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A Discussion of Reversible and Irreversible Sorption for Sr, Cs, Np, and Pu

By

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1.0 Introduction

Here we discuss the possibility that fission product and actinide sorption is reversible when thermodynamic and kinetic factors are accounted for in predictive models. We do this by reviewing the sorption behavior of Sr, Cs, Np, and Pu, and by reviewing our ability to model their sorption behavior. These elements were selected for review because short-lived Sr and Cs isotopes yield high dose and will be the likely constituents of reprocessed nuclear fuel. Np and Pu are important because they have long half-lives and may be transported in groundwater as dissolved Np species or Pu-containing colloidal solids. Here we highlight modeling approaches that have been used in key publications. No attempt is made to generate a comprehensive model for the radioactive elements listed above.

Ion sorption to mineral and amorphous solids has long been recognized as a process that controls the concentration of radioactive and trace elements in water. This process is particularly important for the transport of contaminants in the Earth's surface environment where sorption may retard transport of contaminants in groundwater by removing the contaminant to the non-mobile solid matrix. Efforts to describe sorption in complex geological settings typically uses a purely empirical approach in which distribution coefficients (K_d) are a measure of distribution of an element between the solid and aqueous phases. Although this approach provides a direct measure of the ability of the solid matrix to sequester the contaminant from a specific solution, its empirical nature does not allow it to be applied outside of the specific parameters of the contaminated site. A broader approach is to measure thermodynamic parameters such as surface complexation constants, to describe sorption as a series of specific reactions between dissolved ions and surface sites. In principle, these thermodynamic data can be combined to build a model that represents the complex systems found in nature, especially when coupled with aqueous speciation, mineral solubility, and kinetic databases.

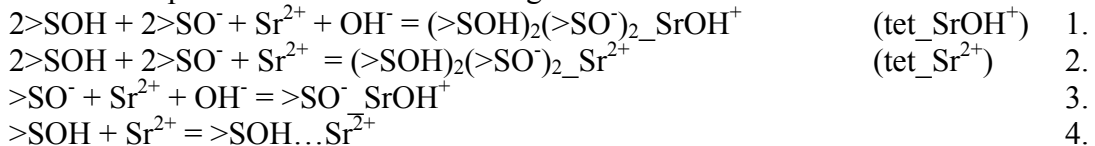
Complicating the accurate prediction of radionuclide fate and transport is the role of redox chemistry and reaction kinetics that control the long-term desorption of some radioactive elements from the solids surfaces back to the solution. For example, Pu sorption and desorption rates are controlled (or at least strongly influenced) by oxidation and reduction rates in solution and on the mineral surface to which it is sorbed (Powell et al., 2010). These complexities are not accounted for by current empirical treatments.

2.0 A predictive surface complexation model using Sr

Generally, alkaline earth elements such as Sr are believed to form outersphere complexes to mineral surfaces, rapidly reach equilibrium and are not limited by reaction kinetics. Here we illustrate a predictive surface complexation model for alkaline earth elements for a wide range of surface substrates by considering the role that strontium sorption may play for the safe disposal of radioactive waste. This is important because, an internally consistent surface complexation database for a wide range of ions and solids found in natural waters that capture the surface charge is still lacking (Ochs et al., 2006). Databases tend to adopt surface complexation models that account for surface charge if only one solid is available for uptake (Dzombak and Morrel, 1980) and non-electrostatic models that ignore surface charge if multiple solids are available for uptake (Davis et al., 1998, Zavarin and Burton, 2004a,b). Similar predictive models are needed for radioactive elements that appear to exhibit irreversible sorption as will be described for Cs, Np, and Pu.

⁹⁰Sr is one of several fission products that are concentrated in nuclear weapon and energy reprocessing waste and may interact with several different oxides depending on the waste form and disposal environment. At the Hanford (Washington, USA) site, caustic liquid waste with high ⁹⁰Sr concentrations was disposed in tanks buried below the subsurface. Some of these tanks have leaked into the subsurface, where the migration of strontium is dependent on both its interaction with natural minerals and the reaction products formed from the interaction of the waste liquid with the subsurface fluvial-glacial sedimentary deposits (Serne et al., 2004; Chorover et al., 2003; Choi et al., 2005). Future disposal of ⁹⁰Sr may include solid waste forms of cement, glass, or ceramics [Bao et al., 2005; Zhang et al., 2005; Grambow, 2006; Nyman and Hobbs, 2006]. The long-term disposal of ⁹⁰Sr depends not only on the stability of the waste form, but also on the sorption of strontium leached from the waste form to possible secondary phases, such as calcite, amorphous silica, iron hydroxides and rutile produced by the degradation of the waste form and corrosion of steel canisters containing the waste.

Sverjensky and colleagues have applied Born solvation and crystal-chemistry theory using a site-occupancy standard state to develop a predictive model for surface protonation, alkali, heavy metal, alkaline earth, and anion sorption (Sverjensky 1993, 1994, 2003, 2005, 2006; Sverjensky and Sahai, 1996, Sahai and Sverjensky, 1997a,b; Criscenti and Sverjensky, 1999, 2002). Carroll et al. (2008) augmented and re-calibrated Sverjensky's model for the prediction of alkaline earth speciation sorbed on oxide surfaces by including the fitted strontium surface complexation reactions for goethite and amorphous silica. Fits to the sorption data using the following surface reactions on goethite and amorphous silica are shown in Figures 1 and 2:



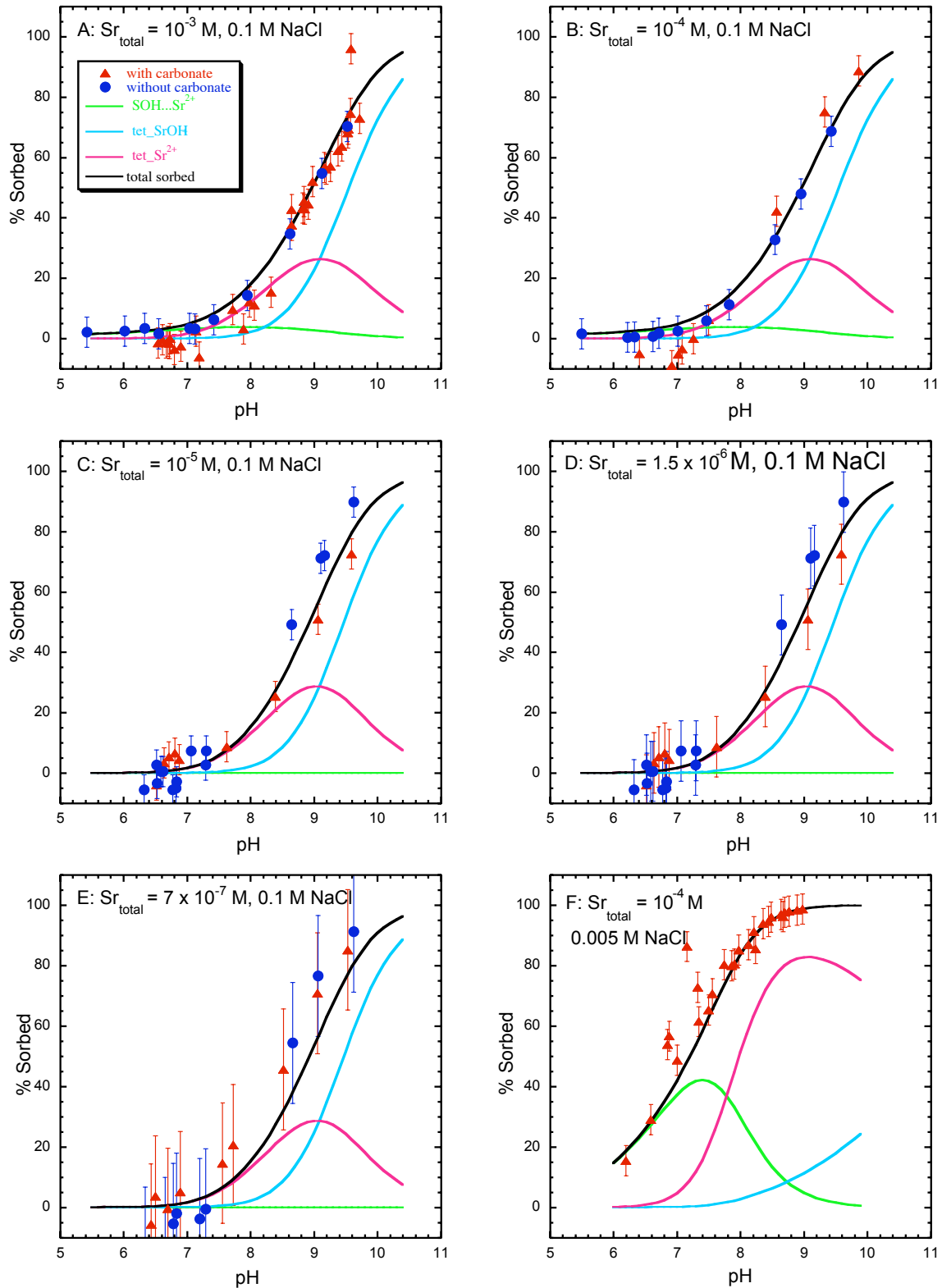


Figure 1. Comparison of experimental and model results for strontium sorption to amorphous silica in 7×10^{-7} to 10^{-3} M SrCl₂ and 0.1 M NaCl solutions with and without dissolved carbonate (A-E), and in 10^{-4} M SrCl₂ and 0.005 M NaCl solutions with dissolved carbonate (F). Symbols are the experimental data and solid lines are fits to the data.

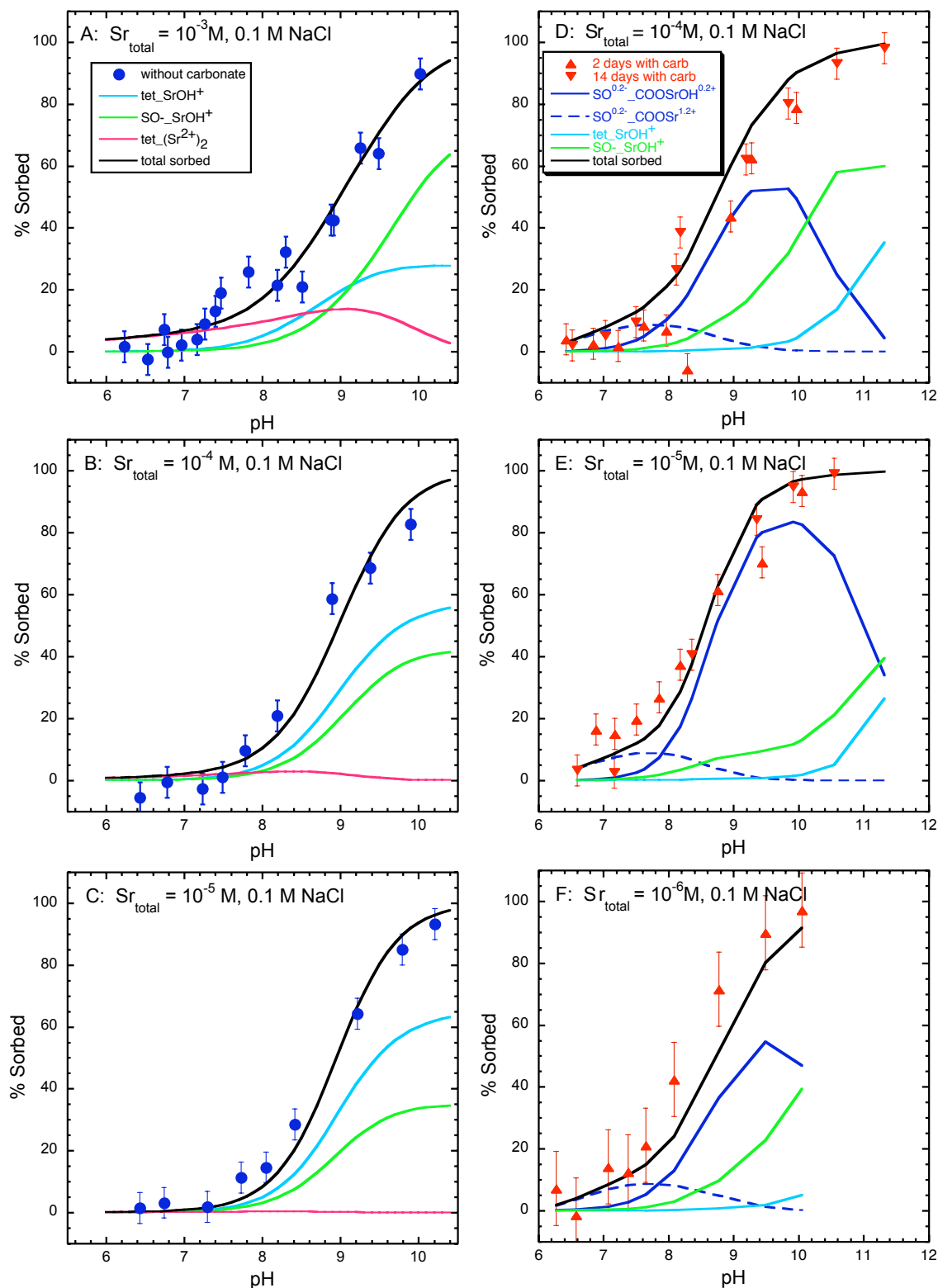


Figure 2. Comparison of experimental and model results for strontium sorption to goethite in 10^{-5} to 10^{-3} M SrCl_2 and 0.1 M NaCl solutions without dissolved carbonate (A-C) and in 10^{-6} to 10^{-4} M SrCl_2 and 0.1 M NaCl solutions with dissolved carbonate (D-F). Symbols are the experimental data and solid lines are fits to the data.

Application of Born solvation and crystal-chemistry theory to metal sorption assumes that the standard Gibbs free energy of sorption ($\Delta G_{r,m}^{\theta}$) depends on contributions from ion solvation ($\Delta G_{s,m}^{\theta}$), electrostatic interactions between the sorbing ion and the surface sites ($\Delta G_{ai,m}^{\theta}$), and contributions specific to the sorbing ion ($\Delta G_{ii,m}^{\theta}$):

$$\Delta G_{r,m}^{\theta} = \Delta G_{s,m}^{\theta} + \Delta G_{ai,m}^{\theta} + \Delta G_{ii,m}^{\theta} \quad 4.$$

such that a given surface complexation equilibrium constant ($\text{Log } K_{r,m}^{\theta}$) can be expressed as:

$$\text{Log } K_{r,m}^{\theta} = -\Delta\Omega_{r,m}/RT*(1/\epsilon_s) - B_m(s/r_m) + \text{log } K''_{ii,m} \quad 5.$$

The first term on the right hand side of equation 5 accounts for ion solvation, where $\Delta\Omega_{r,m}$ is the Born solvation coefficient for the r^{th} reaction containing the metal m and ϵ_s is the dielectric constant for the solid. The second term accounts for the repulsive interaction between the sorbing ion and near surface species, where s is the Pauling's bond strength of the metal-oxygen bonds in the bulk mineral, r_m is the distance the sorbing ion is repulsed by the underlying metal in the solid due to short-range electrostatic interactions, and B_m is a constant characteristic of the surface reaction. The final term represents interactions intrinsic to the sorbing ion as well as solvation contributions from the interfacial dielectric constant and the electrostatic attractive interactions. Equation 5 can be reduced to:

$$\text{Log } K_{r,m}^{\theta} = -\Delta\Omega_{r,m}/RT*(1/\epsilon_s) + \text{log } K''_{ii,m} \quad 6.$$

for a given surface reaction if the repulsive interactions in the electrostatic term are minimal. Linear regressions of $\text{log } K_{r,m}^{\theta}$ versus $1/\epsilon_s$ yield a slope equal to $-\Delta\Omega_{r,m}/RT$ and a y-intercept equal to $\text{log } K''_{ii,m}$ (or $B_m(s/r_m) + \text{log } K''_{ii,m}$ if repulsion interactions are important). This regression serves as a fundamental calibration for the predictive model, because it allows the equilibrium constant for a given surface reaction to be estimated for solids of varying dielectric constants.

Figure 3 compares the difference between equilibrium constants for the formation of $(>\text{SOH})_2(>\text{SO}^-)_2_ \text{MOH}^+$, $(>\text{SOH})_2(>\text{SO}^-)_2_ \text{M}^{2+}$ and $>\text{SO}^-_ \text{MOH}^+$ fitted to sorption data and predicted directly by the regression of $\text{Log } K_{r,m}^{\theta}$ vs $1/\epsilon_s$ (Equation 6) and by substitution of estimated values of $\Delta\Omega_{r,m}$ and $\text{log } K''_{ii,m}$ into Equation 6. The overall alkaline earth model together with its predictive capability suggests that an additive approach can be used to describe sorption reactions in complex geochemical environments. The regression analysis suggests that alkaline earth sorption is largely a function of the solvation of the sorbing cation with minimal contributions between the sorbing cation and metals in the substrate as would be expected for outer-sphere sorption. Although the model can predict equilibrium constants for three non-carbonate surface reactions to within $\pm 0.7 \text{ log } K$, this calibration remains fairly limited.

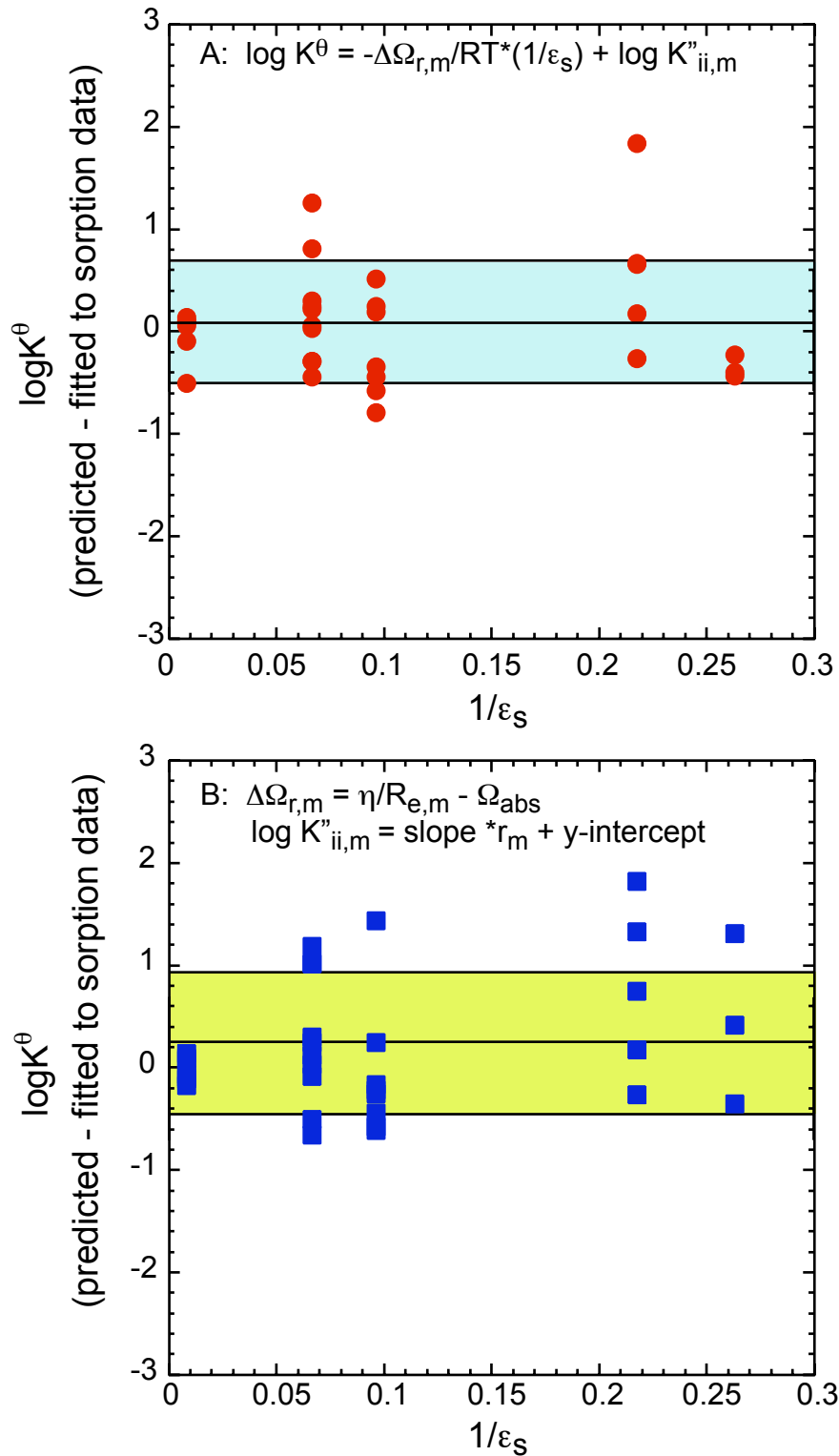


Figure 3. Comparison of $\log K^\theta_{r,m}$ values fitted to sorption data and predicted from Born solvation and crystal chemistry theory using (A) regressions of $\log K^\theta_{r,m} = -\Delta\Omega_{r,m}/RT^*(1/\epsilon_S) + \log K''_{ii,m}$ (Equation 6) and (B) substitution of estimated $\Delta\Omega_{r,m}$ and $\log K''_{ii,m}$ (see Carroll et al, 2008). Colored boxes correspond to standard deviation of 0.6 and 0.7 log K units in A and B respectively.

3.0 A multi-site model to describe reversible ^{137}Cs retardation exchange

^{137}Cs is a by-product of processing of uranium fuels and a major component of nuclear wastes in the United States and other countries around the world. In a few cases, large amounts of ^{137}Cs have been released into the environment accidentally, as at Chernobyl in the former Soviet Union due to a reactor accident and at the Hanford site in the USA as a result of leaking of high level waste (HLW) storage tanks. It is well established that Cs is normally strongly sorbed by the clays and micas (Sawhney, 1970; Francis and Brinkley, 1976; Brouwer et al., 1983; Kemner et al., 1997; Poinssot et al., 1999; Zachara et al., 2002). Cs sorbs via ion exchange reactions to frayed edge sites (FES) on weathered micas and as hydrated cation on planar sites on expansible clays like smectite (Jackson, 1963; Rich and Black, 1964; Sawhney, 1970; Brouwer et al., 1983; Zachara et al., 2002).

Observations of the mobilization of Cs at Hanford led Zachara et al. (2002) and Steefel et al (2003) to conduct a systematic series of exchange experiments over a wide range of Cs^+ , Na^+ , K^+ , and Ca^{2+} concentrations using composite Hanford sediment from the SX tank farm. Their goal was to determine if a multi-site cation exchange model can be used to simulate Cs transport below the leaking Hanford tanks. The column experiments reviewed here provide a direct test of the reversibility of exchange by following the Cs^+ injection with elution of the column with concentrated NaNO_3 or NaOH electrolyte alone (Steefel et al., 2003). Zachara et al. (2002) and Steefel et al (2003) found that multiple exchange sites with different affinities and abundances are needed to capture the large range in the distribution coefficient for Cs (Figure 4). Strong affinity sites are assumed to be associated with the frayed edges sites on weathered micas and weak sites are assumed to be associated with the surfaces of expansible layer silicates. Steefel et al (2003) formulated the multi-site cation exchange using the Gaines–Thomas activity convention, which assumes a reaction stoichiometry of the following form (Appelo and Postma, 1993):



where M is the competing cation (Na^+ , K^+ , Ca^{2+}), m is its charge, and X(i) refers to the i^{th} type of exchange site. The exchange reactions can then be used to write a mass action equation for binary Cs–M exchange:

$$K_{M/Cs} = \frac{[\text{X}(i)_M]^{1/m} [\text{Cs}^+]}{[\text{X}(i)_{Cs}] [\text{M}^{m+}]^{1/m}} \quad 8.$$

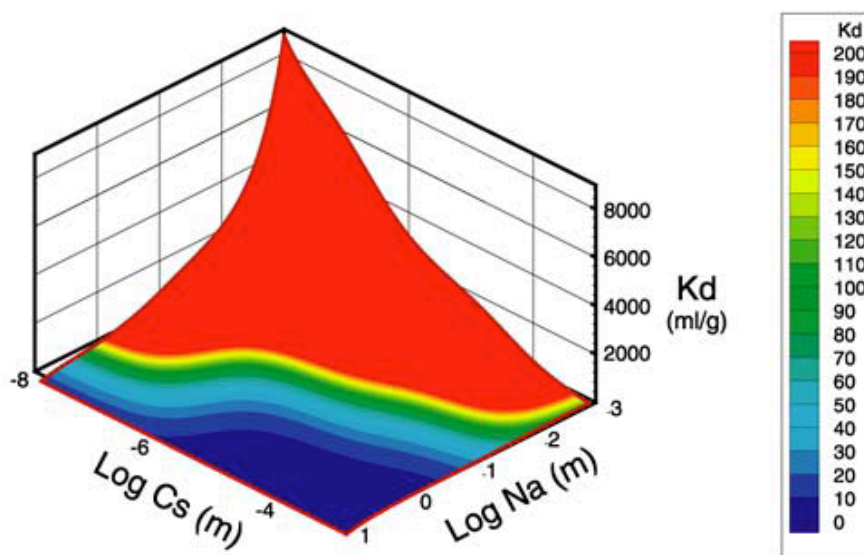


Figure 4: Cs distribution coefficient (K_d) as a function of aqueous Cs and Na concentration for sediment from the SX tank farm, Hanford. Based on a global fit (this paper) of binary exchange data from Zachara et al. (2002). Full range of the K_d (in units of ml/g) is 0 to 8000 as on surface plot—a narrower range of 0-200 is used in color bar for illustration purposes only.

Assessing the reversibility of Cs exchange is crucial for predicting its mobility. Measurements of Cs desorption from contaminated S-SX sediments at Hanford (41-09-39 and SX-108) suggest partial fixation of the sorbed Cs pool (McKinley et al., 2001). The reversibility of Cs exchange was examined by following the sorption stage with a desorption stage using an identical injection solution but without Cs (Figure 5). Column experiments conducted at Cs injection concentrations of 5×10^{-6} and 5×10^{-7} M, and 1 M NaNO_3 were specifically designed to test the reversibility of Cs exchange on FES, since under these conditions exchange on planar sites is minimal. These transport experiments show the strongest evidence for slow uptake of Cs into exchange sites, although it is not clear whether this is a kinetic effect related to slow diffusion into intralamellar sites in micas (e.g., Comans et al., 1991) or to multicomponent equilibrium effects (see Steefel et al 2003 for more details).

It appears that the slow desorption of Cs is primarily the result of the extremely high selectivity of the frayed edge sites for Cs vs. Na, based on the fact that the equilibrium model captures quite well the shape and actual concentrations of Cs during desorption. The slow desorption of Cs, therefore, would appear to be an equilibrium effect and mostly reversible in the thermodynamic sense. Slow diffusion controlled release of Cs, however, cannot be ruled out as a contributor to this effect, since it may be

masked by the very long times required to desorb Cs even under equilibrium conditions. The equilibrium modeling predicts that about 300 pore volumes of 1 M NaNO₃ is required to desorb 95% of the total Cs sorbed in the 5 x 10⁻⁶ M Cs experiment (Figure 5B). The difference between the 72% value actually measured and the 95% predicted by the equilibrium model is primarily the result of the extra mass of Cs sorbed on the Hanford sediment during the Cs uptake stage that was not captured by the modeling. It might be argued, therefore, that this 23% of the total Cs sorbed in this experiment is irreversibly sorbed. In experiments using higher injection concentrations of Cs and where exchange is therefore controlled primarily by sorption to planar sites, there is less evidence for irreversible Cs uptake. Presumably, any irreversible sorption on FES might not be apparent against the background of higher Cs input and output concentrations in these experiments. The Cs elution curves at higher Cs (Fig. 5 A & D) show the closest agreement with the equilibrium exchange model, with only a minor discrepancy observed at Cs elution concentrations within 90% of the injection concentration. Mass balance calculations indicate that 95% of the originally exchanged Cs⁺ was desorbed.

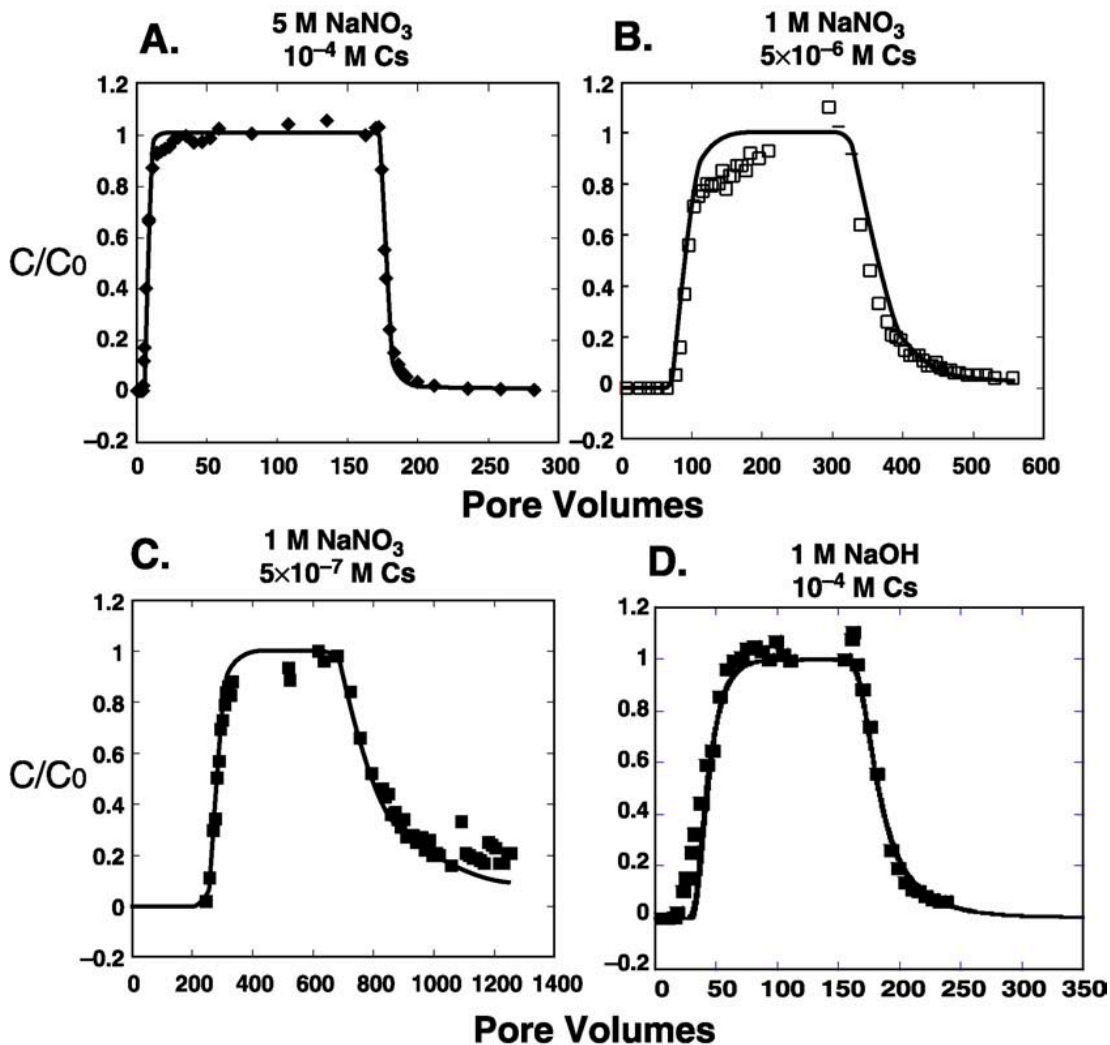


Figure 5. Reversibility of Cs exchange, with equilibrium reactive transport model results based on column weighted parameters to observed Cs elution.

4.0 The role desorption kinetics for Np on goethite

Np desorption in the subsurface will be limited by the rate at which it desorbs from mineral surfaces, unlike the largely equilibrium behaviors of ^{90}Sr and ^{137}Cs . Np desorption studies that assess the reversibility of Np sorption are limited to the numerous Np sorption studies (Keeney-Kennicutt and Morse, 1984; Combes et al., 1992; Girvin et al., 1991; Nakayama and Sakamoto, 1991; Tockiyama, et al., 1995; Kohler et al., 1999; Nakata et al., 2000). Most Np desorption data has been obtained through batch methods and system perturbation (e.g. changes in pH or addition of a complexant). Researchers frequently observed incomplete desorption of Np, suggesting that a fraction of Np is “irreversibly” sorbed. Kenney-Kennicutt and Morse (1984) observed sorption hysteresis in batch experiments with goethite in seawater and distilled water. Nakata et al., (2000) observed greater than 50% desorption of Np from hematite and magnetite into a 1M KCl solution. They also observed an increase in the fraction of unleachable Np over time, even after attempts to leach the Np from the surface with 0.1 M $\text{K}_2\text{C}_2\text{O}_4$.

A recent experimental and modeling study of Np(V) sorption and desorption on goethite was performed by Powell et al (2010) and Tinnacher et al (2010) in a flow-cell system. Figure 6 shows the experimental Np data and fitted results of the adsorption and desorption parts of the experiment. An increase in Np effluent concentration follows each of the stopped-flow periods during the desorption part of the experiment. This indicates that the system did not achieve steady state within the average retention time during flow conditions (50 minutes) and that the Np desorption rate limits the overall reaction. Tinnacher et al (2010) were able to fit the Np sorption and desorption data with a kinetic model based on transition state theory (TST).

Transition state theory has been applied to the kinetics of mineral dissolution reactions (Lasaga 1998), but has not been used before to describe contaminant sorption/desorption kinetics onto minerals. Application of TST allows sorption and desorption rates to be linked to different thermodynamic driving forces and reaction pathways. According to transition state theory, each elementary rate constant (k_f) is proportional to an exponential function of its associated activation energy (E_0)

$$k_f \approx \exp\left(-\frac{E_0}{k_B T}\right) \quad 9.$$

where k_B represents the Boltzmann constant and T temperature in K. High activation energies are related to small rate constants and slow reaction rates, and vice versa. Based on the relationships between kinetics and thermodynamics, the ratio of the forward (R_f) and reverse (R_r) rates of an elementary reaction can be expressed as

$$\frac{R_f}{R_r} = \frac{K_{eq}}{Q} = \exp\left(-\frac{\Delta G}{RT}\right) \quad 10.$$

where K_{eq} is the equilibrium constant, ΔG the free energy change (driving force) of the reaction, and Q the reaction coefficient. For sorption systems, the reaction coefficient represents a conditional sorption constant describing ratios of sorbate and solution

concentrations under non-equilibrium conditions. Thus the net rate of the reaction can be calculated as

$$R_{net} = R_f - R_r = R_f \left(1 - \exp\left(\frac{\Delta G}{RT}\right) \right) = R_f \left(1 - \frac{Q}{K_{eq}} \right) \quad 11.$$

if the reaction is limited by a single elementary reaction. If this is not the case, then equation 11 should be regarded as an empirical relationship describing the net kinetic rate of an overall reaction.

A more general form of the transition rate law formulation is

$$R_{net} = R_f \left(1 - \left(\frac{Q}{K_{eq}} \right)^\Psi \right) \quad 12.$$

where Ψ should primarily be regarded as an empirical parameter for Np sorption.

In principal, transition state theory can be applied to any sorption model.

Tinnacher et al. (2010) found that a 2-site consecutive Freundlich model best fit the data (Figures 6 and 7) describing the change in aqueous Np concentration as:

$$\frac{dC}{dt} = -k_1 C^n \left(1 - \left(\frac{Q_1}{K_1} \right)^{\psi_1} \right) \quad 13.$$

and the change in the abundance of the transfer of Np from the second site to the first site, which represents a slow rate limiting sorption reaction:

$$\frac{dS_2}{dt} = k_2 S_1 \left(1 - \left(\frac{Q_2}{K_2} \right)^{\psi_2} \right) \quad 14.$$

This model calculated activation energies as a function of the direction of the surface reaction by fitting the following parameters: $k_1, k_{-1}, n, \Psi_{1,ad}, \Psi_{1,de}$ for site 1 and $k_2, k_{-2}, \Psi_{2,ad}, \Psi_{2,de}$ for site 2.

Overall their modeling results suggest that desorption kinetics are probably the most important factor controlling Np(V) desorption behavior under constant chemical conditions. Desorption rates are substantially slower than sorption kinetics and show a non-linear dependence on the driving force of the reaction. Aging processes take place after the initial sorption of Np(V) on the mineral surface. Hysteresis in terms of irreversible sorption behavior only plays a minor role if any. Desorption processes in this system are considered kinetically-limited but are not equivalent to irreversible sorption from a chemical perspective. These results are especially relevant for colloid-facilitated transport, since they imply that the reversibility of Np(V) sorption reactions is slow but possible. Slow desorption rates for contaminant desorption from bulk mineral phases may create ‘continuous source terms’ as low concentrations are continuously desorbed over long time-frames, leading to long tailings of contaminant plumes.

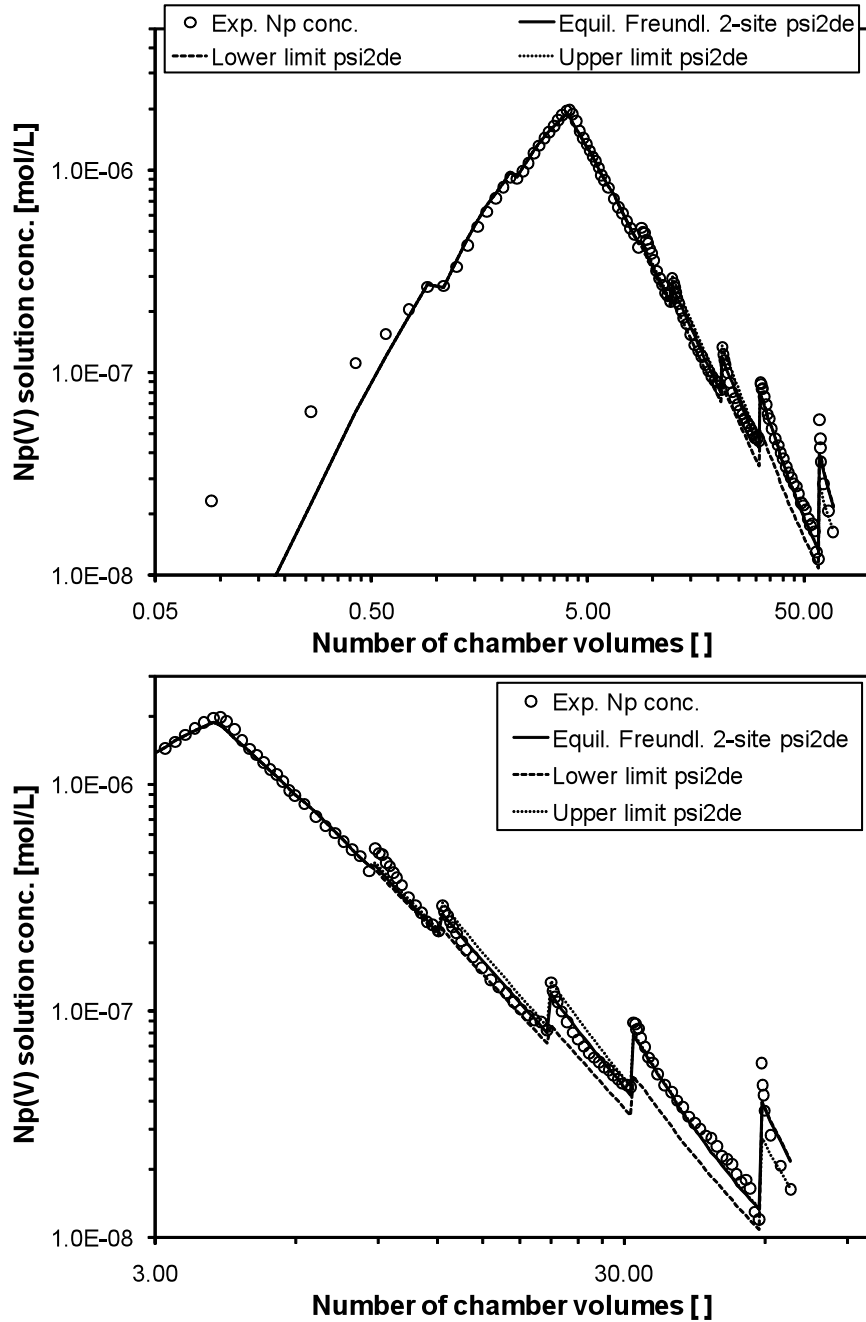


Figure 6. Best model fit with minimum number of fitting parameters: 2-site model including an equilibrium Freundlich site (site 1), a consecutive first order site (site 2) and a fitting parameter $\Psi_{2,de}$. Dashed lines represent calculated model outputs using the upper and lower limit values of $\Psi_{2,de}$ (UL=1.62 $\times 10^{-2}$, LL=3.75 $\times 10^{-3}$).

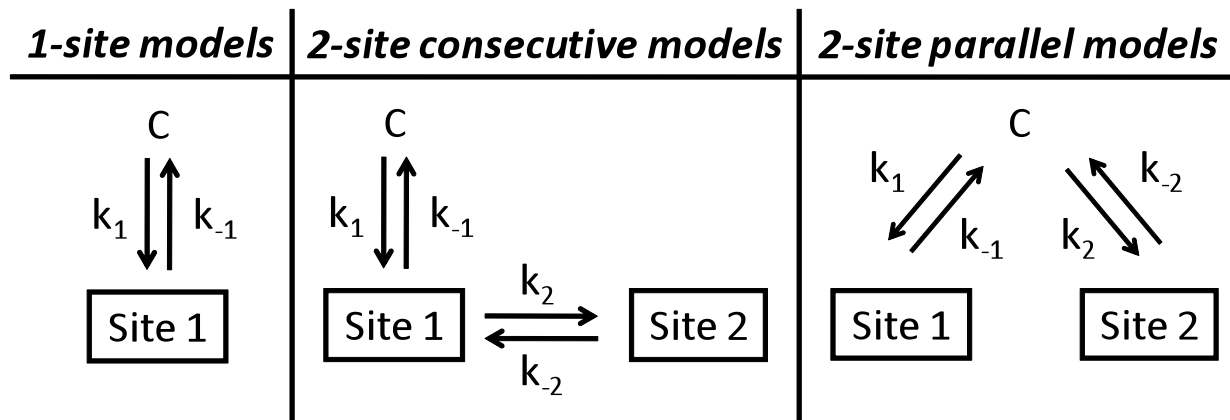


Figure 7. Examples of conceptual models used for the simulation of Np(V) sorption/desorption kinetics to goethite in 1-site and 2-site models. In all models, site 1 represents one of the following types of isotherm-based sorption kinetics: first-order, Langmuir, Freundlich or empirical (Table 1). In 2-site consecutive models, site 2 represents reversible first-order sorption kinetics; in 2-site parallel models site 2 shows the same isotherm kinetics as site 1.

5.0 The role of redox state and desorption kinetics for Pu on goethite

Pu exhibits the largest extent of so-called irreversible sorption of the radioactive elements reviewed here. The mobility of Pu is further complicated by surface-mediated reduction of Pu(V) to Pu(IV) resulting in drastically different sorption behavior. Reduction of Pu(V) to Pu(IV) promotes sorption due to the higher affinity of Pu(IV) for mineral surfaces, relative to Pu(V). Powell et al. (2004) determined an overall rate expression describing Pu(V) reduction by hematite and goethite as a function of solution pH. In continued studies, Powell et al., (2006) found that Pu(IV) was the dominant sorbed oxidation state for all synthetic minerals tested, even on oxidizing minerals such as pyrolusite (β -MnO₂).

The predominance of Pu(IV) on most mineral surfaces and Pu(V) in solution has confounded attempts to directly examine the desorption behavior of each Pu oxidation state. In batch experiments examining Pu desorption from hematite and goethite, less than 1% of the total sorbed Pu (added as either Pu(V) or Pu(IV)) was desorbed in J-13 well water and synthetic groundwater (Lu et al., 1999, 2003). In these studies the oxidation state of the desorbed Pu was not determined. However, the similarity in the desorbed fraction of each system suggests that an equilibrium distribution was reached independent of the initial Pu oxidation state. Incomplete leaching of Pu was observed after re-suspending Pu equilibrated goethite in 0.6 M HClO₄ (Kenney-Kennicutt and Morse, 1985). Furthermore, the fraction of leachable Pu decreased with increasing equilibration time from 1 hour to 30 days (Kenney-Kennicutt and Morse, 1985). This suggests that Pu became more strongly associated with the solids phase over time. This “aging effect” was also observed by Powell et al (2004, 2005) in similar experiments with goethite, hematite, and magnetite.

Tinnacher is currently applying the kinetic modeling approach that is described for Np above to Pu sorption/desorption kinetics on goethite. Here we comment on the experimental data of Powell et al. (2010). The high affinity of Pu uptake on goethite surfaces is shown in flow-through sorption/desorption experiments by the low ratio of Pu

output to input concentrations during the sorption and the additional losses of aqueous Pu to the solid when flow was periodically stopped (Figure 8 and 9; Powell et al., 2010). Very low amounts of Pu desorb from goethite suggesting that kinetics play a key role for the partitioning of Pu back into solution (Figure 9). It is important to emphasize here, that sorption rates are non-zero. A steady decrease in the Pu concentration during active flow suggests there is a type of “aging” effect that caused desorption of Pu to become more unfavorable over the course of the experiment. Only 0.5% of the sorbed Pu was desorbed after passing 122 chamber volumes of Pu-free solution through the flow cell. Powell et al (2010) hypothesize that the “aging effect” represents the repartitioning of sorbed Pu to more energetically favorable, strongly sorbing sites similar to the 2-site consecutive model that was developed for Np (Figure 7). The desorption rate was presumed to be limited by the oxidation of sorbed Pu(IV) to Pu(V) as a result of the previous surface mediated reduction of Pu(V) to Pu(IV) during adsorption.

Pu desorption processes are considered kinetically-limited but are not equivalent to irreversible sorption from a chemical perspective. These results are especially relevant for colloid-facilitated transport, since they imply that the reversibility of Pu sorption reactions may create ‘continuous source terms’ as low concentrations are continuously desorbed over long time-frames, leading to long tailings of contaminant plumes.

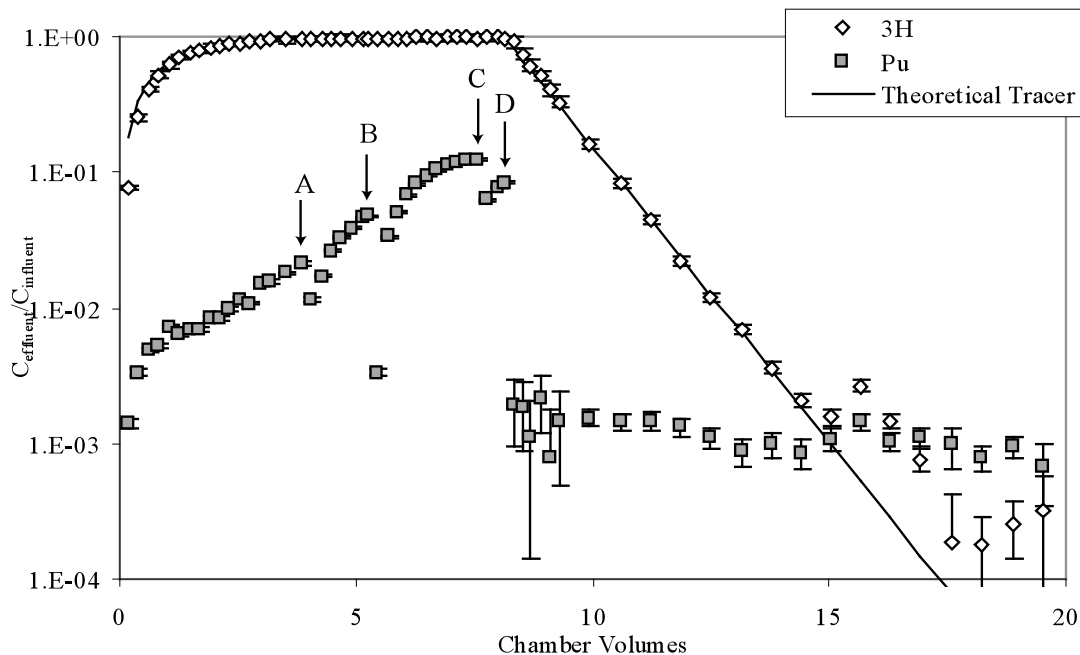


Figure 8: Pu and ^3H effluent profile from stirred flow-cell at pH 8. During the sorption step (0 to 8.3 chamber volumes) the background solution amended with 2.6 nM Pu(V) and 1000 cpm mL $^{-1}$ ^3H was pumped through the flow-cell. During the desorption step (started at point D above) only the background solution was pumped through the flow-cell. Arrows indicate periods of stopped flow for A) 1 hours, B) 18.5 hours, C) 1 hour, and D) 66 hours (also start of the desorption step). Solid line represents theoretical non-reactive tracer calculated using Equations 5 and 6 for the sorption and desorption steps, respectively. System parameters: Flow-rate = 12 mL hr $^{-1}$; Cell volume = 10 mL; Background solution: 5 mM NaCl, 0.7 mM NaHCO $_3$, pH 8.

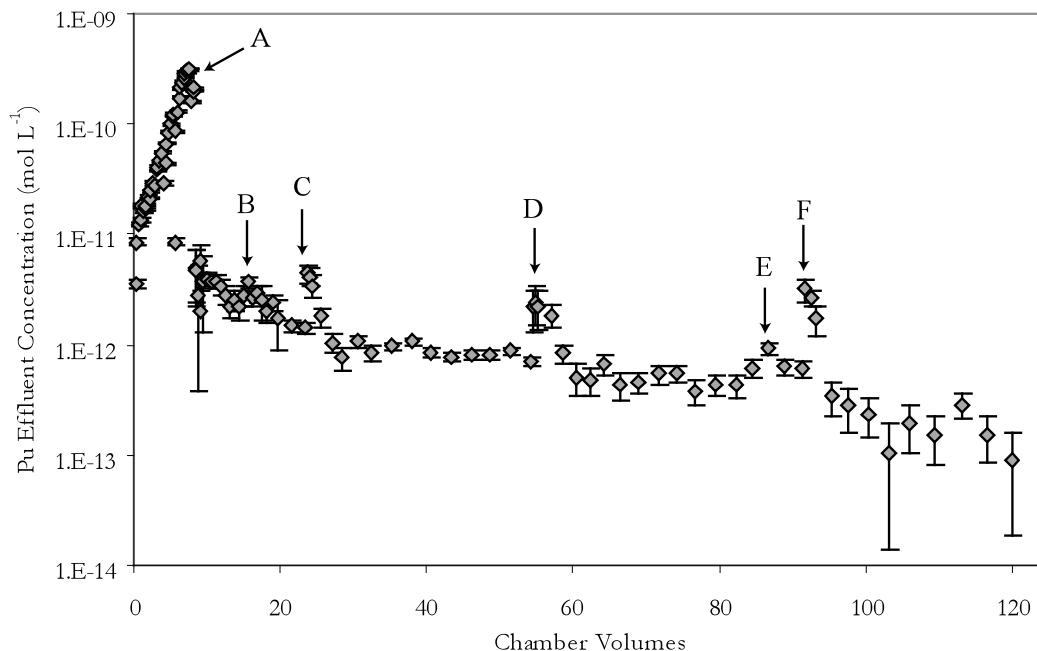


Figure 9: Pu aqueous concentration in the flow-cell effluent representing both sorption and desorption steps at pH 8. During the sorption step (0 to 8.3 chamber volumes) the background solution amended with 2.6 nM Pu(V) and 1000 cpm mL⁻¹ ³H was pumped through the flow-cell. During the desorption step (started at point D above) only the background solution was pumped through the flow-cell. Arrows indicate periods of stopped flow for A) start of desorption step, 66.0 hours, B) 16.3 hours, C) 42.0 hours, D) 96.0 hours, E) flow-rate decreased to 3 mL hr⁻¹, and F) 161.2 hours. System parameters: Flow-rate = 12 mL hr⁻¹; Cell volume = 10 mL; Background solution: 5 mM NaCl, 0.7 mM NaHCO₃, pH 8.

6.0 Summary

Review of key sorption/desorption studies show that Sr, Cs, Np, and Pu cannot be described using only a single, linear distribution coefficient in fate and transport models. All four radioactive elements require multiple sites to capture their sorption behavior over a range of conditions. Equilibrium surface complexation or ion exchange reactions can adequately capture the uptake and release of Sr and Cs over a wide range of ionic strength, total element concentration, and solution pH. Several elements exhibit aging effects where quantification of desorption kinetics are important. This is especially true for Np and Pu transport, but also true for Cs.

This report provides the background information needed to develop a research program for the robust risk assessment radioactive waste disposition in geologic environments. Challenges to state-of-the-art predictive modeling reside in quantification of sorption/desorption rates and identification of appropriate mechanistic modeling approaches. Temperature effects are a fundamental issue that is directly linked (via activation energy) to our understanding of sorption/desorption kinetics and our ability to predict actinide and trace element behavior under thermohydrologically complex conditions.

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