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## NEUTRONIC DATA IN SUPPORT OF SPACE NUCLEAR PROPULSION

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## ABSTRACT

The scattering kernel data for  ${}^7\text{LiH}$  have been generated for the first time in the temperature range 50-1000 K. This is based on a phonon distribution function derived from both experimental data and theoretical calculations. A detailed study of the variation of the moderator temperature coefficient  $\alpha_m(T)$  with temperature,  $T$ , is carried out for a typical space nuclear reactor of the particle bed type. It is established that the moderator temperature coefficient is proportional to  $T^{-1.65}$  where  $T$  is the moderator temperature in Kelvin units.

INTRODUCTION

The thermophysical properties of lithium hydride ( ${}^7\text{LiH}$ ), particularly small density (0.775 gm/cc), high melting point (688° C) and relatively high hydrogen atomic number density makes it an attractive material for use as a neutron moderator and shield (for LiH) in space nuclear thermal propulsion. However, the unavailability of neutronic cross section data in the thermal energy range for  ${}^7\text{LiH}$  in the ENDF/B library necessitated the generation of the relevant data which is required in criticality studies and for the determination of temperature-dependent feedback coefficients in the moderator and fuel regions.

GENERATION OF THE SCATTERING KERNEL DATA

The phonon frequency distribution function of  ${}^7\text{LiH}$  was derived from experimental data as well as theoretical calculations [1]. One interesting feature of this phonon spectrum is the presence of an energy gap between 0.062 and 0.074 eV separating the acoustical and optical phonon modes (Fig. 1). This phonon spectrum, evaluated in the present study, was utilized in GASKET calculations [2] to determine the scattering matrix elements  $S(\alpha, \beta)$ , the Debye-Waller integrals and the effective temperatures in the temperature range 50-1200° K. Subsequently, the calculated  $S(\alpha, \beta)$  values were cast in an ENDF format in order to be processed by the NJOY code [3] which produces files for the MCNP Library (Fig 2).

MODERATOR TEMPERATURE COEFFICIENT

The present results were incorporated in a special Monte Carlo neutron and photon MCNP

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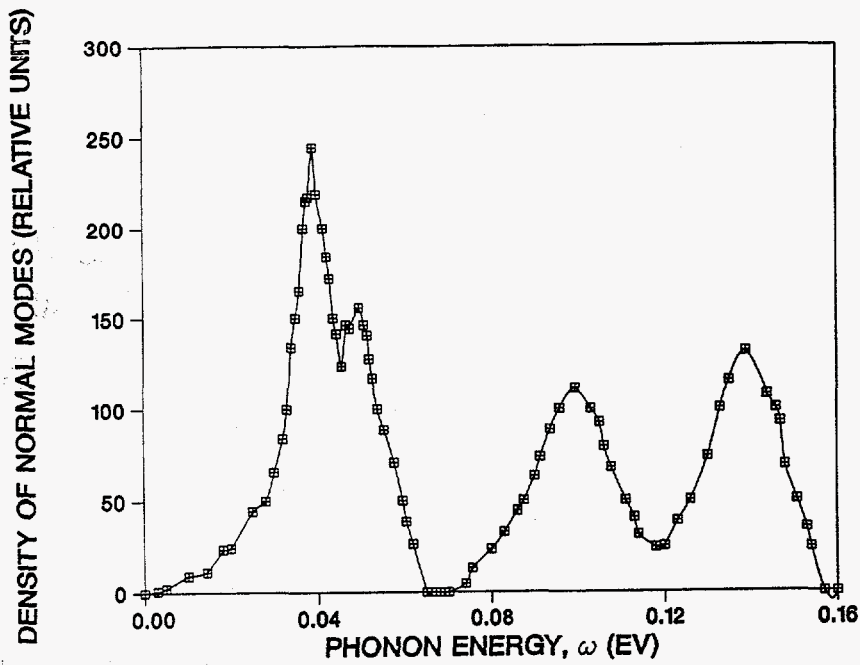


Fig. 1 The Evaluated  $^7\text{LiH}$  Phonon Frequency Distribution Employed In GASKET.

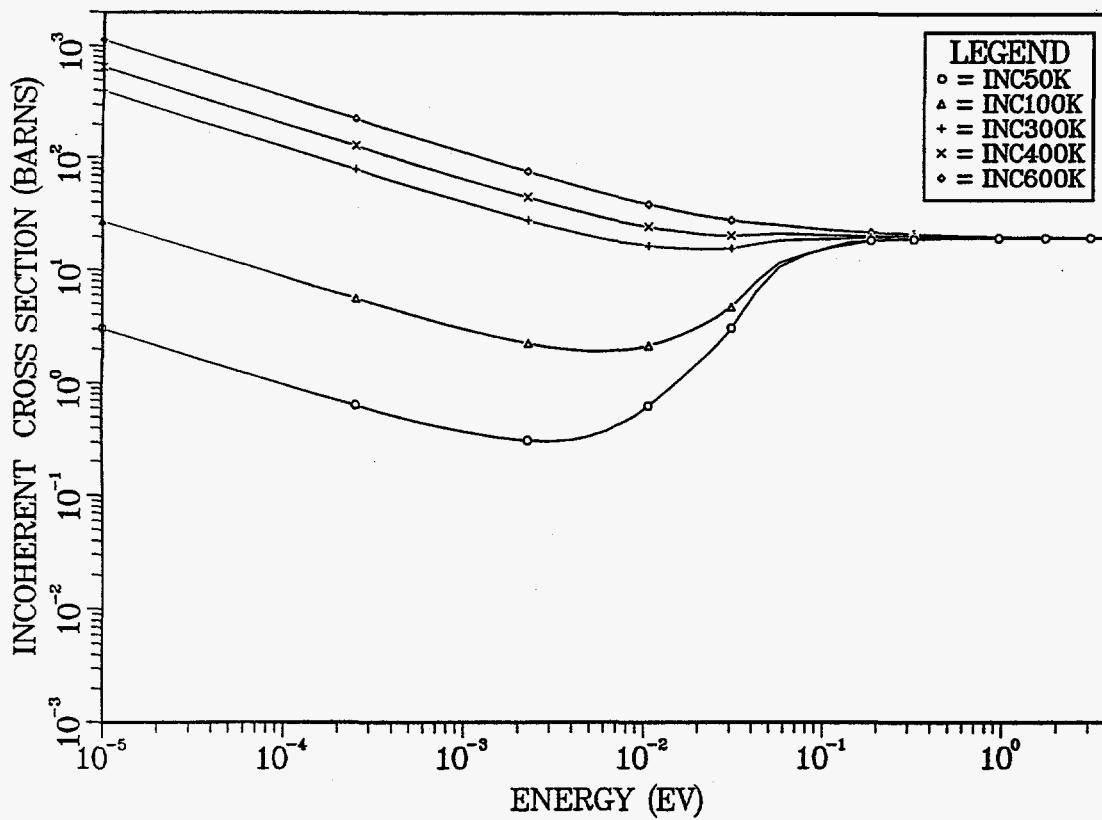


Fig. 2 The Incoherent Cross Sections of  $^7\text{LiH}$  as Computed by GASKET .

library, and tests were carried out to access the magnitude and temperature dependence of the moderator temperature coefficient for typical nuclear space reactors with lithium hydride as the moderator. A particle bed reactor design [4] with a pitch of 12 cm, height 60 cm, 19  $^{235}\text{U}$  fuel elements with a total fuel volume of 30 liters, side, top, bottom beryllium reflectors (10 cm each) was considered. The reactivity temperature coefficients were determined for this configuration with MCNP computations at various temperatures. From the present and previous results [5] the following dependence for the moderator temperature coefficient was deduced.

$$\alpha_m(T) = CF_v(H)^{1.6}T^{-1.65} \quad (1)$$

where  $F_v(H)$  is the volume fraction of the hydrogen moderator and  $C$  is a normalizing constant which depends on the thermal capture cross section of the moderator under consideration. With the four factor formula, it can be shown that, under the assumption of no change in the fission rate with temperature, the  $C$  in Equation 2 is related to the Maxwellian average capture cross section of the moderator[5]. The positive component of the temperature coefficient, which is due to chemical binding effects, can be counteracted by several methods, such as : 1) reduction of the solid homogeneous solid moderator, 2) replacement by a moderator with a small thermal neutron capture cross section such as  $\text{D}$ ,  $^9\text{Be}$ ,  $^{11}\text{B}$ ,  $^{12}\text{C}$ , 3) operation of the moderator at a high temperature such as  $800^\circ\text{K}$ , 4) change in moderator density due to expansion, and 5). combinations of the above methods. Method 3 provides negative temperature coefficient for some moderators. For  $^7\text{LiH}$  moderator, density changes of 20% from 800 K to  $1000^\circ\text{K}$  results in a large negative reactivity if a mechanism of expansion for the  $^7\text{LiH}$  out of the moderator region is allowed in a manner similar to a pressurized boiling water reactor. A preliminary estimate of negative reactivity of 2.5% in this temperature range is achieved for this reactor design.

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## References

- [1] S. F. Mughabghab et. al. and references therein, Tenth Symposium on Space Nuclear Power Systems, Albuquerque, New Mexico, January 10-14, 1993
- [2] J. U. Koppel and D. H. Houston (1978) Reference Manual for ENDF Thermal Scattering Data, GA-8774 Revised (ENDF-269).
- [3] R. E. McFarlane et. al., "The NJOY Nuclear Data Processing System", Los Alamos National Laboratory Report LA 9303-M, Volume 11 (1982).
- [4] H. Ludewig et. al. Proceedings of the Sixth Symposium on Space Nuclear Power Systems, p. 153, CONF-890103-Summs., Albuquerque, NM, 8-12 January, 1989
- [5] S. F. Mughabghab et. al., BNL Reactor Systems Division Internal Report, Part 11, 1990

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