# JV TASK 28 – PILOT-SCALE EVALUATION OF THE IMPACT OF SELECTIVE CATALYTIC REDUCTION FOR NO<sub>X</sub> ON MERCURY SPECIATION

**Final Report** 

Prepared for:

AAD Document Control National Energy Technology Laboratory U.S. Department of Energy PO Box 10940, MS 921-143 Pittsburgh, PA 15236-0940

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2000-EERC-12-01

December 2000

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# ACKNOWLEDGMENTS

This report was prepared with the support of the U.S. Department of Energy (DOE) National Energy Technology Laboratory Cooperative Agreement No. DE-FC26-98FT40321. However, any opinions, findings, conclusions, or recommendations expressed herein are those of the authors(s) and do not necessarily reflect the views of DOE.

The Energy & Environmental Research Center's Principal Investigator wishes to acknowledge the following organizations and people for their support, advice, and help in completing the project and this final report.

## **Energy & Environmental Research Center**

| John Pavlish    | Everett Sondreal |
|-----------------|------------------|
| Greg Weber      | Jeffery Thompson |
| Kevin Galbreath | Richard Schulz   |

## U.S. DOE National Energy Technology Laboratory

Scott Renninger and Richard Read

## **U.S. Environmental Protection Agency**

James Kilgroe and Charles Sedman

## EPRI

Paul Chu, whose support has been vital to the completion of this project.

### **Tennessee Valley Authority**

Thomas Burnett and Edward Stephens

### **Kinectrics and Ontario Power Generation**

Rene Mangal and Blair Seckington

### Cormetech, Inc.

Scott Pritchard and Reda Iskandar

### **Wisconsin Electric Power Company**

Dave Michaud

## Cinergy

J. Michael Geers

## Southern Company Services, Inc.

Larry Monroe

## American Electric Power Company

Manojit Sukul

# ABSTRACT

Full-scale tests in Europe and bench-scale tests in the United States have indicated that the catalyst, normally vanadium/titanium metal oxide, used in the selective catalytic reduction (SCR) of  $NO_x$ , may promote the formation of  $Hg^{2+}$  and/or particulate-bound mercury ( $Hg_p$ ). To investigate the impact of SCR on mercury speciation, pilot-scale screening tests were conducted at the Energy & Environmental Research Center. The primary research goal was to determine whether the catalyst or the injection of ammonia in a representative SCR system promotes the conversion of  $Hg^0$  to  $Hg^{2+}$  and/or  $Hg_p$  and, if so, which coal types and parameters (e.g., rank and chemical composition) affect the degree of conversion.

Four different coals, three eastern bituminous coals and a Powder River Basin (PRB) subbituminous coal, were tested. Three tests were conducted for each coal: 1) baseline, 2)  $NH_3$  injection, and 3) SCR of  $NO_x$ . Speciated mercury, ammonia slip, SO<sub>3</sub>, and chloride measurements were made to determine the effect the SCR reactor had on mercury speciation.

It appears that the impact of SCR of  $NO_x$  on mercury speciation is coal-dependent. Although there were several confounding factors such as temperature and ammonia concentrations in the flue gas, two of the eastern bituminous coals showed substantial increases in Hg<sub>p</sub> at the inlet to the ESP after passing through an SCR reactor. The PRB coal showed little if any change due to the presence of the SCR. Apparently, the effects of the SCR reactor are related to the chloride, sulfur and, possibly, the calcium content of the coal. It is clear that additional work needs to be done at the full-scale level. Full-scale tests in Europe<sup>1</sup> and bench-scale tests in the United States<sup>2</sup> have indicated that the catalyst, normally vanadium/titanium metal oxide, used in the selective catalytic reduction (SCR) of NO<sub>x</sub> may promote the formation of oxidized mercury (Hg<sup>2+</sup>) and/or particulate-bound mercury (Hg<sub>p</sub>). To investigate the impact of SCR on mercury speciation, pilot-scale screening tests were conducted at the Energy & Environmental Research Center (EERC). The primary research goal was to determine whether the catalyst in a representative SCR system promotes the conversion of elemental mercury (Hg<sup>0</sup>) to Hg<sup>2+</sup> and/or Hg<sub>p</sub> and, if so, which coal parameters (e.g., chemical composition) affect the degree of conversion.

Three bituminous coals and a Powder River Basin (PRB) subbituminous coal were fired in a 580-MJ/hr (550,000-Btu/hr) pilot-scale combustion system equipped with an ammonia (NH<sub>3</sub>) injection system, SCR reactor, and electrostatic precipitator (ESP). Table ES-1 provides information about the coals. The selection criteria for the four coals investigated were the significant differences in their sulfur (S) and chloride (Cl) contents. Sulfur and Cl in coal are believed to affect mercury speciation and removal by air pollution control devices. Table ES-2 provides the analyses of each of the test coals. Mercury concentrations (as-received basis) of the two bituminous coals (Paradise and Blacksville) and the PRB coal (Cordero Rojo) were very similar at about 0.1 ppm, whereas the third bituminous coal (Band Mill) contained only 0.02 ppm mercury.

Mercury speciation of the combustion flue gases was determined under three different test conditions: 1) baseline, 2) NH<sub>3</sub> injection (bypassing the SCR), and 3) SCR of NO<sub>x</sub>. The test conditions are shown in Table ES-3. The first test provided baseline mercury emission and speciation data for each test coal. For the second test condition, NH<sub>3</sub> was injected into the duct upstream of the SCR bypass loop at a temperature of about 340°C. The third test was conducted under SCR conditions. For the SCR tests, the NH<sub>3</sub> was injected immediately upstream of the SCR reactor at a targeted NH<sub>3</sub>-to-NO<sub>x</sub> stoichiometric ratio of 1. The Ontario Hydro mercury speciation method was used to collect speciated mercury samples. Ammonia, SO<sub>3</sub>, and Cl measurements were conducted at the ESP inlet-sampling location for each test. ESP hopper ashes were collected and analyzed to investigate the effects of NH<sub>3</sub> injection and the SCR catalyst on fly ash composition and Hg<sub>p</sub> formation.

For the Paradise and Blacksville SCR tests, the  $NH_3$  and  $NO_x$  measurements showed that the  $NH_3$ -to- $NO_x$  stoichiometric ratio was maintained at approximately 1, thus maximizing  $NO_x$  conversion while minimizing  $NH_3$  slip ( $\leq 5$  ppmv). However, for the Cordero Rojo and Band

<sup>&</sup>lt;sup>1</sup> Gutberlet, H.; Schlüten, A.; Lienta, A. SCR Impacts on Mercury Emissions on Coal-Fired Boilers. Presented at EPRI SCR Workshop, Memphis, TN, April 2000.

<sup>&</sup>lt;sup>2</sup> Galbreath, K.C.; Zygarlicke, C.J.; Olson, E.S.; Pavlish, J.H.; Toman, D.L. Evaluating Mercury Transformation Mechanisms in a Laboratory-Scale Combustion System. *The Science of the Total Environment* **2000**, 261 (1–3), 149–155.

#### Table ES-1 Coal Information

| Organization                   | State        | Mine                       | Coal                      | Location              | Rank <sup>ª</sup> | Production, t/yr       |
|--------------------------------|--------------|----------------------------|---------------------------|-----------------------|-------------------|------------------------|
| KenAmerican<br>Resources, Inc. | KY           | Paradise                   | Western Kentucky<br>No. 9 | Illinois Basin        | hvBb⁵             | 1,943,910°             |
| Kennecott<br>Energy Co.        | WY           | Cordero Rojo Complex       | Wyodak-Anderson           | Powder<br>River Basin | subC⁴             | 37,011,000°            |
| Arch Coal<br>Sales, Inc.       | VA and<br>KY | Band Mill (Pardee Complex) | Taggart                   | Appalachian<br>Basin  | hvAb⁵             | 1,700,000 <sup>f</sup> |
| Consolidation<br>Coal Co.      | PA           | Blacksville No. 2          | Pittsburgh                | Appalachian<br>Basin  | hvAb              | 3,898,360°             |

<sup>a</sup>Determined according to American Society for Testing and Materials (ASTM) Designation D388-88.

<sup>b</sup>High-volatile B bituminous.

°1998 mine production statistic from Keystone Coal Industry Manual, Intertec Publishing Corporation,

Chicago, Illinois, 2000, 793 p.

<sup>d</sup>Subbituminous C.

<sup>e</sup>High-volatile A bituminous.

<sup>f</sup>1999 mine production statistic from Arch Coal, Inc., http://www.archcoal.com/ab/ab03a.html (accessed 10/1/2000).

| Element | Laboratory           | Paradise      | Cordero Rojo  | Band Mill       | Blacksville     |
|---------|----------------------|---------------|---------------|-----------------|-----------------|
| Hg, ppm | EERC                 | 0.111 ± 0.002 | 0.085 ± 0.012 | 0.022 ± 0.001   | 0.094 ± 0.006   |
| S, %    | EERC                 | 3.10 ± 0.07   | 0.52 ± 0.04   | $0.75 \pm 0.05$ | 2.00 ± 0.04     |
| CI, ppm | EERC                 | 350 ± 44      | <50           | 58 ± 12         | 758             |
| CI, ppm | HawkMtn <sup>a</sup> | 454 ± 19      | 8.7 ± 2.6     | 59 ± 3          | NA <sup>b</sup> |

#### Table ES-2 Coal Hg and Cl Concentrations

<sup>a</sup> Analysis done using oxidative hydrolysis microcoulometry, which is a more sensitive method than that done by the EERC.
 <sup>b</sup> Not analyzed.

#### Table ES-3 **Test Matrix**

| Test | Coal Mine    | Injection*          | SCR Unit     |
|------|--------------|---------------------|--------------|
| 607  | Paradise     | None                | Bypassed     |
| 608  | Paradise     | 25 ppmv $NH_3$      | Bypassed     |
| 609  | Paradise     | ~750 ppmv $NH_{_3}$ | Flow through |
| 610  | Cordero Rojo | None                | Bypassed     |
| 611  | Cordero Rojo | 10 ppmv $NH_3$      | Bypassed     |
| 612  | Cordero Rojo | ~750 ppmv $NH_{3}$  | Flow through |
| 613  | Band Mill    | None                | Bypassed     |
| 614  | Band Mill    | 10 ppmv $NH_{3}$    | Bypassed     |
| 615  | Band Mill    | ~750 ppmv $NH_{3}$  | Flow through |
| 616  | Blacksville  | None                | Bypassed     |
| 617  | Blacksville  | 10 ppmv NH          | Bypassed     |
| 618  | Blacksville  | ~900 ppmv $NH_3$    | Flow through |

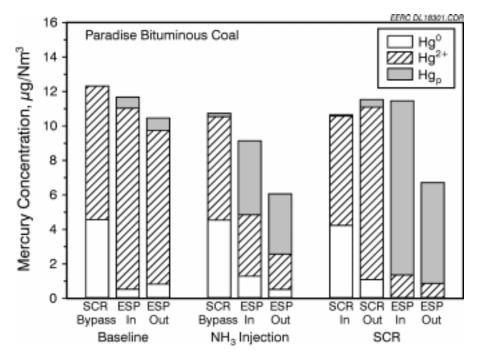
\*The NH<sub>3</sub> injection for Test 608 was 25 ppm instead of 10 ppm. Also, the NH<sub>3</sub>/NO<sub>x</sub> was to be 1.0 for the SCR test, but instead was ~1.2 for Tests 612 and 615.

Mill SCR tests,  $NH_3/NO_x$  was closer to 1.2 because of a calibration error in the  $NH_3$  injection system. As a result of this error,  $NH_3$  slip averaged 143 and 189 ppmv during the Cordero Rojo and Band Mill SCR of  $NO_x$  tests, respectively. For all tests, the SCR reactor reduced  $NO_x$  concentrations by >97%.

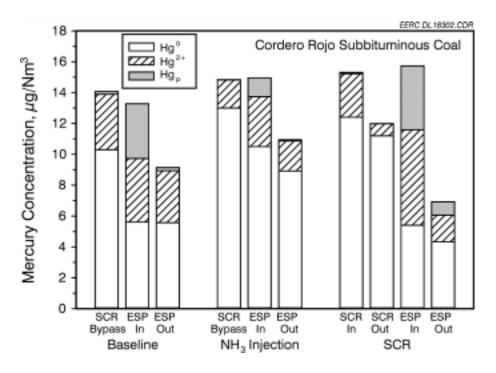
Mercury speciation results for each of the four test coals are summarized in Figures ES-1 through ES-4 and in Table ES-4. Note: In order to make direct comparisons at each sampling location, the mercury results in Table ES-4 are presented as a percentage change in mercury species relative to the baseline condition  $(\Delta Hg^0, \Delta Hg^{2+}, \text{ and } \Delta Hg_p)$ . A negative value shows a decrease in a mercury species with respect to the baseline condition and a positive value indicates an increase. These figures and the table show that NH<sub>3</sub> injection and, possibly, the SCR catalyst promote the conversion of Hg<sup>2+</sup> to Hg<sub>p</sub> in the Paradise and Band Mill coal combustion flue gases, but not in the Cordero Rojo flue gas. Based on the results of these pilot-scale tests, it is more difficult to determine if either the NH<sub>3</sub> injection or SCR conditions impacted mercury speciation when Blacksville coal is fired. For the Paradise coal test, when the SCR reactor was used, there appeared to be conversion of Hg<sup>0</sup> to Hg<sup>2+</sup> between the SCR inlet- and outlet-sampling locations.

Linear regression analyses were completed relating mercury speciation results to the chemical composition of the four test coals. It should be noted that the results of these regression analyses represent data that may not be totally representative of full-scale SCR performance owing to the smaller size and design of the pilot-scale combustor facility, limited number and range of coal types, and the level of ammonia slip.

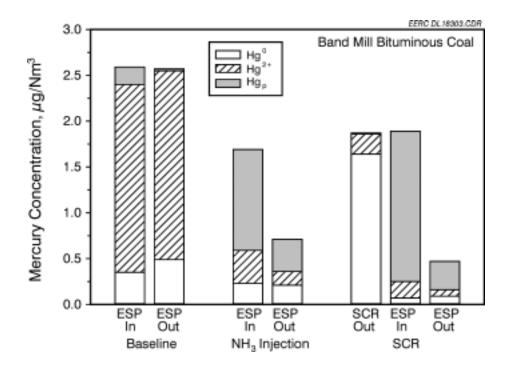
For the regression analysis, the changes in mercury species through the SCR and ESP were correlated with the coal factors (Hg, S, Cl, and Ca concentrations) and operating factors (NH<sub>3</sub> injection and SCR). The most significant variables affecting the total mercury emitted are NH<sub>3</sub> injection, SCR, and Cl in coal. Changes in Hg<sup>0</sup> and Hg<sup>2+</sup> were inversely related, as expected, but both experienced positive and negative changes. Apparently, the SCR resulted in oxidation for coals higher in Hg and Cl, but reduction for coals low in Hg and Cl and higher in Ca. The percentage of coal mercury emitted as Hg<sup>0</sup> at the exit of the ESP is positively correlated with the Ca, negatively with S and Cl, and negatively and secondarily with SCR; the correlation for these four variables combined has an R<sup>2</sup> of 0.84. It would appear that the chemistry of mercury on an SCR catalyst is quite complex.













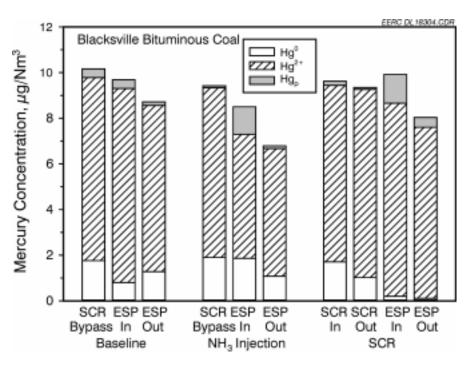


Figure ES-4 Average Mercury Speciation Results for the Blacksville Test Series for Each of the Three Conditions

| Table ES-4   |
|--|
| Percent Change in Mercury Species Proportions Relative to the Baseline Tests |

| Coal:                          | Paradise <sup>a</sup> Cordero Rojo Band Mill |           | Paradise <sup>a</sup> |            |           | Cordero Rojo |            | Band Mill |            |            | Blacksville |            |  |
|--------------------------------|--|-----------|-----------------------|------------|-----------|--------------|------------|-----------|------------|------------|-------------|------------|--|
| Sampling<br>Location:          | SCR<br>Out                                   | ESP<br>In | ESP<br>Out            | SCR<br>Out | ESP<br>In | ESP<br>Out   | SCR<br>Out | ESP<br>In | ESP<br>Out | SCR<br>Out | ESP<br>In   | ESP<br>Out |  |
| NH <sub>3</sub> Injection Only |  |           |                       |            |           |              |            |           |            |            |             |            |  |
| $\Delta Hg^{\circ}$            | NA⁵  | 9.6       | 0.6                   | NA         | 27.9      | 20.6         | NA         | 0.1       | 10.5       | NA         | 13.6        | 1.2        |  |
| $\Delta Hg^{2+}$               | NA   | -51.0     | -51.3                 | NA         | -9.3      | -19.0        | NA         | -57.8     | -59.0      | NA         | -23.9       | -1.3       |  |
| $\Delta Hg_{p}$                | NA   | 41.4      | 50.7                  | NA         | -18.6     | -1.7         | NA         | 57.8      | 48.5       | NA         | 10.3        | 0.1        |  |
| SCR Tests <sup>°</sup>         |  |           |                       |            |           |              |            |           |            |            |             |            |  |
| $\Delta Hg^{\circ}$            | -30.3  | -4.3      | -7.5                  | 12.3       | -7.9      | 1.6          | ND⁴        | -9.8      | 0.1        | -6.9       | -6.2        | -13.3      |  |
| $\Delta Hg^{2+}$               | 27.2   | -78.3     | -72.7                 | -11.9      | 8.3       | -11.7        | ND         | -69.6     | -65.3      | 7.9        | -2.5        | 9.7        |  |
| $\Delta Hg_{p}$                | 3.2  | 82.6      | 80.2                  | -0.5       | -0.4      | 10.1         | ND         | 79.4      | 65.2       | -1.0       | 8.8         | 3.6        |  |

<sup>a</sup> For the Paradise NH<sub>3</sub> injection test, 25 ppm was added, compared to 10 ppm for the remainder of the tests. <sup>b</sup> Not applicable.

<sup>c</sup> For the Cordero Rojo and Band Mill tests, the NH<sub>3</sub>/NO<sub>x</sub> was ~1.2, compared to ~1.0 for Paradise and Blacksville tests. <sup>d</sup> Not determined because of a lack in repeatability among the three SCR bypass/inlet mercury speciation measurements.

Based on the results obtained from this screening evaluation, the following conclusions can be made:

- For some coals, NH<sub>3</sub> appeared to increase the Hg<sub>p</sub> concentration, thereby increasing Hg removal in the downstream ESP. Because NH<sub>3</sub> slips were higher than expected in a full-scale SCR or selective noncatalytic reduction (SNCR) application and NH<sub>3</sub> concentration may directly impact Hg speciation and removal, these results may or may not be consistent with full-scale applications.
- The impact of SCR on mercury speciation and mercury capture appears to be very coaldependent and quite complex.
- Based on a regression analysis, the chlorine, sulfur, and calcium appear to correlate with mercury speciation across the SCR.
- Relatively high concentrations of alkaline-earth metals (i.e., CaO and MgO) in the Cordero Rojo and Blacksville fly ashes may have limited the suspected interactions involving SO<sub>3</sub>, NH<sub>3</sub>, and Cl that promote Hg<sub>p</sub> formation.
- NH<sub>3</sub> injection and/or the SCR catalyst promoted the conversion of Hg<sup>0</sup> to Hg<sup>2+</sup> across the SCR for the Paradise coal, but not for any of the others.
- $NH_3$  injection, with and without the SCR reactions, converted  $Hg^{2+}$  to  $Hg_p$  when the Paradise and Band Mill coals were fired, but not for the Cordero Rojo PRB.
- The increased mercury removals as measured by the flue gas measurements were confirmed with mercury analyses of the corresponding fly ash. The  $Hg_p$  concentrations in Paradise and Band Mill ESP hopper ashes increased by 230%–460% relative to the baseline fly ashes as a result of  $NH_3$  injection and SCR tests.
- Because of the high levels of  $Hg^{2+}$  in the baseline tests, it is not possible to determine whether there was an increase in  $Hg_p$  or oxidation of  $Hg^0$  for the Blacksville coal.

The applicability of the conclusions from this pilot-scale investigation should be evaluated by performing similar flue gas and fly ash measurements at utility-scale boilers equipped with SNCR and SCR units. As part of this proposed utility-scale investigation, flue gas and fly ash samples should be collected when the SNCR and SCR units are off-line and on-line. Size-fractionated fly ash samples should also be collected and analyzed to investigate further the apparent role of particle size and composition on  $Hg_p$  formation. Additional coals also need to be tested because the impact of SNCR and SCR of NO<sub>x</sub> on mercury speciation apparently depends on the coal's chemical composition.

# LIST OF ABBREVIATIONS

| Abbreviation         | Abbreviated Phrase                         |
|----------------------|--|
| ASTM                 | American Society for Testing and Materials |
| CVAAS                | Cold-vapor atomic absorption spectroscopy  |
| EERC                 | Energy & Environmental Research Center     |
| EPA                  | U.S. Environmental Protection Agency       |
| ESP                  | electrostatic precipitator                 |
| Hg⁰                  | elemental mercury                          |
| Hg <sup>2+</sup>     | mercuric compounds                         |
| $Hg_{p}$             | particle-bound mercury                     |
| LOI                  | loss on ignition                           |
| Ν                    | Number of observations                     |
| $\rm NH_x Cl_y SO_z$ | sulfated ammonia and chloride compounds    |
| NO <sub>x</sub>      | nitrogen oxides                            |
| ОН                   | Ontario Hydro mercury speciation method    |
| Ρ                    | Probability                                |
| ppm                  | parts per million                          |
| ppmv                 | parts per million by volume                |
| PTC                  | particulate test combustor                 |
| PTFE                 | polytetrafluoroethylene                    |
| R <sup>2</sup>       | Correlation coefficient                    |
| SCR                  | selective catalytic reduction              |
| SNCR                 | selective noncatalytic reduction           |
| XRF                  | x-ray fluorescence spectrometry            |

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# **1** INTRODUCTION

Coal combustion from electric utilities is a large source of anthropogenic mercury emissions in the United States, according to the U.S. Environmental Protection Agency (EPA) [1], accounting for 52 of the 158 tons/yr of total point-source mercury emissions. More recent data indicate this number may be closer to 45 tons/yr [2]. Clearly, EPA views mercury from coal-fired utilities as a potential public health concern [3]. Many research and development organizations are striving to develop effective and economical mercury emission control technologies for coal-fired utility boilers. The development of mercury control technologies is being spurred by environmental and human health concerns and the resulting potential for mercury emission regulations [1–5].

Mercury emissions from coal-fired boilers can be empirically classified, based on the capabilities of currently available analytical methods, into three main forms: elemental mercury  $(Hg^{0})$ , oxidized mercury  $(Hg^{2+})$ , and particle-bound mercury  $(Hg_{p})$ . Total mercury concentrations in coal combustion flue gas generally range from 3 to 10  $\mu$ g/m<sup>3</sup>; however, Hg<sup>0</sup>, Hg<sup>2+</sup>, and Hg<sub>p</sub> concentrations are much more variable, depending on coal composition and combustion conditions [6].

During combustion,  $Hg^0$  is liberated from coal. However, depending on the coal type, a significant fraction of the  $Hg^0$  can be oxidized to  $Hg^{2+}$  as well as become associated with the fly ash particles in the postcombustion environment of a coal-fired boiler. Relative to  $Hg^0$ ,  $Hg^{2+}$  and  $Hg_p$  are generally more effectively captured in conventional pollution control systems, such as wet scrubbers, fabric filters, and electrostatic precipitators (ESPs) [3, 7–10]. The identification of a process for converting  $Hg^0$  to  $Hg^{2+}$  and/or  $Hg_p$  forms could potentially improve the mercury removal efficiencies of existing pollution control systems.

In addition to mercury, coal-burning power plants are a significant anthropogenic source of nitrogen oxide (NO<sub>x</sub>) emissions to the atmosphere. NO<sub>x</sub> emissions are an environmental concern primarily because they are associated with increased acidification, as well as fine-particle and ozone formation. Depending on the size and type of boiler, the 1990 Clean Air Act Amendments require specific reductions in NO<sub>x</sub> emissions from coal-fired electric utilities. The most common NO<sub>x</sub> reduction strategy is the installation of low-NO<sub>x</sub> burners. These burners have the capability of reducing NO<sub>x</sub> emissions by 40%–60%. However, with possible establishment of PM<sub>2.5</sub>, regional haze, and ozone regulations, there is increased incentive to reduce NO<sub>x</sub> emissions to a level below what can be achieved using low-NO<sub>x</sub> burners. Selective catalytic reduction (SCR) technology, which can reduce NO<sub>x</sub> emissions by >90%, is, therefore, becoming more attractive, particularly because catalyst costs continue to decrease and the knowledge base for using SCR reactors is expanding. Within the next 5 years, 80 to 90 U.S. utilities are planning to install SCR units [11].

## 1.1 Potential Impacts of NO<sub>x</sub> SCR on Mercury Speciation

SCR units achieve lower NO<sub>x</sub> emissions by reducing NO<sub>x</sub> to N<sub>2</sub> and H<sub>2</sub>O. Ammonia (NH<sub>3</sub>) is the most common reductant used for the SCR of NO<sub>x</sub>. The SCR process is generally performed on metal oxide catalysts such as titanium dioxide (TiO<sub>2</sub>)-supported vanadium oxide catalysts (V<sub>2</sub>O<sub>5</sub>). These units are operated at about  $343^{\circ}-371^{\circ}$ C ( $650^{\circ}-700^{\circ}$ F). Laboratory-scale testing indicates that metal oxides, including V<sub>2</sub>O<sub>5</sub> and TiO<sub>2</sub>, promote the conversion of Hg<sup>0</sup> to Hg<sup>2+</sup> and/or Hg<sub>p</sub> in relatively simple flue gas mixtures [12]. In addition, mercury speciation measurements at European coal-fired boilers equipped with SCR reactors have indicated that SCR catalysts promote the formation of Hg<sup>2+</sup> [13, 14]. Therefore, it has been speculated that the installation of an SCR reactor to reduce NO<sub>x</sub> emissions may improve the mercury control efficiency of existing air pollution control devices by promoting Hg<sup>2+</sup> and/or Hg<sub>p</sub> formation. Possible mechanisms that could result in the SCR of NO<sub>x</sub> impacting mercury speciation include:

- Changing the flue gas chemistry. The significant reduction in flue gas NO<sub>x</sub> and slight increase in NH<sub>3</sub> concentrations associated with SCR may affect mercury speciation. It is well known that NO<sub>x</sub>, particularly NO<sub>2</sub>, has a substantial effect on mercury speciation [20]. The gas-phase effects of NH<sub>3</sub> on mercury are unknown. However, tests are being conducted by the University of Cincinnati to help determine possible reactions.
- Catalyzing the formation of  $SO_3$  and, potentially,  $Cl_2$ , which then may react with mercury [15 19].
- Changing the fly ash chemical composition. It is possible that the SCR process may change the surface chemistry of the fly ash particles such that their ability to adsorb or convert mercury species is changed.
- Catalytically oxidizing the mercury. As was reported by the German studies, there is some evidence that vanadium-based catalysts can promote the formation of Hg<sup>2+</sup>[14]. However, the extent to which this can occur and at what temperatures are unknown.
- Increasing wall deposition. SCR systems may result in the deposition of ammonium bisulfate and ammonium sulfate in the air preheater as well as the duct walls. It is unknown whether increased deposition could impact mercury emissions or mercury speciation.

### **1.2 Project Objectives**

The effects of  $NH_3$  injection and the SCR process for  $NO_x$  reduction on mercury speciation were evaluated at the Energy & Environmental Research Center (EERC) using a pilot-scale combustion system equipped with an ESP. The primary research goal was to determine whether  $NH_3$  injection and/or the catalyst in a representative SCR system promote the conversion of  $Hg^0$ to  $Hg^{2+}$  and/or  $Hg_p$  and, if so, the coal types and parameters (e.g., rank and chemical composition) that affect the degree of conversion. Although this project was a screening evaluation and not a complete parametric study, potential mechanisms by which  $Hg^0$  potentially transforms to  $Hg^{2+}$  and/or  $Hg_p$  were investigated.

# **2** EXPERIMENTAL

### 2.1 Coals Tested

Three bituminous coals from the Paradise, Band Mill, and Blacksville No. 2 coal mines and a subbituminous Power River Basin (PRB) coal from the Cordero Rojo mine were selected for this investigation, based on anticipated differences in their sulfur (S) and chloride (Cl) concentrations. Sulfur and Cl concentrations were used as coal selection criteria because it is believed that these parameters affect mercury speciation and removal [2, 18]. Information on the four coals selected for this investigation is presented in Table 2-1.

#### 2.2 Facilities

#### 2.2.1 Pilot-Scale Combustion System

The pilot-scale tests were conducted using the EERC particulate test combustor (PTC), with an ESP as the downstream particulate control device. This combustor has been extensively used by the EERC for a variety of work over the years, including tests to evaluate a catalytic fabric filter for  $NO_x$  reduction, projects to evaluate mercury measurement methods and control technologies, and projects for removing fine particulate matter. The following is a short description of the pilot-scale facilities.

The PTC is a 580-MJ/hr (550,000-Btu/hr) pulverized coal-fired unit designed to generate fly ash and flue gas chemistry representative of that produced in a full-scale utility boiler. Coal is introduced to the primary air stream via a screw feeder and ejector. An electric air preheater is used for precise control of the combustion air temperature. The PTC instrumentation permits system temperatures, pressures, flow rates, flue gas constituent concentrations, and ESP operating data to be monitored continuously and recorded on a data logger.

The PTC (shown in Figure 2-1) is designed to operate in conjunction with an ESP. The ESP, shown in Figure 2-2, is a single-wire, tubular ESP, with a specific collection area of  $125 \text{ ft}^2 / 1000 \text{ acfm} (0.41 \text{ m}^2/\text{m}^3)$  at  $149^{\circ}\text{C} (300^{\circ}\text{F})$  and a plate spacing of 27.9 cm (11 in.). Since the flue gas flow rate for the PTC is 3.67 scmm (130 scfm), the gas velocity through the ESP is 1.5 m/min (5 ft/min). The ESP has an electrically isolated plate that is grounded through an ammeter, allowing continual monitoring of the actual plate current to ensure consistent operation of the ESP from test to test.

#### Table 2-1 **Coal Information**

| Organization                   | State        | Mine                       | Coal                      | Location              | Rank <sup>ª</sup> | Production, t/yr       | Average S, wt% |
|--------------------------------|--------------|----------------------------|---------------------------|-----------------------|-------------------|------------------------|----------------|
| KenAmerican<br>Resources, Inc. | KY           | Paradise                   | Western Kentucky<br>No. 9 | Illinois Basin        | hvBb⁵             | 1,943,910°             | 5.5            |
| Kennecott<br>Energy Co.        | WY           | Cordero Rojo Complex       | Wyodak-Anderson           | Powder<br>River Basin | subC⁴             | 37,011,000°            | 0.32           |
| Arch Coal<br>Sales, Inc.       | VA and<br>KY | Band Mill (Pardee Complex) | Taggart                   | Appalachian<br>Basin  | hvAb <sup>®</sup> | 1,700,000 <sup>f</sup> | 0.77           |
| Consolidation<br>Coal Co.      | PA           | Blacksville No. 2          | Pittsburgh                | Appalachian<br>Basin  | hvAb              | 3,898,360°             | 1.97           |

<sup>a</sup>Determined according to American Society for Testing and Materials (ASTM) Designation D388-88.

<sup>b</sup>High-volatile B bituminous.

°1998 mine production statistic from Keystone Coal Industry Manual, Intertec Publishing Corporation, Chicago, Illinois, 2000, 793 p. <sup>d</sup>Subbituminous C.

<sup>e</sup>High-volatile A bituminous. <sup>f</sup>1999 mine production statistic from Arch Coal, Inc., http://www.archcoal.com/ab/ab03a.html (accessed 10/1/2000).

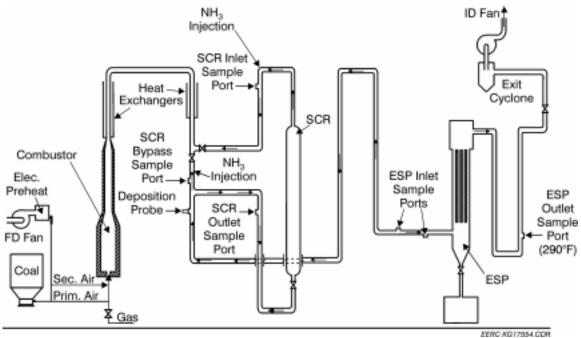


Figure 2-1 Schematic of the EERC Pilot-Scale Combustor

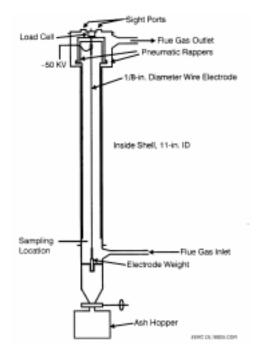


Figure 2-2 Schematic of the EERC ESP

### 2.2.2 SCR Reactor

An SCR reactor, manufactured and supplied by Cormetech, Inc., was installed on the PTC. The SCR reactor is 5.5 m (18 ft) tall and 0.02 m (0.67 ft) in diameter and contains 0.088 m<sup>3</sup> (3.1 ft<sup>3</sup>) of catalyst surface area, providing a space velocity of 2500 hr<sup>-1</sup>. This is approximately the same space velocity of the SCR installed by Cormetech at TVA's Paradise Station. The SCR designed for the PTC was built in three sections. Each section held one module of a honeycomb-type vanadium/titanium catalyst. Enough space was provided between each module so that the modules could be backflushed. Photographs of the SCR and the catalyst are shown in Figures 2-3 and 2-4. At the request of Cormetech, prior to being used for the tests, the SCR catalyst was conditioned for several days with flue gas and sulfur dioxide (SO<sub>2</sub>). The flue gas was generated by firing natural gas in the PTC during which SO<sub>2</sub> was added directly to the combustor to achieve about 1000 ppm in the flue gas.

The SCR reactor was designed to operate at  $343^{\circ}-371^{\circ}$ C ( $650^{\circ}-700^{\circ}$ F) with minimal temperature loss. This was accomplished using electric heaters and insulation. Following the SCR reactor, a cooling loop was added to bring the ESP inlet temperature down to about  $350^{\circ}$ F ( $173^{\circ}$ C).

#### 2.2.3 Ammonium Injection System

The  $NH_3$  used for all the tests was obtained from a tank of anhydrous  $NH_3$ . As shown in Figure 2-1, the  $NH_3$  was injected in the SCR bypass and SCR inlet locations. These locations were selected to ensure that good mixing of the  $NH_3$  with the flue gas occurred prior to its



Figure 2-3 Photograph of the SCR Reactor

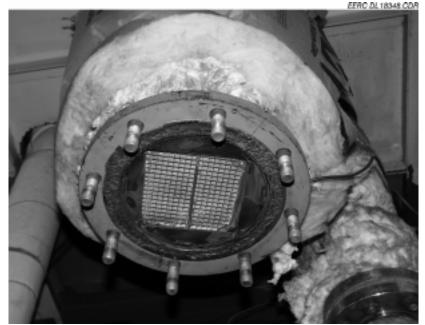


Figure 2-4 Photograph of the SCR Catalyst Following Test

entering the SCR reactor; the NH<sub>3</sub> injection nozzle was designed to aid good mixing. To accurately meter the NH<sub>3</sub> into the combustion system, flowmeters were used. The flowmeters were calibrated prior to the first test firing the Pardise coal; unfortunately, during the tests firing the Cordero Rojo and the Band Mill coals, the calibration of the flowmeter was in error, and about 20% more NH<sub>3</sub> was added than was thought. After another calibration check was conducted, a correction was made prior to testing the Blacksville coal. It is unknown why the flowmeters went out of calibration, as the results from the first test appeared to indicate that they were within specifications. It is possible that the anhydrous NH<sub>3</sub> tank pressure or temperature changed. Gaseous NH<sub>3</sub> and particle-associated NH<sub>3</sub> concentrations were measured at the ESP inlet during every combustion test.

#### 2.3 Test Matrix

As described in Table 2-2, four test series (Tests 607–609, 610–612, 613–615, and 616–618) were conducted firing four different coals in the PTC. The first test condition (Tests 607, 610, 613, and 616) was to provide baseline mercury emission and speciation data. The second test condition (Tests 608, 611, 614, and 617) was to determine if adding a small amount of NH<sub>3</sub> (10 or 25 ppm) to the flue gas impacted mercury speciation. The third condition with each coal (Tests 609, 612, 615, and 618) was the SCR tests. NH<sub>3</sub> was added just upstream of the SCR reactor at a targeted NH<sub>3</sub>-to-NO<sub>x</sub> stoichiometric ratio of 1. Again, this is the stoichiometric ratio used at TVA's Paradise Station. By comparing the baseline results to the results obtained by injecting NH<sub>3</sub> to those obtained during SCR tests, the impact of NH<sub>3</sub> injection and/or SCR catalyst on mercury speciation was determined.

| Test | Coal         | Duration, hr | $\mathbf{NH}_{3}$ Injection, ppmv | SCR Unit     | Test Condition                                 |
|------|--------------|--------------|-----------------------------------|--------------|--|
| 607  | Paradise     | 34.2         | None                              | Bypassed     | Baseline                                       |
| 608  | Paradise     | 30.5         | 25*                               | Bypassed     | $\mathbf{NH}_{\scriptscriptstyle 3}$ injection |
| 609  | Paradise     | 38.1         | ~750                              | Flow through | SCR  |
| 610  | Cordero Rojo | 38.3         | None                              | Bypassed     | Baseline                                       |
| 611  | Cordero Rojo | 27.4         | 10                                | Bypassed     | $\mathbf{NH}_{_3}$ injection                   |
| 612  | Cordero Rojo | 33.9         | ~750                              | Flow through | SCR  |
| 613  | Band Mill    | 37.1         | None                              | Bypassed     | Baseline                                       |
| 614  | Band Mill    | 28.4         | 10                                | Bypassed     | $\mathbf{NH}_{\scriptscriptstyle 3}$ injection |
| 615  | Band Mill    | 37.6         | ~750                              | Flow through | SCR  |
| 616  | Blacksville  | 32.6         | None                              | Bypassed     | Baseline                                       |
| 617  | Blacksville  | 31.7         | 10                                | Bypassed     | $\mathbf{NH}_{\scriptscriptstyle 3}$ injection |
| 618  | Blacksville  | 37.7         | ~900                              | Flow through | SCR  |

# Table 2-2Combustion Test Matrix

\* Reduced to 10 ppm for subsequent tests.

Unless otherwise noted, for the purposes of this report, the following conventions will be used to describe the test conditions:

- Test Condition 1 Baseline
- Test Condition 2 NH<sub>3</sub> injection
- Test Condition 3 SCR

### 2.4 Sampling and Analytical Methods

#### 2.4.1 Coal and Ash Sampling and Analysis

Coal and ESP hopper ash were sampled and analyzed using the methods indicated in Table 2-3. In addition, a deposition probe, maintained at a surface temperature of  $\approx 400^{\circ}$ F (204°C), was inserted downstream of the SCR reactor during each test to simulate an air preheater tube. The deposits that collected on this tube, however, could only be analyzed for a very limited number of analytes because of the small amount of deposition that occurred during each test period (~30 hr).

| Sample<br>Type | Sampling Method(s)   | Analyte(s)  | Analytical Method(s)   |
|----------------|--|---|--|
| Coal           | Grab composite sampling<br>(ASTM D2234)  | Hg  | CVAAS <sup>a</sup> (EPA 245.1 and SW-846<br>Method 7470)                 |
|                |  | Na, Mg, Al, Si, P, S, K, Ca,<br>Sr, Mn, Ti, Ba, and Fe                          | XRF <sup>⊾</sup> (ASTM D4326)  |
|                |  | CI  | ASTM D4208 and oxidative<br>hydrolysis microcoulometry<br>(EPA SWA-846°) |
|                |  | S, C, H, N, O, moisture, ash,<br>heating value,<br>fixed C, and volatile matter | Ultimate (ASTM D3176) and<br>Proximate (ASTM D3172 and<br>D5142)         |
| Fly Ash        | Grab composite sampling<br>(EPA Method S007)   | Hg  | CVAAS (EPA SW-846 Method<br>7470)  |
|                | Cascade 5-stage impactor<br>Sampling filter from the<br>OH mercury speciation<br>sampling method | $NH_{3}(P)$   | Selective ion electrode (Standard<br>Method 4500-B NH <sub>3</sub> )     |
|                |  | Na, Mg, Al, Si, P, S, K, Ca, Ti,<br>Mn, and Fe                                  | XRF (ASTM D4326)   |
|                |  | С   | Leeman Labs Model CE440<br>elemental analyzer                            |
|                |  | ۲OI   | ASTM C114  |
|                |  | CI  | Ion chromatography   |

# Table 2-3Coal and Fly Ash Sampling and Analytical Methods

<sup>a</sup>Cold-vapor atomic absorption spectroscopy.

<sup>b</sup>X-ray fluorescence spectrometry.

<sup>c</sup>Performed by HawkMtn Labs, Inc.

<sup>d</sup>Loss on ignition (LOI).

In addition to collecting and analyzing ESP hopper ash samples, ash samples were also collected at the ESP inlet during Test 609 using a heated 5-stage cascade multicyclone sampler developed by Smith and Wilson [21]. The purpose for doing this sampling procedure was to determine the particle-size distribution of the fly ash and to determine if the mercury is preferentially concentrated on the finer particle fraction. The cascade cyclones were coated with polytetrafluoroethylene (PTFE) to minimize metal contamination. The 50% cutoff diameters ( $d_{50}$ ) for the cyclone stages were 7.2, 4.0, 2.2, 1.5, and 0.6 µm, based on the actual flue gas conditions (temperature, pressure, gas composition, etc.). The filter catch  $d_{50}$  was assumed to be

 $\approx 0.4 \ \mu$ m. Multicyclone measurement results were extrapolated using a cubic spline fit procedure described by McCain et al. [22] to evaluate the particle-size distribution of fly ash.

The third method used to collect fly ash samples was the sample filter used as part of the Ontario Hydro (OH) mercury speciation sampling method. These samples were collected isokinetically according to the method (discussed in the next section). The ash collected on the sample filters was then analyzed as shown in Table 2-3.

### 2.4.2 Flue Gas Sampling and Analysis

As part of each test series (Table 2-2), flue gas samples were collected and analyzed for mercury,  $NH_3$ ,  $SO_3$ , and Cl. The number of samples collected at each location and the average temperature at the sampling location are summarized in Table 2-4. The actual measured temperatures at each sampling location are shown in Appendix A. The temperatures were generally consistent during

 Table 2-4

 Flue Gas Sampling Methods, Frequencies, Locations, and Temperatures at Each Test Condition

| Test Condition                         | Analyte                    | Sampling Method                     | Samples<br>Taken | Sampling<br>Location <sup>®</sup> | Av. Temp.,<br>°F |
|--|----------------------------|-------------------------------------|------------------|-----------------------------------|------------------|
| Baseline and NH <sub>3</sub> Injection | Hg                         | OH method                           | 1                | SCR bypass                        | 615              |
| Baseline and $NH_{3}$ Injection        | Hg                         | OH method                           | 3                | ESP inlet                         | 350              |
| Baseline and $NH_{3}$ Injection        | Hg                         | OH method                           | 3                | ESP outlet                        | 295              |
| Baseline and $NH_{3}$ Injection        | CI                         | EPA Method 26A                      | 2                | ESP inlet                         | 350              |
| Baseline and $NH_{3}$ Injection        | $\mathrm{NH}_{\mathrm{3}}$ | EPA Method 27                       | 2                | ESP inlet                         | 350              |
| Baseline and $NH_{3}$ Injection        | $SO_{_3}$                  | Selective condensation <sup>b</sup> | 2                | ESP inlet                         | 350              |
| SCR                                    | Hg                         | OH method                           | 1                | SCR inlet                         | 650              |
| SCR                                    | Hg                         | OH method                           | 3                | SCR outlet                        | 615              |
| SCR                                    | Hg                         | OH method                           | 3                | ESP inlet                         | 350              |
| SCR                                    | Hg                         | OH method                           | 3                | ESP outlet                        | 295              |
| SCR                                    | CI                         | EPA Method 26A                      | 2                | ESP inlet                         | 350              |
| SCR                                    | $\mathrm{NH}_{\mathrm{3}}$ | EPA Method 27                       | 2                | ESP inlet                         | 350              |
| SCR                                    | $SO_{_3}$                  | Selective condensation <sup>b</sup> | 2                | ESP inlet                         | 350              |

<sup>a</sup>The sampling locations are shown in Figure 2-1.

<sup>b</sup>Described by DeVito and Smith [23].

all the coal combustion tests. In addition to the flue gas samples collected (Table 2-4) the flue gas was also analyzed for  $SO_2$ ,  $NO_x$ , CO,  $CO_2$ , and  $O_2$  concentrations at the furnace outlet.  $SO_2$ ,  $NO_x$ , and  $O_2$  concentrations were also measured at the ESP inlet. These gas concentration measurements were recorded every 5 minutes by a data acquisition system.

#### 2.4.2.1 Ontario Hydro (OH) Method

Mercury speciation analyses for each test were conducted using the OH mercury speciation method. The mercury emission and speciation measurement capabilities of the OH method have been validated through dynamic spike tests and method intercomparisons [24]. Accordingly, this method is being considered by the ASTM Subcommittee D22.03.01 on Sampling and Analysis of Atmospheres as a standard test method for measuring mercury species from coal-fired stationary sources. A detailed description of the OH method is available on an EPA Web site at http://www.epa.gov/ttn/emc under preliminary methods.

It should be noted that the three OH samples were taken as pairs at the ESP inlet and outlet sampling locations. Each of the triplicated pairs was sequential. By comparing the average mercury results, the effect of the SCR reactor and  $NH_3$  injection on mercury speciation was determined and the ESP mercury removal efficiencies calculated.

The samples were analyzed using CVAAS, as stated in the OH method. The mercury mass balances were calculated from the average coal mercury concentrations, coal feed rates, average flue gas flows, total mercury concentrations measured at each sampling location, dust loadings, ESP fly ash collection efficiencies, and ESP hopper ash mercury concentrations. Mercury mass balance closures of 75%–125% are considered acceptable based on experience with the OH method [24, 25]. Sample calculations and mass balance data for mercury are shown in Appendices B and C, respectively.

#### 2.4.2.2 Mercury On-Line Analyzers

During Tests 616–618 (Blacksville coal), two continuous mercury analyzers, a PS Analytical and a Semtech Hg 2010, were used to measure  $Hg^0$  and total mercury concentrations at the ESP outlet sampling location. The PS Analytical instrument is based on atomic fluorescence principles, whereas the Semtech Hg 2000 is a portable Zeeman-modulated CVAAS. These instruments are discussed in detail in a paper recently presented at the Air Quality II Conference [26]. The fly ash-sampling components of an EPA Method 29 sampling train, a glass nozzle and probe, and quartz-fiber filter maintained at the flue gas temperature, were used to obtain particle-free gas samples for analysis. After particle filtration, a proprietary flue gas-conditioning system was used to remove acid gases and reduce any  $Hg^{2+}$  present to  $Hg^0$  for subsequently measuring total mercury.

#### 2.4.2.3 Ammonia Analysis and Measurements

Once the NH<sub>3</sub> samples were collected using EPA Method 27, the solutions were analyzed using a selective ion electrode. NH<sub>3</sub> sample calculations and mass balance data for the Paradise, Cordero

Rojo, Band Mill, and Blacksville combustion flue gases are also presented in Appendices B and C. The flue gas  $NH_3$  measurement results for the baseline tests firing the Paradise and Blacksville coals were greater than corresponding results when  $NH_3$  injected. This suggests that the baseline  $NH_3$  concentrations for these two coals are biased high. The suspected positive bias in the baseline Paradise and Blacksville  $NH_3$  measurements is manifested in low  $NH_3$  mass balance closures for the  $NH_3$  injection tests. The reason for the high  $NH_3$  measurements in the two baseline tests is unknown. It is possible that there was some contamination on the filter or solution or there was something that was interfering with the measurement.

The targeted  $NH_3$ -to- $NO_x$  stoichiometric ratio for all of the SCR tests was 1. As discussed previously, because of a flowmeter calibration error, the ratio for the Cordero Rojo and Band Mill tests was about 1.2. The flowmeter calibration was corrected prior to the Blacksville test. Table 2-5 presents the  $NH_3$ -to- $NO_x$  stoichiometric ratio for each test series.

| Sample  | Paradise    | Cordero Rojo | Band Mill   | Blacksville |
|---------|-------------|--------------|-------------|-------------|
| 1       | 0.89        | 1.31         | 1.37        | 0.97        |
| 2       | 0.97        | 1.15         | 1.22        | 0.96        |
| 3       | 1.10        | 1.13         | 1.16        | 0.98        |
| Average | 0.99 ± 0.11 | 1.20 ± 0.10  | 1.25 ± 0.11 | 0.97 ± 0.01 |

#### Table 2-5 Comparison of Triplicate-Measured NH<sub>3</sub>/NO<sub>x</sub> During the SCR Tests\*

\* These results are based on the average  $NO_x$  concentration measured at the combustor outlet and the  $NH_3$  mass balance ( $NO_x$  reduction plus  $NH_3$  slip).

# **3** RESULTS

## 3.1 Coal Compositions

The proximate–ultimate analysis results for the four test coals are presented in Table 3-1. Composite coal samples were taken directly at the outlet of the pulverized coal feeder. As can be seen, the Paradise and Blacksville bituminous coals have a much higher sulfur concentration than the Cordero Rojo subbituminous and Band Mill bituminous coals. As expected, the moisture content was much higher and the heating value lower for the PRB subbituminous coal compared to the three bituminous coals.

The concentrations of the major and minor elements in the coal ash as measured by XRF are presented in Table 3-2. Again, as expected, the Cordero Rojo PRB subbituminous coal had much higher concentrations of the alkaline elements than the bituminous coals, particularly calcium. The bituminous coals, however, had much higher concentrations of silica and alumina in the coal ash. Comparing the three bituminous coals, there are also clear differences. In addition to high S and Cl concentrations, the Paradise and Blacksville coals had a higher  $Fe_2O_3$  concentration than the Band Mill coal. The Blacksville coal had a higher concentration of CaO and MgO in the coal ash than the other two bituminous coals. As will be discussed in Chapters 3 and 4 of this report, these differences may be important in explaining some of the results observed in this study.

As shown in Table 3-3, there is a difference in the mercury and Cl concentrations among the four coals. The mercury contents of the Paradise, Cordero Rojo, and Blacksville coals are very similar at  $\approx 0.1$  ppm. The Band Mill coal, however, is distinguished by a very low mercury content. Chloride concentration was much higher in the Paradise and Blacksville coals relative to the other two coals. Chloride in the Cordero Rojo coal was not detected by the EERC using ASTM Method D4208; however, HawkMtn Labs, Inc., was able to quantify Cl using oxidative hydrolysis microcoulometry (EPA SWA-846). As anticipated, the S:Cl ratios of the four coals range widely.

### 3.2 Pilot-Scale Coal Combustion Tests

#### 3.2.1 Paradise Bituminous Coal (Illinois Basin)

#### 3.2.1.1 Flue Gas Compositions

Average Paradise coal combustion flue gas compositions are presented in Table 3-4.  $SO_3$  concentrations decreased for the  $NH_3$  injection and SCR tests compared to the baseline. This

| Table 3-1   |
|---|
| Coal Ultimate–Proximate Analysis Results, as-received wt% |

| Analysis Parameters                 | Paradise<br>(Illinois<br>Basin) | Cordero Rojo<br>(PRB) | Band Mill<br>(Appalachian<br>Basin) | Blacksville<br>(Appalachian<br>Basin) |
|-------------------------------------|---------------------------------|-----------------------|-------------------------------------|---------------------------------------|
| Proximate Analysis                  |                                 |                       |                                     |                                       |
| Moisture                            | 5.40 ± 0.27                     | 23.1 ± 2.7            | 1.43 ± 0.10                         | $2.00 \pm 0.00$                       |
| Volatile Matter                     | $39.2 \pm 0.6$                  | 36.7 ± 1.4            | 35.5 ± 0.7                          | $36.6 \pm 0.3$                        |
| Fixed Carbon                        | 45.8 ± 0.8                      | 34.7 ± 1.0            | 55.8 ± 0.5                          | 52.8 ± 0.2                            |
| Ash                                 | 9.56 ± 0.15                     | 5.56 ± 0.23           | 7.22 ± 1.10                         | 8.61 ± 0.15                           |
| Heating Value, Btu/lb               | 12,040 ± 190                    | 8,610 ± 700           | 13,650 ± 550                        | 13,050 ± 110                          |
| Ultimate Analysis                   |                                 |                       |                                     |                                       |
| Carbon                              | 67.0 ± 0.2                      | 50.6 ± 2.1            | 77.8 ± 1.5                          | 72.7 ± 1.1                            |
| Hydrogen <sup>ª</sup>               | $4.64 \pm 0.03$                 | 3.60 ± 0.11           | 4.95 ± 0.06                         | 4.71 ± 0.11                           |
| Nitrogen                            | 2.22 ± 0.05                     | 1.35 ± 0.13           | 2.32 ± 0.05                         | 2.31 ± 0.07                           |
| Sulfur                              | $3.10 \pm 0.07$                 | $0.52 \pm 0.04$       | 0.75 ± 0.05                         | $2.00 \pm 0.04$                       |
| Number of Analyses                  | 4                               | 3                     | 3                                   | 3                                     |
| Ash                                 | 9.56 ± 0.15                     | 5.56 ± 0.23           | 7.22 ± 1.10                         | 8.61 ± 0.15                           |
| Oxygen (by difference) <sup>a</sup> | 8.11 ± 0.31                     | 15.3 ± 0.6            | 5.56 ± 0.95                         | 7.71 ± 1.15                           |
| Total Moisture                      | 5.40 ± 0.27                     | 23.1 ± 2.7            | 1.43 ± 0.10                         | 2.00 ± 0.0                            |
| Number of Analyses                  | 4                               | 3                     | 3                                   | 3                                     |

<sup>a</sup>Hydrogen and oxygen do not include H and O in sample moisture.

observation is believed to result from the formation of bisulfate and/or sulfates because of reaction with  $NH_3$ . Chloride concentrations were very consistent, ranging from 25–29 ppmv.  $NO_x$  concentrations increased because of the gradual temperature increase that occurred in the combustion system with increased operating time as refractory in the combustor reached thermal stability. On average, the SCR reactor reduced the Paradise flue gas  $NO_x$  concentration by 98%. As indicated in Figure 3-1, most of the  $NH_3$  slip is associated with ash particles, although probably in a sulfated form.

| Element                        | Paradise        | Cordero Rojo      | Band Mill         | Blacksville       |
|--------------------------------|-----------------|-------------------|-------------------|-------------------|
| SiO <sub>2</sub>               | 46.2 ± 0.6      | $24.3 \pm 0.5$    | $54.6 \pm 0.6$    | 42.1 ± 0.3        |
| $AI_2O_3$                      | $20.9 \pm 0.4$  | $15.2 \pm 0.8$    | 27.6 ± 3.0        | 22.2 ± 0.8        |
| Fe <sub>2</sub> O <sub>3</sub> | 23.6 ± 0.2      | 6.66 ± 0.71       | 7.12 ± 0.13       | 17.3 ± 0.8        |
| MnO                            | NAª             | $0.036 \pm 0.003$ | $0.054 \pm 0.007$ | $0.029 \pm 0.002$ |
| TiO <sub>2</sub>               | $1.00 \pm 0.00$ | 1.43 ± 0.11       | 1.45 ± 0.06       | $0.92 \pm 0.03$   |
| BaO                            | NA              | $0.46 \pm 0.04$   | $0.08 \pm 0.03$   | 0.073 ± 0.016     |
| $P_2O_5$                       | $0.10 \pm 0.00$ | 0.91 ± 0.05       | 0.17 ± 0.01       | 0.49 ± 0.01       |
| CaO                            | 1.73 ± 0.28     | 23.5 ± 1.6        | $0.82 \pm 0.04$   | 5.53 ± 0.22       |
| MgO                            | $1.50 \pm 0.00$ | $4.46 \pm 0.42$   | 1.67 ± 0.12       | 1.58 ± 0.05       |
| Na <sub>2</sub> O              | $0.40 \pm 0.00$ | $1.26 \pm 0.05$   | 0.61 ± 0.01       | $0.89 \pm 0.03$   |
| K₂O                            | $2.20 \pm 0.00$ | $0.32 \pm 0.04$   | 2.66 ± 0.28       | 1.59 ± 0.03       |
| SO3                            | $2.28 \pm 0.44$ | 23.1 ± 5.0        | 0.67 ± 0.40       | 7.04 ± 0.12       |
| Total                          | 99.8 ± 0.1      | 101.6 ± 0.7       | 97.4 ± 2.3        | 99.8 ± 0.1        |
| No. of Samples                 | 4               | 3                 | 3                 | 3                 |

Table 3-2Coal Ash – Major and Minor Element Oxide Compositions, wt%

# Table 3-3 Coal Hg and Cl Concentrations (as-received ppm) and S–Cl Ratios (as-received basis)

| Element | Laboratory | Paradise       | Cordero Rojo               | Band Mill                  | Blacksville           |
|---------|------------|----------------|----------------------------|----------------------------|-----------------------|
| Hg      | EERC       | 0.111 ± 0.002ª | 0.085 ± 0.012 <sup>₅</sup> | 0.022 ± 0.001 <sup>b</sup> | $0.094 \pm 0.006^{b}$ |
| CI      | EERC       | 350 ± 44ª      | <50                        | 58 ± 12⁵                   | 758°                  |
| CI      | HawkMtn    | 454 ± 19⁵      | 8.7 ± 2.6 <sup>b</sup>     | 59 ± 3⁵                    | NA <sup>d</sup>       |
| S/CI    | EERC       | 77             | 598                        | 128                        | 26                    |

<sup>a</sup>Calculated from four analyses.

<sup>b</sup>Calculated from three analyses.

<sup>c</sup>Average of duplicate analyses.

<sup>d</sup>Not analyzed.

|                                     | Baseline |                        | NH <sub>3</sub> li | $NH_{3}$ Injection |         | CR        |
|-------------------------------------|----------|------------------------|--------------------|--------------------|---------|-----------|
|                                     | Average  | Std. Dev. <sup>a</sup> | Average            | Std. Dev.          | Average | Std. Dev. |
| SO <sub>2</sub> , ppmv <sup>b</sup> | 2480     | 130                    | 2480               | 160                | 2500    | 170       |
| SO <sub>2</sub> , ppmv <sup>c</sup> | 2400     | 130                    | 2370               | 130                | 2400    | 210       |
| SO₃, ppmv⁰                          | 8.2      | NAd                    | 0.7                | NA                 | 0.5     | NA        |
| CO, ppmv⁵                           | 21.0     | 9.5                    | 24.1               | 17.0               | 29.3    | 19.6      |
| CO₂, mol% <sup>▶</sup>              | 14.1     | 0.8                    | 14.1               | 1.0                | 14.5    | 1.2       |
| O <sub>2</sub> , mol% <sup>b</sup>  | 4.27     | 0.79                   | 4.36               | 1.01               | 4.37    | 0.95      |
| O <sub>2</sub> , mol% <sup>c</sup>  | 5.34     | 1.33                   | 5.51               | 1.25               | 4.47    | 1.36      |
| NO <sub>x</sub> , ppmv⁵             | 632      | 82                     | 648                | 95                 | 760     | 120       |
| NO <sub>x</sub> , ppmv <sup>c</sup> | 586      | 76                     | 605                | 89                 | 16.5    | 18.9      |
| NH₃, ppmv°                          | 6.69     | NA                     | 2.50               | 0.17               | 1.14    | NA        |
| Cl, ppmv⁰                           | 26.3     | NA                     | 29.0               | NA                 | 25.2    | NA        |

# Table 3-4 Average Paradise Bituminous Coal (Illinois Basin) Combustion Flue Gas Compositions

<sup>a</sup> Population or sample standard deviation.

<sup>b</sup> Measured at combustor outlet.

 $^{\circ}$  Measured at ESP inlet (gaseous NH<sub>3</sub> only).

<sup>d</sup> Not applicable because only one or two measurements were made.

#### 3.2.1.2 Mercury Speciation

Average mercury speciation results and mass balances for the Paradise coal combustion flue gases produced during the baseline, NH<sub>3</sub> injection, and SCR tests are presented in Tables 3-5–3-7 and shown graphically in Figures 3-2 through 3-4, respectively. Mass balances were acceptable, except during NH<sub>3</sub> injection tests when they were low ( $\leq$ 75%). This appears to be attributable to the very low dust loading collected at the ESP inlet. About 60% of the Hg<sup>0</sup> liberated from Paradise coal during combustion was oxidized at  $\geq$ 340°C ( $\geq$ 650°F) at the SCR bypass and SCR inlet locations. An additional 30% of the Hg<sup>0</sup> oxidized through the cooling loop as the temperature decreased to $\geq$ 175°C ( $\geq$ 350°F) as measured at the ESP inlet. Comparing the mercury species concentrations in Figures 3-2 and 3-3, it appears that the injection of 25 ppmv NH<sub>3</sub> promoted the formation of Hg<sub>p</sub> upstream of the ESP inlet. A concurrent decrease in Hg<sup>2+</sup> and increase in Hg<sub>p</sub> suggests that NH<sub>3</sub> promoted the capture of Hg<sup>2+</sup> by the fly ash. For the SCR test, a comparison of the SCR inlet and outlet mercury species concentrations in Figure 3-4 indicates that the SCR of NO<sub>x</sub> promoted Hg<sup>2+</sup> formation.

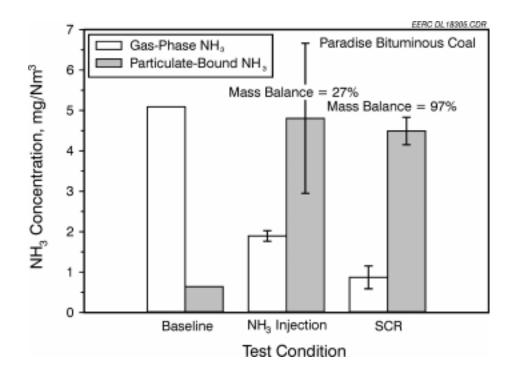


Figure 3-1 Ammonia Concentrations and Mass Balances for the Paradise Tests

| Table 3-5   |
|---|
| Mercury Speciation Results for the Paradise Baseline (Test 607) Test, |
| on a dry, 3% O, basis   |

| Sample<br>Location | Hg⁰, µg/Nm³ | Hg²⁺, µg/Nm³ | Hg <sub>p</sub> , µg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|--------------------|-------------|--------------|--------------------------|---------------------|--------------------|
| SCR Bypass         | 4.57        | 7.74         | 0.01                     | 12.3                | 90                 |
| ESP Inlet          | 0.44        | 11.2         | 0.65                     | 12.3                | 90                 |
| ESP Inlet          | 0.76        | 11.0         | 0.47                     | 12.2                | 89                 |
| ESP Inlet          | 0.38        | 9.34         | 0.82                     | 10.5                | 77                 |
| Average            | 0.53        | 10.5         | 0.65                     | 11.7                | 85                 |
| Std. Dev.          | 0.20        | 1.0          | 0.18                     | 1.0                 | 7                  |
| ESP Outlet         | 0.87        | 8.71         | 0.37                     | 9.95                | 85                 |
| ESP Outlet         | 1.28        | 9.80         | 0.03                     | 11.1                | 94                 |
| ESP Outlet         | 0.35        | 8.23         | 1.77                     | 10.4                | 88                 |
| Average            | 0.83        | 8.91         | 0.72                     | 10.5                | 89                 |
| Std. Dev.          | 0.47        | 0.80         | 0.92                     | 0.6                 | 4                  |

| Sample<br>Location | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub></sub> ,<br>μg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|--------------------|----------------|-----------------|----------------------------|---------------------|--------------------|
| SCR Bypass         | 4.54           | 6.00            | 0.19                       | 10.7                | 75                 |
| ESP Inlet          | 1.40           | 2.75            | 3.69                       | 7.84                | 55                 |
| ESP Inlet          | 0.92           | 4.41            | 3.82                       | 9.15                | 64                 |
| ESP Inlet          | 1.54           | 3.52            | 5.37                       | 10.4                | 73                 |
| Average            | 1.29           | 3.56            | 4.29                       | 9.14                | 64                 |
| Std. Dev.          | 0.33           | 0.83            | 0.93                       | 1.30                | 9                  |
| ESP Outlet         | 0.62           | 1.98            | 2.56                       | 5.16                | 45                 |
| ESP Outlet         | 0.31           | 1.65            | 4.43                       | 6.39                | 54                 |
| ESP Outlet         | 0.63           | 2.51            | 3.47                       | 6.61                | 55                 |
| Average            | 0.52           | 2.05            | 3.49                       | 6.05                | 51                 |
| Std. Dev.          | 0.18           | 0.43            | 0.94                       | 0.78                | 5                  |

## Table 3-6 Mercury Speciation Results for the Paradise NH<sub>3</sub> Injection (Test 608) Test, on a dry, 3% O<sub>2</sub> basis

The SCR of  $NO_x$  also enhanced  $Hg_p$  formation between the SCR outlet and the ESP inlet. The increase in  $Hg_p$  concentration was much more pronounced when the SCR reactor was utilized compared to the  $NH_3$  injection test.

#### 3.2.1.3 Chemical Composition of Fly Ashes and Deposits

In Figure 3-5, the mercury concentrations of the collected fly ash samples are compared. As can be seen in Figure 3-5, the simulated air preheater deposits are depleted in mercury relative to the other fly ash samples. Also, it appears that ash samples collected during the  $NH_3$  injection and SCR tests are more concentrated in mercury relative to corresponding samples collected from the baseline test. Mercury is most concentrated in the ESP outlet ash samples, indicating that mercury is associated primarily with fine ash particles that escape the ESP. As would be expected, the mercury concentration is greatest on the OH filter. The OH filter was a much more efficient collector than the EERC ESP. In addition, it is possible that additional deposition occurs because of the better ash-to-gas contact.

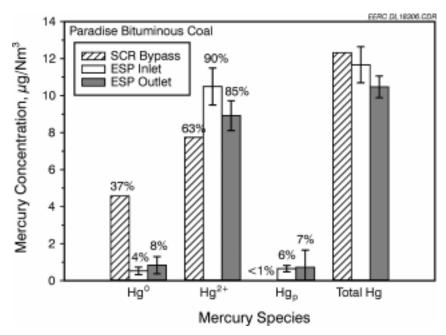
The chemical compositions of ESP hopper ashes generated during the Paradise coal tests are shown in Table 3-8. Fly ashes produced during the  $NH_3$  injection and SCR tests have higher CaO, SO<sub>3</sub>,  $NH_3$ , and Cl concentrations relative to the baseline. These increases, with the exception of CaO, may be a result of  $NH_3$  and SO<sub>3</sub> and  $NH_3$  and Cl reactions. LOI and carbon analysis results for the Paradise ESP hopper ashes are compared in Figure 3-6. LOI concentrations are greater than the corresponding carbon concentrations for a given ash,

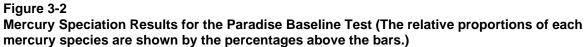
| Table 3-7  |
|--|
| Mercury Speciation Results for Paradise SCR (Test 609) Test, on a dry, 3% O <sub>2</sub> basis |

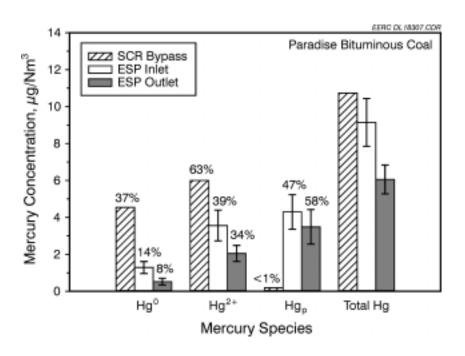
| Sample Location       | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub>p</sub> , μg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|-----------------------|----------------|-----------------|--------------------------|---------------------|--------------------|
| SCR Bypass (Test 607) | 4.57           | 7.74            | 0.01                     | 12.3                | 90                 |
| SCR Bypass (Test 608) | 4.54           | 6.00            | 0.19                     | 10.7                | 75                 |
| SCR Inlet (Test 609)  | 3.58           | 5.29            | 0.01                     | 8.88                | 68                 |
| Average               | 4.23           | 6.34            | 0.07                     | 10.6                | 77                 |
| Std. Dev.             | 0.56           | 1.26            | 0.10                     | 1.7                 | 12                 |
| SCR Outlet            | 0.88           | 8.30            | 1.21                     | 10.4                | 79                 |
| SCR Outlet            | 1.30           | 8.14            | 0.10                     | 9.54                | 73                 |
| SCR Outlet            | 1.08           | 13.6            | 0.01                     | 14.7                | 112                |
| Average               | 1.09           | 10.0            | 0.44                     | 11.5                | 88                 |
| Std. Dev.             | 0.21           | 3.1             | 0.67                     | 2.8                 | 21                 |
| ESP Inlet             | <0.03          | 0.03            | 12.1                     | 12.1                | 92                 |
| ESP Inlet             | 0.06           | 3.95            | 7.19                     | 11.2                | 85                 |
| ESP Inlet             | 0.03           | <0.03           | 11.0                     | 11.0                | 84                 |
| Average               | 0.03           | 1.33            | 10.1                     | 11.4                | 87                 |
| Std. Dev.             | NAª            | NA              | 2.6                      | 0.60                | 5                  |
| ESP Outlet            | <0.03          | <0.03           | 8.30                     | 8.30                | 98                 |
| ESP Outlet            | 0.06           | 2.51            | 5.72                     | 8.29                | 98                 |
| ESP Outlet            | 0.03           | <0.02           | 3.52                     | 3.55                | 62                 |
| Average               | 0.03           | 0.84            | 5.85                     | 6.71                | 86                 |
| Std. Dev.             | NA             | NA              | 2.39                     | 2.74                | 21                 |

<sup>a</sup> Not applicable because less than three analyte concentrations were greater than the lower limit of quantitation.

indicating that additional volatile components (bisulfates/sulfates, carbonates, etc.) were released from ashes during the LOI analysis. It can be seen in Figure 3-6 that the LOI increased for the two conditions with  $NH_3$  injection. Based on the carbon concentration, the LOI for the SCR test is due to an increase in other volatile components and may be attributable to the greater S, N, and Cl contents (Table 3-4). Carbon is more concentrated in fly ashes produced during the  $NH_3$  injection and SCR tests.

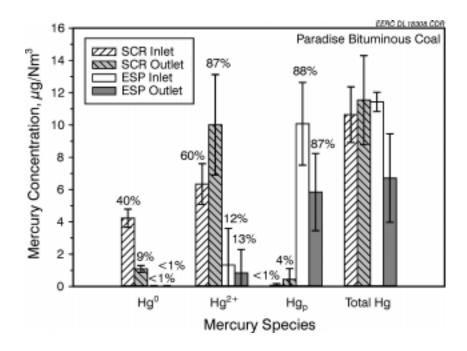








Mercury Speciation Results for the Paradise NH<sub>3</sub> Injection Test (The relative proportions of each mercury species are shown by the percentages above the bars.)





Mercury Speciation Results for the Paradise SCR Test (The relative proportions of each mercury species are shown by the percentages above the bars.)

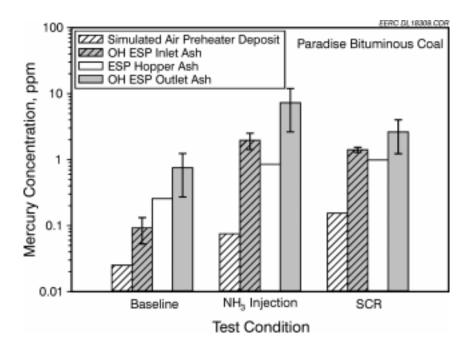
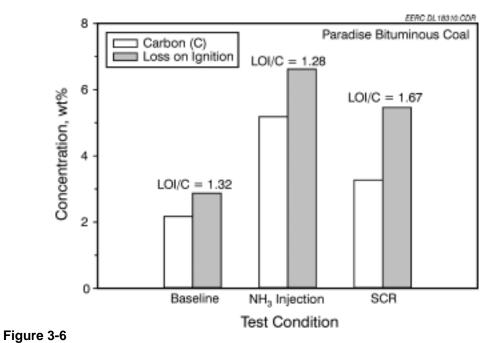


Figure 3-5 Mercury Concentration in the Paradise Ash Samples

| Element, wt%                   | Baseline Test | NH <sub>3</sub> Injection Test | SCR Test |
|--------------------------------|---------------|--------------------------------|----------|
| SiO <sub>2</sub>               | 50.9          | 50.4                           | 50.9     |
| Al <sub>2</sub> O <sub>3</sub> | 21.9          | 21.8                           | 21.8     |
| e <sub>2</sub> O <sub>3</sub>  | 24.5          | 24.8                           | 24.2     |
| ۲iO₂                           | 1.11          | 1.05                           | 1.12     |
| P <sub>2</sub> O <sub>5</sub>  | 0.12          | 0.12                           | 0.11     |
| CaO                            | 1.53          | 1.91                           | 2.20     |
| ИgO                            | 1.36          | 1.35                           | 1.36     |
| BaO                            | 0.049         | 0.054                          | 0.042    |
| Na₂O                           | 0.36          | 0.36                           | 0.37     |
| K <sub>2</sub> O               | 2.45          | 2.41                           | 2.46     |
| SO3                            | 0.80          | 0.95                           | 1.15     |
| NH <sub>3</sub>                | 0.004         | 0.155                          | 0.366    |
| CI, ppm                        | 19            | 25                             | 256      |
| Total, wt%                     | 105.1         | 105.4                          | 106.1    |
|                                |               |                                |          |

| Table 3-8  |
|--|
| Paradise ESP Hopper Ash – Major, Minor, and Trace Element Compositions |



Loss on Ignition and Carbon in the Paradise ESP Hopper Ashes

The chemical compositions of the simulated air preheater deposits produced during each of the tests firing the Paradise coal were compared. As was the case for the ESP hopper ashes, these deposits are much more sulfated for the two conditions when  $NH_3$  is injected relative to the baseline deposit. The deposits were not analyzed for Hg, Cl, or N because not enough sample was available.

#### 3.2.1.4 ESP Fly Ash and Total Mercury Collection Efficiencies

The removal efficiencies of the ESP for particulate matter, total mercury, and  $Hg_p$  for the Paradise coal tests are shown in Table 3-9. Fly ash removal efficiencies were variable and generally low during the tests. The average ESP removal for the three test conditions was only 87%, 70.8%, and 65.3%, respectively. Modifications to the ESP, however, greatly improved fly ash removal efficiencies during subsequent tests with the other three coals. The ESP was relatively ineffective in removing mercury during the baseline combustion test. Total mercury removal efficiencies were significantly greater during the NH<sub>3</sub> injection and SCR tests relative to the baseline condition. The improvement in ESP mercury removal is attributable to the increase in Hg<sub>p</sub> when NH<sub>3</sub> is injected (Figures 3-3 and 3-4). This was the case, even though the ESP efficiency decreased for the three tests.

| Hg, Removal Efficiency of the ESP for the Paradise Coal |          |                           |                    |                   |  |  |  |  |
|---|----------|---------------------------|--------------------|-------------------|--|--|--|--|
| Run No.   | $Hg_{p}$ | % Hg <sub>p</sub> Removal | % Total Hg Removal | % Fly Ash Removal |  |  |  |  |
| 607   | 0.65     | 0.0                       | 10.3               | 87.0              |  |  |  |  |
| 608   | 4.29     | 18.6                      | 33.8               | 70.8              |  |  |  |  |
| 609   | 10.08    | 42.0                      | 58.7               | 63.3              |  |  |  |  |

Table 3-9 Hg, Removal Efficiency of the ESP for the Paradise Coal

#### 3.2.2 Cordero Rojo Subbituminous Coal (PRB)

#### 3.2.2.1 Flue Gas Compositions

Average Cordero Rojo flue gas compositions are presented in Table 3-10. Chloride and SO<sub>3</sub> concentrations in the flue gases were below detection because the Cordero Rojo coal contains such low S and Cl concentrations (Tables 3-2 and 3-3) and high alkali in relation to the S content. The SCR reactor reduced NO<sub>x</sub> concentrations in the Cordero Rojo flue gas by 99%. NH<sub>3</sub> concentrations during the SCR tests were relatively high because of a calibration error in the NH<sub>3</sub> injection system as discussed in Section 2.4.2.3. NH<sub>3</sub> concentrations in the Cordero Rojo baseline, NH<sub>3</sub> injection, and SCR flue gases are compared in Figure 3-7. In contrast to the Paradise tests, gaseous NH<sub>3</sub>:particle-associated NH<sub>3</sub> ratios are much greater than 1, indicating that NH<sub>3</sub>–ash sorption does not occur to any great extent.

|                                    | Baseline Test |                        | NH <sub>3</sub> Inje | NH <sub>3</sub> Injection Test |         | SCR Test  |  |
|------------------------------------|---------------|------------------------|----------------------|--------------------------------|---------|-----------|--|
|                                    | Average       | Std. Dev. <sup>a</sup> | Average              | Std. Dev.                      | Average | Std. Dev. |  |
| SO₂, ppmv <sup>ь</sup>             | 396           | 61                     | 377                  | 26                             | 349     | 39        |  |
| SO₃, ppmv°                         | <0.03         | NAď                    | <0.03                | NA                             | <0.03   | NA        |  |
| CO, ppmv⁵                          | 26.6          | 13.2                   | 21.8                 | 9.2                            | 28.2    | 15.6      |  |
| CO₂, mol% <sup>▶</sup>             | 14.3          | 1.1                    | 14.4                 | 0.9                            | 14.6    | 0.9       |  |
| O <sub>2</sub> , mol% <sup>b</sup> | 4.45          | 0.84                   | 4.56                 | 0.60                           | 4.43    | 0.73      |  |
| O <sub>2</sub> , mol%°             | 4.53          | 0.99                   | 4.48                 | 0.70                           | 4.81    | 0.90      |  |
| NO <sub>x</sub> , ppmv⁵            | 860           | 78                     | 848                  | 61                             | 750     | 55        |  |
| NO <sub>x</sub> , ppmv⁰            | 852           | 67                     | 844                  | 56                             | 6.31    | 2.93      |  |
| NH₃, ppmv⁰                         | 0.82          | NA                     | 13.5                 | 0.6                            | 143     | 64        |  |
| Cl, ppmv⁰                          | <2            | NA                     | <2                   | NA                             | <2      | NA        |  |

 Table 3-10

 Average Cordero Rojo Subbituminous Coal (PRB) Combustion Flue Gas Compositions

<sup>a</sup> Population or sample standard deviation.

<sup>b</sup> Measured at combustor outlet.

<sup>°</sup> Measured at ESP inlet (gaseous NH<sub>3</sub> only).

<sup>d</sup> Not applicable because the analyte concentration was less than the lower limit of quantitation or only one or two measurements were performed.

#### 3.2.2.2 Mercury Speciation

Average mercury speciation and mass balance results for the Cordero Rojo tests are presented in Tables 3-11–3-13 and graphically in Figures 3-8 through 3-10, respectively. Mercury mass balances were acceptable. Mercury speciation measurements at the SCR bypass and inlet locations indicate that about 25% of the Hg<sup>0</sup> released during combustion of the Cordero Rojo coal is oxidized upstream of the SCR at  $\ge 320^{\circ}$ C (610°F). For the Cordero Rojo baseline test (Figure 3-8), about 25% of the Hg<sup>0</sup> becomes associated with the particulate matter between the SCR bypass and ESP inlet sampling locations. Mercury speciation results in Figure 3-9 indicate that the injection of 10 ppmv NH<sub>3</sub> did not promote the formation of Hg<sup>2+</sup> or Hg<sub>p</sub> downstream from the SCR bypass. The mercury speciation results in Figure 3-10 indicate that Hg<sup>0</sup> was not effectively oxidized in the SCR reactor. The relative proportions of Hg<sup>2+</sup> and Hg<sub>p</sub> species downstream from the SCR at the ESP inlet and outlet show an increase in Hg<sup>0</sup> and a decrease in Hg<sup>2+</sup> compared to the baseline Cordero Rojo flue gas, indicating that the SCR was ineffective in enhancing mercury oxidation and Hg<sub>p</sub> formation. This was true, even though the NH<sub>3</sub> slip was very high, >140 ppm.

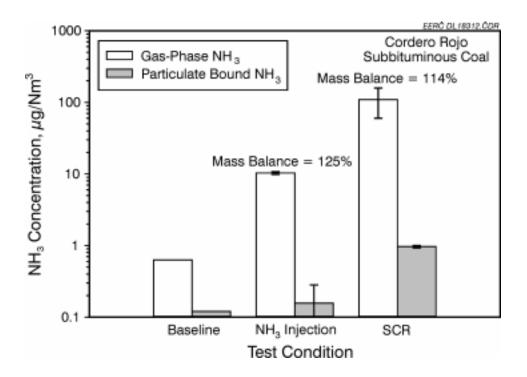


Figure 3-7 Ammonia Concentrations and Mass Balances for the Cordero Rojo Tests

| Table 3-11  |
|---|
| Mercury Speciation Results for the Cordero Rojo Baseline (Test 610) Test, |
| on a dry, 3% $O_2$ basis  |

| Sample<br>Location | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub>ρ</sub> ,<br>μg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|--------------------|----------------|-----------------|-----------------------------|---------------------|--------------------|
| SCR Bypass         | 10.3           | 3.59            | 0.18                        | 14.1                | 96                 |
| ESP Inlet          | 3.84           | 4.23            | 5.84                        | 13.9                | 95                 |
| ESP Inlet          | 6.16           | 2.79            | 3.87                        | 12.8                | 87                 |
| ESP Inlet          | 6.84           | 5.33            | 0.95                        | 13.1                | 90                 |
| Average            | 5.61           | 4.12            | 3.55                        | 13.3                | 91                 |
| Std. Dev.          | 1.57           | 1.27            | 2.46                        | 0.56                | 4                  |
| ESP Outlet         | 4.68           | 2.99            | 0.29                        | 7.96                | 67                 |
| ESP Outlet         | 5.28           | 2.70            | 0.28                        | 8.26                | 69                 |
| ESP Outlet         | 6.75           | 4.39            | 0.07                        | 11.2                | 89                 |
| Average            | 5.57           | 3.36            | 0.21                        | 9.14                | 75                 |
| Std. Dev.          | 1.07           | 0.90            | 0.12                        | 1.80                | 12                 |

| Sample<br>Location | Hg⁰, µg/Nm³ | Hg <sup>2+</sup> , µg/Nm <sup>3</sup> | Hg <sub>p</sub> , µg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|--------------------|-------------|---------------------------------------|--------------------------|---------------------|--------------------|
| SCR Bypass         | 13.0        | 1.82                                  | 0.02                     | 14.8                | 96                 |
| ESP Inlet          | 6.94        | 3.70                                  | 2.69                     | 13.3                | 87                 |
| ESP Inlet          | 11.7        | 3.34                                  | 0.72                     | 15.8                | 102                |
| ESP Inlet          | 12.9        | 2.68                                  | 0.24                     | 15.8                | 102                |
| Average            | 10.5        | 3.24                                  | 1.22                     | 15.0                | 97                 |
| Std. Dev.          | 3.1         | 0.52                                  | 1.30                     | 1.4                 | 9                  |
| ESP Outlet         | 7.33        | 2.07                                  | 0.15                     | 9.55                | 68                 |
| ESP Outlet         | 9.05        | 1.93                                  | 0.03                     | 11.0                | 78                 |
| ESP Outlet         | 10.4        | 1.84                                  | 0.04                     | 12.3                | 86                 |
| Average            | 8.92        | 1.95                                  | 0.07                     | 10.9                | 77                 |
| Std. Dev.          | 1.53        | 0.12                                  | 0.07                     | 1.4                 | 9                  |

Table 3-12 Mercury Speciation Results for the Cordero Rojo  $NH_3$  Injection (Test 611) Test, on a dry, 3%  $O_2$  basis

#### 3.2.2.3 Chemical Compositions of Fly Ashes and Deposits

In Figure 3-11, the Hg<sub>p</sub> concentrations of the ash samples collected during the Cordero Rojo test are compared. The mercury concentration in the simulated air preheater deposits was  $\leq 0.02$  ppm. Only the NH<sub>3</sub> injection test produced enough deposit to be analyzed. As was the case for the Paradise tests, there did not appear to be any deposition of mercury, due to the OH filter, as the ESP hopper ash on Hg<sub>p</sub> concentration was similar to the Hg<sub>p</sub> concentration in ash collected on the ESP inlet OH filter. The Hg<sub>p</sub> is more concentrated in the ESP outlet filters for all test conditions, indicating that mercury is preferentially associated with the finer-particle fraction.

The chemical compositions of Cordero Rojo ESP hopper ashes are compared in Table 3-14. In contrast to the Paradise ESP hopper ashes (Table 3-8), neither  $NH_3$  injection nor the SCR catalyst greatly affected the chemical composition of Cordero Rojo fly ash. The  $NH_3$  concentration in the ash is very low for all tests, even though the  $NH_3$  slip was high. This may be related to the very low SO<sub>3</sub> concentration in the flue gas. Combustion efficiency firing Cordero Rojo coal was very high as indicated by low LOI values of <0.01, 0.05, and 0.09 wt% in Figure 3-12 for each of the three test conditions. The carbon content of the ash was <0.01% in all cases. The chemical compositions of Cordero Rojo simulated air preheater deposits could not be determined because insufficient amounts of ash were deposited.

| Sample Location         | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub>ρ</sub> ,<br>μg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|-------------------------|----------------|-----------------|-----------------------------|---------------------|--------------------|
| SCR Bypass (Test 610)   | 10.3           | 3.59            | 0.18                        | 14.1                | 96                 |
| SCR Bypass (Test 611)   | 13.0           | 1.82            | 0.02                        | 14.8                | 96                 |
| SCR Inlet (Test 612)    | 14.0           | 3.04            | 0.05                        | 17.1                | 128                |
| Average                 | 12.4           | 2.82            | 0.08                        | 15.3                | 107                |
| Std. Dev.               | 1.9            | 0.91            | 0.09                        | 1.6                 | 19                 |
| SCR Outlet              | 11.5           | 0.76            | 0.01                        | 12.2                | 92                 |
| SCR Outlet <sup>a</sup> | 1.79⁵          | 1.43⁵           | 0.01 <sup>b</sup>           | 3.23⁵               | 24                 |
| SCR Outlet              | 10.9           | 0.80            | 0.01                        | 11.7                | 88                 |
| Average                 | 11.2           | 0.78            | 0.01                        | 12.0                | 90                 |
| Std. Dev.               | NA⁵            | NA              | NA                          | NA                  | NA                 |
| ESP Inlet               | 2.32           | 2.69            | 10.4                        | 15.4                | 116                |
| ESP Inlet               | 6.70           | 5.04            | 1.42                        | 13.2                | 99                 |
| ESP Inlet               | 7.22           | 10.8            | 0.56                        | 18.6                | 140                |
| Average                 | 5.41           | 6.18            | 4.14                        | 15.7                | 118                |
| Std. Dev.               | 2.69           | 4.18            | 5.47                        | 2.7                 | 20                 |
| ESP Outlet              | 2.47           | 0.90            | 2.41                        | 5.78                | 54                 |
| ESP Outlet              | 4.75           | 1.65            | 0.15                        | 6.55                | 60                 |
| ESP Outlet              | 5.76           | 2.65            | 0.03                        | 8.44                | 74                 |
| Average                 | 4.33           | 1.73            | 0.86                        | 6.92                | 63                 |
| Std. Dev.               | 1.69           | 0.88            | 1.34                        | 1.37                | 10                 |

Table 3-13

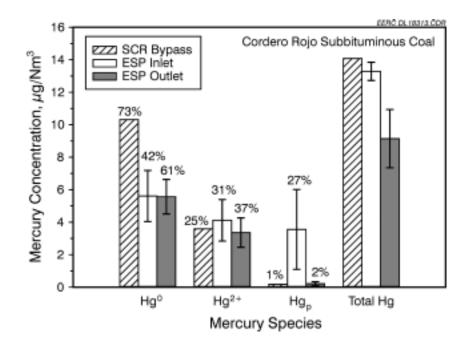
Mercury Speciation Results for Cordero Rojo SCR (Test 612) Test, on a dry, 3% O, basis

<sup>a</sup>Value was not considered in calculating an average or in constructing the bar plot associated with these results.

<sup>b</sup>Not applicable because less than three analyte concentrations were greater than the lower limit of quantitation.

#### 3.2.2.4 ESP Fly Ash and Total Mercury Collection Efficiencies

As shown in Table 3-15, the ESP effectively (>99% removal efficiency) captured the Cordero Rojo fly ash. The ESP mercury removal efficiencies were similar for baseline and NH<sub>3</sub> injection test conditions and just slightly better for the SCR test condition. A comparison of ESP inlet and outlet mercury speciation results in Figures 3-8 through 3-10 also suggests that the ESP was more effective in removing Hg<sup>2+</sup> when the SCR was used. It should be noted that the first sample taken at the ESP inlet location for both NH<sub>3</sub> injection and SCR tests had much higher Hg<sub>p</sub> concentrations than the last two. If these two samples were ignored, there would be a reduction in Hg<sub>p</sub> as a result of NH<sub>3</sub> injection. Table 3-15 presents the Hg<sub>p</sub> removal efficiency for each test as a function of the ESP.





Mercury Speciation Results for the Cordero Rojo Baseline Test (The relative proportions of each mercury species are shown by the percentages above the bars.)

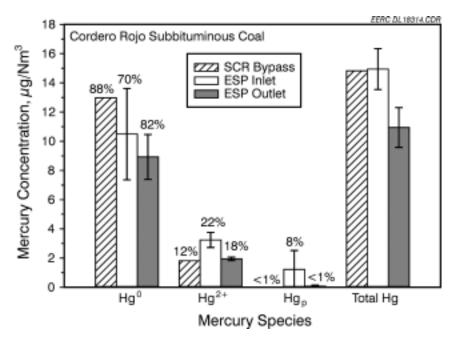
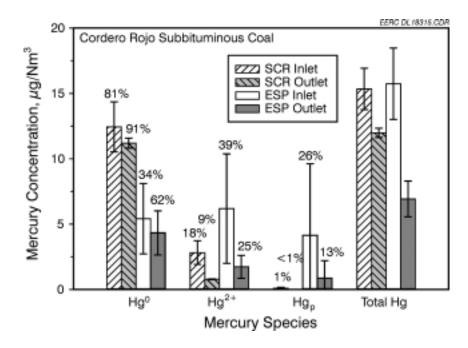


Figure 3-9

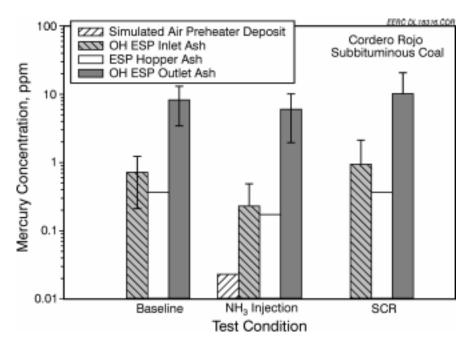
Mercury Speciation Results for the Cordero Rojo NH<sub>3</sub> Injection Test (The relative proportions of each mercury species are shown by the percentages above the bars.)

#### Results





Mercury Speciation Results for the Cordero Rojo SCR Test (The relative proportions of each mercury species are shown by the percentages above the bars.)





Mercury Concentration in Cordero Rojo Ash Samples (The relative proportions of each mercury species are shown by the percentages above the bars.)

| Element, wt%                   | Baseline Test | NH <sub>3</sub> Injection Test | SCR Test |
|--------------------------------|---------------|--------------------------------|----------|
| SiO <sub>2</sub>               | 32.8          | 34.3                           | 32.4     |
| $Al_2O_3$                      | 17.3          | 17.6                           | 18.4     |
| Fe <sub>2</sub> O <sub>3</sub> | 7.66          | 7.40                           | 7.01     |
| MnO                            | 0.044         | 0.042                          | 0.043    |
| TiO <sub>2</sub>               | 1.67          | 1.71                           | 1.65     |
| BaO                            | 0.77          | 0.69                           | 0.80     |
| $P_2O_5$                       | 1.06          | 1.03                           | 1.16     |
| CaO                            | 28.2          | 28.2                           | 28.5     |
| MgO                            | 4.45          | 4.56                           | 4.57     |
| Na₂O                           | 2.41          | 2.38                           | 2.73     |
| K <sub>2</sub> O               | 0.37          | 0.37                           | 0.38     |
| SO3                            | 3.60          | 3.55                           | 3.91     |
| NH <sub>3</sub>                | 0.002         | 0.003                          | 0.016    |
| Cl, ppm                        | <20           | <20                            | <20      |
| Total, wt%                     | 100.3         | 101.8                          | 101.6    |

| Table 3-14   |
|--|
| Cordero Rojo ESP Hopper Ash – Major, Minor, and Trace Element Compositions |

Figure 3-12 Loss on Ignition in the Cordero Rojo ESP Hopper Ashes

| Run No. | $Hg_{p}$ | % Hg <sub>p</sub> Removal | % Total Hg Removal | % Fly Ash Removal |
|---------|----------|---------------------------|--------------------|-------------------|
| 610     | 3.55     | 94.1                      | 21.2               | 99.5              |
| 611     | 1.22     | 94.3                      | 26.8               | 99.7              |
| 612     | 4.14     | 79.2                      | 41.5               | 99.7              |

Table 3-15 Hg<sub>p</sub> Removal Efficiency of the ESP for the Cordero Rojo Coal

#### 3.2.3 Band Mill Bituminous (Appalachian Basin) Coal

#### 3.2.3.1 Flue Gas Compositions

The average Band Mill coal combustion flue gas compositions are presented in Table 3-16. The Band Mill flue gas was characterized by relatively low concentrations of SO<sub>2</sub>, SO<sub>3</sub>, and Cl and low total Hg. SO<sub>2</sub> and Cl concentrations are higher than those obtained firing the Cordero Rojo subbituminous coal but much lower than those obtained burning either the Paradise or Blacksville coal. The SCR reactor reduced NO<sub>x</sub> concentrations in the Band Mill flue gas on average by 99%. As was the case for the Cordero Rojo tests, NH<sub>3</sub> concentrations were greater than expected because the NH<sub>3</sub> injection system was improperly calibrated. NH<sub>3</sub> analysis results for the Band Mill tests are presented in Figure 3-13. NH<sub>3</sub> mass balances were acceptable. The ratio of gas-phase NH<sub>3</sub> to particle-associated NH<sub>3</sub> was about 1 for the NH<sub>3</sub> injection test and more than an order of magnitude higher for the SCR test as a result of excess NH<sub>3</sub> slip. It should be noted that the particle-bound NH<sub>3</sub> concentration did not change.

#### 3.2.3.2 Mercury Speciation

Average mercury speciation and mass balance analysis results for the Band Mill coal tests are provided in Tables 3-17–3-19 and presented graphically in Figures 3-14–3-16. Total mercury concentrations were very low (<3  $\mu$ g/Nm<sup>3</sup>) for these tests; therefore, mercury speciation results were generally more variable compared to those obtained for firing the other three coals. For example, results obtained at the SCR bypass and SCR inlet sampling locations are not used for constructing Figures 3-14–3-16 because of a lack in agreement among the triplicate mercury speciation measurements. These results, however, are shown in Table 3-19. These samples were taken during three different days during the week of testing. Although this was the case for all of the coals tested, the Band Mill appeared to have the greatest variation. Total mercury mass balances were somewhat low ( $\approx 60\%$ ) at the ESP outlet for the NH<sub>3</sub> injection and SCR tests. The baseline Band Mill flue gas (Figure 3-14) consists of about 80% Hg<sup>2+</sup>, 15% Hg<sup>0</sup>, and 5% Hg<sub>p</sub>. Mercury speciation results in Figure 3-15 indicate that the injection of 10 ppmv NH<sub>3</sub> converted Hg<sup>2+</sup> to Hg<sub>p</sub>, thus greatly improving the total mercury removal efficiency of the ESP. For the SCR tests (Figure 3-16), the concentration of Hg<sub>p</sub> is even higher relative to only injecting NH<sub>3</sub>.

| U                                  |         |                        |         |            |          | •         |
|------------------------------------|---------|------------------------|---------|------------|----------|-----------|
|                                    | Basel   | Baseline Test N        |         | ction Test | SCR Test |           |
|                                    | Average | Std. Dev. <sup>a</sup> | Average | Std. Dev.  | Average  | Std. Dev. |
| SO₂, ppmv <sup>ь</sup>             | 451     | 41                     | 429     | 28         | 439      | 33        |
| SO₂, ppmv <sup>c</sup>             | 436     | 43                     | 413     | 26         | 381      | 48        |
| SO₃, ppmv⁰                         | <0.03   | NAd                    | <0.03   | NA         | <0.03    | NA        |
| CO, ppmv⁵                          | 14.8    | 6.4                    | 16.3    | 5.4        | 17.7     | 6.6       |
| CO₂, mol% <sup>▶</sup>             | 13.9    | 1.1                    | 14.2    | 1.0        | 14.2     | 0.8       |
| O <sub>2</sub> , mol% <sup>b</sup> | 4.54    | 1.19                   | 4.51    | 0.86       | 4.49     | 0.65      |
| O₂, mol% <sup>°</sup>              | 5.20    | 1.30                   | 5.15    | 1.08       | 4.99     | 0.91      |
| NO <sub>x</sub> , ppmv⁵            | 694     | 67                     | 725     | 47         | 749      | 43        |
| NO <sub>x</sub> , ppmv⁰            | 689     | 70                     | 722     | 50         | 8.8      | 7.0       |
| NH₃, ppmv⁰                         | 0.43    | NA                     | 4.67    | 0.49       | 189      | 66        |
| CI, ppmv <sup>c</sup>              | 3.7     | NA                     | 2.4     | NA         | 3.4      | NA        |

| Table 3-16  |                              |
|---|------------------------------|
| Average Band Mill Bituminous Coal (Appalachian Basin) Combi | ustion Flue Gas Compositions |

<sup>a</sup> Population or sample standard deviation.

<sup>b</sup> Measured at combustor outlet.

<sup>°</sup> Measured at ESP inlet.

<sup>d</sup> Not applicable because the analyte concentration was less than the lower limit of quantitation or only one or two measurements were performed.

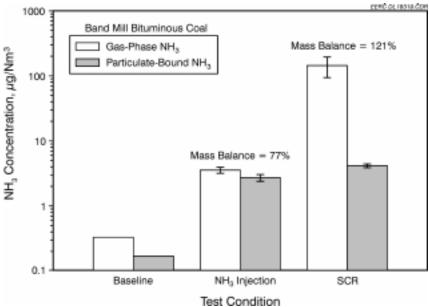


Figure 3-13 Ammonia Concentrations and Mass Balances for the Band Mill Tests

| Table 3-17   |
|--|
| Mercury Speciation Results for the Band Mill Baseline (Test 613) Test, |
| on a dry, 3% O <sub>2</sub> basis                                      |

| Sample<br>Location | Hg⁰,<br>µg/Nm³    | Hg²⁺,<br>µg/Nm³ | Hg <sub>ρ</sub> ,<br>μg/Nm³ | Total Hg,<br>μg/Nm³ | Mass Balance,<br>% |
|--------------------|-------------------|-----------------|-----------------------------|---------------------|--------------------|
| SCR Bypass         | 1.46              | 3.36            | <0.01                       | 4.82                | 192                |
| ESP Inlet          | 0.28              | 2.32            | 0.23                        | 2.83                | 113                |
| ESP Inlet          | 0.36              | 2.11            | 0.22                        | 2.69                | 107                |
| ESP Inlet          | 0.42              | 1.72            | 0.13                        | 2.27                | 91                 |
| Average            | 0.35              | 2.05            | 0.19                        | 2.60                | 104                |
| Std. Dev.          | 0.07              | 0.30            | 0.06                        | 0.29                | 12                 |
| ESP Outlet         | 0.93 <sup>ª</sup> | 5.65°           | 0.02                        | 6.60ª               | 277ª               |
| ESP Outlet         | 0.51              | 2.28            | 0.02                        | 2.81                | 125                |
| ESP Outlet         | 0.47              | 1.84            | 0.02                        | 2.33                | 106                |
| Average            | 0.49              | 2.06            | 0.02                        | 2.57                | 116                |
| Std. Dev.          | NA <sup>b</sup>   | NA              | 0.00                        | NA                  | NA                 |

# Table 3-18 Mercury Speciation Results for the Band Mill $\rm NH_3$ Injection (Test 614) Test, on a dry, 3% $\rm O_2$ basis

| Sample<br>Location | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub>₽</sub> ,<br>µg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|--------------------|----------------|-----------------|-----------------------------|---------------------|--------------------|
| SCR Bypass         | 0.25           | 0.44            | 0.04                        | 0.73                | 30                 |
| ESP Inlet          | 0.32           | 0.31            | 1.49                        | 2.12                | 88                 |
| ESP Inlet          | 0.02ª          | 0.54ª           | 0.57ª                       | 1.13ª               | 47 <sup>ª</sup>    |
| ESP Inlet          | 0.35           | 0.22            | 1.23                        | 1.80                | 75                 |
| Average            | 0.23           | 0.36            | 1.10                        | 1.68                | 81                 |
| Std. Dev.          | 0.18           | 0.17            | 0.47                        | 0.51                | NA                 |
| ESP Outlet         | 0.22           | 0.19            | 0.21                        | 0.62                | 57                 |
| ESP Outlet         | 0.25           | 0.21            | 0.43                        | 0.89                | 68                 |
| ESP Outlet         | 0.15           | 0.05            | 0.42                        | 0.62                | 57                 |
| Average            | 0.21           | 0.15            | 0.35                        | 0.71                | 61                 |
| Std. Dev.          | 0.05           | 0.09            | 0.12                        | 0.26                | 6                  |

<sup>a</sup>Value was not considered in calculating an average or in constructing the bar plot associated with these results.

## Table 3-19 Mercury Speciation Results for the Band Mill SCR (Test 615) Test, on a dry, 3% $O_2$ basis

| Sample Location       | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub>ρ</sub> ,<br>μg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|-----------------------|----------------|-----------------|-----------------------------|---------------------|--------------------|
| SCR Bypass (Test 613) | 1.46           | 3.36            | <0.01                       | 4.82                | 292                |
| SCR Bypass (Test 614) | 0.25           | 0.44            | 0.04                        | 0.73                | 30                 |
| SCR Inlet (Test 615)  | 0.75           | 2.17            | 0.03                        | 2.95                | 124                |
| Average               | 0.82           | 1.99            | 0.03                        | 2.83                | 116                |
| Std. Dev.             | 0.61           | 1.47            | NAª                         | 2.05                | 81                 |
| SCR Outlet            | 1.72           | 0.24            | <0.01                       | 1.96                | 82                 |
| SCR Outlet            | 1.53           | 0.17            | 0.02                        | 1.72                | 72                 |
| SCR Outlet            | 1.67           | 0.25            | <0.01                       | 1.92                | 81                 |
| Average               | 1.64           | 0.22            | 0.01                        | 1.87                | 79                 |
| Std. Dev.             | 0.10           | 0.04            | NA                          | 0.13                | 5                  |
| ESP Inlet             | 0.07           | 0.34            | 1.33                        | 1.74                | 73                 |
| ESP Inlet             | 0.07           | 0.07            | 1.95                        | 2.09                | 88                 |
| ESP Inlet             | 0.08           | 0.14            | 1.65                        | 1.87                | 79                 |
| Average               | 0.07           | 0.18            | 1.64                        | 1.90                | 80                 |
| Std. Dev.             | 0.01           | 0.14            | 0.31                        | 0.18                | 7                  |
| ESP Outlet            | 0.17           | 0.15            | 0.18                        | 0.50                | 60                 |
| ESP Outlet            | 0.06           | 0.02            | 0.35                        | 0.43                | 57                 |
| ESP Outlet            | 0.04           | 0.04            | 0.40                        | 0.48                | 59                 |
| Average               | 0.09           | 0.07            | 0.31                        | 0.47                | 59                 |
| Std. Dev.             | 0.07           | 0.07            | 0.12                        | 0.04                | 2                  |

<sup>a</sup>Not applicable.

<sup>b</sup> Not applicable because <3 analyte concentrations were greater than the lower limit of quantitation.

Mercury speciation results at the SCR outlet in Figure 3-16 suggest that only about 10% of the  $Hg^0$  released firing Band Mill coal is oxidized at temperatures,  $\geq 345^{\circ}C$  ( $\geq 655^{\circ}F$ ). The use of the SCR to reduce  $NO_x$  appeared to promote the formation of  $Hg_p$  between the SCR and the ESP inlet sampling locations compared to the baseline condition. However, the  $NH_3$  slip was much higher (189 ppm) than would be expected in a full-scale system.

Figure 3-14 Mercury Speciation Results for the Band Mill Baseline Test (The relative proportions of each mercury species are shown by the percentages above the bars.)

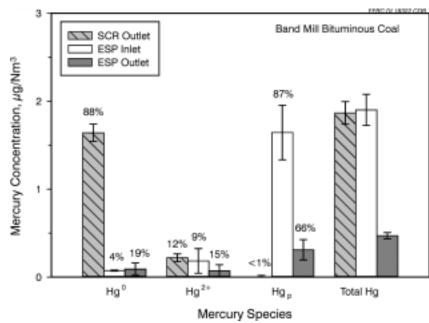


Figure 3-16

Mercury Speciation Results for the Band Mill SCR Test (The relative proportions of each mercury species are shown by the percentages above the bars.)

### 3.2.3.3 Fly Ash Chemical Compositions

The Hg<sub>p</sub> concentrations in Band Mill ash samples are compared in Figure 3-17. Interestingly, for the baseline condition, the mercury concentration in the simulated air preheater deposit is essentially the same as the ESP hopper ash and filter ash samples. However, the deposits collected from the simulated air preheater tube during the NH<sub>3</sub> injection and SCR tests have a very low mercury concentration,  $\leq 0.02$  ppm. The Hg<sub>p</sub> concentration in the ESP hopper ash and filter ash collected during the two test conditions with NH<sub>3</sub> injection was greater than those collected at the baseline condition. Similar to the Paradise and Cordero Rojo fly ashes, mercury is most concentrated in the OH filter ash samples taken at the ESP outlet.

The chemical compositions of Band Mill ESP hopper ash samples are compared in Table 3-20. Fly ashes produced during the  $NH_3$  injection and SCR tests contain greater CaO, SO<sub>3</sub>, and  $NH_3$  concentrations relative to the baseline Band Mill fly ash. Similar enrichments were observed in the Paradise fly ashes. It would be expected that the SO<sub>3</sub> would increase due to SO<sub>2</sub> oxidation by the SCR. Also, an increase in  $NH_3$  concentration in the ash is expected because of the addition of  $NH_3$  to the system. However, the increase in CaO is more than likely not real. The increase is small and may be just the variability in the coal. Also, there does not appear to be a subsequent decrease in the percentage of any other ash component. The total mass balance simply increases. Carbon and LOI analysis results for the Band Mill fly ashes are presented in Figure 3-18. LOI/carbon is much greater for the fly ashes produced for the two tests with  $NH_3$  injection, indicating that these ashes contain greater concentrations of volatile noncarbon components relative to the baseline fly ash.

| Element, wt%                   | <b>Baseline Test</b> | NH <sub>3</sub> Injection Test | SCR Test |
|--------------------------------|----------------------|--------------------------------|----------|
| SiO <sub>2</sub>               | 49.3                 | 47.9                           | 49.0     |
| $Al_2O_3$                      | 24.7                 | 25.8                           | 26.3     |
| Fe <sub>2</sub> O <sub>3</sub> | 6.51                 | 6.94                           | 7.03     |
| MnO                            | 0.056                | 0.058                          | 0.058    |
| TiO <sub>2</sub>               | 1.28                 | 1.43                           | 1.47     |
| BaO                            | 0.12                 | 0.14                           | 0.14     |
| $P_2O_5$                       | 0.14                 | 0.18                           | 0.19     |
| CaO                            | 0.78                 | 0.95                           | 1.24     |
| SrO                            | 0.11                 | 0.14                           | 0.15     |
| MgO                            | 1.68                 | 1.62                           | 1.63     |
| Na₂O                           | 0.53                 | 0.58                           | 0.59     |
| K <sub>2</sub> O               | 2.72                 | 2.49                           | 2.48     |
| SO3                            | 0.37                 | 1.03                           | 1.12     |
| NH₃                            | 0.002                | 0.150                          | 0.380    |
| Cl, ppm                        | <20                  | <20                            | <20      |
| Total, wt%                     | 88.3                 | 89.4                           | 91.8     |

 Table 3-20

 Band Mill ESP Hopper Ash – Major, Minor, and Trace Element Compositions

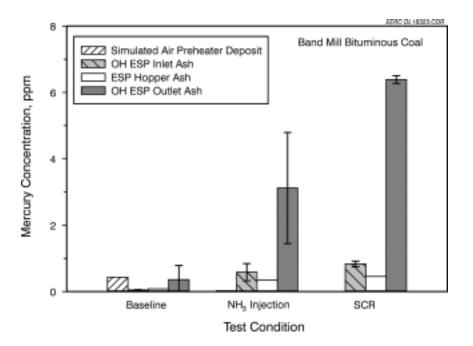


Figure 3-17 Mercury Concentration in the Band Mill Ash Samples

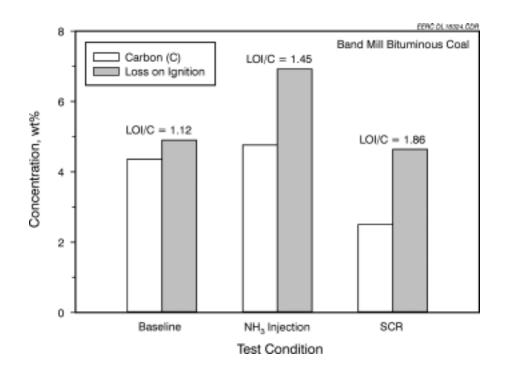


Figure 3-18 Loss on Ignition and Carbon in Band Mill ESP Hopper Ashes

The Band Mill deposits from the simulated air preheater tubes were not chemically analyzed in detail because of a lack of ash deposition on the simulated air preheater tube. Enough sample was obtained, however, for NH<sub>3</sub> analyses. Deposits produced during baseline, NH<sub>3</sub> injection, and SCR conditions contained 0.068, 0.692, and 1.02 wt% NH<sub>3</sub>, respectively. NH<sub>3</sub> was much more concentrated in these deposits relative to the fly ashes, possibly as a result of ammonium bisulfate or sulfate reactions.

#### 3.2.3.4 ESP Fly Ash and Total Mercury Collection Efficiencies

The mercury removal by the ESP is compared to the fly ash removal efficiency in Table 3-21. As can be seen from the table, the fly ash removal efficiencies for the ESP were >92% for the Band Mill coal combustion tests. For the baseline test, the ESP was ineffective at removing mercury. However, the NH<sub>3</sub> injection and SCR tests showed greatly improved mercury removal efficiencies. As was discussed earlier, this was primarily due to an increase in Hg<sub>p</sub> concentrations. ESP mercury removal efficiencies for the NH<sub>3</sub> injection and SCR tests were very similar, suggesting that the presence of NH<sub>3</sub> rather than the SCR catalyst was more of a factor in promoting Hg<sub>p</sub> formation.

| Run<br>No. | Hg <sub>ρ</sub> ,<br>μg/Nm³ | % Hg <sub>p</sub><br>Removal | % Total Hg<br>Removal | % Fly Ash<br>Removal |
|------------|-----------------------------|------------------------------|-----------------------|----------------------|
| 613        | 0.19                        | 89.5                         | 1.2                   | 94.0                 |
| 614        | 1.10                        | 68.2                         | 57.7                  | 92.6                 |
| 615        | 1.64                        | 81.1                         | 76.1                  | 97.6                 |

## Table 3-21 $Hg_{p}$ Removal Efficiency of the ESP for the Band Mill Coal

### 3.2.4 Blacksville Bituminous Coal (Appalachian Basin)

#### 3.2.4.1 Flue Gas Composition

As shown in Table 3-22, the Blacksville coal combustion flue gas contained the highest  $NO_x$  and Cl concentrations of the four coals tested.  $SO_2$  concentrations are also high in comparison to the Cordero Rojo and Band Mill flue gases, but lower than Paradise flue gas. The SCR test resulted in an average  $NO_x$  reduction of 97%. As was the case for the Paradise coal test, there was a

|                                     | Baseline Test |                        | NH <sub>3</sub> Injec | tion Test | SCR Test |           |
|-------------------------------------|---------------|------------------------|-----------------------|-----------|----------|-----------|
|                                     | Average       | Std. Dev. <sup>a</sup> | Average               | Std. Dev. | Average  | Std. Dev. |
| SO₂, ppmv⁵                          | 1458          | 86                     | 1449                  | 74        | 1459     | 67        |
| SO <sub>2</sub> , ppmv <sup>c</sup> | 1392          | 76                     | 1358                  | 74        | 1395     | 50        |
| SO₃, ppmv°                          | 2.4           | NAd                    | <0.3                  | NA        | 1.0      | NA        |
| CO, ppmv⁵                           | 19.7          | 12.2                   | 27.1                  | 10.8      | 20.6     | 9.1       |
| CO₂, mol% <sup>b</sup>              | 14.1          | 1.1                    | 14.3                  | 0.8       | 13.8     | 0.8       |
| O <sub>2</sub> , mol% <sup>b</sup>  | 4.36          | 0.63                   | 4.38                  | 0.68      | 4.46     | 0.56      |
| O <sub>2</sub> , mol% <sup>°</sup>  | 5.31          | 0.60                   | 5.55                  | 0.85      | 4.81     | 0.83      |
| NO <sub>∗</sub> , ppmv⁵             | 861           | 82                     | 913                   | 97        | 924      | 40        |
| NO <sub>x</sub> , ppmv°             | 764           | 76                     | 819                   | 96        | 29       | 19        |
| NH₃, ppmv°                          | 2.18          | NA                     | 0.64                  | 0.18      | 0.40     | 0.18      |
| Cl, pmv°                            | 38.6          | NA                     | 25.9                  | NA        | 38.2     | NA        |

## Table 3-22 Average Blacksville Bituminous Coal (Appalachian Basin) Combustion Flue Gas Compositions

<sup>a</sup> Population or sample standard deviation.

<sup>b</sup> Measured at combustor outlet.

<sup>°</sup> Measured at ESP inlet (gaseous NH<sub>3</sub> only).

<sup>d</sup> Not applicable because the analyte concentration was less than the lower limit of quantitation or only one or two measurements were performed.

measurable amount of  $NH_3$  in the baseline flue gas; in fact, the baseline  $NH_3$  concentration was higher than the  $NH_3$  slip measured in the tests when  $NH_3$  was added to the system. This results in poor mass balances for the  $NH_3$  injection tests. As was suggested previously, it is possible that the baseline  $NH_3$  concentration is biased high. Average  $NH_3$  measurement results for the Blacksville flue gases are shown in Figure 3-19. It is clear that most of the unreacted  $NH_3$  in Blacksville flue gas was adsorbed on ash particles, most likely as bisulfates or sulfates.

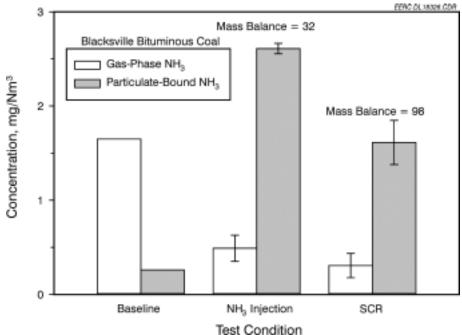


Figure 3-19 Ammonia Concentrations and Mass Balances for the Blacksville Tests

#### 3.2.4.2 Mercury Speciation

Mercury speciation results for the Blacksville coal tests are compared in Tables 3-23–3-25 and shown graphically in Figures 3-20–3-22. Average mass balances for the Blacksville flue gases are acceptable. As shown in Figure 3-20, mercury speciation of the baseline tests was characterized by very high  $Hg^{2+}$  concentrations, accounting for  $\ge 85\%$  of the total mercury. Measurements at the SCR bypass location indicate that most of the conversion of  $Hg^0$  to  $Hg^{2+}$  occurs at  $\ge 335^{\circ}C$  ( $\ge 635^{\circ}F$ ). The ESP was relatively ineffective in removing  $Hg^{2+}$  from the baseline Blacksville flue gas. Mercury speciation results in Figure 3-21 suggest that the injection of 10 ppmv NH<sub>3</sub> into Blacksville flue gas promoted the conversion of  $Hg^{2+}$  to  $Hg_p$  to a small extent. Mercury speciation at the ESP outlet, however, did not change significantly as a result of NH<sub>3</sub> injection. A comparison of Figures 3-20 and 3-22 suggests that passing the flue gas through the SCR reactor did little to increase the Hg<sub>p</sub> concentration.

| Sample<br>Location | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub>₽</sub> ,<br>µg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|--------------------|----------------|-----------------|-----------------------------|---------------------|--------------------|
| SCR Bypass         | 1.76           | 8.02            | 0.38                        | 10.2                | 94                 |
| ESP Inlet          | 1.31           | 8.55            | 0.21                        | 10.1                | 93                 |
| ESP Inlet          | 0.50           | 8.78            | 0.28                        | 9.56                | 88                 |
| ESP Inlet          | 0.60           | 8.16            | 0.66                        | 9.42                | 87                 |
| Average            | 0.80           | 8.50            | 0.38                        | 9.68                | 90                 |
| Std. Dev.          | 0.44           | 0.31            | 0.24                        | 0.34                | 3                  |
| ESP Outlet         | 1.75           | 7.44            | 0.22                        | 9.41                | 96                 |
| ESP Outlet         | 1.18           | 7.43            | 0.03                        | 8.64                | 89                 |
| ESP Outlet         | 0.91           | 6.97            | 0.20                        | 8.08                | 84                 |
| Average            | 1.28           | 7.28            | 0.15                        | 8.71                | 90                 |
| Std. Dev.          | 0.43           | 0.27            | 0.10                        | 0.67                | 6                  |

# Table 3-23 Mercury Speciation Results for the Blacksville Baseline (Test 616) Test, on a dry, 3% $O_2$ basis

For the Blacksville tests, two continuous mercury analyzers were used at the outlet of the ESP and compared to the OH method. The results are shown in Figures 3-23–3-25. Total mercury concentrations measured with the PS Analytical instrument compared very well to the corresponding OH measurements. Conversely, those measured with the Semtech analyzer were generally biased low relative to the OH total mercury measurements. The  $Hg^0$  measurements with the PS Analytical instrument were lower than those measured using the OH method and also measured by the Semtech. In general, the mercury analyzers gave results that were similar to those obtained with the OH method.

#### 3.2.4.3 Fly Ash Chemical Compositions

The  $Hg_p$  concentrations in Blacksville fly ash samples are compared in Figure 3-26. Blacksville simulated air preheater deposits are lower in  $Hg_p$  relative to fly ashes sampled from the ESP hopper and OH filter samples at the ESP inlet and outlet.  $Hg_p$  concentrations in the ESP hopper ashes and on the ash collected on the OH filter at the ESP inlet location are very similar. This indicates that the OH filter was not collecting additional mercury relative to the ESP. However, the  $Hg_p$  concentration is higher in the ash on the OH filter used at the ESP outlet.  $Hg_p$  is slightly more concentrated in fly ashes produced during the  $NH_3$  injection and SCR tests relative to the baseline test, based on the ESP inlet filter and hopper ash data.

| Sample<br>Location | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub>p</sub> ,<br>μg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|--------------------|----------------|-----------------|-----------------------------|---------------------|--------------------|
| SCR Bypass         | 3.42           | 4.69            | 0.90                        | 9.01                | 86                 |
| SCR Bypass         | 1.90           | 7.43            | 0.09                        | 9.42                | 90                 |
| ESP Inlet          | 2.54           | 5.48            | 0.89                        | 8.91                | 85                 |
| ESP Inlet          | 1.69           | 4.55            | 2.00                        | 8.24                | 79                 |
| ESP Inlet          | 1.34           | 6.25            | 0.74                        | 8.33                | 80                 |
| Average            | 1.86           | 5.43            | 1.21                        | 8.49                | 81                 |
| Std. Dev.          | 0.62           | 0.85            | 0.69                        | 0.36                | 3                  |
| ESP Outlet         | 1.38           | 5.69            | 0.07                        | 7.14                | 79                 |
| ESP Outlet         | 0.83           | 5.00            | 0.25                        | 6.08                | 69                 |
| ESP Outlet         | 1.03           | 6.09            | 0.03                        | 7.15                | 79                 |
| Average            | 1.08           | 5.59            | 0.12                        | 6.79                | 76                 |
| Std. Dev.          | 0.28           | 0.55            | 0.12                        | 0.61                | 6                  |

Table 3-24 Mercury Speciation Results for the Blacksville  $NH_3$  Injection (Test 617) Test, on a dry, 3%  $O_2$  basis

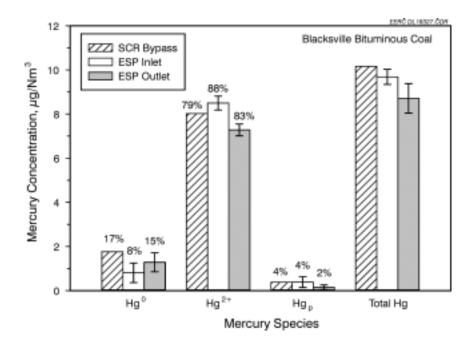
The chemical compositions of Blacksville fly ashes sampled from the ESP hopper during each of the three different test conditions are presented in Table 3-26. Relative to the baseline condition,  $SO_3$  is slightly more concentrated in the fly ashes produced for the two test conditions with  $NH_3$  injection.  $NH_3$  and Cl concentrations in the fly ash produced during the SCR test are greater than those produced in either the baseline or  $NH_3$  injection test. The chemical compositions of Blacksville ash deposits could not be determined because insufficient amounts of ash were deposited on the simulated air preheater tubes.

LOI and carbon analysis results for the Blacksville ESP hopper ash samples are compared in Figure 3-27. Fly ashes produced during  $NH_3$  injection and SCR conditions had a greater LOI/carbon partly because of their greater SO<sub>3</sub> and  $NH_3$  concentrations (Table 3-22).

### Table 3-25 Mercury Speciation Results for Blacksville SCR (Test 618) Test, on a dry, 3% $O_2$ basis

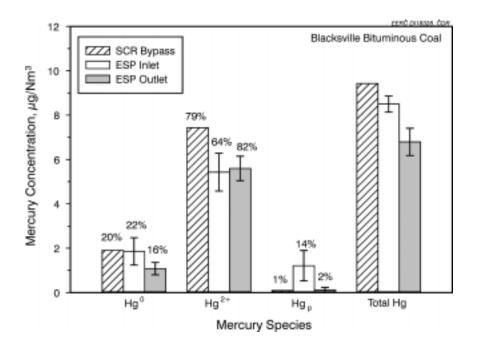
| Sample Location       | Hg⁰,<br>µg/Nm³ | Hg²⁺,<br>µg/Nm³ | Hg <sub>ρ</sub> ,<br>μg/Nm³ | Total Hg,<br>μg/Nm³ | Mass<br>Balance, % |
|-----------------------|----------------|-----------------|-----------------------------|---------------------|--------------------|
| SCR Bypass (Test 616) | 1.76           | 8.02            | 0.38                        | 10.2                | 94                 |
| SCR Bypass (Test 617) | 3.42ª          | 4.69ª           | 0.90ª                       | 9.01ª               | 86ª                |
| SCR Bypass (Test 617) | 1.90           | 7.43            | 0.09                        | 9.42                | 90                 |
| SCR Inlet (Test 618)  | 1.84           | 7.61            | 0.24                        | 9.69                | 89                 |
| SCR Inlet (Test 618)  | 1.33           | 7.86            | 0.02                        | 9.21                | 84                 |
| Average               | 1.71           | 7.73            | 0.18                        | 9.62                | 89                 |
| Std. Dev.             | 0.22           | 0.23            | 0.14                        | 0.36                | 4                  |
| SCR Outlet            | 1.12           | 8.12            | 0.02                        | 9.26                | 85                 |
| SCR Outlet            | 0.91           | 8.42            | 0.06                        | 9.39                | 86                 |
| SCR Outlet            | 1.03           | 8.19            | 0.17                        | 9.39                | 86                 |
| Average               | 1.02           | 8.24            | 0.08                        | 9.35                | 86                 |
| Std. Dev.             | 0.11           | 0.16            | 0.08                        | 0.08                | 1                  |
| ESP Inlet             | 0.17           | 8.18            | 1.01                        | 9.36                | 86                 |
| ESP Inlet             | 0.24           | 8.63            | 2.11                        | 11.0                | 101                |
| ESP Inlet             | 0.19           | 8.56            | 0.67                        | 9.42                | 91                 |
| Average               | 0.20           | 8.46            | 1.26                        | 9.92                | 92                 |
| Std. Dev.             | 0.04           | 0.24            | 0.75                        | 0.92                | 8                  |
| ESP Outlet            | 0.09           | 7.12            | 0.35                        | 7.56                | 80                 |
| ESP Outlet            | 0.24           | 6.96            | 0.55                        | 7.75                | 81                 |
| ESP Outlet            | <0.01          | 8.39            | 0.39                        | 10.2                | 84                 |
| Average               | 0.11           | 7.49            | 0.43                        | 8.51                | 82                 |
| Std. Dev.             | 0.12           | 0.78            | 0.11                        | 1.49                | 2                  |

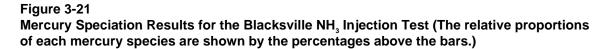
<sup>a</sup>Value was not considered in calculating an average or in constructing the bar plot associated with these results.



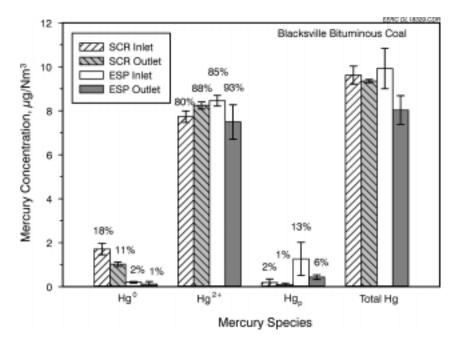


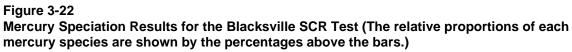
Mercury Speciation Results for the Blacksville Baseline Test (The relative proportions of each mercury species are shown by the percentages above the bars.)





#### Results





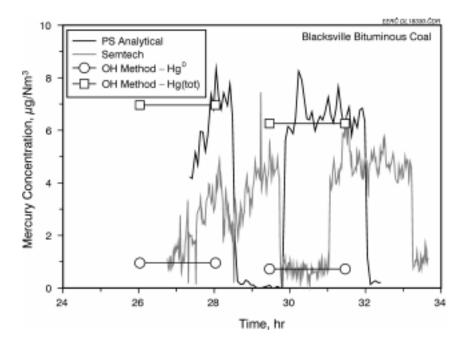
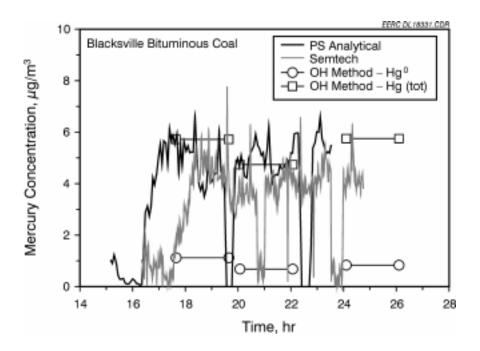
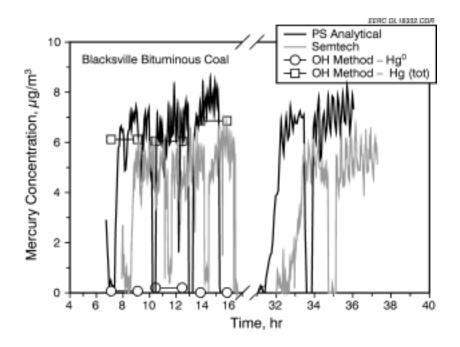


Figure 3-23 Comparison of Two Continuous Mercury Analyzers to the OH Method for the Blacksville Baseline Test









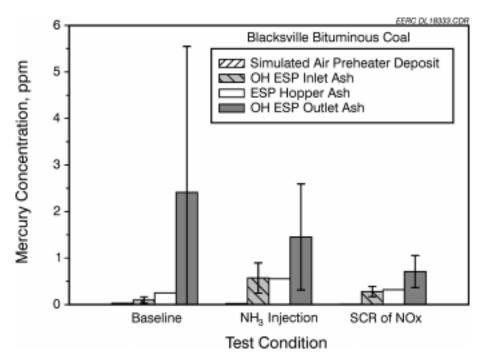


Figure 3-26 Mercury Concentration in the Blacksville Ash Samples

| Table 3-26  |
|---|
| Blacksville ESP Hopper Ash – Major, Minor, and Trace Element Compositions |

| Element, wt%                   | <b>Baseline Test</b> | NH <sub>3</sub> Injection Test | SCR Test |
|--------------------------------|----------------------|--------------------------------|----------|
| SiO <sub>2</sub>               | 45.1                 | 44.6                           | 44.8     |
| $AI_2O_3$                      | 23.6                 | 23.2                           | 23.2     |
| Fe <sub>2</sub> O <sub>3</sub> | 17.2                 | 16.7                           | 16.8     |
| MnO                            | 0.029                | 0.031                          | 0.032    |
| TiO <sub>2</sub>               | 1.08                 | 1.08                           | 1.11     |
| BaO                            | 0.11                 | 0.13                           | 0.12     |
| $P_2O_5$                       | 0.49                 | 0.54                           | 0.54     |
| CaO                            | 5.38                 | 5.84                           | 5.66     |
| MgO                            | 1.45                 | 1.50                           | 1.52     |
| Na₂O                           | 0.97                 | 0.97                           | 1.02     |
| K₂O                            | 1.80                 | 1.78                           | 1.86     |
| SO₃                            | 2.58                 | 3.31                           | 3.06     |
| NH <sub>3</sub>                | 0.0309               | 0.00435                        | 0.11     |
| Cl, ppm                        | 71                   | 69                             | 90       |
| Total, wt%                     | 99.8                 | 99.7                           | 99.8     |

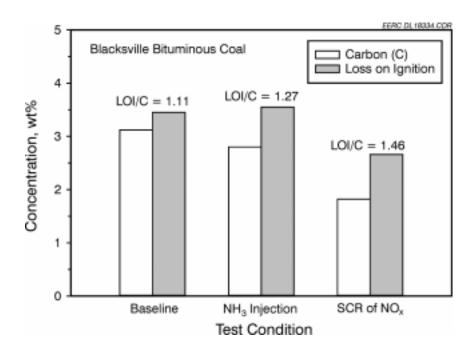


Figure 3-27 Loss on Ignition and Carbon in the Blacksville ESP Hopper Ash

#### 3.2.4.4 ESP Fly Ash and Total Mercury Collection Efficiencies

Table 3-27 presents a comparison of the ESP removal efficiencies for total mercury and fly ash at each of three test conditions conducted firing the Blacksville coal. As can be seen in Table 3-27, there was degradation in the operation of the ESP for the third test as the particulate collection efficiency was much lower. There did not appear to be much, if any, change in the total mercury removal by the ESP for any of the three test conditions.

| Run<br>No. | Hg <sub>ρ</sub> ,<br>μg/Nm³ | % Hg <sub>p</sub><br>Removal | % Total Hg<br>Removal | % Fly Ash<br>Removal |
|------------|-----------------------------|------------------------------|-----------------------|----------------------|
| 616        | 0.38                        | 60.5                         | 10.1                  | 96.9                 |
| 617        | 1.21                        | 90.1                         | 20.1                  | 96.4                 |
| 618        | 1.26                        | 65.9                         | 22.9                  | 82.6                 |

### Table 3-27 $\rm Hg_{p}$ Removal Efficiency of the ESP for the Blacksville Coal

## **4** DISCUSSION

#### 4.1 Mercury Speciation

A primary goal of this investigation was to do a screening evaluation at the pilot-scale level to determine the effects on mercury speciation of NH<sub>3</sub> injection and an SCR reactor for the reduction of NO<sub>x</sub>. In order to make direct comparisons at each sampling location, as a function of coal type and test condition, the mercury results are presented in Table 4-1 as a percentage change in mercury species relative to the baseline condition ( $\triangle$ Hg<sup>0</sup>,  $\triangle$ Hg<sup>2+</sup>, and  $\triangle$ Hg<sub>p</sub>). For example, Hg<sup>2+</sup> at the ESP inlet for the baseline Paradise test was 90% of the total mercury (Figure 3-2), whereas in the NH<sub>3</sub> injection test, the Hg<sup>2+</sup> made up only 39% of the total mercury at the ESP inlet (Figure 3-3). Therefore, injecting NH<sub>3</sub> resulted in a 51% decrease in Hg<sup>2+</sup> (i.e.,  $\triangle$ Hg<sup>2+</sup>, and  $\triangle$ Hg<sub>p</sub> for each of the tests are presented in Table 4-1. Values of <15% in Table 4-1 are considered insignificant based on variability in the mercury speciation results.

## 4.1.1 The Effects of NH<sub>3</sub> Injection Without the SCR Catalyst on Mercury Speciation

As shown in Table 4-1, there was an increase in  $Hg_p$  and a subsequent decrease in  $Hg^{2+}$  as a result of  $NH_3$  injection for the Paradise and Band Mill tests. However, with the Cordero Rojo coal, there appeared to be an increase in  $Hg^0$  as a result of  $NH_3$  injection. However, it is more than likely a result of data variability. For the Blacksville coal test,  $NH_3$  injection showed little, if any, significant change.

#### 4.1.2 The Effects of SCR of NO<sub>x</sub> on Mercury Speciation

 $\triangle$ Hg<sup>0</sup>,  $\triangle$ Hg<sup>2+</sup>, and  $\triangle$ Hg<sub>p</sub> in Table 4-1 show that SCR did not significantly affect the mercury speciation of Cordero Rojo and Blacksville flue gases. However, for the Paradise SCR test, a significant and quantifiable amount of Hg<sup>0</sup> was converted to Hg<sup>2+</sup> between the SCR inlet and SCR outlet sampling locations. There was also increased conversion of Hg<sup>2+</sup> to Hg<sub>p</sub> for the Paradise and Band Mill fuels for the SCR test compared to the NH<sub>3</sub> injection test.

#### 4.2 Fly Ash Chemical Compositions

As was discussed in the previous sections, Paradise, Cordero Rojo, Band Mill, and Blacksville fly ashes produced during the three different test conditions and captured in the ESP were chemically analyzed to evaluate the effects of  $NH_3$  injection and SCR of  $NO_x$  on ash composition including the concentration of  $Hg_p$ . The results are shown in Table 4-2. As can be

| Table 4-1  |
|--|
| Percent Change in Mercury Species Proportions Relative to the Baseline Tests |

| Coal:                          | I          | Paradise  | 3          | Co         | ordero R  | ојо        |            | Band Mill |            | В          | lacksvill | e          |
|--------------------------------|------------|-----------|------------|------------|-----------|------------|------------|-----------|------------|------------|-----------|------------|
| Sampling<br>Location:          | SCR<br>Out | ESP<br>In | ESP<br>Out |
| NH <sub>3</sub> Injection Only | 1          |           |            |            |           |            |            |           |            |            |           |            |
| $\Delta Hg^{\circ}$            | NA⁵        | 9.6       | 0.6        | NA         | 27.9      | 20.6       | NA         | 0.1       | 10.5       | NA         | 13.6      | 1.2        |
| $\Delta Hg^{2+}$               | NA         | -51.0     | -51.3      | NA         | -9.3      | -19.0      | NA         | -57.8     | -59.0      | NA         | -23.9     | -1.3       |
| $\Delta Hg_{p}$                | NA         | 41.4      | 50.7       | NA         | -18.6     | -1.7       | NA         | 57.8      | 48.5       | NA         | 10.3      | 0.1        |
| SCR Tests°                     |            |           |            |            |           |            |            |           |            |            |           |            |
| $\Delta Hg^{\circ}$            | -30.3      | -4.3      | -7.5       | 12.3       | -7.9      | 1.6        | ND⁴        | -9.8      | 0.1        | -6.9       | -6.2      | -13.3      |
| $\Delta Hg^{2+}$               | 27.2       | -78.3     | -72.7      | -11.9      | 8.3       | -11.7      | ND         | -69.6     | -65.3      | 7.9        | -2.5      | 9.7        |
| $\Delta Hg_{p}$                | 3.2        | 82.6      | 80.2       | -0.5       | -0.4      | 10.1       | ND         | 79.4      | 65.2       | -1.0       | 8.8       | 3.6        |

 $^{a}$  For the Paradise NH $_{3}$  injection test, 25 ppm was added, compared to 10 ppm for the remainder of the tests.  $^{b}$  Not applicable.

<sup>c</sup> For the Cordero Rojo and Band Mill tests, the NH<sub>3</sub>/NO<sub>x</sub> was ~1.2, compared to ~1.0 for Paradise and Blacksville tests. <sup>d</sup> Not determined because of a lack in repeatability among the three SCR bypass/inlet mercury speciation measurements.

|              | NH <sub>3</sub> Injection Test | SCR Test |
|--------------|--------------------------------|----------|
| Paradise     | 232                            | 286      |
| Cordero Rojo | -53                            | -0.3     |
| Band Mill    | 330                            | 456      |
| Blacksville  | 120                            | 27       |

Table 4-2 Percent Change in ESP Hopper Ash Hg, Concentrations Relative to Baseline Ashes

seen, there is a substantial increase in  $Hg_p$  for two of the bituminous coals. The unburned carbon particles in fly ash are potential mercury sorbents [27–30]. The carbon and LOI contents of fly ashes measured in the ESP hopper ashes, however, do not strongly correlate to  $Hg_p$  concentrations as shown in Figures 4-1 and 4-2. The R<sup>2</sup> values for carbon and LOI as a function of  $Hg_p$  are 0.211 and 0.456, respectively. The lack of a strong correlation in Figures 4-1 and 4-2 suggests that fly ash components other than carbon are more important in promoting the formation of  $Hg_p$ . These may include the NH<sub>3</sub> concentration and the reactivity of the carbon.

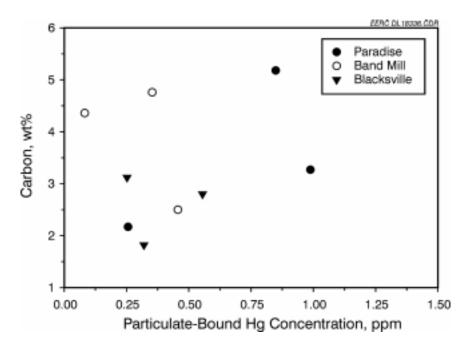


Figure 4-1 Mercury Concentration in the ESP Hopper Ashes as a Function of Carbon Content

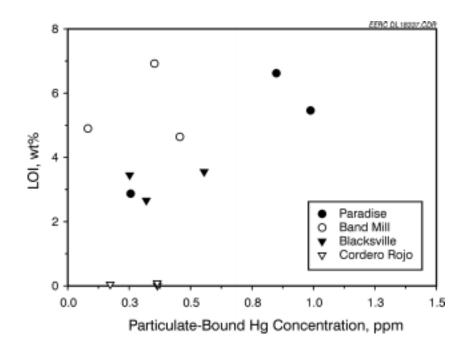
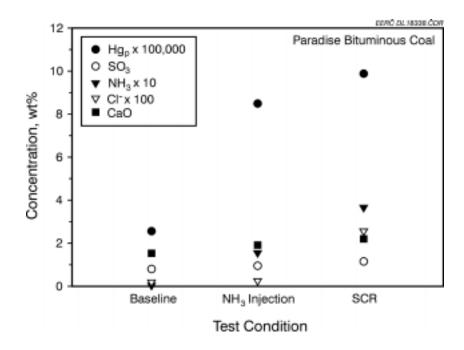
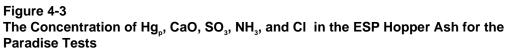


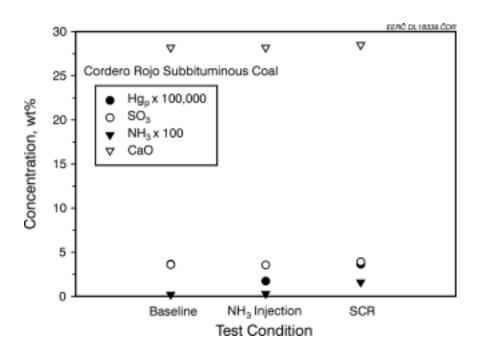
Figure 4-2 Mercury Concentration in the ESP Hopper Ashes as a Function of Loss on Ignition

Figures 4-3–4-6 show an increase in the NH<sub>3</sub> and Hg<sub>p</sub> concentrations in Paradise and Band Mill ESP hopper ashes as a result of adding NH<sub>3</sub> (both the NH<sub>3</sub> injection only and SCR test conditions), but not in the Cordero Rojo tests. Chloride concentrations in Paradise fly ashes (Figure 4-3) also increased. As shown in Table 4-2, the Hg<sub>p</sub> concentrations in the Paradise and Band Mill ESP hopper ashes increased significantly (230%–460%). The concentration of Hg<sub>p</sub> in the Blacksville ash increased as a result of injecting NH<sub>3</sub> into flue gas, but not when the flue gas was passed through the SCR. In all of the tests, the NH<sub>3</sub> concentration in the flue gas was somewhat different. This may have had an impact on the results. However, it is clear that increasing the Hg<sub>p</sub> concentration is advantageous. The collection efficiency of the ESP for Hg<sub>p</sub> is directly proportional to the ESP collection efficiency, as shown by Figure 4-7.

In addition to sulfur, the positive correlations between  $NH_3$  and  $Hg_p$  concentrations in Figure 4-8 imply that the formation of N-rich particles or sorption of N species on the Paradise and Band Mill fly ashes promoted  $Hg_p$  formation. A similar relationship between chlorides and  $Hg_p$  concentrations in Figure 4-8 for Paradise ashes suggests that Cl was involved in enhancing  $Hg_p$  formation. However, Cl does not positively correlate to  $Hg_p$  in the Blacksville ashes. When  $Hg_p$  concentration is compared as a function of Cl concentration (Figure 4-9), there is a positive correlation of  $R^2 = 0.331$ .









The Concentration of  $Hg_p$ , CaO, SO<sub>3</sub>, and  $NH_3$  in the ESP Hopper Ash for the Cordero Rojo Tests

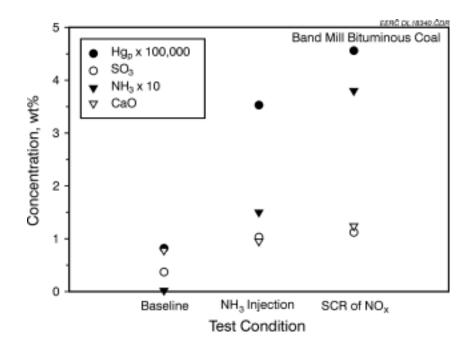


Figure 4-5 The Concentration of  $Hg_p$ , CaO, SO<sub>3</sub>, and  $NH_3$  in the ESP Hopper Ash for the Band Mill Tests

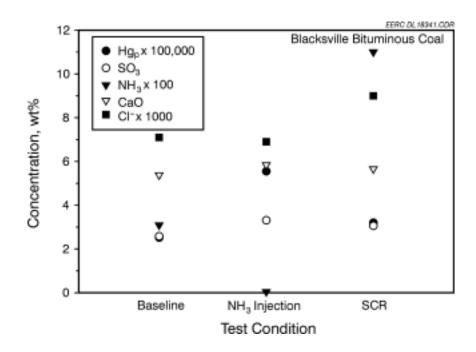


Figure 4-6 The Concentration of  $Hg_p$ , CaO, SO<sub>3</sub>, NH<sub>3</sub>, and CI in the ESP Hopper Ash for the Blacksville Tests

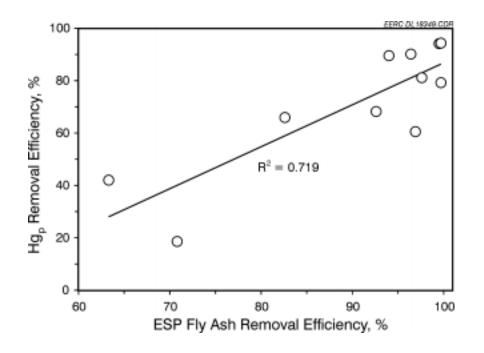


Figure 4-7 Hg<sub>p</sub> Removal Efficiency as a Function of ESP Collection Efficiency

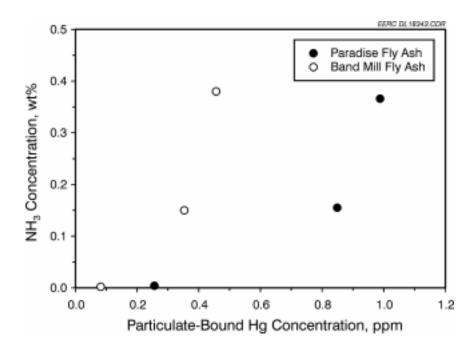


Figure 4-8 Mercury Concentration in the Paradise and Band Mill ESP Hopper Ashes as a Function of  $NH_3$  Concentration

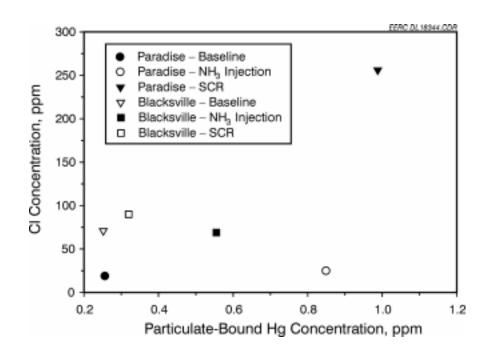


Figure 4-9 Mercury Concentration in the Paradise and Blacksville ESP Hopper Ashes as a Function of CI Concentration

#### 4.3 Linear Regression Analyses of the Results

Linear regression analyses were performed on mercury speciation results in reference to the chemical composition of the four test coals (Hg, S, Cl, and Ca concentrations in parts per million on a moisture-free basis). Selected regression correlations are shown in Appendix D. Appendix D tabulates three statistical parameters which are referred to in the discussion below: 1) a value of  $R^2$  for a specified number of data points (N), 2) the positive or negative "x coefficient" which indicates proportional dependence on the independent regression variable, and 3) the probability (P) that the x coefficient is significantly different from zero. The only independent variables presented are those with the highest statistical significance for a given set of data points. Some of the variables discussed, particularly where N is small, still have what would be considered to be a low statistical significance as indicated by their P values, where a P value of 0.95 is often used to identify a statistically significant variable. For most of the regression data sets, N has a value of 12 (4 coals  $\times$  3 test conditions). However, the regression data sets for the Hg<sup>0</sup> and Hg<sup>2+</sup> species leaving the furnace and entering the SCR are a special case and have an N of only 10 because the three measured values of these species for Band Mill coal were averaged to eliminate a wide divergence at essentially the same furnace conditions. N has a value of 4 for those data sets that represent SCR operation. Because of low values of N and scatter in the data, the regression equations presented in Appendix D should not be interpreted as reliable predictors of speciation but only as general indications of trends. Also, it should be noted that several factors concerned with the overall data set limit the validity of the regressions for full-scale plants. These factors include possible differences in mercury speciation as a function of the much smaller size of the pilot-scale combustor, the limited number and range of coal types, and differences in ammonia slip concentrations. These will be discussed in the recommendation section of this report.

The following discussion of regression equations relates to the order of the four tables in Appendix D, which respectively deal with 1) mercury speciation leaving the furnace and entering the SCR, 2) changes in mercury speciation across the SCR, 3) changes in speciation across the cooling loop, and 4) the percentages of coal mercury emitted as different species at the exit of the ESP. The discussion will identify the positive or negative effects of the coal and operating variables that are most significantly correlated with speciation at these four points.

The speciation of mercury leaving the EERC pilot-scale combustor and entering the SCR was principally correlated with the concentrations of Cl, Ca, and S in the coal (Table D-1). The percentages of coal mercury occurring as elemental mercury increased along with Ca and were reduced by Cl, with both elements indicated to be statistically significant at the 99% confidence level (P = 0.99) and the value of R<sup>2</sup> being 0.95 for N = 10. The percentages occurring as Hg<sup>2+</sup> decreased with increasing Ca and S and increased along with Cl, meaning that the correlations for Hg<sup>2+</sup> are the inverse of those for Hg<sup>0</sup>. This correlation was also statistically significant as indicated by P values of 0.99 for both Ca and S and a lower value of 0.88 for Cl; the value of R<sup>2</sup> was 0.94 at N = 10. The percentages occurring as Hg<sub>p</sub>, which were less well correlated at an R<sup>2</sup> of 0.58 for N = 10, increased along with Ca and Cl and were reduced by higher levels of coal Hg and SCR operation. Chlorine was the most significant variable with a P value of 0.96, followed by Hg at 0.88, SCR at 0.86, and Ca at 0.64.

Changes in mercury speciation across the SCR are represented by the regression equations in Table D-2. All of these correlations are based on the four tests performed with the SCR in operation (N = 4), and all changes are expressed as percent of mercury in coal. The change in total mercury across the SCR was negative for three of the four coals, possibly indicating adsorption. The upward trend from a negative to a positive change increased along with higher levels of coal Hg and higher values of Cl/Ca, with both variables being statistically significant at P values of 0.98 and 0.97 respectively. These high values of P for a two-variable regression with N = 4 (1 degree of freedom) indicate that the data points fall very close to the regression line, which was confirmed by graphing the data. The value of R<sup>2</sup> was 0.9997. Both positive and negative changes were observed in both elemental and oxidized mercury, suggesting that either oxidation or reduction could have occurred for different coals. The change in Hg<sup>0</sup> was negatively correlated with both Hg and Cl in coal at P levels of 0.99 and 0.86, respectively. The R<sup>2</sup> for the regression on changes in Hg<sup>0</sup> had a value of 0.9997. The change in Hg<sup>2+</sup> was positively correlated with Hg and Cl/Ca at P levels of 0.98 and 0.95, with an R<sup>2</sup> of 0.9992.

Changes in mercury species are greater across the cooling loop than across the SCR, but the changes that occur with cooling are not nearly as well correlated with coal and operating factors as are changes across the SCR (Table D-3). The changes in elemental mercury  $Hg^0$  increase from negative to positive along with higher levels of Cl and Hg in coal at P levels of 0.79 and 0.66 respectively;  $R^2$  has a value of 0.37 at N = 12. The change in  $Hg^{2+}$  is positively correlated with Hg and Cl/Ca, and negatively correlated with S in coal, at P levels of 0.84, 0.56, and 0.66, respectively;  $R^2$  is 0.32. The changes in particulate mercury increase with either NH<sub>3</sub> injection or SCR operation and are reduced by higher levels of Cl and Hg in coal; P values are 0.81, 0.65, 0.72, and 0.67, respectively, and  $R^2$  is 0.58.

Regression equations for the mercury species emitted at the exit of the ESP are given in Table D-4. All of these regressions are for N=12, and the emissions are expressed as percent of Hg in coal. The percentages of particulate mercury emitted were influenced by the efficiency of the ESP, but values for Hg<sup>0</sup> and Hg<sup>2+</sup> are believed to represent the chemistry of the system. The total mercury emitted increased along with Cl in coal and was reduced by NH<sub>3</sub> injection, at P levels of 0.68 and 0.92, respectively, and an R<sup>2</sup> of 0.41. The emission of elemental mercury was quite well correlated and was increased by Ca and reduced by S and Cl in coal and by SCR operation. The P levels are 0.99, 0.75, 0.62, and 0.94, respectively, and R<sup>2</sup> is 0.84. The emission of oxidized mercury was increased by Cl and reduced by Ca and NH<sub>3</sub> injection, which are the opposite of the coal effects shown for elemental mercury. P levels are 0.56, 0.86, and 0.97, respectively, and R<sup>2</sup> is 0.60. The emission of particulate mercury was increased by S in coal, NH<sub>3</sub> injection, and SCR operation and reduced by Cl and Ca in coal. P levels are 0.96, 0.73, 0.66, 0.94, and 0.66, indicating that coal S and Cl contents are the most significant variables.

Some of the trends described above are in agreement with the understanding of mercury combustion chemistry emerging from other research. The statistically indicated effect of coal Cl to increase  $Hg^{2+}$  and reduce  $Hg^{0}$  is in this category. The opposite effects indicated for coal Ca and S, tending to increase  $Hg^{0}$  and reduce  $Hg^{2+}$ , support trends that have been observed in other research, but the mechanisms responsible for these effects are less well understood. It is in the area of the statistically significant trends in mercury speciation through the SCR that the present tests and regression results may be providing new insights. The statistical correlations for changes in the SCR suggest a combination of adsorption and chemical oxidation or reduction depending on the levels of Hg, Cl, and Ca in the coal. These trends very much need to be confirmed by additional laboratory research and field testing before they are used generally to describe the effects of SCR on mercury. The positive correlation of an increase in particulate Hg indicated to occur with NH<sub>3</sub> injection, both through the cooling loop and at the EST exit, is another trend indication that may warrant follow-up. For now, as was stated previously, the correlation equations in Appendix D should not be treated as reliable predictors of speciation but only as trend indicators.

#### 4.4 Potential Hg<sub>p</sub> Formation Mechanisms

During combustion, sulfur is liberated from coal and subsequently oxidized to  $SO_2$ . A fraction of the  $SO_2$ , generally 1%–3%, is oxidized to  $SO_3$  [30]. The oxidation of  $SO_2$  to  $SO_3$  is catalyzed by transition metal oxides, such as the  $V_2O_5$ -based catalyst in the SCR reactor, but is neutralized by alkali and alkaline-earth metals in ash [31].  $SO_3$  can react downstream from the SCR with excess NH<sub>3</sub> (i.e., NH<sub>3</sub> that did not react with NO<sub>x</sub>) to create aerosols (particles 0.1–0.2 µm in diameter) that subsequently condense, predominantly as ammonium sulfate or ammonium bisulfate. These small, sticky particles can cause major clogging problems in an air preheater and on SCR catalyst surfaces. More importantly, with regard to this research, these small particles provide significant surface area, possibly for heterogeneous reactions involving mercury. Research indicates that heterogeneous reactions and physisorption are important mechanisms for transforming Hg<sup>0</sup> to Hg<sup>2+</sup> and Hg<sub>p</sub> [16–18].

Alkaline-earth metals such as calcium will react with  $SO_2$  and  $SO_3$ , especially on surfaces, to form calcium sulfite (CaSO<sub>3</sub>) and calcium sulfate (CaSO<sub>4</sub>). The CaSO<sub>3</sub> and CaSO<sub>4</sub> particles generated during combustion are probably very fine and widely distributed, thus increasing the potential for reactions to occur on air heater tube and catalyst surfaces. In addition to  $SO_2$  and  $SO_3$ , CaO will react with Cl [32]. The Cordero Rojo and Blacksville fly ashes possess greater CaO concentrations relative to Paradise and Band Mill fly ashes.

It is expected that sulfated compounds  $(NH_xCl_ySO_z)$  are likely to be small, sticky aerosols/particulate matter in the 0.1–0.2-µm size. Assuming these types of compounds form, they would also significantly increase surface area for mercury heterogeneous condensation reactions. Additionally, because these compounds are chlorinated, they may increase mercury oxidation. If the assumptions stated above are accurate, this may offer an explanation as to why increased mercury and Cl are measured in the Paradise SCR test fly ash but not in the other two Paradise coal tests. This may also explain why the Blacksville ash for the SCR test had less mercury than the NH<sub>3</sub> injection tests. That is, during the Blacksville SCR, there was little unreacted NH<sub>3</sub> to react with SO<sub>3</sub> or possibly Cl.

#### 4.5 Particle–Gas Partitioning of Mercury

The solid-gas partitioning of mercury at the ESP inlet and outlet sampling locations was measured using a part of the OH method. It has been previously seen that particle-gas filtration through a fixed bed of ash particles, especially fine ash particles, can promote Hg<sub>p</sub> formation [33]. In order to investigate whether this occurred during the Paradise test, a heated 5-stage cascade multicyclone sampler was used to collect aerodynamically sized fly ash samples at the ESP inlet. Simultaneously, ash samples were collected at the same location using a standard filter. The measured particle-size distribution using the multicyclone is presented in Figure 4-10. Submicron fly ash particles that most likely penetrated the ESP account for only about 1.5% of the total fly ash mass. However, the total number and surface area of these small particles are high relative to their mass concentration. Mercury concentrations for the size-fractionated Paradise fly ash samples produced during the SCR test are presented in Figure 4-11. Although mercury is most concentrated in the smallest particle-size fraction (i.e., filter catch) and least concentrated in the largest particle-size fraction, on a mass basis, most of the mercury appears to be associated with the larger particles. Mercury concentrations for the bulk fly ashes sampled on the OH sample filter and multicyclones were 1.29 and 1.28 ppm, respectively. These values are essentially identical, within sampling and analytical errors, indicating that the particle-gas filtration through a fixed bed of Paradise fly ash did not promote Hg<sub>p</sub> formation any more than did cyclonic filtration.

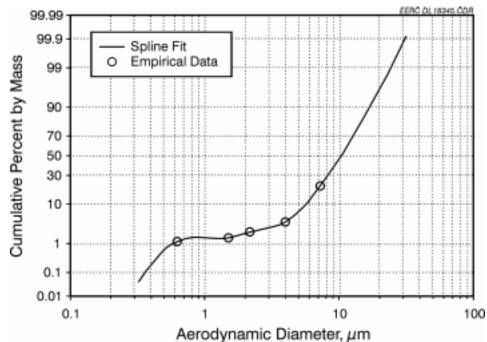
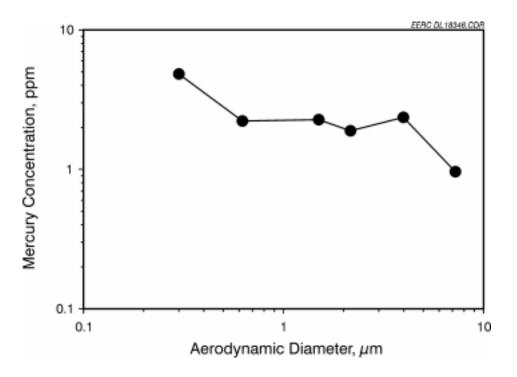


Figure 4-10 Particle-Size Distribution at the ESP Inlet for the Paradise SCR Test





# **5** CONCLUSIONS

Based on the results obtained from this screening evaluation, the following conclusions can be made:

- For some coals, NH<sub>3</sub> appeared to increase the Hg<sub>p</sub> concentration; thereby increasing Hg removal in the downstream ESP. Because NH<sub>3</sub> slips were higher than expected in a full-scale SCR or SNCR application and NH<sub>3</sub> concentration may directly impact Hg speciation and removal, these results may or may not be consistent with full-scale applications.
- The impact of SCR on mercury speciation and mercury capture appears to be very coal dependent and quite complex.
- Based on a regression analysis, the chlorine, sulfur, and calcium appear to correlate with mercury speciation across the SCR.
- Relatively high concentrations of alkaline-earth metals (i.e., CaO and MgO) in the Cordero Rojo and Blacksville fly ashes may have limited the suspected interactions involving SO<sub>3</sub>, NH<sub>3</sub>, and Cl that promote Hg<sub>p</sub> formation.
- NH<sub>3</sub> injection and/or the SCR catalyst promoted the conversion of Hg<sup>0</sup> to Hg<sup>2+</sup> across the SCR for the Paradise coal, but not for any of the others.
- NH<sub>3</sub> injection, with and without the SCR reactions, converted  $Hg^{2+}$  to  $Hg_p$  when the Paradise and Band Mill coals were fired, but not for the Cordero Rojo PRB.
- The increased mercury removals as measured by the flue gas measurements were confirmed with mercury analyses of the corresponding fly ash. The  $Hg_p$  concentrations in Paradise and Band Mill ESP hopper ashes increased by 230%–460% relative to the baseline fly ashes as a result of  $NH_3$  injection and SCR tests.
- Because of the high levels of  $Hg^{2+}$  in the baseline tests, it is not possible to determine whether there was an increase in  $Hg_p$  or oxidation of  $Hg^0$  for the Blacksville coal.

The applicability of the conclusions from this pilot-scale investigation should be evaluated by performing similar flue gas and fly ash measurements at utility-scale boilers equipped with selective noncatalytic reduction (SNCR) and SCR units. As part of this proposed utility-scale investigation, flue gas and fly ash samples should be collected when the SNCR and SCR units are off-line and on-line. Size-fractionated fly ash samples should also be collected and analyzed to investigate further the apparent role of particle size and composition on  $Hg_p$  formation. Additional coals also need to be tested because the impact of SNCR and SCR of  $NO_x$  on mercury speciation apparently depends on the coal's chemical composition.

References

# 6 RECOMMENDATIONS

These pilot-scale tests were completed only as a screening evaluation of the impact of SCR on mercury speciation. In a number of ways, these tests did not mimic a full-scale combustor, SCR, and ESP. For example, it is possible that the mercury flue gas chemistry may be different firing coal in the PTC compared to a full-scale pulverized coal combustor. It appears that PTC generates more Hg<sup>2+</sup> than predicted using the EPRI correlations developed from the ICR results [2]. These correlations are based on the sulfur and chloride content of the coal. Table 6-1 compares the EPRI correlation with the EERC speciation baseline results at the ESP inlet sampling location for the four test coals. The difference may be due to shorter residence time along with a different time/temperature profile for the PTC compared to a full-scale boiler.

| Table 6-1  |
|--|
| Comparison of EERC Mercury Speciation Results to Those Predicted by EPRI's |
| Correlations   |

| Fuel                            | Hg⁰ Concentration based<br>on EPRI Correlations, % | Hg <sup>⁰</sup> Concentration based on<br>EERC Measurement, % |
|---------------------------------|--|---|
| Paradise Bituminous Coal        | 46   | 7   |
| Cordero Rojo Subbituminous Coal | 71   | 61  |
| Band Mill Bituminous Coal       | 69   | 16  |
| Blacksville Bituminous Coal     | 36   | 13  |

The EERC's ESP was never intended to represent a full-scale system. Therefore, for a number of the tests, the particulate collection efficiency was low and varied considerably. The collection efficiency for the three bituminous coal tests averaged about 90% compared to >99% for a well-operating full-scale ESP. Also, because of a calibration error, several of the tests had much higher  $NH_3$  concentrations in the flue gas than would have been desired. This may have complicated the interpretation of the data and resulted in more variability.

Therefore, the applicability of the conclusions from these pilot-scale test must be evaluated by performing similar flue gas and fly ash measurements at utility-scale boilers equipped with SNCR and SCR units.

A final recommendation is that bench-scale studies be completed to provide a better understanding of mercury,  $NH_3$ ,  $SO_3$ , and fly ash chemistry as it relates to SCRs. Currently, some of this work is being done by the University of Cincinnati, but these pilot-scale results may warrant an expansion of that program or the initiation of a new bench-scale project.

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References

# **A** FLUE GAS TEMPERATURE

#### Table A-1

Paradise Bituminous Coal Average Flue Gas Temperatures, °F

|                 | Baseline NH <sub>3</sub> Injection |           | SCR     |           |         |           |
|-----------------|------------------------------------|-----------|---------|-----------|---------|-----------|
|                 | Average                            | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. |
| SCR Bypass      | 610                                | 68        | 603     | 38        | *       | _         |
| SCR Inlet       | —                                  | —         | —       | —         | 651     | 48        |
| SCR             | —                                  | —         | —       | —         | 642     | 22        |
| SCR Outlet      | _                                  | —         | —       | —         | 627     | 39        |
| ESP Inlet       | 349                                | 13        | 372     | 17        | 332     | 16        |
| ESP Outlet      | 294                                | 12        | 309     | 14        | 283     | 15        |
| Deposition Tube | 399                                | 14        | 398     | 12        | 399     | 15        |

\*Not applicable.

#### Table A-2 Cordero Rojo Coal Average Flue Gas Temperatures, °F

|                 | Baseline |           | NH <sub>3</sub> Injection |           | NH <sub>3</sub> Injection |           | SCR |  |
|-----------------|----------|-----------|---------------------------|-----------|---------------------------|-----------|-----|--|
|                 | Average  | Std. Dev. | Average                   | Std. Dev. | Average                   | Std. Dev. |     |  |
| SCR Bypass      | 607      | 42        | 614                       | 21        | *                         | —         |     |  |
| SCR Inlet       | —        | —         | —                         | —         | 661                       | —         |     |  |
| SCR             | —        | —         | —                         | —         | 655                       | —         |     |  |
| SCR Outlet      | —        | —         | —                         | —         | 643                       | 12        |     |  |
| ESP Inlet       | 339      | 7         | 341                       | 7         | 345                       | 7         |     |  |
| ESP Outlet      | 290      | 8         | 291                       | 7         | 294                       | 7         |     |  |
| Deposition Tube | 401      | 6         | 402                       | 8         | 403                       | 5         |     |  |

\*Not applicable.

|                 | Bas     | eline     | NH <sub>3</sub> Injection |           | SCR     |           |
|-----------------|---------|-----------|---------------------------|-----------|---------|-----------|
|                 | Average | Std. Dev. | Average                   | Std. Dev. | Average | Std. Dev. |
| SCR Bypass      | 637     | 67        | 624                       | 34        | *       | —         |
| SCR Inlet       | —       | —         | —                         | —         | 671     | 18        |
| SCR             | —       | —         | —                         | —         | 664     | 11        |
| SCR Outlet      | —       | —         | —                         | —         | 655     | 16        |
| ESP Inlet       | 341     | 4         | 360                       | 26        | 346     | 16        |
| ESP Outlet      | 291     | 3         | 300                       | 11        | 291     | 13        |
| Deposition Tube | 391     | 57        | 398                       | 22        | 399     | 9         |

### Table A-3Average Band Mill Coal Combustion Flue Gas Temperatures, °F

\*Not applicable.

## Table A-4Average Blacksville Coal Combustion Flue Gas Temperatures, °F

|                 | Baseline NH <sub>3</sub> Inj |           | jection | SCR       |         |           |
|-----------------|------------------------------|-----------|---------|-----------|---------|-----------|
|                 | Average                      | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. |
| SCR Bypass      | 636                          | 19        | 625     | 25        | *       | —         |
| SCR Inlet       | —                            | —         | —       | —         | 655     | 6         |
| SCR             | —                            | —         | —       | —         | 653     | 11        |
| SCR Outlet      | —                            | —         | —       | —         | 642     | 19        |
| ESP Inlet       | 344                          | 9         | 351     | 10        | 350     | 7         |
| ESP Outlet      | 293                          | 12        | 303     | 9         | 301     | 7         |
| Deposition Tube | 399                          | 16        | 397     | 22        | 398     | 20        |

\*Not applicable.

# $\boldsymbol{B}$ sample calculations

#### **Example Calculations of NH**, Flue Gas Flow Rates and Mass Balances

#### **Constants**

Molar volume of an ideal gas at 0°C and 1 atm pressure = 22.41 L Formula weight of  $NH_3 = 17.031$  g/mol Combustor flue gas flow rate  $\approx 175$   $Nm^3/hr = 175,000$  L/hr

700  $ppm \times \frac{17.031 \text{ g}/\text{mol} \times 175,000 \text{ L/hr}}{22.41 \text{ L/mol} \times 10^6} = 93.1 \text{ g/hr}$ 

Conversion of 5 ppmv NH<sub>3</sub>(g) to a flue gas flow rate, g/hr

Conversion of 5000  $\mu$ g/Nm<sup>3</sup> NH<sub>3</sub>(p) to a flue gas flow rate, g/hr

 $5000 \ \mu g \ / \ Nm^3 \times 175 \ Nm^3 \ / \ hr \times \frac{1g}{1,000,0000} = 0.88 \ g \ / \ hr$ 

Conversion of NO<sub>x</sub> removal to an equivalent NH<sub>3</sub> removal rate, g/hr

SCR inlet  $NO_x = 700 \text{ ppmv}$ ESP inlet  $NO_x = 20 \text{ ppmv}$  $NO_x \text{ removal} = 680 \text{ ppmv}$ 

680  $ppm \times \frac{17.031 \ g/mol \times 175,000 \ L/hr}{22.41 \ L/mol \times 10^6} = 90.4 \ g/hr$ 

## Example of Mercury Mass Balance Calculations for the SCR of $NO_x$ Paradise Coal Test (609)

Mercury mass balances were calculated from the average coal Hg concentrations, coal feed rates, average flue gas flows, total Hg concentrations measured at each sampling location, electrostatic precipitator (ESP) dust loadings and fly ash collection efficiencies, and ESP hopper ash Hg concentrations. An example of these data is presented in Table B-1 for the selective catalytic reduction (SCR) of NO<sub>x</sub> Paradise Coal Test (609).

| Parameter, unit   | Value  |
|---|--------|
| Coal Feed Rate, g/hr  | 22,093 |
| Coal Hg, as-received, μg/g  | 0.111  |
| Flue Gas Flow Rate, dNm <sup>3</sup> @3% O <sub>2</sub> /hr             | 186.51 |
| ESP Inlet Dust Load, g/hr   | 1355.7 |
| ESP Ash Collection Efficiency, %  | 63.3   |
| ESP Hopper Ash Hg, µg/g   | 0.988  |
| Total Hg at the SCR Bypass/Inlet, $\mu g/dNm^3$ @3% $O_{_2}$            | 10.6   |
| Total Hg at the SCR outlet, $\mu g/dNm^3$ @3% O <sub>2</sub>            | 11.5   |
| Total Hg at the ESP Inlet, $\mu$ g/dNm <sup>3</sup> @3% O <sub>2</sub>  | 11.4   |
| Total Hg at the ESP Outlet, $\mu$ g/dNm <sup>3</sup> @3% O <sub>2</sub> | 6.71   |

| Table B-1  |
|--|
| Average Measurement Data for the SCR of NO <sub>x</sub> Paradise Coal Test (609) |

Hg mass balances for each sampling location are calculated relative to the average coal Hg feed rate during the combustion test where:

coal Hg feed rate = coal feed rate  $\times$  coal Hg

Therefore, the coal Hg feed rate was 2452  $\mu$ g/hr (22,093 g/hr × 0.111  $\mu$ g/g) during the SCR of NO<sub>x</sub> Paradise coal test.

The removal of Hg from the flue gas by the ESP is accounted for using the following equation:

ESP Hg removal rate = ESP inlet dust load × ESP hopper ash Hg × (ESP ash collection efficiency  $\div$  100)

According to the values in Table B-1, the ESP removed Hg from the flue gas at a rate of 847.8  $\mu$ g/hr (1355.7 g/hr × 0.988  $\mu$ g/g × [63.3 ÷ 100]).

Total Hg flow rates at the SCR bypass/inlet, SCR outlet, ESP inlet, and ESP outlet are calculated by simply multiplying the total Hg concentrations in Table B-1 by the flue gas flow rate, for example:

total Hg flow rate at the SCR bypass/inlet =  $10.6 \mu g/dNm^3 @3\% O_2 \times 186.51 dNm^3 @3\% O_2/hr$ =  $1977 \mu g/hr$ 

Total Hg flow rates for the four sampling locations are presented in Table B-2.

Percent Hg mass balances for the SCR inlet/bypass, SCR outlet, and ESP inlet are calculated by dividing the Hg flow rates in Table B-2 by the average coal Hg feed rate and multiplying by 100. For example, Hg mass balance at the ESP inlet was:

$$2126 \,\mu g/hr \div 2452 \,\mu g/hr \times 100 = 86.7\%$$
.

A Hg mass balance for the ESP outlet is calculated by combining the ESP outlet Hg flow rate and ESP removal rate then dividing by the average coal Hg feed rate and multiplying by 100. For example, Hg mass balance at the ESP outlet was:

$$(1251 \ \mu g/hr + 847.8 \ \mu g/hr) \div 2452 \ \mu g/hr \times 100 = 85.6\%$$

Mass balance results for the four sampling locations are presented in Table B-3.

#### Table B-2

Calculated Hg Feed, Flow, and Removal Rates for the SCR of NO<sub>x</sub> Paradise Coal Test (609)

| Parameter                                  | µg/hr |
|--|-------|
| Coal Hg Feed Rate                          | 2452  |
| ESP Hg Removal Rate                        | 847.8 |
| Total Hg Flow Rate at the SCR Bypass/Inlet | 1977  |
| Total Hg Flow Rate at the SCR Outlet       | 2145  |
| Total Hg Flow Rate at the ESP Inlet        | 2126  |
| Total Hg Flow Rate at the ESP Outlet       | 1251  |

#### Table B-3 Hg Mass Balance Results for the SCR of NO<sub>x</sub> Paradise Coal Test (609)

| Location         | Hg Mass Balance, % |
|------------------|--------------------|
| SCR Bypass/Inlet | 80.6               |
| SCR Outlet       | 87.5               |
| ESP Inlet        | 86.7               |
| ESP Outlet       | 85.6               |

# $\boldsymbol{C}$ mercury and $\text{NH}_{\scriptscriptstyle 3}$ mass balance data

#### **Mercury Mass Balance Data**

#### Table C-1

Paradise Bituminous Coal – Tests 607 through 609 Mercury Mass Balance Data

| Coal and Mercury Feed Rates |        |
|-----------------------------|--------|
| Total Coal Burned, Ib       | 5006   |
| Coal Feed Total Time, hr    | 102.8  |
| Coal Feed Rate, lb/hr       | 48.71  |
| Coal Feed Rate, g/hr        | 22,093 |

| Test No.  | 607    | 608    | 609    |
|---|--------|--------|--------|
| Coal Hg, as-received µg/g                             | 0.11   | 0.114  | 0.111  |
| Coal Hg Feed Rate, µg/hr                              | 2430   | 2519   | 2452   |
| Average Flue Gas Flow Rate, scfm                      | 130.9  | 130    | 130    |
| Average Flue Gas O <sub>2</sub> , %                   | 5.34   | 5.51   | 4.47   |
| Average Flue Gas $H_2O$ , %                           | 8.02   | 7.87   | 8.06   |
| Flue Gas Flow, dNm <sup>3</sup> @3%O <sub>2</sub> /hr | 177.99 | 175.13 | 186.51 |
| Hooper Ash Mercury, μg/g                              | 0.256  | 0.849  | 0.988  |
| Avg. ESP Inlet Dust Load, grains/scf                  | 2.6334 | 0.7625 | 2.6822 |
| Avg. ESP Dust, g/hr                                   | 1340.2 | 385.4  | 1355.7 |
| Avg. ESP Collection Efficiency, %                     | 87     | 70.8   | 63.3   |
| Hopper Ash Mercury, µg/hr                             | 298.5  | 231.7  | 847.8  |

### Table C-2 Paradise Bituminous Coal – Tests 607 through 609 Mercury Mass Balance Results

| Run No.      |          |           | 607  |      |           |      |      | 608  |      |           |      |      | 609   |       |           |
|--------------|----------|-----------|------|------|-----------|------|------|------|------|-----------|------|------|-------|-------|-----------|
| Total Mercur | y Flow R | ate, µg/ŀ | nr   |      |           |      |      |      |      |           |      |      |       |       |           |
| Sample       | 1        | 2         | 3    | Avg. | Std. Dev. | 1    | 2    | 3    | Avg. | Std. Dev. | 1    | 2    | 3     | Avg.  | Std. Dev. |
| SCR In       | 2193     | _         | -    | _    | _         | 1879 | _    | _    | _    | _         | 1656 | _    | _     | 1909* | 270*      |
| SCR Out      | _        | _         | _    | _    | _         | _    | _    | _    | -    | _         | 1938 | 1179 | 2740  | 1952  | 781       |
| ESP In       | 2179     | 2173      | 1876 | 2076 | 173       | 1373 | 1602 | 1827 | 1601 | 227       | 2259 | 2089 | 2050  | 2133  | 111       |
| ESP Out      | 1771     | 1977      | 1842 | 1863 | 105       | 904  | 1119 | 1158 | 1060 | 137       | 1548 | 1546 | 662   | 1252  | 511       |
| Mercury Mas  | s Balanc | се, %     |      |      |           |      |      |      |      |           |      |      |       |       |           |
| SCR In       | 90.2     | _         | _    | _    | _         | 74.6 | _    | _    | _    | _         | 67.5 | _    | _     | 77.5* | 11.6**    |
| SCR Out      | -        | _         | _    | _    | -         | _    | _    | _    | _    | _         | 79.0 | 72.6 | 111.7 | 87.8  | 21.0      |
| ESP In       | 89.6     | 89.4      | 77.2 | 85.4 | 7.1       | 54.5 | 63.6 | 72.5 | 63.6 | 9.0       | 92.1 | 85.2 | 83.6  | 87.0  | 4.5       |
| ESP Out      | 85.2     | 93.7      | 88.1 | 89.0 | 4.3       | 45.1 | 53.6 | 55.2 | 51.3 | 5.4       | 97.7 | 97.6 | 61.6  | 85.6  | 20.8      |

| Table C-3   |
|---|
| Cordero Rojo Subbituminous Coal – Tests 610 through 612 Mercury Mass Balance Data |

| Coal and Mercury Feed Rates |        |       |       |
|-----------------------------|--------|-------|-------|
| Total Coal Burned, Ib       | 6812   |       |       |
| Coal Feed Total Time, hr    | 99.68  |       |       |
| Coal Feed Rate, lb/hr       | 68.34  |       |       |
| Coal Feed Rate, g/hr        | 30,998 |       |       |
| Test No.                    | 610    | 612   | 613   |
| Coal Hg. as-received µg/g   | 0.087  | 0.091 | 0.077 |

|   |        |        | ••••   |
|---|--------|--------|--------|
| Coal Hg, as-received µg/g                             | 0.087  | 0.091  | 0.077  |
| Coal Hg Feed Rate, µg/hr                              | 2697   | 2821   | 2387   |
| Average Flue Gas Flow Rate, scfm                      | 133.1  | 131.1  | 132.1  |
| Average Flue Gas $O_2$ , %                            | 4.53   | 4.48   | 4.81   |
| Average Flue Gas $H_2O$ , %                           | 11.06  | 10.42  | 11.30  |
| Flue Gas Flow, dNm <sup>3</sup> @3%O <sub>z</sub> /hr | 184.05 | 183.15 | 179.08 |
| Hooper Ash Mercury, µg/g                              | 0.365  | 0.173  | 0.364  |
| Avg. ESP Inlet Dust Load, grains/scf                  | 1.8002 | 1.9956 | 1.4126 |
| Avg. ESP Dust, g/hr                                   | 932    | 1017   | 726    |
| Avg. ESP Collection Eff., %                           | 99.47  | 99.73  | 99.72  |
| Hopper Ash Mercury, µg/hr                             | 338.2  | 175.5  | 263.3  |

### Table C-4 Cordero Rojo Subbituminous Coal – Tests 610 through 612 Mercury Mass Balance Results

| Run No.      |          |           | 610  |      |           |      |       | 611   |      |           |       |      | 612   |                   |                                   |
|--------------|----------|-----------|------|------|-----------|------|-------|-------|------|-----------|-------|------|-------|-------------------|-----------------------------------|
| Total Mercur | y Flow R | ate, µg/ł | hr   |      |           |      |       |       |      |           |       |      |       |                   |                                   |
| Sample       | 1        | 2         | 3    | Avg. | Std. Dev. | 1    | 2     | 3     | Avg. | Std. Dev. | 1     | 2    | 3     | Avg.              | Std. Dev.                         |
| SCR In       | 2591     | _         | _    | _    | _         | 2714 | _     | _     | _    | _         | 3066  | _    | _     | 2790ª             | 247ª                              |
| SCR Out      | _        | _         | _    | _    | _         | _    | -     | _     | _    | _         | _     | 2190 | 578   | 2101              | 2146 <sup>b</sup> 63 <sup>b</sup> |
| ESP In       | 2560     | 2360      | 2415 | 2445 | 103       | 2441 | 2879  | 2890  | 2737 | 256       | 2767  | 2357 | 3331  | 2818              | 489                               |
| ESP Out      | 1465     | 1520      | 2063 | 1683 | 330       | 1749 | 2016  | 2247  | 2004 | 249       | 1035  | 1173 | 1511  | 1240              | 245                               |
| Mercury Mas  | s Balanc | e, %:     |      |      |           |      |       |       |      |           |       |      |       |                   |                                   |
| SCR In       | 96.1     | _         | _    | _    | _         | 96.2 | _     | _     | _    | _         | 128.4 | _    | _     | 106.9ª            | 18.6ª                             |
| SCR Out      | -        | _         | _    | _    | -         | _    | _     | _     | _    | _         | 91.8  | 24.2 | 88.0  | 89.0 <sup>ь</sup> | 2.7 <sup>b</sup>                  |
| ESP In       | 94.9     | 87.5      | 89.5 | 90.7 | 3.8       | 86.5 | 102.1 | 102.5 | 97.0 | 9.1       | 115.9 | 98.7 | 139.6 | 118.1             | 20.5                              |
| ESP Out      | 66.9     | 68.9      | 89.0 | 74.9 | 12.3      | 68.2 | 77.7  | 85.9  | 77.3 | 8.8       | 54.4  | 60.2 | 74.4  | 63.0              | 10.3                              |

<sup>a</sup>Average and standard deviation of the three runs (610–612).

<sup>b</sup>Sample Number 2 was not used to calculate average and standard deviation.

| Table C-5   |
|---|
| Band Mill Bituminous Coal – Tests 613 through 615 Mercury Mass Balance Data |

| Coal and Mercury Feed Rates |        |  |  |  |  |  |  |  |  |
|-----------------------------|--------|--|--|--|--|--|--|--|--|
| Total Coal Burned, Ib       | 4501   |  |  |  |  |  |  |  |  |
| Coal Feed Total Time, hr    | 103.28 |  |  |  |  |  |  |  |  |
| Coal Feed Rate, lb/hr       | 43.58  |  |  |  |  |  |  |  |  |
| Coal Feed Rate, g/hr        | 19,768 |  |  |  |  |  |  |  |  |

| Test No.  | 613    | 614    | 615    |
|---|--------|--------|--------|
| Coal Hg, as-received µg/g                             | 0.023  | 0.022  | 0.022  |
| Coal Hg Feed Rate, µg/hr                              | 455    | 435    | 435    |
| Average Flue Gas Flow Rate, scfm                      | 131.2  | 129.9  | 130.6  |
| Average Flue Gas O <sub>2</sub> , %                   | 5.20   | 5.15   | 4.99   |
| Average Flue Gas $H_2O$ , %                           | 7.36   | 7.12   | 7.34   |
| Flue Gas Flow, dNm <sup>3</sup> @3%O <sub>2</sub> /hr | 18.28  | 180.5  | 182.89 |
| Hooper Ash Mercury, µg/g                              | 0.082  | 0.353  | 0.456  |
| Avg. ESP Inlet Dust Load, grains/scf                  | 1.5559 | 0.8229 | 0.7559 |
| Avg. ESP Dust, g/hr                                   | 794    | 416    | 384    |
| Avg. ESP Collection Eff., %                           | 94.0   | 92.6   | 97.6   |
| Hopper Ash Mercury, µg/hr                             | 61.2   | 135.9  | 170.8  |

### Table C-6 Band Mill Bituminous Coal – Tests 613 through 615 Mercury Mass Balance Results

| Run No.      |          |           | 613   |       |           |      |      | 614  |      |           |       |      | 615  |                    |                   |
|--------------|----------|-----------|-------|-------|-----------|------|------|------|------|-----------|-------|------|------|--------------------|-------------------|
| Total Mercur | y Flow R | ate, µg/ł | nr    |       |           |      |      |      |      |           |       |      |      |                    |                   |
| Sample       | 1        | 2         | 3     | Avg.  | Std. Dev. | 1    | 2    | 3    | Avg. | Std. Dev. | 1     | 2    | 3    | Avg.               | Std. Dev.         |
| SCR In       | 874      | _         | _     | _     | _         | 132  | _    | _    | _    | _         | 540   | -    | _    | 515 <sup>°</sup>   | 372 <sup>*</sup>  |
| SCR Out      | -        | _         | _     | _     | _         | _    | _    | _    | _    | -         | 358   | 315  | 351  | 341                | 24                |
| ESP In       | 513      | 488       | 412   | 471   | 53        | 383  | 204  | 325  | 304  | 128       | 318   | 382  | 342  | 347                | 32                |
| ESP Out      | 1196     | 509       | 422   | 709   | 424       | 112  | 161  | 112  | 128  | 28        | 91    | 79   | 88   | 86                 | 7                 |
| Mercury Mas  | s Baland | e, %:     |       |       |           |      |      |      |      |           |       |      |      |                    |                   |
| SCR In       | 192.2    | _         | _     | _     | _         | 30.3 | _    | _    | _    | _         | 124.1 | _    | _    | 115.5 <sup>°</sup> | 81.3 <sup>*</sup> |
| SCR Out      | -        | _         | -     | _     | -         | _    | -    | -    | _    | _         | 82.4  | 72.3 | 80.7 | 78.5               | 5.4               |
| ESP In       | 112.8    | 107.3     | 90.5  | 103.5 | 11.6      | 88.0 | 46.9 | 74.7 | 69.9 | 21.0      | 73.2  | 87.9 | 78.6 | 79.9               | 7.4               |
| ESP Out      | 276.6    | 125.5     | 106.4 | 115.9 | 93.3      | 57.0 | 68.2 | 57.0 | 60.7 | 6.5       | 60.3  | 57.4 | 59.5 | 59.0               | 1.5               |

<sup>a</sup>Average and standard deviation of the three runs (613–615).

| Table C-7   |
|---|
| Blacksville Bituminous Coal – Tests 616 through 618 Mercury Mass Balance Data |

| Coal and Mercury Feed Rates |        |  |  |  |  |  |  |  |  |
|-----------------------------|--------|--|--|--|--|--|--|--|--|
| Total Coal Burned, Ib       | 4688.0 |  |  |  |  |  |  |  |  |
| Coal Feed Total Time, hr    | 103.5  |  |  |  |  |  |  |  |  |
| Coal Feed Rate, lb/hr       | 45.31  |  |  |  |  |  |  |  |  |
| Coal Feed Rate, g/hr        | 20,551 |  |  |  |  |  |  |  |  |

| Test No.  | 616    | 617    | 618    |
|---|--------|--------|--------|
| Coal Hg, as-received, µg/g                            | 0.0950 | 0.0899 | 0.0973 |
| Coal Hg Feed Rate, µg/hr                              | 1952   | 1848   | 2000   |
| Average Flue Gas Flow Rate, scfm                      | 131.5  | 130.5  | 129.9  |
| Average Flue Gas $O_2$ , %                            | 5.31   | 5.55   | 4.81   |
| Average Flue Gas $H_2O$ , %                           | 7.24   | 7.32   | 7.76   |
| Flue Gas Flow, dNm <sup>3</sup> @3%O <sub>2</sub> /hr | 180.67 | 176.40 | 183.12 |
| Hooper Ash Mercury, µg/g                              | 0.252  | 0.555  | 0.320  |
| Avg. ESP Inlet Dust Load, grains/scf                  | 1.4053 | 0.7500 | 1.5684 |
| Avg. ESP Dust, g/hr                                   | 718.5  | 380.5  | 792.1  |
| Avg. ESP Collection Eff., %                           | 96.9   | 96.4   | 82.6   |
| Hopper Ash Mercury, µg/hr                             | 175.4  | 203.6  | 209.4  |

### Table C-8 Blacksville Bituminous Coal – Tests 616 through 618 Mercury Mass Balance Results

| Run No.      |          |           | 616  |      |           |      |      | 617  |      |           |      |       | 618  |                   |                 |
|--------------|----------|-----------|------|------|-----------|------|------|------|------|-----------|------|-------|------|-------------------|-----------------|
| Total Mercur | y Flow R | ate, µg/ł | nr   |      |           |      |      |      |      |           |      |       |      |                   |                 |
| Sample       | 1        | 2         | 3    | Avg. | Std. Dev. | 1    | 2    | 3    | Avg. | Std. Dev. | 1    | 2     | 3    | Avg.              | Std. Dev.       |
| SCR In       | 1836     | _         | _    | _    | _         | 1589 | 1662 | _    | _    | _         | 1774 | 1687  | _    | 1710 <sup>°</sup> | 97 <sup>*</sup> |
| SCR Out      | -        | _         | _    | _    | -         | _    | _    | _    | _    | -         | 1696 | 1720  | 1720 | 1712              | 14              |
| ESP In       | 1819     | 1727      | 1702 | 1749 | 62        | 1572 | 1454 | 1469 | 1498 | 64        | 1714 | 2011  | 1817 | 1847              | 151             |
| ESP Out      | 1700     | 1561      | 1460 | 1574 | 121       | 1259 | 1073 | 1261 | 1198 | 109       | 1384 | 1419  | 1470 | 1425              | 43              |
| Mercury Mas  | s Balanc | e, %:     |      |      |           |      |      |      |      |           |      |       |      |                   |                 |
| SCR In       | 94.0     | _         | _    | _    | _         | 86.0 | 89.9 | _    | _    | _         | 88.7 | 84.3  | _    | 88.6              | 4.1             |
| SCR Out      | -        | _         | _    | _    | -         | _    | _    | _    | _    | -         | 84.8 | 86.0  | 86.0 | 85.6              | 0.7             |
| ESP In       | 93.2     | 88.5      | 87.2 | 89.6 | 3.2       | 85.1 | 78.7 | 79.5 | 81.1 | 3.5       | 85.7 | 100.6 | 90.8 | 92.4              | 7.5             |
| ESP Out      | 96.1     | 88.9      | 83.8 | 89.6 | 6.2       | 79.2 | 69.1 | 79.3 | 75.8 | 5.9       | 79.7 | 81.4  | 84.0 | 81.7              | 2.2             |

<sup>a</sup>Average and standard deviation of the three runs (616–618).

#### **NH**<sub>3</sub> Mass Balance Data

#### Table C-9 Paradise NH<sub>3</sub>(g,p) Analysis and Mass Balance Results

| Test                      | NH₃(g), ppmv | NH <sub>3</sub> (g), mg/Nm <sup>3</sup> | NH <sub>3</sub> (p), mg/Nm <sup>3</sup> | Mass Balance, % |
|---------------------------|--------------|---|---|-----------------|
| Baseline                  | 6.69         | 5.09                                    | 0.64                                    | NAª             |
| 25 ppm – $NH_3$ Injection | 2.44         | 1.85                                    | 2.66                                    | 18              |
| 25 ppm – $NH_3$ Injection | 2.36         | 1.79                                    | 5.93                                    | 31              |
| 25 ppm – $NH_3$ Injection | 2.69         | 2.04                                    | 5.82                                    | 32              |
| Average                   | 2.50         | 1.89                                    | 4.80                                    | 27              |
| Std. Dev.⁵                | 0.17         | 0.13                                    | 1.86                                    | 8               |
| SCR of NO <sub>x</sub>    | 1.41         | 1.07                                    | 4.25                                    | 83°             |
| SCR of NO <sub>x</sub>    | 0.88         | 0.67                                    | 4.73                                    | 103°            |
| SCR of NO <sub>x</sub>    | 86.4         | 65.7                                    | 29.4                                    | 106°            |
| Average                   | 29.6         | 22.5                                    | 12.8                                    | 97              |
| Std. Dev.                 | 49.2         | 37.4                                    | 14.4                                    | 12              |

<sup>a</sup>Not applicable.

<sup>b</sup> Sample standard deviation calculated from the average of three analyses.
 <sup>c</sup> Calculated assuming that the ratio of converted moles of NO<sub>x</sub> and NH<sub>3</sub> is 1.

| Test                      | NH₃(g), ppmv | NH <sub>3</sub> (g), mg/Nm <sup>3</sup> | NH <sub>3</sub> (p), mg/Nm <sup>3</sup> | Mass Balance, % |  |
|---------------------------|--------------|---|---|-----------------|--|
| Baseline                  | 0.82         | 0.63                                    | 0.12                                    | NAª             |  |
| 25 ppm – $NH_3$ Injection | 13.7         | 10.4                                    | 0.07                                    | 126             |  |
| 25 ppm – $NH_3$ Injection | 12.9         | 9.80                                    | 0.10                                    | 119             |  |
| 25 ppm – $NH_3$ Injection | 14.0         | 10.7                                    | 0.30                                    | 131             |  |
| Average                   | 13.5         | 10.3                                    | 0.16                                    | 125             |  |
| Std. Dev.⁵                | 0.6          | 0.5                                     | 0.13                                    | 6               |  |
| SCR of NO <sub>x</sub>    | 216          | 165                                     | 0.95                                    | 120°            |  |
| SCR of NO <sub>x</sub>    | 119          | 90.4                                    | 0.94                                    | 116°            |  |
| SCR of NO <sub>x</sub>    | 94.7         | 72.0                                    | 1.01                                    | 105°            |  |
| Average                   | 143          | 109                                     | 0.97                                    | 114             |  |
| Std. Dev.                 | 64           | 49                                      | 0.04                                    | 8               |  |

#### Table C-10 Cordero Rojo NH<sub>3</sub>(g,p) Analysis and Mass Balance Results

<sup>a</sup> Not applicable. <sup>b</sup> Sample standard deviation calculated from the average of three analyses. <sup>c</sup> Calculated assuming that the ratio of converted moles of NO<sub>x</sub> and NH<sub>3</sub> is 1.

| Test                      | NH₃(g), ppmv | NH <sub>3</sub> (g), mg/Nm <sup>3</sup> | NH <sub>3</sub> (p), mg/Nm <sup>3</sup> | Mass Balance, % |
|---------------------------|--------------|---|---|-----------------|
| Baseline                  | 0.43         | 0.33                                    | 0.17                                    | NAª             |
| 25 ppm – $NH_3$ Injection | 4.61         | 3.51                                    | 2.35                                    | 72              |
| 25 ppm – $NH_3$ Injection | 4.21         | 3.20                                    | 2.97                                    | 76              |
| 25 ppm – $NH_3$ Injection | 5.19         | 3.95                                    | 2.82                                    | 84              |
| Average                   | 4.67         | 3.55                                    | 2.71                                    | 77              |
| Std. Dev.⁵                | 0.49         | 0.38                                    | 0.32                                    | 6               |
| SCR of NO <sub>x</sub>    | 262          | 199                                     | 4.47                                    | 129°            |
| SCR of NO <sub>x</sub>    | 173          | 132                                     | 4.03                                    | 118°            |
| SCR of NO <sub>x</sub>    | 132          | 101                                     | 3.96                                    | 114°            |
| Average                   | 189          | 144                                     | 4.15                                    | 121             |
| Std. Dev.                 | 66           | 50                                      | 0.28                                    | 8               |

#### Table C-11 Band Mill NH<sub>3</sub>(g, p) Analysis and Mass Balance Results

<sup>a</sup>Not applicable. <sup>b</sup> Sample standard deviation calculated from the average of three analyses. <sup>c</sup> Calculated assuming that the ratio of converted moles of NO<sub>x</sub> and NH<sub>3</sub> is 1.

| Table C-12   |
|--|
| Blacksville NH <sub>3</sub> (g, p) Analysis and Mass Balance Results |

| Test                      | NH₃(g), ppmv | NH <sub>3</sub> (g), mg/Nm <sup>3</sup> | NH <sub>3</sub> (p), mg/Nm <sup>3</sup> | Mass Balance, % |
|---------------------------|--------------|---|---|-----------------|
| Baseline                  | 2.18         | 1.65                                    | 0.26                                    | NAª             |
| 25 ppm – $NH_3$ Injection | 0.85         | 0.65                                    | 2.66                                    | 35              |
| 25 ppm – $NH_3$ Injection | 0.53         | 0.40                                    | 2.55                                    | 31              |
| 25 ppm – $NH_3$ Injection | 0.55         | 0.42                                    | 2.62                                    | 32              |
| Average                   | 0.64         | 0.49                                    | 2.61                                    | 32              |
| Std. Dev. <sup>b</sup>    | 0.18         | 0.14                                    | 0.06                                    | 2               |
| SCR of NO <sub>x</sub>    | 0.60         | 0.45                                    | 1.52                                    | 98°             |
| SCR of NO <sub>x</sub>    | 0.26         | 0.20                                    | 1.44                                    | 96°             |
| SCR of NO <sub>x</sub>    | 0.35         | 0.27                                    | 1.88                                    | 100°            |
| Average                   | 0.40         | 0.31                                    | 1.61                                    | 98              |
| Std. Dev.                 | 0.18         | 0.13                                    | 0.23                                    | 2               |

<sup>a</sup>Not applicable. <sup>b</sup> Sample standard deviation calculated from the average of three analyses. <sup>c</sup> Calculated assuming that the ratio of converted moles of NO<sub>x</sub> and NH<sub>3</sub> is 1.

## **D** LINEAR REGRESSION ANALYSIS FOR THE PILOT-SCALE SCREENING TESTS EVALUATING THE IMPACT OF SCR ON MERCURY SPECIATION

#### **Linear Regression**

Appendix D presents linear regression equations for mercury speciation in reference to the chemical composition of the four test coals (Hg, S, Cl, and Ca concentrations in parts per million on a moisture-free basis) and operating conditions (NH<sub>3</sub> and SCR are assigned a value of 1 when these operations were used and a value of 0 when they were not). These equations respectively deal with 1) mercury speciation leaving the furnace and entering the SCR, 2) changes in mercury speciation across the SCR, 3) changes in speciation across the cooling loop, and 4) the percentages of coal mercury emitted as different species at the exit of the ESP. All speciation predictions are expressed as percent of coal mercury. The statistical parameters included in these equations include 1) a value of  $R^2$  for a specified number of data points (N), 2) the positive or negative "x coefficient" which indicates proportional dependence on the independent regression variable, and 3) the probability (P) that the x coefficient is significantly different from zero. The only independent variables presented are those with the highest statistical significance for a given set of data points. Some variables, particularly where N is small, still have what would be considered to be a low statistical significance as indicated by their P values, where a P value of 0.95 is often used to identify a statistically significant variable. For most of the regression data sets, N has a value of 12 (4 coals  $\times$  3 test conditions). The regression data sets for the Hg<sup>0</sup> and Hg<sup>2+</sup> species leaving the furnace and entering the SCR are a special case and have an N of only 10 because the three measured values of these species for Band Mill coal were averaged to eliminate a wide divergence at essentially the same furnace condition. N has a value of 4 for those data sets that represent SCR operation. Because of low values of N and scatter in the data, these regression equations should not be interpreted as reliable predictors of speciation but only as general indications of trends. Also, it should be noted that several factors concerned with the overall data set limit the validity of the regressions for full-scale plants. These factors include possible differences in mercury speciation as a function of the much smaller size of the pilot-scale combustor, the limited number and range of coal types, and differences in ammonia slip concentrations. These are discussed in the recommendation section of this report. Appendix D – Linear Regression Analysis for the Pilot-Scale Screening Tests Evaluating the Impact of SCR on Mercury Speciation

## D-1 Regression Equations for Mercury Speciation Leaving the Furnace and Entering the SCR

#### **Elemental Mercury**

 $N = 10, R^2 = 0.95$ 

%  $X^0$  (percent of Hg in coal) = 39.0 + 0.00211 Ca - 0.0391 Cl P = 0.99 P = 0.99

#### **Oxidized Mercury**

 $N=10, R^2=0.94$ 

%  $X^{2+}$  (percent of Hg in coal) = 109 - 0.00471 Ca - 0.00205 S + 0.0190 Cl P = 0.99 P = 0.99 P = 0.88

#### Particulate Mercury

 $N = 10, R^2 = 0.58$ 

%  $X_p$  (percent of Hg in coal) = 1.8 + 0.0000701 Ca + 0.00361 Cl - 21.67 Hg - 1.12 SCR P = 0.64 P = 0.96 P = 0.88 P = 0.86

#### D-2 Regression Equations for Changes in Mercury Species Across the SCR

#### **Total Mercury**

 $N = 4, R^2 = 0.9993$ 

Change in Hg<sub>total</sub> (percent of Hg in coal) = -78.5 + 484 Hg + 174 Cl/Ca P = 0.98 P = 0.97

#### **Elemental Mercury**

 $N = 4, R^2 = 0.9997$ 

Change in Hg<sup>0</sup> (percent of Hg in coal) = 54.7 - 594 Hg - 0.00648 Cl P = 0.99 P = 0.86

#### **Oxidized Mercury**

 $N = 4, R^2 = 0.9992$ 

Change in Hg<sup>2+</sup> (percent of Hg in coal) = -131 + 1063 Hg + 178 Cl/Ca P = 0.98 P = 0.95 Appendix D – Linear Regression Analysis for the Pilot-Scale Screening Tests Evaluating the Impact of SCR on Mercury Speciation

## D-3 Regression Equations for Changes in Mercury Species Across the Cooling Loop, Including When the SCR Is in Operation

#### **Elemental Mercury**

 $N = 12, R^2 = 0.37$ 

Change in Hg<sup>0</sup> (percent of Hg in coal) = -46.2 + 0.0340 Cl + 186 Hg - 0.000210 S P = 0.79 P = 0.66 P = 0.2\*

#### **Oxidized Mercury**

 $N = 12, R^2 = 0.32$ 

Change in Hg<sup>2+</sup> (percent of Hg in coal) = -32.6 + 623 Hg + 219 Cl/Ca - 0.00326 S P = 0.84 P = 0.56 P = 0.66

#### Particulate Mercury

 $N = 12, R^2 = 0.58$ 

Change in Hg<sub>p</sub> (percent of Hg in coal) = 31.5 + 21.2 NH<sub>3</sub> + 14.7 SCR - 0.0253 Cl - 178 Hg P = 0.81 P = 0.65 P = 0.72 P = 0.67

\*S was included because of a value of P = 0.78 for S in a regression on it alone.

## D-4 Regression Equations for Mercury Species Emitted at the Exit of the ESP

#### **Total Mercury**

 $N = 12, R^2 = 0.47$ 

Total Hg Emitted (percent of Hg in coal) =  $68.6 + 0.0195 \text{ Cl} - 25.7 \text{ NH}_3 - 2.65 \text{ SCR}$ P = 0.68 P = 0.92 P = 0.2\*

#### **Elemental Mercury**

 $N = 12, R^2 = 0.84$ 

Hg<sup>0</sup> Emitted (percent of Hg in coal) = 21.0 + 0.00143 Ca - 11.6 SCR - 0.000391 S - 0.00994 Cl P = 0.99 P = 0.94 P = 0.75 P = 0.62

#### **Oxidized Mercury**

 $N = 12, R^2 = 0.60$ 

Hg<sup>2+</sup> Emitted (percent of Hg in coal) = 51.0 + 0.0395 Cl - 38.0 NH<sub>3</sub> - 0.000771 Ca P = 0.56 P = 0.97 P = 0.86

#### Particulate Mercury

 $N = 12, R^2 = 0.74$ 

 $Hg_p$  Emitted (percent of Hg in coal) =

 $\begin{array}{c} -1.8 + \ 0.000889 \ S + 7.7 \ NH_3 + 6.55 \ SCR - 0.0262 \ Cl - 0.000467 \ Ca \\ P = 0.96 \ p = 0.73 \ P = 0.66 \ P = 0.94 \ P = 0.66 \end{array}$ 

\* SCR was included because of a value of P = 0.74 in a regression on it alone.

Appendix D – Linear Regression Analysis for the Pilot-Scale Screening Tests Evaluating the Impact of SCR on Mercury Speciation