

Radiochronological Age of a Uranium Metal Sample from an Abandoned Facility

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- subsequently reprocessed.
- The radiochronology (*i.e.*, age dating) presented here determines the time since purification of a uraniumbearing material based upon the ingrowth of ²³⁰Th toward its parent ²³⁴U in a non-disturbed environment. The uranium decay series and the position of ²³⁰Th and ²³⁴U in the sequence of decay products is shown in Figure 1. The

82 process of radiochronology typically employs several analytical methods that may include thermal ionization mass 83 spectrometry (TIMS) [1-2], inductively coupled plasma mass spectrometry (ICP-MS) [3-8], gamma spectroscopy [9-84 11], and isotope dilution alpha spectrometry [12-13] to determine the isotopic composition and radiological age of a 85 uranium-bearing material.

86 A small sample of a piece of uranium metal rod buried for approximately fifty years in the dirt floor of an 87 abandoned metal rolling milling was analyzed using multi-collector inductively coupled plasma mass spectroscopy 88 (MC-ICP-MS). The uranium metal was likely a deformed piece or an end of a longer rod that was being rolled into 89 a uniform diameter and length for eventual use in a nuclear reactor. A suitable sample for nuclear forensic analysis 90 was obtained from the interior of the rod to minimize the possibility of exposure to environmental factors that could alter its physical and chemical properties. The ²³⁰Th/²³⁴U atomic ratio measured in this small (0.307 g) sample of 91 92 metal was used to determine the date when the uranium metal was last purified. Samples of the dirt in which the bar 93 was buried were also analyzed and appear to be contaminated with recycled uranium. The forensics analyses of the 94 metal and the dirt lead to different conclusions on the origin of the uranium in these samples.

Experimental

97 *Materials* 98

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All acids were from Seastar Chemical, Inc. (Sidney, BC, Canada). Poly prep chromatography columns and
AG 1x8 resin bed (100-200 mesh) were from Bio-Rad Laboratories, Inc. (Hercules, CA). TEVA resin was from
EiChrom Technologies, LLC (Lisle, IL). The materials used for analysis in this work included a ²³³U tracer solution
calibrated with a natural uranium standard solution prepared from NBL CRM 112-A and a ²²⁹Th tracer solution
calibrated with the NIST SRM 4342A ²³⁰Th radioactivity solution [3].

The TEVA resin was prepared by repeated suspensions in a centrifuge tube containing Milli-Q water, centrifugation, and removal of the foamy later using a transfer pipet. This process removes excess organic extraction reagent and produces a more uniform size distribution of the resin particles. The AG 1x8 (100-200 mesh, chloride form) resin was prepared by repeated suspensions in Milli-Q water, allowing it to settle, and decanting and discarding any floating material. The resin was suspended twice in 6 M HCl, allowed to settle, and the acid was decanted and discarded. Finally, the resin was rinsed five times with Milli-Q water as described above.

110 Sample preparation of soil

112 The uranium isotopic content of three different samples of dirt were analyzed including: (1) the 113 surrounding dirt in which the uranium metal rod was buried (raw soil), (2) the dust gently brushed from the surface 114 of the rod (dust), and (3) vellow and white material scraped from the surface of the rod (scrapings). Samples of raw 115 soil, dust, and scrapings were leached in nitric acid with addition of hydrofluoric acid, traced with ²³³U and ²²⁹Th, 116 and dried. The leachate containing uranium and thorium from each sample was purified and separated using a three-117 column procedure. First, anion-exchange chromatography was used to eliminate trace elements and organics 118 (column A). Second, uranium was separated from the thorium using anion-exchange chromatography (column B). 119 Third, the thorium fraction was purified using a TEVA resin bed (column C). The uranium fractions were re-120 dissolved in 3 mL of 2% HNO₃ for isotopic uranium analysis by MC-ICP-MS. The thorium fractions were re-121 dissolved in a 3 mL solution of 2% HNO₃ + 0.005M HF for isotopic thorium analysis by MC-ICP-MS.

122 Radiochemical separation and purification chromatography of soil samples

123 Column A: Removal of Trace Elements

124 Trace elements and organics were removed from the leachate samples using columns containing 1.8 mL of 125 AG1x8 (100-200 mesh) resin bed. The resin beds were pre-cleaned by rinsing with 10 mL of 0.1M HCl and 4 mL of 126 water and then conditioned with 10 mL of 8M HNO₃. The samples (dissolved in 2 mL of 8M HNO₃) were 127 transferred onto the columns and the sample vials were rinsed once with 2 mL of 8M HNO₃ and added to the 128 columns. Iron was removed by rinsing the columns twice with 2 mL of 8M HNO₃. Uranium and thorium were 129 eluted together into a 15 mL Teflon vial using 2 x 1 mL of 9M HCl, followed by 4 x 2 mL of a solution of 0.1M HCl 130 + 0.005M HF and taken to dryness. Three drops of concentrated HNO₃ followed by two drops of concentrated HCl 131 were added to each fraction and dried.

132 Column B: Uranium and Thorium Separation

Uranium and thorium were separated using columns containing a 1.0 mL of AG1x8 (100-200 mesh) resin bed. The columns were conditioned by rinsing with 8 mL of 0.1M HCl and 6 mL of 9M HCl. A 15 mL telfon vial was placed under each column prior to sample loading to collect the thorium fractions. Samples from column A were dissolved in 0.5 mL of 9M HCl + 10 μ L of concentrated HNO₃ and loaded onto the columns, along with a single 1 mL rinse of 9M HCl from each sample container. The thorium fractions were eluted with 5 mL of 9M HCl and dried. Three drops of concentrated HCl followed by two drops of concentrated HNO₃ was added to the thorium vials and dried. Uranium fractions were eluted into a 15 mL Teflon vial using 7 mL of 0.1M HCl and dried. Two

- drops of concentrated HNO₃ was added twice to the uranium vials and dried.
- 141 Column C: Thorium Purification

142 The final thorium purification step was performed using columns with 0.6 mL of TEVA resin. The 143 columns were conditioned by rinsing with 2 mL of water and 4 mL of 4M HNO₃. Thorium samples from column B 144 were dissolved in 0.5 mL of 4M HNO₃ and loaded onto the columns. Sample vials were rinsed with 0.5 mL and 1.0 145 mL of 4M HNO₃ and added to the columns. Residual uranium and other contaminants were removed by rinsing the 146 columns twice with 2 mL of 4M HNO₃. Thorium was eluted with 1.5 mL of 9M HCl, and 8 mL of a solution of 147 0.1M HCl + 0.005M HF solution into 15 mL Teflon vials. After drying the thorium factions, a series of drop 148 additions were added to each fraction and dried down: 1) two drops of concentrated HCl 2) three drops of 149 concentrated HCl + one drop of concentrated HNO₃ and 3) two drops of concentrated HNO₃.

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Sample preparation of uranium metal

152 Surface oxidation on a small piece of the uranium metal rod taken from the interior was removed by 153 soaking in a small volume of 8M HNO₃ followed by a series of rinses using 8M HNO₃, Milli-Q water, and then 154 acetone. The dry, cleaned metal was weighed (0.30705 grams) and was dissolved in 4 mL of concentrated HNO₃ in 155 a 30 mL Teflon vial on a hotplate until nitrogen dioxide vapors were no longer observed. A small amount of 156 concentrated hydrofluoric acid was added to dissolve any residual precipitates. The sample was then diluted with 10 157 mL of 8M HNO₃ and 12 mL of Milli-Q water. A 250 µL sample of this primary solution (0.25525 grams) was 158 further diluted to approximately 1 liter (1003.3 grams) with 2% HNO₃ and called the first dilution solution. This 159 method follows that given in Williams and Gaffney [3].

For the ²³⁴U fraction measurement, a weighed fraction of the first dilution was spiked with ²³³U tracer, equilibrated by heating covered on the hotplate and then dried. This fraction was re-dissolved in 3 mL of 2% HNO₃ and was analyzed without further purification by MC-ICP-MS. For the ²³⁰Th measurement, a weighed fraction of the primary dilution was spiked with a ²²⁹Th tracer and subjected to four separation and purification steps (given below) using anion-exchange resin and TEVA resin prior to analysis. The separated and purified thorium fraction was redissolved in 3 mL of 2% HNO₃ + 0.005M HF solution and analyzed by MC-ICP-MS.

166 Radiochemical separation and purification chromatography of metal thorium fractions

167 Thorium was purified using standard techniques: initial purification was accomplished using column C 168 (presented above); second, thorium was further purified from uranium using a 1.8 mL AG1x8 resin bed in 9 M HCl, 169 on which uranium adsorbs and thorium passes (similar protocol to column B); third, thorium was absorbed on a 1 170 mL AG1x8 resin bed in 8 M HNO₃ and then eluted with 9 M HCl followed by 0.1 M HCl + 0.005 M HF (similar 171 protocol to column A); and lastly, the thorium was passed through a 1 mL AG1x8 resin bed in 9 M HCl.

172 Instrumentation 173

MC-ICP-MS

174 175 176 The uranium and thorium mass spectrometric analyses were performed using a NuPlasma HR multi-177 collector ICPMS with a combination of Faraday and electron multiplier (pulse-counting) detectors. Samples were 178 introduced to the plasma via a CETAC Aridus II system with a 100 mL/min Teflon nebulizer. Instrumental mass 179 bias and detector cross-calibration factors for both the U and Th analyses were determined using a certified 180 reference material (CRM U010) of 1% enriched uranium obtained from the U.S. Department of Energy New Brunswick Laboratory. The isotope dilution tracers, ²³³U for uranium and ²²⁹Th for thorium, were calibrated with 181 182 gravimetrically prepared standard solutions of U metal (NBL CRM 112-A) and NIST SRM 4342A ²³⁰Th radioactivity solution. Thorium was measured by peak-hopping ²³⁰Th-²²⁹Th on an electron multiplier with 183 184 simultaneous analysis of ²³²Th on Faraday cups. Uranium was measured in static multi-collection mode with ²³⁴U and ²³³U on electron multipliers and ²³⁵U and ²³⁸U on Faradays. Memory effects were corrected by measuring blank 185 186 acid solutions that were used to dissolve the purified samples immediately prior to sample analysis. Data reduction 187 involved correcting for detector baseline, acid blank, detector cross-calibration factor, and instrumental mass bias.

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Results and Discussion

189 The uranium isotopic composition determined for each of the samples analyzed is listed in Table 1 and is 190 similar to that of natural uranium (i.e., $^{238}U = 99.2745 \pm 0.0015\%$; $^{235}U = 0.7200 \pm 0.0012\%$; $^{234}U = 0.0055 \pm 0.0015\%$ 191 0.0005%) [14]. The lack of measureable ²³⁶U in the uranium metal and the scraping samples indicates that these 192 samples had not been subjected to nuclear fuel reprocessing or recycling. The presence of a small quantity of 236 U 193 measured in the dust and raw soil samples may reflect contamination from recycled uranium associated with other 194 work at the facility. Table 2 lists the total uranium mass and activity concentration determined for each sample. 195 The piece of metal is 98.37% natural uranium and reflects a composition expected for uranium metal from this era.

196 The yellow and white material scraped from the metal bar are likely uranium metal oxides that were formed on the 197 surface of the metal bar while it was buried for over fifty years and exposed to ambient environmental conditions.

The ratio of 235 U/ 238 U determined for each sample is shown on Figure 2 where the solid line indicates the ratio for natural uranium (0.0072527) and the dashed lines indicate +/- 0.08% [15]. The low ratio observed for the raw soil may suggest that there is some contamination from depleted uranium, which had also been rolled at the facility. The uranium contamination in the dirt floor is very heterogeneous and probably reflects the different types of metals that were rolled at the facility over time.

The calculated radiological age of each sample is listed on Figure 3 and has been determined from ingrowth of 230 Th from radioactive decay of 234 U with the assumptions that (1) no 230 Th was present at the time the uranium metal was last purified, and (2) no thorium contamination was introduced after uranium purification. The mathematical expression for determining the time (t) since last purification, based upon the atom ratio of 230 Th to 234 U is:

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$$t = \frac{1}{(\lambda_{234} - \lambda_{230})} \times \ln \left[1 + \frac{N_{230}}{N_{234}} \times \frac{(\lambda_{234} - \lambda_{230})}{\lambda_{234}} \right]$$

where λ_{234} , λ_{230} , N_{234U}, and N_{230Th} are the decay constants and number of atoms for ²³⁴U and ²³⁰Th, respectively. The number of atoms of uranium and thorium were determined from the isotope dilution MC-ICP-MS analysis. The half-lives used for ²³⁴U and ²³⁰Th are 245,250 ± 490 years (2 σ) and 75,690 ± 230 years (2 σ), respectively [16].

The relative age of uranium metal and the scraping are approximately the same (Fig. 3). The calculated age of the uranium metal is 61 years, corresponding to a purification date of July of 1950 ± 1.5 years. The calculated age of the scrapings is 60 years, corresponding to August of 1951 ± 3.5 years. The radiological age of the raw soil and dust is significantly less than the metal or scrapings and may be an artifact of the heterogeneity of the uranium contamination in the dirt floor, mobility of thorium and uranium due to environmental transport, or housekeeping practices during plant operation that diluted or removed contamination in the floor.

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Conclusions

Radiochronology methods were used to analyze samples from an abandoned site in order to ascertain the material and isotopic composition and radiological age of suspected uranium-bearing materials. The uranium isotopic compositions measured in each sample is similar to that of natural uranium other than the slight ²³⁶U detected in the dust and raw soil samples. The radiological age calculated for the raw soil and dust is significantly

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less than the samples of metal and scrapings. The difference in radiological age may be attributed to environmental transport or the results of clean-up activities to mitigate contamination while the facility was in operation. The findings from these analyses are evident that methods employed in radiochronology are valuable in ascertaining the provenance of intercepted materials. The age determination of the uranium metal was calculated to be 61 years corresponding to a production date of July of 1950 ± 1.5 years. The uranium metal is better suited for forensic analysis, as it is not as subject to the leaching and other factors which may fractionate thorium and uranium in soil samples.

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Table 1. Uranium isotopic composition in samples

Sample Description	²³⁸ U, atom %	²³⁶ U, atom % ^A	²³⁵ U, atom %	²³⁴ U, atom %
U Metal Scrapings	99.27 ± 0.12	None detected	0.7206 ± 0.0006	$0.00541 \pm 1.7 \cdot 10^{-5}$
U Metal Dust	99.27 ± 0.12	$1.68 \cdot 10^{-6} \pm 5.3 \cdot 10^{-7}$	0.7200 ± 0.0006	$0.00541 \pm 1.7 \cdot 10^{-5}$
Raw Soil	99.28 ± 0.12	$2.33 \cdot 10^{-5} \pm 5.5 \cdot 10^{-7}$	0.7176 ± 0.0006	$0.00538 \pm 1.7 \cdot 10^{-5}$
U Metal	99.27 ± 0.14	None detected	0.7200 ± 0.0013	$0.005412 \pm 1.7 \cdot 10^{-5}$
Natural Uranium ^B	99.27 ± 0.0015	0	0.7200 ± 0.0012	0.005505 ± 0.0005

*U uncertainties are given as the combined standard uncertainty.

^{A 236}U was determined to contribute less than 1E-6 atom percent based on the detection limit.

^B Corresponds to reference 14.

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- 315 316

Table 2. Total uranium concentration in samples

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Sample Description	U, g/g	μCi/g
U Metal Scrapings	0.586 ± 0.011	0.3988 ± 0.0074
U Metal Dust	0.257 ± 0.005	0.1748 ± 0.0036
Raw Soil	0.048 ± 0.001	0.0330 ± 0.0007
U Metal	0.984 ± 0.005	0.6696 ± 0.0035

*All uncertainties are the combined standard uncertainty.



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