'W$) were obtained from the Monthly Record. Information on the water holding capacity of the soil within the watershed is not directly available, but can be assessed from the soil types and land use patterns. Water holding capacity of a soil depends basically on two different factors - the soil type and structure, and the type of vegetation growing on the surface. Also, different species of vegetation will send roots down into the soil to different depths. Cultivated crops such as peas or spinach are very shallow rooted and so the depth of the root zone in which water can be stored in the soil is quite small. Tables for use in the computations of the water balance have been prepared for different soils and vegetation types by Thornthwaite and Mather (1957). Detailed information on water holding capacities may be obtained from the Instructions and Tables for Computing Potential Evapotranspiration as referenced earlier in Chapter 1.

Since in the southern Ontario region and in the chosen watershed, the crop pattern ranges from moderately deep rooted crops to deep rooted crops and the soils from

fine sand to silt loam type, an average water holding capacity of 152.4 millimeters (6 inches) was chosen for the present study.

3.2 The Thornthwaite-Mather model

Using the mean monthly temperature and monthly total precipitation and assuming a water holding capacity of 152.4 millimeters, monthly potential evapotranspiration, actual evapotranspiration and direct runoff were calculated according to the standard Thornthwaite and Mather (1957) procedure. Calculated total runoff was then summed on a three month basis, based on the simple arithmetic averages obtained from the four climatic stations within Duffin Creek watershed. The computational procedure for Pickering is presented in Table 1.

Eight years (1966-1973) of streamflow records for the watershed were obtained from the Water Survey of Canada, Surface Water Data, Ontario (1974). Water yield at Pickering is measured with current meters and the reliability of the data according to the Water Survey of Canada lies between \pm 2 to 5 per cent. In general, data measured during periods of ice conditions are less reliable and subject to error.

A measure of the relationship between computed and measured water yield on a seasonal basis for the Duffin Creek watershed can be assessed by calculating the coefficient of correlation. If 'r' is called the correlation

coefficient,

$$r = \frac{\sum xy/n - \bar{x} \cdot \bar{y}}{\sigma_x \sigma_y} \quad (3.2.1)$$

where

- x - Individual seasonal computed runoff
- y - Individual seasonal measured runoff
- n - Number of seasons
- \bar{x} and \bar{y} - Mean runoff of computed and measured
- σ_x and σ_y - Standard deviation of computed
and measured runoff.

The monthly correlations between measured runoff and that computed using the Thornthwaite and Mather approach were found to be of low order, ranging from 0.13 to 0.44. Consequently, the seasonal correlations were obtained considering the Winter to be from December to February, Spring from March to May, Summer from June to August and Fall from September to November. These values are summarized in Table 2. The correlations tabulated in Table 2 differ from season to season remarkably. The correlation coefficient +0.53 for the summer season while the correlation obtained in winter and fall seasons showed that there was little agreement between measured and computed runoff. A comparison of the correlations at the 5% and 1% level of significance indicates that significant correlation exists in summer and spring seasons while winter and fall seasons show least correlation. The

TABLE 2

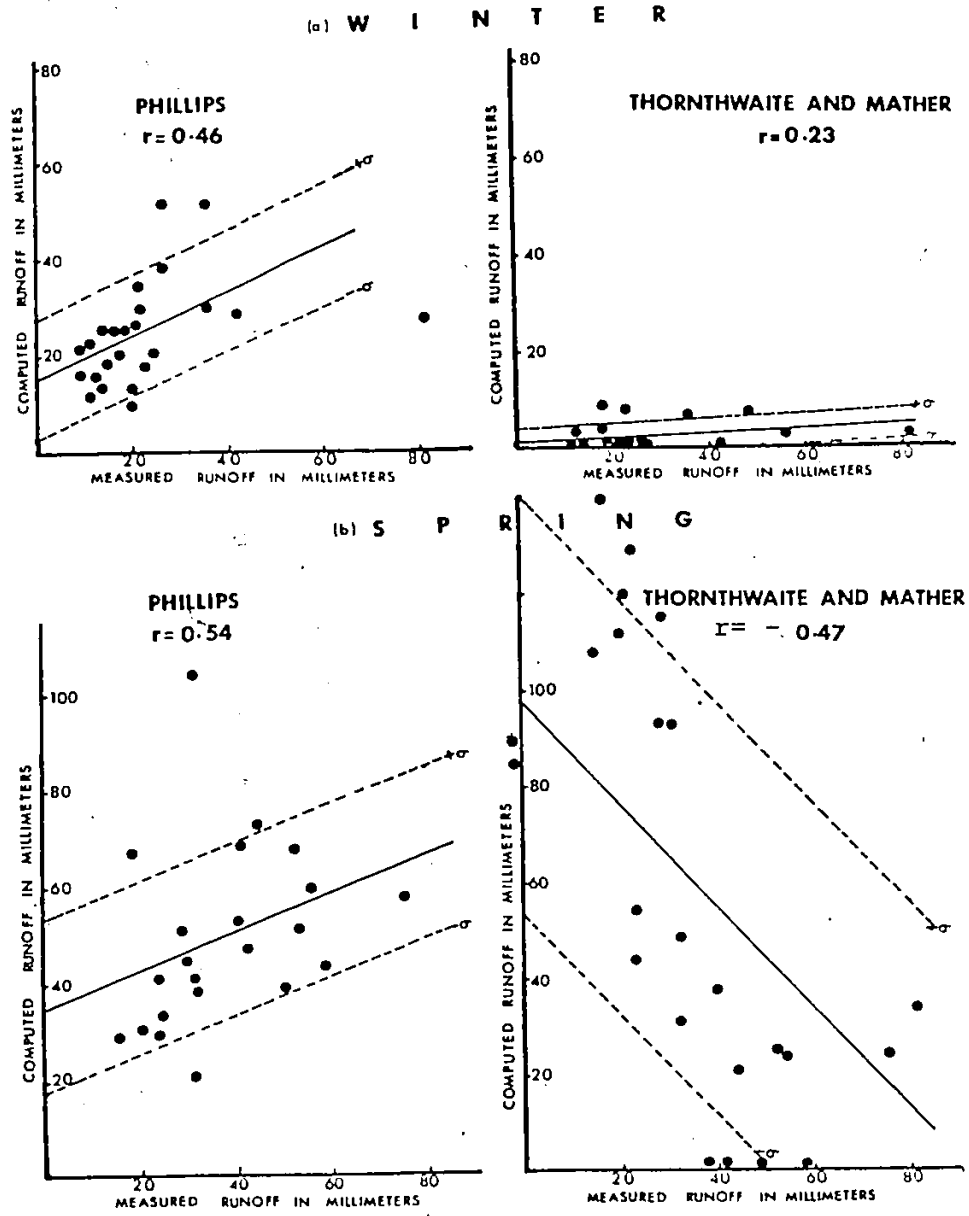
SEASONAL CORRELATIONS BETWEEN COMPUTED AND MEASURED
 RUNOFF FOR DUFFIN CREEK AT PICKERING (1966-1973)
 (Thorntwaite and Mather, 1957)

Season	Correlation Coefficient r	Coefficient of Determination r ²	t-Statistic	Level of Significance
WINTER	+0.23	0.08	1.09	greater than 10%
SPRING	+0.47	0.22	2.49	5 to 10%
SUMMER	+0.53	0.28	2.92	1 to 5%
FALL	+0.29	0.08	1.42	greater than 10%

Significance levels: At 5% = 0.40; 1% = 0.51
 (Snedecor and Cochran, 1968)

coefficient of determination calculated for the seasons indicate that only in spring and summer seasons the Thornthwaite model accounts for 22 and 28 per cent of the runoff while winter and fall seasons account for only 8 per cent. Figure 4 shows the scatter diagrams of computed and measured runoff and the continuous lines are regression lines. On the scatter diagram, the confidence limits, i.e., the standard deviation lines (dotted lines) can be used to assess how closely the computed runoff approximates measured value. These lines indicate that in all seasons, about 68.3 per cent of the computed values lie within \pm one standard deviation.

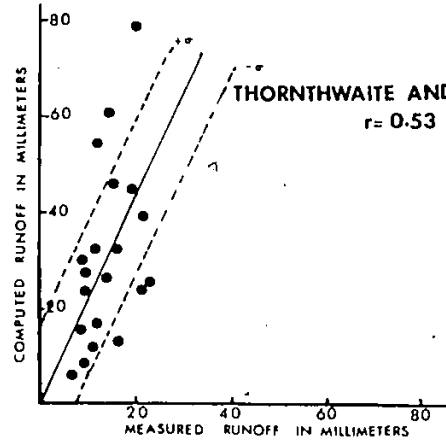
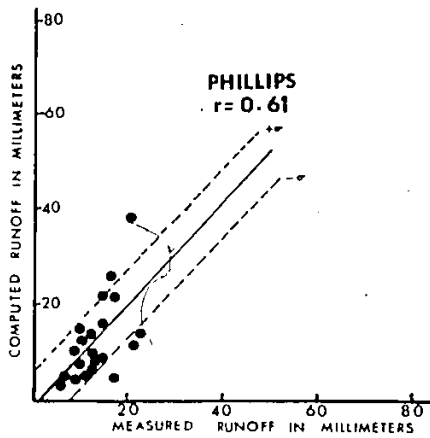
The low correlation in winter and fall is mainly because in many parts of southern Ontario during the period November through February, temperature will be below freezing and precipitation will be deposited in the form of snow. The Thornthwaite-Mather model assumes both evapotranspiration and runoff to be zero during low temperature periods when precipitation is in the form of snow. Under these conditions, total storage may exceed the water holding capacity of the soil, with the excess being deposited as snow or surface storage. When the temperature rises above freezing level in the spring, the snow accumulated above the ground is allowed first to replenish the soil moisture and the excess treated as snowmelt runoff.



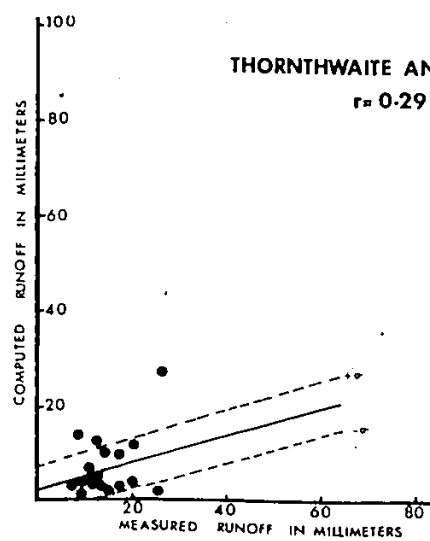
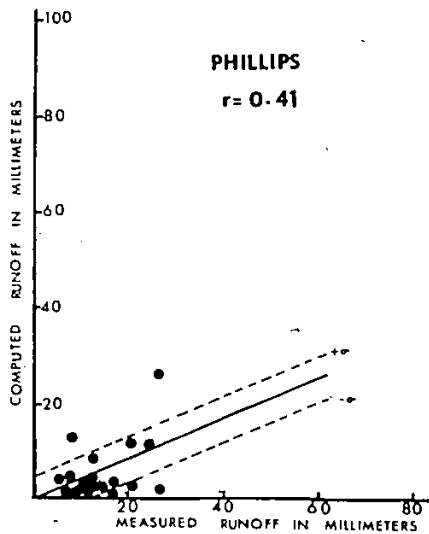
SCATTER DIAGRAMS OF COMPUTED AND MEASURED SEASONAL RUNOFF

Figure 4.

(c) S U M M E R



(d) F A L L



SCATTER DIAGRAMS OF COMPUTED AND MEASURED SEASONAL RUNOFF

Figure 4(cont'd)

3.3 The Phillips model and methodology

Many investigators have criticized the Thornthwaite and Mather model and have attempted to modify the assumptions for snow accumulation and melt. Phillips (1975) introduced a modification to the original Thornthwaite and Mather book-keeping approach to account for winter and spring runoff. The Phillips modification of the water balance in cold climates is mainly an empirical system which is designed to account for seasonal and annual variation of precipitation, evapotranspiration loss, soil moisture storage, and surplus water for runoff from snow.

Using the total number of melting degree days above base temperatures, Phillips obtained a ratio of runoff to potential runoff. Potential runoff, for this purpose, he defined as the positive difference between the storage term and its water holding capacity expressed as a percentage. The variables involved in the Phillips modification are a) the total number of melting degree days above base temperature of 0°C for the month under consideration, b) accumulated total precipitation from December to the end of the month in consideration, c) accumulated melting degree days for the various temperature bases including the month under study, d) precipitation of the month, e) mean temperature of the month, and f) potential runoff, the positive difference between the storage term and its water holding capacity or surface storage. Using these

variables, Phillips chose a multivariate technique of step-wise multiple regression to determine the significant factors by generating a series of regression equations. The following equations have been suggested by Phillips to be added to the Thornthwaite-Mather model for computing snowmelt runoff in spring and winter months:

<u>Month</u>	<u>Regression Equation</u>	
December	$\% = 82.5 + 10.3 T$	(3.3.1)
January	$\% = 37.1 + 2.5 T$	
February	$\% = 35.7 + 1.6 T - 0.8 (X-Y)$	
March	$\% = 50.1 + 3.6 T - 1.0 (X-Y)$	

where

T - is the mean monthly temperature in °C

X - is the storage value for the month

Y - is the assumed water holding capacity

% - is the ratio of actual runoff to potential runoff expressed as a percentage.

In the modified version, computation of the climatic water balance is similar to that of the Thornthwaite-Mather approach until the storage line, as can be seen from a comparison of Tables 1 and 3. Then, for each month when mean monthly air temperature is at or below freezing, precipitation is temporarily added to the soil moisture storage of the present month. When the soil moisture storage is at field capacity or above, the ratio of actual to potential runoff expressed as a percentage is calculated from the

corresponding month's regression equation. Actual runoff is computed as a product of the runoff ratio and potential runoff and entered as snowmelt runoff. The difference (potential-actual runoff) is added to the water holding capacity as the revised storage term for that month. Again in the following month, the Thornthwaite-Mather method is followed until the storage line is reached, and the revised storage and snowmelt runoff and total runoff according to the Phillips modification. Once the surplus has been entered, the next step is to determine the amount of surplus which appears as direct runoff. For southern Ontario, it has been found that 50% of the surplus will appear as runoff in each of the following months until it is all gone (Phillips, 1975). The final calculation is to enter the result (Direct runoff plus snowmelt runoff) as total runoff.

For formulating the above modification, Phillips used twenty-four years of streamflow records (1947-1973) for the Sydenham River at Owen Sound, which has a drainage area of about 110 sq. km., and temperature and precipitation records of two climatological stations, Wiaraton and Owen Sound. In order to test these empirical adjustments, Phillips tested his model in the Thames River at Woodstock (drainage area of about 150 sq. km.) using temperature and precipitation from one station for the period 1952 to 1973, and reported good correlations on a monthly basis (Phillips, personal communication).

A computer listing of the Phillips modification of the climatic water balance was made available to the author and used to compute the water yield in the present study. The program with examples of the computations for some climatic stations are presented in Appendices 1 and 2.

Using the above assumptions and assuming a water holding capacity of 152.4mm. (6 inches), the Phillips modification of the bookkeeping approach for cold climates was tested in the Duffin Creek watershed using streamflow records and climatic data from four stations for the period 1966-1973. A model computation using the Phillips technique, for Pickering, Ontario, is presented in Table 3 and yearly computations for the four climatic stations within the watershed are presented in Appendices 2 and 3. Total runoff in Table 3 was obtained by summing the direct runoff and snowmelt runoff.

Scatter diagrams have been constructed for seasonal computed and measured runoff data to indicate relationships and possible patterns of clustering among some of the data. Figure 4 shows scatter diagrams between measured and computed runoff according to the Thornthwaite and Mather approach as well as with Phillips' modification. The diagrams for all the seasons show less scatter in the case of Phillips' computed runoff verses measured, while the scatter is higher for the Thornthwaite and Mather method.

The regression intercept (a) and coefficient (b) describe how closely the computed runoff approximates the

TABLE 3
CLIMATIC WATER BALANCE (Phillips, 1975)
PICKERING, ONTARIO - 1970

	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Year
TEMP	-8.30	-6.10	0.80	7.10	11.20	18.20	20.60	20.70	16.10	10.90	5.30	-4.00	7.71
UNPE	0	0	0	1.0	1.8	3.0	3.3	3.5	2.5	1.8	0.7	0.	
ADPE	0	0	0	34.0	67.3	117.0	128.0	128.0	79.2	50.5	18.5	0	622.5
PCPN	51.7	31.8	50.2	84.6	62.7	30.0	86.9	49.5	65.0	77.2	46.0	73.4	709.0
P-PE	51.7	31.8	50.2	50.6	-4.6	-87.0	-41.1	-78.5	-14.2	26.7	27.3	73.4	
APWL	0	0	0	0	-4.6	-91.6	-132.7	-211.2	-225.4	-138.6	-82.3	0	
STOR	251.1	282.9	152.4	152.4	148.2	83.6	64.0	38.1	34.8	61.5	89.0	158.2	
DST	0	0	0	0	-4.2	-64.6	-19.6	-25.9	-3.3	26.7	27.5	69.2	
AEV	0	0	0	34.0	66.9	94.6	106.5	75.4	68.3	50.5	18.5	0	514.7
DEF	0	0	0	0	0.4	22.4	21.5	52.6	10.9	0	0	0	107.8
SURP	0	0	130.0	50.6	0	0	0	0	0	0	0	0	180.6
ROFF	0	0	65.0	57.8	28.9	14.5	7.2	3.6	1.8	0.9	0.5	0.2	180.4
WSMRO	13.5	22.6	0	0	0	0	0	0	0	0	0	3.8	39.9
TOTRO	13.7	22.6	65.0	57.8	28.9	14.5	7.2	3.6	1.8	0.9	0.5	4.0	220.5

TEMP Monthly mean daily temperature in °C
 UNPE Unadjusted potential evapotranspiration
 ADPE Adjusted potential evapotranspiration
 PCPN Precipitation in millimeters
 P-PE Precipitation minus potential evapotranspiration
 APWL Accumulated potential water loss
 STOR Storage
 DST Change in storage
 AEV Actual evapotranspiration
 DEF Water deficiency
 SURP Water surplus
 ROFF Direct runoff
 WSMRO Snow melt runoff
 TOTRO Total runoff

All values except temperatures are in millimeters

measured runoff. The regression equations obtained from the plots of computed and measured runoff for each of the seasons in the Duffin Creek watershed using the Phillips and the Thornthwaite and Mather models are presented in Table 4 along with the corresponding standard deviations.

Monthly correlations worked out using the Phillips modification are of low order (from 0.33 to 0.74) and statistically insignificant and will not be discussed here. The seasonal correlations obtained are presented in Table 5.

The highest correlation is for the summer season (+0.61), while the fall season has the lowest correlation. For all the seasons, the correlations obtained are statistically significant at the 5% level, but only spring and summer seasons reach the 1% level of significance. A further test was performed on the data, to test the possibility that these correlations obtained for the seasons could have occurred by chance as a result of sample size. Therefore, the significance of correlation was tested by the use of the Student's t- distribution, using the following formula:

$$t = \frac{r \times \sqrt{n-2}}{\sqrt{1 - r^2}} \quad - (3.3.2)$$

where

n - Number of pairs of data studied

r - Correlation coefficient of the data

The degrees of freedom for the distribution is n - 2.

TABLE 4

Regression Equations to the Scatter Diagrams

	<u>Winter</u>	<u>Spring</u>	<u>Summer</u>	<u>Fall</u>
Phillips	$y = 0.43x + 17.23$ $\sigma = 12.7$	$y = 0.41x + 35.31$ $\sigma = 17.8$	$y = 1.08x - 2.03$ $\sigma = 6.7$	$y = 0.42x - 1.78$ $\sigma = 5.6$
Thornthwaite and Mather	$y = 0.05x + 1.52$ $\sigma = 3.3$	$y = -0.82x + 95.0$ $\sigma = 43.3$	$y = 2.20x$ $\sigma = 16.9$	$y = 0.30x + 2.03$ $\sigma = 5.9$

y - computed runoff
 x - measured runoff
 σ - standard deviation

TABLE 5

SEASONAL CORRELATIONS BETWEEN COMPUTED AND MEASURED
 RUNOFF FOR DUFFIN CREEK AT PICKERING (1966-1973)
 (Phillips)

Season	Correlation Coefficient r	Coefficient of Determination r^2	t-Statistic	Level of Significance
WINTER	+0.46	0.22	2.475	1 - 5%
SPRING	+0.54	0.30	3.06	1%
SUMMER	+0.61	0.38	3.64	0.1 - 1%
FALL	+0.41	0.17	2.11	5%

Significance levels: At 5% = 0.40; 1% = 0.51
 (Snedecor and Cochran, 1968)

The computed t- statistic values for each season are presented along with the correlation coefficients and it can be seen that the percentage probability that these correlation coefficients could have occurred by chance is of the order of 0.1 to 5%. In other words, these coefficients are significant indicating good agreement between runoff computed with Phillips modification and measured runoff.

For fall and winter seasons, the coefficients 0.41 and 0.46 do not reach the 1% level of significance. These low correlations might be because Phillips (1975), in his modification, has made no allowance for accounting runoff due to snowmelt in certain fall months during which period some precipitation will occur as snow. Also, Phillips' modification is based mainly on temperature to determine snowmelt runoff. As discussed earlier, snowmelt at a point location depends upon thermodynamic processes, but the travel of melt water and its time distribution from point to point depends upon both physiographic and hydrodynamic properties and these are not accounted in Phillips' modification.

A comparison of correlation coefficients obtained between measured and computed due to the original Thornthwaite and Mather bookkeeping approach and Phillips modification indicates that, in spite of low correlations in certain seasons, water yield calculated according to the

Phillips modification is a better estimator of water yield on a season to season basis, than the Thornthwaite and Mather climatic water balance model.

However, the coefficient of determination obtained from the correlations suggest that the Phillips model accounts for only 40 per cent of the runoff. Although there is a significant correlation between computed and measured runoff, it is obvious from the scatter diagrams in Figure 3 that the relationship is neither regular nor clear-cut. For this reason, regression lines were calculated in order to obtain the best estimated value from the Phillips values of computed runoff. The following are the regression equations for the Phillips modification and are based on the Duffin Creek basin data.

<u>Season</u>	<u>Regression Equation</u>
Winter	$R_{est} = 2.35 R_p - 40.81$
Spring	$R_{est} = 2.46 R_p - 86.58$ (3.3.3)
Summer	$R_{est} = 0.93 R_p + 1.96$
Fall	$R_{est} = 3.34 R_p - 6.90$

where

R_{est} - Runoff estimated by regression

R_p - Computed runoff from Phillips modification.

On the basis of these results in the Duffin Creek watershed, assumed to be representative of the southern Ontario area, the modifications suggested by Phillips were, therefore, incorporated in the Thornthwaite and Mather

approach and used in the present study. For the construction of seasonal runoff probability maps, estimated runoff evaluated from the regression equations of 3.3.3, based on the computed runoff according to the Phillips modification, were used.

3.4 Seasonal runoff probabilities

Probabilistic analysis of various climatic and weather elements including synoptic patterns of climate, gained increasing popularity after the 1950's with the work of Gregory (1955), Manning (1956 and 1958), Glover, et. al. (1954), Strommen and Horsfield (1969), Sanderson (1974), and Knowles (1974). Using precipitation records of varying lengths, different workers have attempted the probabilistic analysis for constructing maps of probable maximum and minimum values. In all such studies, the basic assumption usually made is that the given set of observations conform to a normal distribution. For testing the normality criteria, a simple method has been proposed by Stidd (1953) who found that for a wide range of periods and localities, rainfall series could be normalized by a cube root transformation. Kendall (1975) used Stidd's hypothesis for monthly rainfall totals for ten Canadian cities for a thirty year period (1921 to 1950) and concluded that the asymptotically normal distribution of a function of sample moments can be used to give approximate

confidence intervals for the estimates made.

Based on either normal distribution or normalized distribution, the probability function is obtained from the following expression:

$$d = \frac{x - \bar{x}}{\sigma} \quad 3.4.1$$

where

d - Required figure

x - Critical value

\bar{x} - Mean value of the distribution

σ - Standard deviation of the distribution.

The above expression indicates the extent to which the critical value differs from the mean expressed in terms of so many standard deviations. Based on the above concept, Glover, *et. al.* (1954) produced maps of rainfall probabilities for East Africa to indicate the probability of receiving thirty inches of rainfall on an annual basis. Bruce (1968) constructed an atlas of probability rainfall intensity, duration and frequency maps for Canada and pointed out the usefulness of these maps for design engineers. Monthly precipitation probabilities for eleven different levels ranging from five per cent to ninety-five per cent, for the eastern United States were reported by Strommen and Horsfield (1969) based on the assumption that precipitation data fit into a gamma distribution.

In Canada, Sanderson (1974) demonstrated the usefulness of the probability analysis for precipitation, and her

results are discussed in terms of confidence limits for the frequency with which minimal totals of monthly precipitation will be exceeded or maxima fail to be reached. Sanderson's work is mainly based on the technique outlined by Gregory (1964), but she has drawn isoline patterns of equal probabilities instead of representing probabilities as dots on the map. More recent work in this direction in southern Ontario is due to Gomes (1975) who reported that monthly precipitation during May to September fit into a normal distribution. He drew precipitation probability maps for southern Ontario for the period May to September. Brown, et. al. (1968) constructed graphs showing the probability of exceeding various amounts of precipitation for ten-day periods at sixteen stations in southern Ontario and a similar study was made by Chapman and Thomas (1968) in northern Ontario.

Because of the small number of runoff measuring stations and the problems involved in the theoretical computation of runoff from measured climatological data, studies on runoff probabilities are meagre and non-existent in southern Ontario, and the present study is aimed at partially filling this gap.

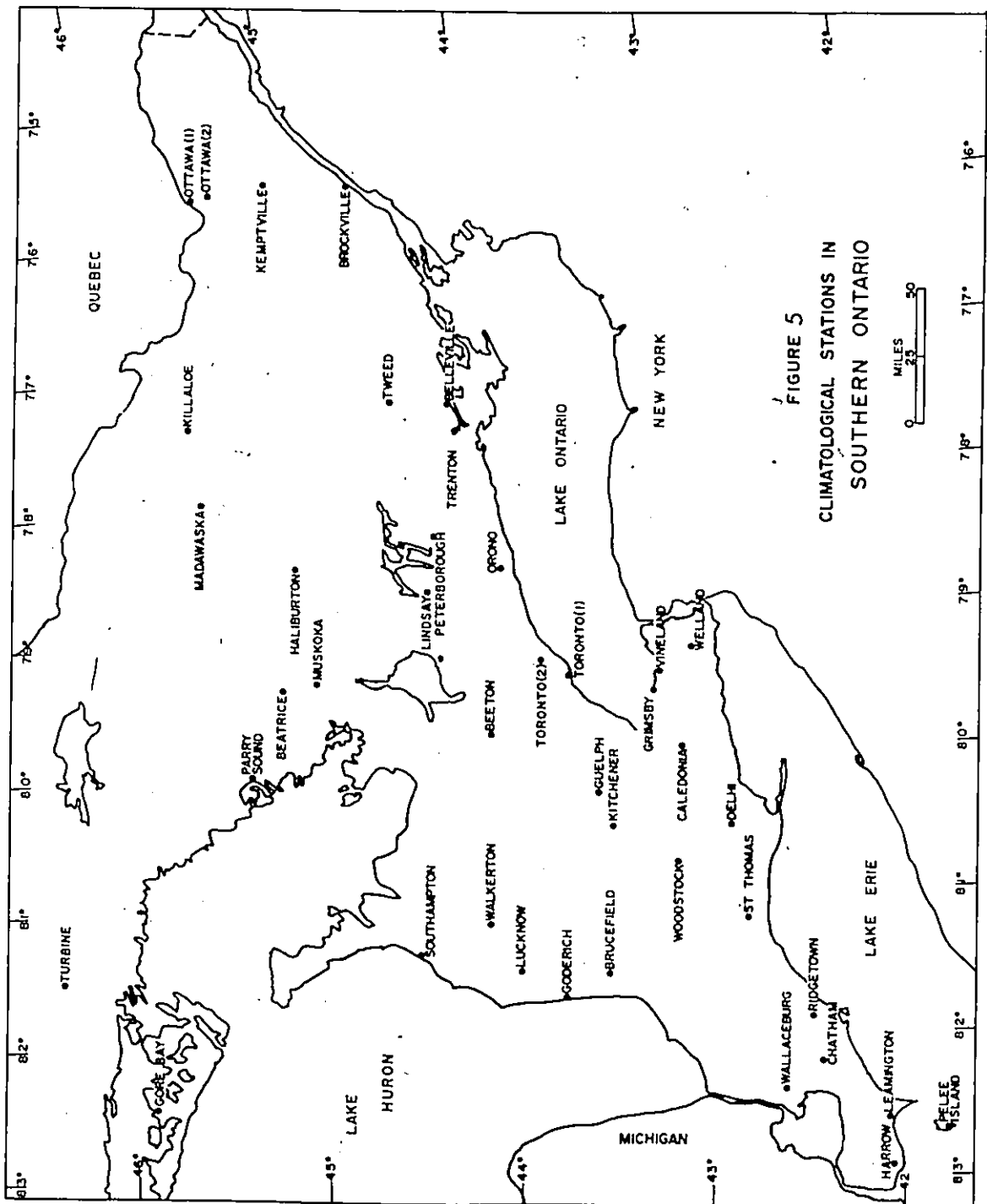
Regional historical monthly precipitation and temperature records of 41 climatic stations obtained from the Monthly Bulletin of the Atmospheric Environment Service, Canada for the period 1938 to 1967 were used to compute runoff

using the Phillips modification. The estimated runoff from the regression equations, based on the Phillips computed runoff values, were used to map the seasonal runoff probabilities which can be anticipated in the region.

Location and elevations of the 41 climatic stations used in the study appear in Appendix 4 and Figure 5. All the climatic stations have periods of record ranging from 25 to 30 years. For the region as a whole, the selected climatological station coverage is adequate, although it is desirable to have data from a greater number of stations, especially in the northern section of southern Ontario where the distribution of the selected stations is uneven.

Having calculated the runoff for each of the selected stations, two stations, Beatrice and Orono, were used to test whether the computed runoff fits the normal distribution, in order to justify using the runoff values in the computation of runoff probabilities. Seasonal runoff is slightly higher at Beatrice, among the selected stations, while Orono represents stations with average amounts of seasonal runoff.

The Chi-square test for the goodness of fit to the normal curve is used to test seasonal runoff for normality at the two stations. From the cumulative normal frequency distribution, (Z) tables (i.e., area under the standard normal curve from 0 to Z), the areas are read from 0 to z_1 , 0 to z_2 , etc., to calculate the expected frequencies



which are used to compute the χ^2 - statistic as follows:

If 'O' is the observed frequency of a distribution and 'E' the expected frequency of the distribution, then the deviation is given by (O-E). Contribution to χ^2 for each of the observed frequencies is then given as $(O-E)^2/E$. Summation of all the contributions to the χ^2 gives the total χ^2 which can be tested for a given degrees of freedom from the number of classes minus the number of estimated parameters minus one. Table 6 summarizes the summed χ^2 values for each of the four seasons at the two stations.

From the table it can be seen that at 5% level of significance, winter, spring and summer seasons runoff at Beatrice and Orono approximate the normal distribution. However, for the fall season at Beatrice, the computed χ^2 -statistic exceeds the value at 5% level of significance by 0.2 and this might indicate high seasonal variability from year to year. The interpretation of these results is a matter of judgment. It seems justifiable to assume that the hypothesis of normality is not disproved by the occurrence of one or two random occurrences and the hypothesis of normality is accepted.

For computing the runoff probabilities, equation 3.4.1 is rewritten as $x = d(\sigma) + \bar{x}$. Since seasonal runoff approximates a normal distribution, sixty-eight and three-tenths per cent of the occurrences must lie between $+\sigma$ and $-\sigma$, and ninety-five per cent of the

TABLE 6
 CHI-SQUARE VALUES FOR THE GOODNESS OF FIT

Station	WINTER		SPRING		SUMMER		FALL	
	X ² Values	D.F.	X ² Values	D.F.	X ² Values	D.F.	X ² Values	D.F.
BEATRICE	4.7	12	4.3	12	4.6	12	5.4	12
ORONO	5.6	13	4.9	12	3.9	12	5.2	12

D.F. = Degrees of Freedom

Significant levels of X², At 12 degrees of freedom

(Spiegel, 1961)

X²_{.05} = 5.2 X²_{.10} = 6.3

At 13 degrees of Freedom

X²_{.05} = 5.8 X²_{.10} = 7.0

occurrences must lie above or below $\pm 1.28 \sigma$. In the equation, when the number of standard deviations that the critical value is above the mean is held constant then the critical values computed at each station is only a function of the mean and standard deviation.

For this study, the appropriate values of 'd' is taken as ± 1.28 to compute critical upper and lower runoff limits that will not be exceeded in 9 out of 10 years.

Probability Runoff Maps

Using the computed runoff values from the 41 stations, runoff probabilities were computed for each of the stations on a monthly basis and are summed on a three month basis to obtain seasonal probabilities. The computer program for the runoff probabilities for the months and the print outs obtained for the climatic stations are presented in Appendix 5.

The probability runoff obtained with $+ 1.28\sigma$ indicate the amounts of highest seasonal runoff expected in nine out of ten years, whereas the computations with $- 1.28\sigma$ indicates the lowest probabilities, and these values in nine out of ten years will not be less than the computed amounts. These computed values were plotted on a contoured base map and isopleths of equal runoff probabilities drawn using the contour lines as reference. The resulting maps for the four seasons in southern Ontario are presented in

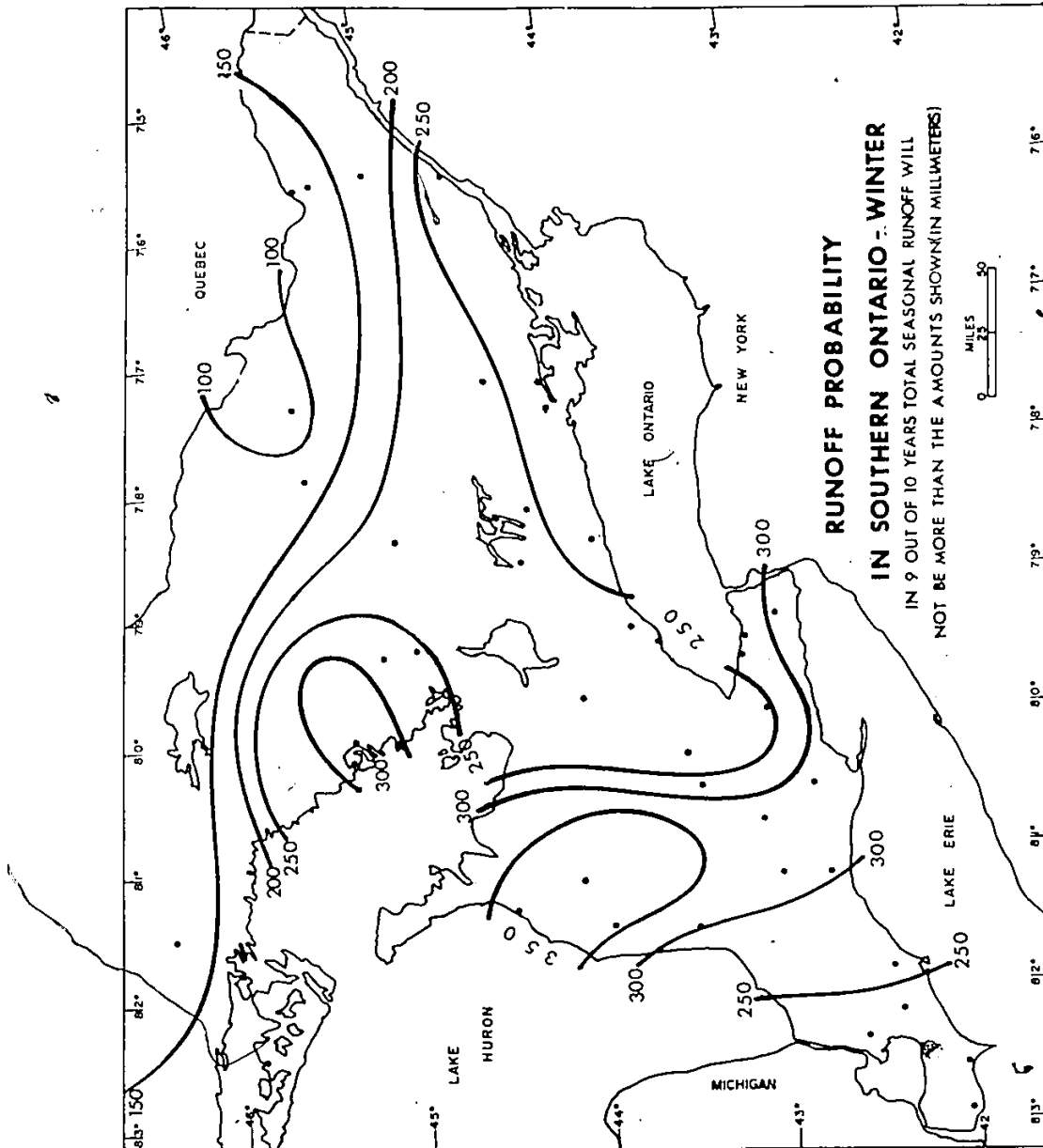


Figure 6

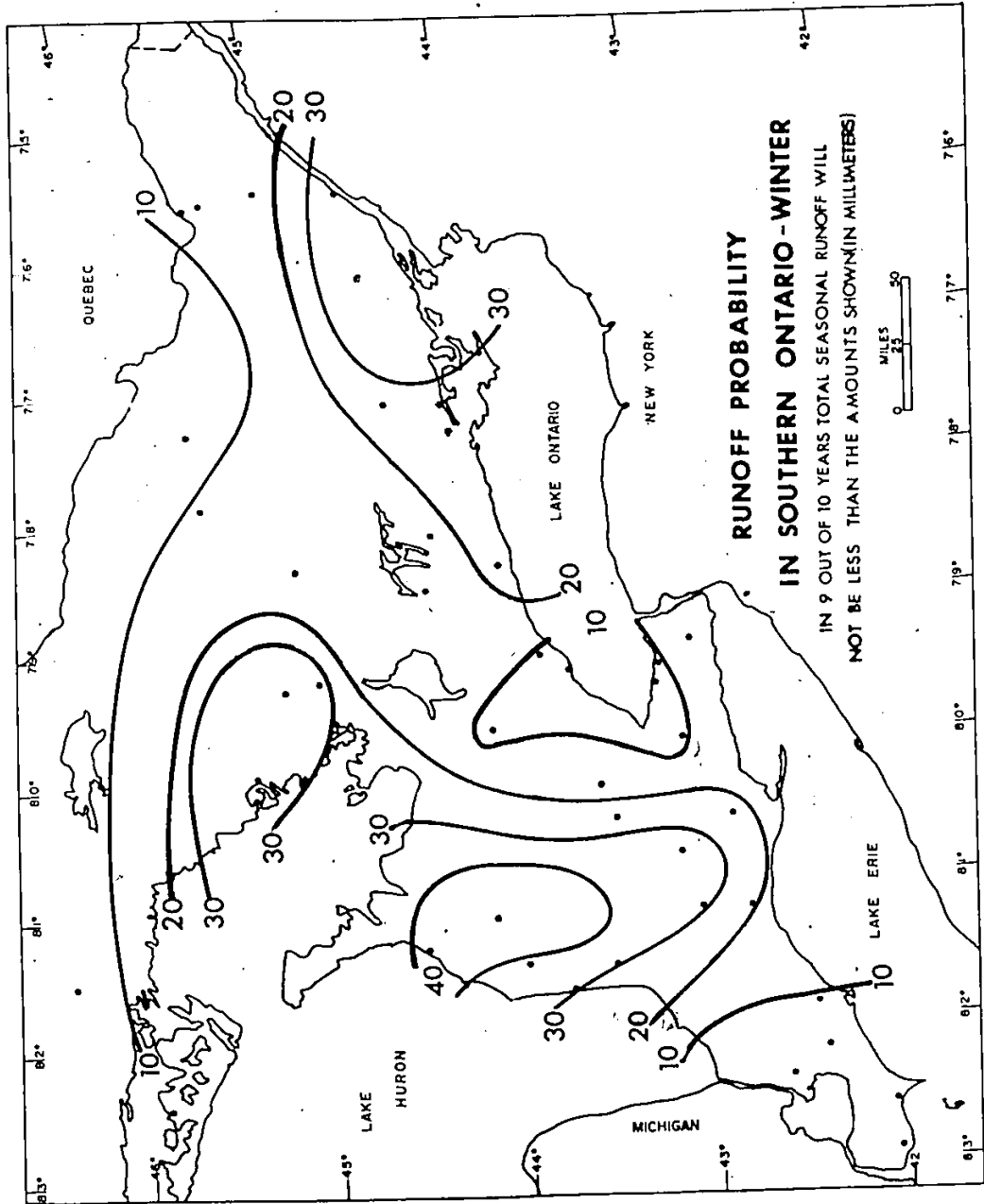


Figure 7

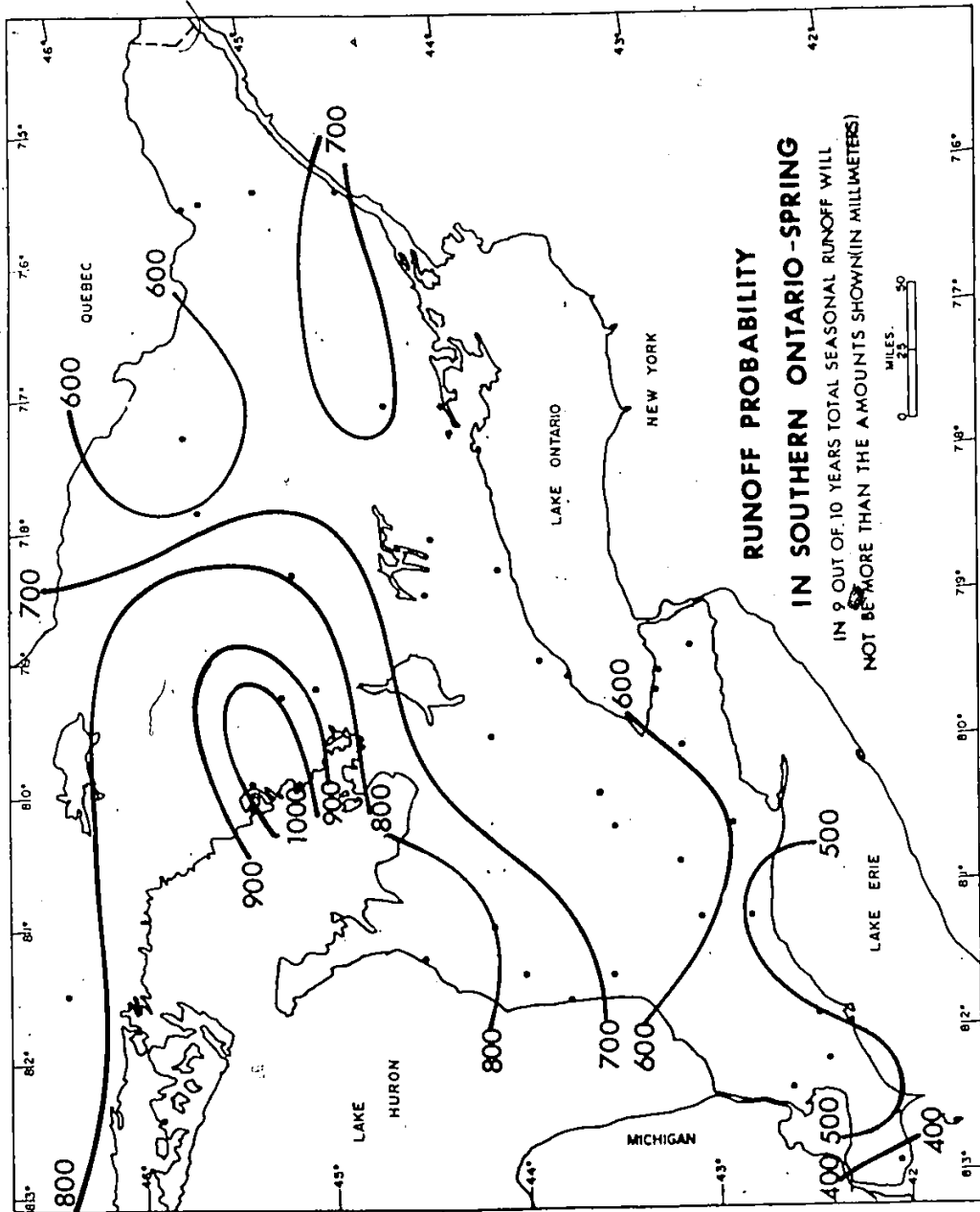


Figure 8

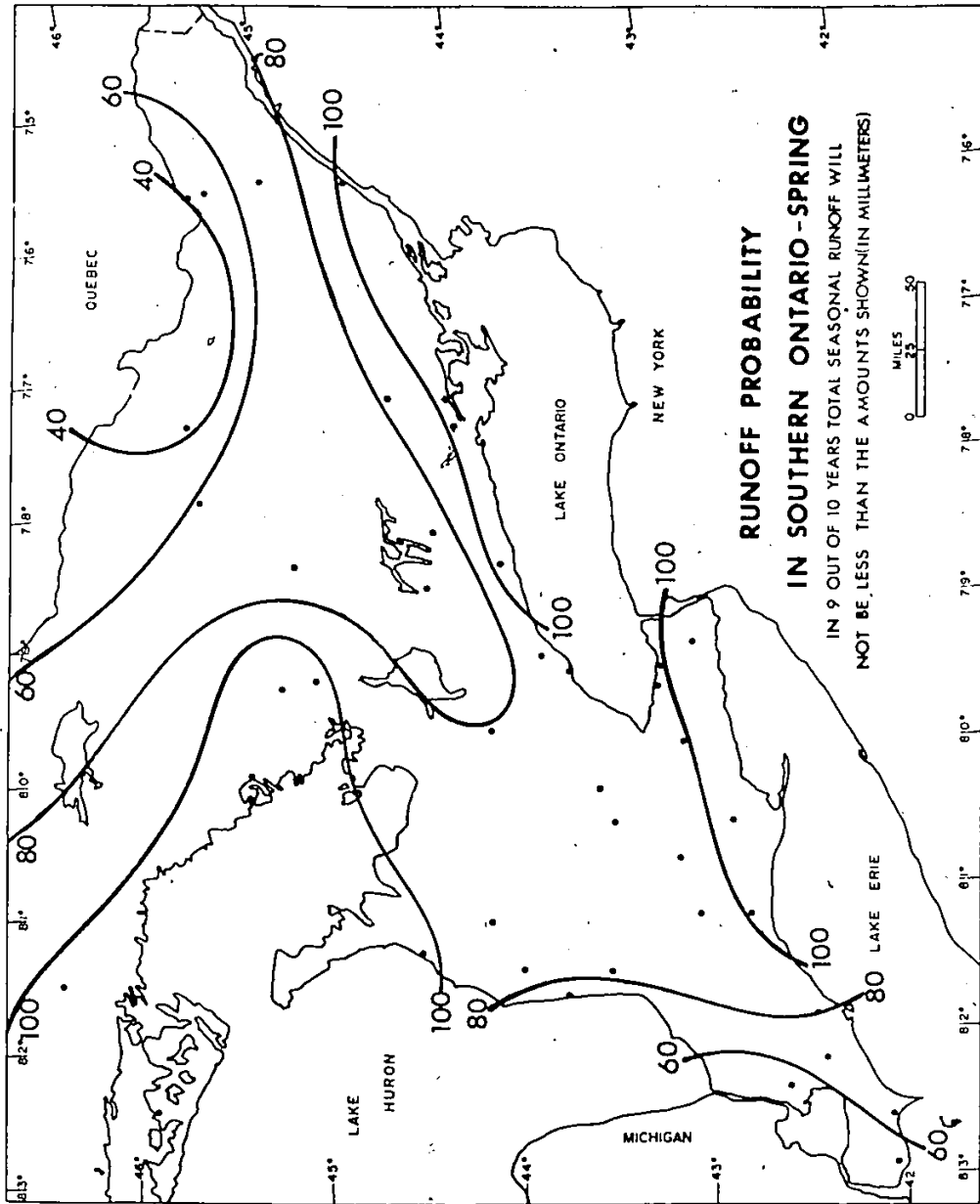


Figure 9

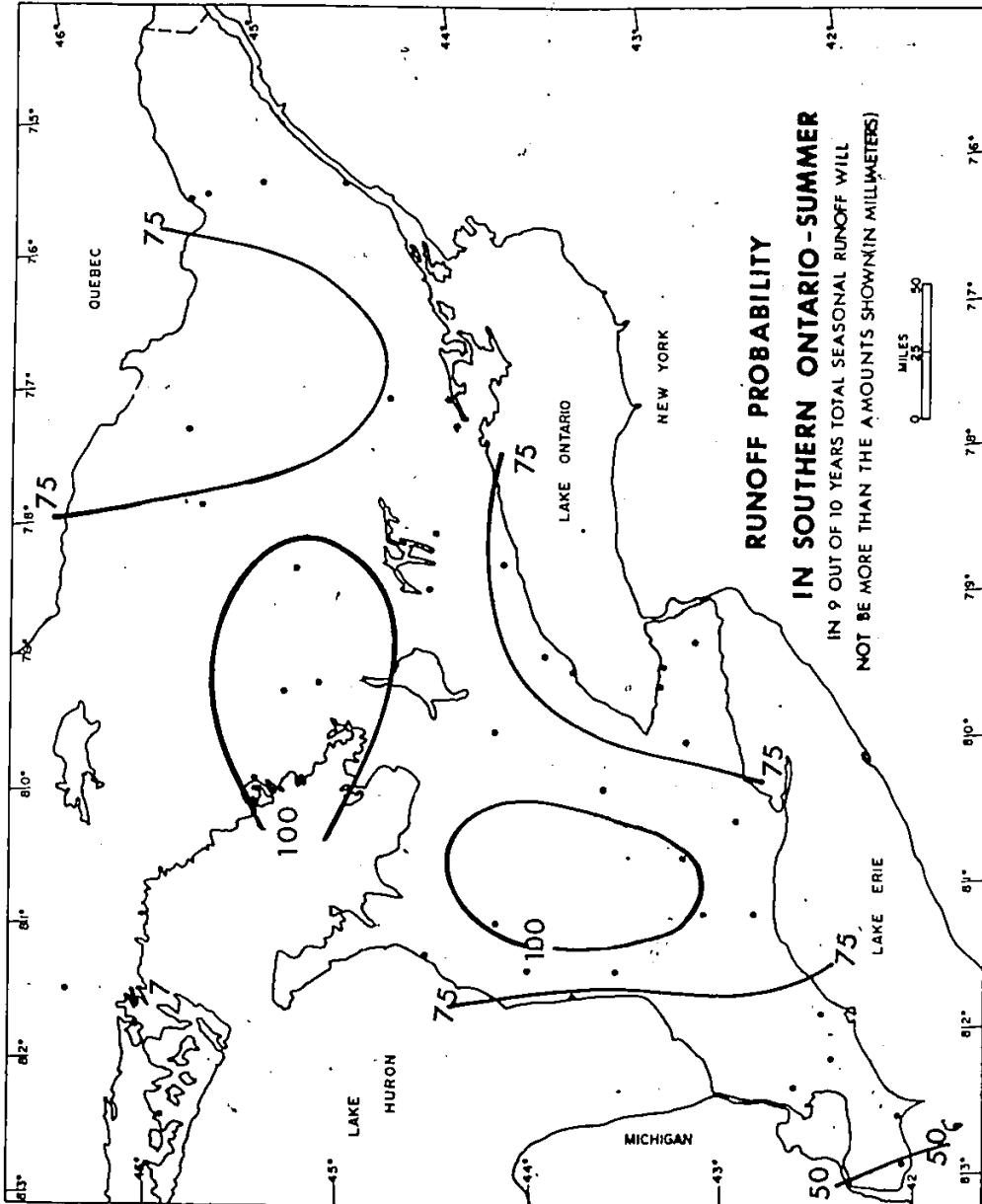


Figure 10

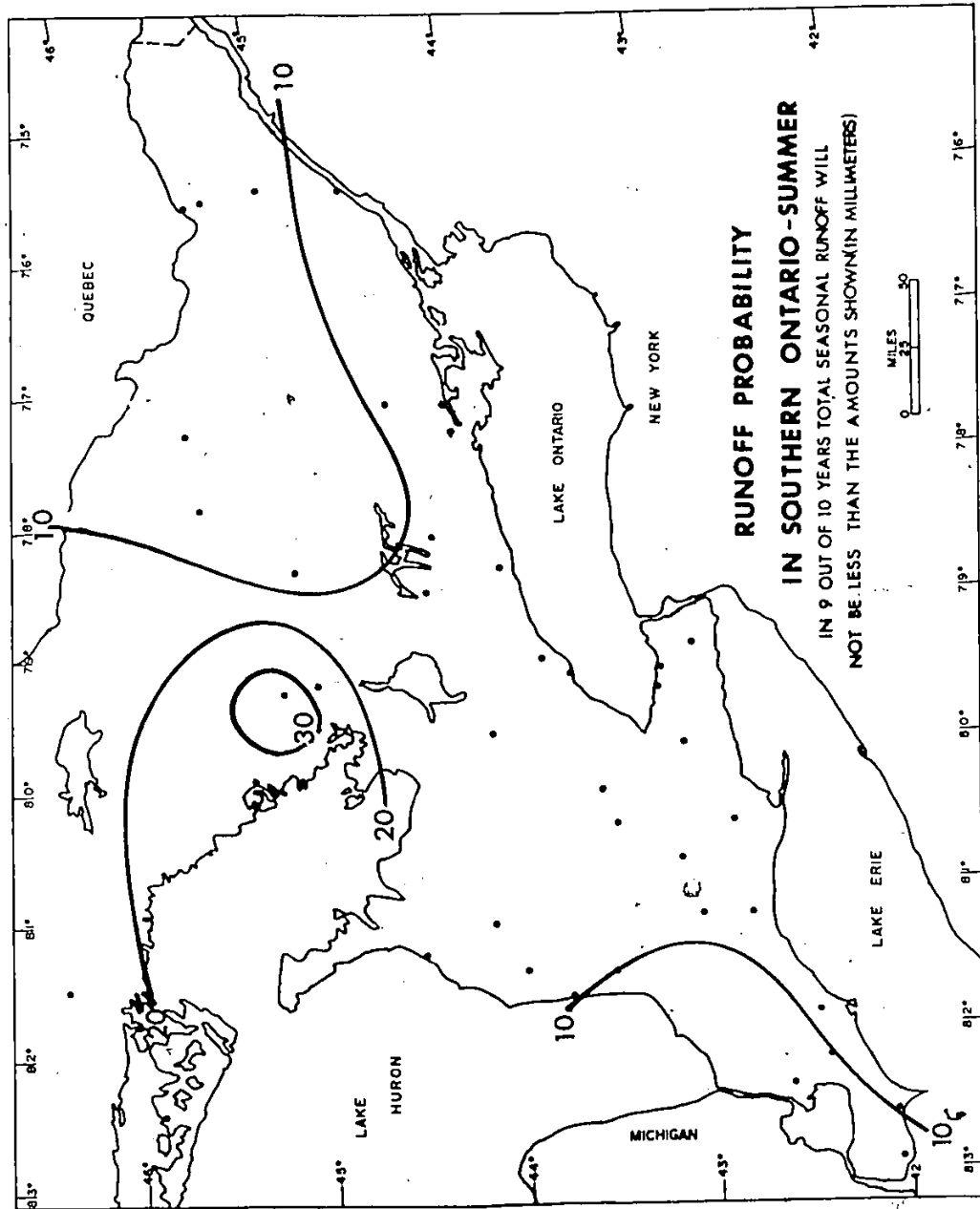


Figure 11

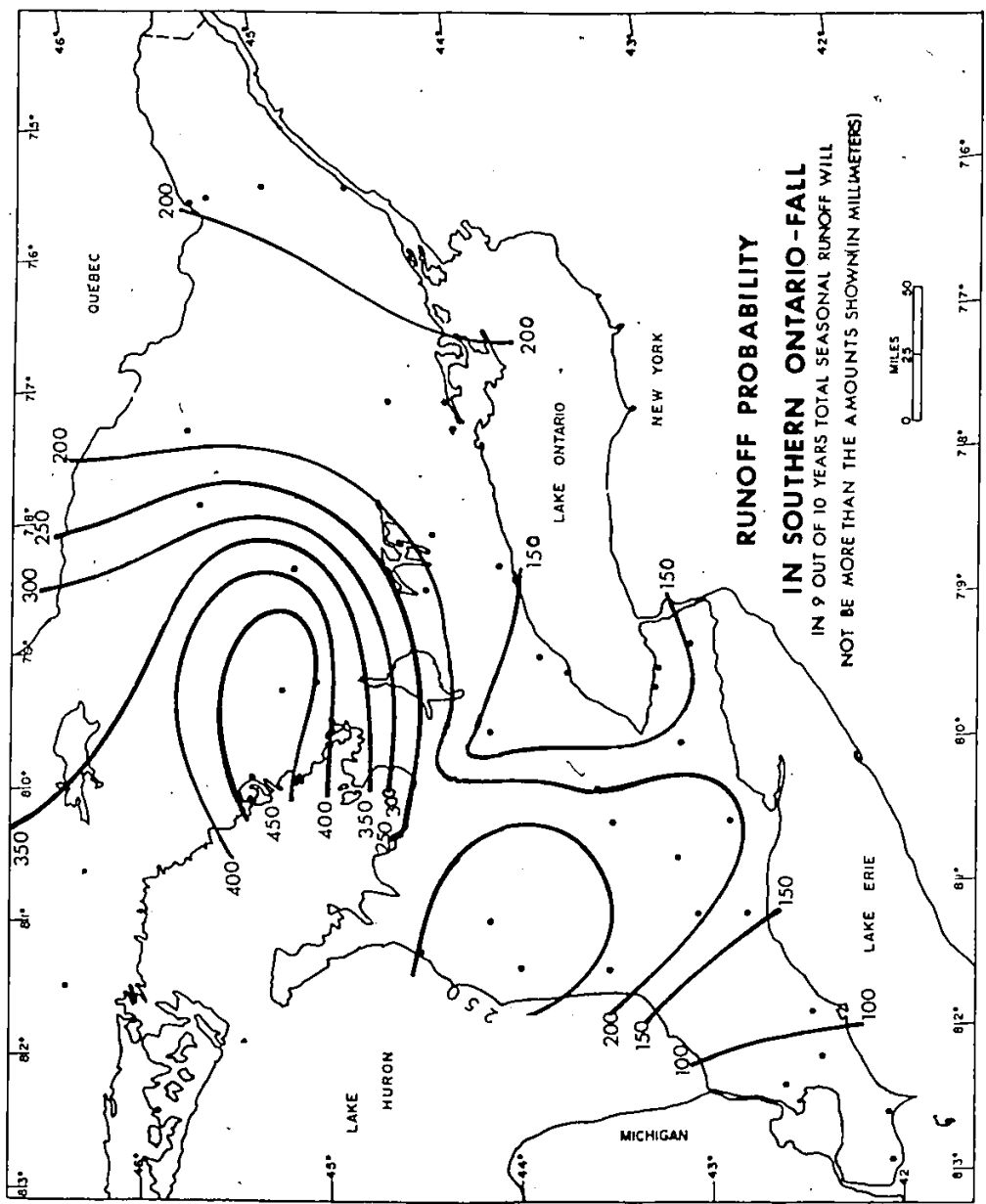


Figure 12

Figures 6 to 12. No map is presented for minimum fall values since, except for four stations (values ranging from 5mm. to 10mm.), the computed values were zero for all the stations. This is also the season when normality of data is suspect.

In general, the runoff probability maps for all the seasons show that, for the entire southern Ontario region, for all the seasons in 9 out of 10 years, average seasonal runoff will not be more than 460 millimeters and will not be less than 30 millimeters. In all seasons, the maximum probable runoff is likely to occur in the areas to the east of Georgian Bay and Lake Huron.

On a seasonal basis, the spring season (Figure 8) has the highest probable amount of runoff (1000mm.), while for the summer season (Figure 10) in 9 out of 10 years, total runoff will not be more than 100 millimeters. The maps indicating the low probable amounts also suggest that at least 60mm. of runoff should occur for the spring season, while summer and fall are the seasons with low runoff probabilities. Large variations of probability of occurrence of runoff within the region for the same period are quite evident in the spring (Figures 8 and 9).

In order to compare the predicted runoff range obtained from these maps, measured values of runoff results for some representative small watersheds for the year 1970 are tabulated in Table 7. In general, the measured runoff fits the predicted range, although low values of runoff

TABLE 7

Measured and Predicted Seasonal Runoff at Representative Watersheds for 1970 (in Millimeters)

Watershed	Drainage Area Sq. Km.	Location		Seasonal Runoff			
		Lat	Long	Winter		Spring	
				Measured	Predicted Range	Measured	Predicted Range
Castor River at Russell	267	45 15	75 20	35	15-170	413	60-650
Cedar Creek at Woodstock	58	43 07	80 46	13	16-270	31	60-550
Conestogo River at Drayton	200	43 45	80 40	79	40-350	243	100-1000
Don River at Todmorden	178	43 41	79 21	66	12-210	134	100-600
Goldwater River at Todmorden	110	44 42	79 38	45	30-300	101	100-1000
Highland Creek near West Hill	54	43 46	79 10	10	30-300	0 26	100-1000
Holland River at Holland Landing	108	44 05	79 29	18	15-200	63	80-600
Lynde Creek near Whitby	66	43 52	78 57	14	15-250	52	80-600
Mimico Creek at Islington	39	43 38	79 31	13	10-250	28	100-600
Salmon River near Shannonville	550	44 12	77 12	230	25-250	592	100-670
Thames River at Ingersoll	320	43 02	80 53	103	10-270	181	70-580
Thames River at Woodstock	157	43 08	80 45	56	10-270	103	70-580

TABLE 7 (cont'd)

Measured and Predicted Seasonal Runoff at
Representative Watersheds for 1970
(in Millimeters)

Watershed	Drainage Area Sq. Km.	Location		Seasonal Runoff			
		Lat o N	Long o W	Summer		Fall	
				Measured	Predicted Range	Measured	Predicted Range
Castor River at Russell	267	45 15	75 20	8	6-80	64	5-220
Cedar Creek at Woodstock	58	43 07	80 46	6	6-60	11	5-130
Conestogo River at Drayton	200	43 45	80 40	8	25-100	42	10-400
Don River at Todmorden	178	43 41	79 21	73	10-80	76	10-200
Goldwater River at Todmorden	110	44 42	79 38	42	30-100	60	10-450
Highland Creek near West Hill	54	43 46	79 10	12	30-600	15	10-450
Holland River at Holland Landing	108	44 05	79 29	11	10-80	16	10-150
Lynde Creek near Whitby	66	43 52	78 57	6	10-80	10	5-200
Mimico Creek at Islington	39	43 38	79 31	14	10-75	12	5-150
Salmon River near Shannonville	550	44 12	77 12	95	10-75	114	5-200
Thames River at Ingersoll	320	43 02	80 53	83	10-90	73	5-170
Thames River at Woodstock	157	43 08	80 45	26	10-90	40	5-170

from the predicted range are slightly higher than the measured in the spring and summer seasons at five watersheds. This tendency of the predicted range, particularly pronounced in spring and summer, might be because the Phillips modification to the Thornthwaite and Mather approach does not take into account the underestimation of evaporation rate in spring and summer months, and hence the direct runoff resulted from precipitation is likely to result in higher values.

CHAPTER 4

Summary and Conclusions

In this study, the Phillips modification of the Thornthwaite-Mather water balance was examined to determine its applicability as an estimator of seasonal surface runoff probabilities in southern Ontario. The use of the historic records of temperature and precipitation from climatological stations in the region made possible the construction of seasonal runoff probability maps which provide background information on the probabilistic occurrence of runoff in all the seasons.

It is hoped that such maps may be useful to the PLUARG study in obtaining data on the inputs of pollutants into the Great Lakes drainage system which have their origins in the complex land use activities of agriculture. Since studies such as PLUARG involve measurements of precipitation and runoff for two years only, it is necessary to determine how representative these two years are of the precipitation-runoff history of the area. The present study is part of this objective.

On the basis of the study, the following conclusions can be drawn. In southern Ontario, the Phillips modification to the Thornthwaite-Mather model provides a better

estimate of seasonal runoff when compared with the original Thornthwaite-Mather model. The seasonal runoff probability maps presented here give quantitative statements of maximum probable runoff that is likely to occur in southern Ontario. On a seasonal basis, the highest probable amount of runoff occurs in the spring. Also, the evaluated range of probable seasonal runoff from the maps shows good agreement with the measured runoff in some representative small watersheds.

Only seasonal runoff probabilities have been considered in the present study, since the Phillips modification failed to give significant correlations when applied on a monthly basis. Further work is needed in the modification of the model to obtain more reliable estimates of monthly runoff.

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Computer program(WATIV)for Phillips modification

```

*JOB      WATFIV  XXXXXXXXXX,TIME=9
C        THIS PROGRAM COMPUTES THE AVERAGE WATER BALANCE BY MONTHS,
C        FOR AS MANY CONSECUTIVE YEARS AS DESIRED.
C
C        FOLLOWING ARE TWO CARD PAIRS, ONE PAIR FOR EACH YEAR OF DATA.
C        FIRST CARD OF PAIR HAS TWELVE MONTHLY AVERAGE TEMPERATURES
C        PUNCHED IN FIVE COLUMN FIELDS, WITH DECIMAL POINT.
C        SECOND CARD OF PAIR HAS TWELVE MONTHLY AVERAGE PRECIPITATION
C        VALUES IN FIVE COLUMN FIELDS, WITH DECIMAL POINTS.
C
C        FOLLOWING THE LAST PAIR OF T-P VALUES, THERE SHOULD BE A PAIR
C        OF BLANK CARDS TO SIGNIFY THE END OF A SET OF DATA.
C        THE PROGRAM IS SET TO PROCESS MULTIPLE SETS OF DATA, UNTIL
C        NO MORE CARDS ARE AVAILABLE.
C
1         DIMENSION V(160,10),C(12,50),W(13,12),T(12),P(12)
2         DIMENSION TITLE(7),HEAT(12),Z(12)
3         DIMENSION PERCNT(12)
4         DIMENSION DEGDAY(12)
5         DIMENSION NAME(13)
6         DIMENSION WSMRD(12),TOTRO(12)
7         DATA NAME/'TEMP','UNPE','ADPE','PCFN','P-PE','APWL','STOR','D ST',
          1'A EV','DEF ','SURP','ROFF','TMDT'/'
8         2 CONTINUE
9         READ (5,508,END=99) WHC
10        WRITE(6,509) WHC
11        1 DO 1000 ISET=1,10
12        READ(5,901) (V(IZ,ISET),IZ=1,160)
13        1000 CONTINUE
14        DO 1005 ILAT=1,50
15        READ(5,907) (C(JZ,ILAT),JZ=1,12)
16        1005 CONTINUE
17        5 W(7,12)=WHC
18        11 CONTINUE
19        TSAVE=25.0
20        SUM=0.0
21        RDS=0.0
22        QST=WHC
23        13 READ(5,934,END=99) IYR, TITLE, LAT, MIN, LONG, LMIN, LEV
24        934 FORMAT(14,3X,7A4,2I2,I3,I2,I4)
25        WRITE(6,911) (TITLE(I),I=1,7),LAT,MIN,LONG,LMIN,LEV
26        911 FORMAT('1',7A4,6X,I2,2X,I2,6X,I3,2X,I2,6X,I4,/)
27        9 READ(5,935) (T(K),K=1,12)
28        READ(5,936) (P(K),K=1,12)
29        935 FORMAT(12F5,2)
30        936 FORMAT(12F5,2)
31        IF(T(7)) 2,20,29
32        20 GO TO 11
33        29 ILAT=LAT-40
34        10 CONTINUE
35        DO 7 IY=1,12
36        WSMRD(IY)=0.0
37        TOTRO(IY)=0.0
38        WMSUM=0.0
39        TOTSUM=0.0
40        21 THEAT=0.0
41        DO 253 J=1,12
42        HEAT(J)=(((0.0026*T(J)**2)-(0.0268*T(J)))-2.2587)
43        IF(HEAT(J).LT.0.0) HEAT(J)=0.0
44        THEAT=THEAT+HEAT(J)
45        253 CONTINUE
46        IF(THEAT.GE.50.0) ISET=10
47        IF(THEAT.GE.45.0.AND.THEAT.LT.50.0) ISET=9
48        IF(THEAT.GE.40.0.AND.THEAT.LT.45.0) ISET=8
49        IF(THEAT.GE.35.0.AND.THEAT.LT.40.0) ISET=7
50        IF(THEAT.GE.30.0.AND.THEAT.LT.35.0) ISET=6
51        IF(THEAT.GE.25.0.AND.THEAT.LT.30.0) ISET=5
52        IF(THEAT.GE.20.0.AND.THEAT.LT.25.0) ISET=4
53        IF(THEAT.GE.15.0.AND.THEAT.LT.20.0) ISET=3
54        IF(THEAT.GE.10.0.AND.THEAT.LT.15.0) ISET=2
55        IF(THEAT.LT.10.0) ISET=1
56        14 CONTINUE
57        30 STL=W(7,12)
58        DO 250 J=1,12
59        W(1,J)=T(J)
60        W(2,J)=0.0
61        35 W(4,J)=P(J)
62        W(11,J)=0.0
63        W(12,J)=0.0
64        IF(T(J)-32.0) 50,40,40

```

```

65      40 IT = 2.0*T(J)-62.5
66      W(2,J)=V(IT,ISET)
67      50 W(3,J)=W(2,J)*C(J,ILAT)
68      W(5,J)=W(4,J)-W(3,J)
69      W(6,J)=0.0
70      IF (W(5,J))60,70,70
71      60 CONTINUE
72      IF (OST-WHC)65,65,63
73      62 W(11,J)=OST-WHC
74      65 CONTINUE
75      SUM=SUM+W(5,J)
76      W(6,J)=SUM
77      W(7,J) = WHC*EXP(SUM/WHC)
78      W(8,J)=W(7,J)-QST
79      QST=W(7,J)
80      W(9,J)=W(4,J)-W(8,J)
81      W(10,J)=W(3,J)-W(9,J)
82      GO TO 200
83      70 CONTINUE
84      W(7,J)=STL+W(5,J)
85      IF(T(J).GT.31.9) GO TO 68
86      POT=W(7,J)-WHC
87      IF(W(7,J)-WHC)68,68,69
88      69 IF(J.EQ.1) GO TO 710
89      IF(J.EQ.2) GO TO 711
90      IF(J.EQ.3) GO TO 712
91      713 PERCNT(J)=(-99.91+5.71*(T(J)))/100.
92      GO TO 71
93      710 PERCNT(J)=(-7.74+1.41*(T(J)))/100.
94      GO TO 71
95      711 PERCNT(J)=(6.93+0.87*(T(J))-0.78*(W(7,J)-WHC))/100.
96      GO TO 71
97      712 PERCNT(J)=(-13.85+1.95*(T(J))-0.95*(W(7,J)-WHC))/100.
98      GO TO 71
99      71 WSMRO(J)=(PERCNT(J)*(W(7,J)-WHC))-(0.5*ROS)
100     72 IF(WSMRO(J).GT.POT) WSMRO(J)=POT
101     IF(WSMRO(J).LT.0.0) GO TO 85
102     W(7,J)=W(7,J)-WSMRO(J)
103     WSMSUM=WSMSUM+WSMRO(J)
104     GO TO 68
105     85 WSMRO(J)=0.0
106     68 CONTINUE
107     TSAVE=T(J)
108     W(9,J)=W(3,J)
109     W(10,J)=0.0
110     IF(W(7,J)-WHC)80, 115,90
111     80 CONTINUE
112     SUM = WHC*ALOG(W(7,J)/WHC)
113     W(6,J)=SUM
114     W(8,J) = W(7,J)-QST
115     QST=W(7,J)
116     GO TO 200
117     90 CONTINUE
118     SUM=0.0
119     W(6,J)=0.0
120     W(8,J)=WHC-QST
121     OST=WHC
122     IF(T(J)-31.9) 200,200,110
123     110 CONTINUE
124     W(7,J)=WHC
125     115 CONTINUE
126     W(11,J)=W(5,J)+STL-W(7,J)
127     200 CONTINUE
128     STL=W(7,J)
129     210 W(12,J)=0.5*(ROS+W(11,J))
130     215 ROS=W(12,J)
131     220 IF(J-1)230,230,240
132     230 DO 235 I=1,12
133     235 W(13,I)=0.0
134     240 DO 245 I = 1,12
135     245 W(13,I)=W(I,J)+W(13,I)
136     TOTRO(J)=W(12,J)+ WSMRO(J)
137     TOTSUM=TOTSUM+TOTRO(J)
138     250 CONTINUE
139     W(13,1)=W(13,1)/12.
140     W(13,7)=W(13,7)/12.
141     WRITE(6,S10)
142     DO 270 I=1,12
143     DO 265 J = 1,12
144     265 T(J) = W(1,J)

```

```

145 W-ASTA = W(13,I)
146 WRITE(6,504) T,IYR,WLASTA,NAME(I)
147 CONTINUE
148 WRITE(6,915) WSMRO,IYR,WMSMSUM
149 WRITE(6,916) TOTRO,IYR,TOTSUM
150 WRITE(7,917)TOTRO,IYR
151 FORMAT(12F6.2,15,2X,C')
**WARNING** EXPECTING COMMA BETWEEN FORMAT ITEMS NEAR ,2X,C'
152 WRITE(6,905)
153 IYR=IYR + 1
154 GO TO 9
155 STOP
156 99 FORMAT (40F2.2)
157 901 FORMAT (12F5.2)
158 902 FORMAT(1H1,18A4)
159 903 FORMAT(1X,12F6.2,15,1X,F7.2,2X,A4)
160 904 FORMAT (1H )
161 905 FORMAT (1A,18A4)
162 906 FORMAT(20X,12F5.2)
163 907 FORMAT(F5.2)
164 908 FORMAT(, SOIL MOISTURE RETENTION = ,F5.2, , INCHES,/)
165 909 FORMAT(, JAN FEB MAR Y APR MAY JUN JUL AUG SEP O
166 1CT NDV DEC YEAR MARY ,/)
167 915 FORMAT(1X,12F6.2,15,1X,F7.2,2X,WSMRO')
168 916 FORMAT(1X,12F6.2,15,1X,F7.2,2X,TOTRO')
END
**WARNING** FORMAT STATEMENT 902 IS UNREFERENCED
**WARNING** FORMAT STATEMENT 903 IS UNREFERENCED
**WARNING** FORMAT STATEMENT 906 IS UNREFERENCED
$ENTRY

```

SOIL MOISTURE RETENTION = 6.00 INCHES

Appendix 2

Model water balance computations based on Phillips model

PROGRAM 30														43	85	79	7	550
JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR	Y					
19.60	19.60	35.00	46.20	49.80	61.20	68.20	67.20	63.20	51.90	38.50	23.50	1968	45.32	TEMP				
0.00	0.00	0.01	0.05	0.06	0.10	0.13	0.13	0.11	0.07	3.02	0.00	1968	0.68	UNPE				
0.00	0.00	0.31	1.68	2.27	3.84	5.03	4.88	3.43	1.99	0.49	0.00	1968	23.72	ADPE				
4.87	3.04	3.47	1.38	3.80	2.74	1.45	2.47	3.02	1.90	4.76	3.88	1968	36.43	PCPN				
4.87	3.04	3.16	-0.33	1.23	-1.10	-3.58	-2.21	-0.41	-0.09	4.27	3.88	1968	12.71	P-PE				
0.00	0.00	0.00	-0.33	0.00	-1.10	-4.68	-6.89	-7.30	-7.40	0.00	0.00	1968	-27.70	APWL				
10.75	12.39	6.00	5.68	6.00	4.99	2.75	1.90	1.78	1.75	6.00	8.56	1968	5.71	STOR				
0.00	0.00	0.00	-0.32	0.32	-1.01	-2.24	-0.85	-0.13	-0.03	4.25	0.00	1968	0.00	D ST				
0.00	0.00	0.31	1.67	2.27	3.75	3.69	3.32	3.15	1.93	0.49	0.00	1968	20.56	A EV				
0.00	0.00	0.00	0.01	0.00	0.09	1.34	1.36	0.29	0.07	0.00	0.00	1968	3.16	DEF				
0.00	0.00	9.56	0.00	0.91	0.00	0.00	0.00	0.00	0.00	0.02	0.00	1968	10.49	SURP				
0.00	0.00	4.78	2.39	1.65	0.82	0.41	0.21	0.10	0.05	0.04	0.02	1968	10.47	ROFF				
1.18	1.39	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	3.00	1.30	1968	3.88	WSMRD				
1.18	1.39	4.78	2.39	1.65	0.82	0.41	0.21	0.10	0.05	0.04	1.32	1968	14.35	TOTRO				

JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR	Y	
24.30	26.50	29.70	44.40	53.10	61.20	69.90	70.80	62.70	49.50	38.90	23.00	1969	46.17	TEMP
0.00	0.00	0.00	0.04	0.07	0.10	0.14	0.14	0.11	0.06	3.02	0.00	1969	0.68	UNPE
0.00	0.00	0.00	1.34	2.65	3.84	5.42	5.04	3.43	1.71	0.49	0.00	1969	23.92	ADPE
2.72	0.34	2.40	3.85	3.21	3.05	2.40	1.83	0.50	2.24	3.94	1.30	1969	29.78	PCPN
2.72	0.34	2.40	2.51	0.56	-0.79	-3.02	-3.21	-2.93	0.53	3.45	3.30	1969	5.86	P-PE
0.00	0.00	0.00	0.00	0.00	-0.79	-3.81	-7.02	-0.95	-7.66	-0.94	0.00	1969	-30.17	APWL
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1969	0.00	STOR
9.89	9.16	9.37	6.00	6.00	5.26	3.18	1.86	1.14	1.67	5.13	7.68	1969	5.52	D ST
0.00	0.00	0.00	0.00	0.00	-0.74	-2.08	-1.32	-0.72	0.53	3.45	0.87	1969	0.00	A EV
0.00	0.00	0.00	1.34	2.65	3.79	4.48	3.15	1.22	1.71	0.49	0.00	1969	18.82	DEF
0.00	0.00	0.00	0.00	0.00	0.05	0.94	1.89	2.21	0.00	3.00	0.00	1969	5.09	SURP
0.00	0.00	0.00	5.87	0.56	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1969	6.44	ROFF
0.01	0.00	3.00	2.94	1.75	0.88	0.44	0.22	0.11	0.05	0.03	0.01	1969	5.40	WSMRD
1.39	1.12	2.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.75	1969	5.40	TOTRO
1.40	1.13	2.14	2.94	1.75	0.88	0.44	0.22	0.11	0.05	3.03	0.76	1969	11.84	TOTRO

JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR	Y	
17.00	21.10	33.40	44.80	52.20	64.80	69.00	69.30	61.00	51.00	41.60	24.80	1970	45.88	TEMP
0.00	0.00	0.00	0.04	0.07	0.12	0.13	0.14	0.10	0.07	0.03	0.00	1970	0.70	UNPE
0.00	0.00	0.00	1.34	2.65	4.61	5.03	5.04	3.12	1.99	0.73	0.00	1970	24.51	ADPE
2.06	1.64	2.85	3.88	2.15	1.02	4.94	3.42	2.43	3.05	2.35	4.57	1970	34.36	PCPN
2.06	1.64	2.85	2.54	-0.50	-3.59	-0.09	-1.62	-0.69	1.06	1.62	4.57	1970	9.85	P-PE
0.00	0.00	0.00	0.00	-0.50	-4.08	-4.17	-5.79	-6.48	-3.98	-1.45	0.00	1970	-26.46	APWL
9.14	9.75	6.00	6.00	5.52	3.04	2.99	2.28	2.04	3.09	4.71	7.92	1970	5.21	STOR
0.00	0.00	0.00	0.00	-0.48	-2.49	-0.05	-0.71	-0.25	1.08	1.62	1.29	1970	0.00	D ST
0.00	0.00	0.00	1.34	2.63	3.51	4.99	4.13	2.88	1.99	3.03	0.00	1970	21.99	A EV
0.00	0.00	0.00	0.00	0.02	1.10	0.05	0.91	0.84	0.00	3.03	0.00	1970	2.52	DEF
0.00	0.00	0.00	2.84	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1970	9.14	SURP
0.01	0.00	3.30	2.92	1.46	0.73	0.36	0.18	0.09	0.05	0.02	0.01	1970	9.14	ROFF
0.60	1.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.36	1970	2.98	WSMRD
0.61	1.03	3.30	2.92	1.46	0.73	0.36	0.18	0.09	0.05	0.02	1.37	1970	12.12	TOTRO

JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR	Y	
17.80	25.30	28.60	40.90	53.40	64.20	68.70	68.50	65.20	63.40	45.00	30.40	1971	47.45	TEMP
0.00	0.00	0.00	0.03	0.07	0.11	0.13	0.12	0.11	0.11	0.04	0.00	1971	0.72	UNPE
0.00	0.00	0.00	1.01	2.65	4.22	5.03	4.32	3.43	3.14	0.97	0.00	1971	24.77	ADPE
2.33	3.69	1.42	1.33	1.06	3.94	4.77	5.20	3.08	1.56	2.51	4.38	1971	35.47	PCPN
2.33	3.69	1.42	0.32	-1.59	-0.28	-0.26	0.88	-0.35	-1.57	1.54	4.38	1971	10.70	P-PE
0.00	0.00	0.00	0.00	-1.59	-1.87	-2.13	-0.99	-1.34	-2.92	-0.83	0.00	1971	-11.67	APWL
9.69	11.67	10.60	6.00	4.61	4.59	4.21	5.09	4.80	3.69	5.23	6.96	1971	6.41	STOR
0.00	0.00	0.00	0.00	-1.39	-0.21	-0.19	0.88	-0.29	-1.11	1.54	0.77	1971	0.00	D ST
0.00	0.00	0.00	1.01	2.45	4.15	4.96	4.32	3.37	2.67	0.97	0.00	1971	23.90	A EV
0.00	0.00	0.00	0.00	0.19	0.07	0.07	0.00	0.05	0.47	0.00	0.00	1971	0.87	DEF
0.00	0.00	0.00	4.92	0.00	0.00	0.00	0.00	0.00	0.00	3.03	0.00	1971	4.92	SURP
0.01	0.00	0.00	2.46	1.23	0.61	0.31	0.15	0.08	0.04	0.02	0.01	1971	4.92	ROFF
0.77	1.71	2.49	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2.65	1971	7.62	WSMRD
0.77	1.71	2.49	2.46	1.23	0.61	0.31	0.15	0.08	0.04	0.02	2.66	1971	12.54	TOTRO

JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR	Y	
22.80	20.20	27.00	38.50	54.80	60.00	67.20	65.40	60.40	44.70	38.50	27.90	1972	43.78	TEMP
0.00	0.00	0.00	0.02	0.08	0.10	0.13	0.12	0.11	0.04	3.02	0.00	1972	0.62	UNPE
0.00	0.00	0.00	0.67	3.02	3.84	5.03	4.32	3.43	3.14	0.49	0.00	1972	21.94	ADPE
1.85	2.27	4.08	2.85	1.48	2.44	2.24	4.68	3.41	3.21	3.41	6.02	1972	37.94	PCPN
1.85	2.27	4.08	2.18	-1.54	-1.40	-2.79	0.36	-0.03	2.07	2.92	6.02	1972	16.00	P-PE
0.00	0.00	0.00	0.00	-1.54	-2.94	-5.73	-4.86	-4.89	-1.43	0.00	0.00	1972	-21.41	APWL
8.13	9.47	11.17	6.00	4.64	3.67	2.31	2.67	2.66	4.73	8.00	8.07	1972	5.86	STOR

0.00	0.00	0.00	0.00	-1.36	-0.97	-1.37	0.36	-0.01	2.07	1.27	0.00	1972	0.00	D ST	
0.00	0.00	0.00	0.00	0.67	2.84	3.41	3.61	4.32	3.42	1.14	0.49	0.00	1972	19.89	A EV
0.00	0.00	0.00	0.00	0.18	0.43	1.42	0.00	0.01	0.00	0.00	0.00	0.00	1972	2.05	DEF
0.00	0.00	0.00	7.34	0.00	0.00	0.00	0.00	0.00	0.00	1.65	0.00	1972	9.00	SURP	
0.00	0.00	0.00	3.67	1.84	0.92	0.46	0.23	0.11	0.06	0.85	0.43	1972	8.58	ROFF	
0.68	0.92	2.39	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	3.15	1972	7.14	WSMRD	
0.69	0.93	2.39	3.67	1.84	0.92	0.46	0.23	0.11	0.06	0.85	3.58	1972	15.72	TOTRO	

JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	YEAR	Y	
18.50	20.60	38.30	43.70	51.50	65.20	70.20	72.30	61.10	51.80	43.00	26.30	1973	46.62	TEMP
0.00	0.00	0.02	0.04	0.06	0.11	0.13	0.15	0.10	0.06	3.02	0.00	1973	0.69	UNPE
0.00	0.00	0.61	1.34	2.27	4.22	5.03	5.40	3.12	1.71	0.49	0.00	1973	24.19	ADPE
2.09	1.31	5.38	2.17	3.47	2.19	2.03	2.28	1.72	3.68	3.33	3.28	1973	32.93	PCPN
2.09	1.31	4.77	0.83	1.20	-2.03	-3.00	-3.12	-1.40	1.97	2.84	3.28	1973	6.74	P-PE
0.00	0.00	0.00	0.00	0.00	-2.03	-5.03	-6.15	-9.55	-3.79	0.00	0.00	1973	-28.57	APWL
10.26	10.54	6.00	6.00	6.00	4.27	2.59	1.54	1.22	3.19	6.00	7.66	1973	5.44	STOR
0.00	0.00	0.00	0.00	0.00	-1.73	-1.68	-1.05	-0.32	1.97	2.81	0.00	1973	0.00	D ST
0.00	0.00	0.61	1.34	2.27	3.92	3.71								

APPENDIX 3

COMPUTED AND MEASURED SEASONAL RUNOFF - DUFFIN CREEK (PICKERING)

(DEPTH IN MILLIMETERS)

(a) WINTER					(b) SPRING				
Year	Month	a	b	c	Year	Month	a	b	c
1966	Dec.	51.3	1.5	26.2	1966	Mar.	72.7	20.8	44.5
1966	Jan.	21.3	8.6	17.0	1966	April	38.6	93.5	31.2
1966	Feb.	26.6	4.3	15.8	1966	May	21.3	48.8	31.8
1967	Dec.	52.8	13.7	35.1	1967	Mar.	39.4	0.3	50.8
1967	Jan.	26.9	0.8	20.3	1967	April	51.0	23.6	53.9
1967	Feb.	19.8	0.5	14.7	1967	May	31.0	112.0	20.3
1968	Dec.	29.7	6.6	21.6	1968	Mar.	89.4	34.3	101.1
1968	Jan.	21.6	5.3	23.9	1968	April	45.2	115.1	29.0
1968	Feb.	27.9	2.5	81.0	1968	May	32.8	43.7	23.6
1969	Dec.	14.7	1.0	13.2	1969	Mar.	43.7	0.8	58.2
1969	Jan.	29.5	3.3	35.3	1969	April	68.1	25.2	51.8
1969	Feb.	25.9	1.5	18.5	1969	May	41.2	120.4	30.7
1970	Dec.	18.3	0.5	22.4	1970	Mar.	68.6	38.1	40.6
1970	Jan.	13.2	0.5	11.2	1970	April	60.2	110.2	54.6
1970	Feb.	22.6	0.3	11.4	1970	May	30.2	55.1	23.1
1971	Dec.	28.9	0.8	41.9	1971	Mar.	52.8	0	39.6
1971	Jan.	11.2	0.3	19.3	1971	April	58.4	24.1	75.2
1971	Feb.	38.9	0	26.2	1971	May	29.2	108.2	15.2
1972	Dec.	71.4	6.9	48.0	1972	Mar.	56.9	0	42.2
1972	Jan.	13.5	0.5	20.1	1972	April	83.8	28.7	136.9
1972	Feb.	22.6	0.3	14.7	1972	May	41.9	129.8	23.4
1973	Dec.	35.1	1.0	21.3	1973	Mar.	104.1	31.2	32.3
1973	Jan.	16.3	3.1	12.2	1973	April	67.3	155.2	17.5
1973	Feb.	26.0	1.8	14.7	1973	May	50.6	92.9	28.5

a = computed runoff (Phillips, 1975)

b = computed runoff (Thorntwaite, 1957)

c = measured runoff

APPENDIX 3 (cont'd)

(c) SUMMER				(d) FALL					
Year	Month	a	b	c	Year	Month	a	b	c
1966	June	10.7	24.4	21.3	1966	Sept.	1.3	3.1	9.7
1966	July	5.3	12.2	5.8	1966	Oct.	0.8	1.5	9.2
1966	Aug.	2.5	6.1	6.4	1966	Nov.	2.8	3.3	20.6
1967	June	37.9	78.2	20.8	1967	Sept.	7.9	13.0	12.7
1967	July	19.0	39.4	21.6	1967	Oct.	11.2	13.7	24.4
1967	Aug.	15.5	25.7	21.6	1967	Nov.	26.4	27.4	25.9
1968	June	15.2	32.8	14.5	1968	Sept.	2.0	4.1	11.4
1968	July	7.6	15.5	8.9	1968	Oct.	3.6	4.8	11.4
1968	Aug.	3.8	8.4	9.4	1968	Nov.	12.5	13.0	19.8
1969	June	20.6	60.2	14.2	1969	Sept.	2.5	7.6	6.9
1969	July	10.4	30.2	8.6	1969	Oct.	1.3	3.8	10.4
1969	Aug.	5.1	15.0	8.4	1969	Nov.	0.8	2.0	16.5
1970	June	15.2	27.7	9.4	1970	Sept.	1.8	3.6	11.9
1970	July	7.4	13.7	12.5	1970	Oct.	1.0	1.8	14.5
1970	Aug.	3.8	6.9	9.9	1970	Nov.	0.5	0.8	20.6
1971	June	14.5	54.1	11.7	1971	Sept.	1.8	6.9	16.5
1971	July	7.4	26.9	13.2	1971	Oct.	1.0	3.3	12.7
1971	Aug.	3.6	13.5	16.5	1971	Nov.	0.5	1.5	16.0
1972	June	21.1	65.0	17.0	1972	Sept.	2.5	7.9	6.1
1972	July	10.4	32.5	11.7	1972	Oct.	1.3	4.1	7.6
1972	Aug.	5.3	16.3	11.7	1972	Nov.	12.7	14.0	8.1
1973	June	25.2	46.5	15.8	1973	Sept.	3.1	5.8	10.7
1973	July	12.7	23.1	9.9	1973	Oct.	1.5	3.6	14.7
1973	Aug.	6.4	11.7	11.9	1973	Nov.	1.3	2.0	26.2

a = computed runoff (Phillips, 1975)

b = computed runoff (Thorntwaite, 1957)

c = measured runoff

APPENDIX 4

Climatological stations used in the study

<u>Station</u>	<u>Latitude</u>	<u>Longitude</u>	<u>Elevation</u> (meters)
Beatrice	45°08'	79°23'	288.8
Beeton	44 06	79 47	232.3
Belleville	44 09	77 24	76.0
Brockville	44 36	75 42	91.2
Brucefield	43 33	81 33	258.4
Caledonia	43 05	79 57	205.2
Chatham	42 24	82 12	182.4
Delhi	42 52	80 33	231.0
Goderich	43 43	81 42	220.4
Gore Bay	45 53	82 34	190.0
Grimsby	43 12	79 34	92.7
Guelph	43 31	80 14	332.9
Harrow	42 02	82 54	190.3
Haliburton	45 01	78 33	319.2
Kemptville	45 00	75 38	97.3
Killaloe	45 34	77 25	173.6
Kitchener	43 26	80 30	342.0
Leamington	42 03	82 38	212.8
Lindsay	44 21	78 45	266.0
Lucknow	43 58	81 31	266.0
Madawaska	45 30	77 59	315.6
Muskoka	44 58	79 18	281.5
Orono	43 58	78 37	147.4
Ottawa CDA (1)	45 23	75 43	79.0

Appendix 4 (cont'd)

<u>Station</u>	<u>Latitude</u>	<u>Longitude</u>	<u>Elevation</u> (meters)
Ottawa International A (2)	45°19'	75°40'	125.6
Parry Sound	45 20	80 00	193.0
Pelee Island	41 45	82 41	174.8
Peterborough	44 17	78 19	193.0
Ridgetown	42 27	81 53	205.2
St. Thomas	42 48	81 11	207.3
Southampton	44 30	81 21	199.4
Toronto (1)	43 40	79 24	115.2
Toronto (Agincourt) (2)	43 47	79 16	179.4
Trenton	44 07	77 32	80.9
Turbine	46 23	81 34	205.2
Tweed	44 30	77 17	144.4
Vineland Station	43 11	79 23	79.0
Walkerton	44 08	81 09	243.2
Wallaceburg	42 35	82 24	176.3
Welland	43 00	79 16	174.8
Woodstock	43 08	80 46	281.2

Appendix 5
Computed monthly runoff probabilities

```
//RUNOFF JOH (XXXXXXXXXX.E.,8888).C.V.RAMASASTRY,CLASS=A          JOB 959
// EXEC WATFIV
//GO,SYSIN CD *
IEF1421 - STEP WAS EXECUTED - COND CODE 0000
IEF3731 STEP /GO / START 75343.1430
IEF3741 STEP /GO / STOP 75343.1431 CPU OMIN 11.30SEC MAIN 150K LCS OK
IEF3751 JOB /RUNOFF / START 75343.1430
IEF3761 JOB /RUNOFF / STOP 75343.1431 CPU OMIN 11.30SEC
```

```
1 JOB WATFIV XXXXXXXXXXXX
2 DIMENSION DATA(35,12), VECTOR(35), ITITLE(20)
3 REAL POSVAR, NEGVAR
4 INTEGER STOP
5 DATA STOP/'99999'/
6 IT=0
7 702 READ (5,100) ITITLE
8 100 FORMAT (20A4)
9 (ITITLE(1).EQ.STOP) GO TO 705
10 READ (5,102) N
11 102 FORMAT (I2)
12 WRITE (6,103) ITITLE, N
13 103 FORMAT (//,5X,'STATION ',20A4,5X,'NUMBER OF YEARS ',I3,/)
14 DO 104 I=1,N
15 READ (5,105) (DATA(I,J),J=1,12)
16 105 FORMAT (12F6.2)
17 104 CONTINUE
18 WRITE (6,500)
19 500 FORMAT (3X,'MONTH',5X,'MEAN',16X,'ST. DEV.',20X,'POSVAR',20X,'NEGV
20 AR',/)
21 DO 1000 J=1,12
22 SUMX=0.0
23 SUMX2=0.0
24 DO 2000 I=1,N
25 VECTOR (I)=DATA(I,J)
26 SUMX=SUMX+VECTOR(I)
27 SUMX2=SUMX2+VECTOR(I)*VECTOR(I)
28 2000 CONTINUE
29 VAR=(FLOAT(N)*SUMX2-SUMX*SUMX)/FLOAT(N*(N-1))
30 STDEV=SQRT(VAR)
31 AMEAN=SUMX/FLOAT(N)
32 POSVAR=(1.28*STDEV+AMEAN)*25.4
33 NEGVAR=(-1.28*STDEV+AMEAN)*25.4
34 WRITE (6,201) J,AMEAN,STDEV,POSVAR,NEGVAR
35 201 FORMAT (5X,I2,F15.5,5X,F15.5,5X,F20.5,5X,F20.5)
36 1000 CONTINUE
37 IT=IT+1
38 GO TO 702
39 705 CONTINUE
40 WRITE (6,555) IT
```

All values in centimeters.

39 555 FURMAT (////.5X.*NUMBER OF STATIONS TREATED*. 15)
 40 STOP
 41 END

ENTRY

STATION	ALCQUIN PARK		4535 7833 1419	
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.39955	0.35136	21.57176	-1.27488
2	0.44682	0.34743	32.83481	10.21347
3	1.07272	1.13604	84.50214	10.63205
4	4.54181	2.37606	192.61229	36.11166
5	2.07454	0.91902	82.57247	22.81415
6	1.14545	0.63463	49.72760	18.46124
7	0.57364	0.31675	24.86844	4.27226
8	0.20591	0.15934	12.41018	2.11399
9	0.23318	0.28630	15.23080	-3.38525
10	0.37227	0.59169	28.69264	-9.78122
11	1.16000	1.04735	63.51547	-4.58761
12	0.32636	0.39257	21.05289	-4.47355

STATION	BEATRICE		4508 7923 950	
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.96643	0.58472	41.55765	5.53673
2	1.22842	0.37403	43.37508	19.05426
3	2.68785	1.35666	112.37919	24.16360
4	5.72092	3.16672	248.47099	42.55821
5	2.98999	0.92593	106.04629	45.84541
6	1.58107	0.58118	59.05428	21.26389
7	0.79335	0.29150	29.55208	10.59790
8	0.40357	0.15476	15.28216	5.21924
9	0.44179	0.42918	25.17473	-2.73205
10	0.66786	0.77286	42.09979	-8.16366
11	2.13178	1.19137	92.88112	15.41325
12	1.23892	0.82127	58.16968	4.76763

STATION	BELLEVILLE		4409 7724 250	
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.78133	0.42807	33.76331	5.92826
2	1.20433	0.26592	39.23543	21.94447
3	2.81476	0.82333	98.26033	44.72433
4	3.19699	1.27295	122.58969	36.81754
5	1.95033	0.93014	79.77895	19.29762
6	1.00800	0.54312	43.26096	7.94519
7	0.54100	0.41922	27.37111	0.11162
8	0.27060	0.20986	13.68095	0.03503
9	0.13500	0.10523	6.85030	0.00762
10	0.17367	0.52011	21.32089	-12.49865
11	0.38533	0.62617	30.14560	-10.57070
12	0.79233	0.34461	55.91618	-5.50589

STATION	KEMPTVILLE		4500 7538 320	
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.52207	0.35481	24.79602	1.72505
2	0.94069	0.29412	33.45596	14.33086
3	2.36827	0.97801	91.95110	28.35693
4	2.83896	1.41778	118.20430	26.01472
5	1.79103	1.07817	80.54543	10.43877
6	0.93620	0.67669	45.77991	1.77918
7	0.48655	0.37407	24.52023	0.19657
8	0.24310	0.18790	12.28393	0.06571
9	0.14724	0.16217	9.01237	-1.53253
10	0.12414	0.19595	9.52381	-3.21762

11 0.50655 0.71116 35.98749 -10.25470
 12 0.60724 0.50224 31.75202 -0.90504

STATION HADAWASKA 4530 7759 1038

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.28333	0.27385	16.10014	-1.70693
2	0.66633	0.30432	26.81891	7.03069
3	1.34533	0.67370	61.15409	17.34792
4	2.93833	1.34711	118.43050	30.83643
5	1.62999	0.68549	63.68855	19.11511
6	0.89900	0.58196	41.75523	3.91380
7	0.46000	0.31248	21.84319	1.52479
8	0.32933	0.15587	10.83275	0.75736
9	0.20833	0.31608	15.56790	-4.98458
10	0.27667	0.63894	27.80049	-13.74586
11	0.72433	0.86584	46.54820	-9.75216
12	0.26333	0.42777	20.59634	-7.21904

STATION LEMINGTON 4203 8238 700

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.68866	0.56677	35.91878	-0.93467
2	0.98800	0.55646	43.18669	7.00349
3	2.41366	0.90534	90.74135	31.87248
4	2.22866	0.95472	87.64784	25.56807
5	1.35699	0.66663	56.14108	12.79422
6	0.74333	0.38066	31.25656	6.50457
7	0.39233	0.22525	17.28842	2.64208
8	0.19567	0.11337	8.65583	1.28401
9	0.11300	0.12052	6.78855	-1.04817
10	0.10233	0.23981	10.39590	-5.19738
11	0.12867	0.34032	14.33264	-7.79640
12	0.68867	0.94104	48.08727	-13.10306

STATION PARRY SOUND 4520 8000 635

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	1.01700	0.55153	43.76294	7.90046
2	1.17233	0.39330	42.56415	16.99007
3	2.70199	1.21215	108.04010	29.22110
4	4.76499	2.11239	189.70890	52.35265
5	2.76099	1.18471	108.64640	31.61186
6	1.41933	0.59574	55.41968	16.68217
7	0.70967	0.29877	27.73926	8.31173
8	0.37267	0.20216	16.03831	2.89311
9	0.36433	0.52865	26.44138	-7.93327
10	0.53167	0.79798	39.44815	-12.43953
11	1.85399	1.45120	94.27296	-0.09009
12	1.42400	0.83002	63.15497	9.18405

STATION LINDSAY 4421 7845 875

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.69566	0.48425	33.41367	1.92605
2	1.03900	0.24441	34.33682	18.44412
3	2.40033	0.92653	91.09164	30.84496
4	3.27866	1.27788	124.82440	41.73145
5	2.01966	1.00210	83.87955	18.71924
6	1.05666	0.51031	43.43047	10.24792
7	0.58967	0.36101	26.71466	3.24031
8	0.29467	0.18137	13.38118	1.56787
9	0.19333	0.25053	13.05602	-3.23472
10	0.24833	0.46752	21.50781	-8.89251
11	0.56033	0.67606	36.21262	-7.74776

STATION	ORONO	4358 8783 485	44.99728	-2.32547
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.87033	0.44740	36.65213	7.56054
2	1.27600	0.27792	41.44585	23.37466
3	2.89299	0.89486	102.32160	44.13437
4	3.33566	1.30212	127.05020	42.39114
5	2.05666	1.00472	84.90468	19.57359
6	1.05033	0.53707	44.13943	9.21721
7	0.42567	0.26902	22.09819	4.60565
8	0.26300	0.13562	11.08960	2.27078
9	0.14400	0.10241	6.99701	0.32817
10	0.15700	0.33203	14.78265	-6.80707
11	0.60100	0.75429	39.78876	-9.25801
12	1.12700	0.88196	57.29982	-0.04850

STATION	HARROW	4202 8254 626		
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.71000	0.62582	38.38068	-2.31207
2	0.94666	0.57528	42.78131	5.30912
3	2.34399	0.91341	89.23430	26.84052
4	2.09433	1.02001	86.35826	20.03351
5	1.21466	0.64407	51.79228	9.91248
6	0.63933	0.33762	27.21570	5.26232
7	0.33600	0.19956	15.02252	2.04826
8	0.16833	0.10014	7.53143	1.01988
9	0.09400	0.08900	5.28123	-0.50605
10	0.08333	0.24206	9.38665	-5.75333
11	0.16200	0.41094	17.47523	-6.24567
12	0.63833	0.93676	46.55962	-19.42334

STATION	BROCKVILLE	4435 7542 300		
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.91433	0.50120	39.51891	6.92901
2	1.31899	0.37041	45.54520	21.45969
3	3.33466	1.14620	121.96540	47.43524
4	3.73299	1.50549	143.76450	45.87148
5	2.24533	1.01790	90.12535	23.93721
6	1.12333	0.50946	45.06354	12.00154
7	0.56767	0.27132	23.23973	5.59764
8	0.29367	0.14789	12.26740	2.65685
9	0.16467	0.10644	7.64304	0.72200
10	0.35533	0.62294	29.27859	-11.22770
11	0.84400	0.92461	51.49834	-8.62130
12	1.22566	0.86168	60.92487	4.89473

STATION	BRUCEFIELD	4333 8133 850		
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.82766	0.47408	37.95993	7.13336
2	1.17366	0.30265	39.55083	19.97136
3	2.50933	0.84225	91.12004	36.35367
4	2.62733	1.17145	104.82030	28.64787
5	1.57633	0.73282	63.86429	16.21312
6	0.79200	0.36878	32.10643	8.12699
7	0.39667	0.18501	16.09045	4.06018
8	0.25900	0.31059	16.67639	-3.51922
9	0.12967	0.15873	8.45427	-1.86722
10	0.20300	0.40581	18.34995	-8.03757
11	0.61733	0.82076	42.36488	-11.00440

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.88814	0.49248	38.57048	6.54725
2	1.21370	0.37026	42.86572	18.79021
3	2.89703	0.97168	101.92440	45.24458
4	2.95592	1.31562	117.85380	32.30681
5	1.87407	0.95125	78.52835	16.67433
6	0.95703	0.51024	40.89738	7.71987
7	0.51222	0.36740	24.95517	1.06569
8	0.25667	0.18343	12.95587	0.54277
9	0.14741	0.13549	8.14928	-0.66101
10	0.13000	0.28188	12.46631	-5.86232
11	0.42407	0.74437	34.97237	-13.42945
12	1.10185	1.04819	62.06549	-6.09166

STATION TRENTON

44 07 7732 266

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.39615	0.27162	18.89314	1.23144
2	0.76577	0.31317	29.53228	9.26861
3	1.83153	0.76906	71.39467	21.64714
4	3.61576	1.17276	129.96910	53.71150
5	2.02692	0.76091	76.22250	26.74480
6	1.12000	0.58824	47.57274	9.32299
7	0.56077	0.29304	23.77075	4.71629
8	0.31808	0.24369	16.00192	0.15635
9	0.28308	0.40315	20.36250	-3.98223
10	0.49538	0.67629	35.22038	-10.05489
11	1.40884	1.23464	75.92511	-4.35594
12	0.53769	0.49805	29.85010	-2.53536

STATION TURBINE

4623 8124 675

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.72652	0.39121	31.17250	5.73476
2	1.21130	0.30925	40.82113	20.71284
3	2.76434	0.92174	100.18180	40.24648
4	3.17869	1.54701	131.03500	30.44231
5	1.96130	1.10479	85.73575	13.89820
6	0.98304	0.55188	42.71182	7.02658
7	0.49130	0.27516	21.42503	3.53320
8	0.24565	0.13846	10.74115	1.73796
9	0.12435	0.06894	5.39987	0.91698
10	0.21522	0.57305	24.09760	-13.16457
11	0.68000	0.83647	44.46722	-9.92327
12	0.95000	0.65777	45.51537	2.74450

STATION TWEED

44 30 7717 475

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.90154	0.46020	37.86095	7.93716
2	1.19923	0.41648	44.02090	16.91995
3	2.56538	1.18765	103.77360	26.54744
4	2.63769	1.85857	127.42310	6.57142
5	1.55769	1.09298	75.10043	4.03028
6	0.78615	0.55298	37.94491	1.99967
7	0.36385	0.27657	18.99559	1.01176
8	0.19615	0.13967	9.52340	0.44120
9	0.09769	0.06858	4.71089	0.25187
10	0.36615	0.61119	29.17143	-10.57084
11	0.66154	0.73826	40.80542	-7.19929

STATION WALKERTON

44 08 8109 800

12 0. PA769 0.81079 47.89183 -4.82910

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	3.62304	0.53137	33.10101	-1.45044
2	3.95261	0.52865	41.38377	7.00867
3	2.27130	1.05181	91.08745	23.49446
4	2.05130	1.06994	86.39895	17.31696
5	1.49217	0.95562	68.37011	6.83207
6	0.75552	0.47635	34.73256	3.72867
7	0.37739	0.23975	17.34796	1.82346
8	0.18956	0.12096	8.74764	0.88225
9	0.09565	0.05927	4.35506	0.50405
10	0.07852	0.11761	5.76747	-1.88019
11	0.20956	0.13947	16.35980	-5.71392
12	0.61739	0.80475	41.04581	-10.48237

STATION WALLACERBURG 4235 8224 580

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	1.07724	0.62414	47.65372	7.06991
2	1.47617	0.38848	50.09940	24.83900
3	3.33099	0.87051	113.13780	56.53369
4	3.06792	0.99259	110.19610	45.65434
5	1.94482	0.74464	73.60805	25.18883
6	0.97207	0.37276	36.80951	12.57141
7	0.48759	0.18518	18.40514	6.36421
8	0.24379	0.09348	9.23156	3.15311
9	0.14724	0.15741	8.85759	-1.37774
10	0.14138	0.32740	14.23543	-7.05339
11	0.25483	0.63699	29.72235	-11.69714
12	1.19793	0.93401	60.79387	0.06073

STATION WOODSTOCK 4308 8046 925

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.82556	0.36106	32.70796	9.23021
2	1.31555	0.29236	42.92030	23.90968
3	2.62000	0.78575	92.09398	41.00172
4	3.09055	1.46021	125.97440	31.02548
5	1.95777	1.02699	83.11690	16.33789
6	1.10555	0.62931	48.54105	7.62098
7	0.56444	0.33229	25.14017	3.53358
8	0.39333	0.37075	22.04460	-2.06330
9	0.23222	0.25202	14.09199	-2.29512
10	0.21833	0.31825	15.89270	-4.80138
11	0.78389	0.71431	43.13426	-3.31276
12	1.44777	1.05490	71.07030	2.47664

STATION VINELAND STATION 4311 7323 260

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.72466	0.56062	36.63329	0.17961
2	1.16333	0.50574	45.99112	13.10591
3	2.55066	0.78611	90.34473	39.22876
4	2.22699	0.92115	86.51398	26.61731
5	1.44033	0.73621	60.52010	12.64857
6	0.74700	0.40825	32.24658	5.70078
7	0.37367	0.20338	16.10327	2.87896
8	0.18733	0.10171	8.06495	1.45156
9	0.12967	0.22415	10.58116	-3.99412
10	0.12500	0.30096	12.95981	-6.60983
11	0.20900	0.48857	21.19290	-10.57572

STATION	PTERBOROUGH	44 17 7819 635		
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.45800	0.32468	22.1991J	1.07723
2	0.84730	0.26218	30.03701	12.98960
3	1.77366	0.81913	76.76254	23.49937
4	2.44633	1.20567	101.33540	22.93733
5	1.55433	0.92521	69.55021	9.39577
6	0.80433	0.47041	35.7238J	5.13615
7	0.41833	0.26597	19.27275	1.97855
8	0.20167	0.13338	9.56187	0.98917
9	0.14167	0.16626	9.0037J	-1.80708
10	0.13900	0.29021	12.96596	-5.90478
11	0.26933	0.48115	22.43409	-8.80199
12	0.51533	0.48025	28.7032J	-2.52440

STATION	PELEF ISLAND	44 45 8241 575		
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.64931	0.55511	34.54019	-1.55534
2	0.88413	0.52551	39.5424J	5.37156
3	2.20965	0.88460	84.88501	27.36508
4	2.30344	1.08754	93.33053	21.08429
5	1.50965	0.74701	62.63176	14.05843
6	0.79827	0.40803	33.5419J	7.01035
7	0.41069	0.20708	17.22905	3.63395
8	0.20724	0.10660	8.72968	1.79816
9	0.10379	0.05301	4.35982	0.91285
10	0.05828	0.04863	3.0612J	-0.10083
11	0.07483	0.18591	7.2448J	-4.14360
12	0.49034	0.95486	43.49915	-18.58966

STATION	MUSKOKA A	44 58 7918 926		
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.84866	0.52124	38.50258	4.60950
2	1.16666	0.30292	39.48158	19.78482
3	2.52033	1.12795	100.68810	27.34438
4	4.60466	1.95739	180.5968J	53.31976
5	2.74866	1.12899	106.5215J	32.11041
6	1.49600	0.66789	59.71259	16.28394
7	0.75033	0.33998	30.11171	8.00506
8	0.38667	0.19302	16.3968J	3.54580
9	0.35067	0.41313	22.40352	-4.58968
10	0.77233	1.00797	52.38814	-12.15376
11	1.83199	1.22017	86.20261	0.86266
12	1.24566	0.72594	55.24171	9.03792

STATION	KILLALORE A	45 34 7725 571		
MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.22800	0.20078	12.31897	-0.73659
2	0.56900	0.26498	23.06772	5.83742
3	-1.38866	0.64426	56.21808	14.32587
4	2.00800	1.29287	93.0368J	8.96939
5	1.22766	0.83264	58.2533J	4.11196
6	0.64200	0.42052	30.23886	2.37465
7	0.32433	0.21973	15.38186	1.09425
8	0.16233	0.10982	7.69365	0.55287
9	0.10067	0.13506	6.94796	-1.83411
10	0.09500	0.30614	12.36625	-7.54025
11	0.17933	0.32205	15.02555	-5.91544

12 0.14767 0.21907 10.87306 -3.37161

STATION ST. THOMAS 4248 8111. 682

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.89233	0.54406	40.35350	4.97675
2	1.22066	0.43337	45.09462	16.91493
3	2.91133	0.95065	104.85500	43.04030
4	2.96099	1.20463	114.37410	36.04430
5	1.82299	0.83350	74.16490	19.96715
6	1.01933	0.52326	42.90320	8.87869
7	0.50967	0.26085	21.42636	4.46466
8	0.31800	0.27941	17.16144	-1.00707
9	0.15933	0.13916	8.57137	-0.47726
10	0.14167	0.20610	10.29895	-3.10230
11	0.42500	0.67894	32.86862	-11.27866
12	1.18366	0.94755	60.87170	-0.74167

STATION ORILLIA 4437 7924 735

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.80333	0.44273	34.79878	6.01045
2	1.13291	0.28167	37.93373	19.61813
3	2.25666	0.92597	87.42438	27.21402
4	3.07874	1.69582	153.65450	43.38554
5	2.45268	1.22572	102.13340	22.43207
6	1.25875	0.61578	51.99225	11.95202
7	0.63833	0.30082	25.99387	6.43341
8	0.31833	0.15199	13.02720	3.14411
9	0.19917	0.12656	9.17344	0.94420
10	0.49875	0.69362	35.21930	-9.88285
11	0.86583	0.92988	52.19171	-8.20753
12	0.96791	0.69561	47.20061	1.96937

STATION SOUTHAMPTON 4430 8121 656

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	1.35143	0.59378	53.63113	15.02127
2	1.50428	0.32438	48.75510	27.66235
3	3.09952	1.20934	118.04560	39.40976
4	3.98476	1.78528	159.25580	43.16968
5	2.33190	1.15955	96.92953	21.23078
6	1.19095	0.59943	49.73863	10.76152
7	0.59524	0.29901	24.84039	5.39766
8	0.29809	0.15085	12.47509	2.66712
9	0.16286	0.09073	7.08630	1.18682
10	0.24238	0.48966	22.07635	-9.76342
11	0.80905	0.89972	49.93142	-8.70190
12	2.22857	1.41778	102.73040	10.51077

STATION RIDGETOWN 4227 8153 675

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.75633	0.60410	38.85120	-0.42969
2	1.10500	0.54030	45.63319	10.50055
3	2.57633	0.87465	93.87520	37.00214
4	2.50333	1.05622	97.92436	29.24466
5	1.60400	0.82078	67.42668	14.05626
6	0.85833	0.48753	37.65210	5.95103
7	0.42933	0.24315	18.81044	2.99066
8	0.21533	0.12213	9.44009	1.49882
9	0.10733	0.06186	4.73759	0.71492
10	0.08567	0.14402	6.85840	-2.50655
11	0.31333	0.50013	24.21896	-8.30166

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	1.22850	0.43177	45.24155	17.16603
2	1.49100	0.28504	47.13844	28.60413
3	2.87199	1.25713	113.82030	32.07692
4	3.17900	1.68453	135.51390	25.97893
5	1.95800	0.93608	80.15676	19.29936
6	1.02300	0.50953	42.55008	9.41813
7	0.54500	0.32150	24.29562	3.39034
8	0.27250	0.16036	12.13502	1.70795
9	0.16850	0.20095	10.81324	-2.25346
10	0.36050	0.67986	31.26016	-12.94679
11	1.00500	1.16184	63.30074	-12.24685
12	1.71750	1.23095	83.64496	3.60385

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.61467	0.45727	30.47920	0.74577
2	0.91800	0.33996	34.36977	12.26442
3	2.13166	1.01648	87.17196	21.09641
4	3.87499	2.61642	183.54040	13.41073
5	2.10566	1.15947	91.15050	15.78711
6	1.20099	0.80377	56.63734	4.37316
7	0.62213	0.41220	29.20866	2.40576
8	0.31200	0.20983	14.71424	1.13534
9	0.30600	0.43430	21.89238	-6.34762
10	0.68900	0.81161	43.88768	-8.88657
11	1.42500	1.04279	70.09819	2.29160
12	0.83333	0.59843	40.62257	1.71060

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.76966	0.51202	36.19612	2.90280
2	1.11466	0.42340	42.37806	14.54679
3	2.58399	0.79158	91.36922	39.89757
4	2.82333	1.25705	112.58170	30.84322
5	1.86833	0.95252	78.42375	16.48723
6	1.12433	0.75117	52.97980	4.13599
7	0.62433	0.50645	32.32376	-0.60774
8	0.35167	0.34817	20.25195	-2.38732
9	0.22867	0.28995	15.23512	-3.61888
10	0.24833	0.43875	20.57236	-7.95706
11	0.63933	0.68058	38.36591	-5.88788
12	1.02400	0.88059	56.16339	-1.09637

MONTH	MEAN	ST. DEV.	POSVAR	NEGVAR
1	0.38840	0.31363	20.06209	-0.33140
2	0.81120	0.31607	30.93628	10.30248
3	2.13839	0.90569	83.75094	24.86940
4	2.91920	1.84108	134.00450	14.29022
5	1.69560	1.24936	83.68734	2.44890
6	0.88720	0.67038	44.30028	0.73929
7	0.44400	0.33526	22.17758	0.37759
8	0.26400	0.33283	17.52649	-4.11533
9	0.14280	0.17375	9.27590	-2.02169
10	0.25560	0.47063	21.79332	-8.80886
11	0.82840	0.82481	47.85750	-5.77486
12	0.57480	0.43926	28.88115	0.31865

VITA AUCTORIS

- 1946 Born on December 10, 1946 in Kakaraparru, India.
- 1964 Enrolled in first year Science at the Sir C. R. Reddy College, Eluru, India.
- 1967 Graduated from Andhra University with the degree of Bachelor of Science (Mathematics, Physics and Chemistry).
- 1970 Graduated from Andhra University with the degree of Master of Science (Technology) in Meteorology and Oceanography. In the same year obtained a Post-Graduate Diploma in Applied Statistics. In September, 1970 enrolled for Doctoral studies in Meteorology at Andhra University, and obtained a Junior Research Fellowship from the Council of Scientific and Industrial Research, India.
- 1973 Senior Research Fellow in the Department of Meteorology and Oceanography, Andhra University.
- 1974 In September 1974 enrolled in the graduate program in Geography at the University of Windsor, Windsor, Ontario, Canada.
- 1975 Graduated from Andhra University with Doctor of Philosophy in Meteorology.
- 1976 Graduated from the University of Windsor with the degree of Master of Arts in Geography.