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VAPORIZATION OF ZIRCONIUM OXIDE

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ABSTRACT

The vaporization rate of zirconium oxide in the temperature range 2410 to 2830 °K was measured using the Knudsen effusion technique, and the composition of the vapor was estimated from a mass spectrometric observation. These data were used, with pertinent thermodynamic quantities obtained from the literature, to calculate the dissociation energies D^o (ZrO) = 7.8 ± 0.2 ev, and D^o (ZrO₂) = 14.9 ± 0.2 ev.

I. INTRODUCTION

The vaporization of ZrO_2 has been reported by Ackermann and Thorn¹. They calculated the partial pressures of $ZrO_2(g)$, ZrO(g), and O(g) over solid ZrO_2 , using free energies of formation of $ZrO_2(s)$, ZrO(g), and O(g); and reported $ZrO_2(g)$ to be the predominant species. More recently, however, the same authors² have reported that congruent evaporation and a minimum in the volatility occur when the dioxide phase has the composition O/Zr = 1.96. At this composition, the ZrO(g) is the predominant species. The dissociation energy of ZrO_2 was given as D° = 15.3 ± 0.3 ev, the value of which is dependent on the acceptance of 7.8 ev^{3,4} for the dissociation energy of ZrO_2 .

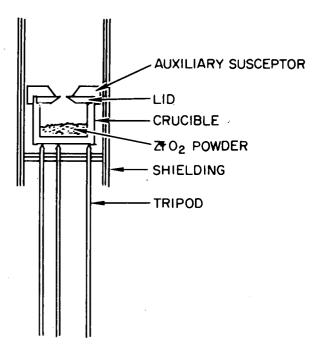
Chupka, Berkowitz and Inghram⁴ made a mass spectrometric analysis of the vapors effusing from a Knudsen cell containing either ZrO_2 or a mixture of Zr and ZrO_2 , and determined the vapor pressures and heats of sublimation of the gaseous species. Their results yielded 7.8 ± 0.2 ev and 14.5 ± 0.2 ev for the dissociation energies of ZrO and ZrO_2 , respectively. The dissociation energy of ZrO_2 given by Chupka, <u>et al</u>, is less than that given by Ackermann and Thorn by 14 kcal, even after correcting for the different values used for the heat of sublimation of zirconium in deriving the value for D[§] (ZrO₂).

In the present work, the evaporation rate of ZrO_2 from a tungsten cell was measured using the Knudsen effusion technique over the temperature range 2410 to 2830 °K. Vapor species were identified at 2575 °K using a time-of-flight mass spectrometer. The dissociation energies of ZrO and ZrO_2 , and the partial pressures of the gaseous species were calculated from these data.

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II. APPARATUS AND EXPERIMENTAL PROCEDURE

A total-weight-loss Knudsen effusion method was used. The effusion rate measurements were made in a vacuum induction furnace heated by a 6-kw Ajax high frequency converter. The vacuum in the system was maintained in the range of 10^{-5} to 10^{-6} mm Hg during the runs, except during the brief warmup period. The temperatures were measured with a Leeds and Northrup optical pyrometer by sighting into the effusion hole. The pyrometer was calibrated against a secondary standard tungsten ribbon lamp; and the maximum estimated uncertainty in the temperature measurements is $\pm 15^{\circ}$.



The tungsten Knudsen cell was made in two parts, as shown in Figure 1. The crucible measured 5/8-in. O. D. 1/2-in. ID, and 1/2-in. high. The lid, with an approximately 1 mm-diameter orifice, was a 1/16in. thick disc which fitted into a recess cut in the crucible. The orifice was ground to a knife-edge, and was placed with the flat surface facing out. An auxiliary tungsten susceptor was used above the cell assembly to reduce heat loss from the lid, and to minimize the temperature differential between the lid and the crucible. Both the Knudsen cell and the auxiliary susceptor were heated in hydrogen for 1-1/2 hr at 1775°K, and then degassed in vacuum at

Figure 1. Tungsten Knudsen Cell Assembly

2900°K for 8 hr, previous to the vaporization runs. The cell was supported on a tungsten tripod and shielded with 1-mil tungsten foil.

Before making the effusion rate runs, the cell containing the ZrO₂ powder was heated in vacuum at 2850 °K for 4 hr. The gray residue obtained was assumed to be the congruently vaporizing zirconium oxide composition.

The orifice diameter was measured before and after each run with a micrometer comparator mounted in a stereomicroscope; and the average reading was used, after applying a small correction for the thermal expansion of tungsten⁵. It is estimated that the orifice diameters are accurate to 0.01 mm. All weight losses were multiplied by the factor 1/0.98 to correct for the thickness of the orifice wall.⁶

The averaging method of Skinner, et al,⁷ was used to correct for the temperature fluctuation during each run, and for the initial heating and cooling periods.

The Knudsen cell was weighed before and after each run on an analytical balance to 0.1 mg. A small weight loss of the empty tungsten cell was sub-tracted from the weight-loss measurements.

The mass spectrometric data were obtained using a Model 12-101 Bendix time-of-flight mass spectrometer. A zirconia sample supported on a resistanceheated tungsten ribbon was used as the spectrometer source. The apparent temperature was observed by sighting on the sample, using a Leeds and Northrup optical pyrometer. The mass spectrum was obtained with an electron energy of 50 v, and was displayed on a Tektronic Model 541 oscilloscope and recorded using a 35-mm Bolsey oscilloscope camera.

The operating procedure consisted of calibrating the spectrometer and adjusting the oscilloscope to display the mass range of interest, 85 to 135. Then, the temperature of the tungsten strip source was raised, keeping the system pressure below 10^{-5} mm Hg. The mass spectrum was photographed, a check for shutter dependency was made, and the temperature observed to complete the measurement.

The zirconium oxide was reactor grade material obtained from The Carborundum Metals Corp.

III. EXPERIMENTAL RESULTS AND DISCUSSION

The effusion data are given in Table I. For convenience in performing the calculations to be described later in this section, the Clausing correction was applied to the measured effusion rates. These corrected or "ideal" values are given in the sixth column of the table. The pressures in the last column were calculated by means of the Knudsen equation⁶,

$$P^*(atm) = 0.02256 G (T/M)^{1/2}, \dots (1)$$

where G is the effusion rate in gram/cm²/sec, T is the absolute temperature, and M is the molecular weight. The pressures, P^* , were calculated assuming the vapor to consist entirely of $ZrO_2(g)$, and are represented as a function of temperature by Equation 2, obtained by a least squares treatment of the P^* values,

$$Log P^{*}(atm) = -34,020/T + 7.828$$
. ...(2)

TABLE I

Run	Temp (°K)	Time (sec)	Orifice Area x 10 ³ (cm ²)	Wt Loss (gm)	Evap Rate x 10 ⁵ (gm/cm ² /sec)	P* x 10 ⁵ (atm)
9	2830	6830	6.94	0.0427	90.1	9.74
6	2800	8100	8.40	0.0216	31.8	3.41
10	2730	10800	6.79	0.0157	21.4	2.27
2	2715	17580	7.54	0.0202	15.24	1.61
7	2625	17910	8.40	0.0115	7.64	0.796
1	2605	14060	7.54	0.0072	6.79	0.705
3	2535	27970	7.84	0.0056	2.55	0.261
8	2515	31400	8.59	0.0053	1.96	0.200
4	2475	31620	8.17	0.0024	0.93	0.094
5	2410	60380	8.17	0.0030	0.61	0.061

EVAPORATION RATES OF ZrO,

The mass spectrometric data are presented in the form of the photograph of Figure 2, which shows the characteristic patterns for the Zr^+ , ZrO^+ , and ZrO_2^+ isotopes; and also those for Hg^{++8} . The Zr^+ peaks are attributed mainly to fragmentation produced by the 50-v electron beam. Comparison of measured effusion rates with those to be expected for simple dissociation to the elements,

$$ZrO_{2}(s) = Zr(g) + 2O$$
, ...(3)

indicates that molecular species and oxygen must greatly predominate in the vapor, and that Zr(g) could have been present to the extent of less than about 2%.

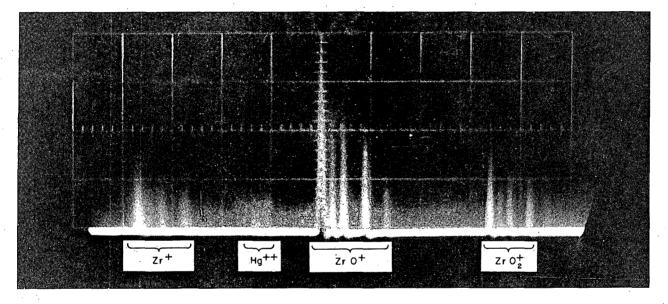


Figure 2. Mass Spectrum of the Vapor Over ZrO₂

An estimate of vapor composition was made, based on the known abundances of the Zr isotopes, as follows: visual inspection showed that the intensity of the $Zr^{91}O$ peak (relative abundance 11.2%) is slightly greater than that of the $Zr^{90}O_2$ peak (relative abundance 51.5%), so that the apparent ZrO- to-ZrO₂ ratio is about 5 to 1. Because of uncertainties resulting from fragmentation, no further analysis will be given, although it is believed that the effect of fragmentation in this case would tend to compensate for differences in ionization probabilities. As will be shown later, dissociation energies of ZrO and ZrO_2 are not sensitive to moderate uncertainties in vapor composition. In summary, therefore, the mass spectrometric examination and thermodynamic considerations lead to the conclusions that the predominant vaporization processes are

$$ZrO_{2}(s) = ZrO_{2}(g), \qquad \dots (4)$$

and

$$ZrO_{2}(s) = ZrO(g) + O, \qquad \dots (5)$$

and that about 5/6 or 83% of the vapor is ZrO and O; and about 1/6, or 17% is ZrO₂ at 2600 °K.

The dissociation energies of ZrO and ZrO₂ may be obtained from the vaporization data, the estimated vapor composition, and thermodynamic data available in the literature, as described below for ZrO.

First, ΔF_T° for reaction 5 is calculated by use of Equation 6,

$$\Delta \mathbf{F}_{\mathbf{T}}^{*} = -\mathbf{R} \mathbf{T} \ln \mathbf{K}_{\mathbf{p}} = -4.576 \mathbf{T} \operatorname{Log} \mathbf{P}_{\mathbf{Z} \mathbf{r} \mathbf{O}} \mathbf{P}_{\mathbf{O}}. \qquad \dots (6)$$

The partial pressures are computed from the evaporation rates corresponding to P_{ZrO2}^* given by Equation 2. It should be noted that although Ackermann and Thorn showed that zirconium dioxide vaporizes congruently at elevated temperatures in vacuum at the composition $ZrO_{1.96}$, no significant error will be made if the assumption of stoichiometry is made. Thus the effusion rates of ZrO and O, in grammol/cm²/sec, will be equal; and would be in the proportion 107.2/16 by weight. The heat of reaction 5 at 0°K is then calculated using free energy functions:

$$\Delta H^{\circ} = \Delta F^{\circ}_{T} - \Delta \left(\frac{F^{\circ}_{T} - H^{\circ}}{T} \right) T \quad . \tag{7}$$

The heat of reaction thus obtained is combined in the usual manner with those for other reactions to give ΔH : for the dissociation of ZrO(g):

 $ZrO_2(s) = Zr(s) + O_2$ $\Delta H^*_s = 260.1 \text{ kcal}$... (8)

$$O_2 = 2 O$$
 $\Delta H_*^\circ = 118.0 \text{ kcal}$... (9)

$$Zr(s) = Zr(g)$$
 $\Delta H_{\circ}^{\circ} = 145.7 \text{ kcal}$... (10)

 $ZrO(g) + O = ZrO_2(s)$ $\Delta H^{\circ} = -343.0 \text{ kcal} - (5)^{*}$

$$ZrO(g) = Zr(g) + O$$
 $\Delta H^{\circ} = 181 \text{ kcal}$... (11)

*The negative sign refers to the reverse of reaction 5.

where ΔH ° = D° (ZrO). The calculations for D° (ZrO₂) are similar. Based on the estimated vapor composition, the calculations outlined above lead to D° (ZrO) = 181 (±4) kcal, or 7.8 (±0.2) ev, and to D° (ZrO₂) = 343 (±5) kcal, or 14.9 (±0.2) ev. The values are based on the effusion rate at 2600 °K, because this temperature is near the midpoint of the experimental temperature range and is also near that at which the vapor composition was determined.

The sources of thermodynamic data used in the calculations were: Stull and Sinke⁹ for heats of formation and free energy functions of the elements; Brewer and Chandrasekharaiah^{10,11} for the free energy functions of ZrO(g) and $ZrO_2(g)$; Kelley^{12,13} for heat capacities and entropies; Coughlin¹⁴ for heat of formation and of transition of $ZrO_2(s)$. The quantity (H_{298}° - H_{*}°) for $ZrO_2(s)$ was estimated to be 2000 cal from the low-temperature heat capacity data in Reference 13. The table of the free energy functions for the temperature range of the experiments is given in the Appendix.

To illustrate the effect of error in vapor composition, the dissociation energies were calculated for a number of other vapor compositions; and these are given in Table II. As may be seen by inspection of the D° values <u>vs</u> composition, a twofold error in the fraction of ZrO_2 in the vapor, i.e., 9% or 34% <u>vs</u> 17% ZrO_2 , would affect D° (ZrO_2) to the extent of only 3.5 kcal, and the corresponding effect on D° (ZrO) would be less.

DISSOCIA TIO	DISSOCIATION ENERGIES OF ZrO AND ZrO ₂ vs COMPOSITION		
% ZrO + O in vapor	% ZrO ₂ in vapor	D:(ZrO) (kcal <u>)</u>	D:(ZrO ₂) (kcal)
100	0	182.7	_
95	5	182.1	336.3
90	10	181.6	339.8
83	17	180.8	342.6
80	20	180.4	343.4
70	30	179.0	345.5
60	40	177.4	347.0
• 0	100		351.8

TABLE II

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IV. CONCLUSIONS

The results of this work appear to be in excellent agreement with those of Chupka, Berkowitz, and Inghram; and in fair agreement with those of Ackermann and Thorn. Somewhat different values of the thermodynamic quantities were used in calculating the dissociation energy of ZrO_2 in each of the two previous reports and in this work. To properly compare the results, therefore, the values given in the two previous reports were adjusted, using the values of the thermodynamic quantities used in this report. The result is that our value is greater than that of Chupka, et al, by 6.4 kcal, or 0.3 ev; and less than that of Ackermann and Thorn in obtaining their value, 15.3 ev, are probably subject to somewhat greater experimental error than those obtained in this work, in that their method involved correcting initial loss rates of stoichiometric ZrO_2 for loss of ZrO-and-O. It is therefore suggested that the weighted average, $342(\pm 4)$ kcal or 14.8 (± 0.2) ev, be taken as the best value for D° (ZrO_2). There appears to be little question concerning D° (ZrO) = 7.8 ev.

To predict the behavior of the oxide in various environments, it would be helpful to have information concerning the equilibrium constants as a function of temperature for the important equilibria. Thus, utilizing the fact that free-energy function differences change very slowly with temperature, one may write for Reaction 4

$$-\Delta \mathbf{F}_{\mathbf{T}}^{\circ} = 4.576 \, \mathrm{T} \, \mathrm{Log} \, \mathbf{P}_{\mathbf{Z} \mathbf{r} \mathbf{O}_{\mathbf{Z}}} = -\Delta \mathrm{H}^{\circ} \cdot -\Delta \left(\frac{\mathbf{F}_{\mathbf{T}}^{\circ} - \mathrm{H}^{\circ}}{\mathrm{T}}\right) \mathrm{T} \, . \qquad \dots (12)$$

Substituting and simplifying,

$$\log P_{ZrO_2}(atm) = -39,730/T + 9.18$$
. (13)

Similarly, for Reaction 5, one finds

$$\log P_{ZrO} P_{O} = -74,910/T + 17.68$$
. ...(14)

Reaction 4 would be predominant in air or in an oxygen-bearing atmosphere, and Reaction 5 would be predominant in vacuum.

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APPENDIX

Species -	Temperature (°K)			
Species	2400	2600	2800	
0	43.93	44.34	44.72	
Zr(g)	50.43	50.95	51.44	
ZrO(g)	68.6	69.4	70.0	
ZrO ₂ (g)	73.7	74.9	75.8	
ZrO ₂ (s)	31.5	32.8	34.0	

TABLE OF - $\frac{F_{T}^{*} - H^{*}}{T}$ USED IN CALCULATIONS