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Title:

A Dynamic Chamber System Coupled With a Tunable Diode Laser for Online Measurements of Delta-13C, Delta-18O, and Efflux Rate of Soil Respired Carbon Dioxide

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A dynamic soil chamber system coupled with a tunable diode laser for online measurements of  $\delta^{13}$ C,  $\delta^{18}$ O, and efflux rate of soil respired CO<sub>2</sub> Running Title: Soil chamber coupled with TDL reveals high frequency response to pulse watering. Heath H. Powers, Corresponding author Earth and Environmental Sciences Division MS-J495 Los Alamos National Laboratory Los Alamos, NM 87545, USA hpowers@lanl.gov, 505-606-0795 John E. Hunt Landcare Research Global Change Processes PO Box 40 Lincoln 7640, New Zealand, David T. Hanson University of New Mexico Department of Biology 167 Castetter Hall Albuquerque, NM 87131, USA Nate G. McDowell Earth and Environmental Sciences Division MS-J495 Los Alamos National Laboratory Los Alamos, NM 87545, USA For submittal to Global Change Biology January 6, 2009 Keywords: soil respiration, delta 13C, delta 18O, tunable diode laser, soil chamber, stable isotope

#### Abstract

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High frequency observations of the stable isotopic composition of CO<sub>2</sub> effluxes from soil have been sparse due in part to measurement challenges. We developed an open-system method that utilizes a flow-through chamber coupled to a tunable diode laser (TDL) to quantify the rate of soil CO<sub>2</sub> efflux and its  $\delta^{13}$ C and  $\delta^{18}$ O signatures. We tested the method first in the laboratory using an artificial soil test column and then in a semi-arid woodland. We found that CO<sub>2</sub> efflux rates of 1.2 to 7.3 µmol m<sup>-2</sup> s<sup>-1</sup> measured by the chamber-TDL system gave similar results to measurements made using the chamber and an infrared gas analyzer (IRGA) (R<sup>2</sup>=0.99) and compared well to efflux rates generated from the artificial test column (R<sup>2</sup>=0.94). Measured  $\delta^{13}$ C and  $\delta^{18}$ O of CO<sub>2</sub> efflux from the test column were not significantly different from measurements of gas inside of the test column across all efflux rates (p > 0.05) after accounting for diffusive enrichment. Isotopic differences between chamber measurements and values from CO<sub>2</sub> gas introduced into the test column resulted primarily from diffusion of atmospheric CO<sub>2</sub> into the test column and pressure artifacts from the chamber. Field measurements during drought demonstrated a strong dependency of CO<sub>2</sub> efflux and isotopic composition on soil water content. Addition of water to the soil beneath the chamber resulted in average changes of +6.9  $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>, -5.0%, and -55.0% for soil CO<sub>2</sub> efflux,  $\delta$ <sup>13</sup>C and  $\delta$ <sup>18</sup>O, respectively, within 25 minutes of water addition. The soil chamber coupled with the TDL was found to be an effective method for capturing high-resolution soil CO<sub>2</sub> efflux and its stable isotopic composition.

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#### Introduction

Atmospheric measurements of CO<sub>2</sub> mole fraction have allowed scientists to determine that globally about half of anthropogenically emitted CO<sub>2</sub> stays in the atmosphere and the rest is absorbed by the biosphere (Battle et al. 2000). The isotopic composition of the carbon and

oxygen ( $\delta^{13}$ C and  $\delta^{18}$ O respectively) of CO<sub>2</sub> in the atmosphere reflect strong fractionation by terrestrial ecosystems dominated by C<sub>3</sub> and to a lesser extent C<sub>4</sub> plants (Bender 1971). Therefore, the isotopic signatures of terrestrial respiratory effluxes are a valuable tracer of CO<sub>2</sub> movement through terrestrial ecosystems (Miller et al. 2003) and provide an opportunity to partition oceanic and terrestrial carbon fixation (Ciais et al. 1995). However, models that partition sources and sinks of carbon based on constant values of terrestrial isotopic fractionation during respiration may give incorrect results (Fung et al. 1997, Randerson et al. 2002b). Soil CO<sub>2</sub> efflux plays a major role in global carbon cycling and in the isotopic content of atmospheric CO<sub>2</sub>. Annually, it is estimated that 68 Gt of CO<sub>2</sub> evolves from the soil (Raich & Schlesinger 1992), more than 10 times the amount emitted anthropogenically through fossil fuel combustion (Randerson et al. 2002a). Soil respired CO<sub>2</sub> is produced from heterotrophic decomposition of organic matter and from autotrophic respiration of plant roots in the rhizosphere (Law et al. 1999). Soil respired  $\delta^{13}$ C ( $\delta^{13}$ C<sub>R</sub>) and  $\delta^{18}$ O ( $\delta^{18}$ O<sub>R</sub>) is variable but the mechanisms regulating these signatures are poorly understood (Cerling 1984, Farquhar et al. 1993, Ehleringer et al. 2000). Several studies have utilized chamber-based measurements of bulk soil CO2 efflux to quantify ecosystem carbon cycling but far fewer have incorporated measurements of stable isotopes of respired CO<sub>2</sub>. Of the studies that incorporated these measurements, several chamber types were used but all involved periodically collecting gas samples and taking them for post

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quantify ecosystem carbon cycling but far fewer have incorporated measurements of stable isotopes of respired CO<sub>2</sub>. Of the studies that incorporated these measurements, several chamber types were used but all involved periodically collecting gas samples and taking them for post analysis with a mass spectrometer (Miller *et al.* 1999, Ekblad & Hogberg 2000, McDowell *et al.* 2004). Although these earlier studies were able to capture *in situ* measurements of the isotopic composition of soil CO<sub>2</sub> efflux, they were unable to conduct experiments with high temporal resolution. In these experiments, the frequency of sample collection was inherently limited by

the time and effort required by flask collection and off-line analysis by a mass spectrometer. An additional complication is that chamber-based samples of soil respired CO<sub>2</sub> are difficult to collect without adversely affecting the soil efflux and isotopic composition. This is partly due to the mass flow of soil gas that is drawn into the chamber headspace in order to replace the volume removed by the sample (Rayment & Jarvis 1997). The replacement gas can either come from the soil, which generally has a high CO<sub>2</sub> concentration ([CO<sub>2</sub>]) and is enriched in heavier isotopes (Cerling et al. 1991), or from the atmosphere, which dilutes the soil gas in the chamber and again alters the isotopic signature in the chamber.

Two system configurations can be employed to measure fluxes and isotopic composition of soil respired  $CO_2$ . Open or flow-through soil chambers have a continuous flow of air through the chamber headspace, an inlet for incoming air, an outlet that exhausts gas from the chamber, and an opening to the soil surface. Information about  $[CO_2]$ ,  $\delta^{13}C_R$  and  $\delta^{18}O_R$  ( $\delta_R$  collectively) are calculated from differences of measurements of the air entering and exiting the chamber. Closed chambers have an opening to the soil but are otherwise closed to the atmosphere; gas exiting the chamber is recirculated into the chamber headspace and determinations of efflux rate and isotopic composition are derived based upon the buildup of  $CO_2$  over time within the chamber and the corresponding changes in isotopic values. Open chambers are known to be susceptible to pressure differentials between the inside of the chamber and ambient pressure due to air either being blown or drawn through the chamber (Davidson *et al.* 2002, Widen & Lindroth 2003). Differences in pressure as little as 1 Pa have been shown to affect efflux measurements by inducing mass flow of  $CO_2$  either into or out of the soil (Fang & Moncrieff 1996). Pressure differences of less than 0.1 Pa are needed to minimize impacts on soil  $CO_2$  efflux measurements (Fang & Moncrieff 1996). Since closed chambers recirculate gas through

their headspace, they keep the entire volume of gas in the system contained and as such they are a constant volume system. If a sub-sample is drawn from a closed chamber, the pressure is decreased proportionally to the volume of the sample removed. Generally, the pressure is subsequently equalized by mass movement of gas from the soil into the chamber or from the atmosphere through a pressure-equalizing vent (Lund *et al.* 1999). In contrast, open chambers are not constant volume systems since gas is constantly introduced into the inlet and exhausted from the outlet.

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An advantage of open chambers for isotopic measurements is that sub-samples can be collected from the inlet and exhaust of the chamber without altering the pressure inside of the chamber. This allows for determination of  $\delta^{13}$ C and  $\delta^{18}$ O of CO<sub>2</sub> emitted from soil using the "on-line" approach of Evans et al. (1986) (equation 2). This technique lends itself well to high frequency analysis using tunable diode laser (TDL) absorption spectroscopy for measurements of CO<sub>2</sub> entering and exiting the soil chamber. The TDL uses a laser that can vary its frequency in order to match the absorption frequency of specific isotopologues and scan the breadth of the absorbance feature (Bowling et al. 2003). This is done for all of the isotopologues of interest (e.g. <sup>13</sup>C<sup>16</sup>O<sub>2</sub>, <sup>12</sup>C<sup>16</sup>O<sub>2</sub>, <sup>12</sup>C<sup>18</sup>O<sup>16</sup>O) with high frequency so mole fractions of each species can be found. The particular instrument used in this study (TGA100A, Campbell Scientific) has a scan rate of 500Hz with data output averaged to 10Hz for high frequency measurements, although typically measurements are averaged for 10-15 seconds for improved precision. TDL measurements have become increasingly important in ecological studies because they allow large numbers of measurements to be collected continuously and they simultaneously measure [CO<sub>2</sub>] and stable isotopic composition (Bowling et al. 2003, Griffis et al. 2005, McDowell et al. 2008).

Here, we explore the use of a TDL coupled to a dynamic flow-through chamber system modified from Fang and Moncrieff (1996) for measuring soil  $CO_2$  efflux and determining  $\delta^{13}C_R$  and  $\delta^{18}O_R$  of soil respiration at high temporal frequency. We used a TDL for sampling the inlet and outlet of the chamber in order to produce these measurements at 2 minute intervals, a frequency sufficient to capture rapid, transient shifts in respiration and  $\delta_R$  value. We assessed the accuracy and precision of this chamber system using an artificial test column with known efflux rates and isotopic composition. Additionally, we field tested the chamber to determine the ability of the system to capture dynamic, transient events associated with pulse wetting of soils.

#### Theory

Soil  $CO_2$  respiration strongly controls near-surface  $[CO_2]$  and its stable isotopic composition. In  $C_3$  dominated ecosystems, plant root and soil microbial respiration generates  $\delta^{13}C_R$  values from -23‰ to -30‰ (Ehleringer et al. 2000). The large surface area of soils and the high  $[CO_2]$  contained within them lend a significant contribution to the  $\delta^{13}C$  of the atmosphere near the surface.

Respiration of plant roots and soil microbes releases  $CO_2$  with a particular  $\delta^{13}C$  and  $\delta^{18}O$  into the soil. The soil matrix through which  $CO_2$  molecules diffuse causes a change in the  $\delta^{13}C$  and  $\delta^{18}O$  relative to their source due to kinetic fractionation, estimated to be 4.4‰ for  $\delta^{13}C$  and 8.8‰ for  $\delta^{18}O$  (Cerling et al. 1991). Under steady state conditions,  $CO_2$  within the soil is isotopically enriched while gas leaving the soil surface has the same isotopic composition as the source emitting  $CO_2$  into the soil (Amundson et al. 1998).

Liquid water in soils has an effect on the respired  $\delta^{18}O$  value of  $CO_2$  in the soil.  $CO_2$  that is in contact with water exchanges oxygen atoms with water molecules. This causes the  $\delta^{18}O$  of

161 CO<sub>2</sub> to be influenced by the δ<sup>18</sup>O of the water. The degree of influence depends on a number of
162 factors including the amount of time the CO<sub>2</sub> is in contact with the water, temperature, and the
163 presence of catalyzing enzymes such as carbonic anhydrase (Tans 1998).

Net soil CO<sub>2</sub> efflux is determined by the mass balance equation modified from Ball (1999):

$$r = \frac{u_o(c_i - c_o)}{s} - E \tag{1}$$

where r is net soil CO<sub>2</sub> efflux ( $\mu mol\ CO_2\ m^{-2}\ s^{-1}$ ),  $u_o$  is flow rate out of the chamber ( $\mu mol\ s^{-1}$ ),  $c_i$  is the mole fraction of CO<sub>2</sub> entering the chamber ( $\mu mol\ mol^{-1}$ ),  $c_o$  is the mole fraction of CO<sub>2</sub> going out of the chamber ( $\mu mol\ mol^{-1}$ ), s is the surface area of soil being measured by the chamber ( $m^2$ ), and E is the efflux rate of water leaving the soil ( $\mu mol\ H_2O\ m^{-2}\ s^{-1}$ ). When there is a large amount of water evaporating from the soil, the E term can be a significant contribution to the mass flow of air exiting the chamber, effectively diluting the mass flow of CO<sub>2</sub> from the chamber.

The equation for the soil evaporative term is modified from Ball (1989):

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$$E = \frac{F(w_0 - w_i)}{Sm^2(1000 - w_i) \times 10^6}$$
 (2)

Where F is the mass flow rate in  $\mu$ mol s<sup>-1</sup> of gas leaving the chamber,  $w_o$  and  $w_i$  are the exiting and entering water vapor, respectively, in mmol H<sub>2</sub>O per mole of air.

A mass balance equation is used to determine the respired  $\delta^{13}C$  and  $\delta^{18}O$  based on the difference in inlet and outlet  $\delta$  values. The equation below is modified from a leaf chamber (Evans et al. 1986) to apply the equation to a dynamic open soil chamber:

$$\delta_{R} = \frac{c_o \delta_o - c_i \delta_i}{c_o - c_i} \tag{3}$$

where  $\delta_R$  is the isotopic value of CO<sub>2</sub> respired from the soil relative to the isotopic standards VPDB for  $\delta^{13}$ C and VSMOW for  $\delta^{18}$ O,  $\delta_o$  is the delta value of the chamber outlet and  $\delta_i$  is the delta value of the chamber inlet.

#### Methods

#### Chamber Design

The soil chamber used in this study is a dynamic flow-through chamber modified from Fang and Moncrieff (1996). The chamber was constructed from 3 mm polycarbonate and was a rectangular design with an internal volume of 2.65 L (Figure 1). The inlet and outlet are located on either side of the chamber with a metal mesh placed in front of both the inlet an outlet to help reduce pressure waves from crossing the chamber. A slowly turning three-bladed fan (18 RPM) was used in the top of the chamber above the soil gas inlet to aid in mixing. The chamber bottom was circular with a diameter of 142 mm and a surface area of 15.8 x 10<sup>-3</sup> m<sup>2</sup>. The bottom edge of the chamber protruded 30 mm from the lower surface and fit into a water-sealed metal soil collar that was driven into the soil or test column medium. The chamber was equipped with a thermocouple for measuring chamber headspace temperature, a port with an attached tube for connection to a differential pressure transducer, and a circular, perforated manifold placed over the bottom opening attached to an external tube for water delivery (watering experiments only).

#### Chamber operation

The flow rate through the chamber was controlled with a mass flow controller (*MFC*, FMA-A2408, Omega Engineering) connected to a diaphragm vacuum pump and attached to the

chamber outlet in order to draw gas through the chamber. In order to minimize pressure differentials induced by restriction of the chamber inlet, a compressed gas cylinder of medical grade air was attached to the chamber inlet and incoming flow was regulated with a mass flow controller in order to balance it with the rate that air was drawn from the chamber (Figure 1). Prior to all measurements, the bottom of the chamber was sealed with closed-cell foam and the chamber flow-rate was set with the outlet flow controller to the desired flow-through rate (between 0.2 and 1 L min<sup>-1</sup>, depending on the experiment). A differential pressure transducer (PX653, Omega Engineering) was connected to measure the pressure difference between the inside of the chamber and the ambient air. The flow rate from the air cylinder was then adjusted in order to bring the pressure differential to within  $\pm$  0.05 Pa, the resolution limit of the pressure transducer. After balancing the pressure of the chamber, the foam was removed from the bottom of the chamber and the chamber was placed on the collar for measurements.

A tee fitting (Figure 1) was placed at both the chamber inlet and outlet to allow subsampling by the TDL and an infra-red gas analyzer (IRGA, LI-840, Li-Cor Biosciences) for determination of chamber  $CO_2$  efflux,  $\delta^{13}C_R$  and  $\delta^{18}O_R$ . The tee for the outlet first entered the IRGA for  $[CO_2]$  analysis, then passed through a critical flow orifice (restricting flow to 200 mL min<sup>-1</sup>) and into the TDL for  $[CO_2]$ ,  $\delta^{13}C$ , and  $\delta^{18}O$  analysis before being exhausted by the vacuum pump. The sub-sample from the chamber's inlet passed directly through the critical flow orifice and to the TDL for the same analyses of air entering the soil chamber. The venting tee (Figure 1) is used to maintain the pressure of the soil chamber at atmospheric pressure.

Artificial test column

A test column was designed to produce a known CO<sub>2</sub> efflux rate with a known isotopic composition for testing the soil chamber (Figure 2). The cylindrical column was constructed of aluminum with a diameter of 1 m and height of 1.3 m. The bottom was sealed with sheet aluminum and the top had a perforated stainless steel grate (holes are 3.2 mm in diameter, 22.3 holes per cm<sup>2</sup>) fitted 10 cm from the top edge. The interior CO<sub>2</sub> delivery manifold of the test column was made from a 1.5 m length of copper tubing (1.3 mm ID) with small perforations approximately 60 mm apart. A similar manifold was constructed from 0.4 m of copper tubing, either end of which was connected to an IRGA (Li- 820, Li-Cor Biosciences) in a closed loop for sampling CO<sub>2</sub> mole fractions in the interior of the column. A slowly rotating mixer (12 RPM) was placed in the bottom of the column above the CO<sub>2</sub> delivery manifold to aid in homogenizing the interior air. An 80 mm layer of dry glass beads (3 mm diameter) was used as the substitute for soil, this was held up by a porous nylon fabric and placed on a perforated metal grate at the bottom of the glass beads in the test column.

Efflux from the test column was generated by creating a large CO<sub>2</sub> gradient between the interior of the column and ambient air, causing CO<sub>2</sub> to diffuse out the top of the column. CO<sub>2</sub> efflux rates from the test column were generated by maintaining a constant [CO<sub>2</sub>] inside the column; efflux was determined by measuring the amount of pure CO<sub>2</sub> gas that was needed to maintain the [CO<sub>2</sub>]. A mass flow controller (FMA-2402, Omega Engineering, 20 mL min<sup>-1</sup> maximum) was used to regulate the flow of CO<sub>2</sub> into the column interspace. A data logger (CR-1000, Campbell Scientific) was programmed with a feedback algorithm, based on measurements of the [CO<sub>2</sub>] in the test column,, regulated the delivery of CO<sub>2</sub> needed to maintain the target concentration. Commands were sent to the mass flow controller every second and flow data was recorded and averaged over 5 minute intervals to determine efflux from the test column.

To determine  $\delta^{13}C_R$  and  $\delta^{18}O_R$  from test column efflux, TDL measurements were made from air drawn from the interior of the test column. In order to bring a gas sample of suitable concentration for TDL sampling, mass flow controllers were used to mix test column gas with  $CO_2$  free air to produce a sample stream with a  $[CO_2]$  of ~400  $\mu$ mol mol<sup>-1</sup>. These values were assumed to be isotopically enriched due to kinetic fractionation and were converted to  $\delta_R$  values were by subtracting 4.4% for  $\delta^{13}C$  and 8.8% for  $\delta^{18}O$ , giving known values of  $\delta^{13}C_R = 39.0\%$   $\pm$  0.3% and  $\delta^{18}O_R = 9.7\%$   $\pm$  0.3%.

### Soil Chamber Operation

Prior to testing, a soil collar was placed in the test column, the test column was sealed and all of the  $CO_2$  was removed using a soda lime scrubber. Testing began by first bringing the interior air of the test column to a steady-state target  $[CO_2]$  as determined by the IRGA. The chamber was then placed on the collar for efflux measurement and the flow rate through the chamber was chosen as either 300 or 500 mL min<sup>-1</sup>. These rates were chosen to optimize the chamber headspace  $[CO_2]$  by maximizing the difference between  $c_0$  and  $c_i$  but remaining within the calibrated range of the TDL (between 300 and 650  $\mu$ mol mol<sup>-1</sup>). Chamber measurements of  $[CO_2]$  were made using both the TDL and IRGA to independently determine efflux rates for comparison of the TDL-based measurement to the traditional IRGA-based measurement. Since the IRGA only measured the chamber outlet, a predetermined value for  $[CO_2]$  from the medical air cylinder was used as the inlet value in IRGA based efflux calculations. Chamber measurements of the test column were conducted at multiple column  $CO_2$  efflux rates. The test column was allowed to equilibrate at each efflux rate for a minimum of 4 hours before

measurements were recorded, and chamber measurements were conducted for a minimum of 6 hours.

### TDL Absorption Spectroscopy Measurements

The *TDL* sampled both the inlet and the outlet of the soil chamber at a frequency of one measurement cycle every two minutes. Each cycle consisted of measurements of two calibration standards (high standard:  $[CO_2] = 558.94 \, \mu \text{mol mol}^{-1}$ ,  $\delta^{13}\text{C} = -30.52\%$ ,  $\delta^{18}\text{O} = 0.68\%$ ; low standard:  $[CO_2] = 339.89 \, \mu \text{mol mol}^{-1}$ ,  $\delta^{13}\text{C} = -30.60\%$ ,  $\delta^{18}\text{O} = -0.33\%$ ) followed by measurements of samples from the chamber inlet and outlet. A multiport manifold was used to direct flow from each inlet into the sample path of the *TDL* for a total of 30 seconds with the last 15 seconds averaged for each measurement. Determinations of mole fractions for  $^{12}\text{C}^{16}\text{O}_2$ ,  $^{13}\text{C}^{16}\text{O}_2$ , and  $^{12}\text{C}^{18}\text{O}^{16}\text{O}$  were corrected during post-processing by applying a linear correction to each measurement cycle derived from the difference between measured and actual values of the calibration standards (see Bowling et al. 2005). Corrected isotopologue values were converted into isotopic compositions and expressed relative to known standards (VPDB, Vienna Pee Dee Belemnite for  $\delta^{13}\text{C}$  and VSMOW, Vienna Standard Mean Ocean Water for  $\delta^{18}\text{O}$ ). For the  $[CO_2]$  values used in equations (1) and (3), measured isotopologues values were summed and a fraction for all other non-measured isotopologues was added (Barbour et al. 2007).

#### Soil Watering Experiment

The field tests were conducted using the piñon-juniper woodland located outside of our *TDL* facility at Los Alamos National Laboratory in northern New Mexico, USA. The soil chamber was configured in the same manner as for the test column. One day prior to

measurements, collars were placed in the soil to allow soil  $CO_2$  efflux to stabilize from disturbance from placement (Law et al. 1999). After adjusting chamber flow-rate and equalizing the chamber pressure with the atmosphere, the chamber was placed on the collar and sealed with water. Data for the chamber inlet and outlet  $[CO_2]$ ,  $\delta^{13}C$  and  $\delta^{18}O$  were collected every two minutes with the TDL, chamber outlet  $[CO_2]$  and water vapor were collected at 1Hz with the IRGA and logged with the data logger. The  $[CO_2]$  in the chamber headspace was allowed to stabilize and data collected for at least 30 minutes prior to water addition. After the initial stabilization and measurement period, a simulated 50 mm rain event was added, without removing the soil collar, through the watering manifold to evenly wet the soil. Water addition was done over approximately a 4 minute period to prevent any water from standing within the soil collar. Data was collected from the soil chamber before, during and after the watering event.

#### Results

Carbon dioxide efflux rates generated in the test column were calculated using [CO<sub>2</sub>] measurements from both the TDL and IRGA for comparison. Both methods yielded comparable data (Figure 3, linear regression  $R^2 = 0.99$ , p<0.0001). The TDL-chamber measurements of efflux rates from the column were in good agreement with the column efflux rates (Figure 4). The 1:1 line (shown) shows that across all efflux rates and for both the 300 and 500 mL min<sup>-1</sup> chamber flow-through rates there is considerable agreement between logger-based efflux measurements and TDL-based efflux measurements (Table 1). For both chamber flow-through rates, the chamber measurements of column  $CO_2$  effluxes were not significantly different from known values (p=0.54). There was a linear relationship across the data (slope = 0.95,  $R^2$ =0.94) for all data and for the 300 and 500 mL flow rates separately (slope = 0.68,  $R^2$ =0.93 and slope =

0.94 and  $R^2$ = 0.95 respectively). Both show no significant difference in measured efflux from test column efflux (p=0.35 and p=0.87 for the 300 and 500 mL min<sup>-1</sup> flow rates, respectively).

For all flow rates and efflux rates on the test column,  $\delta^{13}C_R$  and  $\delta^{18}O_R$  measurements from the chamber were not significantly different than the expected values (Table 1, Figure 5). Likewise, individual comparisons by flow rate and within  $\delta^{13}C_R$  and  $\delta^{18}O_R$  did not show any significant differences between expected values and measurements from the chamber (Table 1).

Field measurements showed an average efflux rate of  $0.3 \pm 0.05~\mu mol~CO_2~m^{-2}~s^{-1}$  for dry soils prior to watering (Table 2, Figure 6). Addition of a 50 mm rain event to the soil caused a 24-fold increase to  $7.2 \pm 0.5 \mu mol~m^{-2}~s^{-1}$ . Isotopic values of dry soil respiration had a value of  $\delta^{13}C_R = -20.6 \pm 3.0\%$  and  $\delta^{18}O_R = 80.3 \pm 7.7\%$ . The addition of water changed  $\delta^{13}C_R$  by -5.0% to -25.6  $\pm$  0.7% and  $\delta^{18}O_R$  by -55.0% to 25.3  $\pm$  1.2%. The addition of water increased the gravimetric water content of the dry soil (0 – 100 mm depth) by 5-fold, from an average of 2.8% to 14.2% and changed the  $\delta^{18}O_R$  from  $2.8 \pm 1.7\%$  to -8.3  $\pm$  1.8%.

## Discussion

Test Column

Soil [CO<sub>2</sub>] is elevated above atmospheric [CO<sub>2</sub>] by autotrophic respiration (roots) and heterotrophic respiration (microorganisms), creating a gradient that drives CO<sub>2</sub> diffusion from the soil. Steady-state CO<sub>2</sub> efflux is achieved when CO<sub>2</sub> is lost to the atmosphere at the same rate that it is introduced to the soil through respiration. We designed a test column to mimic CO<sub>2</sub> effluxes from a dry, coarse soil. The test column simulated this by regulating the [CO<sub>2</sub>] of the volume underneath the soil substrate: as CO<sub>2</sub> was lost from the system through surface efflux, an equivalent amount was added to the column to maintain stable [CO<sub>2</sub>] and by extension, a steady

state CO<sub>2</sub> efflux rate. The ability to precisely monitor the amount of CO<sub>2</sub> needed to maintain the internal [CO<sub>2</sub>] gives an accurate method for determining the efflux from the test column.

The soil chamber used in this study provided accurate measurements of soil  $CO_2$  efflux,  $\delta^{13}C_R$ , and  $\delta^{18}O_R$  (Figures 5 and 6). Since TDL absorbance spectroscopy is a new technology and has not been used in the past for determining soil chamber-based efflux measurements, we verified the accuracy of the  $CO_2$  efflux with simultaneous measurements with a previously tested IRGA. Both methods fall along the 1:1 line (Figure 3) and have comparable degrees of variation. Since the TDL was on a 30 second measurement cycle, there is a 30 second lag between measurements of the chamber inlet and outlet gases. Although this could be problematic if there were significant and rapid changes in inlet  $[CO_2]$ , however, the use of a compress gas cylinder avoids this problem by maintaining a constant isotope and concentration source. This problem can also be ameliorated with the use of a buffer volume to stabilize inlet gas  $CO_2$  fluctuations. Measurements of the inlet  $[CO_2]$  and isotopic composition by TDL showed very little variance (standard deviation = 0.18  $\mu$ mol mol<sup>-1</sup>) and the flux measurements from both instruments corresponded closely (Figure 3).

We verified the accuracy of soil efflux measurements with this chamber system by comparing chamber-based efflux measurements with effluxes generated by the test column. By using glass beads for the diffusive medium, we introduce no potential source of carbon to affect test column effluxes or isotopic values. Secondly, since the glass beads are very porous, they offer a very conservative test for chamber induced anomalies. The high porosity offers very little resistance to mass flow of CO<sub>2</sub> into or out of the beads, so small pressure artifacts from the chamber cause immediately detectible changes in CO<sub>2</sub> efflux.

Chamber measurements showed relatively good agreement with the column effluxes over a wide range of efflux rates at two chamber flow rates (Figure 4). For the chamber flow rate of 300 mL min<sup>-1</sup>, the data adhere to the 1:1 line very well at the lower efflux rates but tend to underestimate at the two highest flux rates. This may be a reason to use higher flow rates when CO<sub>2</sub> efflux is relatively high. Chamber headspace [CO<sub>2</sub>] increases proportionally with increasing efflux rates. The head space [CO<sub>2</sub>] can easily approach two or three times that of ambient with low chamber flows and high efflux rates. This affects the diffusion gradient of CO<sub>2</sub> to the surface inside the chamber, potentially reducing the efflux rate into the chamber. High test column (or soil respired) efflux rates also increase the amount of time needed for the [CO<sub>2</sub>] in the headspace to reach equilibrium. Additionally, though pressure of the chamber is equalized to that of the atmosphere prior to placing the chamber on the collar, long periods for stabilizing allow more time for pressure anomalies to develop that can cause errors in chamber measurements.

Measurements of  $\delta^{13}C_R$  and  $\delta^{18}O_R$  show that this chamber method is also valid for determining isotopic composition from soil respired  $CO_2$  (Figure 5). The difference between measured and actual  $\delta^{13}C_R$  and  $\delta^{18}O_R$  values are not statistically different from zero for all  $CO_2$  efflux rates. At higher efflux rates, measured values of  $\delta^{13}C_R$  tend to be more enriched than the known value; the average difference (Table 1) of +0.08‰ for all measurements becomes +0.28‰ after omitting the two measurements at the lowest column efflux rates. This holds true for  $\delta^{18}O$  measurements as well, while the average measured value is -0.08‰ from the test column value, omitting the same two measurements changes the mean difference to +0.26‰.

Several factors can cause the chamber measured values of  $\delta_R$  to be isotopically enriched. Since the inlet gas into the chamber is medical grade compressed air, its isotopic content is

similar to that of ambient air,  $\delta^{13}C = -8.46\%$  and  $\delta^{18}O = 28.1\%$ . The test column air was from an industrial source and therefore, the  $CO_2$  is depleted relative to the atmosphere by more than 30% for  $\delta^{13}C$  and 18% for  $\delta^{18}O$ . Due to the addition of pure  $CO_2$  as the source gas for efflux, minor pressure artifacts that suppress the surface efflux could bias measured values toward atmospheric levels.

The active mixer and baffles on either end of the chamber are intended to disrupt laminar flow and aid in maintaining a well mixed chamber environment; however there is a chance that inefficient mixing could create a boundary layer near the surface causing a bias towards inlet  $\delta_R$  values, especially at higher flow-through rates. Invasion of atmospheric  $CO_2$  into the interspace of the glass beads as well as into the inner volume of the test chamber would enrich the source for column-respired  $CO_2$ . We accounted for invasion by measuring the test column interspace  $\delta^{13}C$  and  $\delta^{18}O$  directly and correcting for the enrichment due to kinetic fractionation. These interspace values could be affected by a change in diffusion gradients when the chamber is placed on the column and would also be affected by mass movements of  $CO_2$  from temperature changes or pressure changes induced by the chamber.

The error seen in the two measurements at the lowest efflux rates (Figure 5) could be caused by changes of the test column  $CO_2$  due to diffusion of atmospheric air into the test column. Prior to measurements, the column was scrubbed of  $CO_2$  by sealing the top of the column and recirculating its air through a soda-lime scrubber. After this was completed, pure  $CO_2$  gas from an industrial source was immediately introduced and had  $\delta^{13}C = -41.3\%$  and  $\delta^{18}O = 3.8\%$ . The ambient  $CO_2$  in the room where the testing was performed had a  $\delta^{13}C$  value of approximately -9% and  $\delta^{18}O$  value of approximately 42%, both of which are more enriched than the  $CO_2$  source for the test column so diffusion into the test column would enrich the  $\delta$  values for

both isotopes. Since the first two chamber efflux rate measurements of the column (Figure 5, two lowest efflux rates) were the first measurements conducted after scrubbing  $CO_2$  from the column, the diffusion of ambient  $CO_2$  may not have reached equilibrium. The first two measurements (Figure 5) of  $\delta^{13}C_R$  (-40.0% and -39.8%) and  $\delta^{18}O_R$  (7.9% and 8.0% respectively) measured by the chamber were much closer to  $\delta$  values of the source  $CO_2$  and had a high standard deviation that could be explained by the isotopic composition inside of the test column changing toward the more enriched values of ambient  $CO_2$  during these measurements. Later measurements were conducted at least 3 days after scrubbing  $CO_2$  from the column and allowed sufficient time for the influence of ambient  $CO_2$  on the column to stabilize.

#### Water Addition Experiment

In the field, high temporal resolution sampling of soil  $CO_2$  efflux,  $\delta^{13}C_R$  and  $\delta^{18}O_R$  isotope values from the chamber captured dramatic shifts after the addition of water to a dry (Figure 6). Prior to water addition, soil efflux was less than 1  $\mu$ mol m<sup>-2</sup> s<sup>-1</sup>. This was consistent with field measurements conducted in a nearby site using a Li-Cor 6400-09 soil chamber and is typical for dry conditions during late spring in this region. Isotopic measurements of  $CO_2$  were highly variable during the pre-watering period. This variability is likely a result of both inherent spatial heterogeneity as well as a measurement artifact. The differential between chamber inlet and outlet  $[CO_2]$  when efflux rates were very low was small (<30  $\mu$ mol mol<sup>-1</sup>), which leads to poor precision in online estimates of  $\delta^{13}C$  and  $\delta^{18}O$  respired from the soil surface. This is due to the larger impact on  $\delta_R$  values resulting from errors in  $\delta_0$  and  $\delta_i$  measurements when there is a small difference in  $c_0$  and  $c_i$  in equation 5. For example, if the chamber  $c_0$  = 420  $\mu$ mol mol<sup>-1</sup> and  $c_i$  = 400  $\mu$ mol mol<sup>-1</sup>, a measurement error of 0.05% for both  $\delta_0$  and  $\delta_i$  changes the  $\delta_R$  value by

2‰. If the  $CO_2$  differential is raised to 50  $\mu$ mol mol<sup>-1</sup> ( $c_o$  = 450 and  $c_i$  = 400  $\mu$ mol mol<sup>-1</sup>), the same error changes  $\delta_R$  by 0.8‰.

The addition of a 50 mm watering event revealed a large shift in both efflux rate and isotopic composition. On average there was a 6.9 μmol m<sup>-2</sup> s<sup>-1</sup> increase in CO<sub>2</sub> efflux; an increase of nearly 24-fold. The initial increase in CO<sub>2</sub> efflux could be attributed to the displacement of CO<sub>2</sub> in the soil from the 792 mL of water that were added; however, we saw only one soil collar that exhibited a pulse of CO<sub>2</sub> before returning to a stable, elevated flux (Figure 6 panel A). Based on the displacement of 792 mL of soil gas with an estimated [CO<sub>2</sub>] of 2000 μmol mol<sup>-1</sup>, the increase in soil CO<sub>2</sub> efflux cannot be explained solely by displacement (Figure 7). All soil collar measurements showed a sustained increase in CO<sub>2</sub> efflux until measurements were terminated, at least 35 minutes after water addition.

The addition of water to the chamber also produced an average shift of -5.0% for  $\delta^{13}C_R$ . We do not know what caused the shift in  $\delta^{13}C_R$  but we speculate that is due to an increase in heterotrophic activity as well as transient diffusive effect due to non-steady state conditions (Moyes 2008, Risk and Kellman 2008). Since the soil at this site is very low in carbonates, we do not expect any contribution from carbonates to affect efflux  $\delta^{13}C$  values. There were several large *Juniperus monosperma* in the sampling site so there could have been some respiratory response from the root system; however, the *Juniperus* canopies are unlikely to have responded with increased photosynthesis because the water was over a small area and the response happened immediately after watering. Most likely, the addition of water initiated a respiratory response from heterotrophic organisms in the soil that were inactive under dry conditions, prompting a shift in the substrates used for decomposition and hence a shift in the isotopic composition of respired  $CO_2$  (Xu et al. 2004). Isotopic measurements from roots and leaves of

plants from the site (*Juniperus monospera*, *Bouteloua gracilis*, *Gutierrezia sarothrae*, *Poa fendleriana*) have  $\delta^{13}$ C values of approximately -22.3‰, similar to values measured by the chamber before watering (Figure 6 panel B). After watering, chamber  $\delta^{13}$ C measurements are consistent with bulk soil  $\delta^{13}$ C of -29‰, indicating a shift in the source CO<sub>2</sub> for respiration.

The benefit of using high frequency measurements is apparent here in that the measurement rate of one measurement every two minutes captures the rapid change in soil CO<sub>2</sub> efflux and isotopic composition after the pulse watering event (Figure 6). Sampling on a lower frequency time scale of hours or days would likely not capture the change seen here with sufficient resolution to determine the time after watering in which a response is detected and the magnitude of the changes at their maximums. It is conceivable that once-daily measurements would not detect the majority of the response evoked by short lived rain events, particularly in the arid ecosystems of the southwestern United States that are subject to short but intense pulse rain events. The usefulness of soil CO<sub>2</sub> efflux and isotope measurements is drastically increased by higher frequency measurement intervals.

The  $\delta^{18}O_R$  value dropped by -55‰ after water was added within the soil collar, from 80.3‰ to 25.3‰. This was expected since liquid water exchanges  $^{18}O$  atoms with  $CO_2$  and the water we applied had a  $\delta^{18}O$  of -10.8‰, which should impart a  $\delta^{18}O$  value of 22.5‰ onto soil  $CO_2$  in the vicinity of the water (Mook et al. 1974). Mass spectrometer analysis of water extracted from the soil after watering shows water in the top 0-20 mm of soil have approximately the same  $\delta^{18}O$  as the water that was used, with soil water becoming progressively enriched with depth. Prior to watering, extracted soil water values were +5‰ to -2‰, indicating that the  $\delta^{18}O$  of the soil water was enriched due to evaporation. A model was used to predict the  $\delta^{18}O_R$  of  $CO_2$  in isotopic equilibrium with the extracted soil water (Figure 8). For the dry soils,

the model predicts much lower  $\delta^{18}O_R$  values than what was seen with the soil chamber. However, nightly, ecosystem-scale Keeling plots generated from data collected with the TDL at this site gave intercepts between 54‰ and 68‰, closer to the soil chamber data. It is possible that the highly enriched  $\delta^{18}O$  of respired  $CO_2$  measured prior to watering results from a high ratio of invasion of soil "respiration" *per se* during dry conditions.

#### Conclusion

Our data show that the soil chamber- TDL system was capable of measuring soil efflux and isotopic composition effectively and with high frequency. When the soil chamber was used with a test column where efflux rate and isotopic composition were tightly controlled, chamber measurements closely matched the column efflux rate and had an average difference of -0.08‰ for  $\delta^{13}C_R$  of -0.08‰ for  $\delta^{18}O_R$ . We found no statistical difference between measured and test column values for both fluxes and isotopes. Our results confirm prior observations that careful regulation of pressure artifacts and consideration of flow rates relative to  $CO_2$  efflux rates is warranted. The chamber-TDL system also proved capable of high temporal resolution sampling of effluxes and isotope signals from transient responses to *in situ* watering events in a field setting.

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Table 1. Chamber measurements of  $CO_2$  efflux,  $\delta^{13}C_R$ , and  $\delta^{18}O_R$  (mean + SD) from a test column of dry glass beads, Known values for respired  $CO_2$  were  $\delta^{13}C = -39.0 \pm 0.3\%$  and  $\delta^{18}O_R = 9.7 \pm 0.3\%$ . Paired t-test at the 95% confidence level across all chamber flow rates and analyzed for each flow rate gives no significant difference in the chamber mean value and known value of  $\delta_R$ . All flow rates:  $\delta^{13}C_R = -38.9 \pm 0.6\%$  (p = 0.66) and  $\delta^{18}O_R = 9.6 \pm 1.1\%$  (p = 0.81). 300 mL min<sup>-1</sup>:  $\delta^{13}C_R = -39.3 \pm 0.6\%$  (p = 0.40),  $\delta^{18}O_R = 9.0 \pm 1.0\%$  (p = 0.21). 500 mL min<sup>-1</sup>:  $\delta^{13}C_R = -38.7 \pm 0.5\%$  (p = 0.13),  $\delta^{18}O_R = 10.1 \pm 0.9\%$  (p = 0.34)

Chamber flow rate (µmol s <sup>-1</sup> )	Chamber CO <sub>2</sub> efflux (µmol m <sup>2</sup> s <sup>-1</sup> )	S.D. of efflux	Column CO <sub>2</sub> efflux (\(\mu mol m^2 s^{-l}\)	Chamber δ <sup>13</sup> C <sub>R</sub> (‰)	$S.D.$ of $\delta^{13}C_R$	Difference from 39.0%	Chamber δ <sup>18</sup> O <sub>R</sub> (‰)	$S.D.$ of $\delta^{18}O_R$	Difference from 9.7%
300	1.17	0.04	0.94	-40.03	1.34	0.13	7.92	2.26	1.78
300	1.75	0.19	1.83	-39.77	1.60	-0.13	8.00	2.42	1.70
300	2.97	0.28	2.71	-38.43	1.19	-1.47	10.35	1.62	-0.65
300	3.24	0.23	3.86	-39.06	0.60	-0.84	9.39	0.92	0.31
300	3.61	0.27	4.59	-39.06	0.79	-0.84	9.38	1.17	0.32
500	2.60	0.08	2.62	-39.59	1.02	-0.31	8.49	1.34	1.21
500	3.29	0.31	3.35	-38.90	0.72	-1.00	9.60	1.58	0.10
500	4.87	0.27	4.15	-38.11	0.57	-1.79	11.35	0.92	-1.65
500	5.03	0.17	5.08	-38.69	0.48	-1.21	10.05	0.78	-0.35
500	5.41	0.40	5.82	-38.74	0.63	-1.16	9.81	1.05	-0.11
500	7.06	0.53	6.66	-38.13	0.52	-1.77	10.94	0.85	-1.24
500	7.11	0.22	7.51	-38.51	0.54	-1.39	10.17	0.78	-0.47

Table 2.  $CO_2$  efflux,  $\delta^{13}C_R$ , and  $\delta^{18}O_R$  (mean + SD) from a dry grassland, before and after addition of 50 mm of irrigation

								500
Watering	Collar #	Soil CO <sub>2</sub> Efflux (µmol m²s⁻¹)	S.D. of Efflux (µmol m²s⁻¹)	δ <sup>13</sup> C <sub>R</sub> (‰)	S.D. of δ <sup>13</sup> C <sub>R</sub> (%)	δ <sup>18</sup> O <sub>R</sub> (%)	S.D. of δ <sup>18</sup> O <sub>R</sub> (%)	SX/6 0-10 cm (%) I
	1	0.3	0.05	-22.9	2.36	70.4	4.82	602
	2	0.1	0.02	-23.0	4.51	82.9	10.01	3.6
Pre-	3	0.3	0.05	-19.3	3.12	70.7	9.73	2.0
water addition	4	0.2	0.06	-18.3	3.00	85.9	5.59	2.8
addition	5	0.7	0.06	-22.6	2.40	85.6	5.45	2.3
	6	0.2	0.06	-17.6	2.50	86.3	10.40	3.3
	1	4.2	0.2	-27.3	1.4	22.2	2.3	-
	2	3.1	0.3	-27.0	0.6	23.7	0.9	13.9
Post-	3	10.2	0.3	-24.6	0.5	26.5	1.5	11.7
water addition	4	5.9	1.2	-26.6	0.9	23.9	1.2	11.8
addition	5	9.8	0.1	-23.0	0.3	30.0	0.9	15.2
	6	10.1	0.8	-25.1	0.5	25.8	0.6	18.2

**Figure 1.** Dynamic soil chamber and gas sampling system using mass flow controllers connected to a *TDL* analysis system. Flow from a compressed cylinder of air is controlled by a MFC and a tee that acts as a pressure bypass. The air is sub-sampled by the *TDL* before and after it enters the chamber. A mass flow controller regulates the flow out of the chamber to the pump.

Figure 2. The constant-flux test column system maintains a set concentration of  $CO_2$  below the dry glass beads (soil substrate) in order to both generate and precisely measure stable  $CO_2$  fluxes through the substrate.

**Figure 3.** Comparison of two independent  $CO_2$  efflux measurements: calculated using the TDL measurements and an IRGA (LI-840). In both cases the chamber  $CO_2$  efflux rate ( $\mu mol\ m^{-2}s^{-1}$ ) was calculated based on the difference in  $CO_2$  concentration between the air entering and the air exiting the chamber (equation 1). A 1:1 line (dashed) is shown for comparison. Least means squared regression equation: y = 0.99x - 0.02,  $R^2 = 0.99$ .

**Figure 4.** Comparison of TDL-based chamber measurements of CO<sub>2</sub> efflux to known CO<sub>2</sub> efflux from the test column. The test column system produced known efflux rates through manipulation of headspace [CO<sub>2</sub>] below the porous medium on which the chamber rested. Flow-through rates of gas through chamber headspace were varied in order to maintain an adequate differential between sample and reference CO<sub>2</sub> concentrations; flow-through rates of 300 mL min<sup>-1</sup> (closed symbols) and 500 mL min<sup>-1</sup> (open symbols) are shown. A 1:1 line (dashed) is shown for comparison.

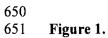
Figure 5. Tests of soil chamber measurements of A)  $\delta^{13}C_R$  and B)  $\delta^{18}O_R$  using constant isotopic sources across a range of  $CO_2$  efflux rates. Dashed lines represent actual isotopic  $(\delta_m)$  values found by sampling the test column headspace and correction for diffusive fractionation  $(\delta^{13}C_R = \delta_m - 4.4\%$  and  $\delta^{18}O_R = \delta_m - 8.8\%$ ). Through flow rates of 300 mL min<sup>-1</sup> (closed symbols) and 500 mL min<sup>-1</sup> (open symbols) are shown.

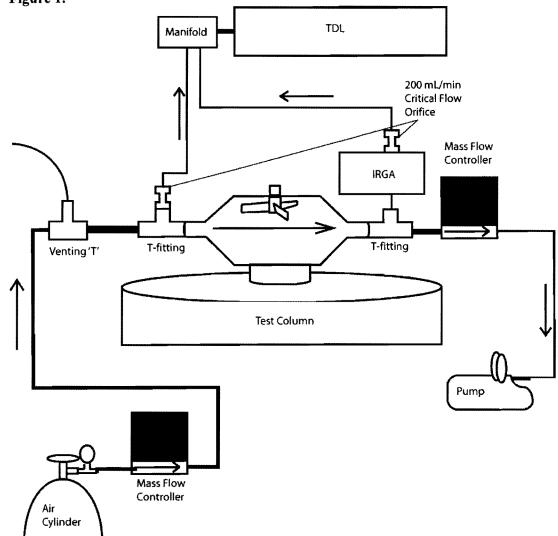
Figure 6. Field measurements of A) soil CO<sub>2</sub> efflux rates, B) respired  $\delta^{13}$ C and C)  $\delta^{18}$ O from six locations in a piñon-juniper woodland. A 50 mm rain event was simulated through application of 183 mL of water through a port within the chamber (time = 0 minutes). (Both  $\delta^{13}$ C and  $\delta^{18}$ O are highly variable prior to watering, resulting from the mixing model's sensitivity to the small differential between incoming and outgoing [CO<sub>2</sub>] concentration caused by the near-zero soil efflux rate. Water addition produces a precipitous increase in soil CO<sub>2</sub> efflux and a shift to more negative  $\delta^{13}$ C<sub>R</sub> values and the expected decline in  $\delta^{18}$ O<sub>R</sub> as the CO<sub>2</sub> picks up the signal of the water (-10.1‰).

Figure 7. Bold line shows contribution to CO<sub>2</sub> efflux that could occur from displacing soil gas during the water addition. Gray lines show chamber CO<sub>2</sub> efflux rates for comparison. Displacement equivalent to 792 mL of soil gas (from water volume) with 1000 μmol mol<sup>-1</sup> [CO<sub>2</sub>]

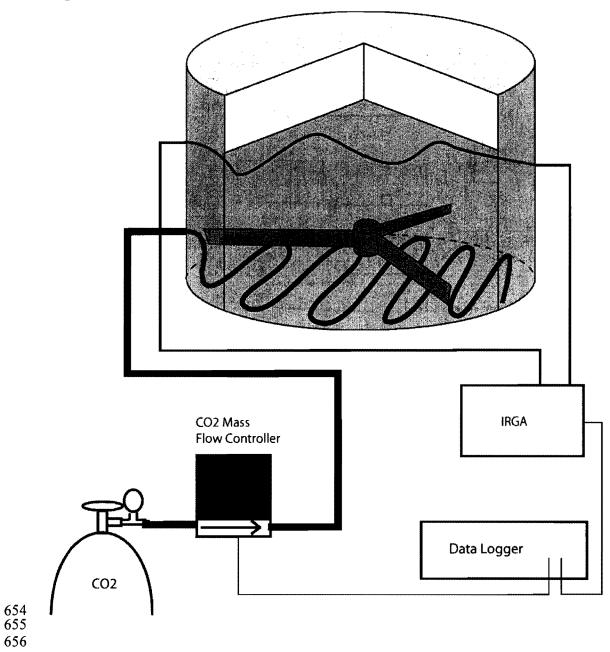
is equivalent to 25  $\mu$ mol of CO<sub>2</sub> which is the area under the bold curve.

Figure 8. A) Modeled δ<sup>18</sup>O of soil CO<sub>2</sub> before (Δ) and after (Δ) the addition of water. B)
 Measured gravimetric water content collected beside the chambers before (•) and under the chamber after (ο) the addition of water.

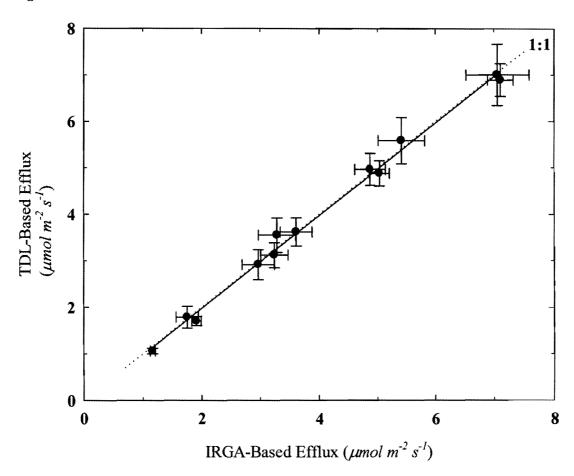




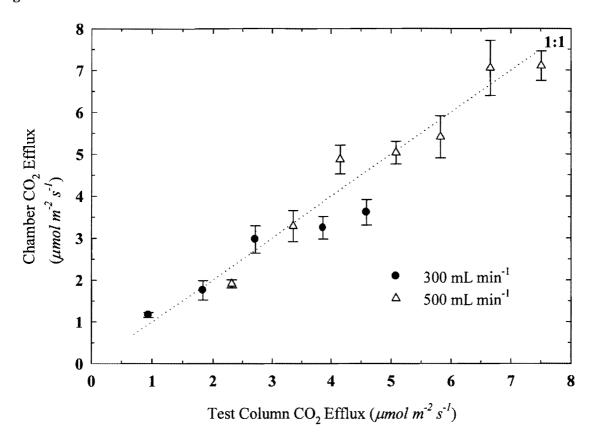
## 653 Figure 2.



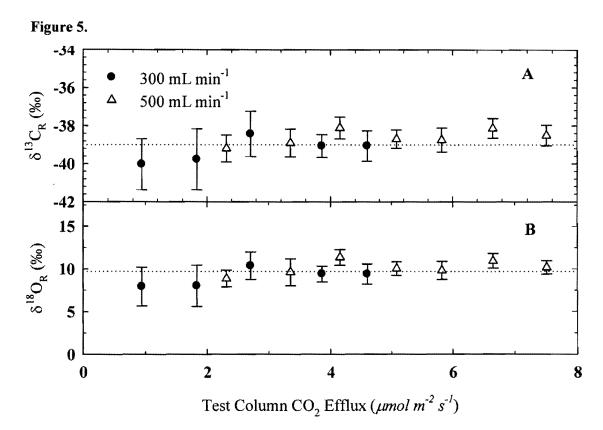
**Figure 3.** 



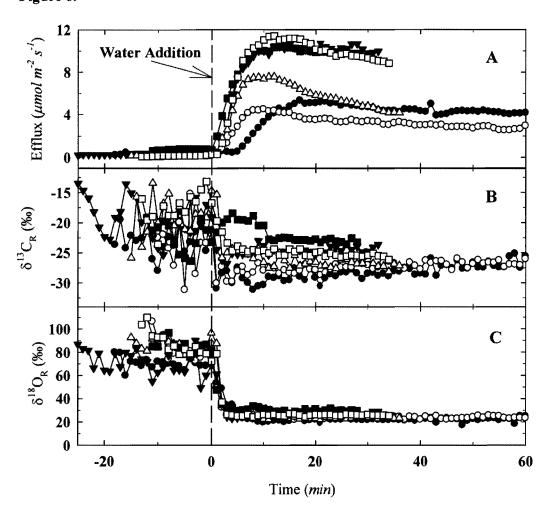
**Figure 4.** 



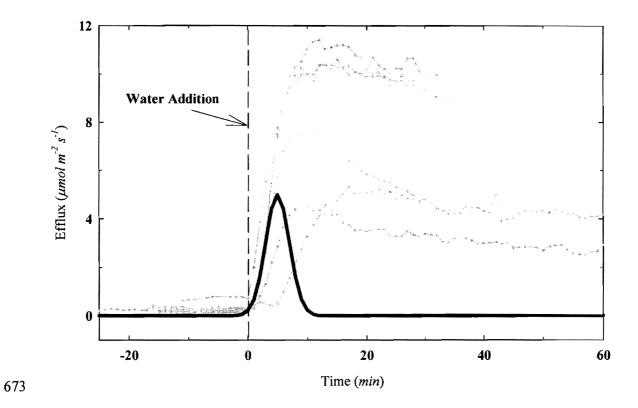




**Figure 6.** 



# **Figure 7.**



**Figure 8.** 

