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EXTRACTION WITHOUT AQUEOUS COMPLEXING AGENTS

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SEPARATION OF TRIVALENT LANTHANIDES AND ACTINIDES
BY SOLVENT EXTRACTION WITHOUT AQUEOUS
COMPLEXING AGENTS*

by

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ABSTRACT

A method of separating the trivalent actinides, mainly Am and Cm, from trivalent lanthanides is presented. This method embodies the sequential use of two different solvent extractants; the first extractant would remove the heavy lanthanides from the lighter lanthanides and Am-Cm, while the second would extract Am-Cm in preference to the lighter lanthanides. In this scheme, no additional complexing agents are required. Thus, waste disposal and corrosion problems are minimized. Overall separation factors for Am-Cm from lanthanide fission products in reactor wastes may be as high as several thousand.

INTRODUCTION

The projected use of fission nuclear reactors to meet the power needs of the United States in the next several decades poses the serious problem of disposal of the highly radioactive waste products from fission and neutron capture in the reactors. One of the most critical aspects of this problem is long-term storage of the waste, necessitated by the need to protect the environment from the long-lived transplutonium elements generated as neutron-capture products of the nuclear fuel. Although the fission products from freshly-processed spent fuel element present a more immediate radiation hazard, this danger decreases at

a considerably faster rate than that for the α -emitting actinides. Thus, while there is a need to store the fission products safely for about a thousand years, the presence of the long-lived actinide elements in the nuclear waste doubles or triples the required storage period.

Several solutions to this problem have been suggested; among them is to separate the α -emitting species from the fission products, storing them separately or returning them to the reactors to be consumed by the (n, fission) reaction. This reaction has a considerable cross-section for the actinide elements, and would thus

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transform the long-lived α -emitting nuclides into less dangerous fission products.

The chemical separation of transplutonium elements from fission products generally fails to eliminate the lanthanide fission products (primarily La to Eu) because of similarities in ionic radii and electronic structures between these two families of elements. Thus, the separation of the transplutonium actinides from the lanthanide elements is crucial to partitioning the short-lived from the long-lived waste products.

Current laboratory separation schemes rely upon the slightly larger complexation strengths of the actinides over the lanthanides, followed by partitioning of the lanthanides into an organic solution by ion-exchange or solvent extraction.¹⁻³ The most effective complexants for this separation are Cl^- , SCN^- , and certain aminocarboxylic acids such as EDTA. However, each has drawbacks when applied to large-scale systems. High concentrations of Cl^- must be used, producing very corrosive solutions and adding significantly to the bulk of the wastes.⁴ Thiocyanate shows a tendency to polymerize in acid solutions, especially in the presence of α -radiation.^{5,6} The separation processes employing aminocarboxylic acids (i.e., TALSPeAK and related processes)^{7,8} leave large quantities of these compounds in their various waste streams, and also require a low-acidity feed solution in which hydrolysis or precipitation of some of the fission products and actinides becomes a problem.¹

We are investigating a solvent-extraction process for the separation of Am(III) and Cm(III) from the trivalent lanthanides in which no aqueous complexants are used. Instead, two successive extractions are performed. For the first, an extractant to which Am and Cm behave like the early lanthanides is used, and for the second, a different extractant in which Am and Cm behave like middle or heavy lanthanides is used.

Numerous studies have shown that Am and Cm behave like Pr or Nd in extractions with di-(2-ethylhexyl)orthophosphoric acid (HDEHP) from dilute mineral acids,^{7,8,9} The heavier lanthanides are progressively more extractable, with an average separation factor $SF_{Z/2-1}$ of 2.4,¹⁰ where the separation factor is defined as the ratio of

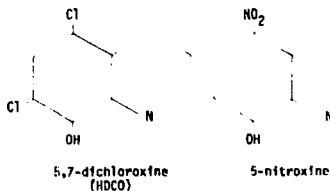


Fig. 1. Structural formulas of the extractants HDClO and 5-nitroxine.

the distribution coefficients for each species between an organic and an aqueous phase. Hence, Am and Cm can be separated from the heavier lanthanides by extraction with HDEHP.

To separate Am and Cm from the lighter lanthanides, which contain the major lanthanide fission products, we are investigating several derivatives of 8-hydroxyquinoline (o-ine) including 5,7-dichloroxine (HDClO) and 5-nitroxine (o-ine, 1). Sekine and Byersson¹¹ have reported Am/Eu separation factors of 10 for extraction from dilute HClO_4 solutions with 0.05 M HDClO in chloroform. If the lanthanide extractabilities increase with Z as expected, Am would behave roughly like Dy, and a clean separation of Am and Cm from the lanthanide fission products should be feasible. The present work was concerned with testing the validity of the separation scheme and determining the optimum conditions for separations.

EXPERIMENTAL

The radioactive tracers used in this work for determining lanthanide-actinide distribution ratios were ^{241}Am and $^{152,154}\text{Eu}$. The Eu tracer was chosen because of its immediate availability and its identity as a medium-heavy lanthanide. The HDEHP and HDClO extractants were obtained commercially, and 5-nitroxine was graciously donated by Dr. H. Gershon, Boyce Thompson Institute for Plant Research, Yonkers, New York, who first synthesized this compound in 1972.

Stock solutions of the radioactive tracers were added to the extraction mixture immediately prior to extraction; the aqueous phases for the oxine-derivative extractions had previously been

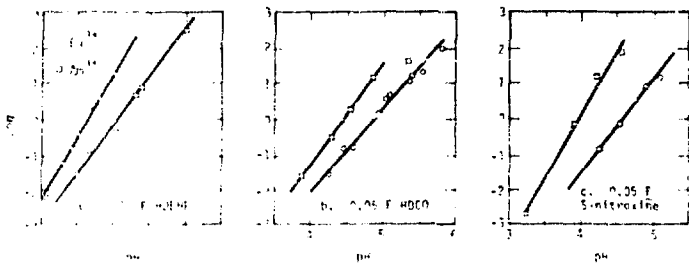


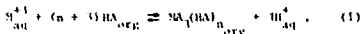
Fig. 2. Extraction of Eu^{3+} and Sm^{3+} from 0.1 M CaCl_2 and 0.1 M $\text{Ca(NO}_3)_2$ organic phases: (a) 0.5% HDEHP in heptane; (b) 0.05% HDEHP in chloroform; (c) 0.05% 5-nitroquinoline in chloroform.

of extraction of the metal species (Eu^{3+}) with a quinoline-derivative extractant in chloroform, CHCl_3 , appears to be similar to the extraction of Eu^{3+} with HDEHP in heptane, as was expected.

From the results of the extraction mixtures was observed that extraction is more efficient when the extraction is carried out with a starting metal ion concentration of the lower equilibrium period (results). The mixture was then centrifuged, and the separated phases were drawn off. Eu^{3+} was counted on a NaI(Tl) scintillation counter to determine the distribution ratios. The pH of the aqueous phase was determined by material balance for OH^- and by a glass electrode otherwise.

RESULTS AND DISCUSSION

The extraction stoichiometry is assumed to be of the form



where E is the metal species to be extracted and HA is the extractant. This implies that the equilibrium position of this reaction is dependent upon the aqueous acid concentration to the third

power. It can be shown that a plot of the logarithm of the distribution ratio (log D_0) versus the pH should be a straight line with a slope of 3.

The results of our experiments are presented in Fig. 2 as plots of log D_0 versus pH for 0.5% HDEHP in heptane, 0.05% HDEHP in chloroform, and 0.05% 5-nitroquinoline in chloroform. The data are also summarized in Table I along with some of the corresponding literature values.¹¹⁻¹³ All six extraction curves show deviations from the third-power acid dependency. This may be because we used reagent concentrations rather than unit activities in calculating the pH values, and/or because of the rather high solubility of the quinoline-derivative extractants in aqueous solution. In each case, the more extractable element shows the higher acid dependency, so that the separation factor increases with pH.

The Am/Eu separation factors of 0.04 for HDEHP and 90 for 5-nitroquinoline imply an overall separation factor of 240 for one pass through each extractant, and a recovery of about 75 percent for the Am . This may be increased in actual experience, since Eu is not a major fission product, and since those lighter lanthanides that are, should be even less susceptible to extraction by the HDEHP.

TABLE I

RESEARCH ACTIVITIES OF THE AEC AND AEC CONTRACTORS IN THE AREA OF RESEARCH ON THE CHEMISTRY OF FUELS

RESEARCH CENTER	PROJECT TITLE	PI	ACCEPTED FOR PUBLICATION		RESEARCH REPORT NUMBER	DATE OF PUBLICATION
			FOUND	DATE		
AEC	Development of a Fuel Cycle for a Fast Reactor	W. L. Marshall	1964	1964	ORNL-3111	1964
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Notes: 1. The dates in the "Found" column are the dates of the original publication of the research report. 2. The dates in the "Date of Publication" column are the dates of the final publication of the research report.

1. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
2. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
3. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
4. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
5. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
6. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
7. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
8. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
9. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
10. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
11. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
12. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
13. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
14. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
15. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
16. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
17. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
18. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
19. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.
20. W. L. Marshall, R. J. C. Brown, and J. C. Beale, "Research on the Chemistry of Fuels for Fast Reactors," ORNL-3111, ORNL, Oak Ridge, Tennessee, 1964.