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D. Antonangeli, J. Siebert, J. Badro, D. L. Farber,
G. Fiquet, G. Morard, F. J. Ryerson

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1 **Composition of the Earth's inner core from high-pressure sound**
2 **velocity measurements in Fe-Ni-Si alloys**

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4 Daniele Antonangeli^{a,b}, Julien Siebert^{a,b}, James Badro^{a,b}, Daniel L. Farber^{b,c},
5 Guillaume Fiquet^a, Guillaume Morard^a, Frederick J. Ryerson^b

6
7 ^a *Institut de Minéralogie et de Physique des Milieux Condensés, UMR CNRS 7590, Institut de*
8 *Physique du Globe de Paris, Université Pierre et Marie Curie, Université Paris Diderot,*
9 *75005 Paris, France.*

10 ^b *Lawrence Livermore National Laboratory, Livermore, California 94550, USA*

11 ^c *Department of Earth and Planetary Sciences, University of California, Santa Cruz, Santa*
12 *Cruz, CA, 95064*

13

14 **Abstract**

15

16 **We performed room-temperature sound velocity and density measurements on a**
17 **polycrystalline alloy, $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$, in the hcp phase up to 108 GPa. Over the**
18 **investigated pressure range the aggregate compressional sound velocity is ~ 9% higher**
19 **than in pure iron at the same density. The measured aggregate compressional (V_P) and**
20 **shear (V_S) sound velocities, extrapolated to core densities and corrected for anharmonic**
21 **temperature effects, are compared with seismic profiles. Our results provide constraints**
22 **on the silicon abundance in the core, suggesting a model that simultaneously matches the**
23 **primary seismic observables, density, P-wave and S-wave velocities, for an inner core**
24 **containing 4 to 5 wt% of Ni and 1 to 2 wt% of Si.**

25

26

27 **1. Introduction**

28

29 The study of seismic wave propagation and normal mode oscillation are, without doubt,
30 two of the most direct probes of the Earth's interior, providing a remote sensing method to
31 obtain sound velocities and density. However, to derive an accurate compositional model,
32 these seismic observations have to be combined with laboratory-based experiments
33 constraining the density and elastic properties of highly compressed minerals. Based on shock
34 wave measurements, Birch proposed in the early 1950's that the Earth's core was mainly
35 composed of iron alloyed with nickel and some "light element(s)", required to account for the
36 observed density difference between the core and pure iron [Birch, 1952]. Since then, a large
37 number of experimental and theoretical studies addressed the nature and concentration of
38 these light elements (see review by Poirier [Poirier, 1994]), with several elements proposed.
39 Geo- and cosmochemical arguments suggest that most likely candidates are sulfur [Williams
40 and Jeanloz, 1990; Sherman, 1991; Sherman, 1995; Sherman, 1997; Li et al., 2001; Vočadlo,
41 2007; Morard et al., 2008; Côté et al., 2008a], oxygen [Sherman, 1991; Sherman, 1995;
42 Stixrude et al., 1997; Rubie et al., 2004; Badro et al., 2007; Asahara et al., 2007; Corgne et al.,
43 2009], and silicon [Sherman, 1997; Dobson et al., 2003; Vočadlo, 2007; Badro et al., 2007;
44 Côté et al., 2008a; Côté et al., 2008b; Asanuma et al., 2008]. Very recently, high-pressure
45 measurements of sound velocity and density of several iron compounds (FeO, FeSi, FeS, and
46 FeS₂) in conjunction with data on pure iron, pointed out inconsistencies when considering
47 sulfur as the only major light element, and proposed an Earth's inner core composed of iron
48 alloyed with silicon (2.3 wt%) and traces oxygen (0.1 wt%) [Badro et al., 2007]. However,
49 these results are based on three primary assumptions:

50 a) a linear dependence of compressional sound velocity (V_p) on density ("Birch's law");

51 b) the P-wave velocity of the alloy is equal to a geometrical average of that of the minor
52 compound and the metal (*i.e.* ideal mixing behaviour);

53 c) the inclusion of up to 5 wt% Ni has a negligible effect on sound velocity.

54 Further, a clear limitation of this model is that only the aggregate compressional sound
55 velocity was taken into account, whereas the largest discrepancy between the seismological
56 observations and the results from molecular dynamics simulations and diamond anvil
57 experiments is observed for the shear wave velocity [Deuss, 2008].

58 Therefore, in order to validate the overall proposed model of the core composition, as
59 well as to address the legitimacy and the possible limits of the adopted approximations, we
60 undertook an experimental investigation of (Fe,Ni,Si) alloy samples. Specifically, we carried
61 out sound velocity and density measurements on polycrystalline samples containing 4.3 wt%
62 of Ni and 3.7 wt% of Si, compressed in diamond anvil cell (DAC) to megabar pressures.
63 Details of sample synthesis and characterization, as well as of the inelastic x-ray scattering
64 (IXS) measurements are reported in the next section, while the obtained results are illustrated
65 and discussed in section 3. Our main conclusions are summarized in section 4.

66

67 **2. Experimental details**

68

69 Polycrystalline homogeneous samples of silicon bearing iron-nickel alloy have been
70 prepared at high pressure and high temperature. Partial oxidation of silicon metal is a critical
71 issue in the synthesis of silicon-rich iron alloy. The experiment has been conducted at
72 superliquidus conditions to segregate from a SiO₂ glass a (Fe,Ni,Si) metallic blob free of SiO₂
73 inclusions. The starting material consisted in homogenized mixture of high purity metallic
74 and oxide powders of Fe, Si, Ni and SiO₂, with a 60 wt. % metallic portion relative to oxide.
75 Piston cylinder experiment was carried out at 10 kbars and 1850°C at the Lawrence

76 Livermore National Laboratory, using a standard 1/2'' BaCO₃ pressure cell assembly, with a
77 graphite furnace and a MgO capsule. The recovered metallic blob of about 1 mm diameter
78 was analyzed with an electron probe micro-analyzer operating at 20 kV and 50 nA. Multiple
79 analyses as well as backscattered electron images show homogenous (Fe,Ni,Si) alloy
80 composition without quench textures at least at the scale of imaging and analytical resolution.
81 Silicon and nickel concentrations are 3.7 wt% and 4.3 wt%, respectively.

82 Compacted pellets of about 90 μm diameter and 20 μm thick were loaded in DACs
83 equipped with Re gasket, using 300 μm flat anvils and neon as pressure transmitting medium
84 for measurements up to 50 GPa, and 150/300 μm beveled anvils with no pressure transmitting
85 medium for higher pressures. Pressures were determined by ruby fluorescence and, most
86 importantly, the densities (ρ) were directly obtained from diffraction measurements and
87 crosschecked with the equation of state previously measured on the same samples [Fiquet et
88 al., 2008].

89 Inelastic x-ray scattering measurements were carried out on the ID28 beamline at the
90 European Synchrotron Radiation Facility, using the Si(8,8,8) instrument configuration, which
91 provides the best compromise between flux and energy resolution (5.5 meV full width half
92 maximum (FWHM)) for polycrystalline samples compressed in DAC. Spectra have been
93 collected in transmission geometry, with the x-ray beam impinging on the sample through the
94 diamonds, along the main compressional axis of the cell, and hence probing exchange
95 momenta q almost perpendicular to the cell-axis. The transverse dimensions of the focused x-
96 ray beam of 30 x 90 μm² (horizontal X vertical, FWHM) were further reduced by slits on the
97 vertical direction. Momentum resolution was set to 0.25 nm⁻¹. Further details of the
98 experimental setup can be found elsewhere [Krisch, 2003; Antonangeli et al., 2004a;
99 Antonangeli et al., 2005]. By scanning the scattering angle at the elastic energy (*i.e.* q -scan at

100 $\Delta E=0$) we collected the [100], [002] and [101] reflections out of our sample, with the
101 momentum resolution of 0.06 nm^{-1} set by slits in front of the analyzer.

102 We collected data in the hcp phase, at 27, 37 and 47 GPa on quasi-hydrostatically
103 compressed samples, and at 32, 68 and 108 GPa on non-hydrostatically compressed samples.
104 At each investigated pressure point, we mapped the longitudinal acoustic phonon dispersion
105 throughout the entire first Brillouin zone collecting 8-9 spectra in the range $3.5\text{-}12 \text{ nm}^{-1}$
106 (Figure 1). The energy positions of the phonons were extracted by fitting a set of Lorentzian
107 functions convolved with the experimental resolution function to the IXS spectra, utilizing a
108 standard χ^2 minimization routine. We then derived the aggregate compressional sound
109 velocity V_P from a sine fit (Born-von Karman lattice-dynamics theory limited to 1st neighbor
110 interaction) to the phonon dispersion [Antonangeli et al., 2004a; Antonangeli et al., 2005],
111 with error bars between ± 2 and $\pm 3\%$ (Figure 1). Combining our measurements of V_P and ρ
112 with the values of bulk modulus, K [Fiquet et al., 2008], we also obtained the aggregate shear
113 sound velocities V_S from the relation $V_S=[3/4 (V_P^2 - K/\rho)]^{1/2}$, although with larger uncertainty
114 ($\pm 4\text{-}6\%$) due to error propagation.

115

116 **3. Results and discussion**

117

118 The measured compressional sound velocities are plotted as a function of density in
119 Figure 2, together with values for pure iron [Fiquet et al., 2001; Antonangeli et al., 2004a] and
120 $\text{Fe}_{0.78}\text{Ni}_{0.22}$ alloy [Kantor et al., 2007]. To provide an analysis unbiased by systematic
121 differences resulting from different techniques, pressure scales or approximations in the
122 equation of state, and thus to be able to resolve variations as low as a few percent, we have
123 only considered data obtained by IXS for conditions where the density was directly measured.
124 While no systematic offsets can be observed between data for pure iron and iron-nickel alloy,

125 our velocity measurements for $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$ are systematically higher, as highlighted by
126 the linear fits to the experimental data (Figure 2). Over the investigated pressure range,
127 $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$ is approximately 9% faster than pure iron at the same density. We also note
128 that our experimental results compare favourably with calculations on $\text{Fe}_{0.9375}\text{Si}_{0.0625}$
129 [Tsuchiya and Fujibuchi, 2009] (Figure 2), further stressing that the increase in the sound
130 velocity is solely due to the silicon incorporation with no observable effect due to nickel.

131 To compare directly with seismic models however, our results need to be extrapolated to
132 core conditions. Within the experimental uncertainties, all the datasets exhibit a linear
133 dependence of V_P with density (*i.e.* follow “Birch’s law”), as also observed in several other
134 high-pressure experimental and theoretical studies [Vočadlo, 2007; Badro et al., 2007; Kantor
135 et al., 2007; Antonangeli et al., 2008; Tsuchiya et Fujibuchi, 2009]. Hence, as a first
136 approximation (see discussion later on), within a quasi-harmonic limit, we assume a linear
137 dependence of the compressional sound velocities with density, irrespective of the specific
138 pressure and temperature conditions.

139 Also, since we are interested in the isotropic aggregate properties, we carefully checked
140 our data for preferential alignment and elastic anisotropy. In the case of non-hydrostatically
141 compressed iron, angular dependence of V_P has been documented starting above ~ 80 GPa
142 [Antonangeli et al., 2004a], as a combined effect of the deformation-related development of
143 preferred orientation and of the intrinsic single-crystalline elastic anisotropy. Preferential
144 alignment of the c -axis along the main compression axis of the cell has been observed for
145 several hcp metals when compressed uniaxially [Wenk et al., 2001; Merkel et al., 2004;
146 Merkel et al., 2006]. Hence, we compared the relative intensities of the [100], [002] and [101]
147 reflections and the c/a ratio obtained under hydrostatic conditions using Ne as pressure
148 transmitting medium with those obtained under non-hydrostatic conditions. While all the
149 diffraction patterns collected from hydrostatically compressed samples show no significant

150 variation on the intensities with increasing pressure. However, the intensity of the [002]
151 reflection exhibits a strong reduction upon compression and almost vanishes at pressures
152 exceeding 30 GPa, for samples loaded without pressure transmitting medium. Such behavior
153 is expected for the utilized diffraction geometry as a consequence of the progressive
154 alignment of the crystalline c-axis with the main compression axis of the cell. However, the
155 volumes and the values for c/a derived solely from the [100] and [101] reflections did not
156 significantly differ from those obtained under quasi-hydrostatic compression up to ~ 90 GPa.
157 Conversely, the volume derived at 108 GPa is quite different from expected according to the
158 quasi-hydrostatic equation of state [Fiquet et al., 2008] and the c/a ratio displays a large
159 deviation. Deviation of individual d-spacings from the values expected in the limit of
160 hydrostatic compression is a direct consequence of the presence of a deviatoric stress within
161 the cell. For elastically isotropic materials, the strain $\epsilon_{hkl} = (d_{hkl} - d_{hkl}^{\text{hydro}}) / d_{hkl}^{\text{hydro}}$ for all the
162 lattice planes is the same. However, this is not the case in the presence of elastic anisotropy
163 [see for instance Sing et al., 1998; Merkel et al., 2009]. Thus, we can conclude that all our
164 non-hydrostatic pressure points (P~ 32, 68 and 108 GPa) exhibit some texture, but a
165 significant deviation from a radially averaged sound velocity is observed only at 108 GPa. To
166 support this conclusion, we note that as a direct consequence of the developed preferential
167 alignment and the predominant contribution of the slow-velocity basal plane [Antonangeli et
168 al., 2004a; Antonangeli et al., 2004b; Antonangeli et al., 2006; Mao et al., 2008], the V_P value
169 at the highest density (highest pressure) is somewhat lower than the linear trend, although still
170 within uncertainties (Figure 2).

171 Due to the deviation from radial average properties at the highest pressures, we only
172 considered data up to 68 GPa for extrapolation of V_P and V_S to core conditions. Our results
173 are reported in Figure 3 along with linear regressions and the density evolution proposed for
174 pure Fe [Badro et al., 2007], and compared with the seismic velocity profile from the radial

175 PREM model for the inner core [Dziewonski and Anderson, 1981]. As already suggested
176 [Fiquet et al., 2001; Badro et al., 2007], V_P for pure hcp-Fe is somewhat lower than the
177 PREM; this study shows that adding 3.7 wt% Si yields a velocity that is too fast relative to
178 PREM (Figure 3). If we consider linear mixing of pure Fe and $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$ (assuming an
179 ideal two-component solid solution), we simultaneously match the PREM values of V_P and ρ
180 for an alloy with 1.2 wt% of Si (gray dashes in Figure 3).

181 Considering V_S significantly increases the complexity of the problem. Both Fe and
182 $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$ exhibit values of shear velocities¹ significantly higher than PREM (Figure 3).
183 The mismatch for $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$ is even larger than for pure iron. Indeed, inclusion of
184 silicon leads to a much larger increase in V_S than in V_P , due to a smaller pressure derivative of
185 the bulk modulus (K') that is only partially balanced by a larger value of K_0 . As a result,
186 $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$ has a larger pressure derivative for V_S than pure Fe, which manifests itself as
187 a considerable divergence between the data sets when extrapolated to core densities. Using
188 this model, it is clear that we cannot simultaneously solve for V_P , V_S and ρ of the core by
189 simply varying the amounts of Ni and Si or pressure.

190 At core temperatures (4000-6000 K) anharmonic effects are expected. These might be
191 particularly relevant to V_S , as already pointed by computational studies [Laio et al., 2000;
192 Steinle-Neumann et al., 2001], that suggest significantly lower values of V_S as temperature
193 approaches the melting point. As such, we applied temperature corrections to our ambient
194 temperature results. Very recent *ab initio* calculations on hcp iron [Vočadlo et al., 2009]
195 suggest about 9.5% and about 35% softening for V_P and V_S respectively, between 0 and 5000
196 K. Such a temperature increase yields a density reduction about 4%. Since we are interested
197 in only the anharmonic high temperature effects (we are comparing data at the same density),
198 we corrected these computational results according to the measured density dependence of

¹ Extrapolated values of V_S are obtained assuming the Birch's law to be valid for both V_P and $V_\phi=(K/\rho)^{1/2}$. The resulting V_S exhibits a sub-linear dependence on density.

199 sound velocities to compensate for the density variation, obtaining 4% softening of V_P and
200 30% softening of V_S at 5000 K and 13000 Kg/m³. The thermal softening of V_P at constant
201 density requires an increase in the Si-content to ~ 1.5 wt% in order to match the seismic
202 observations. Most importantly, this composition appears to provide a simultaneous solution
203 for both V_P and V_S , consistent with PREM values (light gray dots in Figure 3).

204

205

206 **4. Conclusions**

207

208 Our new sound velocity and density measurements on hcp Fe_{0.89}Ni_{0.04}Si_{0.07} polycrystalline
209 samples compressed in DAC to 108 GPa yield values of V_P that are about 9% higher than in
210 pure iron (at the same density). As it has already been shown that alloying with Ni does not
211 significantly influence the elastic properties of Fe, at least up to a concentration of 22 at%
212 [Kantor et al., 2007], we can reasonably assume that the increase in the sound velocity is
213 solely due to the presence of Si. This conclusion is further supported by comparison of our
214 measurements with computational results on Fe_{0.9375}Si_{0.0625} [Tsuchiya and Fujibuchi, 2009].

215 Extrapolation to core densities and comparison with seismic velocity and density profiles
216 from PREM allow us to constrain compositional models of the core. Our results suggest an
217 inner core composition containing 4-5 wt% of Ni and 1-2 wt% of Si. The exact amount of Si
218 might vary depending upon the temperature corrections (here we used values calculated for
219 pure Fe), or if other elements are also present in the inner core. The approximations in our
220 model and the relatively large uncertainties, especially on V_S , do not allow us to definitively
221 rule out other compositional models, and other light elements might be present in amount
222 below our present limit of sensitivity (~ 1 wt%). It should be noted that our conclusions
223 pertain strictly to solid Fe-alloys and hence the inner core. Elements such as oxygen, that

224 may be incompatible in solid relative to liquid Fe-alloys are expected to reside mainly in the
225 outer core (see for instance [Alfe et al., 2002; Badro et al., 2007]) and cannot be adequately
226 constrained here. However, our proposed core composition is consistent with existing
227 experimental data and, for the first time, simultaneously matches all three geophysical
228 observables (V_P , V_S and ρ). Combined with Si partition coefficients between liquid and solid
229 Fe we can estimate the Si concentration of the liquid outer core and, hence, obtain a Si
230 concentration for the entire core. If we assume a molar partition coefficient for silicon
231 between the liquid and solid phase of iron of $1.2 \leq D^{\text{Liq/Sol}} \leq 1.9$ [Alfe et al., 2002], we obtain
232 a core composition with Si ranging from 1.2 to 4 wt%, for an inner core containing 1 to 2
233 wt% of Si. This result is at the lower range of those from core-formation and core-mantle
234 interaction models that often call for large amount of Si in the core (*e.g.* 7.3 wt% [Allègre et
235 al, 1995], 10.3 wt% [Javoy, 1995], 5-7 wt% [Wade and Wood, 2005]).

236 Several mechanisms have been proposed to explain the low shear velocity in the core,
237 including fluid inclusions [Singh et al., 2000; Vočadlo, 2007], viscoelastic relaxation [Jackson
238 et al., 2000] or the presence of randomly oriented anisotropic “patches” [Calvet and Margerin,
239 2008]. According to our present results, none of these is strictly necessary, and V_P and V_S can
240 be matched, although with some uncertainties due to the discussed approximations, by only
241 considering the effect of alloying silicon at the few wt% level with reasonable high
242 temperature anharmonic corrections inferred from recent theoretical calculations [Vočadlo et
243 al., 2007]. However, the above-mentioned possibilities [Singh et al., 2000; Vočadlo, 2007;
244 Jackson et al., 2000; Calvet and Margerin, 2008] become relevant to reconciliation of
245 observed seismic wave attenuation. In addition, seismic anisotropy, its variation with depth,
246 as well core hemisphericity, require higher complexity than the simple radial model discussed
247 here.

248

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261

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383 **Figure Captions**

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386 **Figure 1:** Longitudinal acoustic phonon dispersion of $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$ at ambient temperature
387 and pressures of 27, 37, 47, 68 and 108 GPa (bottom to top). For clarity the dispersion at 32
388 GPa is not plotted. The lines are sine fits to the experimental data.

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391 **Figure 2:** Aggregate compressional sound velocity as a function of density. Circles:
392 $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$; squares: Fe [Fiquet et al., 2001; Antonangeli et al., 2004a]; triangles:
393 $\text{Fe}_{0.78}\text{Ni}_{0.22}$ [Kantor et al., 2007]; open hexagons: computational results on $\text{Fe}_{0.9375}\text{Si}_{0.0625}$
394 [Tsuchiya and Fujibuchi, 2009]. The displayed error bars of the velocities result from the
395 experimental uncertainties, the statistical error of the fit, and the finite-q resolution of the
396 spectrometer. The uncertainties in the densities are smaller than the symbols. Lines are linear
397 regressions to the experimental data (solid - $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$; dotted - Fe; dashed -
398 $\text{Fe}_{0.78}\text{Ni}_{0.22}$).

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401 **Figure 3:** Aggregate compressional (V_P) and shear (V_S) sound velocities and density
402 extrapolations (considering only data up to 68 GPa). Circles: IXS data on $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$;
403 diamonds: PREM [Dziewonski and Anderson, 1981]. Solid lines - $\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$; dotted
404 lines - pure Fe [Badro et al., 2007]. V_S has been derived combining the measured V_P with
405 literature equation of state ($\text{Fe}_{0.89}\text{Ni}_{0.04}\text{Si}_{0.07}$: [Fiquet et al., 2008]; Fe: [Dewaele et al., 2006]).
406 Gray dashes are estimated values of V_P and V_S for $\text{Fe}_{0.936}\text{Ni}_{0.040}\text{Si}_{0.024}$ (Si content ~ 1.2 wt%),
407 neglecting temperature corrections. Light gray dots are estimated values of V_P and V_S for
408 $\text{Fe}_{0.93}\text{Ni}_{0.04}\text{Si}_{0.03}$ (Si content ~ 1.5 wt%) at 13000 Kg/m^3 and 5000 K. For clarity uncertainties
409 in our estimations are not reported.

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