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M. R. Borden, J. A. Folta, C. J. Stolz, J. R. Taylor,
J. E. Wolfe, A. J. Griffin, M. D. Thomas

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Improved Method for Laser Damage Testing Coated Optics

Michael R. Borden*^a, James A. Folta^a, Christopher J. Stolz^a,

John R. Taylor^a, Justin E. Wolfe^a, Andrew J. Griffin^b, Michael D. Thomas^b

^aUniversity of California, Lawrence Livermore National Laboratory, Livermore, CA 94550;

^bSpica Technologies Inc., Hollis, NH 03049

ABSTRACT

The damage test procedure for qualifying a coating run of anti-reflection coated optics consists of scanning a pulsed 1064 nm laser over a 1 cm x 1 cm area on a test sample to illuminate approximately 2400 sites. Scans are repeated at 3 J/cm² increments until the fluence specification for the optic is reached. In the past, initiation of 1 or more damage sites was classified as a failed coating run, requiring the production optics in the corresponding coating lot be reworked and recoated. Recent laser damage growth tests of 300 repetitive pulses performed on numerous damage sites revealed that all were stable up to 20 J/cm². Therefore the acceptance criteria has been modified to allow a moderate number of damage sites, as long as they are smaller than the allowed dig size and are stable (do not grow). Consequently many coating runs that previously would have been rejected are now accepted, resulting in higher yield, lower cost, and improved delivery schedule. The new test also provides assurance that initiated damage sites are stable during long term operation.

Keywords: antireflection coating, laser damage, initiation, growth.

1. INTRODUCTION

The National Ignition Facility (NIF) project is in the production phase of procuring approximately 25,000 small optics (<20 cm) that will be used in the main beamlines and diagnostic systems¹. Of these, roughly 8,000 will be exposed to beam fluences high enough to warrant a laser damage specification for the optical coatings. A laser damage test employing a raster scan of a 1mm (1/e²) spot size beam at a wavelength of 1064 nm was developed to provide the quality assurance that optics from particular coating lots will not damage in use, as well as to qualify coating vendors and perform process control monitoring. This test, which involves illuminating approximately 2400 sites at each fluence level, has been shown to find the damage sites that would initiate at the lowest fluences more readily than alternative damage tests such as ISO 10110-13².

The requirement that a particular coating would “pass” the laser damage test has heretofore been limited to those coatings with no damage sites when tested up to the specification fluence. This requirement has resulted in the rejection of numerous coating runs. Of particular concern was rejection of optic coating runs for which the damage test initiated only a few damage sites, especially when tests on different areas on the same sample provided different results. For example, Figure 1 shows damage test results at 2 locations on the same optic: location A would have failed a specification of 13 J/cm² with 2 damage sites, yet location B would have passed. The authors desired a test which would provide more information for the lot acceptance decision, either that the coating run was of insufficient quality or that the run would reliably withstand the required fluence.

In particular, antireflection coatings have been difficult to obtain consistently with no damage sites at the specification fluence. This is believed to be due to absorbing defects at the substrate and coating interface³. The production of anti-reflected coated optics is complicated by the fact that the coating runs on both sides must pass to yield usable optics.

In order to mitigate this concern, a new test protocol has been developed, tested, and implemented into production. The new testing protocol allows up to 10 damage sites providing they are stable (do not grow) upon subsequent exposure to laser fluences up to the specification fluence. The approach of allowing stable damage sites is consistent with the concepts of a functional damage threshold⁴ and conditioning large optic (>40 cm) mirrors for NIF⁵.

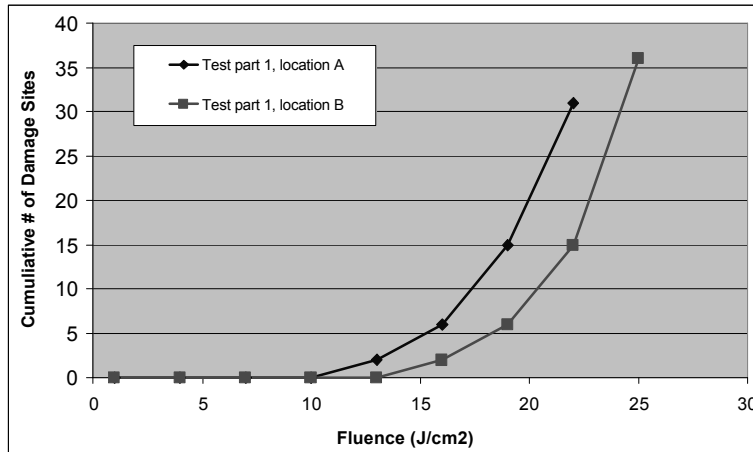


Figure 1. Plot of 2 separate damage test results for different areas tested on the same part. Note the test at location A would result in the coating run failing a damage specification of 13 J/cm² since 2 damage sites occurred, yet the test at location B would result in the coating passing the same 13 J/cm² specification.

2. EXPERIMENTAL

2.1 Damage Test System

The NIF Small Optics laser damage test system currently employed at Spica is shown in Figure 2 (A recently qualified NIF small optics laser damage test system developed by Research Electro-Optics is the subject of another paper in these proceedings)⁶ The system employs a Q-switched 1064 nm Nd:YAG laser with a pulsewidth of 3.5 ns, and repetition rate of 10 Hz. The $1/e^2$ spot size is nominally 1 mm.

Damage is detected with an in-situ scatter-based diagnostic. A HeNe laser is co-aligned such that it overlaps the test beam at the test sample surface. The scatter signal is detected with a CCD camera and 40X magnification. The system operator views the scatter signal in real-time on a CRT display. A DVD recorder is used to provide a back-up video for later playback, if necessary.

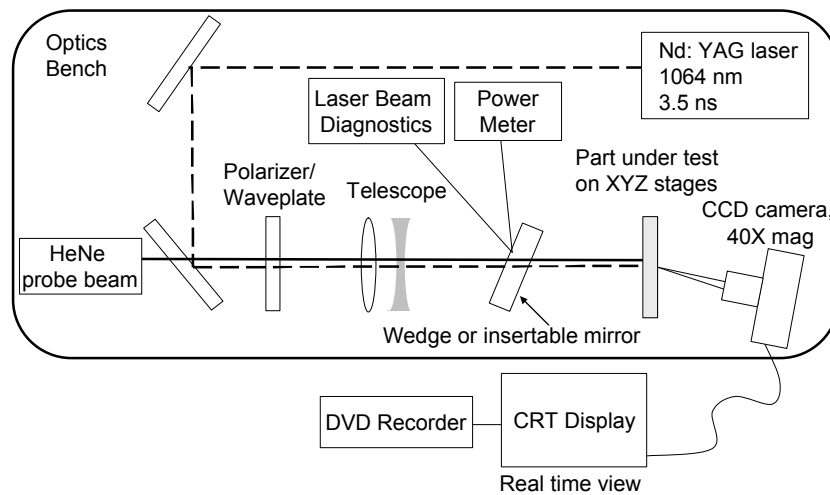


Figure 2. Schematic of the NIF Small Optics laser damage test system in operation at Spica Technologies.

2.2 Damage Test Procedure

The authors believe that damage initiation at isolated defect sites limit the fluence at which an optic can be reliably used. Therefore a large number of test sites are exposed to find isolated defect sites, specifically at the lowest fluence levels at which they would initiate damage. The optic under test is moved with a set of XY stages such that the pulsed laser beam scans a 1 cm x 1 cm area in a serpentine fashion (see Figure 3). The stage velocities are timed such that there is a beam overlap at 90% of the peak fluence (see Figure 4). This results in approximately 2400 spots being tested at a fluence at least 90% of the peak fluence over the entire test area. Mirror and polarizer coatings are tested on the input surface, while anti-reflection coatings are typically tested on the output surface. The typical area tested of 1 cm² per run represents a small fraction of the area of optics being coated; the ratio of the coated area to the tested area varies from 15:1 for the smallest lots to as high as 2400:1 for larger vacuum windows. Testing a larger fraction of the area is cost prohibitive.

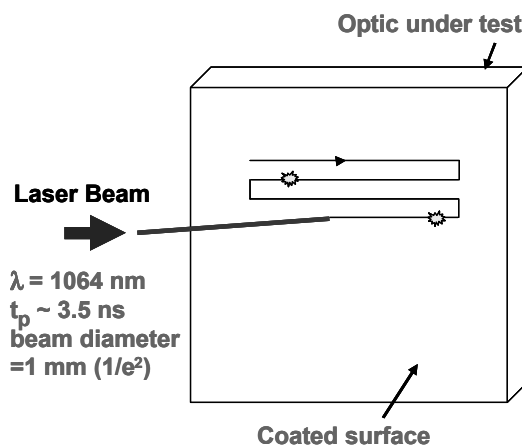


Figure 3. Schematic showing the laser damage test procedure for coated optics.

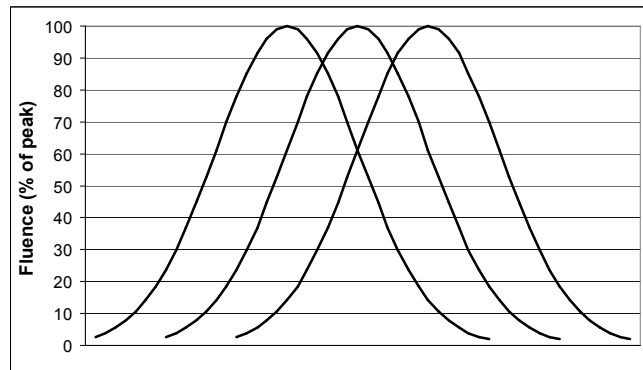


Figure 4. Beam overlap is at the 90% fluence level.

Each scan is performed at a single fluence. Subsequent scans are increased in 3 J/cm² increments. The first scan is performed at a fluence of 1, 2, or 3 J/cm² (selected such that a subsequent scan arrives exactly at the specification fluence). The test is continued at least until the specification fluence is reached.

2.3 Initial Tests for Damage Site Growth

An experiment was designed to elucidate the fluence at which damage sites would begin to grow on representative anti-reflection coated parts. Coated samples were scanned at increasing fluences as described earlier. However, after a damage site was initiated, the scans were stopped. The damage site was inspected with a microscope at 200X magnification to determine the damage site size. The optic was positioned such that the damage site was in the beam, and it was subjected to an additional 300 laser pulses while the scatter signal from the HeNe beam was monitored for any increased scatter level that might indicate an increase in damage site size (damage “growth”). Any change to the site during the first 20 shots was considered cleanup and stabilization of the site, not growth (based on prior experience). Any increase in size occurring after the first 20 shots was considered growth. Following the additional pulses, the damage site size was rechecked with the microscope. If no growth occurred, the fluence was increased by 3 J/cm^2 and the damage site was exposed to an additional 300 shots. This process was continued until growth was deemed to have occurred, or an acceptably high test fluence was reached.

2.4 Implementing New Damage Test in Production

Since the new damage test protocol allowed some damage sites, there was some concern about how close the specification fluence was to the region where the damage sites increased rapidly with fluence (see Figure 1 for example, where the number of sites increased rapidly around 20 J/cm^2). Given the tolerance on test beam fluence of 15%, a sample that tested with 10 sites on the low side of the fluence tolerance may have many more defect sites at the actual specification fluence. Therefore an additional 3 J/cm^2 scan was added to the damage test fluence requirement. The scans would continue to the specification fluence, and then an additional scan would be performed at 3 J/cm^2 above the specification fluence.

A limit of 10 damage sites was selected based on prior experience with the size of the damage sites compared to the obscuration allowed due to scratches and digs in these optics (the area represented by 10 typical laser damage sites is about $1/3^{\text{rd}}$ that of the allowable dig area on a representative NIF small optic). If a total of 10 or fewer damage sites occurs, they would be tested for growth with 300 additional shots at the specification fluence. If no growth occurs on any of the sites, the coating would pass the new acceptance criteria.

3. RESULTS AND DISCUSSION

3.1 Damage Sites Growth Tests

The result of the tests to determine the fluences at which damage sites would begin to grow for test sample #1 is shown in Figure 5. In test sample #1, one site was initiated at a fluence of 7 J/cm^2 . Subsequent 300-pulse growth tests were continued until 28 J/cm^2 , the fluence at which the coating failed catastrophically. Therefore this site was exposed to at least 25 J/cm^2 without growth. Photomicrographs of a damage site after initiation and after the growth tests are shown in Figure 6. Additional initiation scans were conducted until another damage site occurred at 13 J/cm^2 . This site began to grow at a fluence of 25 J/cm^2 .

The results of the tests to determine the fluences at which damage sites would begin to grow for test sample #2 are shown in Figure 7. For test sample #2, one site was initiated at a fluence of 10 J/cm^2 . Subsequent growth tests were continued until 22 J/cm^2 , without any evidence of growth. An additional 3 additional damage sites occurred during a subsequent scan at 13 J/cm^2 . All 3 sites were exposed to the growth tests up to 22 J/cm^2 without any evidence of growth.

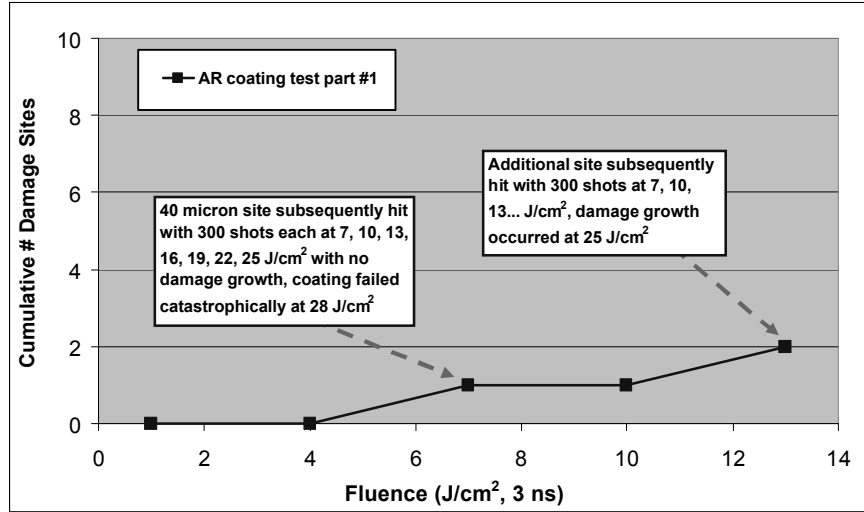


Figure 5. Results of damage site growth tests for anti-reflection coating test sample #1.

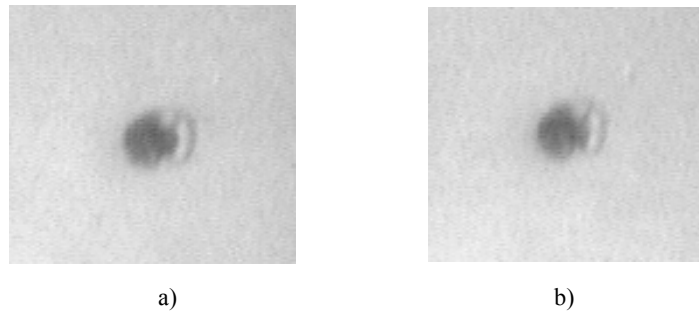


Figure 6. Example of a site tested for growth. Photographs show a nominal 15 micron diameter damage site: a) after initiation; and b) after subsequent exposure to an additional 300 shots at a fluence of 15 J/cm² and 3ns pulsewidth.

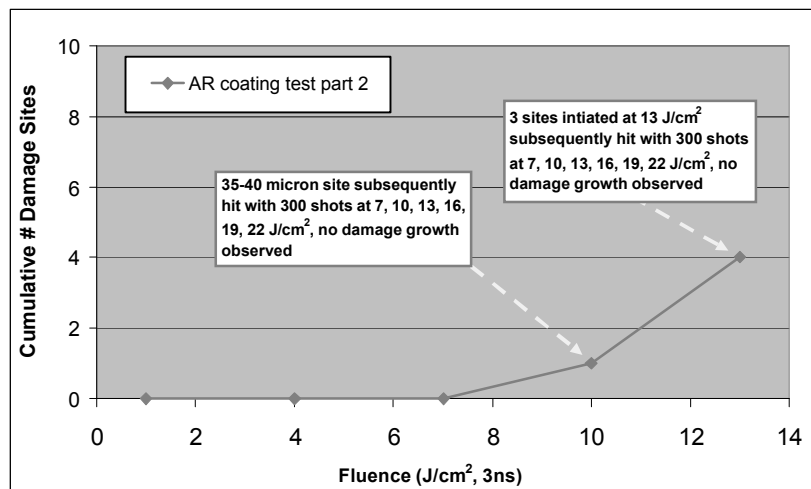


Figure 7. Results of damage site growth tests on anti-reflection coating test sample #2.

3.2 Impact of the New Test on Production Coatings

Numerous anti-reflection coatings with damage sites have been accepted since the new test protocol was implemented. Some of these are shown in Table 1.

Table 1. Damage test results for production coatings that were accepted with the new test protocol with a maximum of 10 stable damage sites. The damage sites that were tested for growth are shown in the grayed cells for clarity.

Fluence (J/cm ²)	Vendor B, BK7	Vendor D, silica	Vendor D, silica	Vendor B, BK7	Vendor B, BK7	Vendor B, BK7	Vendor B, BK7	Vendor B, silica	Vendor B, BK7	Fluence (J/cm ²)	Vendor A, boro-silicate glass	Vendor A, silica	Fluence (J/cm ²)	Vendor C	Vendor C	Vendor C, silica	Vendor B, silica optic	Vendor B	Vendor B
Specification	2	2	2	5	5	5	5	5	5		7	7		12	12	12	12	12	12
2	0	0	0	0	0	0	0	0	0	1	0	0	3	0	0	0	1	0	0
5	1	4	1	0	0	1	0	0	1	4	4	0	6	1	1	0	0	2	0
8				1	1	2	1	1	1	7	0	1	9	0	1	0	2	0	0
11										10	0	0	12	0	1	0	4	0	2
14													15	1	3	2	3	1	2
Number of Sites tested for Growth	1	4	1	1	1	3	1	1	2		4	1		1	6	2	10	3	4

These coating runs represent anti-reflection coatings from 4 different vendors. Both traditional electron beam and ion beam sputtered coatings are represented. The number of damage sites that were tested for growth are summarized at the bottom of each column. Confirmation that damage sites initiated during testing are not susceptible to growth provides increased assurance that the optics will meet NIF lifetime requirements. The authors are not making a universal claim that all damage sites on AR coatings do not grow at any fluence below 20 J/cm²; the fluence at which growth occurs depends upon substrate finishing, cleaning and coating procedures, and must therefore be determined for each supplier and manufacturing process.

3.3 Impact of New Specification on Coating Yield

Since implementation of the new damage test protocol occurred relatively recently, there is not sufficient data to allow extensive comparison of the yield improvement compared to the original test protocol. Therefore a set of approximately 30 anti-reflection coating damage data curves from one vendor was used to compare which coating runs would have passed with the 2 test procedures. The damage curves, which are plots of the cumulative number of damage sites at the various test fluences, are shown in Figure 8.

It was assumed that none of the damage sites would have exhibited growth up to 15 J/cm², which was believed to be a reasonable assumption since none of the sites have grown at these fluences to date. The comparison was performed for 3 typical NIF small optic damage specification fluences: 5, 7, and 12 J/cm².

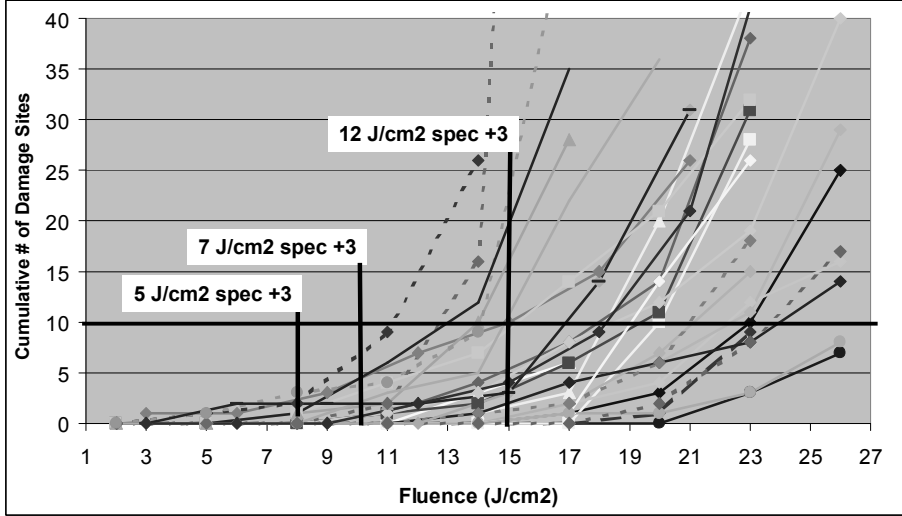


Figure 8. Damage test results for anti-reflection coatings from Vendor A. Three typical specification fluences of 5, 7, and 12 J/cm² were used to judge the yield impact of the new damage test protocol.

The results of the comparison are shown in Figure 9.

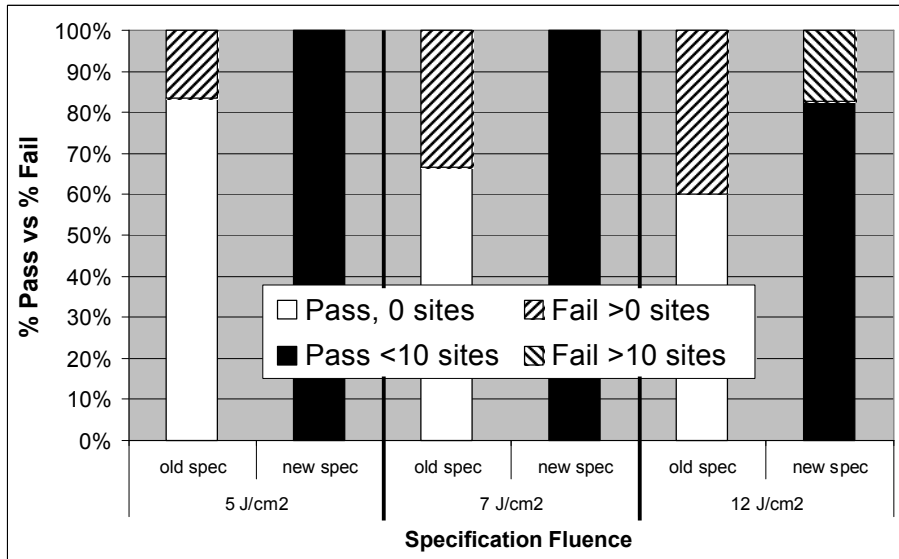


Figure 9. Impact on yield for the damage results of Figure 8 with the new test protocol compared to the original test protocol.

For a 5 J/cm² specification fluence, 83% of the runs would have passed under the original test requirements, compared to 100% under the new test protocol. This represents an improvement of 20%.

For an 8 J/cm² specification fluence, only 66% of the coating runs would have passed the original test requirement. However 100% passed under the new protocol, which represents a 50% improvement in yield.

For the 12 J/cm² specification fluence, 60% of the coating runs would have passed the original test requirement compared to 83% that would have passed with the new test specification, which represents a yield improvement of approximately 38%.

4. CONCLUSIONS

In conclusion, an improved laser damage test protocol has been developed. The capability to return to damage sites and perform growth tests has been implemented on the NIF damage test system. Growth tests consisting of 300 repeat pulses on initiated damage sites on antireflective coatings have shown that the damage sites do not grow at fluences below 20 microns. The new protocol has been formalized and released as NIF document MEL01-013-0D, *Small Optics Laser Damage Test Procedure*⁷.

Using the new protocol has resulted in the acceptance of numerous anti-reflection coating runs which would have been rejected under the original qualification criteria. The predicted yield improvement is as high as 50% depending on the specification fluence. Additionally the new test provides increased assurance that the coated optics are free from damage initiation sites that are susceptible to growth and will therefore meet NIF lifetime requirements.

Future work will involve extending this new test procedure to other types of coatings such as mirrors and polarizers.

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*borden5@llnl.gov; phone 925-423-9006