



LAWRENCE
LIVERMORE
NATIONAL
LABORATORY

Thermodynamic States in Explosion Fields

A. L. Kuhl

October 21, 2009

14th International Detonation Symposium
Coeur d' Alene, ID, United States
April 11, 2010 through April 16, 2010

Disclaimer

This document was prepared as an account of work sponsored by an agency of the United States government. Neither the United States government nor Lawrence Livermore National Security, LLC, nor any of their employees makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States government or Lawrence Livermore National Security, LLC. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States government or Lawrence Livermore National Security, LLC, and shall not be used for advertising or product endorsement purposes.

THERMODYNAMIC STATES IN EXPLOSION FIELDS

Allen L. Kuhl

Lawrence Livermore National Laboratory
P.O. Box 808, Livermore, CA 94551 USA kuhl2@llnl.gov

Here we investigate the thermodynamic states occurring in explosion fields from the detonation of condensed explosives in air. In typical applications, the pressure of expanded detonation products gases is modeled by a Jones¹-Wilkins²-Lee³ (JWL) function: $p_{JWL} = f(v, s_{CJ})$; constants in that function are fit to cylinder test data. This function provides a specification of pressure as a function of specific volume, v , along the expansion isentrope ($s = \text{constant} = s_{CJ}$) starting at the Chapman-Jouguet (CJ) state. However, the JWL function is not a fundamental equation⁴ of thermodynamics, and therefore gives an incomplete specification of states. For example, explosions inherently involve shock reflections from surfaces; this changes the entropy of the products, and in such situations the JWL function provides no information on the products states. In addition, most explosives are not oxygen balanced, so if hot detonation products mix with air, they after-burn, releasing the heat of reaction via a turbulent combustion process. This raises the temperature of explosion products cloud to the adiabatic flame temperature ($\sim 3,000\text{K}$). Again, the JWL function provides no information on the combustion products states.

This conundrum may be overcome by using the Cheetah code⁵ as an equation-of-state module. As inputs, one specifies the chemical composition of the substance and two thermodynamic variables; Cheetah then finds the thermodynamic equilibrium (or constrained equilibrium) solution by minimizing the Gibbs free energy of the system; the output is all thermodynamic variables at that state. This approach was used to analyze the thermodynamic states from the detonation of a C-4 charge ($\rho_0 = 1.6 \text{ g/cc}$) and the combustion of the detonation products with air.

Figure 1 depicts the locus of states of the C-4 detonation products in the pressure-specific volume plane. The locus starts at the *Chapman-Jouguet (CJ)* state, and expands down the isentrope ($s_{CJ} = 1.768 \text{ cal/g-K}$) to atmospheric pressure. The locus was fit with the following JWL function:

$$p_{PG}^{JWL}(v, T) = A \left(1 - \frac{\omega \cdot v_0}{R_1 \cdot v} \right) e^{-R_1 \cdot v/v_0} + B \left(1 - \frac{\omega \cdot v_0}{R_2 \cdot v} \right) e^{-R_2 \cdot v/v_0} + R_{DP} T/v \quad (1)$$

where $A = 5.23 \text{ Mbar}$, $B = 0.154 \text{ Mbar}$, $R_1 = 4.30$, $R_2 = 1.70$ and $R_{DP} = 3.12 \text{ (bar-cc/g-K)}$. Note that for specific volumes larger than $\sim 10 \text{ cc/g}$, the function reduces to the perfect gas law.

Figure 2 presents the same locus in the specific internal energy—temperature plane. Points (red circles) were calculated by the Cheetah code, assuming that the composition of detonation products was frozen for $T < 1,800 \text{ K}$. The solution starts at the *CJ* point ($T_{CJ} = 3,238 \text{ K}$) and expands down the isentrope ($s_{CJ} = 1.768 \text{ cal/g-K}$) to room temperature. The standard energy of C-4 Reactants and Products at *stp* (1 atm, 298K) are: $u_{F,R}^0 = 73.114$ and $u_{F,P}^0 = -1,173.68 \text{ cal/g}$, respectively; their difference is the heat of detonation:

THERMODYNAMIC STATES IN EXPLOSION FIELDS

$u_{F,P}^0 - u_{F,R}^0 \equiv \Delta H_d = -1,248 \text{ cal/g}$, and is indicated on the figure. Also shown in that figure is the *equilibrium* isentrope (blue curve), which assumes chemical equilibrium at all temperatures. At room temperature, it results in energy of -1,350 cal/g which disagrees with the measured heat of detonation. This effect is typical of condensed explosives; quenching induced by the strong rarefaction created when the DP gases expand from the CJ state stops the kinetic reactions at $\sim 1,800 \text{ K}$. A Constant Volume Detonation (CVD) is represented by the $u = u_{F,R}^0$ line from R to P . It gives a CVD detonation temperature of 2,887 K.

Figure 3 depicts the locus of states for the equilibrium products CP for the stoichiometric combustion of C-4 in air ($\sigma_s = 2.1$). The red line represents isobaric ($p = 1 \text{ atm}$) combustion locus. The standard energy of C4-air Reactants and Products at *stp* are: $u_{CP,R}^0 = +9.677 \text{ cal/g}$ and $u_{CP,P}^0 = -1,016.77 \text{ cal/g}$, respectively; their difference is the heat of combustion: $u_{CP,P}^0 - u_{CP,R}^0 \equiv \Delta H_c = -929.04 \text{ cal/g}_m = -2,880 \text{ cal/g}_{C_4}$, which is indicated on the figure. Adiabatic Combustion (AC) is represented by the $u = u_{CP,R}^0$ line from R to P . It gives an adiabatic combustion temperature of 2,816 K. For temperatures below 3,000 K, these curves are only a function of temperature. Therefore the loci of states in Fig. 3 were fit with quadratic functions of temperature:

$$u_k(T) = a_k T^2 + b_k T + c_k \quad k=F, A, R, CP \quad (2)$$

thereby providing a caloric equation of state for the combustion products. In hydro codes, one typically carries the density ($\rho_k = 1/v_k$) and specific internal energy (u_k) as independent variables. Given u_k , the above relation may be inverted:

$$T_k = [-b_k + \sqrt{b_k^2 - 4a_k(c_k - u_k)}] / 2a_k \quad (3)$$

to determine the temperature. Then pressure is calculated from the perfect gas relation:

$$p = RT/v \quad (4)$$

We will show that the above relation is valid for pressures less than one kilo-bar.

The above relations were used to derive the *Fundamental Equation* for the detonation products and combustion products:

$$u(s,v) = aT_*^2 e^{2s/c_v} (v_*/v)^{2R/c_v} + bT_* e^{s/c_v} (v_*/v)^{R/c_v} + c \quad (5)$$

where T_* and v_* represent the temperature and specific volume in the reference state denoted by subscript *. Given the fundamental equation: $u(s,v)$ one can use the Maxwell Relations⁴ to evaluate the temperature, pressure, specific heat and enthalpy of the products:

$$T(s,v) \equiv \left(\frac{\partial u}{\partial s} \right)_v, \quad p(s,v) \equiv - \left(\frac{\partial u}{\partial v} \right)_s, \quad c_v(s,v) \equiv \left(\frac{\partial u}{\partial T} \right)_v = \left(\frac{\partial u}{\partial s} \right)_v \left(\frac{\partial T}{\partial s} \right)_v, \quad h(s,v) \equiv u + pv \quad (6)$$

Summary: the above methodology can be used to specify all thermodynamic states occurring in explosion fields. And it is represented in form suitable for specifying the equations of state for hydro code simulations of explosions. More details, including a description of the historical development of the JWL function and the derivation of the Fundamental Equation (5), will be provided in the paper.

—WORD COUNT = 830 words (without figures)—

References

- [1] H. Jones and A. R. Miller, The Detonation of Solid Explosives, *Proc. Roy. Soc. London A*, **194**, 1948 p. 480
- [2] M. L. Wilkins, *The Equation of State of PBX 9404 and LXO4-01*, Lawrence Radiation Laboratory, University of California, Livermore, **UCRL-7797**, 1964.
- [3] E. L. Lee, H. C. Hornig and J. W. Kury, *Adiabatic Expansion of High Explosive Detonation Products*, Lawrence Radiation Laboratory, University of California, Livermore, **UCRL-50422**, 1968, 35 pp.
- [4] [17] J. Kestin, *A Course in Thermodynamics (vid esp. Chapter 12: Some Consequences of the First Part of the Second Law of Thermodynamics: Relations between Properties, pp. 531-562) Vol. 1*, Hemisphere Pub. 1979.
- [5] L. E. Fried, *CHEETAH 1.22 User's Manual*, **UCRL-MA-117541** (rev. 2), LLNL, 187 pp, 1995.

Abstract Control Number 03040

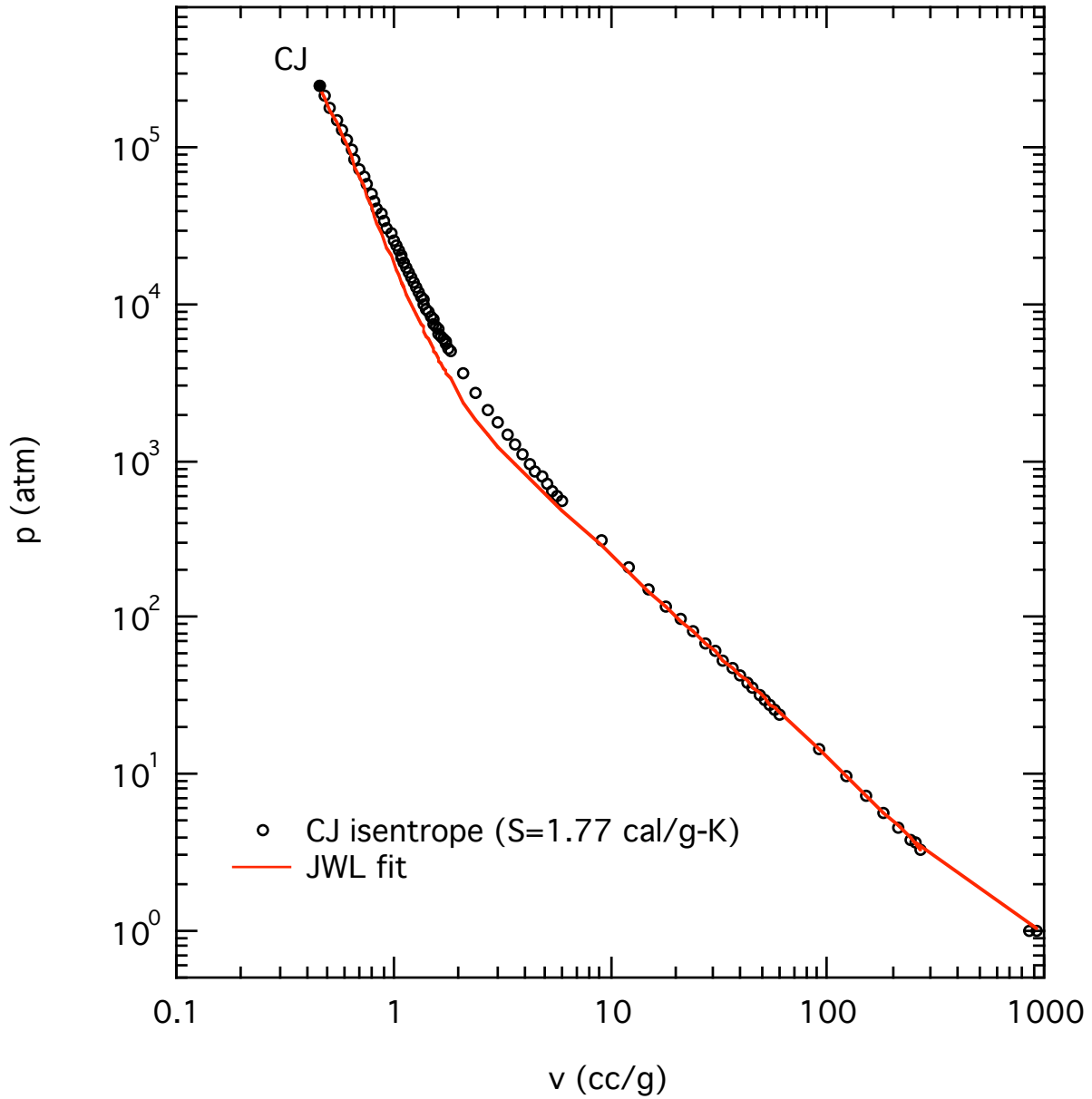


Figure 1. Pressure-volume diagram depicts the locus of states of the detonation products gases as they expand down the CJ isentrope for a C4 charge. Locus is fit with the JWL function (1).

THERMODYNAMIC STATES IN EXPLOSION FIELDS

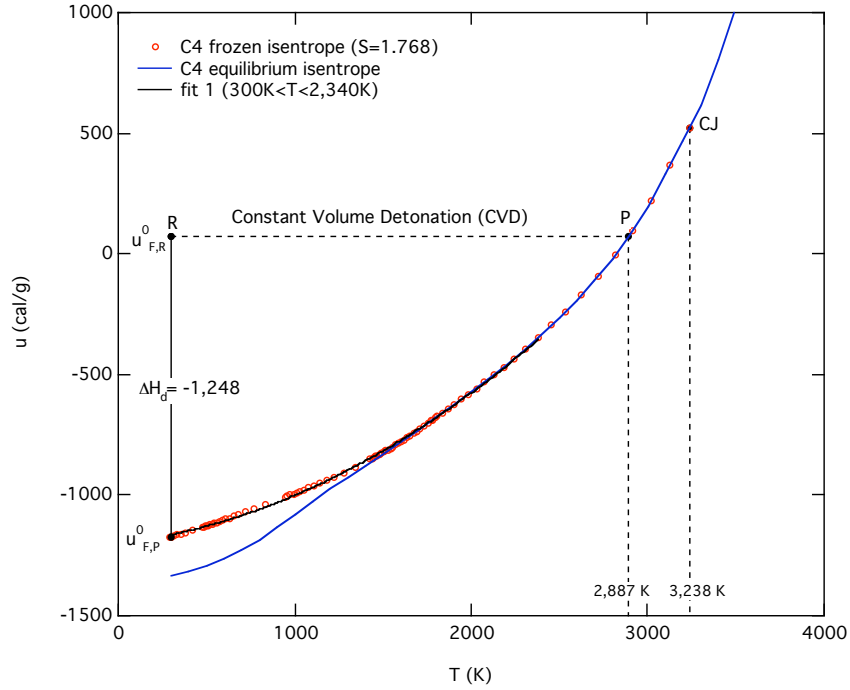


Figure 2. *Le Chatelier* diagram depicting the locus of states of the detonation products of the explosive C-4, starting at the *Chapman-Jouguet* point (*CJ*) and expanding at constant entropy to one atmosphere.

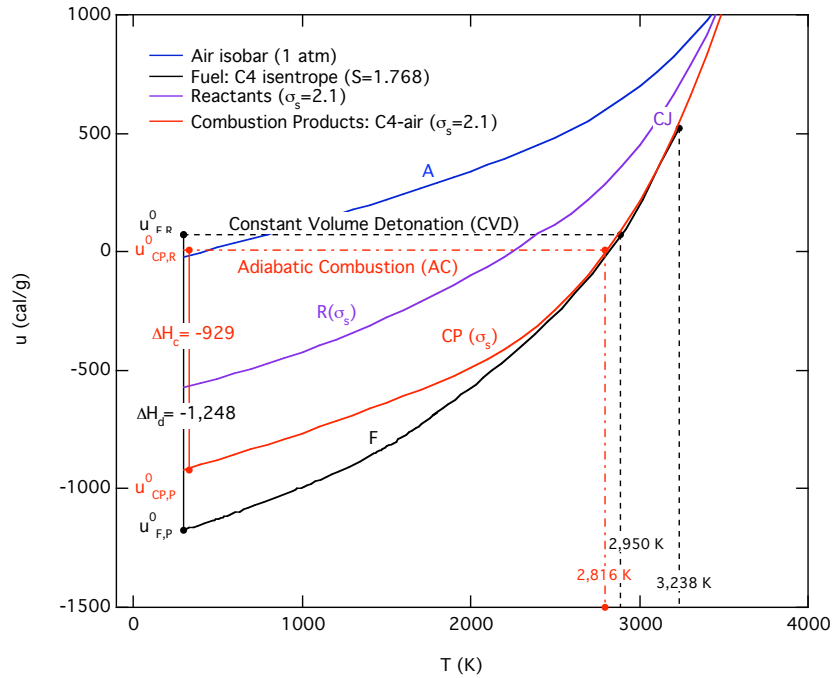


Figure 3. *Le Chatelier* diagram depicting the locus of states for the detonation of a C-4 charge (*curve F*) and its stoichiometric combustion with air (*curve CP*). Also shown are loci of the reactants (*curve R*) and air (*curve A*).