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EVALUATION OF ARG-1 SAMPLES PREPARED BY CESIUM CARBONATE DISSOLUTION DURING THE ISOLOK SME ACCEPTABILITY TESTING

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REVIEWS AND APPROVALS

AUTHORS:

EXECUTIVE SUMMARY

Evaluation of the Defense Waste Processing Facility (DWPF) Chemical Process Cell (CPC) cycle time identified several opportunities to improve the CPC processing time. The Mechanical Systems & Custom Equipment Development (MS&CED) Section of the Savannah River National Laboratory (SRNL) recently completed the evaluation of one of these opportunities — the possibility of using an Isolok sampling valve as an alternative to the Hydragard valve for taking DWPF process samples at the Slurry Mix Evaporator (SME). The use of an Isolok for SME sampling has the potential to improve operability, reduce maintenance time, and decrease CPC cycle time. The SME acceptability testing for the Isolok was requested in Task Technical Request (TTR) HLW-DWPF-TTR-2010-0036 and was conducted as outlined in Task Technical and Quality Assurance Plan (TTQAP) SRNL-RP-2011-00145. RW-0333P QA requirements applied to the task, and the results from the investigation were documented in SRNL-STI-2011-00693.

The objective of that study was to qualify the Isolok for use in sampling the Slurry Mix Evaporator (SME) tank at the DWPF. Measurement of the chemical composition of study samples was a critical component of the SME acceptability testing of the Isolok. A sampling and analytical plan, SRNL-RP-2011-00294, supported the investigation with the analytical plan directing that the study samples be prepared by a cesium carbonate (Cs_2CO_3) fusion dissolution method and analyzed by Inductively Coupled Plasma – Optical Emission Spectroscopy (ICP–OES). The use of the cesium carbonate preparation method for the Isolok testing provided an opportunity for an additional assessment of this dissolution method, which is being investigated as a potential replacement for the two methods (i.e., sodium peroxide fusion and mixed acid dissolution) that have been used at the DWPF for the analysis of SME samples. The $Cs₂CO₃$ testing associated with the Isolok testing does provide additional insight into the performance of the method as conducted by SRNL. The performance is to be investigated by looking to the composition measurement data generated by the samples of a standard glass, the Analytical Reference Glass – 1 (ARG-1), that were prepared by the Cs_2CO_3 method and included in the SME acceptability testing of the Isolok. The measurements of theses samples were presented in SRNL-STI-2011-00693, but no statistical analysis of these measurements was conducted as part of those results.

The ARG-1 measurements, as weight percent (wt%) oxides, generated during the SME acceptability testing for the Isolok are statistically analyzed in this report. Three sources of variation in these measurements were explored: variation due to preparation block effects, variation due to ICP-OES analytical block effects, and within block variation for these measurements, where the within block variation is due to the repeatability of the preparation process for a given preparation block and to the variation in the measurements during an analytical block of work that is due to the repeatability of the ICP-OES measurement process. These results suggest that differences among the preparation blocks played an insignificant role in the variation seen in the ARG-1 results over the course of the Isolok testing. From this investigation, the components of variation (i.e., the analytical block-to-block effects and the within-block effects) as % relative standard deviations are less than 5% for those oxides at concentrations of 0.1 wt% or greater. A bound on the bias in the Cs_2CO_3 method of its measurements for each oxide of interest value is also provided at a 95% confidence. For those oxides present in ARG-1 at concentrations greater than or equal to 0.1 wt%, only B_2O_3 has a bias bound (its value is 9.84%) that is larger than 4.41% (the value for MnO). Thus, only B_2O_3 has a bias bound that is larger than 5%.

The low bias for boron measurements is almost certainly due to volatilization of boron at the 1050 °C fusion conditions of the Cs_2CO_3 method. Cesium species also can be volatilized under these conditions and it is believed that a carrier distillation effect results in the loss of boron. The relatively high fusion temperature was used in anticipation of needing very rigorous fusion conditions for dissolving a 1-1.5 gram wafer of glass that potentially results from vitrifying a 3 mL SME sample taken with the Isolok sampler. Experiments performed at the DWPF Laboratory and at SRNL indicate that the low boron bias from the Cs_2CO_3 method is essentially eliminated when the method is carried out at 900 °C. The lower fusion temperature is effective for attacking powdered glass and small shards of glass, but may not result in complete attack of a1.5 gram wafer of glass.

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LIST OF ABBREVIATIONS

1.0 Introduction

Evaluation of Defense Waste Processing Facility (DWPF) Chemical Process Cell (CPC) cycle time identified several opportunities to improve the CPC processing time. The Mechanical Systems & Custom Equipment Development (MS&CED) Section of the Savannah River National Laboratory (SRNL) recently completed the evaluation of one of these opportunities — the possibility of using an Isolok sampling valve as an alternative to the Hydragard valve for taking DWPF process samples at the Slurry Mix Evaporator (SME). The use of an Isolok for SME sampling has the potential to improve operability, reduce maintenance time, and decrease CPC cycle time. The SME acceptability testing for the Isolok was requested in Task Technical Request (TTR) HLW-DWPF-TTR-2010-0036 [1] and was conducted as outlined in Task Technical and Quality Assurance Plan (TTQAP) SRNL-RP-2011-00145 [2]. RW-0333P QA requirements applied to the task, and the results from the investigation were documented in SRNL-STI-2011-00693 [3].

Measurement of the chemical composition of study samples was a critical component of the SME acceptability testing of the Isolok. A sampling and analytical plan [4] supported the investigation with the analytical plan directing that the study samples be prepared by a cesium carbonate (Cs_2CO_3) fusion dissolution method and analyzed by Inductively Coupled Plasma – Optical Emission Spectroscopy (ICP–OES). The use of the cesium carbonate preparation method for the Isolok testing provided an opportunity for an additional assessment of this dissolution method, which is being investigated as a potential replacement for the two methods (i.e., sodium peroxide fusion and mixed acid dissolution) that have been used at the DWPF for the analysis of SME samples. Earlier testing of the Cs_2CO_3 method yielded promising results [5]-[7] which led to a TTR [8] from Savannah River Remediation, LLC (SRR) to SRNL for additional support and an associated TTQAP [9] to direct the SRNL efforts. A technical report [8] resulting from this work was issued that recommended that the mixed acid method be replaced by the Cs_2CO_3 method for the measurement of magnesium (Mg), sodium (Na), and zirconium (Zr) with additional testing of the method by DWPF Laboratory being needed before further implementation of the Cs_2CO_3 method at that laboratory.

While the SME acceptability testing of the Isolok does not address any of the open issues remaining after the publication of the recommendation for the replacement of the mixed acid method by the $Cs₂CO₃$ method [10] (since those issues are to be addressed by the DWPF Laboratory), the Cs₂CO₃ testing associated with the Isolok testing does provide additional insight into the performance of the method as conducted by SRNL. The performance is to be investigated by looking to the composition measurement data generated by the samples of a standard glass, the Analytical Reference Glass – 1 (ARG-1), that were prepared by the $Cs₂CO₃$ method and included in the SME acceptability testing of the Isolok. The measurements of these samples were presented as part of the study results [3], but no statistical analysis of these measurements was conducted as part of those results. It is the purpose of this report to provide that analysis, which was supported using JMP Version 7.0.2 [11].

2.0 Discussion

The ARG-1 measurements, as weight percent $(wt\%)$ oxides, that are of interest in this investigation are provided in Table A1 in the Appendix. The values were generated by the analytical plan [4] that was issued to support the SME acceptability testing conducted for the Isolok. Table A2 in the Appendix provides the reference composition of the ARG-1 standard as wt% oxides.

2.1 Initial Plots of the Measurements

Exhibit A1 in the Appendix provides a series of plots by oxide of the measurements of Table A1 grouped by test phase, preparation groupings, and analytical groupings. The sample ID and the targeted value for each oxide from Table A2 are also shown as part of the information on the x-axis of each plot. The average of all of the measurements over all three test phases is shown on each plot as a horizontal line. Included in this exhibit is a plot of the sums of oxides for the measurements.

Some interesting observations can be made for the sum of oxides plot. As seen in this plot, the targeted sum for the ARG-1 oxides of interest in this report was 99.43 wt%. Eight of the 54 sums (i.e., \sim 14.8%) fall outside of the interval from 95 to 105 wt%, where this interval is typically used as one of the metrics in assessing the analytical process that was used to generate the chemical composition measurements. There are two aspects of these results that are worth noting here. One is that those samples showing a low sum of oxides also show low recoveries for many of the other oxides, not just $SiO₂$. Of even more interest is the fact that 6 of the 8 samples that have a sum that falls below the 95% value are actually measured in two analytical blocks but their sum only falls below the 95% value in one of the two blocks. See Table 1. This suggests that the preparation of the samples was not an issue in the low sums of oxides seen for some of the results, but the likely problem was the performance of the ICP-OES instrumentation or human errors such mislabeling of sample bottles or an error during sample dilution. There is also a suggestion that one of the bigger contributors to the variation seen in the measurements for all of the oxides is the repeatability of the measurements by the ICP-OES instrumentation. The sources of variation are investigated in the next section.

Test	Preparation Block	Analytical Block	Sample ID	Measurement
Phase 1			$ARG-1B22$	99.62
Phase 1			$ARG-1B22$	91.63
Phase 1		3	$ARG-1B33$	102.38
Phase 1		h	$ARG-1B33$	94.27
Phase 2	っ	っ	$ARG-1B21$	92.86
Phase 2	2		$ARG-1B21$	98.08
Phase 2	\mathfrak{D}	2	$ARG-1B23$	98.93
Phase 2			$ARG-1B23$	93.79
Phase 2		3	$ARG-1B31$	93.92
Phase 2		6	$ARG-1B31$	98.00
Phase 2	3	3	$ARG-1B33$	101.05
Phase 2			$ARG-1B33$	92.75

Table 1. A Subset of the Sums of Oxides Values

2.2 Preparation Block versus ICP-OES Analytical Block Variation

For those ARG-1 samples that were measured twice during the Isolok testing, once in each of two different ICP-OES analytical blocks, there is an opportunity to estimate the variation in these measurements due to preparation block effects and the variation due the ICP-OES analytical block effects. These variations are assessed relative to the within block variation for these measurements,

where the within block variation is due to the repeatability of the preparation process for a given preparation block and to the variation in the measurements during an analytical block of work that is due to the repeatability of the ICP-OES measurement process. The statistical model for the measurement of each of the oxides of interest that facilitates the estimation of the components of variance is given by:

Equation 1.

 $y_{ijk} = \mu + p_i + a_{j(i)} + e_{ijk}$

where

- y_{ijk} is the measurement of the kth sample in analytical block j for a sample prepared in preparation block i,
- μ represents the average measurement for the given oxide,
- p_i represents a random effect for the ith preparation block that captures block-to-block effects,
- $a_{i(i)}$ represents a random effect for the jth analytical block nested within the ith preparation block, this random effect captures block-to-block effects for the analytical process, and
- e_{ijk} represents the within block variation, and as described above this variation is due to the repeatability of the preparation process for a given preparation block and to the variation in the measurements during an analytical block of work that is due to the repeatability of the ICP-OES measurement process.

The a's in this model are assumed to be normally distributed with a zero mean and with a constant but unknown standard deviation that may be represented by σ_a . The p's in the model are assumed to be normally distributed with a zero mean and with a constant but unknown standard deviation that may be represented by σ_{p} . The e's in this model are random effects that are assumed to be normally distributed with a zero mean and with a constant but unknown standard deviation that may be represented by σ_e .

To facilitate the analysis of this model using JMP, the preparation blocks and analytical blocks were uniquely tied to the test phases as indicated in Exhibit 1. The results from the JMP analysis are provided in Exhibit A2 in the Appendix, and they include tests for the statistical significance of two components of variation of the model in equation (1) (i.e., σ_p and σ_a) relative to the size of the within block component, i.e., the standard deviation, σ_e . The outcome of one of these tests indicates a statistically significant component of variation by its p-value, which is labeled as "**Prob > F**" in the portion of the results with the heading "**Tests wrt Random Effects**." When the p-value is less than 0.05, then the estimated component of variation is statistically significant at the 5% level. To help with this interpretation, the p-values in Exhibit A2 have been shaded: green if the variance component is not statistically significant and red if it is. The estimated variance for the analytical blocks is statistically significant for several of the oxides (specifically, B_2O_3 , Li₂O, MgO, MnO, and NiO), while the estimated variance for the preparation blocks is statistically significant for only CuO and ZnO (two minor oxides for ARG-1). These results suggest that differences among the preparation blocks played an insignificant role in the variation seen in the ARG-1 results over the course of the Isolok testing. This allows for the use of a less complex model with a more complete set of the measurements.

Exhibit 1. Nested, Random Effects Model for Preparation and Analytical Block Effects

2.3 ICP-OES Analytical Block Variation

In this section two sources for the variation in the ARG-1 measurements is investigated: an ICP-OES analytical block-to-block effect and the within analytical block variation. For this analysis, all of the ARG-1 measurements were used. Once again, the within block variation is due to the repeatability of the preparation process for a given preparation block and to the variation in the measurements during an analytical block of work that is due to the repeatability of the ICP-OES measurement process. The statistical model for the measurement of each of the oxides of interest that facilitates the estimation of the components of variance is given by:

Equation 1.

$$
y_{ij} = \mu + a_i + e_{ij}
$$

where

- y_{ij} is the measurement of the jth sample in analytical block i for a prepared sample,
- μ represents the average measurement for the given oxide,
- a_i represents a random effect for the ith analytical block that captures block-to-block effects,
- e_{ii} represents the within block variation, and as described above this variation is due to the repeatability of the preparation process for a given preparation block and to the variation in the measurements during an analytical block of work that is due to the repeatability of the ICP-OES measurement process.

The a's in this model are assumed to be normally distributed with a zero mean and with a constant but unknown standard deviation that may be represented by σ_a . The e's in this model are random effects that are assumed to be normally distributed with a zero mean and with a constant but unknown standard deviation that may be represented by σ_{e} .

To facilitate the analysis of this model using JMP, the analytical blocks were uniquely tied to the test phases as indicated in Exhibit 2. The results from the JMP analysis are provided in Exhibit A3 in the Appendix, and they include a test for the statistical significance of the σ_{α} variation of the model in equation (1) relative to the size of the within block variation, i.e., the standard deviation, σ_e . The outcome of one of these tests indicates a statistically significant component of variation by its p-value, which is labeled as "**Prob > F**" in the portion of the results with the heading "**Tests wrt Random**

Effects." When the p-value is less than 0.05, then the estimated block-to-block component of variation is statistically significant at the 5% level. To help with this interpretation, the p-values in Exhibit A3 have been shaded: green if the variance component is not statistically significant and red if it is. The estimated variance for the analytical blocks is statistically significant for several of the oxides (especially, B_2O_3 , BaO, CaO, Cr₂O₃, CuO, Li₂O, MgO, MnO, and NiO). These results suggest that differences among the analytical blocks can play a significant role in the variation seen in the ARG-1 results.

Exhibit 2. Random Effects Model for Analytical Block Effects

In Table 2, the information from Exhibit A3 for each oxide is summarized and used to determine a 95% confidence interval for the mean of the measurements for each oxide. If the confidence interval for an oxide does not contain the reference concentration for that oxide (also provided in Table 2), then there is a statistically significant bias (at the 5% level) in the measurements. The results in Table 2 indicate that there are biases for all of the oxides except CaO, K_2O , Na_2O , SiO_2 , and TiO_2 . Regardless of the statistical significance of the bias, a bound on its value (at a 95% confidence) is also provided in Table 2. For those oxides present in ARG-1 at concentrations greater than or equal to 0.1 wt%, only B_2O_3 has a bias bound (its value is 9.84%) that is larger than 4.41% (the value for MnO). Thus, only B_2O_3 has a bias bound that is larger than 5%.

The low bias for boron measurements is almost certainly due to volatilization of boron at the 1050 $^{\circ}$ C fusion conditions of the Cs_2CO_3 method. Cesium species also can be volatilized under these conditions, and it is believed that a carrier distillation effect results in the loss of boron. The relatively high fusion temperature was used in anticipation of needing very rigorous fusion conditions for dissolving a 1-1.5 gram wafer of glass that potentially results from vitrifying a 3 mL SME sample taken with the Isolok sampler. Experiments performed at the DWPF Laboratory and at SRNL indicate that the low boron bias from the Cs_2CO_3 method is essentially eliminated when the method is carried out at 900 °C. The lower fusion temperature is effective for attacking powdered glass and small shards of glass, but may not result in complete attack of a1.5 gram wafer of glass.

Also, note that Table 2 presents the components of variation (i.e., the analytical block-to-block effects and the within-block effects) as % relative standard deviations, and from Table 2, all of these values are less than 5% for those oxides at concentrations of 0.1 wt% or greater.

Table 2. Summary of Results from the Model of Random Analytical Block Effects

3.0 Conclusions

The ARG-1 measurements, as wt% oxides, generated during the SME acceptability testing for the Isolok are statistically analyzed in this report. Three sources of variation in these measurements were explored: variation due to preparation block effects, variation due the ICP-OES analytical block effects, and within block variation for these measurements, where the within block variation is due to the repeatability of the preparation process for a given preparation block and to the variation in the measurements during an analytical block of work that is due to the repeatability of the ICP-OES measurement process. These results suggest that differences among the preparation blocks played an insignificant role in the variation seen in the ARG-1 results over the course of the Isolok testing. From this investigation, the components of variation (i.e., the analytical block-to-block effects and the within-block effects) as % relative standard deviations are less than 5% for those oxides at concentrations of 0.1 wt% or greater. A bound on the bias in the Cs_2CO_3 method of its measurements for each oxide of interest value is also provided at a 95% confidence. For those oxides present in ARG-1 at concentrations greater than or equal to 0.1 wt%, only B_2O_3 has a bias bound (its value is 9.84%) that is larger than 4.41% (the value for MnO). Thus, only B_2O_3 has a bias bound that is larger than 5%. The low boron bias results from boron volatilization at the 1050 °C fusion conditions used to enable the Cs_2CO_3 method to completely attack large wafers of glass.

4.0 References

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5.0 Appendix

Supplemental Tables and Exhibits

Table A1. ARG-1 Measured Oxide Concentrations (part 1)

Table A1. ARG-1 Measured Oxide Concentrations (part 1)

Table A1. ARG-1 Measured Oxide Concentrations (part 2)

Table A1. ARG-1 Measured Oxide Concentrations (part 2)

Analyte=B2O3 (wt%)

Analyte=CaO (wt%)

Analyte=CuO (wt%)

Analyte=K2O (wt%)

Analyte=MgO (wt%)

Analyte=Na2O (wt%)

Analyte=SiO2 (wt%)

Analyte=TiO2 (wt%)

Analyte=ZrO2 (wt%)

Response Measurement Analyte=Al2O3 (wt%), Target Value=4.73 Summary of Fit

RSquare 0.476283
RSquare Adj 0.236246 RSquare Adj 0.236246
Root Mean Square Error 0.117536 Root Mean Square Error 0.117536
Mean of Response 4.624026 Mean of Response 4.624026
Observations (or Sum Wets) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

Variance Component Estimates

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=B2O3 (wt%), Target Value=8.67 Summary of Fit

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value.

Response Measurement Analyte=BaO (wt%), Target Value=0.09 Summary of Fit

RSquare 0.483184
RSquare Adj 0.246309 RSquare Adj 0.246309
Root Mean Square Error 0.003393 Root Mean Square Error 0.003393
Mean of Response 0.092217 Mean of Response 0.092217
Observations (or Sum Wets) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

Variance Component Estimates

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=CaO (wt%), Target Value=1.43 Summary of Fit

RSquare 0.55286
RSquare Adi 0.347921 RSquare Adj 0.347921
Root Mean Square Error 0.037126 Root Mean Square Error Mean of Response 1.445879
Observations (or Sum Wgts) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value.

Response Measurement Analyte=Cr2O3 (wt%), Target Value=0.09 Summary of Fit

RSquare 0.642053
RSquare Adj 0.477994 RSquare Adj 0.477994
Root Mean Square Error 0.004037 Root Mean Square Error 0.004037
Mean of Response 0.098276 Mean of Response 0.098276
Observations (or Sum Wets) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

Variance Component Estimates

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=CuO (wt%), Target Value=0 Summary of Fit

RSquare 0.931258
RSquare Adj 0.899751 RSquare Adj 0.899751
Root Mean Square Error 0.002567 Root Mean Square Error 0.002567
Mean of Response 0.009868 Mean of Response 0.009868
Observations (or Sum Wgts) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value.

Response Measurement Analyte=Fe2O3 (wt%), Target Value=14 Summary of Fit

RSquare 0.315326
RSquare Adj 0.001517 RSquare Adj 0.001517
Root Mean Square Error 0.337976 Root Mean Square Error 0.337976
Mean of Response 13.88874 Mean of Response 13.88874
Observations (or Sum Wets) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

Variance Component Estimates

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=K2O (wt%), Target Value=2.71 Summary of Fit

RSquare 0.386106
RSquare Adj 0.104737 RSquare Adj 0.104737
Root Mean Square Error 0.119957 Root Mean Square Error 0.119957
Mean of Response 2.69295 Mean of Response 2.69295
Observations (or Sum Wets) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Response Measurement Analyte=Li2O (wt%), Target Value=3.21 Summary of Fit

RSquare 0.501718
RSquare Adj 0.273339 RSquare Adj 0.273339
Root Mean Square Error 0.074837 Root Mean Square Error 0.074837
Mean of Response 3.164763 Mean of Response 3.164763
Observations (or Sum Wgts) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

Variance Component Estimates

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=MgO (wt%), Target Value=0.86 Summary of Fit

RSquare 0.568216
RSquare Adi 0.370315 RSquare Adj 0.370315
Root Mean Square Error 0.020047 Root Mean Square Error 0.020047
Mean of Response 0.841495 Mean of Response 0.841495
Observations (or Sum Wgts) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Response Measurement Analyte=MnO (wt%), Target Value=1.89 Summary of Fit

RSquare 0.584912
RSquare Adj 0.394663 RSquare Adj 0.394663
Root Mean Square Error 0.044103 Root Mean Square Error 0.044103
Mean of Response 1.828483 Mean of Response 1.828483
Observations (or Sum Wets) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=Na2O (wt%), Target Value=11.5 Summary of Fit

RSquare 0.366715
RSquare Adj 0.07646 RSquare Adj 0.07646
Root Mean Square Error 0.303192 Root Mean Square Error Mean of Response 11.46699
Observations (or Sum Wgts) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value.

Response Measurement Analyte=NiO (wt%), Target Value=1.05 Summary of Fit

RSquare 0.60098
RSquare Adj 0.418095 RSquare Adj 0.418095
Root Mean Square Error 0.026981 Root Mean Square Error 0.026981
Mean of Response 1.018919 Mean of Response 1.018919
Observations (or Sum Wets) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=SiO2 (wt%), Target Value=47.9 Summary of Fit

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Response Measurement Analyte=Sum of Oxides (wt%), Target Value=99.43 Summary of Fit

RSquare 0.407881
RSquare Adj 0.136494 RSquare Adj 0.136494
Root Mean Square Error 2.407604 Root Mean Square Error 2.407604
Mean of Response 98.39457 Mean of Response 98.39457
Observations (or Sum Wgts) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=TiO2 (wt%), Target Value=1.15 Summary of Fit

RSquare 0.444705
RSquare Adj 0.190195 RSquare Adj 0.190195
Root Mean Square Error 0.028767 Root Mean Square Error 0.028767
Mean of Response 1.147074 Mean of Response 1.147074
Observations (or Sum Wgts) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value.
Test Demonstration Sunthering **Test Denominator Synthesis**

Response Measurement Analyte=ZnO (wt%), Target Value=0.02 Summary of Fit

RSquare 0.424851
RSquare Adj 0.161241 RSquare Adj 0.161241
Root Mean Square Error 0.001236 Root Mean Square Error 0.001236
Mean of Response 0.024322 Mean of Response 0.024322
Observations (or Sum Wets) 36 Observations (or Sum Wgts)

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

Variance Component Estimates

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Tests wrt Random Effects

Response Measurement Analyte=ZrO2 (wt%), Target Value=0.13 Summary of Fit

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Source 58 MS Num DF Num F Ratio Prob > F
Phase-AB&Random 2.5766 0.15156 17 2.1995 0.0231

Source SS MS Num DF Num F Ratio Prob > F Phase-AB&Random 0.04557 0.00268 17 2.0631 0.0335

Tests wrt Random Effects

Source SS MS Num DF Num F Ratio Prob > F Phase-AB&Random 0.25934 0.01526 17 0.9670 0.5118

Tests wrt Random Effects

Tests wrt Random Effects

Source SS MS Num DF Num F Ratio Prob > F Phase-AB&Random 2.35091 0.13829 17 1.5111 0.1461

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Source MS Den DF Den Denom MS Synthesis
Phase-AB&Random 0.0007 36 Residual Phase-AB&Random 0.0007

Tests wrt Random Effects Source SS MS Num DF Num F Ratio Prob > F Phase-AB&Random 0.02875 0.00169 17 2.4193 0.0128

Response Measurement Type of Material=ARG-1, Analyte=SiO2 (wt%), Target Value=47.9 Summary of Fit

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

 plus 1.0 times Residual Error Variance **Variance Component Estimates Component Var Comp Est Percent of Total** Phase-AB&Random 0.190775 11.403

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis MS Den DF Den Denom MS Synthesis**
1.48231 36 Residual

Phase-AB&Random 1.48231

Tests wrt Random Effects SS MS Num DF Num F Ratio Prob > F Phase-AB&Random 34.9288 2.05464 17 1.3861 0.2003

Response Measurement Type of Material=ARG-1, Analyte=Sum of

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

Oxides (wt%), Target Value=99.43

Summary of Fit

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Source MS Den DF Den Denom MS Synthesis
Phase-AB&Random 6.16881 36 Residual Phase-AB&Random 6.16881

Tests wrt Random Effects

Source SS MS Num DF Num F Ratio Prob > F Phase-AB&Random 105.162 6.18602 17 1.0028 0.4774

Response Measurement Type of Material=ARG-1, Analyte=TiO2 (wt%), Target Value=1.15 Summary of Fit

Analysis of Variance

Expected Mean Squares

The Mean Square per row by the Variance Component per column

plus 1.0 times Residual Error Variance

 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis**

Source MS Den DF Den Denom MS Synthesis
Phase-AB&Random 0.00084 36 Residual Phase-AB&Random 0.00084

Response Measurement Type of Material=ARG-1, Analyte=ZnO (wt%), Target Value=0.02 Summary of Fit RSquare 0.324582
RSquare Adj 0.005635 RSquare Adj 0.005635
Root Mean Square Error 0.001376 Root Mean Square Error 0.001376
Mean of Response 0.02441 Mean of Response 0.02441
Observations (or Sum Wgts) 54 Observations (or Sum Wgts) 54 **Analysis of Variance Source DF Sum of Squares Mean Square F Ratio** 0.00003274 1.9262e-6 1.0177
0.00006814 1.8927e-6 **Prob** > **F** Error 36 0.00006814 1.8927e-6 **Prob > F** $C. Total 53$ **Expected Mean Squares** The Mean Square per row by the Variance Component per column EMS **Intercept Phase-AB&Random** Intercept 0 0 0
Phase-AB&Random 0 3 Phase-AB&Random 0 3 plus 1.0 times Residual Error Variance **Variance Component Estimates Component** Var Comp Est Percent of Total
Phase-AB&Random 1.115e-8 0.585 Phase-AB&Random 1.115e-8 0.585
Residual 1.893e-6 99.415 Residual 1.893e-6 99.415

Total 1.904e-6 100.000 Total 1.904e-6 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis Source MS Den DF Den Denom MS Synthesis**
Phase-AB&Random 1.89e-6 36 Residual Phase-AB&Random 1.89e-6 **Tests wrt Random Effects Source** SS MS Num DF Num F Ratio Prob > F Phase-AB&Random 3.27e-5 1.93e-6 17 1.0177 0.4635 **Response Measurement Type of Material=ARG-1, Analyte=ZrO2 (wt%), Target Value=0.13 Summary of Fit** RSquare 0.384584
RSquare Adj 0.093971 RSquare Adj 0.093971
Root Mean Square Error 0.004641 Root Mean Square Error 0.004641
Mean of Response 0.131821 Mean of Response 0.131821
Observations (or Sum Wgts) 54 Observations (or Sum Wgts) **Analysis of Variance Source DF Sum of Squares Mean Square F Ratio**
Model 17 0 00048462 0 000029 1 3234 0.00048462
 0.00077549 Error 36 0.00077549 0.000022 **Prob > F**
C Total 53 0.00126011 0.2337 $C. Total 53$ **Expected Mean Squares** The Mean Square per row by the Variance Component per column EMS **Intercept Phase-AB&Random** Intercept 0 0 0
Phase-AB&Random 0 3 Phase-AB&Random plus 1.0 times Residual Error Variance **Variance Component Estimates Var Comp Est Percent of Total**
2.322e-6 9.730 Phase-AB&Random 2.322e-6 9.730
Residual 2.154e-5 90.270 Residual 2.154e-5 90.270
Total 2.386e-5 100.000 Total 2.386e-5 These estimates based on equating Mean Squares to Expected Value. **Test Denominator Synthesis Source MS Den DF Den Denom MS Synthesis** Phase-AB&Random 2.15e-5 36 Residual

Distribution:

