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ESTIMATING THE CUBIC FOOT VOLUME
OF
INDIVIDUAL SLASH PINE TREES
PLANTED IN EAST TEXAS

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by
Terry L. Hackett

REPORT NUMBER 8
TO
PARTICIPATING COMPANIES
IN THE
EAST TEXAS PINE PLANTATION RESEARCH PROJECT

A STUDY OF
LOBLOLLY AND SLASH PINE PLANTATIONS
IN
EAST TEXAS

CENTER FOR APPLIED STUDIES
SCHOOL OF FORESTRY
STEPHEN F. AUSTIN STATE UNIVERSITY
NACOGDOCHES, TEXAS 75962

Janis Leikent 1988

October, 1986

This is the eighth in a continuing series of reports describing results from the East Texas Pine Plantation Research Project.

Subject and content of each ETPRP report will be regional in scope and of particular interest to loblolly and slash pine plantation owners in East Texas.

Any suggestions, ideas or comments will always be welcomed.

* * * * *

Support from the participating companies...
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* * * * *

This report is based on a thesis being developed by Mr. Terry L. Hackett in his pursuit of a MSF degree. Expected graduation is May '87.

J. David Lenhart
Project Director
October 16, 1986

ESTIMATING THE CUBIC FOOT VOLUME
OF
INDIVIDUAL SLASH PINE TREES
PLANTED IN EAST TEXAS

by

Terry L. Hackett
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ABSTRACT. Equations are presented to estimate the cubic foot content of the wood and bark in the stem and branches of individual slash pine trees planted on site-prepared land in East Texas. Taper functions are also developed.

INTRODUCTION

The estimation of the content of individual trees is a principal component in the measurement process to determine per acre yields. In particular, the content of individual trees is a value needed in the last stages of the diameter distribution yield prediction method. Also, tree information is useful in timber cruising.

In this report, equations are presented to estimate the cubic foot content of individual planted slash pines on non-old-fields in East Texas as:

1. Complete Tree Cubic Foot Wood and Bark: CTCFWB.
2. Complete Tree Cubic Foot Wood only: CTCFW.
3. Total Stem Cubic Foot Wood and Bark: TSCFWB.
4. Partial Stem Cubic Foot Wood and Bark: PSCFWB.
5. Total Stem Cubic Foot Wood only: TSCFW.
6. Partial Stem Cubic Foot Wood only: PSCFW.

By appropriate subtraction, the cubic feet of bark and the cubic feet of branches can be determined. Differences between total stem and partial stem values can be obtained for various multiple-product computations.

TREE MEASUREMENTS

A total of 52 slash pine sample trees located in the buffer zones of 26 of our 81 ETPRP permanent plots in slash pine plantations were felled during January - March, 1966. Two trees were sampled per plantation. The distribution of the 52 sample trees by county and by dbh and height classes is shown in Figure 1.

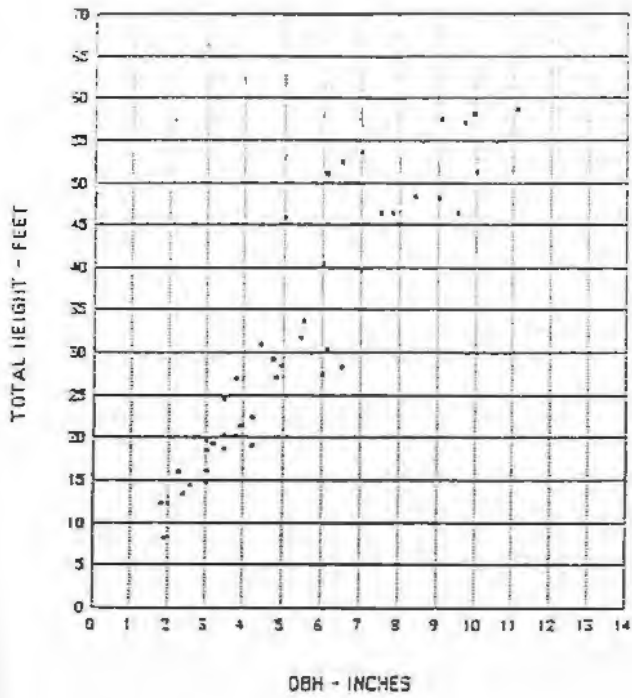
Prior to felling a tree, the dbh and crown class were determined. After felling, the branches were removed and weighed. A typical branch was weighed with and without needles. Eight branch segments (12" long) were cut and weighed with and without bark.

At 3-foot cut points along the stem, dob was recorded. Then the stem was bucked into 3-foot long bolts. Each bolt was weighed. At the bottom of each bolt, a 1- to 2-inch disk was cut. Each disk was weighed with and without bark. In addition, dib for each disk was noted. The top stem segment was also weighed and considered part of the stem.

The necessary field data was now available to compute observed cubic foot tree volume with and without bark as:

1. Partial stem to the top of each successive bolt.
2. Total stem.
3. Branches.

Branch volume was calculated using appropriate ratios of cubic feet to green weight. Complete tree cubic feet was determined by summing total stem and branch values.



NUMBER OF SLASH PINE SAMPLE TREES
BY DBH AND HEIGHT. n = 52 trees.



Figure 1.

SLASH

n = 52 trees

Number of sample trees by county in Texas.

COMPLETE TREE ESTIMATION

Plottings of CTCFWB and CTCFW over dbh (D) and total tree height (H) indicated a model originally suggested by Schumacher and Hall (1933) as

$$\text{Tree content} = b_0 D^{b_1} H^{b_2} \quad (1)$$

represented the relationships seen in the plottings.

Non-linear regression analysis of the data set produced the following prediction equations as

$$\text{CTCFWB} = 0.004023 D^{2.010570} H^{0.934455} \quad (2)$$

and

$$\text{CTCFW} = 0.001090 D^{2.016044} H^{1.117842}, \quad (3)$$

with $R^2 = 99\%$ for both equations*.

* All R^2 values in this report were calculated using non-linear regression results as:

$$R^2 = ((n-1)(\text{std dev dep var})^2 - \text{Residual SS}) / ((n-1)(\text{std dev dep var})^2) (100)$$

PARTIAL AND TOTAL STEM ESTIMATION

In a dissertation by McTague (1965), a new stem content estimation model was presented, that has several desirable properties:

1. Treats total stem content as a special case of partial stem content.
2. Predicts stem content between stump and any upper stem diameter limit.
3. Convertible to a well-behaved taper function.
4. Also, suitable for estimating green or dry weight of the total or partial stem.

Subsequently, Pienaar and others (1985) developed variations of the original McTague model as

$$\begin{aligned} \text{Volume wood \& Bark in the stem} &= b_0 D^{b_1} H^{b_2} \\ &- b_3 (d^{b_4} / D^{b_4} - 2)(H - 4.5), \end{aligned} \quad (4)$$

where d = upper stem diameter o. b. and

$$b_3 = 0.00545415(1 - 2/b_4),$$

and

$$\begin{aligned} \text{Volume wood only in the stem} &= c_0 D^{c_1} H^{c_2} \\ &- c_3 (d^{c_4} / D^{c_4} - 2)(h - 4.5), \end{aligned} \quad (5)$$

Equation (4) was used in non-linear regression analysis with a data set comprised of 540 cases of cubic feet wood and bark . The resulting equation is

$$\begin{aligned} \text{PSCFWB} = & 0.002021D^{1.790506}H^{1.183087} \\ & - 0.0024438d^{3.62363}D^{-1.623631}(H - 4.5) \end{aligned} \quad (6)$$

with $R^2 = 98\%$.

If the value for the variable d (upper stem diameter o. b.) in Eq. 6 is set to zero (or the top of the stem), the latter part of Eq. 6 disappears, and the result is an equation to estimate

$$\text{TSCFWB} = 0.002021D^{1.790506}H^{1.183087} \quad (7)$$

Equation (5) was used in non-linear regression analysis with a data set comprised of 540 cases of cubic feet wood only . The resulting equation is

$$\begin{aligned} \text{PSCFW} = & 0.000838D^{1.859712}H^{1.301838} \\ & - 0.001916d^{3.508595}D^{-1.508595}(H - 4.5) \end{aligned} \quad (8)$$

with $R^2 = 98\%$

and

$$\text{TSCFW} = 0.000838D^{1.859712}H^{1.301838} \quad (9)$$

Tables 1 and 2 show predicted cubic foot volumes for various combinations of D, H and d based on Eqs. 6 and 8, respectively.

TABLE 1. ESTIMATED CUBIC FEET OF WOOD AND BARK IN THE STEM TO SPECIFIED UPPER DIAMETER LIMITS FOR INDIVIDUAL SLASH PINE TREES ON NON-OLD-FIELD PLANTATIONS IN EAST TEXAS.

DBH (IN)	UPPER STEM DIAMETER (IN)	TOTAL TREE HEIGHT (FEET)						
		20	30	40	50	60	70	80
2	0	0						
4	0	1	1					
	2	1	1					
6	0		3	4	5			
	2		3	4	5			
	4		2	3	4			
8	0			7	9	11		
	2			7	9	11		
	4			6	8	10		
	6			5	6	8		
10	0				13	16	19	
	2				13	16	19	
	4				12	15	18	
	6				11	14	16	
12	0					22	26	31
	2					22	26	31
	4					22	26	30
	6					20	24	29
	8					17	21	25
14	0					29	35	41
	2					29	35	41
	4					29	34	40
	6					28	33	39
	8					25	31	36

TABLE 2. ESTIMATED CUBIC FEET OF WOOD ONLY IN THE STEM TO SPECIFIED UPPER DIAMETER LIMITS FOR INDIVIDUAL SLASH PINE TREES ON NON-OLD-FIELD PLANTATIONS IN EAST TEXAS.

DBH (IN)	UPPER STEM DIAMETER LIMIT (IN)	TOTAL TREE HEIGHT (FEET)						
		20	30	40	50	60	70	80
2	0	0						
4	0	1	1					
	2	0	1					
6	0		2	3	4			
	2		2	3	4			
	4		2	2	3			
8	0			5	7	8		
	2			5	6	8		
	4			4	6	8		
	6			3	4	6		
10	0				10	13	15	
	2				10	12	15	
	4				10	12	15	
	6				8	11	13	
12	0					18	21	26
	2					18	21	26
	4					17	21	25
	6					16	20	24
	8					14	17	21
14	0					23	29	34
	2					23	29	34
	4					23	28	34
	6					22	27	33
	8					20	25	30

TAPER FUNCTIONS

Based on a procedure outlined by Clutter (1980) and Pienaar et al. (1985), Eq. 6 was converted into the following taper equations as

$$\text{Upper stem dob} = D((H - L)/(H - 4.5))^{0.6159034}, \quad (10)$$

Where L = Position on upper stem where dob occurs,

and

$$L = H - (H - 4.5)(\text{dob}/D)^{1.623631}. \quad (11)$$

Eq. 8 was converted into the following taper equations as

$$\text{Upper stem dib} = 0.871278D((H - L)/(H - 4.5))^{0.580480}, \quad (12)$$

and

$$L = H - 1.267900(H - 4.5)(\text{dib}/D)^{1.722714}. \quad (13)$$

where L = Position on upper stem where dib occurs,

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