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Abstract

This quarterly report documents significant achievements in the Enhanced Practical Photosynthetic CO₂ Mitigation project during the period from 4/03/2001 through 7/02/2001. Most of the achievements are milestones in our efforts to complete the tasks and subtasks that constitute the project objectives. Note that this version of the quarterly technical report is a revision to add the reports from subcontractors Montana State and Oak Ridge National Laboratories

The significant accomplishments for this quarter include:

- Development of an experimental plan and initiation of experiments to create a calibration curve that correlates algal chlorophyll levels with carbon levels (to simplify future experimental procedures)
- Completion of debugging of the slug flow reactor system, and development of a plan for testing the pressure drop of the slug flow reactor
- Design and development of a new bioreactor screen design which integrates the nutrient delivery drip system and the harvesting system
- Development of an experimental setup for testing the new integrated drip system / harvesting system
- Completion of model-scale bioreactor tests examining the effects of CO₂ concentration levels and lighting levels on Nostoc 86-3 growth rates
- Completion of the construction of a larger model-scale bioreactor to improve and expand testing capabilities and initiation of tests
- Substantial progress on construction of a pilot-scale bioreactor
- Preliminary economic analysis of photobioreactor deployment

Plans for next quarter's work are included in the conclusions. A preliminary economic analysis is included as an appendix.

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Results and Discussion

Task 1.0. Evaluate and rank component and subsystem level alternative design concepts

Subtask 1.1 Investigate critical properties of alternative photosynthetic agents (cyanobacteria)

Subtask 1.1.1 Quantify agent growth rate characteristics in controlled experiments as a function of temperature, bicarbonate concentration, moisture content, and nutrient level.

Ohio University

Efforts on this subtask continue both at Ohio University and at Montana State. Ohio University researchers are currently focused on developing improved procedures for quantifying organism growth rates on a large scale (for example in the bioreactor) by correlating algal chlorophyll levels with carbon levels. If successful, we only have to perform chlorophyll A measurements in the future rather than a more complicated, involved method for determining primary productivity. The experimental procedure that will be followed is included below. Step 1 (testing screens for heterogeneity) is currently underway. It is expected that actual test runs will begin the week of July 16th. The Primary Productivity Protocol (PPP) is described here

1. First, we must determine any heterogeneity of algal application within and among screens
 - If there exists a zonation within the screens (i.e., more algae on the top than the bottom or vice versa), document that variation
 - With no vertical heterogeneity, horizontal patterns do not matter
 - Using any zonation patterns, set up 4, 2x2 inch squares across the filters (see below)
 - Employ three replicates up and down

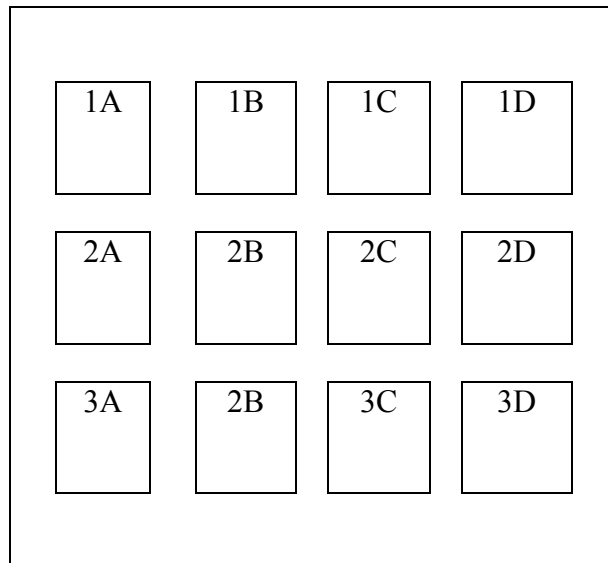


Figure 1. Schematic of the screen sectors

2. After a full test run (3 days), cut out all pre-selected areas
 - samples A and C will be subjected to acetone extraction (see below)
 - samples B and D will be subjected to carbon-analysis
3. Afterwards, correlation statistics will be performed

Carbon-analysis

1. Ten non-inoculated, 2x2 inch squares will be placed in the carbon-analyzer to serve as blanks and determine variability within and between filters
2. Samples B and D from multiple filters (10 filters, for 60 total samples) will be dried at 50°C overnight and subjected to carbon analysis

Chlorophyll extraction

1. Soak each 2x2 filter piece in a cleaned test tube with 90% Mg-acetone solution
 - continue for 24 h, with occasional agitation
2. Remove the filter, and measure the final volume of acetone
3. Filter the acetone mixture onto a GF/C filter
4. Place disks in aluminum foil, and freeze for later use
5. Send samples to BSA Environmental services for chlorophyll a analysis

From Montana State University

Laboratory investigations. Since Yellowstone National Park was not open for foot travel until early June 2001 [snow, bear activity], we have been working with cultures provided by the University of Oregon Culture Collection [UOCC]. We found that none of those we obtained were axenic or even unialgal, but all grew at temperatures above 45°C and thus were potentially of use in the CO₂ Remediation Facility (CRF). We have begun experiments to isolate axenic clones of these organisms. In addition we have determined conditions for optimal growth of several of these mixed cultures. In general, the cultures respond positively to additions of sodium bicarbonate, but as growth continues, this caused alkalization of the medium and cell death. It is essential that the medium pH is controlled at below pH 9. Growth was measured as absorbance at 680nm and/or as chlorophyll a content of a sample. The results obtained using these distinct measures of biomass were not different. The most promising cyanobacterial cultures from this work were *Synechococcus* C-1 and K-Bogoria. These are culture collection designated names for identification purposes only. No attempt to obtain 16-S derived nomenclature has been made so far. Note that K-Bogoria is actually a consortium of cyanobacteria.

Although the CO₂ remediation bioreactor will house solid supports for the growth of the cyanobacterial isolates, inocula for the initial colonization of these supports will be produced in liquid cultures. To allow this and to investigate growth properties in liquid cultures, we have designed and have operating a multi tubular bioreactor in which light, temperature and CO₂ supply can be controlled. There is provision for 12 replicate reactors each with a working volume of 50-100mL. (Figure 2) This apparatus will be used to quantify characteristics of organisms isolated from Yellowstone National Park and its environs. It has already been used to show that growth of *Synechococcus* C-1 becomes photo saturated at 75 $\mu\text{moles}\cdot\text{m}^{-2}\cdot\text{sec}^{-1}$. The doubling time for this organism in the presence of 5% CO₂ in air and 5mM NaHCO₃ was 17 hr. Growth

responses between tubes was excellent providing the bubbling rate was constant. No organism we have been working with grows well in the absence of fixed nitrogen in the form of nitrate.

Yellowstone National Park (YNP) and other thermal areas visited. Using a GIS data base belonging to YNP, we have identified sites within the Park where there are cyanobacteria growing at pH levels from pH 7-9.5 and at temperatures from 45-65°C. So far one of these has been visited and samples taken. These were placed in various cyanobacterial media [BG-11, Medium D and medium DH]. Microscopic assessment of the enrichments indicate that a major component of these cultures are species of *Synechococcus*. If these prove sensitive to the presence of the Scotchbrite polymer, it will be necessary to isolate minor components of the mixture. In order to overcome this potential problem we are trying to select only those organisms from the environment that will grow on Scotchbrite from the outset. To do this we have deployed anchored Scotchbrite coupons in thermal areas with the idea that only Scotchbrite -resistant organisms will colonize them.

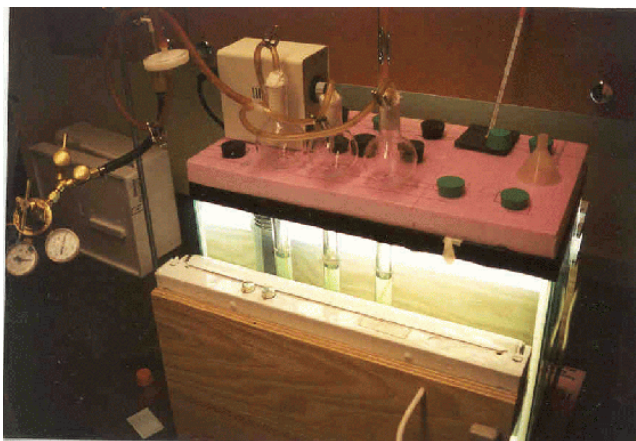
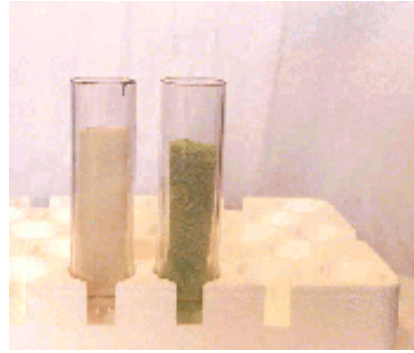


Figure 2. 12-place tubular bioreactor for cyanobacterial growth studies

Sub-task 1.1.2 Quantify adhesion characteristics

All of the above experiments have been made with organisms in liquid culture. Since the CRF will utilize a solid support for the cyanobacterial cells, we have investigated the ability of two organisms selected on the basis of their growth physiology to attach to a solid surface and form a biofilm. We used a glass surface so that quantification could be made easily by measuring surface-associated chlorophyll *a*. *Synechococcus* C-1 did not attach in three hours, but *K-Borgoria* reached a saturation point in two hours. This augurs well for the use of *K-Borgoria* in the CRF. Organisms were also offered the opportunity to attach to the surface which at the moment is a candidate for use in the CRF, i.e., the 3-M Company, Scotchbrite. This polymer, which is a nylon matrix with embedded aluminum oxide, proved toxic to two *synechococcal* species. Cell death occurred within a few days. On the other hand *K-Borgoria* grew well on Scotchbrite (Figures 3 and 4). From our relative small sample, it appears essential that an early test in assessing the usefulness of an organism in the CRF is its compatibility with the substratum to which it will be attached. The toxicity of this polymer to a cyanobacteria was not expected. We have cryo-preserved all *Synechococcal* species in case other less toxic substrata are proposed for use in the CR in the future.



(a). Scotchbrite colonized with cyanobacteria (b). After centrifugation

Figures 3(a) and (b) show the ability to colonize and the tenacity of K-Borgoria for Scotchbrite.

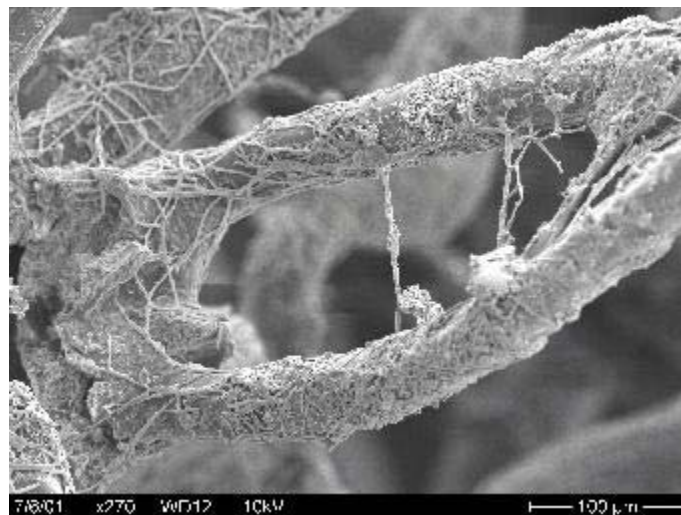


Figure 4. Scanning electron microscope image (gold shadowed) of K-Borgoria on Scotchbrite. *(The fibers of the Scotchbrite are colonized with cyanobacterial cells. Magnification is 250X)*

Subtask 1.2 Design deep-penetration light delivery subsystem

Work continued on the lighting system development task. ORNL began testing several solar concentrator primary mirror prototypes and two associated tracking systems. Primary mirrors being tested included a modified satellite dish with an adhesive-backed reflective film and a ground and polished glass mirror with a deposition-based enhanced aluminum coating. The surface quality of the glass mirror was found to be superior. The two tracking systems under evaluation include a sun-sensor (SS) system and a microprocessor-controlled system. The tracking accuracy of the SS tracker was found to be inadequate for our application while the microprocessor-based system has yet to be fully evaluated.

ORNL also fabricated a second light distribution sheet for use in the photobioreactor. The design used 3M's side-emitting optical fiber wrapped in a progressively smaller oval pattern such that the bend radius of the fiber continually decreased and the fibers became closer to one another towards the center. The unit is still under test in ORNL illumination test cell. A third design approach that reduces the amount of optical fiber and uses cylindrical fresnel lens to evenly distribute light from a center-mounted side-illuminator is also under development.

Studies were also conducted to more fully characterize the side-emitting capabilities and transmission loss of optical fibers as a function of bend radius. These tests included the use of a Cogent light source (used as a simulated sunlight source), a Prometric CCD camera (to evaluate side-illumination resulting from bends) and a large integrating sphere (to record transmission losses).

Work also continued on the evaluation of the light-carrying capacity of large-core optical fibers. This was done using a fresnel lens mounted on a two-axis solar tracker that collected sunlight and focused it onto a large-core optical fiber. The temperature of the fiber end-face was monitored using a thermocouple as the amount of collected sunlight was progressively increased. Initial results of these tests are encouraging although the data has yet to be completely analyzed.

Subtask 1.4 Investigate the use of a hydraulic jump to improve the system's overall CO₂ conversion efficiency

The debugging work for the slug flow reactor has been finished, which includes checking the wiring of the transducers and flow meters and calibrating the pipeline pressure transducer, the differential pressure transducer and the orifice plate flow meter. Tests will begin as soon as test rig maintenance repairs are completed.

Considering the importance of pressure drop across the reactor, our first tests will focus on quantifying the pressure drop of the slug flow reactor and investigating how the gas and liquid velocities affect the pressure drop. The results of the pressure drop experiments will be used to optimize the gas and liquid velocities and understand the basic pressure drop of the slug flow reactor.

Once the pressure drop is understood we will begin the CO₂ solubility experiments, by which we will obtain CO₂ solubility as a function of operating conditions such as slug frequency, CO₂ concentration additive, and pH. An operating condition that maximizes CO₂ solubility will be identified by these experiments.

The first additive that will be added to the water in order to improve the CO₂ solubility is sodium hydroxide. Titration will be applied to detect the concentration of OH⁻, HCO₃⁻ and CO₃²⁻. A carbon analyzer will be used to examine the total carbon content in the solution.

Subtask 1.5 Design harvesting subsystem

Results from preliminary tests of water jet harvesting systems have shown that sufficient cleaning can be obtained at relatively low flow velocities and shallow incidence angles. This information has caused us to shift our focus from nozzle-based water jet harvesting methods which spray water on the growth surfaces to differential pressure water supply systems that function as both nutrient delivery drip systems (at low delivery pressures) and algae harvesting systems (at high delivery pressures). The integrated system requires a special bioreactor screen design (shown in Figure 5) which delivers moisture to the screen via capillary action under normal operation, but which creates a high flow “sheeting action” of fluid which displaces a percentage of the algae clinging to the surface when the fluid delivery pressure is increased. The experimental setup constructed to allow testing of this new design is shown in Figure 6.

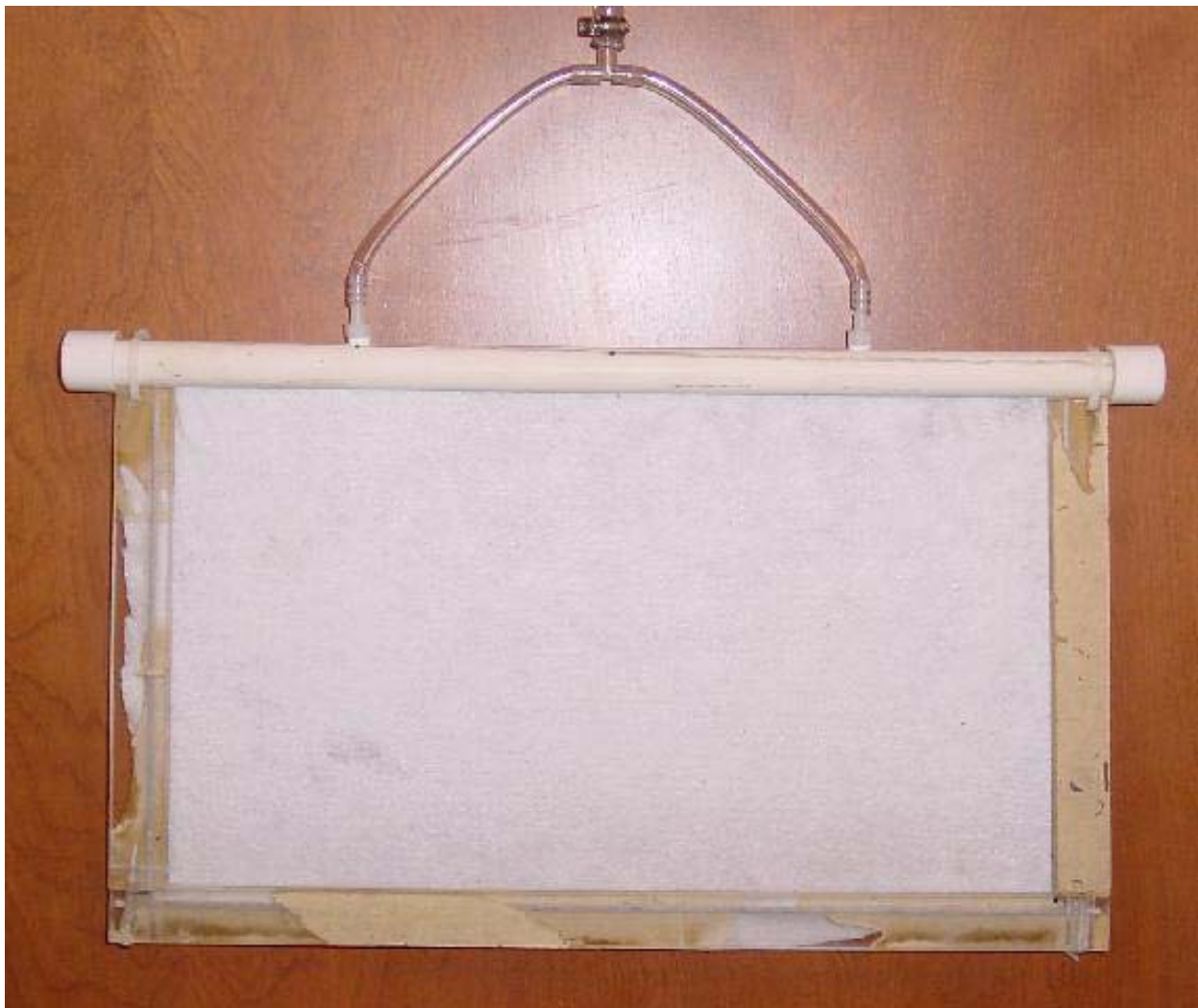


Figure 5a. Bioreactor screen with combined nutrient delivery drip system and harvesting system

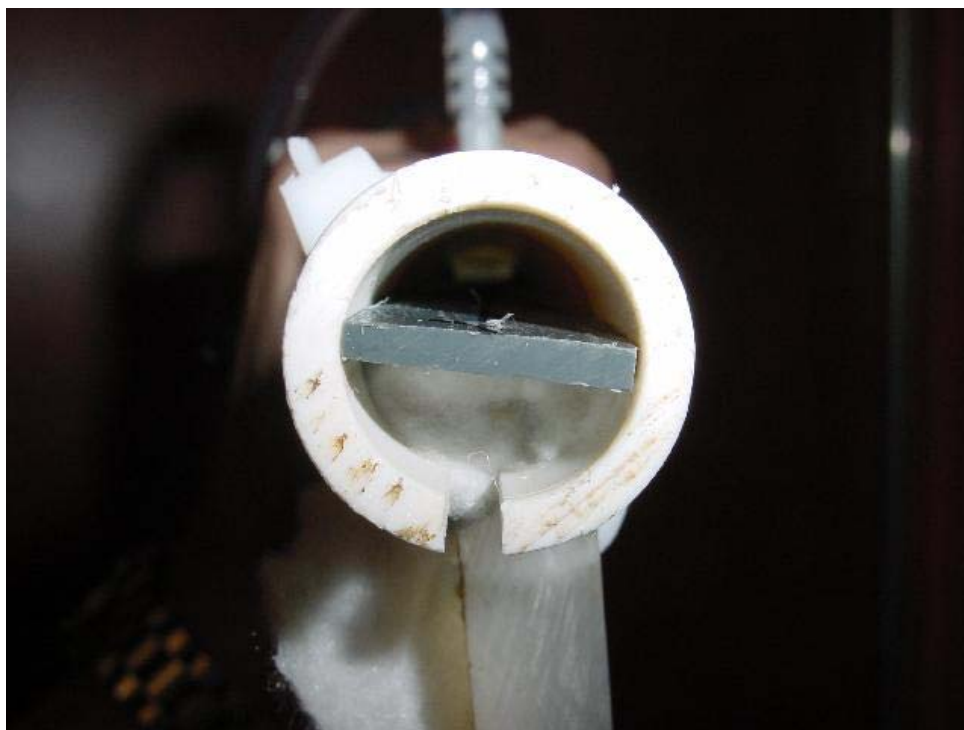


Figure 5b. Side view of header pipe and separation plate. Small holes in the plate separate the pressurized area above from the fabric bundle and slot opening below to create the desired capillary action.



Figure 6. Harvesting system experimental test facility

Subtask 1.5.1 Examine harvesting methods for efficiency of biomass removal

An experimental test plan is being developed for the new harvesting system design to quantify cleaning efficiency and system sensitivity to the control parameters. Recall that the goal of the harvesting system is to provide partial removal of the organisms in the cleaned area of the growth surface since total removal causes a lag in growth and CO₂ uptake. Initial experiments will quantify mass percentage of algae removed as a function of supply pressure, harvesting time, etc. for a Scotch Brite growth surface fabric and Nostoc algae.

The original CRF is now available for operation as a test bed for continual harvesting system experiments. The current CRF “processing chamber” is being modified to allow extra space for the water supply pipes necessary in the new bioreactor screen design. Tests in this facility are on hold until more information is known about the performance of the new harvesting system design. Plans are to install an "optimized" version of the new combined drip/harvesting system once sufficient off-line tests have been completed.

Subtask 1.6 Quantify properties (higher heating value, elemental composition, volatile content) of dried biomass for potential end-uses.

No experimental work has been completed in this area, as current experiments are focused on identifying organisms with maximum rates of CO₂ uptake in the conditions of the bioreactor.

Task 2.0. Evaluate subsystem combinations and select an “optimum” system design

Model-scale bioreactor tests in the original Carbon Recycling Facility (CRF-1) have been underway throughout the project period in an effort to develop proper experimental procedures and to accumulate system-level experience in dealing with bioreactor systems. The organisms, growth surfaces, nutrient delivery systems, etc. currently being tested have not been optimized because the subsystem level experiments are still in process. However, tests to quantify gains in algae mass as a function of light intensity levels and CO₂ levels have been completed for Nostoc 86-3 cyanobacteria. Results from many of these experiments have been included in previous reports, and results from two recent light intensity test runs are summarized at the end of this section.

Two new system level experimental facilities are currently under construction, a new model-scale bioreactor and a pilot scale bioreactor. The pilot scale system is discussed in the Task 3.0 section of this report. The new model-scale bioreactor (CRF-2) is 4 times larger than CRF-1 in terms of growth surface area. Construction of CRF-2 is complete and debugging of the system is underway. Air line stability appears to be affecting the burner, so a surge volume (tank) is being added to damp out air pressure fluctuations. Also, work continues on improving the new bioreactor screen design (discussed above in the harvesting section). A new organism (cyanidium) will be tested in this bioreactor.

Summary of CRF-1 Test Run 4/4-9/01

The test specimen for *Test Run 4.4-9.01* was the cyanobacteria, Nostoc 86-3. The target values for the gas concentrations were 3%, 10% and less than 50 parts per million for oxygen, carbon dioxide, and carbon monoxide, respectively, with a temperature range between 120°F-125°F. The gas concentration averages for the 120 hours were 3.6%, 10.1%, and 44.7 ppm for oxygen, carbon dioxide, and carbon monoxide, respectively. The 120-hour temperature average was 120.0°F.

The lighting was not altered from *Summary of Light Intensity Test for Test Run 4.4-9.01* and was cycled 12-hours on, and 12-hours off. The intensity averages for the four membranes were 68.6 $\mu\text{mols/s}\cdot\text{m}^2$ for membrane-1, 72.3 $\mu\text{mols/s}\cdot\text{m}^2$ for membrane-2, 72.9 $\mu\text{mols/s}\cdot\text{m}^2$ for membrane-3, and 84.4 $\mu\text{mols/s}\cdot\text{m}^2$ for membrane-4

Test Run 4.4-9.01 had a total dry algae mass gain of 1.38 grams, or a 44.4% increase over the initial estimated dry mass. The following table describes each membrane and final test results. More details are provided in Table 1.

Table 1. Data Sheet Test Run 4.4-9.01.

Membrane Number	1	2	3	4
Membrane Initial Dry Mass (no loading) (g)	21.90	18.05	17.08	17.49
Membrane and Algae Final Dry Mass (g)	22.73	18.89	18.54	18.58
Final Dry Mass of Algae (g)	0.83	0.83	1.46	1.09
Membrane Loading Estimated Dry Mass (g)	0.70	0.76	0.82	0.85
Mass Gain for Each Membrane (g):	0.13	0.08	0.65	0.24
Percent Mass Gain for Each Membrane	18.51%	9.97%	79.40%	28.27%
Mass Gain From Filter (g)	0.07			
Mass Gain from Beaker (g)	0.23			
Total Estimated Initial Dry Mass (g)	3.12			
Total Mass Gain (g)	1.39			
Total Percent Mass Gain	44.43%			

Uncertainty Analysis

The uncertainty analysis is based on the results from the *Algae Dry Mass Determination Test* and the final results of *Test Run 4.4-9.01*. The average percent dry mass of the initial twelve samples was 4.46% with a standard deviation of 0.19%. The same technique used to gather the twelve initial samples was used to load the membrane. An algae sample taken from the bulk tank was poured across a wire mesh to remove most of the water content, but still retaining the algae mass. The sample remained on the wire mesh for 9-minutes to further reduce water content. The remaining sample was scooped into a beaker and weighed. The algae sample in the beaker was then applied to the membrane and the beaker was weighed again to determine the algae loading weight. This was repeated for each membrane. 4.4581% of the total loading wet weight was used as the initial estimated dry mass for each membrane.

The following sample calculation is the uncertainty at 90% confidence in the estimated initial dry mass for membrane-4. It is based on the 12-samples taken from *Algae Dry Mass Determination Test*, using Student's t-distribution and using four weighed samples to load each membrane.

Data from *Algae Dry Mass Determination Test, Test Run 4.4-9.01* and Student's t-distribution:

$$\text{Mean} = 4.4581\%$$

$$\text{Std. Dev} = 0.1933\%$$

$$\text{Degree's of freedom} = 11 \text{ (based on Student's t-distribution for 12 samples)}$$

$$t_{90} = 1.796 \text{ (Student's t-distribution for 12 samples)}$$

$$\text{Uncertainty} = \frac{t \times \sigma}{\sqrt{n}}$$

$$t = \text{Student's t-distribution for 12 samples at 90\% confidence}$$

$$\sigma = \text{Standard deviation of the 12 samples}$$

$$n = \text{Number of samples applied to membrane-4}$$

$$\text{Uncertainty}_{90} = \frac{1.796 \times 0.1933\%}{\sqrt{4}} = 0.1735\%$$

$$\text{Algae wet weight applied to Membrane-4} = 19.0884 \text{ grams}$$

$$\text{Uncertainty of estimated dry weight} = 19.0884 \times 0.001735 = \pm 0.0331 \text{ grams}$$

$$\text{Estimated initial dry weight} = 19.0884 \times 0.044581 = 0.8510 \pm 0.0331 \text{ grams}$$

$$\text{Mass gain for Membrane-4} = \text{Membrane final dry weight} - \text{initial dry weight} = 0.2406 \text{ g}$$

$$\text{Uncertainty}_{90} = \frac{0.0331 \text{ g}}{0.2406 \text{ g}} \times 100 = 13.8\% \text{ (uncertainty of mass gain at 90\% confidence)}$$

Table 2. Uncertainty of the mass gain for each membrane

Uncertainty of Mass Gain	Membrane-1	Membrane-2	Membrane-3	Membrane-4
<i>At 90% Confidence</i>	21.04%	39.04%	4.90%	13.77%
At 95% Confidence	25.78%	47.84%	6.01%	16.87%
At 99% Confidence	36.37%	67.50%	8.48%	23.81%

The second uncertainty analysis is on a total mass gain basis for the four membranes, instead of the mass gain for each membrane. The benefit of this uncertainty analysis is that the four membranes are looked at as four samples for the total mass gain, which will increase the number of samples in the uncertainty equation. All other values remain the same as in the above calculation.

$$\text{Uncertainty}_{90} = \frac{1.796 \times 0.1933\%}{\sqrt{4}} = 0.1736\%$$

Total wet weight applied to membranes = 69.9995 grams

Uncertainty of total estimated dry weight = $69.9995 \times 0.001736 = \pm 0.1215$ grams

Estimated initial dry weight = $69.9995 \times 0.044581 = 3.1206 \pm 0.1215$ grams

Total algae mass gain (from membranes) for test run = 1.0928 grams

$$\text{Uncertainty}_{90} = \frac{0.1215\text{g}}{1.0928\text{g}} \times 100 = 11.1\% \text{ (uncertainty of mass gain at 90\% confidence)}$$

Table 3. Uncertainty values on a total mass basis for the four membranes combined.

Uncertainty of Total Mass Gain	
At 90% Confidence	11.1%
At 95% Confidence	13.6%
At 99% Confidence	19.2%

The results conclude with 90% certainty that the mass gain of *Test Run 04.4-9.01* was 1.3864 ± 0.1539 grams, i.e. the mass gain was between 1.2325 grams and 1.5403 grams.

The total uncertainty associated with the scale (used for mass measurements) is estimated as a root-sum-square of the repeatability uncertainty, the resolution uncertainty, and the calibration uncertainty. The following calculation is the uncertainty at 95% confidence.

$$\text{Uncertainty}_{95} = \sqrt{(2 \times 0.00015\text{g})^2 + (0.0001\text{g}/2)^2 + (0.0002\text{g})^2} = \pm 0.00036\text{g}$$

This would be the uncertainty for a single measurement made with this device. Since the uncertainty associated with the scale is so small, with respect to the uncertainties calculated for the mass gains, the uncertainty in the scale is neglected.

Summary of Test Run 4/19-24/01

The test specimen for *Test Run 4.19-24.01* was the cyanobacteria, *Nostoc 86-3*. The target values for the gas concentrations were 3%, 10% and less than 50 parts per million for oxygen, carbon dioxide, and carbon monoxide, respectively, with a temperature range between 120°F-125°F. The gas concentration averages for the 120 hours were 3.6%, 10.1%, and 44.3 ppm for oxygen, carbon dioxide, and carbon monoxide, respectively. The 120-hr temperature average was 120°F.

The lighting was not altered from *Summary of Light Intensity Test for Test Run 4.19-24.01* and was cycled 12-hours on, and 12-hours off. The intensity averages for the four membranes were 38.9 $\mu\text{mol/s}\cdot\text{m}^2$ for membrane-1, 51.5 $\mu\text{mol/s}\cdot\text{m}^2$ for membrane-2, 51.7 $\mu\text{mol/s}\cdot\text{m}^2$ for membrane-3, and 55.4 $\mu\text{mol/s}\cdot\text{m}^2$ for membrane-4

Test Run 4.19-24.01 had a total dry algae mass gain of 0.3827 grams, or a 14.5% increase over the initial estimated dry mass. The following table describes each membrane and final test results. More details are provided in Table 4.

Table 4. Data Sheet Test Run 4.19-24.01.

Membrane Number	1	2	3	4
Membrane Initial Dry Mass (no loading) (g)	18.93	24.84	20.75	24.92
Membrane and Algae Final Dry Mass (g)	19.61	25.46	21.46	25.65
Final Dry Mass of Algae (g)	0.67	0.62	0.72	0.73
Membrane Loading Estimated Dry Mass (g)	0.66	0.65	0.68	0.65
Mass Gain for Each Membrane (g):	0.01	-0.02	0.03	0.08
Percent Mass Gain for Each Membrane	2.13	-3.65	5.00	12.14
Mass Gain From Filter (g)	0.10			
Mass Gain from Beaker (g)	0.18			
Total Estimated Initial Dry Mass (g)	2.64			
Total Mass Gain (g)	0.38			
Total Percent Mass Gain	14.52			

Table 5. Uncertainty of Mass Gain for each membrane

Uncertainty of Mass Gain	Membrane-1	Membrane-2	Membrane-3	Membrane-4
At 90% Confidence	183.2%	-106.8%	77.8%	32.1%
At 95% Confidence	224.4%	-130.8%	95.4%	39.3%
At 99% Confidence	316.6%	-184.5%	134.5%	55.5%

Table 6. Uncertainty values on a total mass basis for the four membranes combined.

Uncertainty of Total Mass Gain	
At 90% Confidence	99.5%
At 95% Confidence	121.9%
At 99% Confidence	172.0%

The results conclude with 90% certainty that the mass gain of *Test Run 04.19-24.01* was 0.3827 \pm 0.3808 grams, i.e. the mass gain was between 0.0019 grams and 0.7635 grams.

Task 3.0. Implement the optimum system in scaled model

The pilot scale bioreactor test facility is under construction at the Ohio University Corrosion Center. Ohio University technician Shyler Switzer is leading the construction effort and is working closely with representatives of Oak Ridge National Laboratories to ensure proper placement of the solar collectors. The current status of the pilot scale bioreactor construction is detailed below.

Group Accomplishments:

- (a) Met with Tonya McFadden (Oak Ridge Intern) on 5-17-01 and brought her up to speed on the bioreactor projects.
- (b) Updated a map of the Corrosion Center including the existing McBee stack, true north, and the proposed bioreactor site and emailed it to Tonya on 6-4-01 for use with their sunlight simulation program.
- (c) Pictures of the proposed bioreactor site taken and emailed to Tonya on 7-5-01 to aid in the generation of the sunlight program.
- (d) Met with Al Schubert from the Corrosion Center to finalize acceptance for the location of the bioreactor outside the building.
- (e) Manufactured eight frames utilizing the new integrated wicking/harvesting system.
- (f) Modified the harvesting test chamber on 6-27-01 for trial of the new integrated wicking/harvesting frame system.
- (g) In the process of investigating alternate suppliers for a prefabricated shelter to house the bioreactor when moved to the Corrosion Center.

Tasks to Complete:

- (h) Complete drawings of the Corrosion Center building addition by 7-13-01.
- (i) Review final drawings with Al Schubert by 7-18-01 and break ground.
- (j) Dismantle the bioreactor for relocation to the Corrosion Center.

Webpage

The web page is running at <http://132.235.19.45/DOE>. All parties involved in the project have received e-mail instructions and the password to access the information.

Conclusions

The activities and accomplishments detailed throughout this report indicate significant progress towards completion of project objectives. Since we have just completed the third quarter of a multi-year project, most of the test results are still preliminary and the majority of the activities underway are focused primarily on development and improvement of test facilities and procedures. Some of the most significant accomplishments this quarter include:

- Development of an experimental plan and initiation of experiments to create a calibration curve that correlates algal chlorophyll levels with carbon levels (to simplify future experimental procedures)
- Completion of debugging of the slug flow reactor system, and development of a plan for testing the pressure drop of the slug flow reactor

- Design and development of a new bioreactor screen design which integrates the nutrient delivery drip system and the harvesting system
- Development of an experimental setup for testing the new integrated drip system / harvesting system
- Completion of model-scale bioreactor tests examining the effects of CO₂ concentration levels and lighting levels on Nostoc 86-3 growth rates
- Completion of the construction of a larger model-scale bioreactor to improve and expand testing capabilities and initiation of tests
- Substantial progress on construction of a pilot-scale bioreactor

These activities and the others discussed in the report will be continued in the next quarter in support of the overall project objectives.

Appendix A – Review of Photosynthetic System Efficiency and Practicality

There are several factors that make photosynthetic-based systems attractive for CO₂ mitigation.

1. The process works well in nature.
2. Use/ recycling of CO₂ is preferable to disposal.
3. Photosynthetic systems should be applicable to a variety of potential host units.
4. Multi-pollutant control, include metals and NO
5. Generation of valuable O₂.

In addition, focus on development of systems to make photosynthesis a potentially viable industrial process, not organism development, allows for focus on process optimization, cost reduction, land use reduction, and ultimately can use whatever organisms may be identified as optimal in the laboratory, or even (if perfected) could deploy artificial photosynthetic reactions.

Despite such promise, there are several objections to the use of photosynthetic systems in the control of CO₂ emissions. Many of these are explained well in Benemann, 1997 and are discussed here

1. Photosynthetic systems are inefficient.

True. When considering incident sunlight on rooted systems, conversion (on an energy basis) is about 1%. Microalgae and cyanobacteria do better. In full sun, they do about 1-10%. But there is a reason for this. At full sun, 2000 $\mu\text{mol m}^{-2} \text{s}^{-1}$ is too great an incident photon level for the plant to process. Most organisms/plants maximize their productivities at somewhat less than 200 $\mu\text{mol m}^{-2} \text{s}^{-1}$. When kept at low photon intensities, conversion efficiency is routinely measured over 24% with levels as high as 38% reported. (If you will note, the reactor light distribution design will keep photon levels at or below 200 $\mu\text{mol m}^{-2} \text{sec}$.) Also, two other external factors should be noted:

- a. Even at 25% conversion, the power source is “free.”
- b. Research and development into reduction of antenna pigment and even chemical simulation of photosynthesis could push this efficiency higher. And while this is not in the scope of our work, such projects are underway. (I will be visiting Australia’s CSIRO lab where the artificial photosynthesis research is being conducted in December.)

2. Photosynthetic systems use up too much area.

This may well be true. Photosynthetic photon flux is only 2000 $\mu\text{mol m}^{-2} \text{s}^{-1}$ (approximately a gigawatt per Km²) at peak, with much lower instantaneous (and average) values being typical. However, a carefully designed system can reduce that area by increasing incident photon flux and using vertical space.

- the use of solar collector keeps PPFD at a peak by always having the collector incident with the sun
- stacking vertical organism suspension plates reduces bioreactor footprint

Also, while it is doubtful that this process will be useful at all power generation units, most existing power plants are sited on large tracks of land, far from urban development. Most of the land at these sites is otherwise non-usable land. (except perhaps for landfill construction.) The conversion to a solar-based bioreactor would be as good a use of the land as any.

3. This process of photosynthetic carbon dioxide mitigation cost too much

At the present moment, YES. But you can say the same for every other option currently being studied. Who has a <\$10/ ton solution ready to go? It is interesting that a “natural” solution is dismissed for cost, when membrane, amine, (or whatever) separation and later land or ocean sequestration systems are just as cost prohibitive, but are widely touted as the answer to CO₂ buildup.

In this section, the costs of sequestration are more closely examined, and various assumptions of process efficiency and subsystem costs are studied. The case being examined is for a powerplant with a gross capacity of 200 MW, a capacity factor of 65% operating as a load-following unit (peaking during the day when solar photons are available), with a heat rate of 9000 BTU/kW-hr, burning a coal containing 70% carbon by mass and a HHV of 12,000 BTU/lbm.

The bioreactor will be designed to remove 50% of all CO₂ during daylight hours (during peak use), and the incident photon flux on the solar collectors as delivered to the bioreactor is 1200 μmols m⁻² s⁻¹. (This value assumes that the directional control of the collector surface can collect approximately 2100 μmols m⁻² s⁻¹ without cloud cover and the effect of weather and fiber attenuation reduces the value to 1200.)

A copy of the code used to implement the analysis based on these assumptions follows

Program Code for Engineering Equation Solver

```

P=200000           {Power generation output in kilowatts}
cf=0.65           {Plant capacity factor}
HeatRate = 9000   {Btu/kw-h}
f_C=0.70          {Fraction of the coal that is carbon}
MWr=44/12         {Ratio of molecular weights of carbon dioxide to carbon}
HHV=12000        {Higher heating value of coal in Btu/lbm}
reduction=0.5     {reduction of CO2 emissions, divide by two to get total}
systemlife=30    {30 years of analysis}
reflectorcost=500 {Cost per unit collector}

m_dot_CO2=P*cf*HeatRate*f_C*MWr*reduction/(HHV*1/0.454)/3600
CO2=m_dot_CO2*8766*3600/1000*.5
reflectorarea=pi*2.5*2.5/4
reflectorprice=500/reflectorarea

```

*{Lets say it takes 8 quanta (mole) of photons to convert one mole of CO₂, then X=8
Absolute best efficiency you could expect of a biological agent is X=4
For an artificial process, the best would be about X=2.7}*

*Mole_Co2=M_dot_co2/44
photons=1000*Mole_Co2*X
growtharea2=photons/200E-06
reactorwidth=500
platespacing=0.05
reactorlength=growtharea2/3/reactorwidth/(1/platespacing)
collectorarea=photons/1200E-06
area2=collectorarea^.5
collectors2=collectorarea
collectorcost=collectors2*reflectorprice
PerTon=collectorcost/(CO₂*systemlife)*

Analysis of Results

Before discussing the graphs of costs for various assumptions, it should be noted that the key cost parameter is the cost of the solar collectors. Right now, it is estimated that the collectors, built by hand, would cost \$90,000 a piece to install. Without mass production and economies of scale, \$90,000 per collector would make the cost of one ton of CO₂ removed from the flue gas approximately \$6000.

However, commercialization and mass manufacture of the solar collector technology seems much more likely. The design team, headed by Oak Ridge National Laboratories, received \$3 million from DOE (DE-PS36-00GO10500) to further their hybrid lighting work. Their technology, while extremely useful (if not absolutely necessary) for the bioreactor, is actually focused towards use as a lighting system in commercial buildings. More information on their program related to development can be found at <http://www.ornl.gov/hybridlighting/>.

In order to examine the effect of photon conversion efficiency at a collector cost of \$2000 per unit, Figure 1 was generated. Using the previously stated assumptions, the minimum cost for collection of one ton of CO₂ over the lifetime of the bioreactor, assuming continuous use with the unit, would be \$44, with a more likely cost (assuming an optimistic 30% conversion efficiency) is \$146 per ton.

At \$500 per collector, the costs are more reasonable, as shown in Figure 2. Using the same assumptions used to generate Figure 2, except for the \$500 per collector cost, the cost of removing one ton of CO₂ over the life of the bioreactor falls to a minimum of \$11 and a more likely value of \$37 per ton.

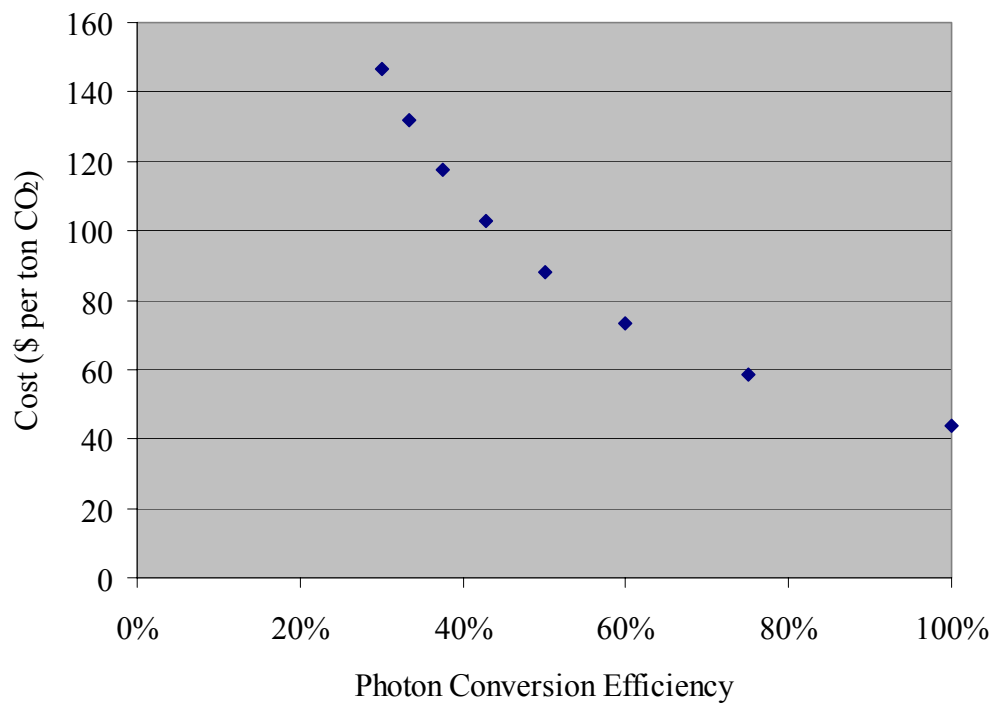


Figure 7. Cost of one ton of CO₂ removed as a function of photon conversion efficiency for a collector price of \$2000 per unit.

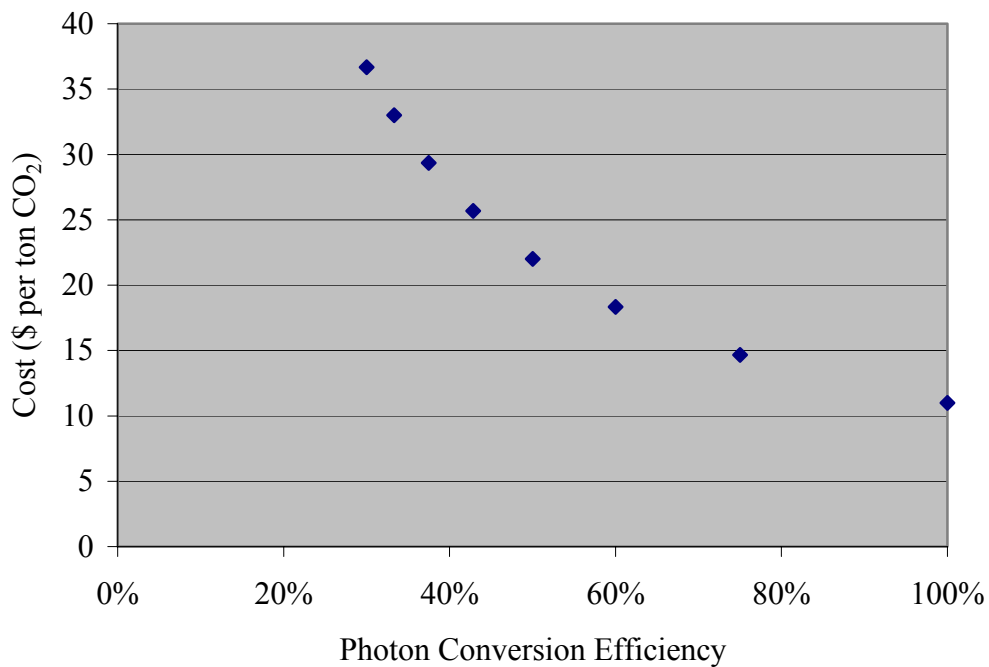


Figure 8. Cost of one ton of CO₂ removed as a function of photon conversion efficiency for a collector price of \$500 per unit.

If line losses (photon attenuation) is reduced and deployment of such a unit occurs in a “sunnier” location, the incident photon level could increase to approximately $1500 \mu\text{mol m}^{-2} \text{s}^{-1}$, the cost of CO_2 removal (per ton) at a conversion efficiency of 30% is \$29.

While not all the analysis done on economics is presented here (it will be given in the final report), it is clear that current system design, even if deployed in “sunny” locations, will require a more efficient organism or process to carry out photosynthesis. It is important to note that the target economics, as described in the proposal (\$8-\$10 per ton), would require 50% conversion efficiency and a collector cost of \$250 per unit.

Value of Byproduct (biomass)

Of course, another key parameter, and the one sought after by many proponents of photosynthetic control, is the value of the harvested biomass. It is well accepted that biomass could be used in a number of applications, including

- fertilizer
- H_2 source
- animal feed stock
- biodiesel
- pigment/ dyes
- Dietary supplement(beta carotene)

Work has not yet been done under this program to investigate other potential uses of the biomass. However, any positive revenue (or offsetting cost) of the biomass would positively influence the overall economics.

This aspect will also be discussed in more detail in the final report.