



Idaho National Laboratory

# Geocentrifuge Studies of Flow and Transport in Porous Media

**Carl D. Palmer**

Idaho National Laboratory

**Earl D. Mattson**

Idaho National Laboratory

**Robert W. Smith**

University of Idaho

**Environmental Remediation Sciences Program**

**PI Meeting**

**Airlee Conference Center, Warrenton, VA**

**April 3-5, 2005**

# INL Geocentrifuge

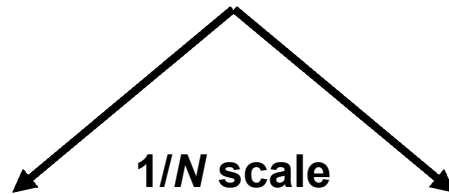
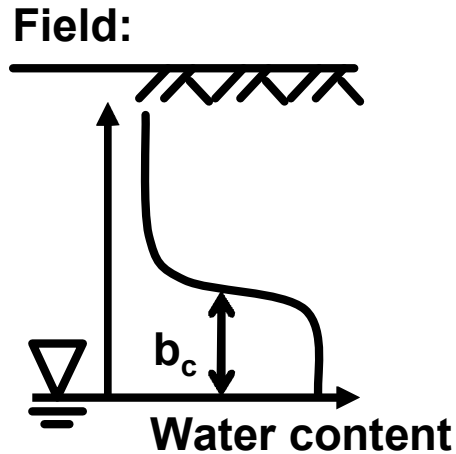
- Actidyn Systemes
- 2-meter radius
- 5-130 g acceleration



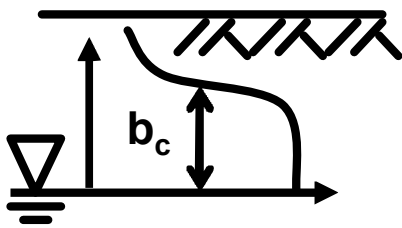
# Motivation for Geocentrifuge

- Decrease the time required to complete an experiment compared to 1g experiments.
- Obtain spatial scaling real-world problems according to the acceleration.
- Study a wider range of conditions than is capable under 1g acceleration.

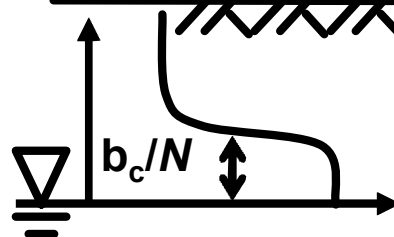
# Vadose Zone Transport



1g model:



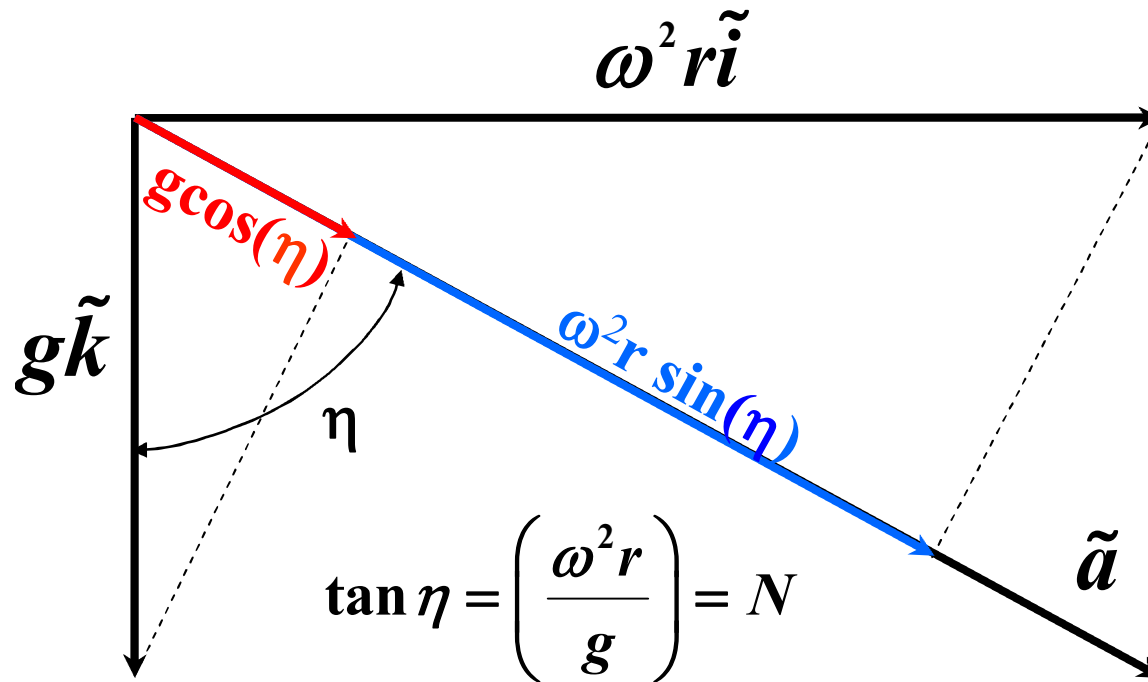
Centrifuge model:



## Scaling Factors

<i>Gravity</i>	$1/N$
<i>Length</i>	$N$
<i>Velocity</i>	$1/N$
<i>Time</i>	$N^2$
<i>Decay Rate</i>	$1/N^2$
<i>Dispersion</i>	$1$
<i>Porosity</i>	$1$
<i>Temperature</i>	$1$
<i>Pressure</i>	$1$
<i>Density</i>	$1$
<i>Viscosity</i>	$1$
<i>Mass Fractions</i>	$1$

# Accelerations



# Fluid Potential

$$\phi = -\frac{\omega^2 r^2}{2} + 2\omega u_r (\theta - \omega t) + gz + \frac{\tilde{\mathbf{u}} \cdot \tilde{\mathbf{u}}}{2} + \frac{p}{\rho_f}$$

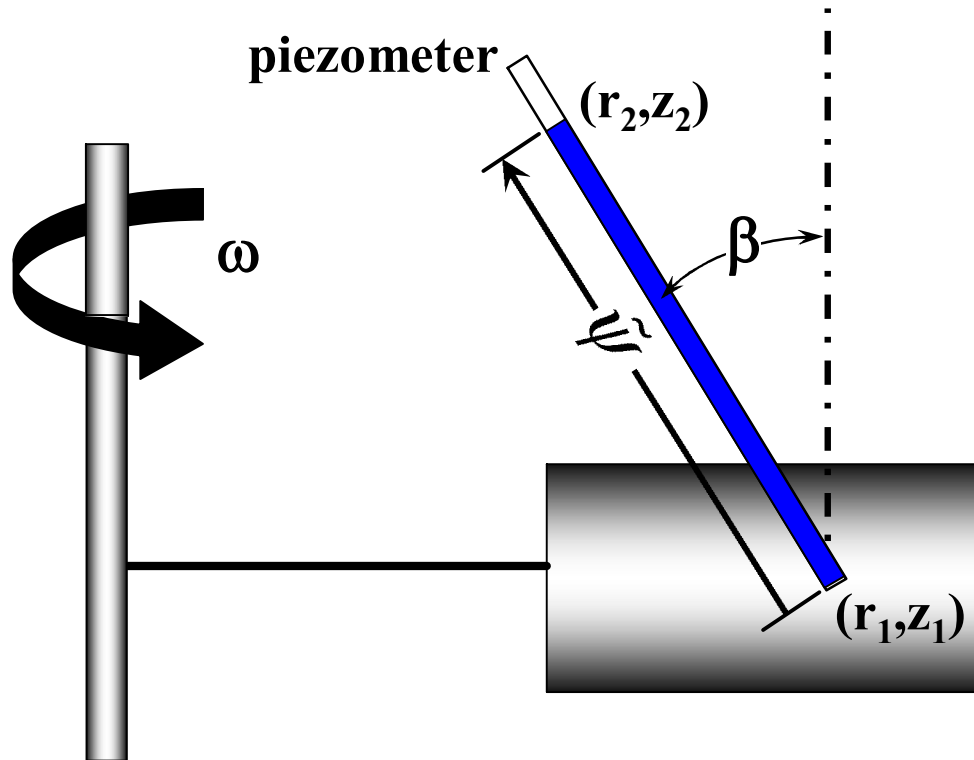
**Centripetal Force**                      **Coriolis Term**                      **Gravitational Term**                      **Velocity Term**  
**Work-Pressure Term**

If Coriolis term is insignificant, velocity is small, and steady-state flow:

$$\phi = -\frac{\omega^2 r^2}{2} + gz + \frac{p}{\rho_f}$$

# Pressure and Piezometers

$$p = p_c + p_g = -\rho_f \omega^2 (r_2^2 - r_1^2) + \rho_f g (z_2 - z_1)$$



$$p = -\rho_f \left[ (\omega^2 \sin^2 \beta) \psi^2 - (2\omega^2 r_1 \sin \beta + g \cos \beta) \psi \right]$$

# Pressure and Piezometers

For  $\beta = \pi / 2$

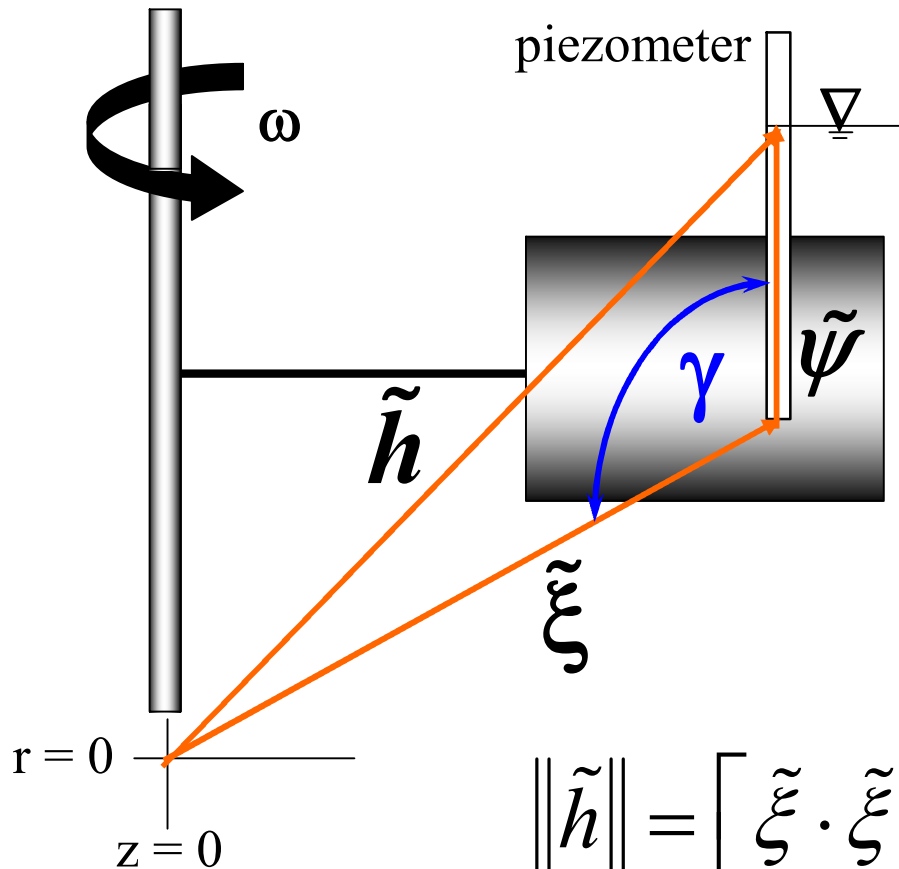
$$\psi_{\pi/2} = r \left( 1 - \sqrt{1 - \frac{p}{\rho_f \omega^2 r^2}} \right)$$

For  $\beta = 0$

$$\psi_0 = \frac{p}{\rho_f g}$$



# Elevation Head and Hydraulic Head



$$\tilde{h} = \tilde{\xi} + \tilde{\psi}$$

$$\|\tilde{h}\| = \left[ \tilde{\xi} \cdot \tilde{\xi} + \tilde{\psi} \cdot \tilde{\psi} + 2(\tilde{\xi} \cdot \tilde{\psi}) \right]^{1/2}$$

$$= \left[ \|\tilde{\xi}\|^2 + \|\tilde{\psi}\|^2 + 2\|\tilde{\xi}\|\|\tilde{\psi}\|\cos\gamma \right]^{1/2}$$

# Specific Discharge

$$\tilde{q} = -\frac{\rho_f}{\mu} \bar{k} \tilde{\nabla} \phi$$

$$q_r = -\frac{\rho_f}{\mu} \left[ k_{rr} \left( -\omega^2 r + \frac{1}{\rho_f} \frac{\partial p}{\partial r} \right) + k_{rz} \left( g + \frac{1}{\rho_f} \frac{\partial p}{\partial z} \right) \right]$$

$$q_z = -\frac{\rho_f}{\mu} \left[ k_{zr} \left( -\omega^2 r + \frac{1}{\rho_f} \frac{\partial p}{\partial r} \right) + k_{zz} \left( g + \frac{1}{\rho_f} \frac{\partial p}{\partial z} \right) \right]$$

# Specific Discharge

$$q_r = -\frac{k_{rr}\rho_f}{\mu} \left[ -\omega^2 r - (2\omega^2 \sin^2 \beta) \psi \frac{\partial \psi}{\partial r} + (2\omega^2 \sin \beta) \psi \right. \\ \left. + (2\omega^2 r \sin \beta + g \cos \beta) \frac{\partial \psi}{\partial r} \right]$$

$$q_z = -\frac{k_{zz}\rho_f}{\mu} \left[ g - (2\omega^2 \sin^2 \beta) \psi \frac{\partial \psi}{\partial z} \right. \\ \left. + (2\omega^2 r \sin \beta + g \cos \beta) \frac{\partial \psi}{\partial z} \right]$$

# Specific Discharge

For  $\beta = \pi/2$

$$q_r = -\frac{k_{rr}\rho_f\omega^2}{\mu} \left[ (2\psi - r) + 2(r - \psi) \frac{\partial \psi}{\partial r} \right]$$

$$q_z = -\frac{k_{zz}\rho_f}{\mu} \left[ g + 2\omega^2 (r - \psi) \frac{\partial \psi}{\partial z} \right]$$

# Specific Discharge

For  $\beta = 0$

$$q_r = -\frac{k_{rr}\rho_f g}{\mu} \left[ -\frac{\omega^2 r}{g} + \frac{\partial \psi}{\partial r} \right] = -K_{rr} \left[ -N + \frac{\partial \psi}{\partial r} \right]$$

$$q_z = -\frac{k_{zz}\rho_f g}{\mu} \left( 1 + \frac{\partial \psi}{\partial z} \right) = -K_{zz} \left( 1 + \frac{\partial \psi}{\partial z} \right)$$

# Non-dimensionalization of the Navier-Stokes Equation for Flow in a Centrifugal Field

Or

$$\frac{\partial^2 u^*}{\partial r^{*2}} - \frac{2}{Ek} u^* = \frac{1}{Ek Ro} r^* + \frac{\partial p^*}{\partial r^*}$$

where

$$Ek = \nu / \omega r_0^2$$
$$= \frac{\text{viscous force}}{\text{Coriolis force}}$$

$$Ro = V_0 / \omega r_0$$
$$= \frac{\text{inertial forces}}{\text{Coriolis force}}$$

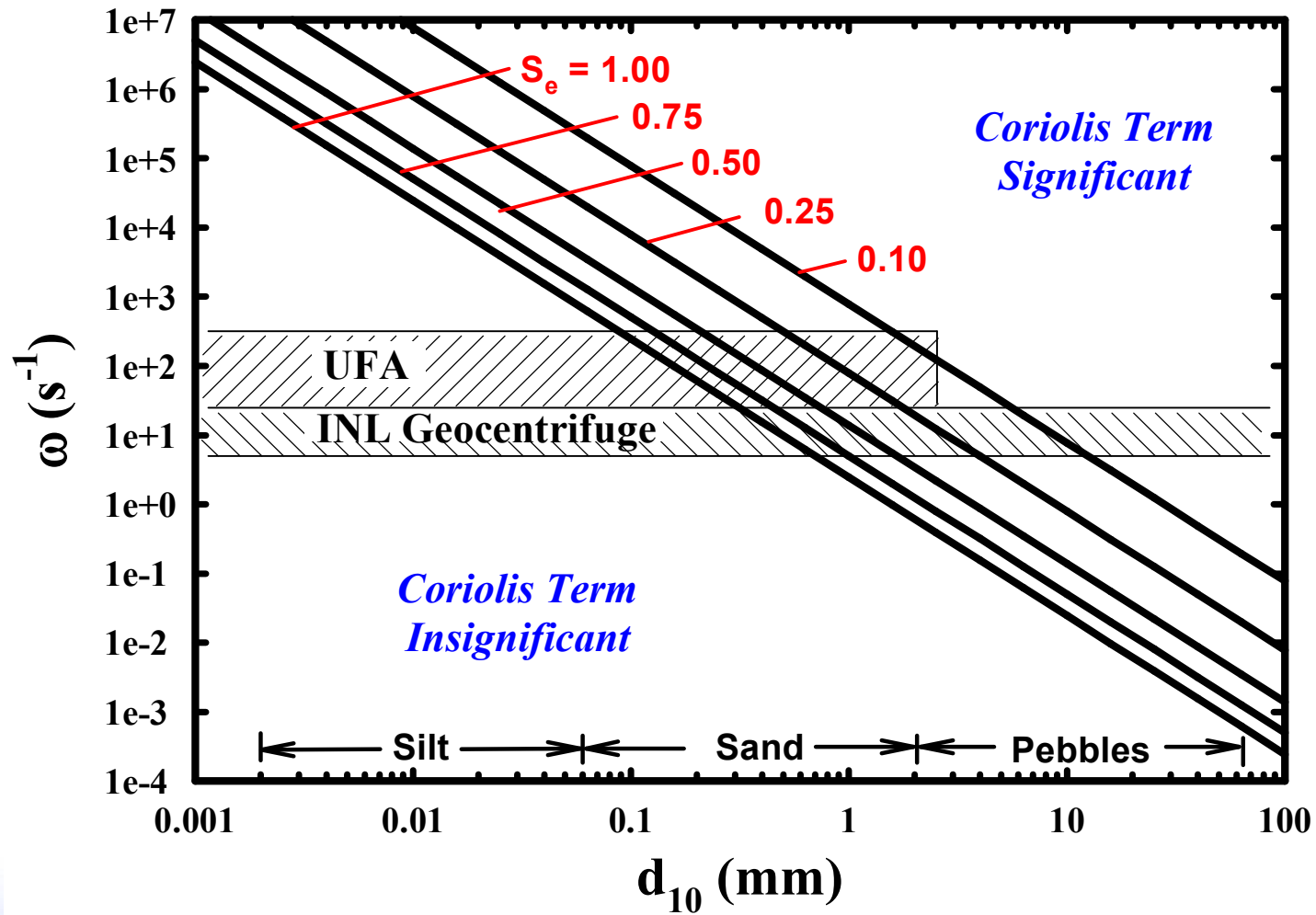


# Coriolis Effects

Coriolis effects can be ignored if:

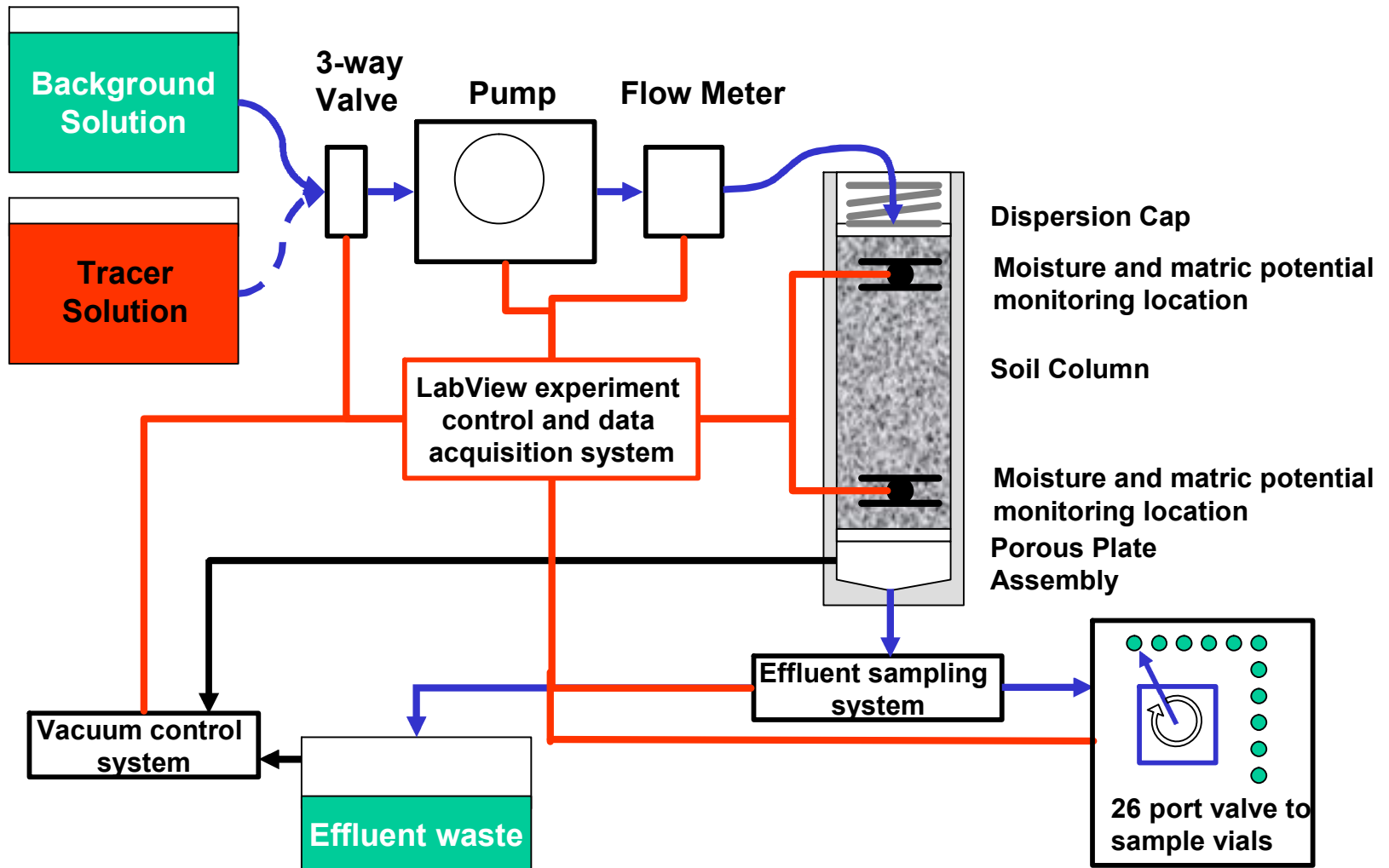
$$\frac{2Ro}{r^* / u^*} = \frac{2u}{\omega r} \ll 1$$

# Coriolis Effects

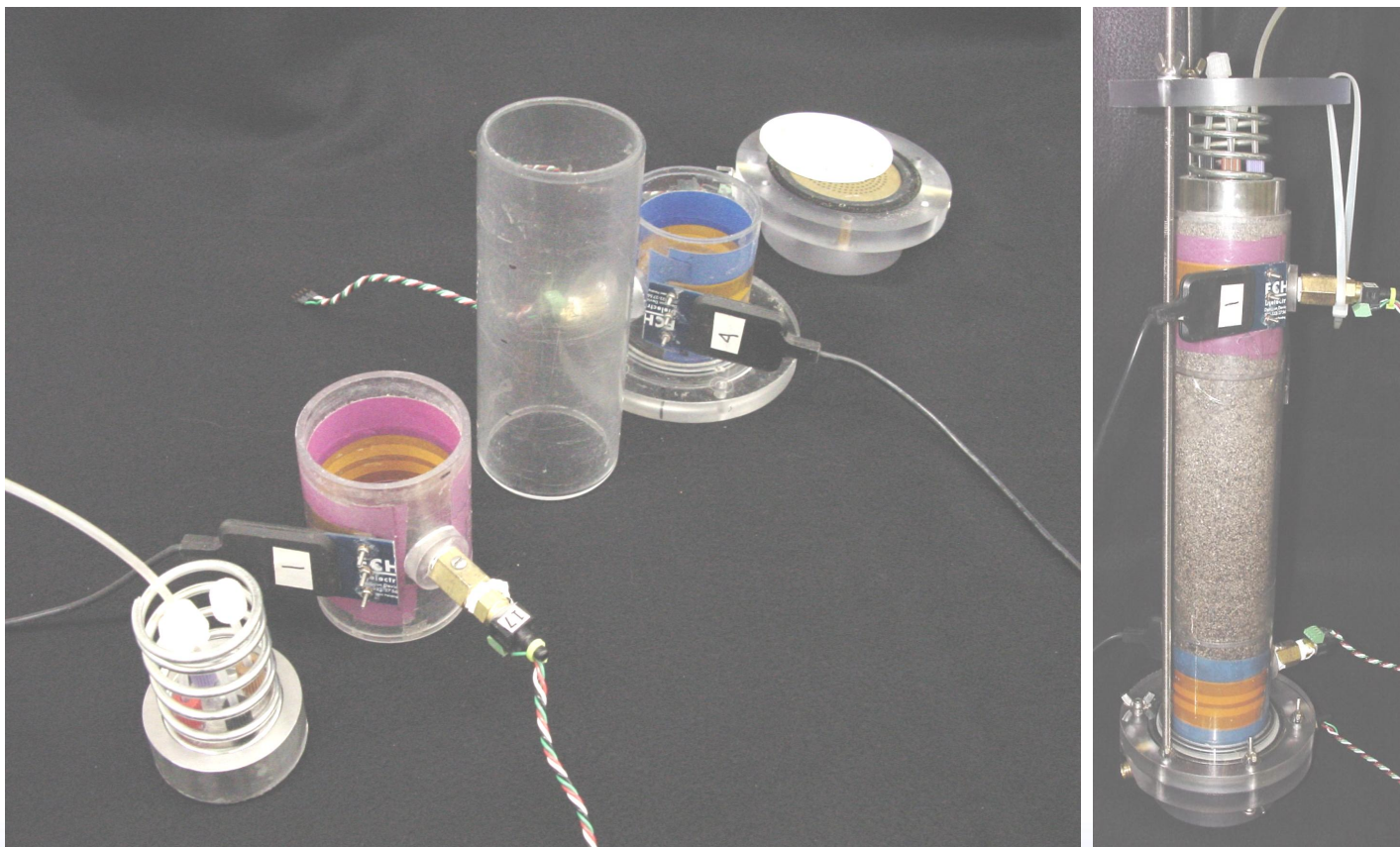




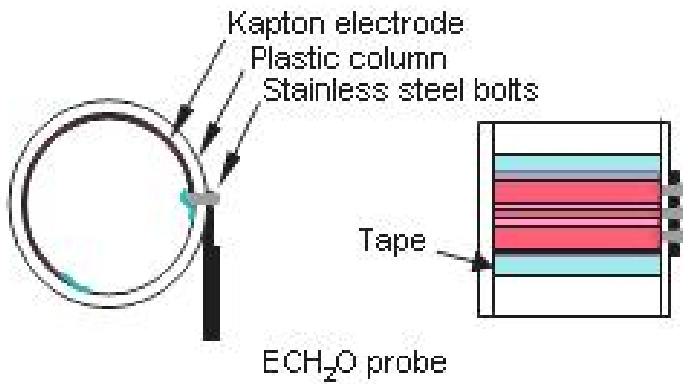
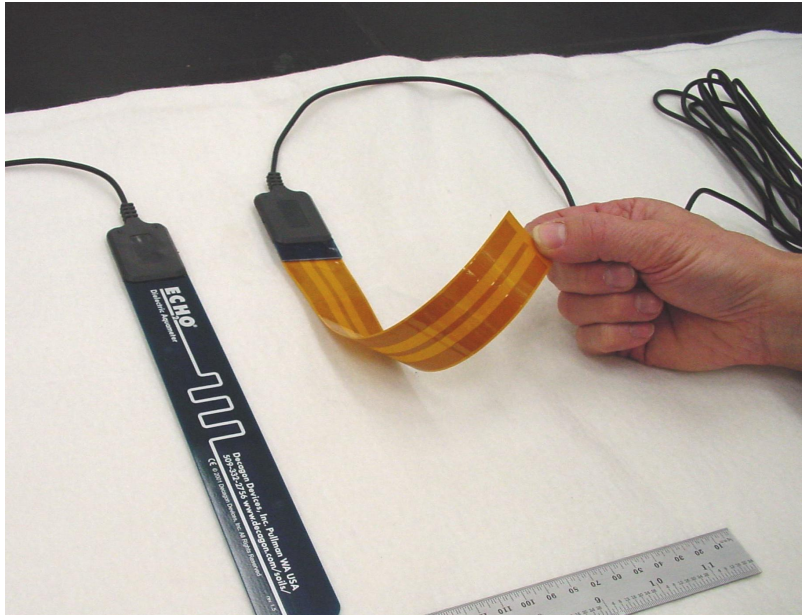
# Column Design Schematic



# Columns



# New Flexible Moisture Probe Design



a)

b)

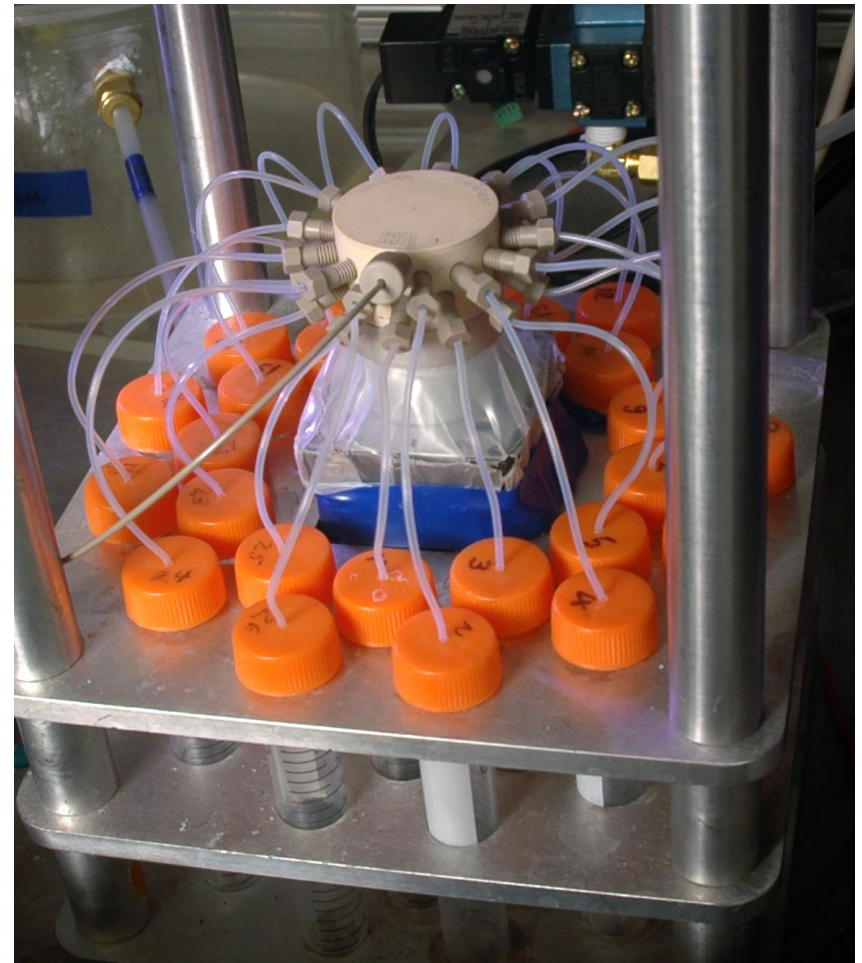
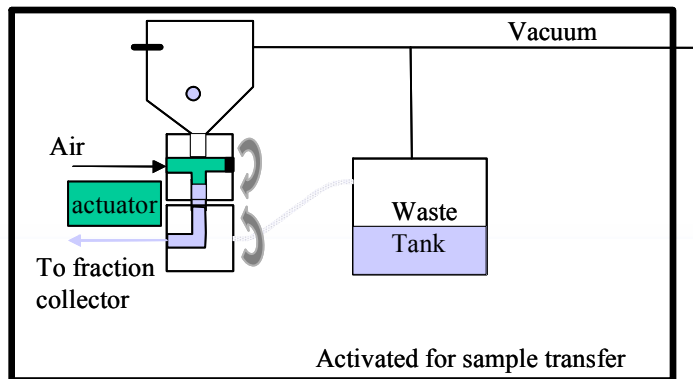
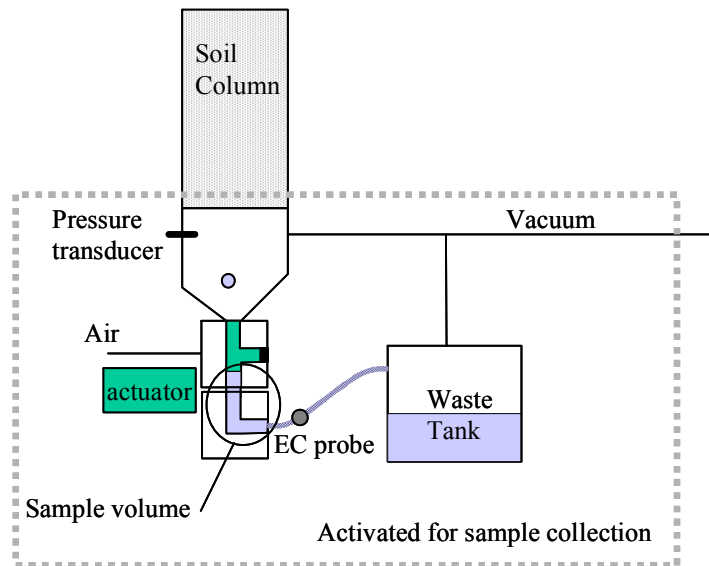


c)

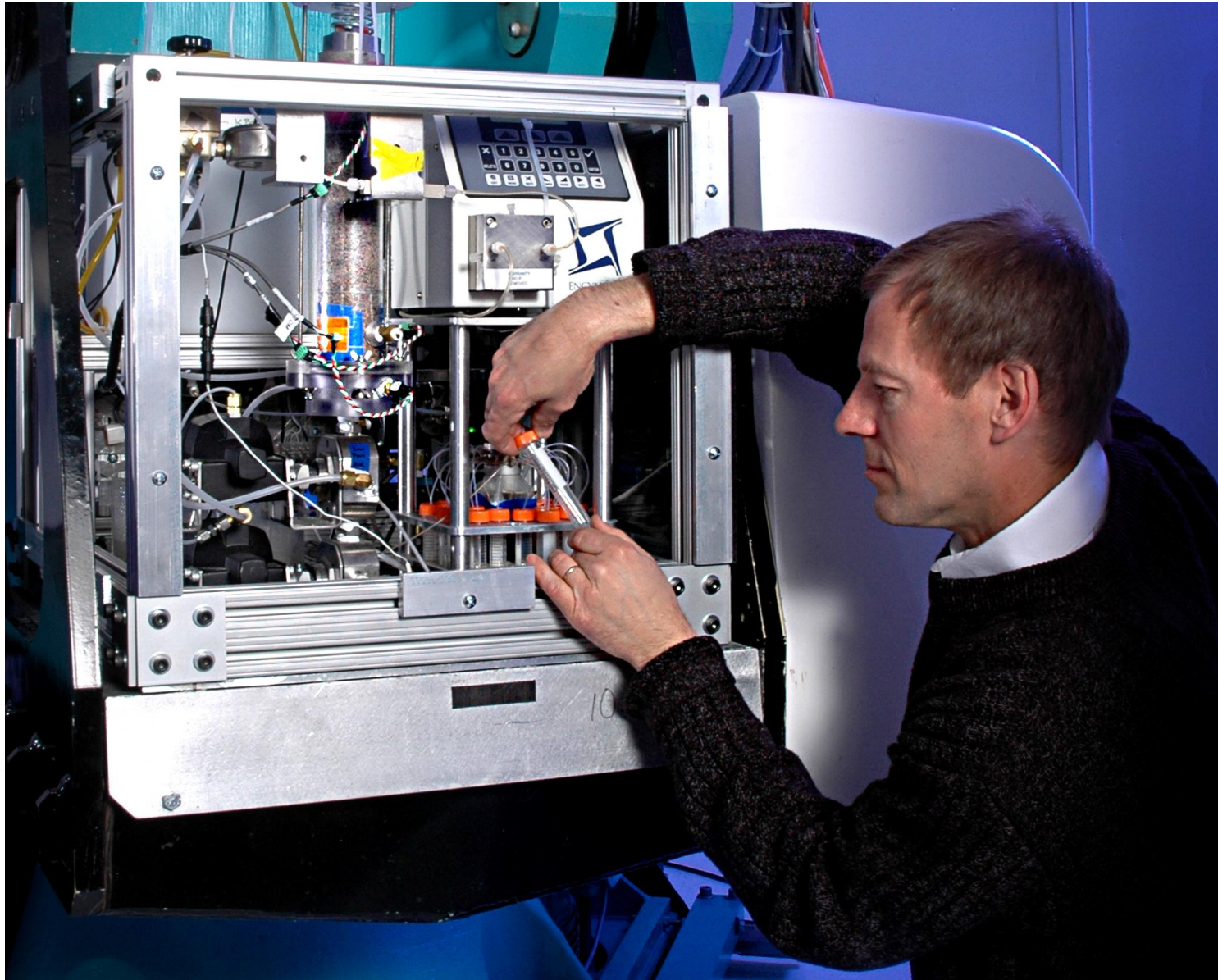


d)

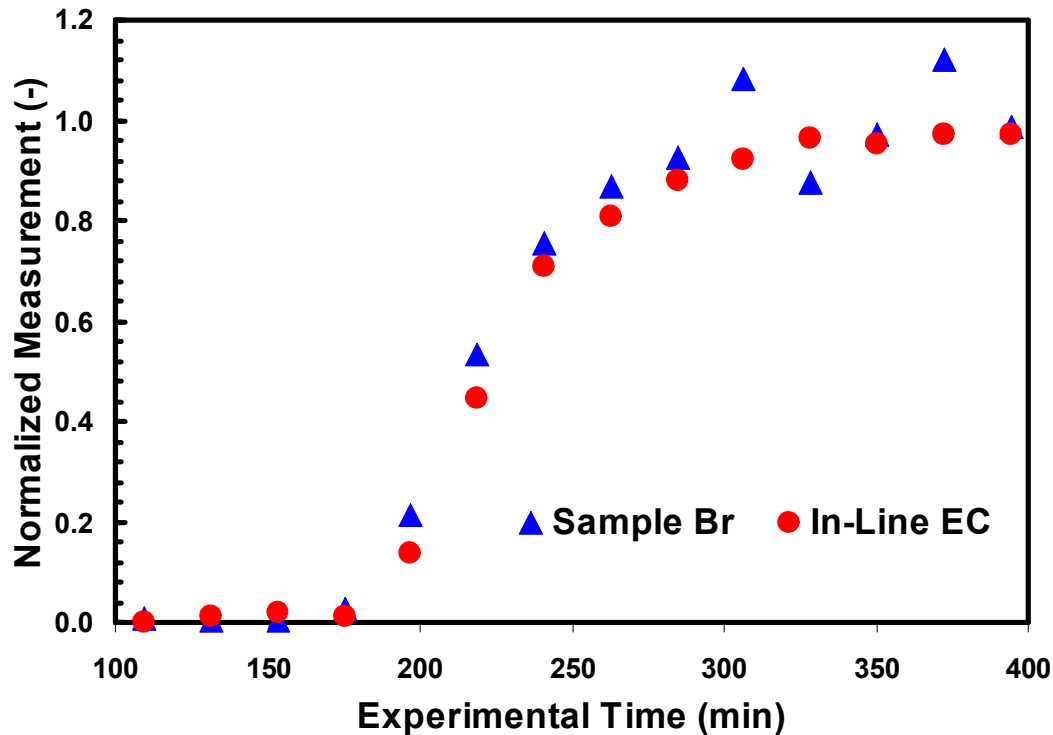
# Fraction Collector Designed to withstand High Accelerations



# Column Experiments

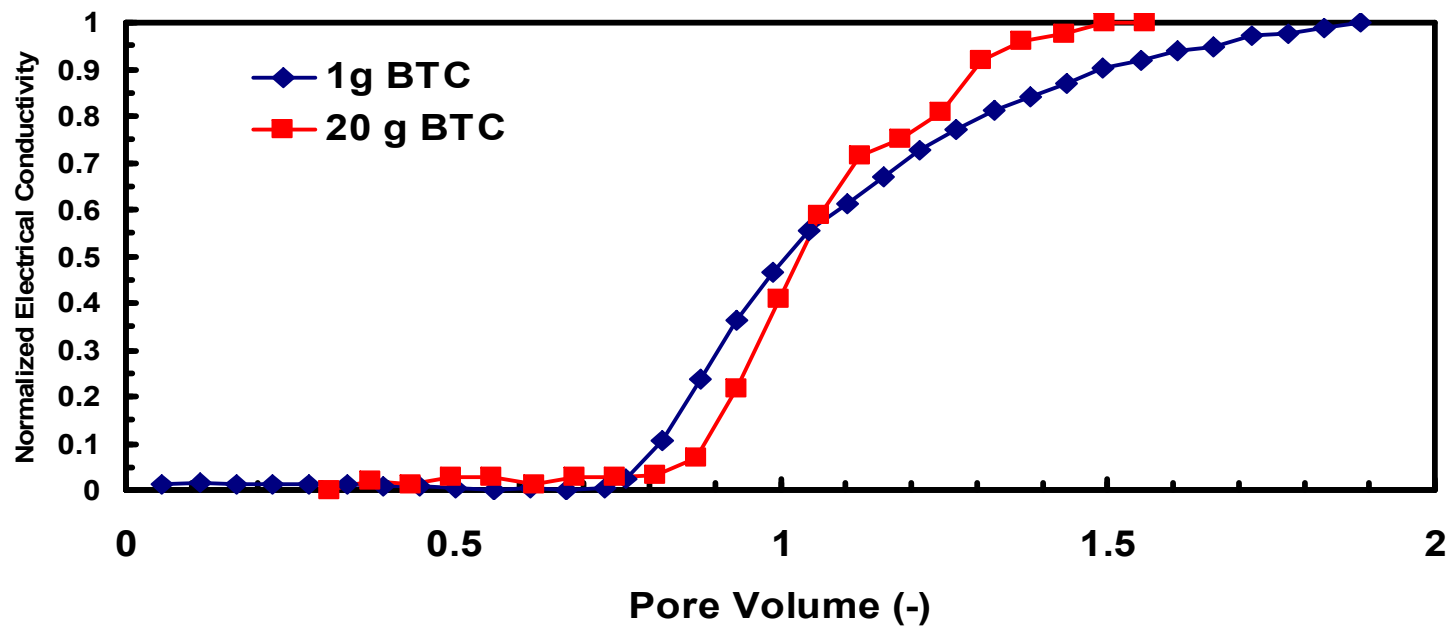
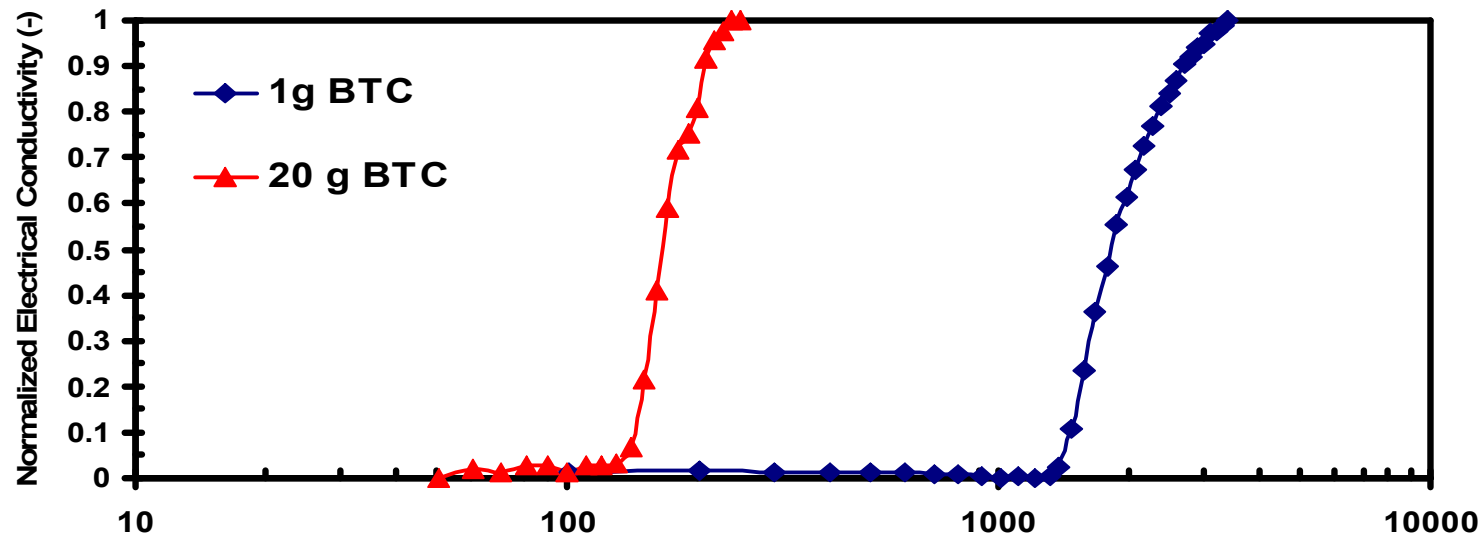


# Column Experiments

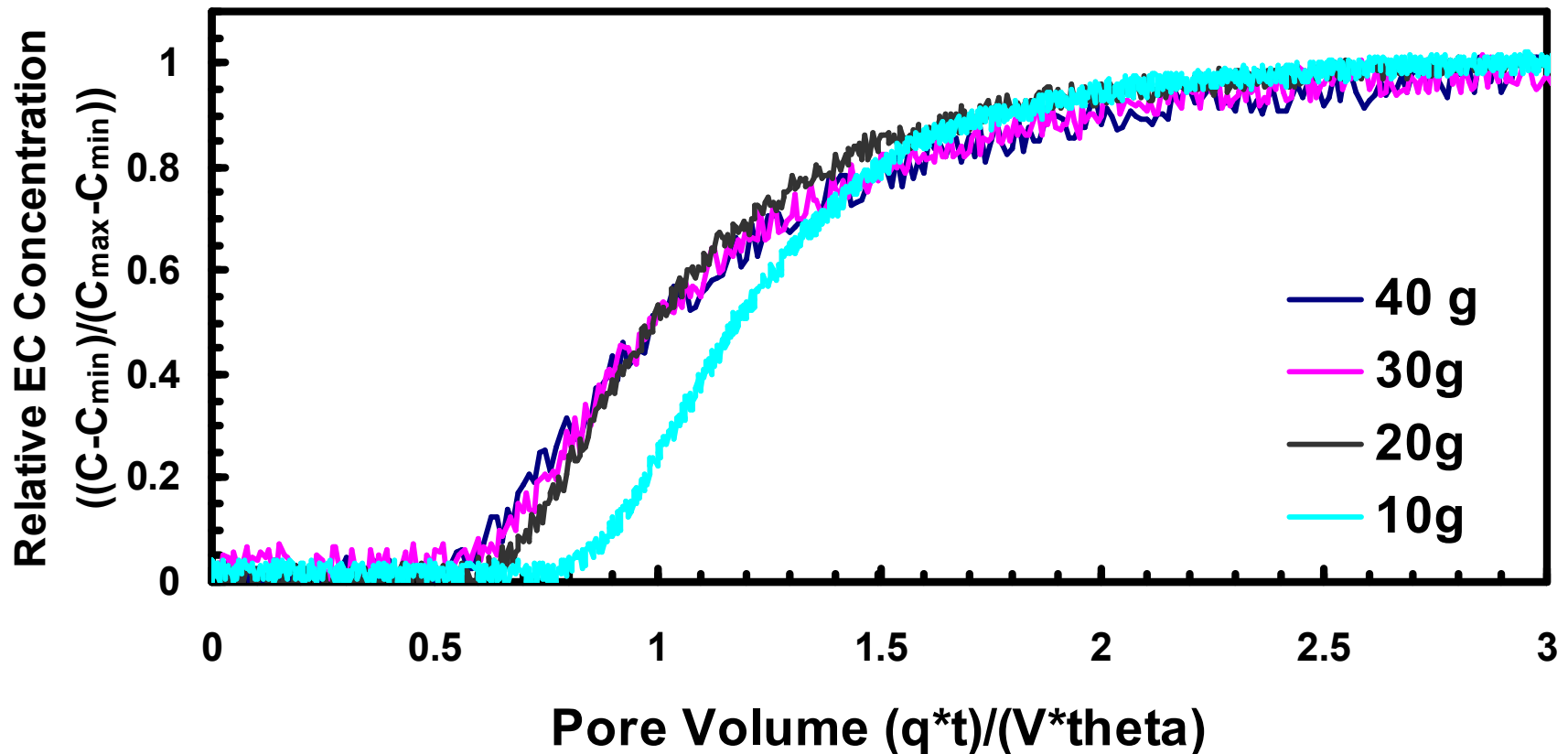


	Analysis of Normalized Br effluent sample concentrations	Analysis of Normalized in-line electrical conductivity measurements
Regressed velocity (cm min <sup>-1</sup> )	0.140	0.135
Regressed dispersion (cm <sup>2</sup> min <sup>-1</sup> )	0.0437	0.0517

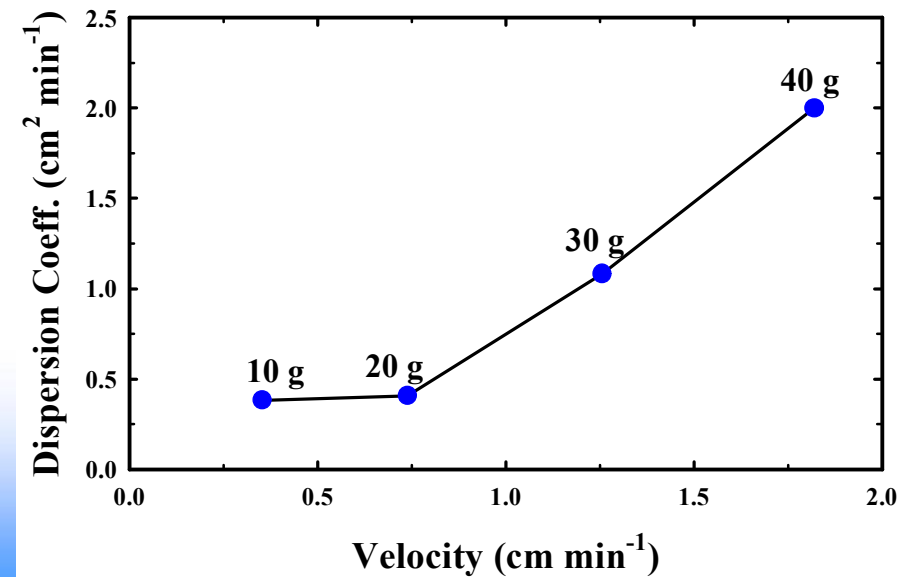
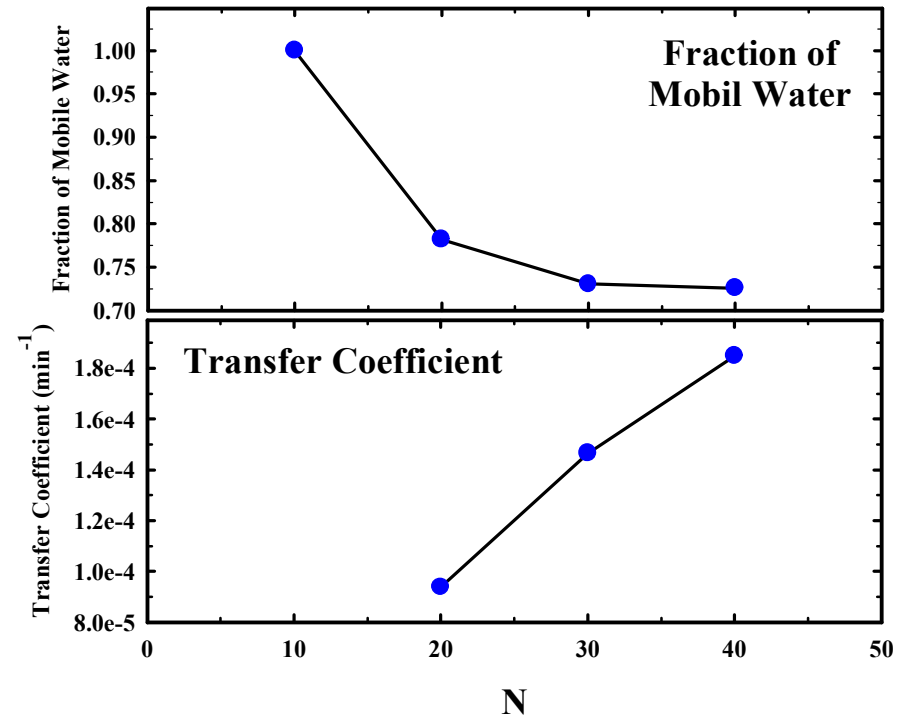
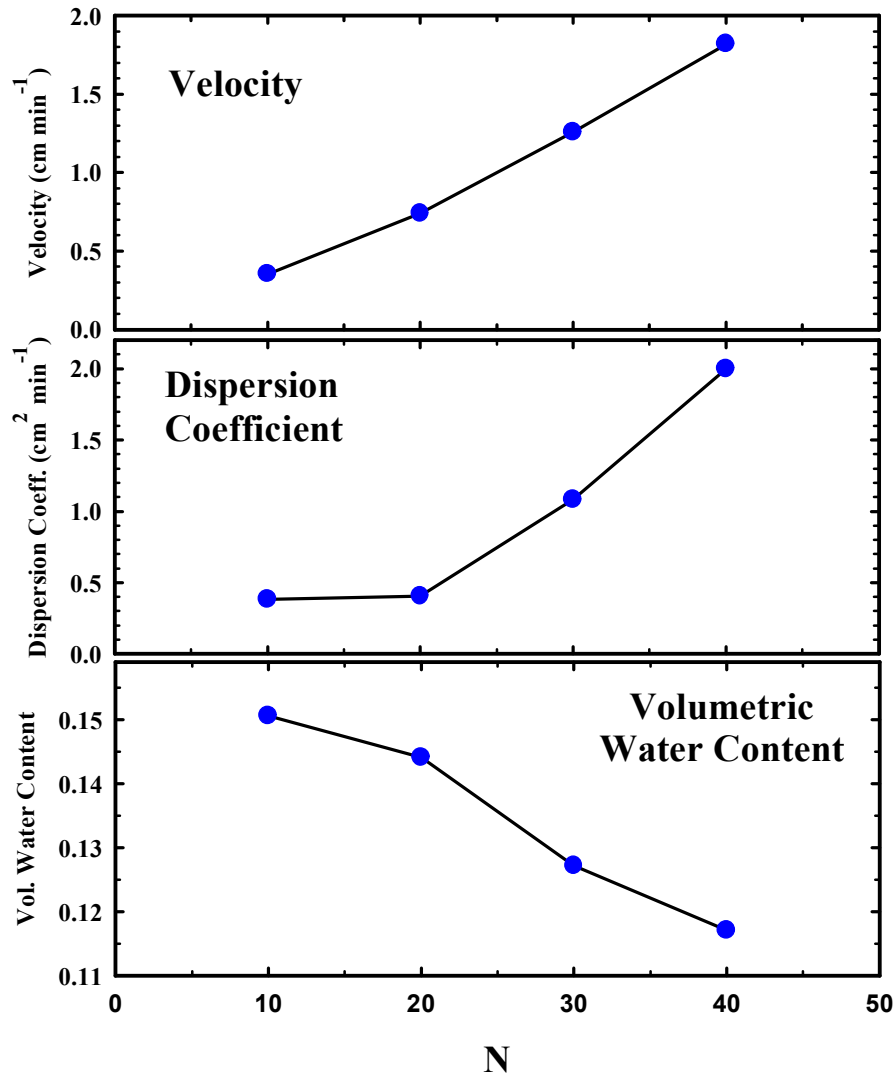
# Comparison of 20-g and 1-g Experiments



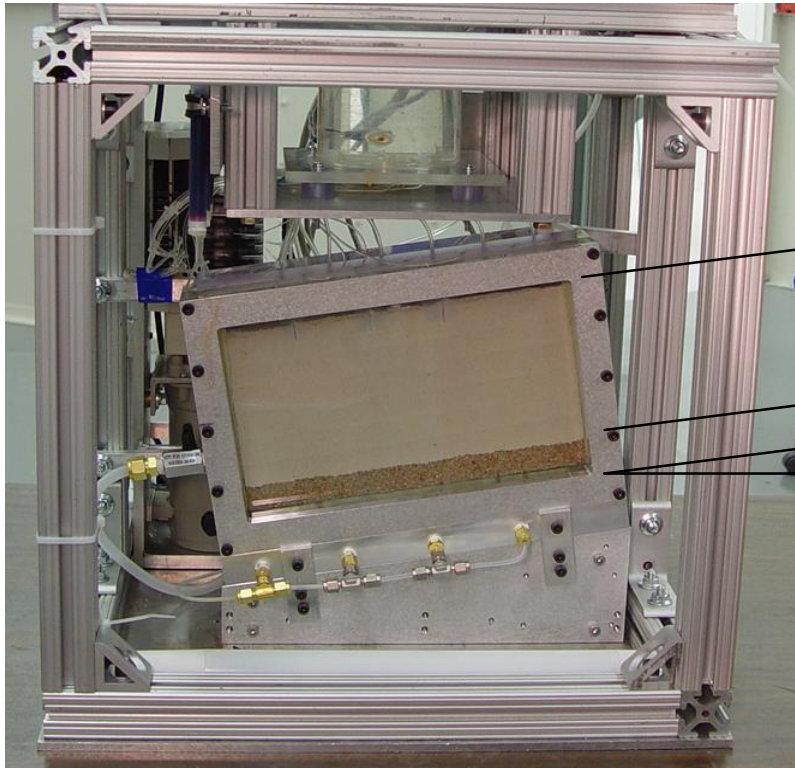
# Column Experiments





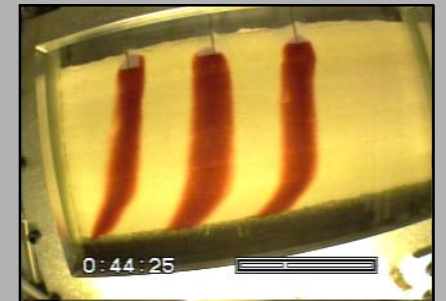
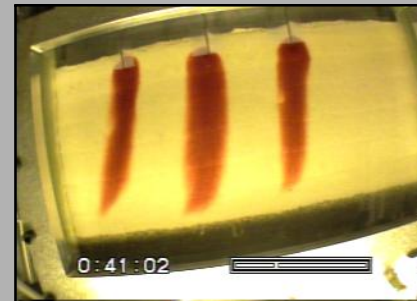
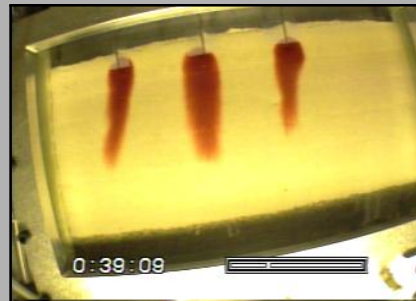
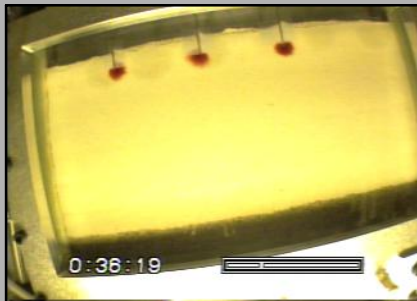


# Capillary Barrier Studies



Fine soil

Coarse soil  
90°



# Summary

- **Developed theoretical background that serves as a basis for improved design, interpretation, and simulation of experiments**
  - fluid potential,
  - pressure, pressure head, & hydraulic head in centrifugal field,
  - specific discharge,
  - Coriolis effects,
- **Advanced techniques needed to conduct in-flight sampling and monitoring on the geocentrifuge,**
  - Improved moisture probes,
  - fraction collector for geocentrifuge,
  - general experimental setups for geocentrifuge
- **Conducted experiments that demonstrate that the geocentrifuge technique is a viable experimental method for the study of subsurface processes where gravitational acceleration is important**

# Summary

## Key Advantages of Geocentrifuge Approach:

- Decrease time required to complete an experiment compared to 1g experiments.
- Obtain spatial scaling real-world problems according to the acceleration.
- Study a wider range of conditions than is capable under 1g acceleration.

# Coriolis Effects

