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# Pulse-Echo Ultrasonic Inspection System for In-Situ Nondestructive Inspection of Space Shuttle RCC Heat Shields

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### Pulse-Echo Ultrasonic Inspection System for In-Situ Nondestructive Inspection of Space Shuttle RCC Heat Shields

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#### Abstract

The reinforced carbon-carbon (RCC) heat shield components on the Space Shuttle's wings must withstand harsh atmospheric reentry environments where the wing leading edge can reach temperatures of 3.000°F. Potential damage includes impact damage, micro cracks, oxidation in the silicon carbide-to-carbon-carbon layers, and interlaminar disbonds. Since accumulated damage in the thick, carbon-carbon and silicon-carbide layers of the heat shields can lead to catastrophic failure of the Shuttle's heat protection system, it was essential for NASA to institute an accurate health monitoring program. NASA's goal was to obtain turnkey inspection systems that could certify the integrity of the Shuttle heat shields prior to each mission. Because of the possibility of damaging the heat shields during removal, the NDI devices must be deployed without removing the leading edge panels from the wing. Recently, NASA selected a multi-method approach for inspecting the wing leading edge which includes eddy current, thermography, and ultrasonics. The complementary superposition of these three inspection techniques produces a rigorous Orbiter certification process that can reliably detect the array of flaws expected in the Shuttle's heat shields. Sandia Labs produced an in-situ ultrasonic inspection method while NASA Langley developed the eddy current and thermographic techniques. An extensive validation process, including blind inspections monitored by NASA officials, demonstrated the ability of these inspection systems to meet the accuracy, sensitivity, and reliability This report presents the ultrasonic NDI development process and the final hardware requirements. configuration. The work included the use of flight hardware and scrap heat shield panels to discover and overcome the obstacles associated with damage detection in the RCC material. Optimum combinations of custom ultrasonic probes and data analyses were merged with the inspection procedures needed to properly survey the heat shield panels. System features were introduced to minimize the potential for human factors errors in identifying and locating the flaws. The in-situ NDI team completed the transfer of this technology to NASA and USA employees so that they can complete "Return-to-Flight" certification inspections on all Shuttle Orbiters prior to each launch.

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### Pulse-Echo Ultrasonic Inspection System for In-Situ Nondestructive Inspection of Space Shuttle RCC Heat Shields

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## Pulse-Echo Ultrasonic Inspection System for In-Situ Nondestructive Inspection of Space Shuttle RCC Heat Shields

Configuration Information on: Technique, Hardware, Software, Design, and Performance Testing for Certification of UT Inspection System

Information for NASA Report: NASA RCC NDE Test Report KSC-5600-7412





#### 1.0 RCC In-Situ NDI Program Background

After the loss of OV-102 during STS-117, the Columbia Accident Investigation Board (CAIB) was formed to investigate the accident and make recommendations to increase system safety prior to return to flight (RTF). One of these recommendations was R3.3-1: *Develop and implement a comprehensive inspection plan to determine the structural integrity of all Reinforced Carbon-Carbon system components. This inspection plan should take advantage of advanced non-destructive inspection technology.* An integrated team of participants from NASA-JSC, NASA-Langley, Sandia National Laboratories, United Space Alliance (USA), Oceaneering Space Systems (OSS) and Boeing has been working since 2003 to develop and demonstrate nondestructive inspection (NDI) systems capable of performing inspection of Reinforced Carbon-Carbon (RCC) leading edges on-wing in the Orbiter Processing Facility (OPF). This report details the system development and validation of the ultrasonic testing (UT) system for detecting flaws in RCC on the Shuttle Orbiter wing leading edge panels and mating Tee Seals.

#### NASA Response to the *Columbia* Accident Investigation Board

NASA must Continue to Manage the Space Shuttle as a Development Vehicle:

- Be cognizant of the risks of using the Shuttle in an operational mission, and manage accordingly.
- Perform more testing on Space Shuttle hardware rather than relying on computer-based analysis and extrapolated experience to reduce risk Inspection plan for recertification of Shuttle for Flights.
- Address aging issues through the Space Shuttle Service Life Extension, including midlife re-certification.
- Collaborate with high-risk industries such as nuclear power & aviation to identify and incorporate best practices.

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### Leading Edge Shuttle System – Reinforced Carbon-Carbon

**LESS/RCC Overview - Basic Requirements** 

- Thermal Protection (3200°F)
- Aerodynamic Shape
- Load Distribution
- Impact Resistance

Health Monitoring Objective: Develop a comprehensive NDE program for the in-situ health monitoring of Orbiter RCC components.



### **Space Shuttle Orbiter RCC Components**





#### Areas To Be Inspected on Wing Leading Edge



# **RCC Component Configurations**



Nose Cap Assembly(78"x66"x41", 544 lbs)



POINT 3

Wing Leading Edge Assembly 22 panel/seal sets on each wing (31"x42"x35, 42 lbs– typical for each)



ET Arrowhead Assembly (17"x14"x0.25", 2 lbs)

#### **Composition of RCC Heat Shield Panels**

RCC is composed of carbon substrate, SiC conversion layer and sealant



#### **Deployment of NDI Devices in Orbiter Processing Facility**



Nose section

Lower RCC (from OPF floor or platform floor)



**Upper RCC with** large overhang from work platform

#### Shuttle In-Situ NDI Program

Repetitive flight certification effort -



Dark streaks showing projectile impact area

Production NDI: UT, EC, X-ray, tap test In situ NDI: consisted of visual and tactile inspections

Goal: deploy a variety of NDI methods to detect RCC degradation that may compromise LESS performance

RCC Damage Scenarios - impact damage, loss of coating integrity on the outer surfaces, carbon cracks/fracture, delaminations, disbonds at Si-C to C-C interface, SiC craze cracks & subsequent subsurface oxidation produces mass loss & reduction in strength.



SiC Coating Loss Mechanism via **Convective Mass Loss** 

#### LESS Thermal Data: WLE Temperature Profile



### **RCC Panel Inspection Requirements**

- NDE Feature Detection Criteria
  - Delaminations, Laminar Voids and Local Mass Loss
    - Detect delaminations, laminar voids & local mass loss in C-C using IR thermography.
    - Detection sensitivity at SiC/C-C interface on OML side: 1/8" diameter with 0.005" thickness.
    - Detection sensitivity at 0.12" depth from OML: 3/8" diameter with 0.005" thickness.
    - Everywhere else in C-C, interpolate/extrapolate this criteria.
      - $D = 2.8 \text{ x} \text{ d} 0.042^{\circ}$ , where D = diameter in inches, d = depth from OML in inches.
  - Cracks
    - IR Thermography is not required to detect OML cracks, but any cracks (excluding craze cracks) detected by IR thermography shall be reported.
    - Detection Sensitivity: A crack with 1/2" length and 0.030" depth in C-C (or 0.060" surface depth from OML for nominal coating thickness of 0.030") and complete separation between crack faces.

### **RCC Panel Inspection Requirements**

- NDE Feature Detection Criteria
  - Suspect area is identified by visual inspections, IR inspections, or evidence of an impact/damage event.
  - Criteria for further evaluation of suspect area using in-situ NDE.
    - Delaminations and impact damage
      - Detection sensitivity: 1/4" dia. Use ultrasonic hand scanning.
    - Coating
      - SiC coating thickness measurement range: 0.005" thru 0.060". Spot size ≤ 1/4" dia. Use eddy current.
    - Cracks
      - Detection sensitivity: Same as for screening inspection. Use eddy current.
  - C-scan is not mandatory but handheld mapping is required.
    - Cover the entire suspect area at the suspect location.

#### Flaw Detection Requirements for Depths Beyond the Initial Si-C to C-C Interface





#### **Ultrasonic Attenuation vs. Flexural Strength**

### **RCC Mass Loss Relationships**

- Mass loss of RCC substrate is directly related to temperature – especially over 2500°F
  - Radiant areas (lugs, ribs, flanges) lose mass <u>uniformly</u> through the thickness and have a 0.10 psf loss limit
  - Convective areas (OML) loose mass preferentially at the coating interface and have a 0.03 psf mass loss limit
- "Invisible" RCC defects are caused by subsurface mass loss in the <u>convective</u> regions
  - This is the key item for flight-to-flight NDE inspections



SiC Coating Loss Mechanism via Convective Mass Loss

RCC CONVECTIVE MASS LOSS RATE COMPARISON





Interface Block Diagram of Shuttle Inspection in Orbiter Processing Facility

#### 2.0 Description of Pulse-Echo Ultrasonic NDI Technique

<u>Pulse-Echo Ultrasonic</u> (P-E UT) inspections, short bursts of high frequency sound waves are introduced into materials for the detection of surface and subsurface flaws in the material. The sound waves travel through the material with some attendant loss of energy (attenuation) and are reflected at interfaces. The reflected beam is displayed and then analyzed to define the presence and location of flaws. Complete reflection, partial reflection, scattering, or other detectable effect on the ultrasonic waves can be used as the basis of flaw detection. In addition to wave reflection, other variations in the wave that can be monitored include: time of transit through the test piece, attenuation, and features of the spectral response. The types of RCC flaws detectable by the ultrasonic method include cracks, delaminations, voids, local mass loss, global mass loss, and impact damage.

<u>Wide Area Inspections Aided by C-Scan Mode</u> - It is sometimes difficult to clearly identify flaws using ultrasonic A-Scan signals alone. Small porosity pockets commonly found in composites, coupled with signal fluctuations caused by material nonuniformities can create signal interpretation difficulties. Significant improvements in disbond and delamination detection can be achieved by taking the A-Scan signals and transforming them into a single C-Scan image of the part being inspected. C-scans are two-dimensional images (area maps) produced by digitizing the point-by-point signal variations of an interrogating sensor while it is scanned over a surface. A computer converts the point-by-point data into a color representation and displays it at the appropriate point in an image. Specific "gates" can be set within the data acquisition software to focus on response signals from particular regions within the structure. C-

Scan area views provide the inspector with easier-to-use and more reliable data with which to recognize flaw patterns. This format provides a quantitative display of signal amplitudes or time-of-flight data obtained over an area. The X-Y position of flaws can be mapped and time-of-flight data can be converted and displayed by image processing-equipment to provide an indication of flaw depth.

Amplitude and Time-of-Flight Data - Once the digitized A-scan waveforms are recorded during the ultrasonic pulse-echo inspection of the RCC material, the amplitude and time of flight peak signals can be displayed as a C-scan image and analyzed to determine if a flaw exists within the material. The reflected beam from the back surface of the RCC material can be used as the starting point for this analysis. The pseudo colored C-scan image can reveal several variations within the RCC material and will be displayed in the pseudo colored C-scan image. Any large amplitude change (>12db) in the C-scan image shall be reported. Depending upon the geometry of a flaw and location within the RCC material, the amplitude might not appear very different than that of the surrounding back surface. This is where the time of flight C-scan image can show a slight shift in the pseudo color of the back surface. By analyzing both pseudo colored images (amplitude and time of flight) and the A-scan waveforms, the inspector can determine if a flaw exists within the RCC material. The time of flight C-scan image also shows thickness variations or the taper along the edges of the RCC panel.

### **Pulse-Echo Ultrasonic NDI**



Schematic of Pulse-Echo Ultrasonic Inspection and Reflection of UT Waves at Assorted Interfaces

Transducer is both transmitter & receiver to keep footprint small



Composite Doubler A-Scan Signal Trace – Gate 1: delam & porosity Gate 2: bond interface Gate 3: alum. back wall echo

Gates allow users to focus on specific phenomenon

UT Niche – penetration for deep flaw detection

### Pulse-Echo Ultrasonic NDI – C-scan Approach



- 1", 1/2", & 1/4" Disbonds characteristics of the sum
- Gate settings, appropriate gain, & data acquisition mode are key elements
- Dynamic display of data is best for flaw detection
- Optimum probe (signal strength) is critical in highly attenuative RCC material



**C-Scan Approach** 

Color coded image produced from relative

total of signals received

### Pulse-Echo Ultrasonic NDI – C-Scan Approach



Manual Scanner



**Automated Scanner** 

**Inspection Impediments and Considerations** 

- Thickness of structure and energy level of excitation
- Attenuation & near-surface signal clarity
- Optimizing S/N ratios; flaw size & depth sensitivity

#### Pulse-Echo Ultrasonic Set-Up

- Smallest footprint for best coverage and navigation of curved or uneven surfaces
- Probe variables studied:
  - Ø 1", 2", 3", 5" focus Ø 0.5", 1", 1.5" dia.
  - Ø 1- 2.25 MHz freq.
  - Ø flat & focused beam
- Probe optimization Harisonic 1 MHz, 1" dia., 2" focus (RCC mat'l passes 1.5 MHz)
- Probe offset water column of 1.1" to 1.2"



#### Pulse-Echo Ultrasonic NDI – Flaw Detection Applicability

Technique	Physical Contact Required	Detect Deep Flaws	Delams	Large Voids	Significant Porosity	Local Mass Loss	Impact Damage	Coating Msmts.	Fasteners/ Tubular Voids
Contact P-E Ultrasonics	X	X	Х	х	X	X	x		Voids

Goal: detect structural anomalies at all depths within RCC

NDE Requirements Document:

Sensitivity issue (ref. arc jet disks)

Pulse-Echo Ultrasonics (P-E UT) will detect structural anomalies with at least 0.25" X 0.25" planform dimensions (minimum aspect ratio of 1.0), at any depth within the RCC material at or below the outer surface interface between the Si-C and C-C, and within 0.5" of the panel edge at the interface with the T-seal. Inspections will be performed using a frequency of 1 MHz. Structural variations that manifest themselves as attenuation of an interrogating ultrasonic wave will be assessed in accordance with existing guidance for allowable attenuation levels in a Through-Transmission Ultrasonic (TTU) inspection. Attenuation levels produced in TTU will be related to equivalent attenuation levels in P-E UT so that the same resolution and sensitivity can be achieved. Attenuation levels will be obtained by reference to adjacent locations of the same thickness. Structural anomalies detected as per the above discussion include: cracks, delaminations, and voids/porosity/mass loss. They do not include coating thickness measurements.

### **Ultrasonic Method Trade Study**

- Feasibility study for in-situ RCC ultrasonic inspection performed May to November 2003
  - Assessed multiple ultrasonic composite inspection options using RCC test specimens: pulse-echo UT, resonance, mechanical impedance analysis, low frequency bond test
  - Research performed by Sandia Labs with support from Lockheed-Martin, General Electric Corp. Research, SAIC, Boeing, Krautkramer, and Staveley
  - Assessed scanner systems based on following criteria: wide area inspection, automated X-Y coverage, portability, established I/O (data acquisition & reduction software), lab and field technical support, rapid accommodation of customization needs
  - Results presented at RCC NDE downselect TIM November 2003
- Decision to proceed with UT for in-situ inspection received Dec. 2003
  - UltraSpec scanner system with 1 MHz, 1" dia., 2" spherical focus transducer selected for thru-thickness flaw detection

### **Timeline and Decision Tree for Ultrasonic Method**



### **UltraSpec Pulse-Echo Scanning - Equipment Summary**

- Probe Assembly
  - Sensor
  - Sensor Housing
  - Gimbal Assembly
  - Z-Axis Assembly
- Scanner Assembly
- Support Equipment
  - I/O Box
  - Water Management
- Operator Workstation

### SAIC Ultraspec-MP with LPS-100 Manual Scanner



Technical Specifications

Physical Characteristics

- Scanner height: 2.00 inches
- Scanner width: 6.0 inches
- Scanner length: 12.0 inches
- Scanner weight: 7.0 pounds



- Encoder resolution:
- Positional accuracy: + or 0.005 inches
- Repeatability:
- Stroke:
- 910 pulses/inch
  - + or 0.005 inches

6.0 inches X-axis, 12 inches Y-axis



### Pulse-Echo Ultrasonic NDI System

- Lightweight (6 lb.), manual scanner •
- Local flaw detection assessment in areas identified by thermography
- Can scan up to 12" X 6" area

Advantage: easier & more rapid to deploy

Limitation: restricted to small area scans



### **Pulse-Echo UT System Components**

- LPS-100 manual scanner, Data Acquisition System (DAS), laptop
- NASA LaRC linear spring probe mount; probe housing, weeper couplant

LPS-100 Scanner, Tripod positioning

DAS and Laptop



UT Transducer and Housing



LaRC Linear Spring

### UT/EC Manual Scanner (LPS-100)

- Integrates with existing SAIC scanning station
- Designed for 12" X 6" max scan area
- Weight with UT probe is 7 lbs.



#### **UltraSpect-MP**



Dimensions

Laptop – Sony VAIO, Model PCG-8N1L 13.9" x 11.8" x 2.0" (Closed) 13.9" x 11.8" x 13.1" (Open @ 90 deg) DAS Unit – 16.5" x 12.6" x 7.4" Utility Box (Vacuum) – 20.5" x 16.5" X 16.5" Manual Scanner – 20" x 15" x 3.5"

### **UltraSpect-MP Electrical System**

#### Output Voltage Levels: Maximum Values

- Ø Encoder Cable 5 V
- Ø UT Pulser 400 V, maximum duration 1000 nsec
- Ø EC Coil Drive 20 V

#### **Output Amperage Levels:**

- Ø Encoder output to the scanner encoders is 5VDC and is fused at 1.25 amps, however, the actual encoders only draw about 35 milli amps
- Ø UT Pulser (peak amperage) UT pulser charges a capacitor of 0.3 microfarad. It is then discharged to generate a pulse. At the maximum pulser voltage of 400 V, and a given transducer impedance (typical value 50 ohms), the current draw (according to Ohm's law) is 400/50 = 8 amps for the duration of the pulse. If a square wave pulser is used, this duration can be varied up to 1000 nanoseconds.

ØUT Pulser (RMS amperage) -

RMS current = peak current \* SQRT (T1/T2) where T1 is the pulse on time (width) and T2 is the off time, which is related to scan speed and grid size.

Apply Sandia Labs inspection set-up: Transducer impedance = 75 ohms Pulser voltage/duration = 300 V, 700 nanoseconds Scan speed 6 in/sec Scan index = 0.020" (estimate) Max current = 300 v/75 ohms = 4 amps T1 = 700 nsec =  $700 \times 10^{-9} \text{ sec}$ T2 = 1/((6 in/sec) / 0.020" index) = 1/300 pts/sec = 0.003333 secRMS current =  $4 \times \text{SQRT}[700 \times 10^{-9})/(0.003333] = 58 \text{ milli amps}$ 

\* For the safety of the operator, never change a UT probe with the pulser running. Always close the UT calibration application before changing probes since it is possible to generate a spark between the connector and probe if the connect/disconnect is made while the pulser is running.

### **UltraSpect Software Description**

Analysis package is the UltraSpect System. The data acquisition software is used to set up the the process for collecting the information from the different inspection methodologies. The analysis package allows the acquired data to be analyzed on another computer without tying up the Control Laptop computer.

The set-up features for data acquisition software does the following:

Ultrasound Pick the type of scanner Set up the scanner parameters (x & y scan length, grid size, scan speed) Ultrasonic parameters (i.e. number of transducers, frequency, time base, number of gates, and other UT parameters) Display data acquisition results while scanning. **Eddy Current** Pick the type of scanner Set up the scanner parameters (x & y scan length, grid size, scan speed) Eddy Current parameters (i.e. number of probes, frequency, time base, etc) Display data acquisition results while scanning. Data analysis for UT This allows the data acquired to be viewed in various formats (A-scan, B-scan, C-scan). Specific areas can be zoomed in to view features, gate position and amplitude can be moved to create additional views Data Analysis for ET This allows the data acquired to be viewed in various formats (Lissaious pattern, strip chart, color C-scan) Certain parameters may be changed to create new images without rescanning the part

A list of the software items follows:

UltraSpect-MP system with Ultrasonic and Eddy Current Capability

Each scanner system includes the following software: Ultrasonic Data Acquisition Acquisition software Ultrasonic Data Analysis software. Eddy Current Data Acquisition software Eddy Current Data Analysis Software

Microsoft Windows XP Operating System Microsoft Office XP

Additional Ultrasonic Data Analysis software and Eddy Current Data Analysis software was purchased (2<sup>nd</sup> seat) to allow the acquired data to be analyzed on another computer without tying up the Control Laptop computer.

The procedures for the use of the software is included in the training/operating manuals.

The latest version of software is Version 6.12.2

### **UT Sensor Description**

- Manufacturer: GE Inspection Technologies / Krautkramer Benchmark Series Immersion Transducer
  1 MHz / 1 inch diameter
  2 inch spherical focus
- Transducer Part Number : 389-058-620
- Special Descriptor for Custom NASA Probe: SPFPA-IS8B1NOKNURL2"UHF

### **Equipment List (For One UT Scanner Unit)**

LPS-100 Scanner & DAS – SAIC UT Transducer – GE/Krautkramer Weeper System & Transducer Housing – Test Tech Linear Spring - NASA

<u>Recommended Spares</u>: transducers, scanner cable bundles, transducer housing, transducer articulation (yoke, linear spring), weeper system with recovery

#### **UT/EC LPS-100 Manual Scanner Details**



Y-axis thumb wheel and lead screw for precise indexing



### **Pulse-Echo UT System Components**

- Component list:
  - Operator workstation  $\rightarrow$  Laptop and DAS software
  - I/O Controller  $\rightarrow$  Data acquisition module
  - Sensor housing → Weeper body/transducer with yoke & spring



### **UT and EC Scanner System Hook-Up**



#### Manual Scanner with Linear Spring and Probe Attached







#### UT Sensor Housing, Gimbal Assembly, and Z-Axis Tracking Hardware



Assembled View of Weeper Body/Transducer with Yoke & Spring

#### UT Sensor Housing, Gimbal Assembly, & Z-Axis Hardware

Individual View of Weeper Body and End Cap with Yoke & Spring





Individual View of Weeper Body, Ultrasonic Transducer, Connectors and Coax Cable

### Schematic of Assembled Ultrasonic Sensor System

#### Weeper Body and Ultrasonic Transducer



### View of Assembled Ultrasonic Sensor System

Weeper Body, Yoke, Ultrasonic Transducer, Connectors, and Coax Cable



### UT/EC Sensor Surface Following with Z-Axis Linear Spring





#### UT Sensor Housing, Gimbal Assembly, & Z-Axis Hardware

**Component Weights** 

- 1. Ultrasonic Probe 178.9 g (6.3 oz.)
- Probe Housing 56.8 g (2 oz.) 2.
- 3. Linear Spring – 147.7 g (5.2 oz.)

Linear Spring Force

- Left Spring 1.12 lbs.
- **Right Spring 1.12 lbs.**
- Both Springs Engaged 2.24 lbs. •

Pressure Loads – see section on shear and normal force assessment





Membrane

#### Water Management Equipment Description

Weeper Water Supply and Return (not shown: reservoir top and base for secondary/safety water containment)

Housing End Cap



# **Top Level Drawing of Pulse-Echo Scanner System**



# Pulse-Echo Scanner System – Top Assembly List of Materials

Scanner Tripod Assembly List of Materials						
Qty	Part No.	Description	Note	Item No.		
				50		
2		Nut, Hex, Plain, Steel, .190 (#10)-32UNF-2B		49		
				48		
4		Screw, 82 Csnk Head, Steel, .190 (# 10) - 32UNF - 2A X 1.50" Lg.		47		
4		Screw, 82 Csnk Head, Steel, .190 (# 10) - 32UNF - 2A X .625" Lg.		46		
6		Screw, Socket Head, Steel, .190 (# 10) - 32UNF - 2A X .75" Lg.		45		
2		Screw, Socket Head, Steel, .190 (# 10) - 32UNF - 2A X .625" Lg.		44		
				43		
				42		
8		Screw, Pan Head, Steel, .164 (# 8) - 32UNC - 2A X .625" Lg.		41		
4		Screw, Socket Head, Steel, .164 (# 8) - 32UNC - 2A X .50" Lg.		40		
				39		
				38		
8		Screw, Socket Head, Steel, .138 (# 6) - 32UNC - 2A X .50" Lg.		37		
4		Screw, Socket Head, Steel, .138 (# 6) - 32UNC - 2A X .375" Lg.		36		
				35		
8		Washer, Lock, Nom. I.D. # 10 (.190")		34		
12		Washer, Lock, Nom. I.D. # 8 (.164")		33		
12		Washer, Lock, Nom. I.D. # 6 (.138")		32		
				31		
1	30701AM067	BNC to BNC 12" lg. RG174 (50 ohm) Coaxial Cable	6	30		
1	30701AM063	BNC/RA Adapter	6	29		
1	30701AM62	UHF/BNC Adapter	6	28		
1	30701AM100	Weeper Captive Water Column Kit	6	27		
1	PSC-3057	Bogen Tripod, Head, Model 3057		26		
1	PSC-3058	Bogen Tripod, Model 3058		25		
				24		
1	ALRB02	Lemo Right Angle Plug/BNC Receptacle	5	23		
1	LPS100	SAIC Ultra Spec Manual Scanner System	4	22		
1	1245825	Eddy Current Probe Assembly RCC	3	21		
1	1245938	Ultrasonic Probe Assembly RCC	3	20		
				19		
3	3032T64	Eyebolt, Stainless Steel, W/ Nut, 1/4"-20 thd.	2	18		
2	92373A115	Spring Pin, Steel, .062" dia X 1.00" Lg.	2	17		
2	90079A245	Knurled Head Pilot (Dog Point) Thumb Screw 1/4"-20 x 1.00" Lg.	2	16		
				15		
				14		
				13		
1	NASA-3-WC	Probe Holder Assembly		12		
				11		
3	NASA-10-SC	Tripod Leg Tiedown Strap		10		
2	NASA-9-SC	Linear Slide Stop Plate		9		
2	NASA-8-SC	Linear Slide Positioning Stop		8		
1	NASA-7-SC	Modified Tripod Head Mounting Plate		7		
1	NASA-6-SC	Modified Linear Slide Mount		6		
1	NASA-5-SC	Scanner Mounting Plate		5		
1	NASA-4-SC	Tripod Tiedown Collar		4		
1	NASA-3-SC	Probe Holder Extended Attachment Bracket		3		
1	NASA-2-SC	Probe Holder Standard Attachment Bracket		2		
2	NASA-1-SC	Scanner Spring Lock Shim		1		

# Design Drawing Set for Pulse-Echo Ultrasonic System

SNL Drawings for NASA Scanner Assembly					
Drawing Title	Drawing No.				
Captive Water Column	NASA-1-WC				
Modified Membrane	NASA-2-WC				
Probe Holder Assembly	NASA-3-WC				
Scanner Spring Lock Shim	NASA-1-SC				
Probe Holder Standard Attachment Bracket	NASA-2-SC				
Probe Holder Extended Attachment Bracket	NASA-3-SC				
Tripod Tiedown Collar	NASA-4-SC				
Scanner Mounting Plate	NASA-5-SC				
Modified Linear Slide Mount	NASA-6-SC				
Modified Tripod Head Mounting Plate	NASA-7-SC				
Linear Slide Positioning Stop	NASA-8-SC				
Linear Slide Stop Plate	NASA-9-SC				
Tripod Leg Tiedown Strap	NASA-10-SC				
Scanner Tripod Assembly	NASA-1				
Maximum Height Tripod Deployment Layout	NASA-2				
Minimum Height Tripod Deployment Layout	NASA-3				

# **UT Transducer Housing**

Drawing of Delrin body, for proper probe offset from inspection surface, and water coupling




# **UT Transducer Housing**

# UT Transducer Housing – Water Column Membrane



### UT Sensor Housing, Gimbal Assembly, & Z-Axis Hardware

Assembled View of Weeper Body/Transducer with Yoke & Spring





#### Normal Bracket for Connecting Probe Housing to Scanner Arm

#### **Reach Extension Bracket for Connecting Probe Housing to Scanner Arm**



3.0 Tripod Positioning Mechanism for Manual Ultrasonic Scanner

## **Tripod Positioning Mechanism Design Parameters**



\* Assumes PIC boards are not in place & are not available for supporting tripod legs

### Integration of Manual Scanner with Tripod Positioning





### Modified COTS Linear Slide Mount for Scanner Base – Placed on Top of Tripod



Y-Arm Rotational Spring Locking Shim (Prevents Rotation of Y-Arm)



### Mounting Plate for Placing Scanner on Tripod Positioning Mechanism

NOTES:

- 1. MATERIAL: ALUMINUM, 6061-T6, .250" THK.
- 2. TOLERANCES NOT SHOWN ARE AS FOLLOWS: .XX" =  $\pm$  .03" AND .XXX" =  $\pm$  .005" .



#### Adapter Plate for Mounting Linear Slide on Tripod



1. PART TO BE MODIFIED IS A BOGEN ADAPTER PLATE PART NO. 3297.





#### Locking Plates for Holding Linear Slide Position

Safety Stop Plate for Retaining Linear Slide on Tripod



### **Connection of Manual Scanner to Positioning Mechanisms**

X-rail feet will be connected to scanner positioning mechanism surface scans



Lower plate & suction cups retained for upper

Lower plate & suction cups removed for connection to external positioning mechanisms

## Integration of Manual Scanner with Positioning Mechanisms





Integration of Manual Scanner with Tripod Positioning

Tripod Configuration and Scanner Reach for <u>Maximum</u> <u>Underwing Height</u> Inspections of 56"

Integration of Manual Scanner with Tripod Positioning





### Manual Scanner and UT Probe Configuration

4.0 Scanner Deployment in Orbiter Processing Facility

## **Concept Of Operations on Wing Leading Edge**

- Portable step-up stands (supplied by KSC) will be used as needed to reach upper WLE surfaces
- Rail cart (shown below) is first option for positioning all NDI devices





## **RCC** Panel Layout with Respect to OPF Floor

Three Scanner Positioning Options for Inspections



## Three Types of UT/EC Scanner Deployment

- 1. Connection to OSS positioning mechanism
- 2. Connection to tripod positioner
- 3. Resting on top of RCC panel



Option 2



Option 1



Option 3

### Scanner Deployment in Orbiter Processing Facility



Gantry Positioning Mechanism

Tripod with Linear Slide

Upper Surface Scan



Scanner Deployment in Orbiter Processing Facility Option 1: Connection to Rail Cart Positioning Mechanism





Scanner Deployment Option 1: Connection to Rail Cart Positioning Mechanism Connection of Manual Scanner to Rail Cart Arm

### Scanner Deployment in Orbiter Processing Facility



### **Option 2: Scanner Deployed on Tripod Positioning Mechanism**



#### **Tripod Positioning Mechanism**



51

# Manual Scan of RCC Upper Surface



# Manual Scan of RCC Apex Region



### Manual Scan of RCC Lower Surface



# **Manual Scanner Tripod Tiedown Options**

Either the center-column collar fixture or the leg straps can be used to secure the tripod to the floor in the OPF inspection area



## **Tripod Tie-Down Collar**

- · Mounts to center column of tripod positioning mechanism and is connected to OPF floor
- · Prevents unintentional movement or tipping of scanner system when deployed on LE RCC panels



### **Tripod Tie-Down Strap**

- · Mounts to each leg of tripod positioning mechanism and is connected to OPF floor
- · Prevents unintentional movement or tipping of scanner system when deployed on LE RCC panels



#### **Tripod Positioning Mechanism – Floor Tiedown Fixtures**



Straps (2000 lb. Nylon) Attached to each Tripod Leg



Restraint Collar Attached to Tripod Center Column

#### Inspecting Upper Surface - Scanner Resting on Top of RCC Panel



Option 3







Pulse-Echo UT – Scanner Deployment & Data Acquisition

## **Class 1, Div 2 Compliance Status**

• Class 1 Div 2 compliant Flash Thermography equipment enclosures being evaluated by OSS.



A larger enclosed box is placed over the Rack mounted components and purge gas is maintained at positive pressure throughout the enclosure.



Investigating commercially available class 1 Div 2 enclosures. Requires repackaging of Equipment.



5.0 Performance Assessment of Pulse-Echo Ultrasonic Inspection System

#### Validation Plan for UT System

Complete inspections on all RCC test specimens using PE-UT system hardware

#### Sample Specimens Include:

- 1. Boeing disks with arc jet exposure
- 2. 0.25" th. RCC central section
- 3. 0.44" th. RCC edge section
- 4. 0.25" th., 2" X 6" Boeing coupon
- 5. 8L flight hardware (Bill's Box)
- 6. Columbia panel with flaws of different aspect ratios
- 7. Slotted specimens (sloping, straight, & corner slots)
- 8. NASA impact panels
- 9. Coupons from 9L RCC panel with engineered flaws
- 10. 11L RCC panel with engineered flaws

Pulse-Echo Ultrasonic Inspection of Boeing Disks (Arc Jet Specimen Set)







**Backside Inspection** 





## Arc Jet Disk Inspection with P-E Ultrasonics

**Frontside Flaw Detection - Serial Numbers in Back** 



**Backside Flaw Detection - Serial Numbers in Front** 



Waveform Comparisons – UT PE Signals from Flawed and Good Areas of ARC JET Specimen #01-24





RCC Flight Hardware – 0.24" Th. Panel with Coating



1 MHz Pulse-Echo UT Flaw detection obtained with weeper coupling





Gate 1 - Amplitude



### RCC Flight Hardware – 0.24" Th. Panel with Coating

# Sample P- E Ultrasonic Signals

### Acquired from 1MHz Probe on NASA 0.24" Specimen

Longitudinal wave velocity in RCC is ~ 0.1 inches/microsecond so the back wall reflection is seen at 5 microseconds for movement back and forth through the 0.25" specimen





# Validation Standards S03-48 and S03-49



### Validation Results, Standard S03-48



# Validation Results, Standard S03-49







Amplitude



Time of Flight

Sample Scan Images

### Validation Results, Standards S03-51 and S03-53



### Validation Results, Standard S03-51 and S03-53



# RCC Flight Hardware – 0.44" Th. Panel with Coating



RCC Flight Hardware – 0.44" Th. Panel with Coating



### **RCC Panel Recovered from Columbia Orbiter**







Flaws with different aspect ratios were engineered into panel

# **Columbia Panel with Flaws of Different Aspect Ratios**

Flaw detection in the presence of varying/high attenuation



Gate 2 Time of Flight

# **Columbia Panel with Flaws of Different Aspect Ratios**



# Phase 1 Specimen #03-63 with Corner Slots





### Phase 1 Specimen #03-54 with Side Slots and FBH (back surface)



# **Inspection of NASA Impact Panels**





# NASA Impact Panel R1-117-14 (R1-47-14)

### Lowest impact velocity of 1470 ft/s with no visible impact damage



Gate 2 Time of Flight

Gate 1 Amplitude

**Pulse-Echo UT** 

# NASA Impact Panel T8015-1













90 degree impact at 2054 fps

Gate 2 ToF

### NASA Impact Panel T8015-1 - UT PE Images & Waveforms



# NASA Impact Panel T8015-3

#### Impact velocity of 1717 ft/s with no visible impact damage



## NASA Impact Panel 8015-4



## NASA Impact Panel 146-2



Note: The ultrasonic signal can be affected by water seeping into the edge of the delamination area.

# NASA Impact Panel 146-2


# NASA Impact Panel 284-20



Photo of Impact Surface





**Pulse-Echo UT** 

45 degree impact at 2230 fps – visible damage on backside only

Gate 2 Time of Flight

### NASA Impact Panel 20L-23





Pulse-Echo UT

Back Surface



Gate 2 Time of Flight

90 degree impact at 2077 fps – no visible damage on front; small cracks visible on back side /



### Impact Test - OV105 Panel 16R

Photo of Crack at Apex



Thermography Image After panel was Impacted with Ablator Projectile



### Ultrasonic Pulse Echo C-scan of OV105 Panel 16R



## NDI Image of "Argonne" Specimen

Supplied by Sam Russell with suspected "worm holes" in 0.25" th. plate



Pulse-Echo Ultrasonic Scan of 0.25" th. Flight Hardware RCC Panel



Gate 1 interaction for near-surface delaminations

Pulse-Echo UT Inspection of "Bill's Box" NASA RCC Panel



Pulse-Echo UT Inspection of "Bill's Box" NASA RCC Panel





Gate 2 Time of Flight

Flaw Profile

### Pulse-Echo UT Inspection of "Bill's Box" NASA RCC Panel



### Pulse-Echo UT System Results Using Manual Scanning



### Pulse-Echo UT System Results Using Manual Scanning



Flaw Image from Manual Scan

### Pulse-Echo UT System Results Using Manual Scanning

2" X 6" X 0.25" th. Specimen 03-58 with Sloped Slots



### Pulse-Echo UT System Results Using Manual Scanning

2" X 6" X 0.25" th. Specimen 03-58 with Sloped Slots



### **RCC Panel 9L Validation Test Series**





#### Validation Results, Phase 2 Specimen 9L – Lower 1 (Q)

Validation Results, Phase 2 Specimen 9L – Lower 1 (Q)

6.00



Time of flight 3

Time of flight 4



#### Validation Results, Phase 2 Specimen 9L – Lower 2 (P)

Validation Results, Phase 2 Specimen 9L - Lower 2 (P)





#### Validation Results, Phase 2 Specimen 9L – Lower 4 (R)

Transition Region with Thickness Tapering from 0.233" to 0.340"

#### Validation Results, Phase 2 Specimen 9L – Lower 4 (R)



## Validation Results, Phase 2 Specimen 9L – Lower 4 (R)





#### Validation Results, Phase 2 Specimen 9L – Upper 2 (B)

Validation Results, Phase 2 Specimen 9L - Upper 2 (B)



Time of Flight 1



#### Validation Results, Phase 2 Specimen 9L – Upper 3 (A)

-

Time of Flight 3

Flaws not found



#### Validation Results, Phase 2 Specimen 9L – Upper 4 (D)

Validation Results, Phase 2 Specimen 9L – Upper 4 (D)



Time of Flight 4

Time of Flight 3

	Dete	ction of 1	/8" Diam	eter Flaw	s in RCC	9L Speci	mens			
Specimen	Flaw l	dentificati	on and Fla	aw Depth f	rom Front	Surface (	inches)	Detect Pulse-	tion by Echo UT	
	0.200 (+)	0.178	0.120	0.080	0.070	0.050	0.040 (-)	Yes	No	
		10							V	
9L-Lower 1 (Q)		A-2			C-2			-	X	
9L-Lower 1 (Q)			D-1		0-2				X	
9L-Lower 1 (Q)	E-2								X	
9L-Lower 2 (P)	A-2								Х	
9L-Lower 2 (P)				C-2			İ		Х	
9L-Lower 2 (P)			D-1						Х	1/8
9L-Lower 2 (P)	E-2								Х	de
9L-Lower 4 (R)	A-1								Х	
9L-Lower 4 (R)						C-5		Х		
9L-Lower 4 (R)		D-1						Х		
9L-Lower 4 (R)			F-5						Х	
9L-Upper 2 (B)	A-2								х	
9L-Upper 2 (B)				C-2					Х	
9L-Upper 2 (B)			D-1						Х	
9L-Upper 2 (B)	E-2							Х		
9L-Upper 3 (A)		A-2							х	
9L-Upper 3 (A)					C-2				Х	
9L-Upper 3 (A)			D-1					Х		
9L-Upper 3 (A)	E-2								Х	
9L-Upper 4 (D)		A-2							х	
9L-Upper 4 (D)					C-2				Х	
9L-Upper 4 (D)			D-1						Х	
9L-Upper 4 (D)	E-2								Х	

#### Flaw Detection Summary for 1/8" Dia. Flaws in 9L Specimens

#### 1/8" dia. flaw detection = 16.8%

#### Flaw Detection Summary for 1/4" Dia. Flaws in 9L Specimens

	Detection of 1/4" Diameter Flaws in RCC 9L Specimens												
Specimen	Flaw I	dentificati	ion and Fla	aw Depth f	rom Front	Surface (i	inches)	Detect Pulse-E	tion by Echo UT				
	0.200 (+)	0.178	0.120	0.080	0.070	0.050	0.040 (-)	Yes	No				
9L-Lower 1 (Q)			B-3					Х					
9L-Lower 1 (Q)					C-1			Х					
9L-Lower 1 (Q)						D-3		Х					
9L-Lower 1 (Q)		E-1						Х					
9L-Lower 2 (P)			B-3					X					
9L-Lower 2 (P)				C-1				X					
9L-Lower 2 (P)	<b>F</b> 4				D-3			Х	V	1/4" c			
9L-Lower 2 (P)	E-1								X	dotoo			
OL Lower 4 (P)	۸.E							×		detec			
9L-Lower 4 (R)	A-5		D 2					×					
9L-LOWER 4 (R)			D-3				C-3	×					
9L-Lower 4 (R)			D-3				00	X					
9L-Lower 4 (R)			F-1					X					
9L-Lower 4 (R)			F-1	1				X					
9L-Upper 2 (B)			B-3					Х					
9L-Upper 2 (B)				C-1				Х					
9L-Upper 2 (B)					D-3			Х					
9L-Upper 2 (B)	E-1							Х					
9L-Upper 3 (A)			B-3					Х					
9L-Upper 3 (A)				C-1				Х					
9L-Upper 3 (A)					D-3			Х					
9L-Upper 3 (A)		E-1						Х					
9L-Upper 4 (D)			B-3			ļ		Х					
9L-Upper 4 (D)	ļ			C-1		ļ		Х					
9L-Upper 4 (D)					D-3			Х					
9L-Upper 4 (D)	E-1								Х				

1/4" dia. flaw detection = 92%

	Dete	ction of 3	3/8" Diam	eter Flaw	s in RCC	9L Speci	mens		
Specimen	Flaw lo	dentificati	on and Fla	aw Depth f	rom Front	Surface (i	inches)	Detect Pulse-E	ion by icho UT
	0.200 (+)	0.178	0.120	0.080	0.070	0.050	0.040 (-)	Yes	No
9L-Lower 1 (Q)		A-1	5.4					X	
9L-Lower 1 (Q)			B-1			0.0		X	
9L-Lower 1 (Q)						C-3	5.0	X	
9L-Lower 1 (Q)							E-3	X	
9L-Lower 2 (P)	A-1							х	
9L-Lower 2 (P)			B-1					Х	
9L-Lower 2 (P)					C-3			Х	
9L-Lower 2 (P)						E-3		Х	
			Da					V	
9L-Lower 4 (R)			B-3				0.4		
9L-LOWER 4 (R)			DE				0-1	$\hat{\mathbf{v}}$	
9L-Lower 4 (R)			D-5 E 5					Ň	
9L-LOWER 4 (R)			E-3					×	
3L-LOWEI 4 (IX)			1-5					^	
9L-Upper 2 (B)	A-1							Х	
9L-Upper 2 (B)			B-1					Х	
9L-Upper 2 (B)				C-3				Х	
9L-Upper 2 (B)						E-3		Х	
		A 4						V	
9L-Upper 3 (A)		A-1	D 1						
OL Upper 3 (A)			D-1		<u> </u>				
9L-Upper 3 (A)					0-3	F-3		× ×	
9L-Upper 4 (D)		A-1						х	
9L-Upper 4 (D)			B-1					X	
9L-Upper 4 (D)				C-3				Х	
9L-Upper 4 (D)	1				E-3			Х	

### Flaw Detection Summary for 3/8" Dia. Flaws in 9L Specimens

# 3/8" dia. flaw detection = 100%

### Flaw Detection Summary for 1/2" Dia. Flaws in 9L Specimens

	Dete	ction of <sup>r</sup>	1/2" Diam	eter Flaw	s in RCC	9L Spec	imens		
Specimen	Flaw lo	dentificati	on and Fla	aw Depth f	rom Front	Surface (	inches)	Detect Pulse-E	ion by cho UT
	0.200 (+)	0.178	0.120	0.080	0.070	0.050	0.040 (-)	Yes	No
9L-Lower 1 (Q)		A-3						х	
9L-Lower 1 (Q)			B-2					X	
9L-Lower 1 (Q)						D-2		Х	
9L-Lower 2 (P)	A-3							х	
9L-Lower 2 (P)			B-2					X	
9L-Lower 2 (P)					D-2			Х	
OL Lower 4 (P)	A 2							v	
9L-Lower 4 (R)	A-3			B_1				×	
9L-Lower 4 (R)		E-3						X	
	4.0							X	
9L-Upper 2 (B)	A-3							X	
9L-Upper 2 (B) 9L-Upper 2 (B)			B-2		D-2			X	
9L-Upper 3 (A)	A-3							Х	
9L-Upper 3 (A)			B-2					Х	
9L-Upper 3 (A)					D-2			Х	
9L-Upper 4 (D)	A-3							х	
9L-Upper 4 (D)			B-2					X	
9L-Upper 4 (D)					D-2			Х	

1/2" dia. flaw detection = 100%



Probability of Detection Curve for Pulse-Echo UT Flaw Detection in Panel 9L – NDI Reference Standard Specimens

Validation Results, Phase 2 Specimen 9L - 3 Pt. Bend



3 Pt. Bend Specimens 1 (T), 2 (U), 3 (V), 4 (W), 5 (F), 6 (G), 7(H)

Specimens 1-4 from Lower Surface; 5-7 from Upper Surface

### Validation Results, Phase 2 Specimen 9L – 3 Pt. Bend UT Through Transmission Characterization



Crack / Delamination Mean 63.7751 dB Total Area: 1.2000 Sq In

Crack / Delamination Mean 60.9639 dB Total Area: 1.3536 Sq In Crack / Delamination Mean 53.0924 dB Total Area: 0.4608 Sq In

#### Spec. #1 MWM EC Results at 5.0 MHz Amplitude 1 Time of Flight 1 Amplitude 2 Time of Flight 2 Specimen #1 Spec. #2 MWM EC Results at 5.0 MHz Spec. #1 (side view showing crack)

### Validation Results, Phase 2 Specimen 9L – 3 Pt. Bend

#### Eddy Current Inspection Results for Comparison to P-E Ultrasonics Testing

Spec. #1 UltraSpect EC Results at 2.6 MHz



Spec. #2 UltraSpect EC Results at 2.6 MHz

Spec. #1 MWM EC Results at 5.0 MHz



Spec. #2 MWM EC Results at 5.0 MHz





### Validation Results, Phase 2 Specimen 9L – 3 Pt. Bend

#### Eddy Current Inspection Results for Comparison to P-E Ultrasonics Testing

Spec. #3 UltraSpect EC Results at 2.6 MHz



Spec. #4 UltraSpect EC Results at 2.6 MHz



Spec. #3 MWM EC Results at 5.0 MHz



Spec. #4 MWM EC Results at 5.0 MHz



### Validation Results, Phase 2 Specimen 9L – 3 Pt. Bend



#### Eddy Current Inspection Results for Comparison to P-E Ultrasonics Testing



Spec. #6 UltraSpect EC Results at 2.6 MHz



Spec. #7 UltraSpect EC Results at 2.6 MHz



Spec. #5 MWM EC Results at 2.5 MHz



Spec. #6 MWM EC Results at 5.0 MHz



Spec. #7 MWM EC Results at 5.0 MHz



### Use of UT Signal Database to Assess Structural Integrity

Comparison of Current UT Signature with UT History

Comparison of signal from Boeing 03-24 specimen when gain is set to:

1) gain used in NASA Upper 8L specimen



Gain used for Boeing 03-24 Specimen



Gain used for NASA Upper 8L Specimen (indicates that attenuation in pucks is higher than in 8L specimen)

# Validation Testing with RCC Panels 11L & 12L

Objectives of Validation Testing on Retired, Orbiter RCC Panels 11L & 12L

The objectives of this test program are:

- To validate the functionality of the Ultraspec Ultrasonic data acquisition system with LPS 100 manual scanner by performing blind in situ inspection of a full scale RCC Orbiter Wing leading edge (WLE) Panel and Tee Seal (Panel 11L and Tee Seal 12L) installed on a test stand to represent actual installed hardware on the Orbiter.
- To validate the ability of each system to detect artificially induced flaws (such as flat bottom holes) in undeclared locations within four test zones machined into the inner mold line (IML) of Panel 11L ranging from 0.040 to 0.190 inches in depth and from 0.125 to 0.5 inches in diameter
- To validate the ability of each system to detect artificially induced flaws on the IML and web junction of Tee Seal 12L
- To validate the ability of each system to accurately inspect hardware in a configuration that encompasses curvature and thickness variations representative of a RCC Panel (upper, lower, apex and thickness transition areas) and a RCC Tee Seal (Tee section, vent holes and non-parallel surfaces)
- To validate that the inspection processes are capable of meeting the applicable requirements of relevant Boeing MT specifications (MT0501-510 for UT) as witnessed by a Boeing Level 3 NDE engineer.
- To quantify the range of detection capability of each system on a relevant hardware configuration per Boeing and USA Level 3 NDE data assessment

### Validation Testing with RCC Panel 11L and 12L – Ref. TPS #KF0520168 Final Results and Grading from

Ultrasonic Pulse-Echo Validation Tests for Inspection of Shuttle RCC Material Test Articles: Orbiter Leading Edge Panel 11L and Tee Seal 12L

#### Full Scale Mock-up of Wing Leading Edge at OSS



Panel 11L

Panel 12L T-Seal



#### Wing Leading Edge RCC T-Seal

#### Wing Leading Edge RCC T-Seal WLE Gap Seal Geometry Schematic Refer to Geometric Data on the Following Page H H-Upr H-S Wing Reference Xw110 Reference Water Line (RWL) Plane Xw120 (WRP) T-Lug D (4 PL) H-L Note: Left seal shown, right side is a mirror image. LLwr STS-107 LESS/RCC Data 12 of 36 REFERENCE ONLY

RCC Panel 11L – Seven Zones (4 val., 3 ref.) RCC T Seal 12L – Three Zones (Z1 – Z3)



RCC Panel 11L – Seven Zones (4 val., 3 ref.) RCC T Seal 12L – Three Zones (Z1 – Z3)



Flaw Zone Layouts on Panel 11L



- Each region was scanned in two sections:
- (a) designation is for upper portion of region
- (b) designation is for lower portion of region

Note that scan (a) and scan (b) are <u>NOT</u> related so the X-Y scales on the two plots <u>CANNOT</u> be used together for flaw placement from one window to the next; they have similar but slightly different scan windows

### Reference and Validation Zones Inside Panel 11L

0.250" Thick Area									
FBH Ø	Rem	aining Mat Thickness	erial						
	0.040	0.115	0.190						
1/8	Х	Х	X						
1/4	Х	X	X						
3/8	Х	Х	Х						
1/2	Х	<b>x x</b>							
0.365	5" Thick 8	Transitior	n Area						
FBH Ø	Rem	aining Mat Thickness	erial						
	0.040	0.182	0.325						
1/8	X	X	X						
1/4	Х	Х	X						
3/8	Х	X	X						
1/2	Х	X	X						



LOWER RCC SURFACE

### Flaw Regions Included in Test



# 11L Reference Zone 1 (11L-R1)





Gate 2 Amplitude (a)

#### 11L Reference Zone 1 (11L-R1)



= flaw not detected #6, (1/8" dia.) was not detected in Zone 11L-R1





	Flaw Detection Summa	ry for Panel 11L Uppe	er Surface Reference Zone 1
--	----------------------	-----------------------	-----------------------------

	Zone 11L-R1											
	Drilled FBH		Laser Mea	asurements		FBH Detected by NDE						
Reference Hole #	FBH Ø @ Hole Depth	Ø	Remaining Material Thickness	Thickness Near Hole	Actual Hole Depth	ET	MWM	UT PE				
1	3/8 @ 0.040	0.381	0.222	0.251	0.029	N/A	N/A	D				
2	1/2 @ 0.040	0.509	0.220	0.249	0.029	N/A	N/A	D				
3	3/8 @ 0.115	0.383	0.138	0.247	0.109	D	D	D				
4	1/8 @ 0.115	0.128	0.130	0.246	0.116	U	D	D				
5	3/8 @ 0.190	0.381	0.057	0.246	0.189	D	D	D				
6	1/8 @ 0.190	0.132	0.058	0.249	0.191	D	D	U				
7	1/2 @ 0.115	0.512	0.140	0.249	0.109	D	D	D				
8	1/4@ 0.040	0.241	0.215	0.250	0.035	N/A	N/A	D				
9	3/8 @ 0.115	0.384	0.136	0.250	0.114	D	D	D				
10	3/8 @ 0.190	0.384	0.061	0.251	0.190	D	D	D				
11	1/2 @ 0.040	0.507	0.212	0.250	0.038	N/A	N/A	D				
12	1/4 @ 0.115	0.235	0.130	0.250	0.120	D	D	D				
13	1/4 @ 0.190	0.236	0.057	0.250	0.193	D	D	D				
14	3/8 @ 0.040	0.380	0.213	0.251	0.038	N/A	N/A	D				

# 11L Reference Zone 2 (11L-R2) - Apex





Gate 4 Amp dB (b)



Gate 3 Amp dB (a)

11L Reference Zone 2 (11L-R2) - Apex



Flaw Profile

= flaw not detected #3 (1/8") was not detected in Zone 11L-R2



Gate 4 Amp dB (a)

### 11L Reference Zone 2 (11L-R2) - Apex



#### Flaw Detection Summary for Panel 11L Apex Surface Reference Zone 2

	Zone 11L-R2										
Zones	Drilled FBH		Laser Mea		FBH Detected by NDE						
Referenc e Hole #	FBH Ø @ Hole Depth	ø	Remaining Material Thickness	Thickness Near Hole	Actual Hole Depth	ET	MWM	UT PE			
1	3/8 @ 0.040	0.378	0.221	0.258	0.037	N/A	N/A	D			
2	1/2 @ 0.040	0.501	0.225	0.254	0.029	N/A	N/A	А			
3	1/8 @ 0.115	0.129	0.148	0.259	0.111	U	А	U			
4	1/8 @ 0.190	0.131	0.093	0.252	0.159	D	D	D			
5	3/8 @ 0.115	0.382	0.142	0.252	0.110	D	D	D			
6	1/4 @ 0.115	0.244	0.137	0.248	0.111	D	D	D			
7	3/8 @ 0.190	0.383	0.072	0.254	0.182	D	D	D			
8	1/4 @ 0.040	0.242	0.224	0.255	0.031	N/A	N/A	А			
9	1/2 @ 0.115	0.510	0.144	0.252	0.108	D	D	D			
10	1/4 @ 0.190	0.246	0.070	0.251	0.181	D	D	D			

# 11L Reference Zone 3 (11L-R3)





Gate 4 Time of Flight (a)

### 11L Reference Zone 3 (11L-R3)



Flaw Profile (rotated 180° to match UT scans)







Gate 1 Amplitude (a)



Gate 4 Time of Flight (a)



Flaw Detection Summary for Panel 11L Lower Surface Reference Zon
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	Zone 11L-R3											
	Drilled FBH		Laser Mea	FBH Detected by NDE								
Reference Hole #	FBH Ø @ Hole Depth	Ø	Remaining Material Thickness	Thickness Near Hole	Actual Hole Depth	ET	MWM	UT PE				
1	3/8 @ 0.325	0.384	0.056	0.355	0.299	D	D	D				
2	3/8 @ 0.040	0.380	0.324	0.359	0.035	N/A	N/A	D				
3	1/4 @ 0.182	0.256	0.223	0.357	0.134	U	U	D				
4	1/4 @ 0.325	0.257	0.060	0.354	0.294	D	D	D				
5	1/8 @ 0.300	0.146	0.078	0.354	0.227	D	D	U				
6	1/8 @ 0.185	0.129	0.165	0.345	0.181	U	U	D				
7	1/4 @ 0.182	0.257	0.173	0.347	0.174	D	D	D				
8	3/8 @ 0.185	0.381	0.173	0.348	0.179	D	D	D				
9	1/4 @ 0.185	0.257	0.110	0.291	0.181	D	D	N/A				
10	1/8 @ 0.185	0.129	0.085	0.267	0.182	D	D	U				
11	1/2@ 0.040	0.503	0.220	0.260	0.040	N/A	N/A	D				
12	3/8 @ 0.150	0.381	0.085	0.267	0.182	D	D	D				

### 11L Validation Zone 1 (11L-V1)



Photo of Flaw Layout with Sandia Flaw Calls Superimposed





L = large flaw	1
M = medium flaw	l
S = small flaw	l



#### 11L Validation Zone 1 (11L-V1)



Gate 1 Time of Flight (a)



(mirrored to match UT scans)



Gate 2 Time of Flight (a)

Caution: data drop zone; check other scans for confirmation



Gate 4 Time of Flight (a)

11L Validation Zone 1 (11L-V1)





Gate 2 Amplitude (b)



Gate 3 Amplitude (b)



Gate 4 Amplitude (b)

#### 11L Validation Zone 1 (11L-V1)



#### Flaw Detection Summary for Panel 11L Upper Surface Validation Zone 1

	Zone 11L-V1											
	Drilled FBH		Laser Me		FBH Detected by NDE							
Verification Hole #	Ø @ Hole Depth	Ø	Remaining Material Thickness	Thickness Near Hole	Actual Hole Depth	ET	MWM	UT PE				
1	1/2 @ 0.040	0.496	0.218	0.246	0.028	N/A	N/A	D				
2	1/4 @ 0.115	0.257	0.134	0.246	0.112	D	D	D				
3	1/8 @ 0.115	0.128	0.123	0.241	0.118	U	D	U				
4	3/8 @ 0.190	0.381	0.059	0.242	0.183	D	D	D				
5	1/4 @ 0.190	0.257	0.058	0.251	0.193	D	D	D				
6	3/8 @ 0.115	0.381	0.141	0.250	0.109	D	D	D				
7	1/8 @ 0.115	0.128	0.138	0.252	0.114	А	D	D				
8	3/8 @ 0.040	0.381	0.218	0.252	0.034	N/A	N/A	D				
9	1/2 @ 0.115	0.512	0.137	0.247	0.110	D	D	D				
10	1/4 @ 0.040	0.256	0.213	0.249	0.036	N/A	N/A	D				
## 11L Validation Zone 2 (11L-V2) - Apex



Photo of Flaw Layout with Sandia Flaw Calls Superimposed

Sandia Labs Flaw Call Layout (see C-scan images that follow)



= flaw not detected #7 (1/8") was not detected in Zone 11L-V2



11L Validation Zone 2 (11L-V2) - Apex



Gate 4 Amp dB (a)



Gate 3 Time of Flight (a)







2

Gate 4 Amp (b)

11L Validation Zone 2 (11L-V2) - Apex





#### 11L Validation Zone 2 (11L-V2)

#### **Flaw Pattern and Size Prediction**



## Flaw Detection Summary for Panel 11L Apex Surface Validation Zone 2

Zone 11L-V2										
	Drilled FBH		Laser Mea	surements		FBH Detected by NDE				
Verificatio n Hole #	Ø @ Hole Depth	ø	Ø Remaining Material Thickness Near Hole Depth			ET	MWM	UT PE		
1	1/4 @ 115	0.245	0.156	0.259	0.103	D	D	D		
2	1/2 @ 0.040	0.496	0.230	0.256	0.026	N/A	N/A	D		
3	3/8 @ 0.115	0.381	0.140	0.254	0.114	D	D	D		
4	1/4 @ 0.190	0.243	0.067	0.253	0.186	D	D	D		
5	1/8 @ 0.115	0.128	0.126	0.253	0.127	D	D	D		
6	3/8 @ 0.190	0.382	0.073	0.253	0.180	D	D	D		
7	1/8 @ 0.115	0.129	0.140	0.253	0.113	А	А	U		
8	1/2 @ 0.115	0.511	0.138	0.253	0.115	D	D	D		
9	3/8 @ 0.040	0.376	0.221	0.248	0.027	N/A	N/A	D		
10	1/4 @ 0.040	0.244	0.213	0.250	0.037	N/A	N/A	D		

## 11L Validation Zone 3 (11L-V3)



Photo of Flaw Layout with Sandia Flaw Calls Superimposed

Sandia Labs Flaw Call Layout (see C-scan images that follow)



#2, (1/8" dia.) and #9 (1/8") were not detected in Zone 11L-V3

L = large flaw
M = medium flaw
S = small flaw

#### 11L Validation Zone 3 (11L-V3)







Flaw Profile (mirrored to match UT scans)

#### 11L Validation Zone 3 (11L-V3)













#### 11L Validation Zone 3 (11L-V3)

#### **Flaw Pattern and Size Prediction**



Flaw Detection Summar	y for Panel 11L L	_ower Surface	Validation Zone 3
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Zone 11L-V3										
	Drilled FBH		Laser Mea	asurements		FBH Detected by NDE				
Verification Hole #	Ø @ Hole Depth	Ø Remaining Thickness Actual Material Near Hole Hole Thickness Depth				ET	MWM	UT PE		
1	3/8 @ 0.040	0.383	0.207	0.241	0.034	N/A	N/A	D		
2	1/8 @ 0.190	0.127	0.077	0.242	0.165	D	D	U		
3	3/8 @ 0.190	0.384	0.056	0.240	0.184	D	D	D		
4	1/4 @ 0.115	0.257	0.136	0.241	0.105	D	D	D		
5	1/4 @ 0.190	0.243	0.059	0.241	0.182	D	D	D		
6	3/8 @ 0.115	0.383	0.137	0.244	0.107	D	D	D		
7	1/2 @ 0.115	0.497	0.145	0.242	0.097	D	D	D		
8	1/2 @ 0.040	0.502	0.211	0.247	0.036	N/A	N/A	D		
9	1/8 @ 0.115	0.125	0.133	0.240	0.107	A	D	U		
10	1/4 @ 0.040	0.258	0.211	0.247	0.036	N/A	N/A	D		



Gate 2 Time of Flight (a)

115

Gate 4 Time of Flight (a)

11L Validation Zone 4 (11L-V4)



Gate 2 Time of Flight (b)

Gate 2 Amp dB (b)

11L Validation Zone 1 (11L-V4)



	Zone 11L-V4										
	Drilled FBH		Laser Mea	FBH Detected by NDE							
Verification Hole #	Ø & Hole Depth	Ø	Remaining Material Thickness	Thickness Near Hole	Actual Hole Depth	ET	MWM	UT PE			
1	1/4 @ 0.040	0.255	0.327	0.355	0.028	N/A	N/A	D			
2	1/4 @ 0.115	0.257	0.241	0.359	0.118	U	U	D			
3	3/8 @ 0.182	0.381	0.224	0.358	0.134	U	U	D			
4	1/8 @ 0.300	0.120	0.066	0.359	0.293	D	D	U			
5	3/8 @ 0.300	0.382	0.244	0.357	0.113	U	U	D			
6	1/2 @ 0.040	0.509	0.328	0.358	0.030	N/A	N/A	D			
7	1/4 @ 0.185	0.257	0.155	0.341	0.186	А	D	D			
8	1/8 @ 0.185	0.131	0.160	0.342	0.182	U	U	U			
9	3/8 @ 0.190	0.384	0.155	0.340	0.185	D	D	D			
10	1/4 @ 0.150	0.257	0.141	0.285	0.144	D	D	D			
11	1/8 @ 0.190	0.125	0.051	0.248	0.197	D	D	U			
12	1/2 @ 0.125	0.514	0.140	0.257	0.117	D	D	D			

Flaw Detection Summary for Panel 11L Lower Surface Validation Zone 4

## Flaw Detection Summary for 1/8" Flaws in RCC Panel 11L

Detection of 1/						
Specimen	Flaw Identifie From	cation and Fla nt Surface (in	Detec Pulse-E	tion by Echo UT		
	0.190	0.120	0.060	Yes	No	
11L-Reference Zone 1 (upper)		4		Х		
11L-Reference Zone 1 (upper)			6		Х	
111 -Reference Zone 2 (apex)	3				X	
11L-Reference Zone 2 (apex)			4	Х		1/8" dia, flaw
						dotoction - 21%
11L-Reference Zone 3 (lower)			5		Х	
11L-Reference Zone 3 (lower)	6			Х		
11L-Reference Zone 3 (lower)		10			Х	
11L-Validation Zone 1 (upper)		3			Х	
11L-Validation Zone 1 (upper)		7		X		
111 Validation Zana 2 (anax)		F		V		
11L-Validation Zone 2 (apex)		<b>3</b> 7		^	v	
TTL-Validation Zone 2 (apex)		1			^	
11L-Validation Zone 3 (lower)			2		Х	
11L-Validation Zone 3 (lower)		9			Х	
11L-Validation Zone 4 (lower)			4		X	
11L-Validation Zone 4 (lower)	8				X	
11L-Validation Zone 4 (lower)			11		Х	

			Detection of 1/4" Diameter Flaws in RCC 11L Specimen							
Specimen	Flaw Identific	ation and Fla	w Depth from	Detect	tion by The LIT					
opecimen	0.190	0.120	0.060	Yes	No					
11L-Reference Zone 1 (upper)			8	Х						
11L-Reference Zone 1 (upper)		12		Х						
11L-Reference Zone 1 (upper)	13			Х						
11L-Reference Zone 2 (apex)		6		Х						
11L-Reference Zone 2 (apex)	8			Х						
11L-Reference Zone 2 (apex)			10	Х		1/4" dia. flaw				
						detection = 100%				
11L-Reference Zone 3 (lower)	3			Х						
11L-Reference Zone 3 (lower)			4	Х						
11L-Reference Zone 3 (lower)	7			Х						
11L-Reference Zone 3 (lower)	9			N/A *						
· · · · · · · · · · · · · · · · · · ·										
11L-Validation Zone 1 (upper)		2		X						
11L-Validation Zone 1 (upper)			5	X						
11L-Validation Zone 1 (upper)	/			X						
11L-Validation Zone 2 (apex)	1			Х						
11L-Validation Zone 2 (apex)			4	Х						
11L-Validation Zone 2 (apex)	10			Х						
111 ) (alidation Zana 2 (lawar)		4		V						
11L Validation Zone 3 (lower)		4	Б			* Flaw #9 out of scan region				
11L Validation Zone 3 (lower)	10		5			$\Delta$ Flaw #1 is in scan by itself so no				
	10			^		location info available				
11L-Validation Zone 4 (lower)	1			Χ <sup>Δ</sup>						
11L-Validation Zone 4 (lower)	2			Х						
11L-Validation Zone 4 (lower)		7		Х						
11L-Validation Zone 4 (lower)		10		Х						

## Flaw Detection Summary for 1/4" Flaws in RCC Panel 11L

## Flaw Detection Summary for 3/8" Flaws in RCC Panel 11L

Detection of 3/	8" Diameter	Flaws in RC	C 11L Specim	en		
Specimen	Flaw Identification and Flaw Depth from Detection				tion by	
Specimen	0.190	0.120	0.060	Yes	No	
11L-Reference Zone 1 (upper)	1			Х		
11L-Reference Zone 1 (upper)		3		Х		
11L-Reference Zone 1 (upper)			5	Х		
11L-Reference Zone 1 (upper)		9		Х		
11L-Reference Zone 1 (upper)			10	Х		
11L-Reference Zone 1 (upper)	14			Х		
11L-Reference Zone 2 (apex)	1			Х		3/8" dia. flaw
11L-Reference Zone 2 (apex)		5		Х		detection $-100\%$
11L-Reference Zone 2 (apex)			7	Х		
11L-Reference Zone 3 (lower)			1	Х		
11L-Reference Zone 3 (lower)	2			Х		
11L-Reference Zone 3 (lower)	8			Х		
11L-Reference Zone 3 (lower)		12		Х		-
11L-Validation Zone 1 (upper)			4	Х		
11L-Validation Zone 1 (upper)		6		Х		
11L-Validation Zone 1 (upper)	8			Х		
11L-Validation Zone 2 (apex)		3		Х		
11L-Validation Zone 2 (apex)			6	Х		]
11L-Validation Zone 2 (apex)	9			Х		-
11L-Validation Zone 3 (lower)	1	}		Х		
11L-Validation Zone 3 (lower)			3	Х		]
11L-Validation Zone 3 (lower)		6		Х		
11L-Validation Zone 4 (lower)	3			Х		-
11L-Validation Zone 4 (lower)	5			Х		1
11L-Validation Zone 4 (lower)		9		Х		1

Detection of 1/2	2" Diameter	Flaws in RC	C 11L Specim	en		
Specimen	Flaw Identifi	cation and Fla				
Specifien	0.190	0.120	0.060	Yes	No	
11L-Reference Zone 1 (upper)	2			Х		
11L-Reference Zone 1 (upper)		7		Х		
11L-Reference Zone 1 (upper)	11			Х		
11L-Reference Zone 2 (apex)	2			Х		
11L-Reference Zone 2 (apex)		9		Х		
11L-Reference Zone 3 (lower)	1			Х		1/2" dia. flaw
						detection = 100%
11L-Validation Zone 1 (upper)	1			Х		
11L-Validation Zone 1 (upper)		10		Х		
11L-Validation Zone 2 (apex)	2			Х		
11L-Validation Zone 2 (apex)		8		Х		
11L-Validation Zone 3 (lower)		7		Х		
11L-Validation Zone 3 (lower)	8			Х		
11L-Validation Zone 4 (lower)	6			Х		
11L-Validation Zone 4 (lower)		12		Х		

## Flaw Detection Summary for 1/2" Flaws in RCC Panel 11L

Probability of Detection Curve for Pulse-Echo UT Flaw Detection in Panel 11L – Flaws in Validation Zones Only UT Validation PoD - Panel 11L Validation Zones





Probability of Detection Curve for Pulse-Echo UT Flaw Detection in Panel 11L – Flaws in Reference and Validation Zones

12L Tee Seal

Three Similar Flaw Zones (1, 2, 3) – 2 rows of flaws on each side of middle flange in each zone















Gate 2 Time of Flight (b)







12L Tee Seal – Zone 1



	Zone 12L-1										
	Drilled FBH		Laser Me	easurement		FBH Detected by NDE					
Lock Sid Hole #	de Ø & Hole Depth	Ø	Remaining Material Thickness	Thickness Near Hole	Actual Hole Depth	ET	MWM	UT PE			
1	1/4 @ 0.190	0.249	0.190	0.249	0.059	D	D	D			
2	1/8 @ 0.190	0.119	0.164	0.294	0.130	D	D	D			
3	3/8 @ 0.190	0.382	0.218	0.296	0.078	U	D	D			
4	1/2 @ 0.190	0.507	0.232	0.299	0.067	U	D	D			
Slip Sid	le										
5	1/4 @ 0.125	0.244	0.231	0.292	0.061	U	U	D			
6	1/8 @ 0.125	0.120	0.212	0.296	0.084	U	U	U			
7	3/8 @ 0.125	0.379	0.213	0.301	0.088	U	U	D			
8	1/2 @ 0.125	0.509	0.249	0.300	0.051	U	U	D			
Notch #		1/2	Width EDM Not	tches Machined	d @ the Web J	unction					
1	1/2 Width	N/A		N/A		U	U	U			
2	1/2 Width	N/A		N/A		U	U	U			
3	1/2 Width	N/A		N/A		U	U	U			
4	1/2 Width	N/A		N/A		U	U	U			

## Flaw Detection Summary for Panel 12L Tee Seal Upper Surface Validation Zone 1

## 12L Tee Seal – Zone 2 (Apex Region)







Flaw Detection Summary for Panel 12L Tee Seal
Apex Surface Validation Zone 2

Zone 12L-2										
	Drilled FBH		Laser M	easurement		FBH	FBH Detected by NDE			
Lock Side Hole #	Ø & Hole Depth	Ø	Remaining Material Thickness	Thickness Near Hole	Actual Hole Depth	ET	MWM	UT PE		
1	1/4 @ 0.190	0.249	0.206	0.280	0.074	U	U	U		
2	1/8 @ 0.190	0.124	0.213	0.276	0.063	U	U	U		
3	3/8 @ 0.190	0.380	0.093	0.276	0.183	D	D	D		
4	1/2 @ 0.190	0.500	Drilled Through	0.284		D	D	D		
Slip Side										
5	1/4 @ 0.125	0.247	0.187	0.308	0.121	U	U	U		
6	1/8 @ 0.125	0.119	0.226	0.301	0.075	U	U	U		
7	3/8 @ 0.125	0.374	0.193	0.294	0.101	D	D	D		
8	1/2 @ 0.125	0.500	0.207	0.277	0.070	U	U	D		
Notch #		1/2	Width EDM Note	ches Machined	@ the Web Ju	nction				
1	1/2 Width	N/A		N/A		U	U	U		
2	1/2 Width	N/A		N/A		U	U	U		
3	1/2 Width	N/A		N/A		U	U	U		
4	1/2 Width	N/A		N/A		U	U	U		





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11L Side

12L (open) Side



# Flaw Detection Summary for Panel 12L Tee Seal Lower Surface Validation Zone 3

Zone 12L-3										
	Drilled FBH	Laser Measurement			FBH Detected by NDE					
Lock Side Hole #	Ø & Hole Depth	ø	Remaining Material Thickness	Thickness Near Hole	Actual Hole Depth	ET	MWM	UT PE		
1	1/4 @ 0.190	0.248	0.178	0.281	0.103	D	D	D		
2	1/8 @ 0.190	0.119	0.193	0.280	0.087	U	U	D		
3	3/8 @ 0.190	0.373	0.212	0.284	0.072	U	D	D		
4	1/2 @ 0.190	0.495	0.193	0.290	0.097	D	D	D		
Slip Side										
5	1/4 @ 0.125	0.248	0.245	0.302	0.057	D	U	U		
6	1/8 @ 0.125	0.119	0.222	0.302	0.080	U	U	U		
7	3/8 @ 0.125	0.373	0.234	0.296	0.062	U	D	U		
8	1/2 @ 0.125	0.500	0.222	0.294	0.072	D	D	D		
Notch #	1/2 Width EDM Notches Machined @ the Web Junction									
1	1/2 Width	N/A		N/A		U	U	U		
2	1/2 Width	N/A		N/A		U	U	U		
3	1/2 Width	N/A		N/A		U	U	U		
4	1/2 Width	N/A		N/A		U	U	U		

Detection Flaws in RCC Tee Seal 12L										
Flaw Size	Flaw Size a	Detection by Pulse-Echo UT								
	Lock Side (11L)	Slip Side (12L)	Yes	No						
1/8" diameter	#2 (Zone 1)		Х							
1/8" diameter		#6 (Zone 1)		Х						
1/8" diameter	#2 (Zone 2)			Х						
1/8" diameter		#6 (Zone 2)		Х						
1/8" diameter	#2 (Zone 3)		Х							
1/8" diameter		#6 (Zone 3)		Х						
1/4" diameter	#1 (Zone 1)		Х							
1/4" diameter		#5 (Zone 1)	Х							
1/4" diameter	#1 (Zone 2)			Х						
1/4" diameter		#5 (Zone 2)		Х						
1/4" diameter	#1 (Zone 3)		Х							
1/4" diameter		#5 (Zone 3)		Х						
3/8" diameter	#3 (Zone 1)		Х							
3/8" diameter		#7 (Zone 1)	Х							
3/8" diameter	#3 (Zone 2)		Х							
3/8" diameter		#7 (Zone 2)	Х							
3/8" diameter	#3 (Zone 3)		Х							
3/8" diameter		#7 (Zone 3)		Х						
1/2" diameter	#4 (Zone 1)		Х							
1/2" diameter		#8 (Zone 1)	Х							
1/2" diameter	#4 (Zone 2)		Х							
1/2" diameter		#8 (Zone 2)	Х							
1/2" diameter	#4 (Zone 3)		Х							
1/2" diameter		#8 (Zone 3)	Х							

## Flaw Detection Summary for All Flaws in RCC Tee Seal 12L

#### Probability of Detection Curve for Pulse-Echo UT Flaw Detection in Panel 12L Tee Seal

PoD Curve for Pulse Echo Ultrasonic NDI Validation on RCC Tee Seal Panels





#### Probability of Detection Curve for Pulse-Echo UT Flaw Detection in All NASA RCC Test Specimens (Phase I & Phase II)

UT Validation PoD - All NASA RCC Specimens

#### Probability of Detection Curves for Pulse-Echo UT Flaw Detection in Various NASA RCC Test Specimen Sets





### Summary of UT Flaw Detection Evaluation in 11L & 12L

#### **UT Pulse Echo Flaw Detection Summary**

- 11L Panel Reference Zones: 29 detected, 5 undetected, 0 mislocated, 2 ambiguous and 0 false
   (Reference Zone Misses = five 1/8" flaws; all flaws larger than 1/8" dia. were detected with no false calls)
- 11L Panel Validation Zones: 35 detected, 7 undetected, 0 mislocated, 0 ambiguous and 0 false
  - (Validation Zone Misses = seven 1/8" flaws; all flaws larger than 1/8" dia. were detected with no false calls)
- 12L Tee Seal Validation Zones: 16 detected, 8 undetected, 0 mislocated, 0 ambiguous and 0 false

(Validation Zones Misses = four 1/8" dia. flaws, one 3/8" dia. flaw, & three 1/4" dia. flaws; all flaws larger than 3/8" dia. were detected with no false calls)

• 12L Tee Seal EDM Notches: 0 detected, 12 undetected, 0 mislocated, 0 ambiguous and 0 false

(EDM notches located 0.6" below surface & 0.30" below skin-to-vertical flange interface; notches are below depth of penetration for UT)

Final Conclusions on Pulse-Echo Ultrasonic Inspection Method for In-Situ Orbiter Health Monitoring

- 18 month test series for UT system certification was completed in March 2005; tests utilized 46 specimens containing 306 flaws
- 306 flaws → 257 hits, 49 misses; 45 of the misses (92%) were 1/8" dia.; 98% of flaws larger than 1/8" dia. were detected
- Pulse-Echo Ultrasonics is able to locate flaws through the entire RCC thickness
- Pulse-Echo UT sensitivity ≈ 1/4" dia. flaw in <u>RCC LE panels;</u>
  90% PoD level = 0.21" dia. flaw
- Pulse-Echo UT sensitivity ≈ 3/8" dia. flaw in <u>RCC Tee seals;</u>
  90% PoD level = 0.38" dia. flaw

## **APPENDIX** A

RCC Life Cycle Wear Study -Effect of UT/EC Scanner System on Surface of RCC Panels

## RCC Life Cycle Wear Study -Effect of UT/EC Scanner System on Surface of RCC Panels

#### **Reference: RCC NDE Wear Test Plan (Document Number - KSC-5600-7096)**

#### Background

The Orbiter RCC In-Situ NDE System will be used during Orbiter turnaround flow to perform inspections of the entry critical RCC panels of the leading edge structural subsystem. Design and fabrication of the complete RCC In-situ NDE systems are underway at various organizations. The complete NDE system will be comprised of flash Thermography, Pulse echo ultrasonic subsystem, and eddy current. During implementation of these inspection tools, caution will be required to protect the RCC from further damage.

#### Objective

The objective of this test was to perform a wear study on flat panel RCC using the pulse echo ultrasonic system to determine if any degradation of the RCC coating material could occur during inspections. The test was carried out based on the likelihood that a certain area of the RCC will be inspected a finite number of times over the remaining life of the vehicle. The data from these tests was used for certification of the equipment. Therefore, the data integrity had Quality oversight.

#### **Test Article**

The test article was an 8.5" L x 4.5" H piece of flight hardware RCC material that was cut from the lower surface of Panel 9L.

#### **Test Description**

The test article was pre-scanned using Eddy Current Si-C thickness measurement at NASA Langley. A pre-scan flaw profile assessment with Thermography was performed at NASA Langley. Sandia labs performed pre- and post scan mechanical testing. The ultrasonic scans on the RCC test article were performed at Sandia labs using the same equipment that will be used during actual shuttle RCC inspections. Once the wear test was completed, Eddy Current and Thermography post-scans were performed at NASA Langley.

## RCC Life Cycle Wear Study - UT/EC Scanner System

- Wear specimen RCC specimen of sufficient size to include a scan area with adjacent un-scanned area
- Conduct pre-scan surface characterization EC Si-C thickness measurement; IR baseline; mechanical thickness measurement; surface profilometry; microscopic cleanliness baseline
- Scan the surface using NASA linear spring with Sandia probe, probe housing, and weeper couplant system (60 cycles)
- · Conduct mid- and post-scan surface characterization



Surface Texture/Profile Measurement



Sample Three Dimensional Surface Topography Map

#### NDE RCC UT Wear Study Test Plan

- 1. Obtain flat RCC specimen of sufficient size to include a scan area with adjacent un-scanned area (e.g. 3" x 3" scan on the interior of a 4" x 4" specimen)
- 2. Conduct pre-scan surface characterization
  - a) Eddy current Si-C thickness measurement
  - b) Perform infrared flash Thermography
  - c) Perform mechanical thickness measurement (1/2" grid over entire surface)
  - d) Perform mechanical and / or optical surface profilometry
  - e) Visually scan the sample surface with a 10x to 30x microscope to check for traces of Delrin housing or urethane membrane material. (Initially for part cleanliness verification only)
  - f) Measure the thickness of UT fixture contact area using appropriate micrometer
- 3. Scan the surface using NASA linear spring with Sandia probe housing / transducer
  - a) Scan at max spring load to be used on orbiter
  - b) Perform <u>60</u> scans over the same area per the following reasoning:
    - i. Max orbiter remaining flights = 15
    - ii. Estimate 2 possible scans to the same area after any flight (based on possible re-scan needed
    - iii. Use a factor of safety of 2
    - iv. So 15 flights x 2 scans x 2 safety factor = 60 possible scans over one location during the orbiters remaining flights
- 4. Conduct surface characterizations identical to Step 2 above after the 30<sup>th</sup> scan and final characterization after the 60<sup>th</sup> scan (IR and ET to be performed pre-test and after 60<sup>th</sup> scan only)
- 5. Section RCC panel in a minimum of 3 locations after final characterizations to observe the surface at scanned areas as well as un scanned (must assure that the Si-C layer can not be smeared by the cutting process
- 6. Record and report all results

#### NDE RCC UT Wear Study and Normal/Shear Load Measurement Test Plan

#### **Quality Assurance Checks**

- Ø Use a Sandia Quality Assurance to sign off on activities at predetermined steps in the testing. Suggested steps are:
- Ø Verify surface characterization at 0 cycles
- $\ensuremath{\varnothing}$  Check test set-up prior to wear testing and sign off on scanning operation
- $\varnothing$  Verify surface characterization performed after 30 cycles
- $\varnothing$  Verify surface characterization performed after 60 cycles
- $\varnothing$  Verify shear stress plan operations are completed per test plan
- $\ensuremath{\varnothing}$  Verify normal stress measurement operations are completed per test plan
- $\varnothing\,$  Utilize a USA and / or NASA Quality Assurance inspector as needed to verify the entire test plan is completed as written

#### Wear Test Panel Cut from RCC Panel 9L



Wear Test to Assess Potential Wear of RCC Surface Caused by Ultrasonic Sanning System



Grid Points Layout on Wear Test Specimen for Data Logging



Scanning Wear Test Panel with Ultrasonic System



#### Microscopic Surface Assessment - Avant 300 Optical Inspection System

Microscopic photography of RCC panel was performed to determine if any materials from the probe housing (delrin or plastic membrane) are deposited on the surface during UT scanning – photos on following pages indicate that there are no deposits on the surface following 30 and 60 scans with the UT probe housing













Grid Point 57

O.G.P. AVANT Photo Microscope with a 71X magnification



After 60 UT Scan Cycles

Grid Point 41





Note: Grid dots reinstalled with sharpie after 30 scans so shape of black grid pts. are different

## Surface Profilometry - Taylor/Hobson Pneumo (TalySurf Series 2)

Mechanical profilometry (resolution of 1  $\mu$ in.) was used to determine if the UT scans produced any wear in the RCC Si-C coating – profile data on the following pages show that the surface was unchanged by the UT probe housing after 60 scans over the same area







Surface Contour Plots of Entire Specimen Before and After UT Scanning -No Removal of RCC Material Measured



Contour Plots Across Grid Line 19-27 Before and After UT Scanning – No Removal of RCC Material Measured



Contour Plots Across Grid Line 37-45 Before and After UT Scanning – No Removal of RCC Material Measured



Contour Plots Across Grid Line 55-63 Before and After UT Scanning – No Removal of RCC Material Measured



Contour Plots Across Grid Line 3 to 75 Before and After UT Scanning – No Removal of RCC Material Measured


Contour Plots Across Grid Line 5 to 77 Before and After UT Scanning – No Removal of RCC Material Measured



Contour Plots Across Grid Line 7 to 79 Before and After UT Scanning – No Removal of RCC Material Measured















# Eddy Current Results - 9LX Wear Test, MWM Scan Direction 1

Eddy Current Results - 9LX Wear Test, MWM Scan Direction 2





Eddv Current Results - 9LX Wear Test. Spot Probe Data

Eddy Current Results - 9LX Wear Test, Spot Probe Data





# Eddy Current Results - 9LX Wear Test, Spot Probe Data

# scans, as the shift also extends beyond the wear test region into the unscanned area.

# Conclusions from RCC Life Cycle Wear Study

Contact ultrasonic scanning system was applied to an RCC panel

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- 60 scans were completed to conservatively assess any RCC wear or degradation stemming from repeated exposure to the ultrasonic transducer housing
- Series of inspections were performed on the RCC panel before and after scanning to assess any changes in the surface
- Surface profilometry (resolution of 1 µin.) determined that the UT scans did not produce any wear in the RCC Si-C coating; profile data showed that the surface profile was unchanged by the UT probe housing after 60 scans over the same area
- Eddy current thickness mapping showed that there was no change in the thickness of the Si-C coating after 60 scans nor was there any change in the EC inspection images
- Microscopic photography of RCC panel determined that there were no materials from the probe housing (delrin or plastic membrane) deposited on the surface during UT scanning

# **RCC Normal and Shear Loads Assessment**

- Measure Normal Loads force needed to actuate the vertical, surface-follower springs in the linear spring, probe holder device
- Measure Shear Loads A force transducer will be used to measure the force needed to actuate the scanner arm (determine the friction load at the transducer-RCC interface)



# **RCC Contact Loads**

Scope

- These contact definitions prescribe the loads allowed to be applied to the RCC by NDE devices and define the allowed materials for devices applying loads to RCC
- These contact definitions are for the RCC NDE devices including
  - Flash Thermography hood
  - Eddy Current probe
  - Eddy Current MWM conformal array probe
  - Pulse Echo Ultrasound probe with weeper
  - Marking system templates

# **RCC Contact Loads Allowables**

- Contact materials for this interface
  - Ensolite, Nylon, Delrin, Kapton, Mylar, urethane, phenolics, Mystic 7000/7001 tape
- Force applied is from the maximum allowed operator or equipment induced load
- Load applied normal to RCC surface with conforming contact
  - not to exceed 6 psi
  - not to exceed 30 lb total per panel (WLE, nose, chin) or gap seal
- Load applied normal to RCC surface with flat or nonconforming contact
  - projected contact area not to exceed 3 sq. inches
  - not to exceed 3 psi averaged over projected area
- Shear load not to exceed 3 psi



# **Flat or Nonconformal Contact**

# RCC Contact Configuration

# NDE RCC UT Normal and Shear Load Measurement Test Plan

- 1. Shear Stress Measurement (max 3 psi allowable)
  - a) Use a force transducer to measure the force needed to move the scanner arm when the transducer is in the air (not conacting surface); Linear Slide Resistance in Air = R1
  - b) Use a force transducer to measure the force needed to move the entire scanner arm so that the UT transducer moves across the RCC surface at maximum load. Friction Shear Load + Slide Resistance = R2
  - c) Calculate friction force at RCC surface. Friction Force at RCC Surface = R2 R1
  - d) Divide this force by the projected surface area in contact with the RCC to determine shear stress.
- 2. Normal Stress Measurement (max 6 psi allowable; 3 psi for projected area)
  - a) Use a force transducer to measure the force needed to actuate the vertical, surface-follower springs.
  - b) Divide this force by the projected surface area in contact with the RCC to determine normal stress.

#### **Assessment of Shear Forces on RCC**

#### Measurement Device: Quantrol Advanced Force Gage 100N (resolution = 0.1 oz.)

#### Shear Loads

A force transducer will be used to measure the force needed to actuate the scanner arm as shown below. One measurement will be made without the transducer in place. This will determine the amount of force needed to move the scanner arm along the rail (resistance in the linear slide scanner arm). This is called the linear slide resistance force (R1). A second measurement will be made with the transducer mounted and an RCC panel in place under the transducer. In the second measurement, the UT transducer will move across the RCC surface. This second measurement will determine the friction load at the transducer-RCC interface as well as the resistance in the linear slide (scanner arm). This is called the friction shear load plus the linear slide resistance force (R2). The first force measurement will be subtracted from the second to determine the friction shear load on the RCC (R3) will be divided by the surface area in contact with the RCC to determine the shear stress on the RCC panel. The shear

stress shall not exceed 3 psi.

R2 - R1 = R3(friction shear load on RCC)



## **Determining Shear Forces on RCC**

Average Three Measurements

Linear Slide Resistance in Air = 31 oz., 31.5 oz., 30 oz. R1 = 1.93 lbs. (30.8 oz.)

Friction Shear Load + Slide Resistance = 52.7 oz., 54 oz., 56 oz. R2 = 3.39 lbs. (54.2 oz.)

Friction at RCC Surface = R2 - R1 = 1.46 lbs.

Surface Shear Stress = Friction at RCC/Surface area

**Surface Shear Stress** = 0.61 psi (min) to 1.88 psi (max)

Allowable shear stress on RCC panel is 3 psi

(membrane dia. = 1.0" for min contact area) (delrin housing dia. = 1.75" for max contact area)





# Assessment of Normal Forces on RCC

Measurement Device: Quantrol Advanced Force Gage 100N (resolution = 0.1 oz.)

#### Normal Loads

A force transducer will be used to measure the force needed to actuate the vertical, surface-follower springs in the NASA linear spring, probe holder device. The measured force will be divided by the surface area in contact with the RCC to determine the normal stress on the RCC panel. The normal stress shall not exceed 6 psi. The force will be measured at the base of the probe housing and in the direction shown below



# **Determining Normal Forces on RCC**

Average Three Measurements

Normal Force = 49.5 oz., 50.5 oz., 50 oz.  $F_n = 3.13$  lbs. (50.0 oz.)

**Normal Surface Stress** = Normal Force at RCC/Surface area

Normal Surface Stress = 1.30 psi

Allowable normal stress on RCC panel is 3 psi if projected contact area is used

(delrin housing dia. = 1.75" for projected contact area A= 2.4 in.<sup>2</sup>)



# **APPENDIX B**

# PULSE-ECHO ULTRASONIC INSPECTION PROCEDURE for SPACE SHUTTLE SILICON CARBIDE COATED REINFORCED CARBON-CARBON (RCC) HEAT SHIELD PANELS

## PULSE-ECHO ULTRASONIC INSPECTION PROCEDURE for SILICON CARBIDE COATED REINFORCED CARBON-CARBON (RCC) HEAT SHIELD PANELS USED ON THE SPACE SHUTTLE

## April 2005 Phil Walkington and Dennis Roach Sandia National Laboratories - Albuquerque, NM

## **Prepared for NASA**

## 1.0 SCOPE

This procedure describes the criteria and procedure for ultrasonic (UT) inspection of silicon carbide coated reinforced carbon-carbon (RCC).

## 2.0 REFERENCES

2.1 SAIC Ultra Image International Operation Manual UltraSpect-MP

## 3.0 REQUIREMENTS

## 3.1 Inspection Equipment

- 3.1.1 Ultra Image Low Profile 2-Axis Manual Scanner (LPS-100) per Figure 1 & 2
- 3.1.2 UltraSpect-MP Data Acquisition System per Figure 3
- 3.1.3 Sony laptop computer with SAIC Ultraspect software
- 3.1.4 Ultrasonic Probe (GE Inspection Technologies / Krautkramer 1 MHZ; 1.0 inch diameter; 2.0 inch SPH Focus part # 389-058-620) per Figure 4
- 3.1.5 Testech Weeper per Figure 5 & 6
- 3.1.6 Ultrasonic Calibration Standards
- 3.1.7 Bogen Tripod: manual scanner positioning mechanism (Model # 3058) per Figure 2

## 3.2 Supplemental Equipment and Materials

- 3.2.1 Ultrasonic Couplant Distilled Water
- 3.2.2 Mystic Tape approved for placement on RCC surface

## 3.2.3 120 V AC power

- 3.2.4 Personnel stand/ladder to allow access to points 76" from floor
- 3.2.5 Mylar film (0.001" thick)

## 3.3 Personnel

It is recommended that the inspector using this procedure be experienced and knowledgeable in the fundamentals of ultrasonic testing. Inspectors should fully possess the qualification of ultrasonic testing personnel as defined in <u>Recommended Practice No. SNT-TC-1A</u>, <u>Personnel Qualification and Certification in Nondestructive testing</u>, available from ASNT (American Society for Nondestructive Testing), ATA 105 or other approved certification standard. It is recommended that the inspector has taken the SAIC Ultra Image International UltraSpect-MP Scanner Course so that they are familiar with all system software and controls.

## 4.0 PROCEDURES

Refer to the referenced operation manuals for the description of the software as needed. A brief overview of the System setup and Calibration Icons are shown in Figure 7.

- 4.1 Instrument Set-Up
  - 4.1.1 Connect the cables between the laptop PC and data acquisition system (DAS) as shown in Figure 3. Setup the tripod and attach the manual scanner as shown in Figure 2. Attach the probe holding fixture (linear spring) to the manual scanner and then attach the WEEPER body to the yoke on the linear spring as shown in Figure 2. Place the ultrasonic (UT) probe into the WEEPER body and connect the water line to the weeper body from the water distribution system as shown in Figure 2. Finalize the cable connections from the DAS, manual scanner and ultrasonic probe as shown in Figure 3.
  - 4.1.2 Position the manual scanner system over the UT Calibration Standard. Position the tripod with the manual scanner so that the linear spring which holds the Weeper body is in contact with the RCC surface. The linear spring should be at middle range of travel so that the Weeper body can follow gradual contour changes and move smoothly across the surface. Position the UT probe on the appropriate UT Calibration Standard at an unflawed area. Turn the power on to the recirculation pump in the water distribution system and set the recirculation valve to open. Next, adjust the water flow to the WEEPER body and clear out any air bubbles in the water column by turning the weeper end cap up so that any air can escape from the holes in the membrane. The UT Calibration Standard contains a series of flat bottom holes (FBH) at various depths from the front surface. These FBH locations are referenced in the following inspection procedure and can be used to interpret the inspection results.

- 4.1.2.1 During inspection of the calibration standard, the scanner and ultrasonic probe should be in the same orientation as they will be deployed in subsequent RCC inspections. The cal standard inspection can be completed on an adjacent work surface or by placing the calibration standard over the region of interest on the RCC panel. If necessary, Mylar film can be placed between the cal standard and the RCC surface. By looking at the resulting flaw pattern on the C-scan and comparing it to the known flaw layout in the calibration standard, this process will allow the inspector to determine the orientation of the C-scans produced by the system. This will ensure that any flaw indications found during the actual inspection will be accurately located on the RCC panel.
- 4.1.3 Turn the power on to the laptop PC. Once the laptop computer has booted up, go to the SYSTEM UTILITIES Icon and select which scanner will be used for this inspection (manual or automatic). The manual scanner can be selected in 'Defaults' at "Custom 1" as shown in Figure 8. The manual scanner can now be set up to perform an ultrasonic inspection. Turn the power on to the DAS. Now right click the red A icon in the lower right corner of the screen and then left click 'Status' for the System Status window to appear. In approximately 30 seconds to three minutes, the DAS Subsystem will indicate 'Online' as shown in Figure 9.
- 4.1.4 Now the ultrasonic test parameters can be set up by selecting the UT CALIBRATION Icon and selecting the 'OMASTER.tiff' file as shown in Figure 10. Once the 'OMASTER.tiff' file is open, go to 'File' and do a 'Save As' (example PE03482). The file is now unlocked so new setup parameters can be entered. Now go to 'Channel' and select "Channel 1" and then go to 'Settings' to select 'Select Ch/Gt' as shown in Figure 11. Four gates have been selected in this example. The ultrasonic transducer information can be documented in the 'Transducer' section (Figure 12).
- 4.1.5 Select "Pulser Preamp" and set PULSER TYPE to Sq. Wave and the WIDTH to 700 nanoseconds. Adjust the DAMPING to 100 ohms, GAIN to 35 dB, and VOLTAGE to 300 volts. Set the LP FILTER to off and the HP FILTER to 0.25 MHz.
- 4.1.6 Set the correct focus of the UT probe in the Weeper body in order to image the BS of the RCC material. Right now, the time base for the A-trace display is set to show the first twenty microseconds with the main bang on the left side as shown in Figure13. Go to "Gate Adjust", set the A-DELAY and A-WIDTH for 40 microseconds each and the C-DELAY for 45 microseconds and the C-WIDTH for 12 microseconds. Set the PEAK MODE to Max so that the highest peak in the gate is recorded. The A-trace display now displays a flat A-trace on the screen (Figure 14) because the back surface (BS) is later in time and could be viewed by changing the time base. As the inspector pushes the UT probe into the Weeper body an echo will appear in the A-trace display for a viewing window of 44 to 60 microseconds and push the UT probe into the Weeper body until the large negative peak is at approximately 47 to 48 microseconds as shown in Figure16. The A-trace signal on the screen from left to right shows: (A) echo from the WEEPER membrane / front surface (FS) echo, (B) region between front and back surface, and (C)

the back surface (BS) echo of the RCC material. The BS echo is approximately 5 microseconds from the FS (time base 53 microseconds). Due to the inspection frequency of 1 MHz there is a long ring down which makes it difficult to image flaws close to the FS. The signal variations between (B) and (C) are used to detect flaws in the RCC material.

- 4.1.7 Move the transducer around the RCC surface with the manual scanner X-Y Controls and adjust the "Pulser Preamp" GAIN until the amplitude of the echo from the back surface (BS) of the RCC reads approximately +80% Full Screen Height (FSH). These settings can vary from probe to probe and are somewhat dependent on operator preferences.
- 4.1.8 Set up the necessary parameters to do a full wave capture of the ultrasonic signals between the front surface (FS) and back surface (BS) of the RCC specimen. In the "Acquisition" menu, set the VIDEO MODE to collect "Full" wave (positive and negative peaks) data acquisition as shown in Figure17. Set the 'A/D Rate' to 50 Msps. Select "Signal Processing" and set the I-Gate from Off to SW (software gate) (Figure 18) and in the 'Gate' menu select the Interface Gate (Figure 19). Now the SURFACE FOLLOWER is on. The surface follower threshold can be set to approximately 50% by going to 'File' and unlocking this file. This selection should give a consistent signal display with the A-trace screen display triggering on the front surface echo signal (A) as shown in Figure 20.
- 4.1.9 To detect flaws in the RCC material, a series of gates will be positioned in the data acquisition system. The gates are set in order to control the acquisition of appropriate UT information. User specified depth gates allow only those echo signals that are received within a limited range of delay times following the front surface (FS) echo to be in the C-scan plot.
  - 4.1.9.1 Now the inspector is ready to select "Gate Adjust" while the Interface Gate is still selected. The operator can set the V-DELAY to 45 microseconds, V-WIDTH to 20 microseconds for the full wave signal capture interval (green color on the A-trace display ) and the I-DELAY to 46 microseconds, I-WIDTH to 12 microseconds for the C-scan plot (red color on the A-trace display) as shown in Figure 20. The full wave capture will allow the operator to re-adjust gate delays and widths after the RCC material has been scanned and generate new C-scan plots. The position and number of gates will determine the C-scan data plotted. The operator can select up to four separate gates consisting of either positive, negative, or both signal amplitudes or time of flight intervals. The gates can be positioned by selecting 'GATE' and selecting either Gate 1, 2, 3 or 4 in the menu (Figure 21 and 22).
  - 4.1.9.2 By employing a series of gates in one scan, it is possible to display data over a wide range of depths. Once 'Gate 1' has been selected, the operator can set the I-DELAY and I-WIDTH for each of the four gates to display C-scan information. Repeat the gate selection process for each of the four gates.

- 4.1.9.3 Set-up information will be saved for this file upon exit. It is important to understand that once a file is unlocked, any changes will be saved upon exit. To recall a particular setup, just go back to the UT CALIBRATION icon and select that FILE (example PE03482) and go to 'File' and do a 'Save As' (example PE03482x). By opening this file, all the old scanning parameters are called in and will be saved under a new test name. This way the original file won't be altered.
- 4.1.10 Complete the calibration standard inspection.
  - 4.1.10.1 Position the UT probe over the reference standard that represents the inspection zone to be scanned and adjust the water flow to the weeper body to ensure optimum UT coupling with the RCC surface.
  - 4.1.10.2 Use engineered flaws on the reference standard to check equipment operation and data acquisition gate settings. Use this set-up and standard to adjust the position (focus) of the UT probe in its housing so that an optimal back surface signal is produced.
  - 4.1.10.3 Adjust the gain until the amplitude of the echo from the back surface of the RCC is approximately 80% of full screen height over a non-flawed area and record the gain level used.
  - 4.1.10.4 Establish scan boundaries to cover the region of interest, set the step size for data acquisition in the X and Y direction to 0.040" increments, and complete a scan of the reference standard.
  - 4.1.10.5 Save the recorded data to the computer hard disk
- 4.2 Inspection Procedure
  - 4.2.1 Position the tripod with the manual scanner so that the linear spring which holds the Weeper body is in contact with the silicon carbide coated reinforced carbon-carbon (RCC) surface. The linear spring should be at middle range of travel so that the Weeper body can follow gradual contour changes and move smoothly across the surface. Turn the power on to the recirculation pump in the water distribution system and set the recirculation valve to open. Next adjust the water flow to the WEEPER body and clear out any air bubbles in the water column by turning the weeper end cap up so that any air can escape from the holes in the membrane. Now the ultrasonic test parameters can be set up by selecting the EXAM icon and selecting the current test name (example 'PE03482.tiff') file. After this file is opened, go to 'Scanner' and select "Exam Setup/Position" as shown in Figure 23. Then enter the X-Y scanning dimensions and the interval for the X-Y data collection in the "Exam Setup/Scanner Position" menu as shown in Figure 24.
  - 4.2.2 Establish the scan boundaries to cover the region of interest and set the step size for data acquisition in the X and Y direction to 0.040" increments.
    - 4.1.2.1 Prior to initiating the inspection scan, place a piece of Mystic tape on the RCC panel such that it is inside the edge of the scan boundary but not over any inspection area of interest. When the UT probe encounters the tape, a distinct signal and

thus a distinct image – will be produced in the C-scan. This unique portion of the C-scan will allow the inspector to determine the orientation of the C-scans produced by the system. This will ensure that any flaw indications found during the actual inspection will be accurately located on the RCC panel.

- 4.2.3 Adjust the water flow to the weeper body to ensure optimum UT coupling with the inspection surface.
- 4.2.4 Move the UT transducer to at least three different locations within the inspection area of interest. Adjust the gain until the amplitude of the echo from the back surface of the RCC is approximately 80% of full screen height over a non-flawed area and record the gain level used. Gain adjustments from the levels set using the calibration standard will not exceed  $\pm 4$  dB and may not be changed during a scan. The difference between the reference standard gain and the inspection zone gain used is referred to as the transfer gain.
- 4.2.5 Complete the UT inspection by using the manual scanner to move the UT transducer over the prescribed region of interest. The probe can now be indexed to the starting position and the "Zero Position" selected so that each axis is set to zero (Figure 24). The scanning parameters are:

Index Axis: Y		
Scan Axis: X		
X & Y Resolution	EXAMPLE	0.04 inches
Y-Scan Length	EXAMPLE	6 inches
X-Scan Length	EXAMPLE	6 inches
Y-Scan Exam Vel	EXAMPLE	1.0 (Manual)
X-Scan Exam Vel	EXAMPLE	1.0(Manual)

Finally, the inspector can check all the Scan Setup Parameters and, if satisfied, the scan can be started by selecting "Scan" (Figure 25). At the end of the scan, the operator can STOP and then save the data (Figure26). The engineered flaws are clearly visible when viewed side-by-side with adjacent, unflawed material.

- 4.2.6 To RESCAN a specific region within the scan area before the scan is saved, just use the X-Y controls to go back over an area and the new data will be rewritten.
- 4.2.7 Save the recorded data to the computer hard disk.
- 4.2.8 Data analysis: utilize the "Amplitude" and "Time of Flight" C-scan images, along with select A-scan waveforms from critical regions to determine the presence of flaws in the material.
- 4.2.9 To SCAN a new area, go to the UT CALIBRATION Icon and select the "test.tiff" file that has the right scanning test parameter. Once the "test.tiff" file is open, go to 'File' and do a 'Save As' (example PE03482x). Now the inspector has the new test file ready. The file is now unlocked so new setup parameters can be entered if needed. Next the ultrasonic test scan parameters can be set up by selecting the EXAM icon and selecting

the new test name (example 'PE03482x.tiff') file. Once this file is open, go to 'Scanner' and check the X-Y scanning dimensions and the interval for the X-Y data collection. The probe can now be indexed to the starting position and the "Zero Position" selected so that each axis is set to zero. Then select "Scan" to start the data collection for the new test.

## 5.0 EVALUATION

5.1 Once the digitized A-scan waveforms are recorded during the ultrasonic pulse-echo inspection of the RCC material, the amplitude, dB (attenuation), and time of fight peak signals can be displayed as a C-scan image and analyzed to determine if a flaw exist within the material. The reflected beam from the back surface of the RCC material can be used as the starting point for this analysis. The pseudo colored C-scan image can reveal several variations within the RCC material. The peak amplitude from the back surface is affected by the attenuation within the material and will be displayed in the pseudo colored C-scan image. Any large amplitude change (>12db) in the C-scan image shall be reported. Depending upon the geometry of a flaw and location within the RCC material, the amplitude might not appear very different than that of the surrounding back surface. This is where the time of flight Cscan image can show a slight shift in the pseudo color of the back surface. By analyzing all pseudo colored images (amplitude, dB, and time of flight) and the A-scan waveforms, the inspector can determine if a flaw exists within the RCC material. The time of flight C-scan image also shows thickness variations or the taper along the edges of the RCC panel. Figure 27 is a photo of an RCC test specimen containing flat bottom holes on the backside. Inspections were completed from the opposite (unflawed) side and the resulting C-scan image is shown in Figure 28. The flaws are detected by the UT system and clearly imaged in the color-coded scans.

## 6.0 INSPECTION RESULTS

6.1 Report all flaws greater than 0.25 inches in diameter and any large amplitude changes (greater than 12 dB) that appear in the C-scan image to the appropriate engineering personnel on site for further evaluation / action.



Figure 1: Ultra Image Low Profile 2-Axis Manual Scanner



Figure 2: Manual Scanner Mounted on Tripod with Weeper

# **UT and EC Scanner System Hook-Up**



Figure 3: Cable Connections Between Laptop, DAS, Manual Scanner and UT Probe



Figure 4: Individual View of Weeper Body, Ultrasonic Transducer Connectors and Coax Cable



Figure 5: Assembled View of Weeper Body, Ultrasonic Transducer, Connectors and Coax Cable



Figure 6: Testech Weeper Water Supply

# **System Setup and Calibration**

As with all inspection processes, Calibration file selection is the first step to setting up the instrument for data acquisition. Double clicking the calibration icon (shown below) will bring up the file selection window as shown on the next page. The other system icons and a brief explanation of their function are also given.

UT Calibration:

Ultrasonic parameters setup and calibration module. Setup files may be selected or created; UT calibrations are performed in this module.



Exam: Data acquisition module. All scanner functions and data collection parameters are controlled from this module. Motion control for jogging and positioning scanner head can be performed here.



Analysis:

All data analysis and report functions are performed in this module.



Scanner Position: Contains the same motion control for jogging and positioning as found in Exam but does not require an Exam file to be opened.



System Utilities: Scanner selection, Motion enable and other functions are found in this module.



# Figure 7: System Setup and Calibration Icons





DAS Subsyst	em Online col	ntaining
2 L ECT Subsysti	em Offline	or Data

Figure 9: System Status

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<b>Z.</b>	0363.tff	21528K	ut1	
/	03631.tff	21528K	ut1	
	03632.tff	21528K	ut1	
	OMASTER.tff	10K		
	25refstd.tff	29483K	ut1	
	25refstd1.tff	29483K	ut1	
	25refstd2.tff	18349K	ut1	
	44refstd.tff	19462K	ut1	
H	44refstd1.tff	19462K	ut1	V
ব্যস				12
	Selection			
	OMASTER.tff			
	1			

Figure 10: UT File Selection



Figure 11: Channel 1 Gate Selection



Figure 12: Transducer Settings



Figure 13: UT Main Bang Signal on A-trace Display



Figure 14: UT signal on A-trace Display during Weeper/probe adjust



Figure 15: UT signal on A-trace Display during Weeper/probe adjust



**Figure 16: UT signal on A-trace Display at Inspection Focus** 



Figure 17: Acquisition Menu/Video Mode set to Full wave capture



Figure 18: Signal Processing Menu/SW Gate selected



Figure 19: Gate Menu/Interface Gate selected



Figure 20: Surface Follower Threshold set to 50% FSH



Figure 21: Gate 1 setup to display data at C-Delay of 5 microseconds

Calibration - PE03482	x - Unlocked		_0×
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Amp. 0 2 120 - 110 - 100 - 90 - 80 - 70 - 60 - 50 - 40 - 30 - 20 - 10 - 0 - 10 - 0 - 10 - 1	OD <u>Corrosion Gate</u> OD <u>Corrosion Gate</u> Set	HIT+C  V  M Path 2.000 in.  Phased Angle    Alt+C	~~~~Y

Figure 22: Gate Menu with Gate 2 selected

<mark>/</mark> ДЕхат -	Manual_	TStop1 - Unio	cked		A DESCRIPTION OF THE OWNER OF THE			- 🗆 ×
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File: Mar	ual_TSto	p1 Exam Dat	e: 02/18/	2005 Time:	Exam Setup/Position	Ctrl+i	1	
Channel: Gain: 32,	1 Gate: 0 dB Da	SW 2 Mode: c:OFF Offse	Max Vide t: 0.0 db	o Mode: Full Pulser Vol	Track Correction	Alt+T		
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Figure 23: Exam Setup/Position Menu

and a second second		From	To	Interval	Exam Vel
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					and the second
Axis	Current F	Pos. New Po	os. VJoystick	ADS MOVE Sca	nner
Axis X-axis	Current F 0.000	Pos. New Po	os. VJoystick	Zero Positi	on

Figure 24: Exam Setup/Scanner Position

🖉 Exam -	Manual_	TStop1 - Unio	cked					
File	Mode	C <u>h</u> annel	Gate	<u>C</u> -Scan	<u>S</u> canner	<u>S</u> ettings		Help
Sca	an	Stop	Pause	Con	tinue	A-Scope	Track Correct	OFF
File: Mar Channel: Gain: 32.	nual_TSto 1 Gate: .0 dB Da	p1 Exam Dat SW 2 Mode: c:OFF Offse	e: 02/18/3 Max Vide t: 0.0 db	2005 Time: D Mode: Full Pulser Vol	16:37 - 17:00   Video Filte  tage: 300   F	6 WP:N/A MT:1.0 er: 2 Plotting: Max		
Copyrigh	t 2002-20	)04 Wesdyne Ir	nternation	al, LLC				

Figure 25: Exam Scan Start

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Exam	was	halted	by	operator	
		σκΙ			
	atus Exam	atus Exam was	atus Exam was halted	atus Exam was halted by	atus Exam was halted by operator

Figure 26: Exam Stopped



Figure 27: Photo of RCC Specimen 03-51 Containing Simulated Flaws



Figure 28: Amplitude and Time-of-Flight C-scan Images Showing Flaws in RCC Test Specimen

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