

IBS in a CAM-Dominated Electron Beam

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Abstract. Electron cooling of the 8.9 GeV/c antiprotons in the Recycler ring requires high-quality dc electron beam with the current of several hundred mA and the kinetic energy of 4.3 MeV. That high electron current is attained through beam recirculation (charge recovery). The primary current path is from the magnetized cathode at high voltage terminal to the ground, where the electron beam interacts with the antiproton beam and cooling takes place, and then to the collector in the terminal. The energy distribution function of the electron beam at the collector determines the required collector energy acceptance. Multiple and single intra-beam scattering as well as the dissipation of density micro-fluctuations during the beam transport are studied as factors forming a core and tails of the electron energy distribution. For parameters of the Fermilab electron cooler, the single intra-beam scattering (Touschek effect) is found to be of the most importance.

Keywords: Touschek effect, coupled optics, canonical angular momentum.

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INTRODUCTION

In the Fermilab e-cooler¹, energy distribution of the electrons at the collector affects the current loss and, consequently, possibility of operations in the DC mode. Core of the energy distribution is formed by multiple intra-beam scattering (IBS), as well as the dissipation of density micro-fluctuations. Extended tails of the electron energy distribution, significant for the charge recovery, are formed by single IBS, or Touschek effect. Because the electron beam is CAM-dominated²; conventional IBS results (as Bjorken-Mtingwa, Piwinski-Martini) cannot be applied. Both multiple and single IBS phenomena are treated here on a base of the Landau collision integral³; the present paper is a more extended and refined version of Ref.⁴.

Parameter	Symbol	Value	Units
Beam current	I_e	0.1-0.5	A
Electron momentum	p	4.8	MeV/c
Cathode radius	r_c	0.38	cm
Electron temperature at the cathode	T_c	0.11	eV
Length of trajectory	l	99	m
Collector potential with respect to the cathode	U_{coll}	2 – 4	kV
Longitudinal magnetic field on the cathode	B_c	90	G

CORE OF THE DISTRIBUTION

An electron with a longitudinal velocity $v_{\parallel} \ll c$ in the beam frame has the energy deviation $U = pv_{\parallel} = \mathbf{g}bmcv_{\parallel}$ in the laboratory frame. This value is not changed by acceleration and deceleration; thus, according to kinematics, the beam longitudinal temperature $T_{\parallel} \equiv \overline{mv_{\parallel}^2} \cong mT_c^2 / p^2$ gets to be extremely small with the acceleration.

IBS transfers high transverse temperature of electrons, which is not changed by the acceleration, to low longitudinal temperature; the evolution of the longitudinal distribution is described by the Landau kinetic equation³. When $T_{\parallel} \ll T_{\perp}$, the kinetic equation on the longitudinal distribution function $f_{\parallel}(v_{\parallel})$ reduces to a pure diffusion with the diffusion coefficient independent on the longitudinal velocity:

$$\frac{\partial f_{\parallel}}{\partial t} = \frac{D}{2} \frac{\partial^2 f_{\parallel}}{\partial v_{\parallel}^2}, \quad D = 4pn_e r_e^2 c^4 L_c \iint d^2 \mathbf{v} d^2 \mathbf{v}' \frac{f_{\perp}(\mathbf{v}) f_{\perp}(\mathbf{v}')}{|\mathbf{v} - \mathbf{v}'|}. \quad (1)$$

Here \mathbf{v} is 2D transverse velocity vector, and the electron density n_e is supposed to be constant (Pierce regime) over the elliptic cross-section with half-axes a_x, a_h . Assuming the transverse distribution $f_{\perp}(\mathbf{v})$ to be Gaussian with main axes r. m. s. velocities $\overline{v_x^2}, \overline{v_y^2}$, it yields

$$D = \frac{2p^{3/2} n_e r_e^2 c^4 L_c}{\sqrt{\overline{v_x^2} \overline{v_y^2}}} \int_0^{2p} dj \frac{1}{2p \sqrt{\frac{\cos^2 j}{\overline{v_x^2}} + \frac{\sin^2 j}{\overline{v_y^2}}}}. \quad (2)$$

At the end of the transfer line, beam acquires energy spread given by an integral over the beam line:

$$\overline{U_{IBS}^2} = \frac{2\sqrt{p} I_e r_e^2 L_c}{ec^2 \mathbf{e}_{4n}} (mc^2)^2 \int_0^l dz \int_0^{2p} dj \frac{1}{2p \sqrt{\frac{\cos^2 j}{\overline{v_x^2}} + \frac{\sin^2 j}{\overline{v_y^2}}}}, \quad (3)$$

where $\mathbf{e}_{4n} = a_x a_h \sqrt{\overline{v_x^2} \overline{v_y^2}}$ is a normalized 4D emittance, $L_c = \ln(r_{\max}/r_{\min})$ is the Coulomb logarithm. For the design optics⁵, this yields $\sqrt{\overline{U_{IBS}^2}} \approx 75$ eV.

Another source of longitudinal temperature growth is dissipation of density fluctuations in the beam. Excessive potential energy (beam frame) $U_{exc} \approx 2e^2 n^{1/3}$ (see Ref⁶) transforms into the r. m. s. energy spread

$$\overline{U_{DF}^2} \cong 2(\mathbf{g}b)^{5/3} r_e \left(\frac{I_e}{p e c a_e^2} \right)^{1/3} (mc^2)^2.$$

For $I_e = 0.2$ A, this yields $\sqrt{U_{DF}^2} \cong 50$ eV, and $\sqrt{U^2} = \sqrt{U_{IBS}^2 + U_{DF}^2} = 90$ eV.

TAILS OF THE DISTRIBUTION

A portion of particles $\Delta(U)$ which energy deviation exceeds a given collector potential U is referred here as losses. Losses as low as $\Delta(U) = 10^{-6}$ correspond to $U = 4.75\sqrt{U^2} = 430$ V low-energy tail of the Gaussian distribution $f(U)$. However, when the loss level is so small, it is determined rather by single scatterings (Touschek), than by multiple ones. In non-relativistic case, the Rutherford differential cross-section gives a cross-section for events when one of the scattering particles acquires longitudinal velocity larger than $v_{||}$, assuming v_0 as a relative velocity:

$$\mathbf{s}(v_0, v_{||}) = \int_0^{2p} d\mathbf{j} \cdot 2 \int_0^{\arccos(2v_{||}/v_0)} \frac{d\mathbf{s}}{do} \sin \mathbf{q} d\mathbf{q} = \frac{4pr_e^2 c^4}{v_0^2 v_{||}^2} \left(1 - \frac{4v_{||}^2}{v_0^2} \right). \quad (4)$$

The instantaneous loss rate in the beam frame is

$$\frac{1}{n_e} \frac{dn_e}{dt} = \frac{n_e}{2} \int dv dv' \mathbf{s}(|\mathbf{v} - \mathbf{v}'|, v_{||}) |\mathbf{v} - \mathbf{v}'| f_{\perp}(\mathbf{v}) f_{\perp}(\mathbf{v}').$$

For the Gaussian transverse distribution, the above 4D integral reduces to a single integral

$$\Delta(U) = \frac{\sqrt{p} I_e r_e^2 L_c}{ec^2 e_{4n}} \left(\frac{mc^2}{U} \right)^2 \int_0^l dz \int_0^{2p} d\mathbf{j} \frac{S(\Xi(\mathbf{j}))}{\sqrt{\frac{\cos^2 \mathbf{j}}{v_x^2} + \frac{\sin^2 \mathbf{j}}{v_y^2}}} \quad (5)$$

$$\Xi(\mathbf{f}) = \frac{U}{p} \sqrt{\frac{\cos^2 \mathbf{f}}{v_x^2} + \frac{\sin^2 \mathbf{f}}{v_y^2}}, \quad S(x) = (1 + 2x^2) \operatorname{erfc}(x) - \frac{2x}{\sqrt{p}} \exp(-x^2).$$

For the 99 m long cooling line, the losses vary moderately (<50%) for drastically different beam envelopes. For the short U-bend line⁷, the calculated dependence on the envelope is much stronger. Increase of the beam size leads to significant drop of the losses. Fig. 1 shows calculated (line) and measured (dots) dependences of the beam losses versus the collector potential for design optics of the cooling line (left) and the U-bend line (right). For the cooling line, the growing discrepancy at high voltage is thought to be caused by secondary electrons escaped from the collector.

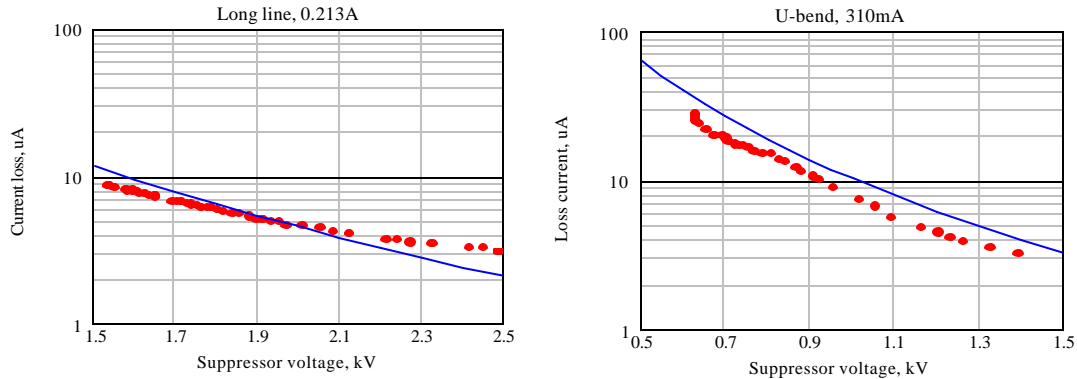


FIGURE 1. Measured and calculated current loss in long line (0.213A) and U-bend (0.310A)

CONCLUSIONS

1. Single IBS places a limitation for the minimum collector voltage U_{coll} . Acceptable level of losses of $\Delta = 2.5 \cdot 10^{-6}$ corresponds to the minimum value of $U_{coll} = 2$ kV.
2. The r.m.s. energy spread of the beam due to the multiple IBS is below the acceptable limit for the electron cooling process.
3. Tails of the multiple IBS Gaussian distribution are insignificant in comparison with the single large-angle IBS tails.
4. Any increase of the beam size is beneficial for both the multiple and single IBS as it leads to a lower transverse temperature and lower beam density.
5. Loss dependence on the envelope seems to be weak in the long line and very strong in the U-bend.
6. Geometrical beam parameters are obtained using 4D formalism for coupled optics.

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APPENDIX: PRINCIPAL AXES OF THE BEAM DISTRIBUTION

Geometrical beam parameters can be calculated via generalized Twiss functions for coupled optics⁸. All functions for the simulation were calculated by OptiM code⁹. Particle coordinate vector can be represented through the linear combination of two complex vectors $\hat{\mathbf{v}}_1(s)$ and $\hat{\mathbf{v}}_2(s)$ satisfying the equation $\mathbf{M}(s|s')\hat{\mathbf{v}}_i(s) = e^{im(s,s')}\hat{\mathbf{v}}_i(s')$.

$$\hat{\mathbf{x}}(s) = \text{Re}(\sqrt{2I_1}e^{-iy_1}\hat{\mathbf{v}}_1(s) + \sqrt{2I_2}e^{-iy_2}\hat{\mathbf{v}}_2(s))$$

$$\hat{\mathbf{x}} = \begin{pmatrix} x(s) \\ x'(s) - \frac{eB_s}{2pc}y(s) \\ y(s) \\ y'(s) + \frac{eB_s}{2pc}x(s) \end{pmatrix}, \quad \hat{\mathbf{v}}_1 = \begin{pmatrix} \sqrt{b_{1x}(s)} \\ \frac{i(1-u(s)) + \mathbf{a}_{1x}(s)}{\sqrt{b_{1x}(s)}} \\ \sqrt{b_{1y}(s)}e^{in_1(s)} \\ \frac{i(1-u(s)) + \mathbf{a}_{1y}(s)}{\sqrt{b_{1y}(s)}}e^{in_1(s)} \end{pmatrix}, \quad \hat{\mathbf{v}}_2 = \begin{pmatrix} \sqrt{b_{2x}(s)}e^{in_2(s)} \\ \frac{i(1-u(s)) + \mathbf{a}_{2x}(s)}{\sqrt{b_{2x}(s)}}e^{in_2(s)} \\ \sqrt{b_{2y}(s)} \\ \frac{i(1-u(s)) + \mathbf{a}_{2y}(s)}{\sqrt{b_{2y}(s)}} \end{pmatrix}$$

B_s is longitudinal magnetic field, I_i , y_i are new canonical variables, actions and phases for the two transverse modes. Defining emittances (un-normalized) as $e_1=2I_{1\max}$, $e_2=\langle I_2 \rangle$, the 4D emittance $\mathbf{e}_T = r_c\sqrt{mT_c}/p$ is a product of two emittances defined above⁸: $\mathbf{e}_T^2 = \mathbf{e}_1\mathbf{e}_2$ with

$$\mathbf{e}_1 = \frac{B_c r_c^2}{B\mathbf{r}}, \quad \mathbf{e}_2 = \frac{mcT_c}{peB_c}, \quad \frac{\mathbf{e}_1}{\mathbf{e}_2} = \frac{B_c^2 r_c^2}{T_c mc^2} \approx 8 \cdot 10^3,$$

$B_c = pc/e = 16.2$ kG-cm for the 4.35 MeV electrons. Emittance e_1 corresponds to the total magnetic flux on the cathode and is responsible for the beam hydrodynamic motion and its shape. Emittance e_2 relates to the thermal velocities, driving intrabeam scattering. For the hydrodynamic mode, $x = \sqrt{2I_1 b_{1x}} \cos y_1$ and $y = \sqrt{2I_1 b_{1y}} \cos(n_1 - y_1)$, yielding the half-axes $a_{x,y}$, the beam cross-section S , and the axes tilt angle \mathbf{j}_1 :

$$a_{x,h}^2 = I_1[(b_{1x} + b_{1y}) \pm \sqrt{b_{1x}^2 + 2b_{1x}b_{1y}\cos 2n_1 + b_{1y}^2}] \quad (6)$$

$$S = pe_1\sqrt{b_{1x}b_{1y}}|\sin n_1|, \quad \text{tg} 2\mathbf{j}_1 = \frac{2\sqrt{b_{1x}b_{1y}}\cos n_1}{b_{1y} - b_{1x}}.$$

Emittance of the thermal mode \mathbf{e}_2 determines the r.m.s. transverse velocities in the beam frame in \mathbf{j}_2 -tilted principal axes

$$\overline{v_{\bar{x},\bar{y}}^2} = \frac{B\mathbf{r}}{B_c I_{\bar{x},\bar{y}}} \frac{T_c}{mc^2}, \quad I_{\bar{x},\bar{y}} = \frac{1}{2}[(b_{2x} + b_{2y}) \pm \sqrt{b_{2x}^2 + 2b_{2x}b_{2y}\cos 2n_2 + b_{2y}^2}]$$

$$\text{tg} 2\mathbf{j}_2 = \frac{2\sqrt{b_{2x}b_{2y}}\cos n_2}{b_{2y} - b_{2x}}.$$