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## Assessment Groundwater Monitoring Plan for Single Shell Tank Waste Management Area B-BX-BY

J. A. Caggiano

Westinghouse Hanford Company, Richland, WA 99352 U.S. Department of Energy Contract DE-AC06-87RL10930

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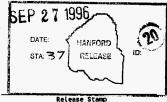
Key Words: Groundwater Monitoring, Single Shell Tanks, 241-B, 241-BX,

241-BY Tank Farms, RCRA

Abstract: Single Shell Tank Waste Management Area B-BX-BY has been placed into groundwater quality assessment monitoring under interim-status regulations. This document presents background and an assessment groundwater monitoring plan to evaluate any impacts of risks/spills from these Single Shell Tanks in WMA B-BX-BY on groundwater quality.

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## METRIC CONVERSION CHART

Into metric units

Out of metric units

		·					
If you know	Multiply by	To get	If you know	Multiply by	To get		
	Length		Length				
inches	25.40	millimeters	millimeters	0.0393	inches		
inches 2.54		centimeters	centimeters	0.393	inches		
feet	0.3048	meters	meters	3.2808	feet		
yards	0.914	meters	meters	1.09	yards		
miles	1.609	kilometers	kilometers	0.62	miles		
	Area		Area				
square	6.4516	square	square	0.155	square		
inches		centimeters	centimeters	<u> </u>	inches		
square feet	0.092	square	square	10.7639	square		
		meters	meters		feet		
square	0.836	square	square	1.20	square		
yards		meters	meters	`	yards		
square	2.59	square	square	0.39	square		
miles		kilometers	kilometers		miles		
acres	0.404	hectares	hectares	2.471	acres		
	Mass (weight		Mass (weight)				
ounces	28.35	grams	grams	0.0352	ounces		
pounds	0.453	kilograms	kilograms	2.2046	pounds		
short ton	0.907	metric ton	metric ton	1.10	short ton		
	Volume	•	Volume				
fluid	29.57	milliliters	milliliters	0.03	fluid		
ounces					ounces		
quarts	0.95	liters	liters	1.057	quarts		
gallons	3.79	liters	liters	0.26	gallons		
cubic feet	0.03	cubic	cubic	35.3147	cubic feet		
		meters	meters				
cubic yards	0.76456	cubic	cubic	1.308	cubic		
<u></u>		meters	meters		yards		
	Temperature		Temperature				
Fahrenheit	subtract	Celsius	Celsius	multiply	Fahrenheit		
	32 then			by			
Į.	multiply			9/5ths,			
	by 5/9ths		1	then add			
	F		32				
ļ,	Force	177	Force				
pounds per	6.895	kilopascals	kilopascals	1.4504 x	pounds per		
square inch				10-4	square		
					inch		

Source: Engineering Unit Conversions, M. R. Lindeburg, PE., Second Ed., 1990, Professional Publications, Inc., Belmont, California.

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# GROUNDWATER QUALITY ASSESSMENT MONITORING PLAN FOR THE SINGLE-SHELL TANK SYSTEM WASTE MANAGEMENT AREA B-BX-BY

J.A. Caggiano, C.J. Chou, and V.G. Johnson, Westinghouse Hanford Company

#### 1.0 INTRODUCTION

The groundwater monitoring program conducted for the Single-Shell Tank (SST) System waste management area (WMA) B-BX-BY (Figure 1) will be changed from detection-level monitoring to a groundwater quality assessment program as described in Washington State Department of Ecology (Ecology) Dangerous Waste Regulations, Washington Administrative Code (WAC) 173-303-400 [refer to 40 Code of Federal Regulations (CFR) 265 Subpart F] because of elevated specific conductance. The average of quadruplicate measurements of groundwater samples collected on February 6, 1996 from downgradient well 299-E33-32 was 369 micromhos per centimeter, which exceeded the background level of 365.7 micromhos per centimeter for this parameter. Required verification sampling was conducted on June 21, 1996 [40 CFR 265.93 (c)(2)]. Results of the verification sampling (two sets of quadruplicate measurements) averaged 427 micromhos per centimeter thereby confirming that the initial increase statistically was significant. Additionally, nitrate and chloride have more than doubled in this well since the inception of groundwater monitoring in 1990. Nearby downgradient wells do not exhibit a similar pattern. Ecology was notified of the exceedances and that the SST System may be affecting groundwater quality [40 CFR 265.93(d)(1)]. This plan satisfies requirements specified in 40 CFR 265.93(d)(3).

#### 2.0 SCOPE AND OBJECTIVES

The purpose of this document is to present a groundwater quality assessment monitoring plan for the WMA B-BX-BY in accordance with Resource Conservation and Recovery Act (RCRA) of 1976 interim-status regulations (WAC 173-303-400 and 40 CFR 265 Subpart F). The primary objective is to determine if the observed changes in groundwater quality are due to the regulated unit, and if so, identify source(s), driving force(s), and pathway(s) to groundwater so that corrective measures can be taken [40 CFR 265.93(d)(4)]. A two-phased groundwater monitoring program is proposed. The first determination will be focused on a false positive investigation [40 CFR 265.93(d)(5)]. Key to this investigation is the development of a conceptual model. This involves conceptualization of waste migration through the vadose zone to groundwater and is an integral part of the data quality objective (DQO) process.

Based on the results of the first determination, if it is found that no dangerous waste or dangerous waste constituents from the SST System WMA B-BX-BY have entered the groundwater, the site will be reinstated to a detection-level monitoring program [40 CFR 265.93(d)(6)]. If, however, the first determination confirms that the SST System WMA B-BX-BY is the source of contamination or is inconclusive, a second phase assessment program will be

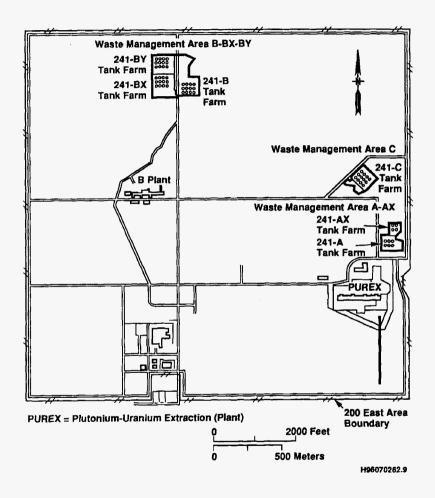


Figure 1. Location Map of Waste Management Area B-BX-BY.

initiated to fully characterize the rate and extent of contaminant migration [40 CFR 265.93(d)(7)]. Any vadose zone investigations will be a part of the more comprehensive vadose zone characterization program being instituted by the Tank Waste Remediation System (TWRS) organization. Figure 2 is a flow chart depicting the sequence of events that illustrates the process adopted for the WMA B-BX-BY groundwater quality assessment plan. Key elements of this plan are discussed in the following sections. Historical background on tank dimensions, construction, waste processing, and tank monitoring for conceptual model development is provided in Appendix A.

#### 3.0 HYDROGEOLOGIC CONDITIONS

Understanding the hydrogeology near the regulated unit is fundamental to interpretation of contaminant sources, subsurface contaminant migration, and plume distribution patterns. Therefore, this section summarizes the existing stratigraphic and hydrologic information relevant to assessing possible contaminant sources and pathways to groundwater beneath the WMA B-BX-BY.

#### 3.1 STRATIGRAPHY

Geology of the 241-B, 241-BX, and 241-BY Tank Farms was first reported by Price and Fecht (1976a, 1976b, 1976c) shortly after the dry well boreholes were completed in the 1970s. Drilling logs are available for many of these boreholes, but the level of detail is inadequate to make current stratigraphic interpretations. Geology and hydrogeology of WMA B-BX-BY are discussed in the groundwater monitoring plan (Caggiano and Goodwin 1991). Geology also has been described for the adjoining 200-BP-1 operable unit (the 216-BY cribs located north of the 241-BY Tank Farm) (Hoffman 1992).

The major stratigraphic units of the suprabasalt unconfined aquifer present beneath WMA B-BX-BY are three facies of the Hanford formation: the lower gravel, sand, and upper gravel units (in ascending order). Some undifferentiated Ringold gravel could be present beneath the southern part of WMA B-BX-BY (Lindsey 1992).

Three units of the Hanford formation are present: an upper coarse unit, a middle fine to medium-grained sandy unit, and a lower coarse unit. Both the upper and lower coarse units consist of pebble and cobble gravel with interbedded plane bedded to planar cross-bedded medium to coarse, basaltic sand. In places, the gravel could be openwork and clast supported, while elsewhere the clasts occur in a matrix of medium to coarse basaltic sand. The sandy sequence consists mostly of plane to planar cross-bedded medium to coarse sand, with some fine sand and silt present as thin laminae or lenses. Clasts could be present as isolated pebbles or as pebbly sandy units or sandy gravels much like the overlying and underlying gravel sequences. These units rest directly atop the Elephant Mountain member and generally thicken toward the south into the Cold Creek Syncline. Basalt was reached at a depth of 255 and 252 feet in RCRA groundwater monitoring wells 299-E33-31 and 299-E33-33, located west and east of WMA B-BX-BY, respectively.

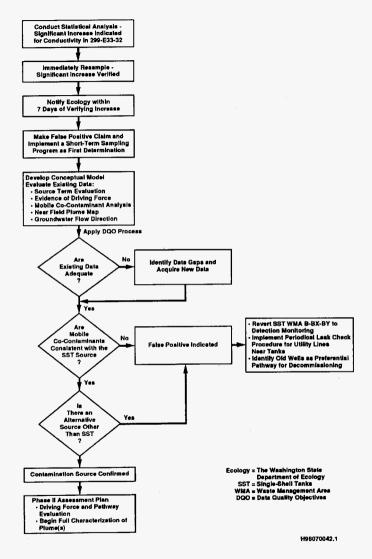


Figure 2. Flow Chart for Phase I Groundwater Quality Assessment Monitoring Program.

Basalt was reached at 238 and 229 feet below ground in well 299-E33-38 and 299-E33-39 (respectively), reflecting the general southward dip of the Elephant Mountain member of Columbia River Basalt toward the axis of the Cold Creek Syncline. The thickness of suprabasalt sediments generally increases to the south toward the axis of the Cold Creek Syncline. North-south and east-west cross-sections beneath WMA B-BX-BY are shown on Figure 3.

Backfill is a mix of Hanford formation coarse and fine sandy units that is a slightly silty medium to coarse sand and gravel from which the larger clasts were removed before placing back in the excavation. The backfill was placed in 4-foot lifts, so some compaction occurred during construction with the movement of vehicles and equipment across the existing surface. No concerted effort was made to compact the fill, which is about 39 to 42 feet thick (the base of the tanks) in the 241-B and 241-BX Tank Farms and about 49 feet thick beneath the 241-BY Tank Farm.

Clastic Dikes as Preferential Pathways. Clastic dikes are common in the Hanford formation and are generally 6 to 16 inches wide. Clastic dikes were detected but not mapped in drilling dry well boreholes in the 241-B, 241-BX, and 241-BY Tank Farms (Price and Fecht 1976a, 1976b, 1976c). Clastic dikes commonly have exterior margins of thin (less than 0.25 inch) clayey silt (locally termed clay skins). There could be several laminae of similar texture and composition within the interior of a dike. Within any one dike, strata could be well sorted and continuous while others are discontinuous. Delicate sedimentary structures could be present in some, while others contain more massive bedding. The vertical and lateral variation in grain size and strata within a dike can be abrupt and extreme. From any one dike, smaller dikes and/or sills can branch. Clastic dikes were mapped recently in the excavation for the Environmental Restoration Disposal Facility in sandy units of the Hanford formation (Fecht and Weekes 1996). Clastic dikes also have been observed in the excavation for disposal vaults of the Grout Treatment Facility east of the PUREX Facility in the 200 East Area. Clastic dikes also have been observed in the excavation for WMA 2 of the Low-Level Burial Grounds (trench 94 of the 218-E-12B Burial Ground) in the northeast corner of the 200 East Area.

The mechanism(s) of formation of clastic dikes is not well known, but is likely some form of soft-sediment deformation attributable to liquefaction in rapidly deposited sediments. Rapid sedimentation in hydraulically dammed water north of Wallula Gap likely represents the conditions of deposition responsible for the formation of the dikes.

Where clastic dikes intersect the ground surface, they form patterned ground that can be recognized from aerial photographs as zones of more intense vegetation (presumably because of greater water retention capacity than the surrounding 'host rock'). Fecht and others (1994) have found a relationship between the size of the clastic dikes and the diameter of the polygons that

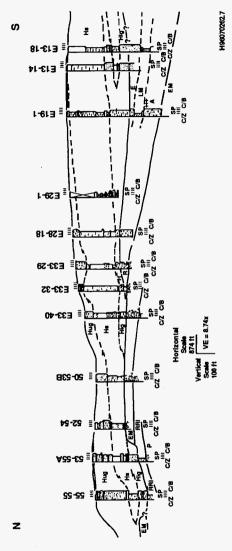


Figure 3a. North-South Geologic Cross-Sections Beneath Waste Management Area B-BX-BY.

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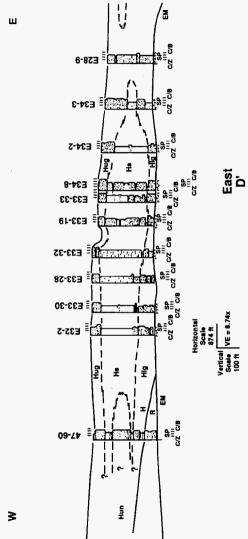


Figure 3b. West-East Geologic Cross-Sections Beneath Waste Management Area B-BX-BY.

these form. The clastic dikes in WMA B-BX-BY generally are not exposed, but can be of a width that the polygons formed are on the order of 50 to 90 feet in diameter. Considering that the SSTs in WMA B-BX-BY are 75-foot diameter with 100 feet between adjacent tank centers, it is highly likely that several clastic dikes are intercepted by tanks or dry wells within WMA B-BX-BY and could serve as preferential pathways to influence both lateral and vertical movement of liquids and contaminants. Clastic dikes could intersect the bottom and sides of the excavation for the tanks, could intersect the bottom of a tank or lateral lines beneath a tank, could intersect various other structures within the farm that could release liquids, or could intercept one of numerous unsealed boreholes or partially sealed groundwater monitoring wells within WMA B-BX-BY.

Clastic dikes can have a significant effect on the movement of liquids and thus the transport of contaminants. If liquid is added directly above a clastic dike, the 'clay skins' could restrict and confine infiltration to the width of the dike, thereby preferentially enhancing vertical transport. If liquid impinges laterally on a dike, fluids could be 'dammed' temporarily before the clay skin becomes saturated to permit infiltration into the interior of a dike. Varying grain sizes of units and bedding within could further influence the movement of liquids within a dike.

#### 3.2 HYDROLOGY

Groundwater movement beneath WMA B-BX-BY is influenced by both historical discharges and water table gradients in the immediate area and by the hydrogeology of the aguifer.

#### 3.2.1 Water Levels

The water table occurs in the lower coarse unit of the Hanford formation at a depth that varies from about 239 to 261 feet below ground surface (water table elevation is about 400 feet above sea level). With the decline of the water table beneath WMA B-BX-BY (Caggiano 1996), the saturated zone above basalt slowly is diminishing. The saturated thickness of the suprabasalt aguifer generally is less than 10 feet in most of WMA B-BX-BY.

#### 3.2.2 Groundwater Flow Direction

The WMA B-BX-BY is located in an area of very low hydraulic gradient between the water table mound beneath 216-B-3 Pond and eastward moving water from the 200 West Area (Serkowski et al. 1996). The B Pond System (216-B-3 Pond and three smaller lobes) received about 250,000,000 gallons of liquid effluent from 1945 to 1995. By 1960, this resulted in a rise of about 35 feet in the water table elevation from the pre-Hanford Site water table. This water table mound caused eastward flowing groundwater following the regional gradient to divert around the areas with higher hydraulic head and resulted in radial flow out from the apex of the mound. The B Pond water table mound has controlled the direction of groundwater flow in the suprabasalt aquifer beneath WMA B-BX-BY since the inception of PUREX Facility

operations in 1956. Before the rapid buildup of the water table mound beneath B Pond, groundwater flow in the suprabasalt aquifer from the northern part of the 200 East Area was to the southeast towards the PUREX Facility. The large volume of liquid effluent disposed to the 216-BY cribs and the low volume of liquid effluent discharged to B Pond before the startup of the PUREX Facility accounts for this early 1950s groundwater flow direction. With the development and expansion of the water table mound and the rise of the water table, groundwater was able to flow north across subsurface ridges in the basalt such that contaminants in the suprabasalt aquifer from the 216-BY cribs have migrated north toward Gable Gap (e.g., Serkowski and Jordan 1989; Serkowski et al. 1988). However, for any high density waste that might sink to the base of the suprabasalt aquifer, transport to the south might have occurred as the basalt surface and the Elephant Mountain member dip southward into the axis of the Cold Creek Syncline.

The elevation of the water table has continued to decline beneath the 200 East Area because discharges to cribs, unlined trenches, and B Pond have decreased. All liquid effluent discharges to the ground ceased in June 1995 except for facilities that were granted operating permits by Ecology. The decline and shrinkage of the B Pond mound has lowered the hydraulic head beneath WMA B-BX-BY resulting in a nearly flat water table and an uncertain present direction of groundwater flow (refer to Section 4.1).

### 3.3.3 Aquifer Communication

North of the 200 East Area, two wells (699-55-55 and 699-53-55) have passed from the Hanford formation directly into the Rattlesnake Ridge interbed. The Elephant Mountain member (of the Columbia River Basalt) that usually is the base of the suprabasalt aquifer in the 200 East Area and separates the Hanford formation from the Rattlesnake Ridge member is absent (Hoffman 1992). The extent of this window is unknown, but hydraulic communication between the Rattlesnake Ridge and the suprabasalt aquifer occurs in this area of stratigraphic superposition. The bottom of the uppermost aguifer in this window through the Elephant Mountain member is the Pomona member--the flow below the Rattlesnake Ridge interbed. Whether the exchange of groundwater is upward from the Rattlesnake Ridge to the Hanford formation or vice versa is a function of the difference in the hydraulic head between the two aquifers. Water will move from areas of higher hydraulic head to lower head. Except in the area of the B Pond mound, the head in the Rattlesnake Ridge typically is higher than in the suprabasalt aquifer and is likely to remain so with a continually declining water table beneath WMA B-BX-BY. However, as discussed previously, contaminants generated on the Hanford Site have been found in the Rattlesnake Ridge in well 299-E33-12 (completed in the Rattlesnake Ridge member), suggesting that communication between the suprabasalt and Rattlesnake Ridge aguifer has occurred in the past, perhaps only as a result of this poorly sealed well.

#### 4.0 DESCRIPTION OF DETECTION MONITORING SYSTEM

This section describes the detection monitoring system for the RCRA groundwater monitoring program. Historic surveillance conducted to monitor the integrity of the SST System is described in Appendix A.

#### 4.1 WELL NETWORK

Seven RCRA wells constitute the monitoring network for WMA B-BX-BY (Figure 4): two wells installed as upgradient wells (299-E33-33 and 299-E33-36) and five wells installed as downgradient wells (299-E33-31, 299-E33-32, 299-E33-42, 299-E33-43 and 299-E33-41). With the present uncertainty of groundwater flow direction, these "upgradient" and "downgradient" designations remain enigmatic. Well 299-E33-41 is located within WMA B-BX-BY east of the perimeter fence of the 241-BX Tank Farm. The other four wells are located along the western perimeter fence of the 241-BX and 241-BY Tank Farms. In addition, two wells (299-E33-38 and 299-E33-39), north and northeast of WMA B-BX-BY constructed to WAC 173-160 specifications during investigations for the 200-BP-1 operable unit, are used for supplemental sampling and water level information. The RCRA well as-built diagrams are provided in Appendix B. These wells were constructed between 1989 and 1991 in accordance with the original groundwater monitoring plan for the SST System (Jensen et al. 1989), its revision (Caggiano and Goodwin 1991), or the remedial investigation/feasibility study work plan for the 200-BP-1 operable unit. All post-1986 wells were constructed using cable tool methods and were completed as 4-inch diameter wells with stainless steel casing and screens, filter pack, full annular (bentonite crumbles) and surface seals (Caggiano 1992: 1993). All RCRA wells comply with construction specifications in WAC 173-160. All wells have a 20-foot screen, the bottom of which is at or close to the top of basalt. All wells were located outside the perimeter fences of tank farms and at least 100 feet from the nearest tank by agreement with Ecology to prevent the driving of contaminants deeper into the vadose zone during well construction.

Several older carbon steel wells are located within and around WMA B-BX-BY (refer to Figure 4). These wells were constructed of carbon steel casing that is perforated over different lengths within the uppermost aquifer. Many of the older wells were constructed adjacent to cribs and were used to monitor these facilities. These older wells can be used to supplement data from RCRA wells, but cannot be used to sample for dangerous constituents per the policy on existing wells jointly issued by EPA and Ecology in July 1990. Regulatory decisions regarding these sites must be based on sampling of dangerous constituents from RCRA-compliant wells. A fitness-for-use evaluation will be made of some of these older wells to test their suitability for use in an expanded groundwater monitoring network under assessment monitoring status.

Three of the older wells are located within the perimeter fences of WMA B-BX-BY: 299-E33-9 is adjacent to the 241-BY-102 tank; 299-E33-27 is adjacent to the 241-BX-102 tank; 299-E33-18 is adjacent to and north of the 200-series tanks in the 241-B Tank Farm. Wells 299-E33-19 and 299-E33-20 are

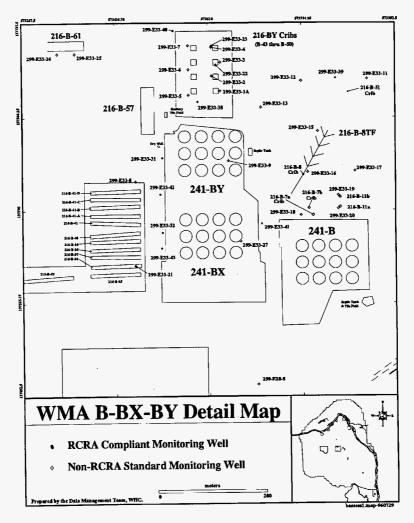


Figure 4. Map of Groundwater Monitoring Wells Around Waste Management Area B-BX-BY.

located north of the 241-B Tank Farm and were constructed to monitor the nearby 216-B-11A and B reverse wells. Other older wells are located north and west of WMA B-BX-BY and were constructed to monitor nearby cribs and trenches (refer to Figure 4), such as the 216-BY cribs (200 BP-1) that are located north of the 241-BY Tank Farm. One well worthy of note is well 299-E33-12, an 8-inch well drilled in 1953 to the Rattlesnake Ridge interbed, with the screen actually landing in what appeared to be the flow top of the Pomona member of Columbia River Basalt.

The RCRA groundwater monitoring network was designed in 1989 for a west to west northwest direction of groundwater flow in the suprabasalt aguifer. The MEMO indicates that the efficiency of the network is about 85 to 88 percent for a west to west northwest direction of groundwater flow (Caggiano and Goodwin 1991, p. 104). Hydrographs of RCRA wells (Figure 5) indicated that well 299-E33-33 has had a higher hydraulic head than those on the west side of WMA B-BX-BY and was the upgradient well when the network was designed and installed. The decline and shrinkage of the B Pond mound has lowered the hydraulic head beneath WMA B-BX-BY resulting in a nearly flat water table and an uncertain present direction of groundwater flow. Figure 5 also shows the long-term trend in water levels near WMA B-BX-BY. The rapid increase in the late 50's and early 60's followed by a moderate decline in the early 70's was attributed to PUREX Facility operations from 1955 through 1971. The return to higher water levels in the mid 80's was due to resumption of fuel reprocessing at the PUREX Facility in 1983 that continued until 1989. The significance is that the mound created by waste water discharges to PUREX Facility cribs and B Pond has persisted for 35 years and probably has sustained an overall flow reversal (west-to-east to southeast-to-northwest) over this period. The steep decline in recent years, however, could be causing a shift in flow direction.

Borehole flow meter measurements in 1995 in several wells (including 299-E33-31, a WMA B-BX-BY downgradient well) in 200-BP-1 (located north of WMA B-BX-BY) indicate that groundwater flow now appears to be more to the south to southwest. However, the water table beneath 200 East Area is extremely flat. The measured difference in hydraulic head between wells 299-E33-33 and 299-E33-31 in February 1996 was 0.03 foot. These two wells are about 1,950 feet apart. The maximum difference in hydraulic head among all wells in the network for February 1996 is 0.75 foot, well within the combined measurement errors for all the variables involved in depth to water measurements. A new simultaneous geodetic survey of all wells has been requested because different dates, field crews, and bench marks were used to obtain the present surveyed elevations of these wells.

#### 4.2 SUMMARY OF RCRA SAMPLING AND ANALYSIS RESULTS

Required quarterly sampling for drinking water standards (DWS), water quality parameters, general contamination indicator parameters, and site-specific constituents was completed in 1992. Semi-annual sampling in accordance with the groundwater monitoring plan has been conducted since 1992.

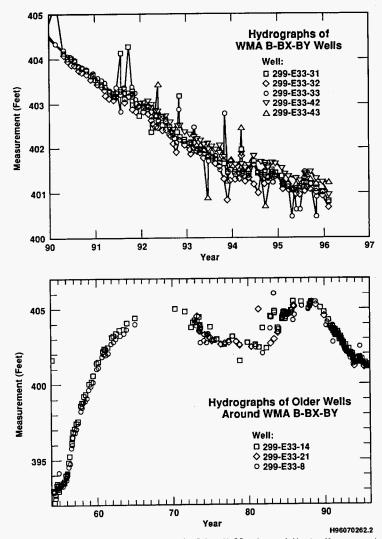


Figure 5. Hydrographs of RCRA and Older Wells Around Waste Management Area B-BY.

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The only exceedance of a DWS at WMA B-BX-BY has been a single value of 1.000 picocuries per liter for technetium-99 in well 299-E33-31 in early 1993. which appears to be an outlier. All other results for this isotope are 500 picocuries per liter or below in this and other wells. Radioisotopes that were a characteristic of the waste disposed to WMA B-BX-BY (e.g., cesium-137, strontium-90, cobalt-60, hydrogen-3) are below regulatory limits and barely above detection limits except for tritium. The exceedance of the critical mean for specific conductance in well 299-E33-32 in February 1996 appears to be caused by a steady increase in nitrate and chloride in this well. Since the inception of monitoring in this well in 1990, chloride has risen from 4,200 parts per billion in 1990 to 10,000 parts per billion in February 1996. while nitrate has risen from 8,200 parts per billion in 1990 to 29,000 parts per billion in 1996. Chloride also has been on the rise in nearby well 299-E33-43, but nitrate has not been increasing. Nitrate has not exceeded the DWS of 45.000 parts per billion in any well in WMA B-BX-BY. Technetium-99 also has risen during the period 1990 to 1996 from about 20 picocuries per liter to over 200 picocuries per liter in well 299-E33-32. Time series plots of selected constituents are shown on Figures 6 and 7. Variation of field specific conductance with time is shown in Figure 8. Map of boreholes surrounding tanks in 241-BY Tank Farm is shown in Figure 9.

#### 4.3 NON-RCRA GROUNDWATER MONITORING

A jointly issued policy by Ecology and the EPA in July 1990 restricts groundwater sampling for regulatory decisions regarding dangerous waste constituents to wells that comply with construction specifications in WAC 173-160. Older wells that do not comply with these specifications could be used to collect supplemental information (e.g., water levels, radionuclides). Four older wells are present within and close to WMA B-BX-BY. Well 299-E33-9 was drilled adjacent to the BY-102 tank in 1949 to a depth of 275 feet (top of basalt). The well was modified in 1978 with the installation of a partial annular seal and, presumably at that time, placement of a grout plug from 261 to 275 feet. This well has been monitored as dry well 22-02-07 as part of the gross gamma surveillance program by the Tank Waste Remediation System organization and its predecessors but was not logged by RUST because of high radiation exceeding conditions of the Radiation Work Permit.

Groundwater monitoring data for well 299-E33-9 date back to 1956 and show extremely high values for gross beta (multiple values exceeding 1,000,000 picocuries per liter regularly between November 1956 and early 1957, with values regularly exceeding 500,000 picocuries per liter through 1959). Values for nitrate, cobalt-60, and sodium also are very high for this same period. Strontium-90 values are up to 260 and 200 picocuries per liter (multiple values of 200 picocuries per liter for strontium-90 indicate this is a detection limit). Single values for strontium-90 for three other older wells at this time range up to 25,000 picocuries per liter, but this validity could not be substantiated. Ruthenium-106 was not analyzed in samples from this well before 1978. Technetium-99 was not analyzed before 1986, but the very high values for gross beta and relatively low strontium-90 and ruthenium-106 suggest that technetium-99 might have been a significant contributor (as well as cobalt-60) to the high gross beta values. Spectral gamma logging in dry wells in the 241-BY Tank Farm indicate the presence of

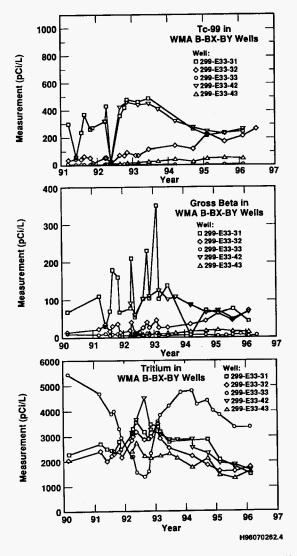


Figure 6. Time Series Plot of Selected Radionuclides for Waste Management Area B-BX-BY.

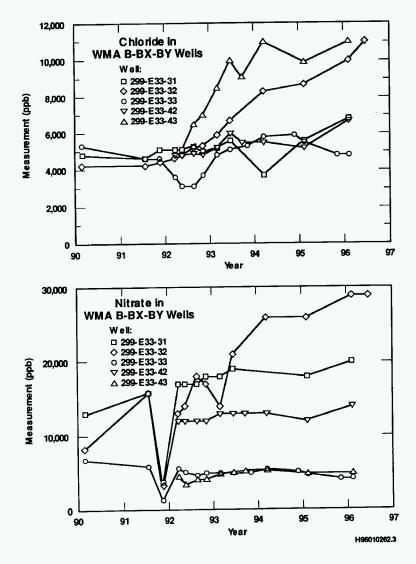


Figure 7. Time Series Plot of Selected Constituents for Waste Management Area B-BX-BY.

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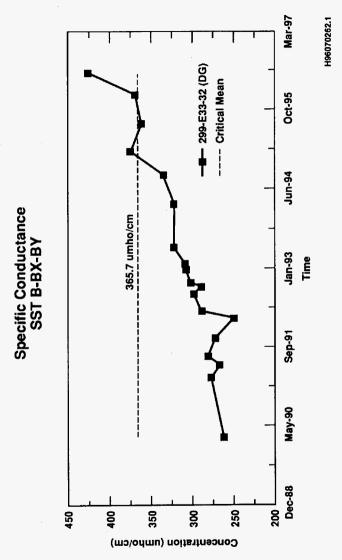


Figure 8. Time Series Plot of Specific Conductance for Waste Management Area B-BX-BY.

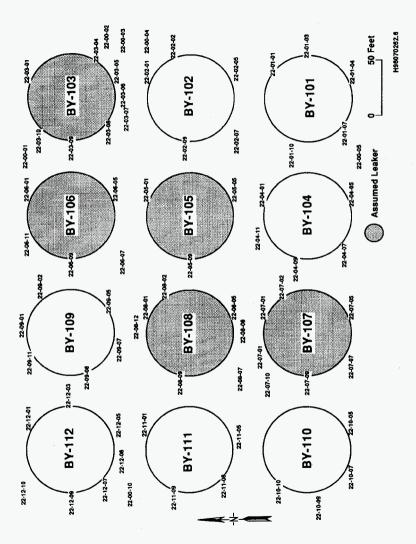


Figure 9. Map of Boreholes Surrounding Tanks in 241-BY Tank Farm.

antimony-125 in the soils, which might also contribute to the gross beta results (antimony-125 was not analyzed in groundwater samples in the 1950s). The BY-102 tank is classified as a sound tank; it is clear that waste that escaped containment was clearly getting to groundwater from some unspecified source. However, because the bottom of this well is at the top of basalt, the waste could have been part of a high salt discharge (with a density greater than 1.0) that migrated along the southward-dipping basalt from some location to the north, such as the 216-BY cribs that were active at this time.

Well 299-E33-27 was constructed in 1970 to a depth of 265 feet using 6-inch diameter casing and cable tool drilling methods. The well was drilled through the area where the plume of waste leaked from the adjacent 241-BX-102 tank in 1971 and was unsealed until 1976. An estimated 30,000 to 90,000 gallon spill between the 241-BX-102 and 241-BX-103 tanks occurred in 1951 (Womack and Larkin 1971), and this well might have been drilled through at least a part of the contaminated soil remaining from that spill. The driller's notes report contamination was encountered during drilling from 214 to 254 feet, with a maximum of 10,000 counts per minute at 214 feet. Contamination decreased with depth, suggesting that at least some contamination was smeared downward (there was no sealing and downsizing of the casing string proceeding through the contaminated zone). The well was remediated with installation of a 4-inch casing in 1976, at which time the 6-inch casing was perforated and cement grout was emplaced. Groundwater samples taken from this well in 1971 showed 34,000 and 36,000 picocuries per liter gross beta and continued above 1,000 picocuries per liter through at least 1983. Analyses for cesium-137 in 1972 reached 8,000 picocuries per liter and were about 7,000 picocuries per liter in 1977. Womack and Larkin (1971) report that cesium-137 activity was higher in groundwater when sampled in 1971, but below the then established (and unspecified) Atomic Energy Commission release limit. However, the value for cesium-137 was higher in this well than in groundwater from wells monitoring the BY cribs to the north. It was concluded that the cesium-137 in groundwater beneath the BX-102 tank likely was carried to groundwater by drilling through contaminated sediments in the vadose zone. The few ruthenium-106 values obtained from this well are below 200 picocuries per liter for the period 1977 to 1983. Several values of tritium in the period 1978 to 1983 exceeded 30,000 picocuries per liter, with a peak of 48,000 picocuries per liter in 1983.

Waste from WMA B-BX-BY and/or surrounding cribs and trenches clearly had reached groundwater by the early 1970s. Womack and Larkin (1971) reported that breakthrough to groundwater had occurred in 1957 and 1959, presumably referring to the 216-BY cribs north of WMA B-BX-BY, but perhaps also to the 216-B-35 through 216-B-42 specific retention trenches west of WMA B-BX-BY.

A pair of wells completed in the Rattlesnake Ridge interbed provide conflicting results that illustrate the possible effects of poorly sealed wells. Well 299-E33-12 was completed in the Rattlesnake Ridge aquifer in 1953 and was not adequately sealed. Well 299-E33-40 was completed into the Rattlesnake Ridge aquifer in 1991 and was sealed. Analysis of groundwater samples from 299-E33-40 reveal essentially no contamination; data from 299-E33-12 reveal significant contamination suggesting that the well was poorly sealed and served as a pathway at a time when uranium scavenging and use of the 216-BY cribs was in full swing. Gross beta above

60,000,000 picocuries per liter, cobalt-60 up to 450,000 picocuries per liter and nitrate approaching 6,000,000 parts per billion in 1957 to 58 provide clear evidence of anthropogenic contaminants reaching the Rattlesnake Ridge during the operational history of WMA B-BX-BY. Data for the period 1991 to present for gross beta, technetium-99, nitrate, and sodium provide clear evidence that contamination still exists in well 299-E33-12, but not in well 299-E33-40. The implication is that contamination is not widespread in the Rattlesnake Ridge and that the poorly sealed well 299-E33-12 provided a preferential pathway that led to local contamination of the Rattlesnake Ridge. However, hydraulic communication between the suprabasalt aquifer and the Rattlesnake Ridge exists to the north of the 200 East Area, suggesting other possible scenarios for contamination reaching the Rattlesnake Ridge.

#### 5.0 GROUNDWATER QUALITY ASSESSMENT PROGRAM

A two-phased program of investigation is proposed. Initially, Phase I investigations (3 to 6 months) will focus on whether the elevated conductivity could be a 'false positive'; i.e., the constituents causing elevated conductivity are not coming from the regulated unit. If the SSTs are the cause of groundwater contamination or the source is indeterminate and could be the SSTs, a Phase II assessment monitoring program to fully characterize the plume(s) will commence. Because Phase II investigations will be contingent on the outcome of Phase I activities, a separate Phase II assessment monitoring plan will be prepared. Phase II investigations would target the identification of pathways and sources of fluid as driving forces of contaminants to groundwater. The overall objectives of the Phase I investigation are as follows:

- Substantiate or negate the false positive claim
- Implement near-term corrective measures as needed.

Descriptions of proposed activities to accomplish the Phase I objectives are discussed in the following sections.

#### 5.1 CONCEPTUAL MODEL

A conceptual model of hypothetical pathways and driving forces that would be required to account for the occurrence of tank farm related constituents in groundwater will be developed as the first step in the Phase I investigation. This is also the initial activity required for applying the DQO process. For this purpose, the conceptual model for the WMA S-SX (Caggiano et al. 1996) will be modified as necessary to accommodate different source term characteristics and hydrogeologic conditions at WMA B-BX-BY.

#### 5.2 EVALUATION OF EXISTING DATA

As indicated in Figure 2, existing data will be reviewed to determine if information is adequate for a first determination to support the false

positive claim. Specific data and information that will be required and evaluated for this purpose are as follows.

Driving Force Evaluation. Possible driving forces that could account for the occurrence of tank farm constituents in groundwater will be evaluated. This will consist of first reviewing the status of water distribution lines near the SST's to ensure there are no potential sources of water in or adjacent to the SST's. Proximity of water lines to adjacent cribs and trenches will be noted as well. If active water lines are identified, the water purveyor will be contacted and alternatives will be explored for either rerouting or eliminating this potential driving force. Other sources of water include enhanced natural infiltration due to cover type and depressions or other topographic features. Such conditions will be noted and mapped to the extent possible. Based on this review, the solute transport modeling performed for the WMA S-SX assessment plan could be modified to accommodate differing conditions at WMA B-BX-BY.

The information from this task will be used to assess the likelihood that tank waste constituents in the soil column could reach groundwater at a rate and over a period consistent with the observed trend in co-contaminants in downgradient monitoring wells.

Source Term. Evaluation of waste composition based on available SST System sampling results and on process chemical knowledge will be conducted to identify the most likely mobile constituents that potentially could migrate to groundwater from a tank leak. The source term will be evaluated by reviewing available data on discharges (dates, volumes, constituents) to SSTs in WMA B-BX-BY and to cribs, trenches, reverse wells, and french drains surrounding WMA B-BX-BY. Waste handling and treatment processes for tanked versus cribbed waste (especially any fractionation of the waste into components that were discharged to different types of facilities) will be reviewed and evaluated.

Mobile Co-contaminant Analysis. Co-contaminant ratios for SST waste, as identified in the source term evaluation, will be compared with observed ratios in groundwater. Concordance between source term ratios and ratios observed in groundwater would indicate there is a tank farm source (or an adjacent crib source that intentionally received liquid waste from the tank farm). The ratios  $^{99}\mathrm{Tc/U}$  and  $^{3}\mathrm{H/^{99}Tc}$  have been used to indicate that two contaminant populations (one from cribs and another from tanks) are present in groundwater at WMA S-SX and these approximate fractionated components of the waste that leaked or was discharged to soils (Caggiano et al. 1996). Similar analyses will be performed for WMA B-BX-BY to determine whether different populations of groundwater contaminants could be present and whether these can be attributed to different sources.

Near Field Plume Maps. Areal contaminant distribution patterns will be evaluated in the vicinity of the tank farms. Available groundwater data will be contoured to produce plume maps to the extent possible. Plume maps might provide clues to groundwater flow direction/source relationships and if there is evidence of more than one plume source. For example, there are some trends apparent in a few constituents (specific conductance, nitrate, chloride, technetium-99) in downgradient wells 299-E33-32 and 299-E33-43 that are not present in other downgradient wells at WMA B-BX-BY. These differences imply

that different contaminant populations might be present and that a contaminant plume from a localized unknown source might be impinging on these wells. This information could be used to either reject the tank farm as the source or to identify alternate sources such as adjacent cribs. However, if there is inadequate well coverage, supplemental sampling might be needed.

Groundwater Flow Direction. Water level data and water table maps will be compiled to determine the present direction of groundwater flow as it might affect the distribution of contaminants. To the extent possible, the borehole velocity flowmeter will be run in key wells at different levels in the well screen to determine actual direction of groundwater flow. Data on groundwater flow direction and velocity will be used to compare the plume maps and changes in the distribution patterns with time. Wells in the RCRA monitoring network (and some beyond the immediate area of WMA B-BX-BY) will be resurveyed to a common datum to provide consistent top of casing elevations. The present geodetic surveys of wells were performed at the completion of well construction in three different years using different field crews and bench marks and these differences could account for some of the scatter in water level data (refer to hydrograph on Figure 5).

New geodetic survey elevations for the top of casing will be obtained, along with a water table map showing the present configuration of the water table and estimated groundwater flow direction. Tables and plots illustrating the interpretation of groundwater flow direction and velocity will be prepared for the assessment report. Any differences in the direction of flow with depth in the screens also will be plotted to determine whether any changes in flow direction might help explain the distribution of contaminants in relationship to a tank farm source or an alternative.

#### 5.3 NEAR-TERM DECISIONS TO BE MADE

The DQO process will be used to design a cost efficient short-term sampling program (if required) based on the outcome of the review of existing data. Even if no new data are required, the DQO logic process will be used to address the following key questions or decisions:

- Are mobile co-contaminants in downgradient groundwater consistent with a SST source?
- Is the pattern observed in key well 2-E33-32 consistent with flow directions and an SST source? (i.e., is there an alternative source other than SSTs?).

The same general process and test parameters as described in WMA S-SX assessment plan (Caggiano et al. 1996) will be followed. The product of the DQO process will be a sampling and analysis plan (SAP) to guide the acquisition of any additional or new data needed to address the key decisions.

#### Decision Rule

The expected mobile constituents in SST waste that could be transported through the soil column to groundwater include, but are not limited, to the constituents listed in Table 1.

Table 1. Mobile Constituents Expected in Groundwater if Single-Shell System Tank is the Source.

Mobile constituent (chemical form)	Comments
Chromate (CrO <sub>4</sub> <sup>2-</sup> )	Might be present because of REDOX waste transferred to B-BX-BY tank farm
Technetium-99 (TcO <sub>4</sub> <sup>-</sup> )	Common fission product in all SST System waste
Nitrate (NO <sub>3</sub> <sup>-</sup> )	From multimolar nitric acid used in dissolution of irradiated fuel
Chloride (Cl <sup>-</sup> )	A co-contaminant in the sodium hydroxide used to neutralize the nitric acid
Fluoride (F <sup>-</sup> )	Used in a chemical separation step in the bismuth phosphate process
Cobalt-60 (as Co <sup>2+</sup> in CN <sup>-</sup> complex)	Normally immobile but formed anionic complex with cyanide used to separate strontium/cesium from waste stream before discharge to cribs and trenches

These constituents could be extended or modified depending on available SST System sampling results and inferences from process knowledge (Agnew 1995).

Rule Number 1. If the expected mobile co-contaminants are covariant in the downgradient monitoring well(s), and approximate their relative concentrations (e.g., ratio of constituent to technetium-99 or nitrate) in soluble fractions of tank waste, this will be taken as evidence of a SST (or related) source. An affirmative result for the contaminant consistency test, however, would not be conclusive evidence of a tank farm source because similar waste also was discharged to adjacent trenches and cribs.

Rule Number 2. The groundwater flow direction in relation to potential source locations is critical for distinguishing between an SST System source and a crib source. Flow velocity and direction (based on in situ measurements) in at least well 2-E33-32, and inferred flow directions based on contaminant plumes, will be used to determine if the monitoring well lies within a likely

contaminant dispersion corridor from any upgradient SST. An affirmative for both rules 1 and 2 would implicate the tank farm as a source and the decision would be made to proceed to Phase II. The Phase II step also would be initiated in the case of an affirmative result for rule 1 and an inconclusive result for rule 2.

#### 5.4 DELIVERABLE

A report summarizing the findings of the Phase I effort will be prepared and submitted within 3 months following completion of the 3- to 6-month investigation. A detailed description of the content of the Phase I report is provided in Section 7.0.

#### 6.0 OUALITY ASSURANCE PROGRAM

Groundwater sampling procedures, sample collection documentation, and chain-of-custody will be performed in accordance with onsite standard operating methods.

#### 6.1 SAMPLING PROCEDURES

All field sampling activities will be recorded in the proper field logbook. Before sampling each well, the static water level will be measured and recorded. Based on the measured water level and well construction details, the volume of water in the well will be calculated and documented on the well sampling form or field notebook. Each well will be purged until the approved criteria are met. Purgewater will be managed according to the Purgewater Monitoring Plan [Attachment 5 of the Hanford Facility RCRA Permit (Ecology 1994)]. If a well pumps dry because of very slow recharge or low water levels, samples will be collected after recharge.

Overall quality assurance (QA) program requirements are defined by onsite programs and Article 31 of the Hanford Federal Facility Agreement and Consent Order (Ecology et al. 1996). The RCRA sampling and analysis program is presently transitioning to Pacific Northwest National Laboratory (PNNL). Equivalent PNNL procedures will be used as applicable and relevant for preservation of samples and chain of custody.

#### 6.2 ANALYTICAL PROCEDURES

Procedures for field measurements (e.g., pH, conductivity, etc.) are specified in the user's manuals for the meters used. Most of the analytical methods (WHC 1995) are selected from those provided in SW-846 (EPA 1992). For constituents with no analytical method specified by SW-846, other methods will be selected by PNNL.

#### 7.0 PHASE I ASSESSMENT REPORT

After completing Phase I investigations, all data will be compiled, analyzed, interpreted, and reported in a Phase I assessment report. The objective will be to determine whether the SSTs in WMA B-BX-BY have had any significant effect on groundwater quality. If the SSTs in WMA B-BX-BY have had no impact on groundwater quality, the site will return to interim status detection-level monitoring. If the analysis indicates that groundwater could have been impacted, a Phase II investigation will be planned and implemented contingent on the results of the Phase I investigation. Phase II, if needed, likely would expand on the investigations conducted for Phase I to provide additional information/data for a more complete analysis. Phase II investigations would be incorporated into TWRS characterization of the nature and extent of waste in the vadose zone beneath the tank farms to facilitate remediation/closure. Data obtained in Phase I assessment investigation will be used to guide and/or support operational decisions affecting tank farm operations and the repair and/or maintenance of utility lines.

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## APPENDIX A

## REVIEW OF SOURCE FACILITIES/PROCESSES

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APP A-ii

#### APPENDIX A

#### REVIEW OF SOURCE FACILITIES/PROCESSES

The SSTs in WMA B-BX-BY are part of the SST System, a RCRA treatment, storage and/or disposal (TSD) unit that stores mixed waste remaining from the chemical processing of spent fuel rods to recover and refine weapons grade plutonium and uranium. No waste has been added to these tanks since November 1980, and many ceased receiving waste earlier than 1980 because of failed integrity (refer to Table H-1 in Hanlon 1996). All the SSTs will be closed as RCRA TSD units under WAC 173-303-610. A closure work plan for the SSTs was submitted to Ecology in 1989; revision A of this plan was submitted to Ecology in June 1995, and revision 1 incorporating Ecology comments was submitted in June 1996 (DOE/RL-89-16). The WMA B-BX-BY is coincident with Comprehensive Environmental Response, Compensation, and Liability Act of 1980 200-BP-7 operable unit. Anderson (1990) documents the history of tank farm operations. Chemical and radioactive waste inventories of SSTs are documented (WHC 1993).

High-level waste streams from the processing of spent fuel rods, mostly using the bismuth-phosphate process in B Plant were discharged to various tanks in WMA B-BX-BY. Records (Anderson 1990) indicate that some REDOX, tributyl phosphate, and hot semi-works waste was transferred to different tanks in WMA B-BX-BY at some point in their history. The waste was discharged to the SSTs as alkaline slurries, with pH increased to above 9 by the addition of NaOH before release of the waste to tanks. These tanks also were used in the uranium scavenging operations from 1954 to 1957. Uranium originally discharged to these tanks as waste from BiPO4 operations was recovered and processed for use as a special nuclear material (Gerber 1993), with high-level waste returning to SSTs for storage and precipitation. Potassium ferrocyanide was added to the tanks to precipitate cesium-137. Most of the strontium-90 also precipitated in the tanks, initially unassisted and later with the addition of either calcium or strontium nitrate. Supernatant from this process was discharged to the 216-BY cribs (200-BP-1) or the 216-BC cribs, or to specific retention trenches 216-B-35 through 216- B-42 located west of the 241-BX Tank Farm. Liquid effluent facilities surrounding WMA B-BX-BY are listed on Table Al.

All the SSTs in WMA B-BX-BY are constructed of reinforced concrete with a single liner of ASTM A283 Grade C carbon steel. The 100 series of tanks are all 75 feet in diameter and are buried from 6 to 8 feet below ground surface. The cylindrical tank beneath the domed top of each tank extends to varying depth depending on the capacity of the tank and its position in a cascade sequence. Smaller 200-series tanks are 20 feet in diameter and held 55,000 gallons, but these are found only in the original four tank farms (241-B is one of the original tank farms,). Twelve (of 16) SSTs in the 241-B Tank Farm are 100-series tanks, each of which held 530,000 gallons and were constructed in 1943 and 1944. There are also four 200-series tanks in the 241-B Tank Farm. Ten (of 16) tanks in the 241-B Tank Farm are 'assumed leakers'. The 12 SSTs in the 241-BX Tank Farm are all 100-series tanks, each of which held 530,000 gallons, and were constructed in 1946 and 1947. Five of

the 12 tanks in the 241-BX Tank Farm are assumed leakers, including the 241-BX-102 tank, which leaked an estimated 70,000 gallons in 1971 [the second largest known Hanford Site tank leak (Womack and Larkin 1971)]. The 12 100-series tanks in the 241-BY Tank Farm were constructed in 1948 and 1949, with each holding 758,000 gallons. Five tanks in the 241-BY Tank Farm are classified as assumed leakers. All the 100-series tanks in each of these farms have a dished bottom; i.e., a curving intersection of the sidewall and bottom. Only the 241-B Tank Farm contains the smaller 200-series tanks.

All of the tanks in the 241-B, 241-BX, and 241-BY Tank Farms were constructed such that waste could flow laterally (i.e., cascade) through connecting pipes from one tank into another once waste exceeded the level of the cascade line in a tank. Waste would be placed initially in the first tank and allowed to cascade to the other two tanks in a cascade line. There were four rows of cascading tanks (three in each line) in each of the 241-B, 241-BX, and 241-BY Tank Farms. In addition, the end tank in a cascade in the 241-BX Tank Farm was plumbed such that waste could cascade from the BX Tank Farm to the first tank in a cascade line in the BY Tank Farm. Thus, the 241-BX-103 tank would cascade to 241-BY-101; BX-106 tank would cascade to 241-BY-104, etc.

Cascade lines connecting groups of tanks were plugged on several occasions and also were not sealed adequately at the junction with tanks (cascade lines were welded to the liner), thereby leading to escape of waste from containment. Waste went from processing plants through settling tanks and diversion boxes to the SSTs and was directed to various tanks by valves allowing flow of waste along transfer lines coming out of diversion boxes. There are several sets of diversion boxes in WMA B-BX-BY, with transfer lines emanating from each to the various tanks. None of the transfer lines were double contained and leaks were known to have occurred along each. As with cascade lines, the junction of lines with the tank either was not properly sealed or developed leaks during operations, for these intersections were routes of egress of waste from tanks to the soil. Leak testing of the tank liners during construction was performed after welding of the constituent plates was completed and the liner was finished. Photos of the tanks under construction reveal this process, but no evidence of additional testing of the tanks was found to indicate additional testing after the cascade and transfer lines were plumed into the tanks.

#### MONITORING THE SINGLE SHELL TANKS

#### Historic Surveillance

The SSTs were monitored to detect leaks using in-tank measurements of liquid levels and gross gamma surveillance logging in external boreholes (Welty 1988). A drop of liquid levels between successive readings would signify possible loss of fluids which, if not explained by other phenomena, suggested a loss of integrity of the tank. Gross gamma logging in radially disposed boreholes adjacent the tanks (refer to Figure 9 in text) was used to confirm the loss of liquid from a tank and/or to monitor the movement of fluids once escaped from a tank. Any sudden change in the amplitude or depth of an above-background peak was cause for suspicion about failed integrity and would trigger further study. Once declared to be leaking, waste would be

pumped from the subject tank to other sound SSTs or double-shell tanks and the tank would await interim stabilization.

#### Current Monitoring Program

Spectral gamma logging is now conducted in boreholes surrounding the Spectral gamma logging can be used to identify and quantify the specific gamma-emitting isotope present at a given level in a borehole. Spectral gamma logging in the SST System is being conducted by RUST Geotech contracted directly to DOE-RL. In logging these boreholes, 100-second counting times at increments of 0.5 foot are taken in each borehole. These data are reduced, interpreted, and plotted as continuous logs in individual tank data reports (refer to list of reports for the 241-BY Tank Farm at end of references) for baseline logging. Results of logging in the BY Tank Farm are summarized on Table A2. Cesium-137, antimony-125, and cobalt-60 are the principal anthropogenic isotopes that have been identified in boreholes in the BY Tank Farm and represent some of the waste that has escaped these tanks. Ruthenium-106, with a half life of 1.02 years, has been used to monitor the depth of penetration of waste in tank farms and certainly was among some of the short half-life isotopes that were present in the waste discharged to WMA B-BX-BY. Like many of the short-lived isotopes, ruthenium-106 has decayed to ground state and can no longer be detected. However, some of the high gross beta levels in groundwater from historic data are likely the result of the presence of this isotope in groundwater, as it is very mobile.

# Waste Migration

Once waste escaped containment, natural and artificial recharge has enhanced mobility and led to deeper infiltration of the waste. The proportion of natural recharge that infiltrates beneath the top few feet is not known with any precision. Where coarse cover materials have been placed as cover materials and vegetation is prohibited (as has been true for tank farms), natural precipitation (mean annual is 6.25 inches per year) could infiltrate deeper than in areas covered with finer soils and vegetation (Gee et al. 1992). By severely restricting evapotranspiration through placement of gravel and restricting vegetation, recharge from natural precipitation is enhanced. The domed roof of each tank serves to collect and channel infiltrating liquids along the tank margins where both unsealed boreholes and leaked waste could be present. Natural recharge can be further enhanced through other preferential pathways that channel infiltration deeper into the vadose zone. For example, unsealed boreholes in the WMA B-BX-BY might have assisted the further infiltration of natural and artificial recharge. Sudden melting of snowcover following prolonged periods of subfreezing weather have occurred during several winters since the 1940s when these tanks were constructed. Chinook winds rapidly melt snow producing meltwater that cannot infiltrate into frozen substrate. This phenomenon leads to ponding of water in tank farms that can preferentially infiltrate along unsealed boreholes and/or clastic dikes. Water also has been indiscriminately added to the soils in and around tank farms through hydrocompacting of fill in newly excavated trenches and through leaks in raw and sanitary water distribution lines.

Lateral and vertical spreading of artificial recharge (discharge of liquid effluent to surrounding cribs and french drains) also has assisted in mobilizing and transporting waste that has escaped containment. A well documented case of such phenomena occurred in the 200 West Area when effluent discharged in 1985 to the 216-U-16 crib served to mobilize uranium previously discharged to the 216-U-1 and 216-U-2 cribs (Law and Schatz 1986). Uranium eventually was recovered through extraction, pumping, and treatment of contaminated groundwater by an ion exchange process.

Lateral spreading of fluids discharged to soils is enhanced by stratification in the sediments. Not only are there significant differences in unsaturated hydraulic conductivity between various units of the Hanford formation, but also between superposed sedimentation units within the formation. Thin and discontinuous beds/lenses of mud-rich units are present in the various cyclic sedimentation units in the Hanford formation and these favor lateral spreading. Lateral spreading waste also can encounter other preferential pathways (e.g., unsealed boreholes, wells, clastic dikes) that can enhance vertical infiltration and short circuit natural interstitial infiltration.

#### INTERIM STABILIZATION

A program of interim stabilization has been instituted in the SST System. The objective of interim stabilization is to minimize the risk of further leaks by removing as much liquid from the tanks as possible. All but three of the 40 tanks in WMA B-BX-BY have been interim stabilized. Only BY-103, BY-105, and BY-109 remain to be stabilized (Hanlon 1996). The 241-BY 103 and 241-BY-105 tanks are assumed leakers.

Liquid Effluent Facilities Surrounding Waste Management Area B-BX-BY.

Table A1.

Facility	Туре	Operating Dates	Volume (gals.)#	Waste Type##	Nitrate (kg)	Ammon. Nitrate (kg)
acinty	1100					
216-B-7A & B	Crib	10/46 - 5/67	11,519,200	Effluent from 224-B (via settling tank), cell drainage from 221-B and decon waste from 22	1,800,000	22,000
		4/48 - 7/53	7,186,262	2nd cycle supernatant, cell drainage from 221-B; decon waste from 224-B	1,400,000	160,000
216-B-11A & B			7,820,340	Process condensate from 242-B Evaporator	NA	NA
216-B-35**	Trench+		280,000	1st cycle supernatant from 221-B	90,000	
	Trench+		510,000	1st cycle supernatant from 221-B	160,000	
	Trench+		1,140,000	1st cycle supernatant from 242-B Evaporator	1,700,000	
216-B-38**	Trench+	7/54 - 7/54	380,000	1st cycle supernatant from 221-B	120,000	
216-B-39**	Trench+	12/53 - 11/54	390,000	1st cycle supernatant from 221-B	120,000	
216-B-40**	Trench+	4/54 - 7/54	430,000	1st cycle supernatant from 221-B	210,000	
216-B-41**	Trench+	11/54 - 11/54	380,000	1st cycle supernatant from 221-B	2,100,000	
216-B-42**	Trench	1/55 - 2/55	396,301	Scavenged TBP supernatant from 221-U	210,000	NA
216-B-43**	Crib	11/54 - 11/54	560,106	Scavenged TBP supernatant from 221-U	400,000	NA
216-B-44**	Crib	11/54 - 3/55	1,479,520	Scavenged TBP supernatant from 221-U	800,000	NA
216-B-45**	Crib	4/55 - 6/55	1,299,870	Scavenged TBP supernatant from 221-U	90,000	NA
216-B-46**	Crib	9/55 - 12/65	1,770,150	Scavenged TBP supernatant from 221-U	1,200,000	NA
216-B-47**	Crib	9/55 - 9/55	980,185	Scavenged supernatant from 221-U	700,000	NA
216-B-48**	Crib	11/55 - 11/55	1,080,580	Scavenged TBP supernatant from 221-U	1,000,000	NA
216-B-49**	Crib	11/55 - 12/55	1,770,150	Scavenged TBP supernatant from 221-U	1,500,000	NA
216-B-50	Crib	1/65 - 1/74	14,478,200	Storage tank condensate from ITS#1 in 241-BY Tank Farm	1,500	10,000
216-B-51	French Drain	1/56 - 1/58	264	Flush drainage from BC Crib pipeline	190	NA
216-B-57	Crib	2/68 - 5/73	22,298,500	Storage tank condensate from ITS#2 in 241-BY Tank Farm	_	
NOTES					L	<del> </del>
*Ru-106 was a	mong the original	radionuclides disc	harged to these fa	cilities, but it has decayed to non-detectable levels in soils and groundwater (half life of 1.02	yr)	
** Eacility recei	ved high-salt was	te			<u> </u>	
+ Specific reter	ntion trench (i.e., f	luid added to trenc	h until calculated	specific retention equalled)		<u> </u>
# Volume estin	nates from WIDS	T				
##All facilities	received Cs-137, 5	Sr-90, Pu and U		<u> </u>		٠

APP A-T1

Table A2. Summary of Spectra-Gamma Logging Results in the BY Tank Farm. (sheet 1 of 3)

ank No.	Tk. Farm No.		Constructed	Diam.	Depth (ft.)	Surface Contam.	Cs-137 Contamination	Co-60 Contam.	Sb-125 (or other) Contam.	Detector Sat.
		No.		(in.)	(10)					1
	00.04.04	E33-176	12/22/71	-	100	0 - 35'; <110 pCi/g)	<2 pCl/g; 35 - 98'	NO		No
BY-101	22-01-01		4/31/74	2	100	0 - 20'; <20 pCi/g	<0.9 pCi/g; 28 - 32'	IND		No
	22-01-03	E33-245 E33-177	12/20/71	6	100	0 - 33'; <120 pCi/g	<120 pCi/g @ 25'; ,20 p(Ci/g @ 31'	28 - 55, peak ,2 pCi/g @ 29'; <0.5 pCi/g @ 70 - 82'		No
	22-01-04	E33-177	12/20//1	ľ	100	0 - 35, 1120 polig	1120 poug @ 20 , ,20 p(oug @ 01	1		ľ
	22 21 27	E33-178	12/16/71	6	100	0 - 43'; <300 pCi/g	10 pCi/g @ 11.; 3 pCi/g @ 23'; 1 pCi/g @100'	1 - 2' <3 pCi/g; <0.5 pCi/g @46 & 50'		No
	22-01-07		5/7/74	6	100	0 - 99"; <80 pCi/a	<30 pCi/g @21 & 28"; <10 pCi/g @100"	ND		No
	22-01-10	E33-246	5/1/14	P	1100	0 - 33 , 400 pcsg	too poug (gz i u zo, 110 poug (g iou			
77. 100	22-02-01	E33-101	7/10/70	6	100	0 - 100'; <100 pCi/g	<300 pCi/g @ 44 - 52; <3 pCi/g @60';	<0.6 pCi/g @ 83 - 99'		No
3Y-102	22-02-01	E33-101	7710770	ľ	1,00	0 - 100, -100 pong	<4 pCi/g @ 100'	,,	1	
	22-02-02***	E33-227	10/27/73	6	100	0 - 37; <200 pCi/g	Spotty >37; <1 pCl/g	ND		No
	22-02-05	E33-228	10/16/73	6	100	0 - 38'; <200 pCi/g	Spotty <1 pCVg . 38'	ND		No
	22-02-05	E33-9++	7/31/49	8.4	275	0 - 00, 1200 posg	openy 11 pergree			
	22-02-07	E33-102	9/2/70	6	100	0 - 100': <30 pCi/q	<2 pCi/g @ 45'; <1 pCi/g @100'	<1 pCi/g @24 - 25'; <2 pCi/g @31 - 50';		No
	22-02-09+++	233-102	3/2/10	Ľ.	100	0 - 100, 100 poug	20038 10, 1,003	<0.5 pCi/g @61 - 63		-
BY-103	22-03-01	E33-104	8/7/70	6	100	0-96"; <100 pCi/g	<100 pCl/g @0 - 10'; continuous to bottom	ND		No
				1			<2 pCVg >10'			
	22-03-04	E33-211	12/5/72	6	100	0-31'; <400 pCi/g;	<1 pCi/g @ 35 - 39'; <1 pCi/g @ 45 - 50'; <2 pCi/g @ 101'	<1 pCi/g @ 45 - 60'; <1.5 pCi/g @ 66 - 81'; <1 pCi/g @ 101'	<1.5 pCi/g @ 50 - 52	No
	22-03-05	E33-103	8/12/70	6	100	0 - 100°; <1,100 pCi/g	10 ->1,000 pCl/g 0 - 100'	<10 pCi/g @46 - 100'	ND	Yes
	22-03-03	200-100	10,12,10	ľ						24 - 45'
	22-03-06	E33-210	12/22/72	6	100	0 - 58": <400 pCi/g	Continuous 10 - ~200 pCi/g 0 - 25'; >25',	<1.1 pCi/g 41 - 47"; <0.5 pCi/g 78 - 99";	<6 pCi/g	No
	22-03-00	200.210	1.020.2	ľ			peaks of <5 pCl/g 30 - 35'; <100 pCl/g@ 41 - 50	<2 pCi/g @ 100*	@ 42 - 48'	
	22-03-07	E33-242	12/17/73	6	100	0 - 23" <100+ pCi/g	Spotty @31, 50, and 100 ' < 1 pCi/g	52 - 95'; <0.5 pCi/g	ND	No
	22-03-08	E33-244	12/6/73	6	100	0 - 12; <50 pCi/g	<3 pCi/g @ 19 - 25'	<0.5 pCi/g @ 45 - 51"; <0.4 pCi/g @90 - 97"	ND	Nο
	22-03-09	E33-105	8/6/70	6	100	0 - 40": <80 pCi/g	1 - 10 pCi/g @ 0 - 32'; 11 pCi/g peak @ 16';	< 1 pCi/g 5 - 8'; spotty ,1 pCi/g 30 - 50';	ND	No
	22.00			1	l'	1	spotty < 2 pCl/g >32' (Eu-154 <3 pCl/g 5 - 7')	<11 pCi/g 61 - 98'		
	22-03-10	E33-243	12/7/73	6	100	0 - 50'; <40 pCi/g	Broad peaks 1 - 10 pCl/g @ 14 - 50'; spotty < 1 pCl/g. 50'; <2 pCl/g @ 100'	ND	ND	No
	<u> </u>				I					
BY-104	22-04-01	E33-106	9/2/70	6	100	0- 100'; <90 pCl/g	Peaks 90 pCi/g @0 " <11 pCi/g @ 100";	ND	ND	No
				1	l		0.5 - 10 pCi/g continuous 1 - 98'		ļ	
	22-04-05	E33-107	7/21/70	6	100	0 - 38'; <6 pCl/g	Spotty <0.5 pCi/g >40'; <2 pCi/g 95 - 98'	ND	ND	No
	22-04-07	E33-248	5/13/74	6	100	0 - 35'; <40 pCl/g	Few detections < 0.5 pCi/g > 35'	<3 pCl/g 90 - 100'	ND	No
	22-04-09#	E33-108	8/31/70	6	125@	0 - 60"; <40 pCi/g	Spotty >60'; <0.5 pCi/g	<10 pCVg @ 86 - 125	ND	No
	22-04-11	E33-249	6/1/74	6	100	0 - 44'; <100 pCVg	Broad peak 1 - 10 pCl/g @ 11 - 36'; <7 pCl/g 38 - 43'; few detections <0.5 pCl/g > 44'	<3 pCl/g @99 - 100'	ND	No
								CO 6 nCt/n @ 04 00!	ND	Yes
BY-105*	22-05-01	E33-109	7/9/70	6	100	0 - 41'; >100 pCi/g	<1 pCl/g 8 - 41'; <1 pCi/g 50 - 61'; <2 pCi/g @ 98'	<0.6 pCl/g @ 84 - 98'	IND	(0 - 3')
	ļ		<b> </b>	I	1.00	@ ground surface	Continues 12 - City OF DELICE POUR OF DO	ND	ND	No.
	22-05-05	E33-110	7/15/70	6	100	0 - 97; <25 pCl/g	Continuous <2 pCi/g @5 - 95'; <5 pCi/g @ 96'	<1 pC/g 61 - 70'; <1 pC/g 75 - 96';	ND	No
	22-05-09	E33-111	7/27/70	6	100	0 - 45" <9 pCi/g	<2 pCi/g 4 - 45'; few detections >45'; ,1 pCi/g @ 98'	<5 pCi/g 95 - 98'	NO	140
				<u> </u>				115-01-0-10-10-11-01-0-55-01	ND.	- Nia
BY-106*	22-06-01	E33-112	8/3/70	6	100	0 - 99'; <70 pCi/g	<2 pCi/g @ 5 - 98"; 1 pCi/g peaks @ 36 & 45"; <6 pCi/g 98 - 99"	<1.5 pCi/g@ 46 - 49"; <1 pCl/g @ 55 - 64"	ND	No
	22-06-05	E33-113	7/14/70	6	100	0 - 38'; <50 pCi/g	Few detections >40'; <1 pCi/g	<11 pCi/g @28 - 87'; broad peak <2 pCi/g @ 63 - 82'	ND	No
	22-06-07**	E33-86	8/31/49	7	150	0 - 28"; <80 pCi/g	Continuous 38' - 131'; peaks : 5pCi/g @45';	Continuous 56 - 82'; peaks 1.5 pCl/g @57';	ND	No
				4	1		<11 pCi/g @49"; 10 pCi/g @74"; 6 pCi/g @ 95"	2 pCi/g @ 70": <0.5 pCi/g @ 126 - 130" Spotty detections <0.25 pCi/g @72 - 90"	ND	No
	22-06-09	E33-114	7/31/70	6	100	0 - 32; <50 pCi/g	Nearly continuous <1 pCi/g @38 - 96'		ND ND	No
	22-06-11	E33-250	5/3/74	6	100	0 - 38" <25 pCi/g	Few detections <0.6 pCi/g @ 44-48'; 60'	ND	INU	INO
						1		14 - CV- C4C - C4b	LUD	Na
BY-107*	22-07-01	E33-115	8/25/70	6	100	0 + 99'; <246 pCi/g	<3 pCi/g continuously @12 - 99"; <6 pCi/g @98 - 99"	<1 pCl/g @46 - 51'; continuous 56 - 97'; <7 pCl/g, broad peak 59 - 86'	ND	No
	22-07-02	E33-206	1/5/73	6	100	0 - 40'; <11 pCi/g	<0.8 pCi/g @37 - 44'; 45 - 96' scattered detections <1 pCi/g; <3 pCi/g @ 96 - 100'	<1 pCi/g 1 - 7'; few detects <0.5 pCig @ 31 - 41'; continuous 48 - 100', <10 pCi/g	ND	No

Table A2. Summary of Spectra-Gamma Logging Results in the BY Tank Farm. (sheet 2 of 3)

Tank No.	Tk. Farm No	No.	Constructed	Diam. (in.)	Depth (ft.)	Surface Contam.	Cs-137 Contamination	Co-60 Contam.	Sb-125 (or other) Contam.	Detector Sat.
	22-07-05	E33-116	7/23/70	6		0 - 31'; <12 pCi/g	Scattered detects <1 pCi/g @ 34 - 97	Scattered detects <1 pCi/g @28 - 39'; continuous <1 pCi/g 41 - 55'; broad peak <8 pCi/g 57 - 98	ND	No
	22-07-07	E33-251	5/8/74	6	100	0 - 36'; <50 pCi/g	Continuous <1 pCi/g @ 3 - 42';<2 pCi/g @ 100'	Scattered detects <0.5 pCi/g @ 41 - 43', 59 - 61', 66'; broad peak @86 - 99' <3 pCi/g	ND	No
	22-07-09	E33-117	8/25/70	6	100	0 - 100'; <200 pCl/g	10 -100 pCl/g @ 0 - 33', peak 3,000 pCl/g @24'; 10 pCl/g @35'; broad peak <5 pCl/g @ 42', continuous <1 pCl/g to 100'	<0.5 pCl/g 40 - 41'; Broad peak <8 pCl/g 77 - 100'	ND	No .
	22-07-10	E33-252	7/31/70	6	100	0 - 44'; <150 pCi/g	10 - 100 pCi/g @ 0 - 18' & 21 - 40'; <2 pCi/g @ 60 - 69"; few detects >70';	ND	ND	No
	20 00 04	E33-118	7/22/70		100	0-36'; >10 pCi/g	Continuous surface to 36'; 0 - 8' 1 - >10 pCl/g; 8 - 36';	Continuous 28 - 41', <5 pCl/g; <11 pCl/g 44 - 99';	ND	Yes
3Y-108*	22-08-01	E33-110	112210	•	100	i	few detects 36 - 94'; <1 pCi/g; <1 pCi/g 98 - 100'	peaks @ 43' (4 pCi/g) & 56' (<11 pCi/g)		(2 - 4')
-	22-08-02	E33-208	1/9/73	6	103	0 - 51', >500 pCi/g	Continuous to 51°, 0 - 18° >1 pCl/g; <1 pCl/g 18 - 26°; >1 pCl/g 26 - 41°; <1 pCl/g 41 - 51°	Continuous 50 - 103", <1 pCi/g 50 - 68"; >1 pCi/g 68 - 71", <1 pCi/g 71 - 74', >1 pCi/g to 96"; broad peak @75 - 83" >10 pCi/g	ND	Yes (0 - 4")
	22-08-05	E33-119	7/20/70	6	100	0 - 44"; <70 pCi/g	Continuous 0 - 44", 0 - 3' > 10 pCl/g; 3 - 31' > 1 pCl/g; <1- pCl/g 31 - 44'; <1 pCl/g 49 - 52'; few detects 52 - 96'; <3 pCl/g 96 - 99'	Continuous 39 - 80'; >1 pCi/g 48 - 50', 56 - 58', 66 - 78'; <1 pCi/g 96 - 98'	ND .	No
	22-08-06	E33-207	1/31/73	6	100	0 - 40'; <100 pCi/g	Continuous 10 - 100 pCi/g 0 - 12', 1 - 10 pCi/g; 12 - 26' > 1 pCi/g; <1 pCi/g @26 - 40'; few detects > 40'	Spotty <0.2 pCl/g 3 - 11 & 50 - 56'; continuous 64 - 74' <4 pCl/g; 77 - 93' @ <1 pCl/g	ND	No
	22-08-07	E33-87**	8/17/49	8	150	0 - 4', <150 pCi/g	0 - 4'; >1 pCi/g; spotty detects <1 pCi/g @ 6 - 24'; continuous 39 - 90' mostly >1 pCi/g 39 - 69'; <1 pCi/g 70 - 98'; <2 p Ci/g @ 127 - 131'	<1 pCi/g @96 - 98*	ND	No
	22-08-09	E33-120	7/28/70	6	100	0-100'; >10 pCi/g 1 - 6'	>1 pCi/g 6 - 17'; <1 pCi/g 17 - 99'; <2 pCi/g 99 - 100'	ND .	ND	No
	22-08-12	E33-209	126/73	6	104	0 - 40'; 10 - 800 pCl/g @ 1 - 6'	>12 pCi/g 7 - 30'; <1 pCi/g 30 - 40'; few detects >40'	<1 pCVg @ 3-4; 0.1 - 8 pCVg 45 - 57; 0.1 - 3 pCVg @ 69 - 80*	ND	No
BY-109	22-09-01	E33-123	2/28/70	6	100 -	0 - 37'; <60 pCl/g	>1 pCl/g @ 0 - 8'; 0.2 - 1 pCl/g @ 8 - 38'; few detects <0.5 pCl/g 38 -96'; <2 pCl/g 96 - 98'	<0.5 pCVg @ 44 - 47'	ND .	No
	22-09-02	E33-259	6/10/74	6	100	0 - 49"; <200 pCl/g	10 - 200 pCi/g @ 0 - 31'; 10 - 100 pCi/g @ 31 - 40'; <1 pCi/g 49 - 49'; few detects <0.9 pCi/g 49 - 98'; <2 pCi/g 98 - 100'	Few spotty detections <0.1 pCl/g @ 70, 90, 92, and 96	ND	No
	22-09-05	E33-122	2/20/70	6	100	0 - 11'; <6 pCi/g	1 - 6 pCl/g @ 0 - 3"; <1 pCl/g 3 - 97"; 2 pCl/g @ 98"	2 detections <0.2 pCi/g @ 49 & 61'	ND	No
	22-09-07	E33-260	6/30/74	6	100	0 - 20'; <11 pCi/g	-1 - 11 pCi/g 0 - 13'; <1 pCi/g 13 - 20'; 1 detect > 20' @0.2 pCi/g	Continuous 25 - 60' @<2 pCi/g; peak 2.5 pCi/g @59", <1 pCi/g @ 66 - 73", <0.5 pCi/g 79 - 83"	NO	No
	22-09-08	E33-121	2/28/70	6	100	0 - 26'; <11,00 pCi/g	0.8 - 3 pCi/g @ 0 - 21"; 1 - 11,00 pCi/g @ 21 - 26"; spotty detections <1 pCi/g 29 - 61"; <0.8 pCi/g @ 98'	<1 pCVg @ 28 - 35'; 0.1 - 1.5 pCVg @ 40 - 51'; 0.2 - 2.5 pCVg @ 81 - 89'	ND	No
	22-09-11	E33-253	5/31/74	6	100	0 - 30'; <100 pCi/g	10 - 100 pCl/g @ 2 - 10";1 - 10 pCl/g @ 10 - 20*10 - 12 pCl/g @ 20 - 21", 1 - 10 pCl/g @ 21 - 25", <1 pCl/g @ 25 - 34", few detects >35" <0.5 pCl/g	Spotty detections <0.3 pCi/g @ 21 - 50'	ND	No
BY-110	22-10-05	E33-124	8/31/70	6	100	0 - 31'; <13 pCi/g	1 - 13 pCi/g @ 0 - 18'; <1 pCi/g @ 18 - 31'; few detections 31 - 98'; <2 pCi/g @ 98 - 99'	Continuous detections <0.5 pCi/g @ 48 - 76; <0.5 pCi/g @ 97 - 99'	ND	No
	22-10-07	E33-254	5/31/74	6	100	Missing data 0 - 22	1 - 3 pCi/g @ 22 - 30'; <1 pCi/g @ 30 - 33'; no detects >36'	0.1 - 0.5 pCi/g @ 48 - 60*	ND	No
	22-10-09	E33-255	5/31/74	6	100	0 - 20"; <5 pCi/g	Mostly >1 pCi/g 0 - 4'; <1 pCi/g @ 4 - 20' <0.5 pCi/g	ND	ND	No

APP A-12.

Table A2. Summary of Spectra-Gamma Logging Results in the BY Tank Farm. (sheet 3 of 3)

Tank No.	Tk. Farm No.	Hanford No.	Constructed	Diam.	Depth (ft.)	Surface Contam.	Cs-137 Contamination	Co-60 Contam.	Sb-125 (or other) Contam.	Detector Sat.
	22-10-10	E33-125	8/31/70	6		0 - 24'; <6 pCl/g	1 - 6 pCl/g @ 0 - 3'; <1 pCl/g @ 3 - 24'; few detects > 25' <1 pCl/g	<1 pCi/g @ 65 - 74'; <0.6 pCi/g @ 85 - 93'	ND	No
BY-111	22-11-01	E33-126	8/31/70	6	100	0 - 35'; <100 pCi/g; 10 - 100 pCi/g @ 0 - 8'	0.1 - 3 pCi/g @ 8 - 35'; peak <3 pCi/g @ 22 - 25'; few detects > 35' 0.2 - 8 pCi/g @ 95 - 101'	Scattered detects < 0.2 pCi/g @ 97 , 101	NO	No
	22-11-05	E33-127	8/31/70	6	100	0 - 36'; <200 pCi/g	10 - 200 pCl/g @ 3 - 6; 1 - 10 pCl/g @ 0 - 3', 6 - 10'; 0.4 - 2 pCl/g @ 10 - 36'; few detect >36'	<0.5 pCi/g @ 2 - 4'; <0.2 pCi/g @ 56 - 58'	<0.5 pCl/g Eu-154 @ 2'	No
	22-11-08	E33-56	12/31/44	6	100##	0 - 29'; <5 pCi/g	1 - 5 pCi/g @ 1 - 9'; <1 pCi/g 9 - 20'; 1 - 4 pCi/g @ 20 - 27'; <1 pCi/g 27 - 29'; few detects <0.6 pCi/g > 30'	ND	<12 pCi/g Pa-234 @62	No
	22-11-09	E33-128	8/31/70	6	100	0 - 21'; <8 pCi/g	1 - 8 pCi/g @ 2 - 5'; <1 pCi/g @ 5 - 31'; 0.05 pCi/g @ 100'	<0.2 pCi/g @ 3 - 5"; 1 - 3 pCi/g @ 26"; <1 pCi/g @ 27 - 56"	ND	No
BY-112	22-12-01	E33-100	11/30/67	6	1016	0 - 39'; <5 pCi/g	1 - 10 pCVg (M0stly) @0 - 8*; 1 - 3 pCVg @ 11 - 14*; 0.1 - 1 pCVg @ 24 - 39*; few detects > 40* (<1 pCVg); <5 pCVg @ 98 - 100*	Single detect <0.2 pC//g @ 100*	ND	No
	22-12-03	E33-94	11/30/67	6	100	0 - 46°; >1000 pCl/g	0 - 5' 10 - > 1000 pCl/g; 10 - 20 pCl/g @ 7 - 19'; <1 pCl/g @ 19 - 23'; 1 - 10 pCl/g @ 23 - 40'; <1 pCl/g @ 40 - 46'; few detects <1 pCl/g > 46'; 0.5 - 2 pCl/g @ 90 - 100'	0.1 - >100 pCl/g @ 0 - 5'; 1 - 11 pCl/g @ 6 - 8'; few detects <1 pCl/g @ 84 - 99'	0.1 ->1,000 pCi/g Eu-154 @ 0 - 5'; 0.3 - 25 pCi/g @ 7 - 9'	Yes (5 - 7')
	22-12-05	E33-95	11/30/67	6	100	Continuous 0 - 100; <50 pCi/g	1 - 50 pC/g @ 0 - 20";;<1 pC/g @ 21 - 26"; 1 - 4 pC/g @ 27 - 34"; <2 pC/g 34 - 100"; peak 4 pC/g @ 32"	1 detect <0.2 pCi/g @ 52	ND	No .
	22-12-06	E33-96	12/31/67	6	102	0 - 39'; <100 pCi/g	1 - 100 pCl/g @ 0 - 18'; <1 - 3 pCl/g @ 18 - 39'; undetected 40 - 98'; <1 pCl/g @ 99-100'	0.2 - 0.6 pCi/g @ 4 - 6'; scattered detects <0.2 pCi/g @ 57 - 62'	<1 pCi/g Eu-154 @ 4 - 6*	No
	22-12-07	E33-97	11/30/67	6	102	0 - 5'; <11 pCi/g	Few scattered detections > 5' < 0.7 pCi/g	ND	ND	No
	22-12-09	E33-98	12/31/67	6	102	0 - 21'; <11 pCl/g	<0.5 pCi/g @ 20 - 49'; undetected 49 - 99'; <4 pCi/g @ 100-101'	ND	ND	No
	22-12-10	E33-99	12/31/67	6	100	0 - 15'; <60 pCi/g	>1 pCVg @ 0 - 1'; 8 - 9'; <1 pCVg @ 9 - 99'; <2 pCVg @ 100'	ND	ND	No
BY Farm	22-00-01**	E33-85	8/3/49	8	150	0-101'; <12 pCi	Broad peak ,12 pCi/g @ 40 - 60"; <10 pCi/g 75 - 81"; <11 pCi/g @ 90 - 98"; <1 pCi/g 100-102"	ND	ND	No
	100 00 00	E33-240	12/7/73	6	100	0 - 16'; <400 pCi/g	Spotty 20 - 48'; <1 pCi/g; 1 pCi/g @ 100'	<0.5 pCi/g 50 - 60'; <2 pCi/g @65 - 97'	<1 pCi/g @52 - 53	No
<b>-</b>	22-00-02	E33-84	7/22/49	8	150	0 - 101'; <300 pCi/g	Continuous <20 pCi/g @ 5 - 101'; <1 pCi/g @ 141 - 146'	<5 pCi/g @ 45 - 146; peaks <12 pCi/g @ 124' & <5 pCi/g @ 137'	<5 pCVg @ 52 -72	No
<u> </u>	22-00-04	E33-241	12/12/73	6	100	0 - 35'; <12 pCl/g	Spotty >35", <20 pCi/g @95 - 100"	<0.6 pCi/g @56 - 86'	ND	
	22-00-05	L35-241	121213	1	1.50	S CC, III PONG	1			
<u> </u>	22-00-10**	E33-88	8/18/49	8	150**	0 - 5'; <6 pCi/g.	<7 pCVg @ 41 - 58'; <1 pCVg @ 67 - 68'; <2 pCVg @ 79 - 92'	ND	ND	No

#### NOTES

\* Tank is an assumed leaker

<sup>\*\*</sup> Screhole is perforated ~40 - 100'

<sup>\*\*\*</sup>Driller noted that samples at 35 and 45 ft. were "dripping wet"

<sup>+ 3</sup> ft. casing may have been welded to top of original casing, as borehole occurs in small bern.

<sup>++</sup> Well constructed as a groundwater monitoring well and remediated in 1978 with installation of 4 1/2 inch liner. Original casing perforated 252 - 262:

<sup>+++</sup> Samples collected from 26 - 51 ft showed contamination.

<sup>@</sup> Borehole deepened from 100 to 125 feet in 1983

<sup>#</sup> Some grout added to a part of the borehole

<sup>##</sup> Borhole originally drilled to 150 ft in 1944. May be grounted between casing strings of different diameter.

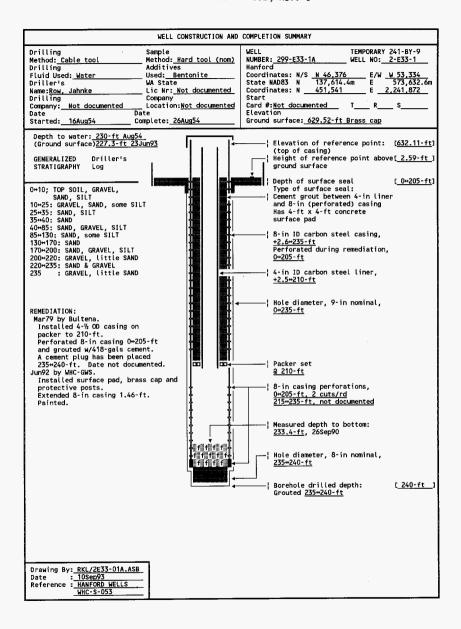
# WHC-SD-ENV-AP-002, Rev. 0

# APPENDIX B

# AS-BUILT DIAGRAMS OF SINGLE-SHELL TANK SYSTEM WASTE MANAGEMENT AREA B-BX-BY GROUNDWATER MONITORING WELLS

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APP B-ii



WELL DESIGNATION 299-E33-1A • SST-241-BY-Farm

RCRA FACILITY CERCLA UNIT

200 Aggregate Area Management Study (200-BP-1) N 46,376 W 53,334 [13Aug92-200E] N 451,540 E 2,241,871 [HANCONV] N 137,614.4m E 573,632.6m [13Aug92-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Aug54

240-ft

DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 233.4-ft, 26Sep90 230-ft Aug54; DEPTH TO WATER (GS) :

227.3-ft, 23Jun93 CASING DIAMETER

8-in carbon steel, +2.59+235-ft; 4-in carbon steel, \*+2.5+210-ft

632.11-ft, [13Aug92-NGVD'29] NOTE: 629.04-Tt before remediation 0+205-ft and 215+235-ft ELEV TOP OF CASING : ELEV GROUND SURFACE :

PERFORATED INTERVAL : SCREENED INTERVAL .

FIELD INSPECTION, 230ct89,

COMMENTS Carbon steel casing, (2).

2-ft round pad, no posts, capped, not locked. Brass cap in pad. FIELD INSPECTION, 17Jun92, 4 and 8-in carbon steel casings. Capped and locked.

4-ft by 4-ft concrete pad, 4 posts. Identification stamped on brass marker in pad.

In underground radiation zone. OTHER:

AVAILABLE LOGS : Driller

TV SCAN COMMENTS Depths referenced to ground surface;

07Nov89; Depth to bottom: 231-ft Bottom of casing: 231-ft

Depth to water: 219-ft Perforations began at 210 ft, 6 rd/ft. Scale/crud buildup below water level excessive making perforations indistinguishable. Some perforations were visible at bottom of casing. The camera travel knocked enough crud off casing on trip in that nothing could be seen coming out due to the murky water. This well requires

scrubbing and redevelopment.

20Sep90:

Depth to bottom: 233-ft, soft silty looking.

Depth to better 231.4-ft, some floating debris.

Perforations began at 211-ft, 6 per rd/ft. Those perforations visible were open.

Because of going from 4-in to 8 in casing, the 8-in didn't come real clean.

Most of the real heavy rust and scale has been removed. Water is clear.

13Nov90

DATE EVALUATED EVAL RECOMMENDATION :

PUMP TYPE

1. Remove existing 2-ft round concrete collar.

2. Install protective posts and concrete pad per WAC 173-160-510 and field conditions.

3. Survey to water level measurement standards.

SST monthly water levels measurement, 270ct54+23Jun93; LISTED USE

CURRENT USER WHC ER characterization,

WHC ES&M w/l monitoring and RCRA sampling, PNL sitewide sampling 93

Electric submersible, intake at 226.1.0-ft, (GS). 270ct89; Pulled electric submersible pump. No contamination encountered.

MAINTENANCE

O'Nov89; TV camera survey.
01bec89; Installed electric submersible pump.
10ulu90; Putlled submersible pump and scrubbed casing. Bailed debris.
30Aug90+05Sep90; Bailed and developed with pump to <5 NTU.

20Sep90; TV camera survey.

26Sep90; Set pump and installed new cap.

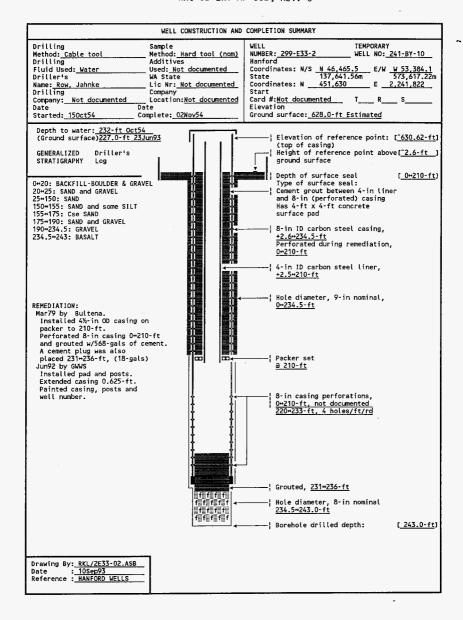
02-09Jun92 - Remediation rig set up. Checked depth to concrete between 4 & 8-in casing. Placed fill around wellhead. REMEDIATION

Excavated for and set 4 posts.

Poured 4-ft by 4-ft concrete pad & installed brass cap.

10-11Jun92 - Extended 8-in casing 1.46-ft. Cleaned site.

18Jun92; Primed, painted and stenciled numbers on casing, cap and posts.



WELL DESIGNATION 299-E33-2 •

SST-241-BY-Farm RCRA FACILITY

CERCLA UNIT 200 Aggregate Area Management Study

N 46,465.5 W 53,384.1 [13Apr91-200E] N 451,630 E 2,241,822 [HANCONV] N 137,641.56m E 573,617.22m [13Apr91-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Nov54

243-ft

DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 234.6-ft, Sep90 232-ft, Oct54; DEPTH TO WATER (GS) :

227.0-ft, 23Jun93

CASING DIAMETER 8-in, carbon steel, +2.6+234.5-ft 4-in, carbon steel, +2.0+210-ft

ELEV TOP OF CASING : ~630.62-ft

ELEV GROUND SURFACE : 628.0-ft, Estimated 0+210-ft and 220+233-ft PERFORATED INTERVAL : SCREENED INTERVAL Not applicable : FIELD INSPECTION, 29Mar91, COMMENTS

Carbon steel casing (2).

2-ft round pad, no posts, not capped or locked. Brass cap in pad with stamped well number. FIELD INSPECTION, 17Jun92,

4 and 8-in casing, capped and locked.

4-ft by 4-ft concrete pad, 4 posts. Identification stamped on brass marker in pad.

In underground radiation zone.

AVAILABLE LOGS Driller

Depths referenced to ground surface TV SCAN COMMENTS 07Nov89;

Depth to bottom: 234-ft

Bottom of casing: 4-in surface to 215-ft, 8-in to bottom?

Depth to water: 219-ft

Perforations start at 217-ft and were visible to the bottom at 234-ft. Water remained clear while running the camera. Appeared to be a seperation

in the 8-in casing at 230-ft. Will require further review.

20Sep90;

Depth to bottom: 233-ft, debris on bottom.

Depth to water: 223.4-ft, some floating debris.

Perforations start at 219-ft. Those visible above and below water were open. Appeared to be open hole below the 8-in casing at 230-233-ft. Heavy rust and scale removed but light stuff to some extent was left.

13Nov90 DATE EVALUATED

EVAL RECOMMENDATION : 1. Remove existing 2-ft round concrete collar.

2. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

3. Survey to water level measurement standards. LISTED USE

200 BP-1 quarterly water level measurement, 22Dec54+23Jun93;

WHC ES&M w/l monitoring, CURRENT USER

Electric submersible, PUMP TYPE

270ct89; Removed electric submersible pump. 6,000 dpm contamination encountered. MAINTENANCE

07Nov89; TV camera survey. 01Dec89: Installed submersible pump.

12+13Jul90; Removed submersible pump, brushed casing and bailed debris. 06+07Sep90; Developed well by pumping to <5 NTU.

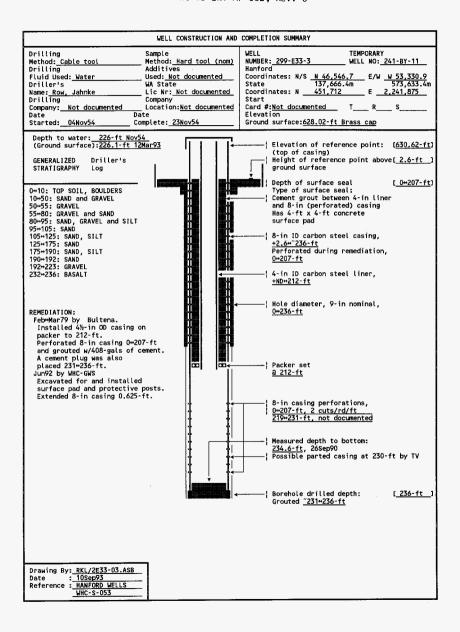
20Sep90; TV camera survey. 26Sep90; Installed electric submersible pump and new cap.

02Jum92+11Jum92; Tagged grout between 4&B-in casing. Cut windows in 8-in casing. Pulled pump. Excavated for posts and pad. Installed 4 posts and REMEDIATION:

protective pad. Extended 8-in casing 0.625-ft.

Set and stamped brass marker in pad. Cleaned site.

18Jun92: Primed and painted post, casing and cap. Stenciled well number.



299-F33-3 WELL DESIGNATION

RCRA FACILITY SST-241-BY-Farm

200 Aggregate Area Management Study (200-BP-1) N 46,546.7 W 53,330.9 (13Aug92-200E) N 451,712 E 2,241,875 [HANCONV] CERCLA UNIT HANFORD COORDINATES : I AMBERT COORDINATES : N 137,666.4m E 573,633.4m [13Aug92-NAD83]

DATE DRILLED Nov54

DEPTH DRILLED (GS) : 236-ft

MEASURED DEPTH (GS) : 234.6-ft, Sep90 DEPTH TO WATER (GS) :

226-ft, Nov54; 226-ft, Nov54; 226.1-ft, 12Mar93 8-in, carbon steel, +2.6+~236-ft; CASING DIAMETER 4-in, carbon steel, +ND+212-ft

630.62-ft, [13Aug92-NGVD'29] 628.02-ft, Brass cap [13Aug92-NGVD'29] ELEV TOP OF CASING : FLEV GROUND SURFACE : 0+207-ft and 219+231-ft

PERFORATED INTERVAL : SCREENED INTERVAL :

Not applicable FIELD INSPECTION, 29Mar91.

COMMENTS

Carbon steel casing (2). 2-ft round pad, no posts, not capped or locked. Brass cap in pad with stamped well number. FIELD INSPECTION, 17Jun92,

4 and 8-in casing, capped and locked.

4-ft by 4-ft concrete pad, 4 posts. Identification stamped on brass marker in pad.

In underground radiation zone. OTHER:

AVAILABLE LOGS Driller :

TV SCAN COMMENTS :

Depths referenced to ground surface 07Nov89;

Depth to bottom: 234-ft

Bottom of casing: 4-in surface to 215-ft, 8-in to bottom?

Depth to water: 219-ft

Perforations start at 217-ft and were visible to the bottom at 234-ft. Water remained clear while running the camera. Appeared to be a seperation

in the 8-in casing at 230-ft. Will require further review.

20Sep90;

Depth to bottom: 233-ft, debris on bottom.

Depth to water: 223.4-ft, some floating debris.

Perforations start at 219-ft. Those visible above and below water were open.

Appeared to be open hole below the 8-in casing at 230-233-ft. Heavy rust and scale removed but light stuff to some extent was left.

13Nov90

DATE EVALUATED EVAL RECOMMENDATION :

1. Remove existing 2-ft round concrete collar.

2. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

3. Survey to water level measurement standards.

LISTED USE 200 BP-1 quarterly water level measurement, 22Dec54+28Jun93; CURRENT LISER

WHC ER characterization, WHC ES&M w/l monitoring PNL sitewide sampling 93

PUMP TYPE Electric submersible, ٠ MAINTENANCE

270ct89; Removed electric submersible pump. 6,000 dpm contamination encountered.

07Nov89; TV camera survey. 01Dec89; Installed submersible pump.

12+13Jul90; Removed submersible pump, brushed casing and bailed debris.

06+07Sep90; Developed well by pumping to <5 NTU.

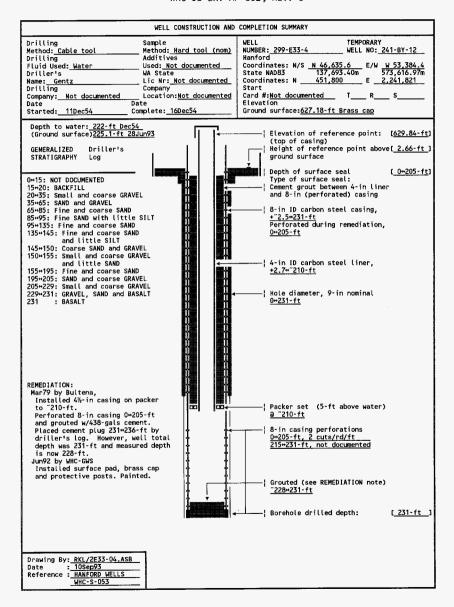
20Sep90; TV camera survey.

26Sep90; Installed electric submersible pump and new cap.

02Jun9241Jun92; Tagged grout between 4&8-in casing. Cut windows in 8-in casing. Pulled pump. Excavated for posts and pad. Installed 4 posts and REMEDIATION:

protective pad. Extended 8-in casing 0.625-ft. Set and stamped brass marker in pad. Cleaned site.

18Jun92: Primed and painted post, casing and cap. Stenciled well number.



WELL DESIGNATION : 200-F33-4

RCRA FACILITY SST-241-BY-Farm ٠

CERCLA UNIT 200 Aggregate Area Management Study (200-BP-1) N 46,635.6 W 53,384.4 [13Aug92-200E] N 451,800 E 2,241,821 [HANCONV] N 137,693.40m E 573,616.97m [13Aug92-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Dec54

DEPTH DRILLED (GS) : 231-ft MEASURED DEPTH (GS) : 228-ft, Sep90 221.1-ft Dec54; DEPTH TO WATER (GS) :

225.1-ft, 28Jun93 CASING DIAMETER

2c3.1-rt, ZBJun93
8-in, carbon steel, "+2.5+231-ft;
4-in, carbon steel, +2.66+210-ft
629.84-ft, [13Aug92-NGVD'29]
627.18-ft, Brass cap [13Aug92-NGVD'29]
0+205-ft and 215+231-ft ELEV TOP OF CASING

ELEV GROUND SURFACE : PERFORATED INTERVAL :

SCREENED INTERVAL COMMENTS .

Not applicable FIELD INSPECTION, 20Mar91,

Carbon steel casing (2). No pad, no posts, capped not locked.

No permanent identification. FIELD INSPECTION, 17Jun92,

4 and 8-in carbon steel casings, capped and locked.

4-ft by 4-ft concrete pad, 4 posts, identification stamped on brass marker in pad.

In underground radiation zone. OTHER -

AVAILABLE LOGS Driller :

TV SCAN COMMENTS Depths referenced to ground surface;

Jan90;

Depth to bottom: 221-ft

Depth to water: 209-ft Could not determine perforation location. Hung up at 212-ft coming out.

20Sep90;

Depth to bottom: 229-ft, gravel on bottom.

Depth to water: 221.1-ft Perforations start at 219-ft. Some visible and open below water surface. 8-in casing below water had some scale because of the way the well had to

be cleaned. Water very clear.

DATE EVALUATED 13Nov90

EVAL RECOMMENDATION : 1. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

2. Survey to water level measurement standards. LISTED USE 200 BP-1 quarterly water level measurment, 22Dec54+28Jun93, WHC ES&M w/l monitoring, ٠

CURRENT USER :

WHC ER characterization

PUMP TYPE Hydrostar, intake at 227.7-ft, (top-of-casing).

MAINTENANCE 08Aug90; Brushed casing and bailed debris. No contamination encountered.

12→13Sep90; Bailed and developed well with pump to <5 NTU.

20Sep90; TV camera survey.

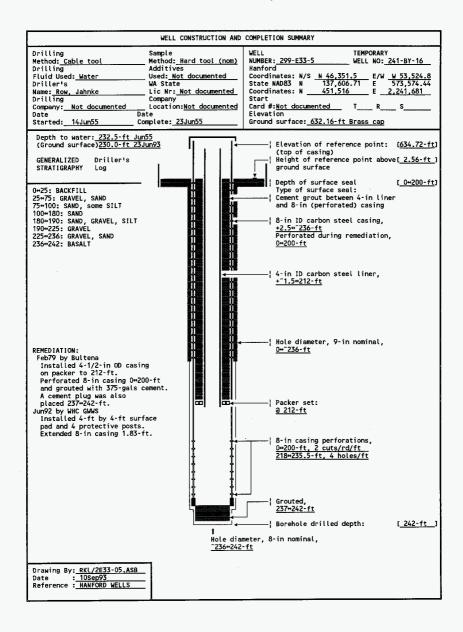
27Sep90; Installed Hydrostar pump and new cap.

REMEDIATION: 01+11Jun92: Pulled pump. Tagged grout between 8-4-in casing. Cut windows in 8-in casing. Excavated for posts and pad. Installed 4 posts

protective pad, and brass marker in pad. Stamped number on marker.

Cleaned site. Did not extend casing.

18Jun92: Primed and painted posts, casing and cap. Stenciled well number.



WELL DESIGNATION 299-E33-5

RCRA FACILITY SST-241-BY-Farm

CERCLA UNIT

200 Aggregate Area Management Study (200-BP-1) N 46,351.5 W 53,524.8 [13Aug92-200E] N 451,516 E 2,241,681 [HANCONY] N 137,606.71m E 573,574.44m [13Aug92-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Jun55

242-ft

DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : DEPTH TO WATER (GS) : 238-ft, Sep90 TV 232.5-ft, Jun55; 230.0-ft, 23Jun93

CASING DIAMETER

8-in, carbon steel, +2.56+"236-ft; 4-in, carbon steel, +1.5+212-ft 634.72-ft, [13Aug92-NGVD129] 0+200-ft and 218+235.5-ft ELEV TOP OF CASING : ELEV GROUND SURFACE :

PERFORATED INTERVAL : SCREENED INTERVAL

Not applicable FIELD INSPECTION, 29Mar91 COMMENTS

Carbon steel casing (2).

2-ft round pad, no posts, capped not locked. Brass cap in pad with stamped well number. FIELD INSPECTION, 17Jun92

4 and 8-in carbon steel casing, capped and locked.

4-ft by 4-ft concrete pad, 4 posts, identification stamped on brass marker in pad.

In underground radiation zone. OTHER:

AVAILABLE LOGS Driller

Depths referenced to ground surface TV SCAN COMMENTS Nov89;

Depth to bottom: 236-ft

Bottom of casing: 4-in surface to 212-ft, 8-in to 236-ft Depth to water: 226-ft

Perforations start at 217-ft and were fairly visible below the water level clear

to the bottom at 236-ft. No appreciable scale buildup.

20Sep90; Depth to bottom: 238-ft, silty

Depth to water: 225-ft

Perforations began at 219-ft, those visible below the water level were open. Light scale below water because of the way the well was cleaned. Water clear.

DATE EVALUATED 13Nov90

EVAL RECOMMENDATION : 1. Remove existing 2-ft round concrete collar.

2. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

3. Survey to water level measurement standards.

SST monthly water level measurement, 19Aug55+23Jun93, LISTED USE CURRENT USER WHC ES&M w/l monitoring,

WHC ER characterization. PNL sitewide sampling 93

Hydrostar PUMP TYPE

MAINTENANCE

270ct89; Removed electric submersible pump.

07Nov89; TV camera survey. 13+15Nov89; Fished pipe and pump from well. OlDec89; Installed electric summersible pump. 16Jul90; Removed pump and cleaned well.

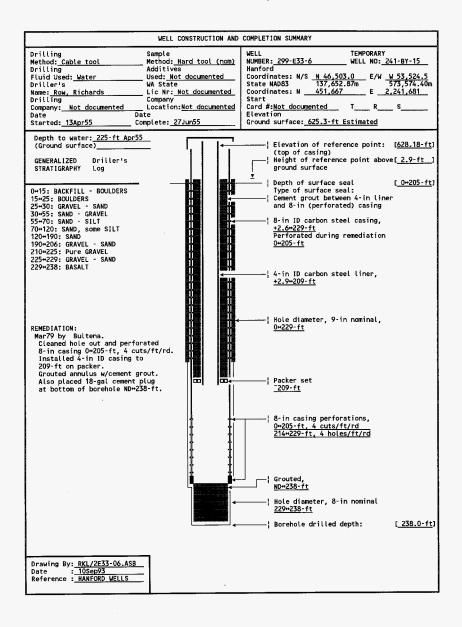
28-29Aug90; Bailed clean, developed with pump to <5 NTU.

20Sep90; TV camera survey.

28Sep90; Set electric submersible pump and installed new cap on well. REMEDIATION

02+10Jun92; Pulled pump. Cut windows in 8-in casing. Placed fill around well site. Excavated for posts and pad. Installed 4 posts, protective pad and brass marker. Stamped well number on marker. Extended 8-in casing 1.83-ft. Cleaned site. 18Jun92; Primed and painted post, casing and cap.

Stenciled well number on casing and post.



WELL DESIGNATION 299-E33-6

SST-241-BY-Farm RCRA FACILITY

CERCLA UNIT

331-241-51-731 200 Aggregate Area Management Study N 46,503.0 W 53,524.5 [13Apr91-200E] N 451,667 E 2,241,681 [HANCONV] N 137,652.87m E 573,574.40m [13Apr91-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

Apr55, extended Jun55 238-ft

DATE DRILLED DEPTH DRILLED (GS) :

MEASURED DEPTH (GS) : Not documented 225-ft, Apr55;

DEPTH TO WATER (GS) : 223-11, APF39; 8-in, carbon steel, +2.6\*229.0-ft 4-in, carbon steel, +2.9\*209-ft 628.18-ft, [13Apr91-NG 625.3-ft, Estimated 0\*205-ft and 214\*229-ft CASING DIAMETER

[13Apr91-NGVD 29] ELEV TOP OF CASING :

ELEV GROUND SURFACE: PERFORATED INTERVAL :

Not applicable SCREENED INTERVAL : COMMENTS

FIELD INSPECTION, 02Mar91, 4 and 8-in carbon steel casing. No pad, no posts, capped not locked.

In surface radiation zone.

OTHER: AVAILABLE LOGS Driller :

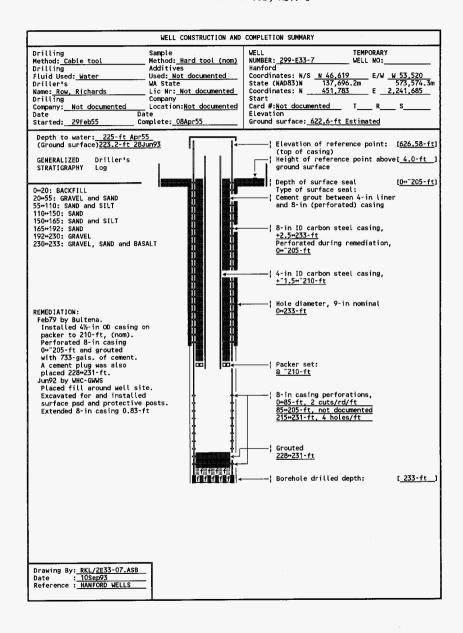
TV SCAN COMMENTS Not applicable : DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

Water levels measured 28Apr55+04Feb86, LISTED USE

None documented CURRENT USER

PUMP TYPE None MAINTENANCE Casing extended 07May91?

casing lowered 18Jun91, amount not documented.



WELL DESIGNATION 299-F33-7 Not applicable RCRA FACILITY

200 Aggregate Area Management Study (200-BP-1) N 46,645.3 W 53,524.5 [13Aug92-200E] N 451,810783 E 2,241,681 [HANCONY] N 137,696.24m E 573,574.28m [13Aug92-NAD83] CERCLA UNIT HANFORD COORDINATES :

LAMBERT COORDINATES :

Apr55 233-ft DATE DRILLED DEPTH DRILLED (GS) :

234-ft, Sep90 TV 225-ft, Apr55; 223.2-ft, 28Jun93 MEASURED DEPTH (GS) : DEPTH TO WATER (GS) :

CASING DIAMETER 8-in, carbon steel, +2.54+231-ft; 4-in, carbon steel, "+1.5+"210-ft ELEV TOP OF CASING :

4-III, Calladd (13Aug92-NGVD 22) 627.82-ft, 8-ass cap [13Aug92-NGVD 29] 0+85-ft, 85+200-ft and 215+231-ft ELEV GROUND SURFACE : PERFORATED INTERVAL : SCREENED INTERVAL :

FIELD INSPECTION, 230ct89, COMMENTS

Carbon steel casing (2). 2-ft round pad, no posts, capped not locked.

No permanent identification. FIELD INSPECTION, 17Jun92,

4 and 8-in carbon steel casing, capped and locked.

4-ft by 4-ft concrete pad, 4 posts, identification on brass marker in pad.

In underground radiation zone. OTHER:

AVAILABLE LOGS Driller

Depths referenced to ground surface; TV SCAN COMMENTS

Nov89: Depth to bottom: Unable to determine

Bottom of casing: 4-in surface to 212-ft

Depth to water: 213-ft

Small pipe, possibly bailer at 224-ft. Wire in hole at 226-ft. Perforations start at 214-ft.

20Sep90; Depth to bottom: 234-ft

Depth to water: 219.5-ft, some floating debris.
Perforations start at 213-ft, 4 cuts/ft. Perfs above water good, those visible below water open. Some debris on bottom, looked like plastic or metal of some kind. Well had extensive fishing trying to remove pump

and other debris. 13Nov90

DATE EVALUATED

EVAL RECOMMENDATION .

1. Remove existing 2-ft round concrete collar.
2. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

Survey to water level measurement standards.

200 BP-1 monthly water level measurement, 28Apr55+28Jun93; LISTED LISE

WHC ES&M w/l monitoring, CURRENT USER WHC ER characterization

B0000000 000000

PNL sitewide sampling 93

PLIMP TYPE

Hydrostar, 20Jul89: PNL TV camera survey. MAINTENANCE

17-26Jul90; Cleaned junk/debris from well, and scrubbed casing. 14-175ep90; Bailed and developed well with pump to <5 NTU.

20Sep90; TV camera survey.

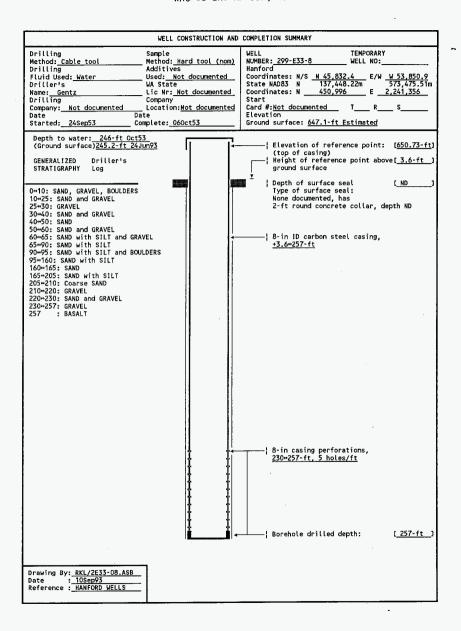
27Sep90; Set Hydrostar pump and installed new cap.

REMEDIATION 01+11Jun92; Placed fill material around well site.

Excavated for posts and pad. Cut windows in 8-in casing. Installed 4 posts, surface pad and brass marker in pad. Stamped well number on brass marker.

Extended 8-in casing 0.83-ft. Cleaned site. 18Jun92; Primed and painted posts, casing and cap.

Stenciled well number on casing and post.



WELL DESIGNATION 299-E33-8

RCRA FACILITY SST-241-BY-Farm

CERCLA UNIT 200 Aggregate Area Management Study (200-BP-1) HANFORD COORDINATES :

N 450,996 E 2,241,356 [HANCONV]
N 137,448.22m E 573,475.51m [17Sep90-NAD83] LAMBERT COORDINATES :

DATE DRILLED 0ct53 257-ft DEPTH DRILLED (GS) :

MEASURED DEPTH (GS) : 257+-ft, Nov89 TV DEPTH TO WATER (GS) :

246-ft, 0ct53; 245.2-ft, 24Jun93 8-in, carbon steel, +3.6+257-ft 650.73-ft, [17Sep90-200E] CASING DIAMETER

ELEV TOP OF CASING : ELEV GROUND SURFACE : 647.2-ft, Estimated 230+257-ft

PERFORATED INTERVAL : SCREENED INTERVAL :

Not applicable COMMENTS

FIELD INSPECTION, 01Feb90, Carbon steel casing.

2-ft round pad, no posts, capped and locked. Brass cap in pad with stamped identification.

OTHER. AVAILABLE LOGS Driller

TV SCAN COMMENTS Depths referenced to ground surface: :

Nov89: Depth to bottom: 259-ft

Bottom of casing: 257-ft Depth to water: 246.3-ft

The perforations started at "225-ft, 4 perfs rd/ft. The perforations couldn't be distinguished below the water level, but could occasionally

be picked out. Casing has heavy scale and crud build-up.

Will require scrubbing and redevelopment prior to use. DATE EVALUATED Not applicable

EVAL RECOMMENDATION : Not applicable

LISTED USE SST monthly water level measurement, 21Jan54+24Jun93;

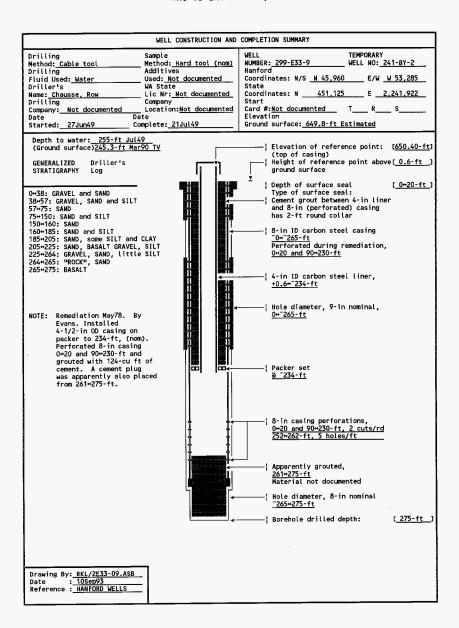
CURRENT USER WHC ES&M w/l monitoring,

PUMP TYPE Hydrostar

MAINTENANCE

OSSep89; Installed cap and hasp and locked well. 12Oct89; Removed electric submersible pump. 02Nov89; TV camera survey.

29+30Nov89; Installed electric submersible pump. 15May90; Removed electric submersible pump. 16May90; Scrubbed casing and bailed debris.



WELL DESIGNATION 299-E33-9

RCRA FACILITY SST-241-BY-Farm

331-241-51-741 m 200 Aggregate Area Management Study (200-BP-1) N 46,960 W 53,285 N 451,125 E 2,241,922 CERCLA UNIT

HANFORD COORDINATES :

LAMBERT COORDINATES : DATE DRILLED Jul49

275-ft

DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 260-ft, Mar90 TV 255.5-ft Jul49; DEPTH TO WATER (GS) :

245.3-ft Mar90 TV CASING DIAMETER

8-in, carbon steel, 0+~265-ft; 4-in, carbon steel, +0.6+234-ft

ELEV TOP OF CASING : 650.40-ft

ELEV GROUND SURFACE : 649.8-ft Estimated

0+20-ft, 90+230-ft, and 252+262-ft Not applicable PERFORATED INTERVAL :

SCREENED INTERVAL :

FIELD INSPECTION, 270ct89, COMMENTS Carbon steel casing.

2-ft round pad, no posts, capped and locked. No permanent identification. Access to well seriously impeded by structures.

In radiation zone >4 mrem dose rate, also asbestos hazard zone.

OTHER: Surface/annular seal by remediation in 1979. 4-in liner grouted to 234-ft

integrity indeterminate.

AVAILABLE LOGS

Driller TV SCAN COMMENTS

28Mar90, depths referenced to ground surface; Depth to bottom: 259.8-ft, silty. May have large rock on bottom.

Bottom of casing: Not determined.

Depth to water: 245.3-ft, floating debris.
Water murky, dislodged scale and suspended debris.

Vadose zone casing: Some rust. Submerged casing: Some scale. Perforations not observed.

Not applicable DATE EVALUATED

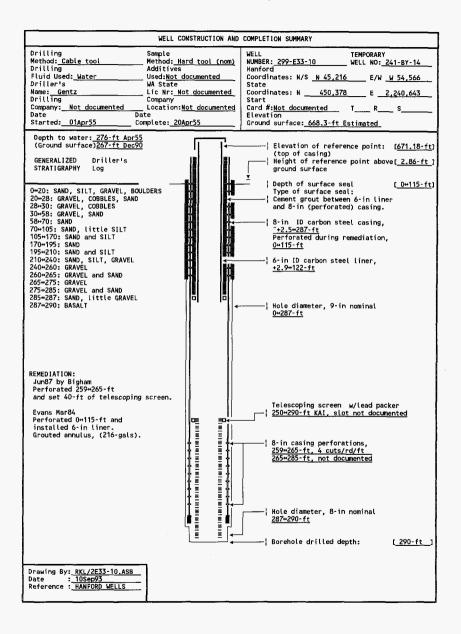
EVAL RECOMMENDATION : Not applicable

Water levels measured 12Sep49+29Mar56, removed from w/l schedule LISTED USE

WHC TWRS radiation monitoring CURRENT USER

PUMP TYPE None documented

MAINTENANCE 28Mar90; TV camera survey.



WELL DESIGNATION 299-E33-10 RCRA FACILITY 216-B-Trenches

200 Aggregate Area Management Study (200-BP-5) N 45,216 W 54,566 N 450,378 E 2,240,643 CERCLA UNIT :

HANFORD COORDINATES : LAMBERT COORDINATES :

Apr55 DATE DRILLED

DEPTH DRILLED (GS):
MEASURED DEPTH (GS):
DEPTH TO WATER (GS): 290.0-ft Not documented 276-ft, Apr55, 267.0-ft, Dec90

8-in, carbon steel, +3.0+~287.0-ft; 6-in carbon steel, +2.86+122-ft CASING DIAMETER

671.18-ft ELEV TOP CASING ELEV GROUND SURFACE :

668.3-ft Estimated 0+115-ft; 259+285-ft 250+290-ft PERFORATED INTERVAL : SCREENED INTERVAL : COMMENTS

FIELD INSPECTION, 23Mar92
No pad. Capped and locked. No posts, no permanent identification.
8-in and 6-in carbon steel casing.

In underground radiation zone.

AVAILABLE LOGS Driller

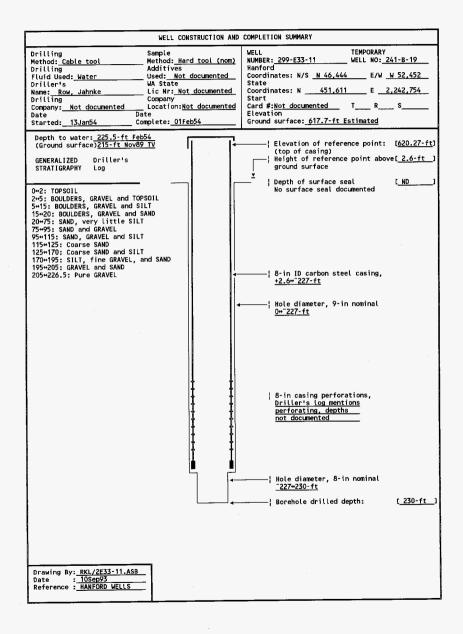
Not applicable TV SCAN COMMENTS DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

Water levels measured 28Apr55÷20Dec90 PNL sitewide sampling 93 LISTED USE :

CURRENT USER PUMP TYPE Electric submersible

MINERAL DIA 12.5

MAINTENANCE



WELL DESIGNATION 299-E33-11 . RCRA FACILITY Not applicable •

CERCLA UNIT 200 Aggregate Area Management Study (200-BP-1) N 46,444 W 52,452

HANFORD COORDINATES :

LAMBERT COORDINATES : N 451,611 E 2,242,754

DATE DRILLED Feb54 DEPTH DRILLED (GS) : 230-ft

MEASURED DEPTH (GS) : DEPTH TO WATER (GS) : Not documented 225.5-ft Feb54: 215-ft Nov89 TV

8-in, carbon steel, +2.6+227-ft 620.27-ft. CASING DIAMETER

ELEV TOP OF CASING :

ELEV GROUND SURFACE : 617.7-ft Estimated PERFORATED INTERVAL : Not documented SCREENED INTERVAL : Not applicable

COMMENTS

Not appricante
FIELD INSPECTION, 07Feb90,
8-in carbon steel casing. No pad, no posts, capped and locked.
No permanent identification.

Not in radiation zone.

OTHER:

AVAILABLE LOGS : Driller

02Nov89, depths referenced to ground surface; TV SCAN COMMENTS

Depth to bottom: Could not determine.

Bettom of casing: 227-ft Bettom to water: 215-ft Casing extremely scaled over below the water level. The scale/crud build-up was so bad it interfered with the camera travel. The camera knocked so much debris off the well casing that nothing could be seen on the trip out. A bailer and cable were found at the bottom of the well.

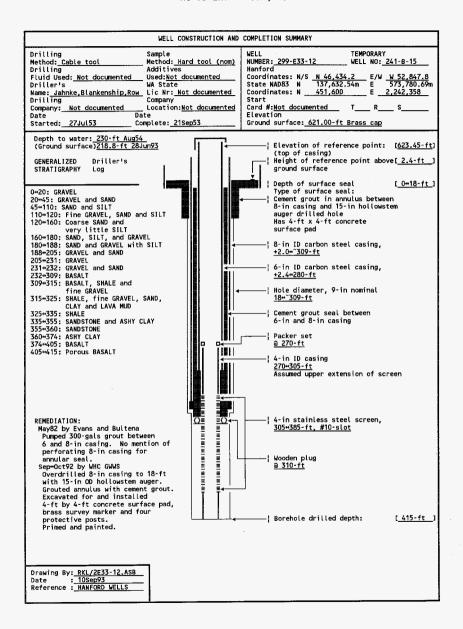
No perforations could be distinguished.

DATE EVALUATED Not applicable :

EVAL RECOMMENDATION : Not applicable LISTED USE Water levels measured 18Feb54+29Mar56 None documented

CURRENT USER ī PUMP TYPE None documented ٠

MAINTENANCE 02Nov89: PNL TV camera survey.



WELL DESIGNATION 299-F33-12 • Not applicable RCRA FACILITY

200 Aggregate Area Management Study (200-BP-1) CERCLA UNIT N 46,434.2 W 52,847.8 [270ct92-200E] N 451,600 E 2,242,358 [HANCONV] N 137,632.54m E 573,780.69m [270ct92-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

Sep53/Remediation-May82 DATE DRILLED

DEPTH DRILLED (GS) : 415-ft

414-ft, Aug90 TV 230.5-ft, Aug54; MEASURED DEPTH (GS) : DEPTH TO WATER (GS) :

218.8-ft, 28Jun93 CASING DIAMETER

8-in, carbon steel, +2.0+~309-ft; 6-in, carbon steet, +2-45+280-ft; 623.45-ft, [270ct92-NGVD'29] 621.00-ft, Brass cap [270ct92-NGVD'29] ELEV TOP OF CASING : ELEV GROUND SURFACE :

None documented

PERFORATED INTERVAL : SCREENED INTERVAL

COMMENTS

REMEDIATION

4-in stainless steel telescoping, 305+385-ft FIELD INSPECTION, 060ct89 Three carbon steel casings.

No pad, no posts, capped and locked. No permanent identification.

OTHER: Driller's log shows 6-in liner to 280-ft, grouted 0+290-ft, 4-in to 415-ft. No mention of perforating 8-in. 4-in casing assumed to be bottom blank section

attached to 4-in screen.

AVAILABLE LOGS Driller

TV SCAN COMMENTS Depths referenced to ground surface;

Jan90:

Depth to bottom: ~407-ft, soft muck Bottom of casing: 4-in surface to 265-ft

Depth to water: 214.5-ft

Top of water cruddy, cleaned up at 220-ft. Top of screen 300↔301-ft. Screen crudded up. Blank casing from 384↔385-ft to bottom.

27Aug90;

Depth to Bottom: 414-ft, soft silt Bottom of Casing: 4-in to 280-ft

Depth to Water: 216.9-ft, top of water floating debris, dislodged scale and suspended debris. Quality improves from 305-ft to bottom. Screen 305-385-ft.

Blank casing from 384+385-ft to bottom.

DATE EVALUATED 13Nov90

1. Install surface seal to at least 18-ft. EVAL RECOMMENDATION :

2. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

3. Shorten monitored interval to approximately 15-ft by plugging back to

approximately 325-ft below ground surface. 4. Survey to water level measurement standards.

200 BP-1 quarterly water level measurement, 21Jan54+28Jun93:

LISTED USE CURRENT USER WHC ES&M w/l monitoring,

WHC ER characterization PNL sitewide sampling 93

PUMP TYPE Hydrostar, 18 Jul89; PNL TV survey. MAINTENANCE

16+17May90 - Removed obstruction at top of screen and cleaned screen.

17&20Aug90 - Bailed and developed well with pump. Minimum NTU 27,

<5 NTU not achieved.

27Aug90; TV camera survey.

31Aug90; Installed Hydrostar pump. 15+17Jun92: Geophysically logged hole.

21Sep92; Removed pump, geophysically logged hole. 22+24Sep92; Prepared site.

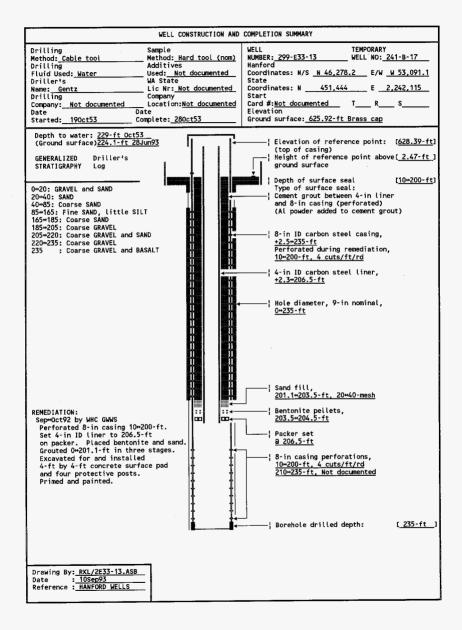
25Sep92; Overdrilled 8-in casing w/10%-in ID/15-in OD hollowstem auger to 18-ft.

28+30Sep92; Cemented annulus outside 8-in casing w/20 sacks cement.

15+190ct92; Excavated for posts, set form. Poured concrete pad,

set brass marker in pad. Stamped well number on marker. Set posts.

270ct92: Primed, painted and stenciled well head.



299-F33-13 WELL DESIGNATION RCRA FACILITY Not applicable

300 Aggregate Area Management Study (200-BP-1) N 46,278.2 W 52,091.1 [270ct92-200E] N 451,444 E 2,242,115 [HANCONV] N 137,584.72m E 573,706.68m [270ct92-NAD83] CERCLA UNIT . HANFORD COORDINATES :

I AMBERT COORDINATES :

Oct53 DATE DRILLED DEPTH DRILLED (GS) : 235-ft 231-ft, Sep90 TV 229-ft, Oct54; 224.1-ft, 28Jun93 MEASURED DEPTH (GS) : DEPTH TO WATER (GS) :

224.1-Tt, 203UN3 8-in, carbon steel, +2.47+235-ft; 4-in, carbon steel, +2.3+206.5-ft 628.39-ft, [270ct92-NGVD'29] 625.92-ft, Brass cap [270ct92-NGVD'29] CASING DIAMETER FLEV TOP OF CASING :

ELEV GROUND SURFACE : 210+235-ft PERFORATED INTERVAL : SCREENED INTERVAL : Not applicable

COMMENTS

Not applicable
FIELD INSPECTION, 230ct89,
Carbon steel casing. No pad, no posts, capped not locked.
No permanent identification. In surface radiation zone.

No permanent identifications
FIELD INSPECTION, 180ct92,
8-in carbon steel casing, capped and locked.

4-ft by 4-ft concrete surface pad, identification stamped on brass marker in pad.

Not in radiation zone. OTHER:

AVAILABLE LOGS : Driller

TV SCAN COMMENTS Depths referenced to ground surface:

Nov89:

Depth to bottom: 231-ft Bottom of casing: 231-ft Depth to water: 219-ft Perforations began at 210-ft, 6 rd/ft. Scale/crud build-up below water level excessive making perforations indistinguisable. Some perforations were visible at bottom of casing. The camera knocked enough crud off casing on trip in that nothing could be seen coming out due to the murky water. This well requires scrubbing and redevelopment.

20Sep90;

Depth to Bottom: 231-ft, gravel, Depth to Water: 219-ft
Perforations began at 209-ft, 6 per rd/ft. Some visible every now and then.
The casing below water had some algae buildup. Water was clear.

DATE EVALUATED

1. Perforate per WAC 173-160-415(2) to approximately 200-ft. EVAL RECOMMENDATION :

2. Install 4-in liner with cement basket to approximately 205-ft.

Pressure grout by use of tremie pipe.

3. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

4. Survey to water level measurement standards. 200 BP-1 quarterly water level measurement, 18Feb54+28Ju 93:

LISTED USE

CURRENT USER WHC ES&M w/l monitoring, WHC ER characterization

PUMP TYPE Electric submersible 21Jul89: PNL TV camera survey. MAINTENANCE

07Nov89; TV camera survey. 03Aug90; Scrubbed casing and bailed debris.

Contamination to 1,500 cpm encountered. 10+11Sep90; Developed well to <5 NTU.

25Sep90; Installed electric submersible pump.

28Aug+11Sep92; Site surveyed and contamination found. REMEDIATION

Contamination removed and fill placed for contamination control.

15+17Sep92; Perforated casing 10+200-ft, 4 cuts/rd/ft. 17+23Sep92; Set 4½-in OD liner, 2-in below top of 8-in casing

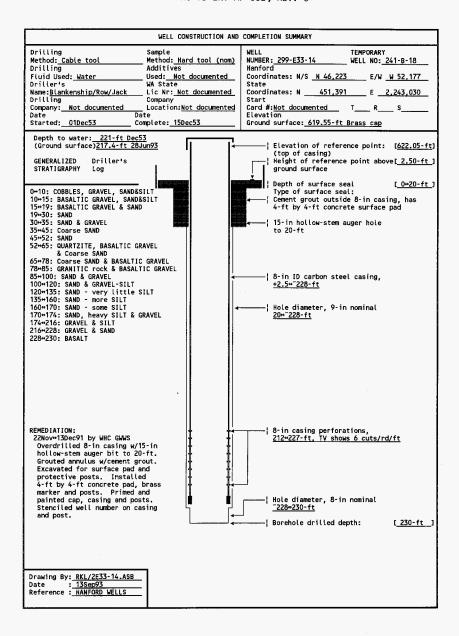
Placed 2.5-gal of 1/2-in bentonite pellets 203.5\*204.8-ft. Placed 6-gals silica sand 201.1\*203.5-ft.

Grouted annulus with cement grout (Al powder added) in three stages. 193.2-201.1-ft, 102.3-193.2-ft and ground surface+102.3-ft.

24Sep92: Excavated for pad and posts.

28+30Sep92; Installed 4-ft by 4-ft concrete surface pad, brass marker in pad and four protective posts. Stamped identification on brass marker 010ct92; Installed drain hole in 8-in casing.

190ct92; Primed and painted casing and posts.



299-E33-14 WELL DESIGNATION ٠ RCRA FACILITY Not applicable

CERCLA UNIT

200 Aggregate Area Management Study (200-BP-1)

N 46,223 W 52,177 N 451,391 E 2,243,030 [HANCONV] HANFORD COORDINATES :

LAMBERT COORDINATES :

DATE OFFICE Dec53 DEPTH DRILLED (GS) : 230-ft

MEASURED DEPTH (GS) : 229.6-ft, Aug90 TV

221-ft, Dec53; 217.4-ft, 28Jun93 DEPTH TO WATER (GS) :

8-in, carbon steel, +2.5+~228-ft CASING DIAMETER 622.05-ft, ELEV TOP OF CASING : [25Feb92-NGVD 129] 619.55-ft, Brass cap [25Feb92-NGVD'29]

PERFORATED INTERVAL : 212+227-ft

SCREENED INTERVAL Not applicable

FIELD INSPECTION, 07Feb90, COMMENTS Carbon steel casing.

No pad, no posts, capped and locked.

No permanent identification.

FIELD INSPECTION, 150ct92, 8-in carbon steel csing, capped and locked.

4-ft by 4-ft pad, 4 posts, identification stamped on brass marker in pad.
Not in radiation zone.

OTHER:

AVAILABLE LOGS : Driller

Depths referenced to ground surface: TV SCAN COMMENTS ٠

Nov89: Depth to bottom: 226-ft, soft/silty-apparently fill.

Bottom of casing: Could not determine

Depth to water: 215-ft

Perforations start at 212-ft, 6 per rd/ft. Perforations were distinguishible

to some extent below the water level. Slight scale build-up. This well will require scrubbing and redevelopment prior to use.

27Aug90:

Depth to Bottom: 229.6-ft, silt, debris

Depth to Water: 217.2-ft

Perforations start at 215-ft. Some open slots visible. Submerged casing

appeared to have corrosion but may be algae. 13Nov90

DATE EVALUATED

EVAL RECOMMENDATION : 1. Install a 2-in void surface seal outside 8-in casing to approximately 18-ft, OR; Perforate 3+18-ft and install a 4-in liner with cement basket to approximately 20-ft. Pressure grout to 40-psi.

2. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

Survey to water level measurement standards. 200 BP-1 water level measurement, 18Feb54+28Jun93,

LISTED USE CURRENT USER

WHC ES&M w/l monitoring,

WHC ER characterization

PNL sitewide w/l monitoring 93

Hydrostar,

DIMD TYPE MAINTENANCE

02Nov89; TV camera survey. 11May90: Scrubbed casing and bailed debris. 09+14Aug90; Developed well with pump to <5 NTU.

30Aug90; Installed Hydrostar pump.

22Nov91: Removed vegetation and concrete pad. REMEDIATION

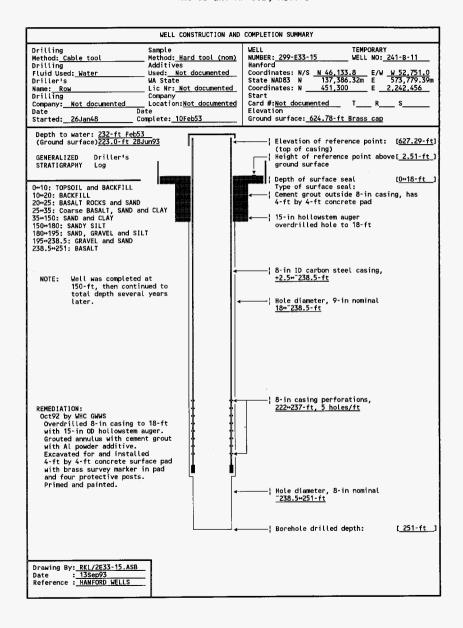
27Nov91; Overdrilled 8-in casing to 20-ft w/15-in hollow-stem auger bit. Grouted annulus w/cement grout (Al powder added).

04Dec91; Excavated for surface pad and protective posts.

O6Dec91; Installed 4-ft by 4-ft concrete surface pad, placed brass marker

and 4 protective posts.

09Dec91; Repaired casing. Casing was not extended. 13Dec91; Primed and painted cap, casing and posts.



299-F33-15 WELL DESIGNATION

RCRA FACILITY Not applicable CERCLA UNIT

200 Aggregate Area Management Study (200-BP-1) 200 Aggregate Area Management Study (200-BP-1) N 46,133.8 W 52,751.0 [270ct92-200E] N 451,300 E 2,242,456 [HANCONY] N 137,386.32m E 573,779.39m [270ct92-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Feb53 DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 251-ft 250-ft, Sep90

232-ft, Feb53; 223.0-ft, 28Jun93 8-in, carbon steel, +2.51+~238.5-ft DEPTH TO WATER (GS) :

CASING DIAMETER 627.29-ft, [270ct92-NGVD'29] 624.78-ft, Brass cap [270ct92-NGVD'29] [270ct92-NGVD 1291 ELEV TOP OF CASING : FLEV GROUND SURFACE :

PERFORATED INTERVAL : 222+237-ft Not applicable SCREENED INTERVAL :

FIELD INSPECTION, 240ct89, COMMENTS

Carbon steel casing.

No pad, no posts, capped not locked. No permanent identification.

No permanent of the control of the c

Not in radiation zone.

OTHER -Driller

AVAILABLE LOGS TV SCAN COMMENTS Depths referenced to ground surface:

07Nov89: Depth to bottom: 249-ft Bottom of casing: 240-ft Depth to water: 221-ft

Perforations could be seen beginning at 222-ft. Excessive scale/crub build-up made it difficult to distinguish perforations. Nothing could be seen coming out of hole with camera due to debris knocked off casing while running in. Well needs scrubbing and redevelopment. 20Sep90;

Depth to bottom: 250.3-ft Depth to water: 219.8-ft

Perforations could be seen beginning at 222-ft and extending to 237-ft at 6 cuts/rd/ft. Apparent open hole from 237-ft to bottom.

13Nov90 DATE EVALUATED

 Install a 2-in void surface seal outside 8-in casing to approximately EVAL RECOMMENDATION : 18-ft, OR; Perforate 3+18-ft and install a 4-in liner with cement basket

to approximately 20-ft. Pressure grout to 40-psi.
2. Install protective posts and concrete pad per WAC 173-160-510 and

field conditions.

3. Survey to water level measurement standards.

200 BP-1 water level measurement. 18Feb53+28Jun93: LISTED USE CURRENT USER WHC ES&M w/l monitoring,

employed to the control of the contr

WHC ER characterization PUMP TYPE Electric submersible, MAINTENANCE

07Nov89; TV camera survey. 02Aug90; Brushed casing and bailed debris.

18+19Sep90; Bailed and developed with pump to <5 NTU.

20Sep90: TV camera survey.

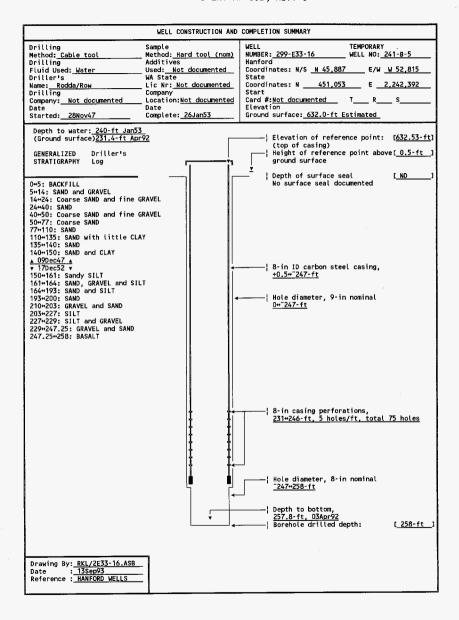
01+050ct92; Overdrilled 8-in casing to 18-ft w/15-in OD hollowstem auger. Grouted annulus with 13 sacks cement w/Al powder additive. REMEDIATION

15+160ct92; Excavated for and installed 4-ft by 4-ft concrete pad,

brass survey marker in pad and 4 protective posts.

190ct92: Extended casing 1.04-ft. Stamped well number on survey marker.

270ct92; Primed and painted wellhead and protective posts.



WELL DESIGNATION 299-E33-16 : 216-B-8 Crib RCRA FACILITY

200 Aggregate Area Management Study (200-BP-5) N 45,887 W 52,815 N 451,053 E 2,242,392 [HANCONV] CERCLA UNIT

HANFORD COORDINATES :

LAMBERT COORDINATES :

DATE DRILLED Jan53 :

DEPTH DRILLED (GS): MEASURED DEPTH (GS): 258.0-ft 257.8-ft 240.3-ft, Jan53, 231.4-ft, 03Apr92 8-in, carbon steel, +0.5+~247.0-ft; 632.53-ft DEPTH TO WATER (GS) :

CASING DIAMETER

ELEV TOP CASING

ELEV GROUND SURFACE : 632.0-ft, Estimated 231+246-ft PERFORATED INTERVAL : Not applicable SCREENED INTERVAL :

COMMENTS

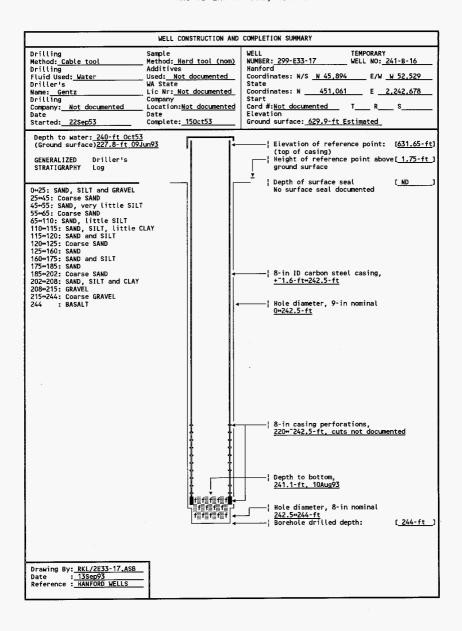
NOT applicable FIELD INSPECTION, 03Apr92 No pad. Capped, not locked. No posts, no permanent identification. 8-in carbon steel casing. No pump installed.

Driller AVAILABLE LOGS :

Not applicable TV SCAN COMMENTS DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

Water levels measured 22Jan53+29Mar56 LISTED USE . .

None documented CURRENT USER PUMP TYPE None documented MAINTENANCE



299-E33-17 WELL DESIGNATION : RCRA FACILITY 216-B-8 Crib .

200 Aggregate Area Management Study (200-BP-5) N 45,894 W 52,529 N 451,061 E 2,242,678 [HANCONV] CERCLA UNIT .

HANFORD COORDINATES :

LAMBERT COORDINATES :

DATE DRILLED 0ct53

DEPTH DRILLED (GS): MEASURED DEPTH (GS): 244.0-ft 241.1-ft, 10Aug93 240.0-ft, 0ct53, 227.8-ft, 09Jun93 DEPTH TO WATER (GS) :

8-in, carbon steel, +1.75+~242.5-ft; 631.65-ft CASING DIAMETER

ELEV TOP CASING

630.0-ft, Estimated 220+242.5-ft ELEV GROUND SURFACE : PERFORATED INTERVAL : SCREENED INTERVAL : Not applicable

FIELD INSPECTION, 10Aug93 COMMENTS

No pad. Not capped or locked. No posts, no permanent identification. 8-in carbon steel casing. No pump installed.

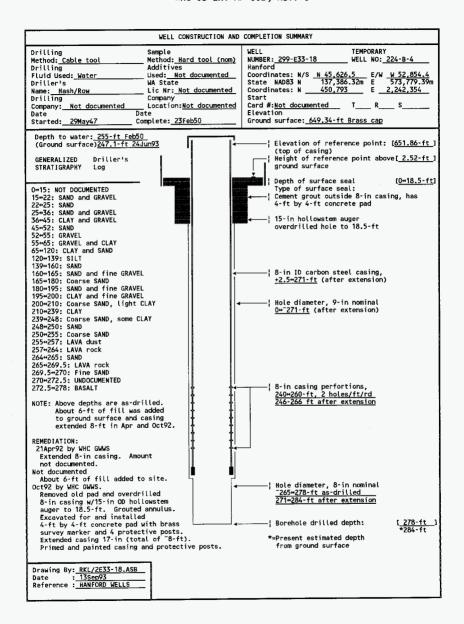
AVAILABLE LOGS : TV SCAN COMMENTS : Driller

Not applicable Not applicable DATE EVALUATED EVAL RECOMMENDATION : Not applicable

LISTED USE Seperations area semiannual water level measurement, 19Nov53+09Jun93; :

CURRENT USER WHC ES&M w/l monitoring,

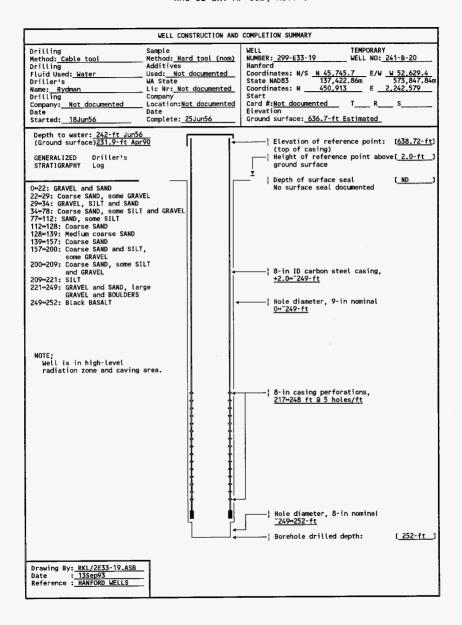
PUMP TYPE None documented



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299-F33-18 WELL DESIGNATION ÷ RCRA FACILITY SST-241-B Farm 200 Aggregate Area Management Study (200-BP-1) N 45,626.5 W 52,854.4 [270ct92-200E] N 450,793 E 2,242,354 [HANCONV] CERCLA UNIT HANFORD COORDINATES : LAMBERT COORDINATES : N 137,386.32m E 573,779.39m [270ct92-NAD83] DATE DRILLED Feb50 DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 278-ft 262.5-ft, Aug90 TV 255-ft, Feb50; 247.1-ft, 24Jun93 DEPTH TO WATER (GS) : 8-in, carbon steel, +2.52+~265-ft 651.86-ft, [270ct92-NGVI CASING DIAMETER [270ct92-NGVD'29] was 643.62-ft (17Sep90-200E) ELEV TOP OF CASING : 649.34-ft, Brass cap [270ct92-NGVD'29] was 643.0-ft Estimated ELEV GROUND SURFACE : PERFORATED INTERVAL : 240+260-ft Not applicable SCREENED INTERVAL . FIELD INSPECTION, 240ct89, COMMENTS Carbon steel casing. 2-ft round pad, no posts, capped not locked. Identification on brass cap. Identification on blass cap. FIELD INSPECTION, 200ct92, 8-in carbon steel casing, capped and locked. 4-ft by 4-ft concrete pad, identification stamped on brass marker in pad. Not in radiation zone. OTHER: AVAILABLE LOGS Driller : Depths referenced to ground surface; TV SCAN COMMENTS Nov89; Depth to bottom: 259-ft; Bottom of casing: 252-ft; Depth to water: 236-ft Sample bottle floating at 236-ft. Another sample bottle was suspended at 245-ft and two more sample bottles were on bottom. Perforations could not be seen due to the scale build-up. Sample bottles need to be removed from the well. The well needs to be scrubbed and redeveloped. Depth to bottom: 262.5-ft, sample bottle on bottom; Bottom of casing: 255-ft; Depth to water: 238.8-ft
Perforations started at 250-ft, last perf seen at 251-ft. Water clear. 13Nov90 DATE EVALUATED EVAL RECOMMENDATION : 1. Remove 2-ft collar and install a 2-in void grout surface seal outside 8-in casing to approximately 18-ft, OR;
2. Perforate 3+18-ft and install a 4-in liner with cement basket to approximately 20-ft. Pressure grout to 40-psi. 3. Install protective posts and concrete pad per WAC 173-160-510 and field conditions. 4. Perforate 8-in casing approximately 238+250-ft. 5. Shorten monitored interval to approximately 15-ft by plugging back to approximately 260-ft below ground surface. Survey to water level measurement standards. LISTED HISE SST monthly water level measurement, 17Aug50+24Jun93; WHC ES&M w/l monitoring and RCRA sampling, CURRENT USER WHC ER characterization Electric submersible PUMP TYPE 09Nov89; Removed electric submersible pump. 13Nov89; TV camera survey. MAINTENANCE 29Nov89: Installed electric submersible pump. 27Jul&01Aug90; Pulled pump, brushed casing and bailed debris. 20-21Aug90; Bailed and developed with pump to <5 NTU. 31Aug90; Removed 2 sample bottles. Installed pump and capped well. 21Apr92; Casing extended, amount not documented. 05+070ct92; Overdrilled 8-in casing to "5-ft. REMEDIATION Obstruction encountered, probable undocumented 10-in casing. 08+100ct92; Removed old pad. 120ct92; Overdrilled to 18.5-ft w/15-in OD, 10.25-in ID hollowstem auger. 130ct92; Grouted annulus between 8-in casing and overdrilled hole with 19 sacks cement, Al powder added. 140ct92; Excavated for pad and posts. 160ct92; Installed 4-ft by 4-ft concrete surface pad with brass survey marker and 4 protective posts. 190ct92; Extended 8-in casing 17-in. Stamped identification on survey marker. 270ct92: Primed and painted wellhead and posts.

BERROLLE 1.1.1.



299-E33-19 WELL DESIGNATION :

RCRA FACILITY SST-241-B-Farm •

200 Aggregate Area Management Study (200-BP-5) CERCLA UNIT 200 Aggregate Area Management Study (200-8P-5) N 457,745.7 W 52,629.4 [17Sep90-200East] N 450,913 E 2,242,579; [HANCONY] N 137,422.86m E 573,847.84m [17Sep90-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Jun56 DEPTH DRILLED (GS) : 252-ft

MEASURED DEPTH (GS) : 236.5-ft 242-ft, Jun56; ~231.9-ft, Apr90 DEPTH TO WATER (GS) :

8-in, carbon steel, +2.0+~249-ft. CASING DIAMETER

638.72-ft, [17Sep90-200East] 637.0-ft, Estimated 217+248-ft ELEV TOP CASING

ELEV GROUND SURFACE : PERFORATED INTERVAL :

SCREENED INTERVAL : Not applicable FIELD INSPECTION 01Apr92, COMMENTS .

No permanent identification. No pump.
Well in high-level radiation zone, also surface caving.

OTHER; AVAILABLE LOGS Driller . TV SCAN COMMENTS 10Apr90;

Depth to bottom: 236.5-ft
Depth to water: 231.9-ft, floating debris. Dislodged scale and floating debris.

Vadose zone casing: Scale/rust visible, a piece of rusted casing was

protruding into well.

Perforations not visible. Submerged casing: Casing in bad shape, scale/rust.

Areas of rusted casing protruding into well.

DATE EVALUATED Aug90

DECOMMISSION: Decommissioning required. This well has extremely degraded casing, EVAL RECOMMENDATION :

is located in a radiation zone and is in a crib cave-in area. Access is difficult for equipment or personnel. Any modification or maintenance

is dependent on gaining required access.

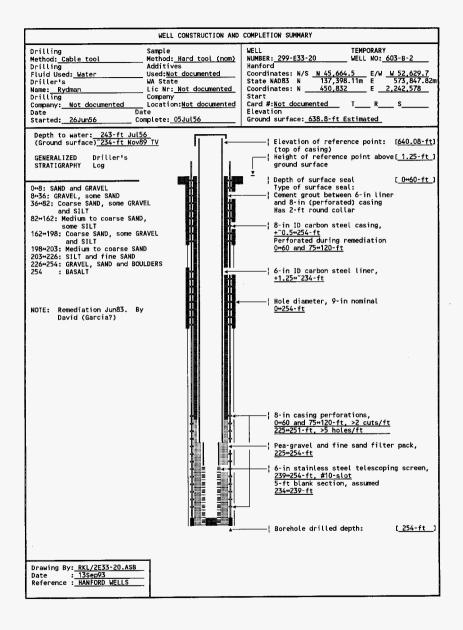
1) Perforate from 3-ft below ground surface to total depth. 2) Install sand plug 230-ft to total depth. Set bentonite plug 225+230-ft. 3) Place cement grout 3+225-ft.

4) Cut casing at 3-ft. Fill excavation and compact to grade.

Water level measurered Apr72+Jul74 LISTED USE

CURRENT USER None documented .

None documented DIMO TYPE .



299-E33-20 WELL DESIGNATION

RCRA FACILITY : SST-241-B-Farm S31-241-B-Farm 200 Aggregate Area Management Study (200-BP-1) N 45,664.5 W 52,629.7 [17Sep90-200 East] N 450,832 E 2,242,578; [HANCONV] N 137,339.11m E 573,847.82m [17Sep90-NAD83] Jul56/Remediation - Jun83 CERCLA UNIT :

HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED :

DEPTH DRILLED (GS) : 254-ft

254-ft, Nov89 TV 243-ft, Jul56; 234-ft, Nov89 TV MEASURED DEPTH (GS) : DEPTH TO WATER (GS) :

8-in, carbon steel, ~0.5+254-ft; 6-in carbon steel, +1.2+~234-ft CASING DIAMETER

640.87-ft

ELEV TOP OF CASING : 639.6-ft Estimated

039,5-ft Estimated 0+60, 75+120 and 225+251-ft 239+254-ft, 6-in telescoping, stainless steel, 10-slot FIELD INSPECTION, 01Apr92, PERFORATED INTERVAL : SCREENED INTERVAL :

COMMENTS . Carbon steel casing (2). 2-ft round pad,

capped not locked, no posts. No permanent identification.

Ground caving area and high radiation zone.

OTHER:

AVAILABLE LOGS Driller :

Nov89, depths referenced to ground surface; TV SCAN COMMENTS

Depth to bottom: 254-ft Bottom of casing: 254-ft Depth to water: 234-ft

Screen started at 236-ft and ended at 254-ft. Very little scale build-up on casing or screen. Sediment build-up on bottom.

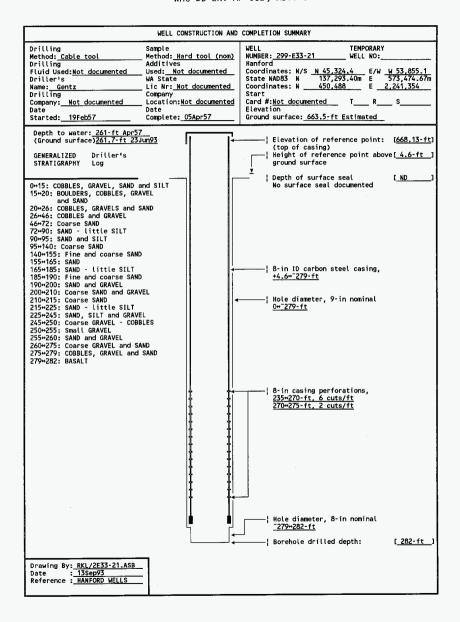
Well can be used as is.

DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

Water levels measured 18Aug65+04Feb86 LISTED USE :

CURRENT USER None documented PUMP TYPE None documented .

07Nov89; TV camera survey. MAINTENANCE



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WELL DESIGNATION 299-E33-21 :

RCRA FACILITY SST-241-BX-Farm CERCLA UNIT

200 Aggregate Area Management Study (200-BP-5) N 45,324.4 W 55,855.1 [17sep90-200E] N 450,488 E 2,241,354 [HANCONU] N 137,293.40m E 573,474.67m [17sep90-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Apr57 DEPTH DRILLED (GS) : 282-ft MEASURED DEPTH (GS) : 279-ft DEPTH TO WATER (GS) : 261-ft, Apr57; 261.7-ft, 23Jun93

CASING DIAMETER 8-in, carbon steel, +4.6. 279-ft.

668.13-ft, [17Sep90-200E] 663.5-ft, Estimated 235+275-ft ELEV TOP CASING

ELEV GROUND SURFACE :

PERFORATED INTERVAL : SCREENED INTERVAL : Not applicable

COMMENTS FIELD INSPECTION, 230ct89,

Carbon steel. No pad, no posts, capped, not locked. No permanent identification. Submersible pump installed.

OTHER;

AVAILABLE LOGS Driller TV SCAN COMMENTS 20Mar90;

Depth to bottom: 278.8-ft Depth to water: 259.1-ft, floating debris.

Water clear with some dislodged scale.

Vadose zone casing: Considerable scale from 257.5-ft to water.

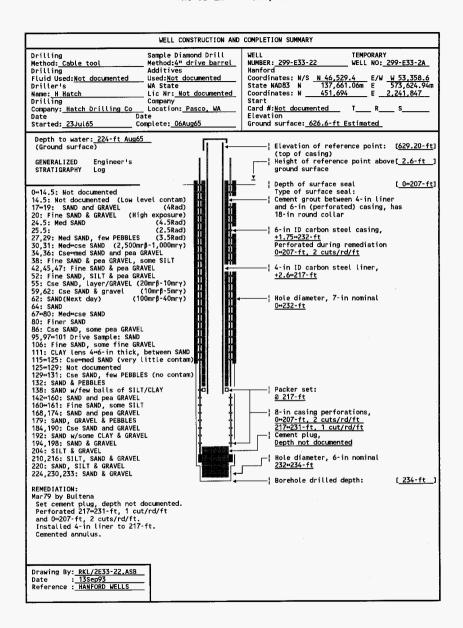
Submerged casing: Heavy scale below water. Perforations started at 236.8-ft, 4 cuts/rd/ft.

Clean and in good shape above water. Not visible below water. DATE EVALUATED Not applicable

EVAL RECOMMENDATION : Not applicable

LISTED USE SST water level measurement, 20Apr73+23Jun93: WHC ES&M w/l monitoring and RCRA sampling :

CURRENT USER PUMP TYPE Electric submersible -



299-E33-22 WELL DESIGNATION

RCRA FACILITY Not applicable

CERCLA UNIT

300 Aggregate Area Management Study N 46,529.4 W 53,358.6 [200E-13Apr91] N 451,694 E 2,241,847 [HANCONV] N 137,661.06m E 573,624.94m [NAD83-13Apr91] HANFORD COORDINATES : LAMBERT COORDINATES :

Aug65 234-ft DATE DRILLED DEPTH DRILLED (GS) : MEASURED DEPTH (GS) :

Not documented 224-ft, Aug65 DEPTH TO WATER (GS) :

6-in, carbon steel, +1.75+232-ft; 4-in, carbon steel, +2.60+217-ft CASING DIAMETER

ELEV TOP CASING 629.20-ft

ELEV GROUND SURFACE : 626.6-ft, Estimated 0+207, 217+231-ft FIELD INSPECTION, 29Mar91 PERFORATED INTERVAL : SCREENED INTERVAL :

4 and 6-in carbon steel casing. Capped, not locked

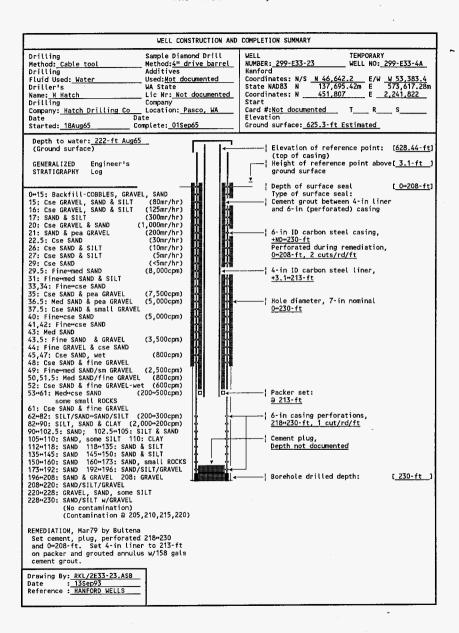
No pad, no permanent identification, no posts.
In surface radiation zone.

COMMENTS Driller, Engineer Not applicable AVAILABLE LOGS TV SCAN COMMENTS DATE EVALUATED Not applicable Not applicable EVAL RECOMMENDATION : LISTED USE No water level data;

CURRENT USER None documented : PLIMP TYPE None

MAINTENANCE

Casing extended Apr91? 18Jun91 - Casing lowered, amount not documented



299-E33-23 WELL DESIGNATION RCRA FACILITY Not applicable

CERCLA UNIT

200 Aggregate Area Management Study N 46,642.2 W 53,383.4 [200E-13Apr91] N 451,807 E 2,241,822 [HANCONV] N 137,695.42m E 573,617.28m [NAD83-13Apr91] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Sep65 DEPTH DRILLED (GS) : 230-ft MEASURED DEPTH (GS) : Not documented DEPTH TO WATER (GS) : 222-ft, Aug65

CASING DIAMETER

ELEV TOP CASING ELEV GROUND SURFACE :

222-ft, Augos 6-in, carbon steel, +ND+230-ft; 4-in, carbon steel, +3.12+213-ft 628.44-ft, [MgVD\*29-29Mar91] 625.3-ft, Estimated 0+207, 217+231-ft Not documented PERFORATED INTERVAL : SCREENED INTERVAL : FIELD INSPECTION, 29Mar91 COMMENTS

4 and 6-in carbon steel casing. Capped, not locked

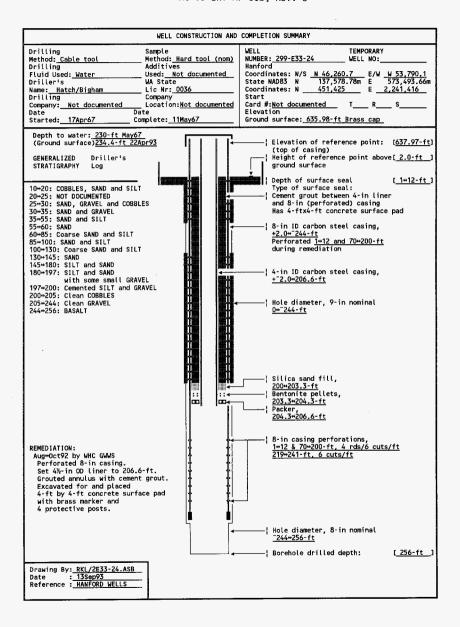
No pad, no permanent identification, no posts.

In surface radiation zone.

AVAILABLE LOGS Driller, Engineer Not applicable TV SCAN COMMENTS DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable No water level data; LISTED USE CURRENT USER None documented ٠

PUMP TYPE None .

MAINTENANCE 15Apr91 - Casing extended, amount not documented. 17Jun91 - Casing lowered, amount not documented.



299-E33-24 WELL DESIGNATION

RCRA FACILITY SST-241-BY-Farm

CERCLA UNIT

200 Aggregate Area Management Study (200-BP-1) N 46,260.7 W 53,790.1 [270ct92-200E] N 451,425 E 2,241,416 [HANCONY] N 137,578.78m E 573,493.66m [270ct92-NAD83] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED May67

DEPTH DRILLED (GS) : 256-ft MEASURED DEPTH (GS) : DEPTH TO WATER (GS) :

250-ft, Sep90 TV 230-ft, May67; 234.4-ft, 22Apr93

8-in, carbon steel, +2.0+"244-ft; 4-in, carbon steel, "+2.0+207-ft CASING DIAMETER 637.97-ft, [270ct92-NGVD'29] 635.98-ft, Brass cap [270ct92-NGVD'29] ELEV TOP OF CASING :

ELEV GROUND SURFACE: PERFORATED INTERVAL : 219+241-ft

SCREENED INTERVAL : Not applicable

FIELD INSPECTION, 230ct89, COMMENTS

Carbon steel casing. 2-ft round pad, capped not locked, no posts.

Identification stamped on brass cap in pad.

Identification stemped on an account of the FIELD INSPECTION, 1900ct92, 8-in carbon steel casing, capable and locked. 4-ft by 4-ft concrete pad with survey marker. 4 protective posts. Not in radiation zone.

OTHER: AVAILABLE LOGS Driller •

TV SCAN COMMENTS

Depths referenced to ground surface: 07Nov89:

Depth to bottom: 248-ft; Bottom of casing: "248-ft; Depth to water: 231-ft

Perforations start at 217-ft, 6 per rd/ft. Perforations could not be seen below the water level due to scale build-up.

Well needs to be scrubbed and redeveloped.

20Sep90:

Depth to bottom: 250-ft, silty; Depth to water: 231-ft Perforations start at 217-ft, 6 per rd/ft. The perfs above water level looked good. There were a lot visible below water and they were open.

DATE EVALUATED EVAL RECOMMENDATION :

PUMP TYPE MAINTENANCE 13Nov90 1. Remove existing 2-ft pad and perforate per WAC 173-160-415(2) to

approximately 200-ft. 2. Install 4-in liner with cement basket to approximately 205-ft.

Pressure grout by use of a tremie pipe.

3. Install protective posts and concrete pad per WAC 173-160-510 and field conditions.

Survey to water level measurement standards.

09Sep93

1. Decommission. Well is in crib stabilization area and would penetrate

impermeable pad to be installed. SST monthly water level measurement, 04Feb86+23Jun93.

LISTED USE CURRENT USER

WHC ES&M w/l monitoring and RCRA sampling,

WHC ER characterization PNL sitewide sampling 93

Electric submersible, intake at 239.4-ft, (top-of-casing).

270ct89; Pulled electric submersible pump.

07Nov89: TV camera survey.

O1Dec89; Installed electric submersible pump.

24&29May90; Pulled pump. Brushed casing. Bailed debris. 24&27Aug90; Bailed and developed well with pump to <5 NTU.

20Sep90; TV camera survey.

28Sep90; Installed pump and replaced cap.

17Aug92; Perforated 70+200 and 1+12-ft. DEMEDIATION

18Aug+02Sep92; Welded casing packer on 4%-in OD casing. Ran casing to 206.6-ft, top of packer @204.3-ft. Placed 2-gal bentonite pellets, 203.3\*204.3-ft. Placed 6-gal silica sand, 200\*203.3-ft.

Tremie grouted annulus between 4 and 8-in casing with

cement grout back to 1-ft, (Al powder added to cement).

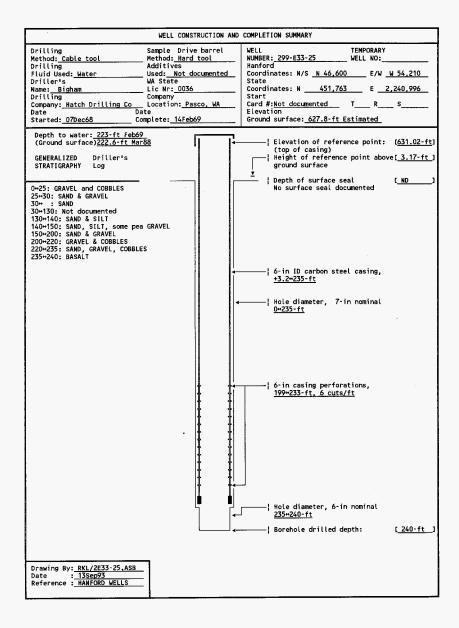
11Sep92; Excavated for posts and pad.

28Sep92: Installed 4-ft by 4-ft concrete pad, brass survey marker

and 4 protective posts.

010ct92; Extended casing to 24-in and stamped well identification on marker.

190ct92; Primed and painted wellhead and protective posts.



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WELL DESIGNATION 299-E33-25 : RCRA FACILITY Not applicable

NOT applicable
200 Aggregate Area Management Study
N 46,600 W 54,210
N 451,763 E 2,240,996 [HANCONV] CERCLA UNIT

HANFORD COORDINATES :

LAMBERT COORDINATES : Feb69 DATE DRILLED

DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 240-ft Not documented DEPTH TO WATER (GS) :

Not accumented 223-ft, 14Feb69 222.6-ft, 31Mar88 6\_in, carbon steel, +3.17+235-ft CASING DIAMETER

ELEV TOP OF CASING : ELEV GROUND SURFACE : 631.02-ft,

627.85-ft, Estimated PERFORATED INTERVAL : 199+233-ft

Not applicable SCREENED INTERVAL

COMMENTS

-

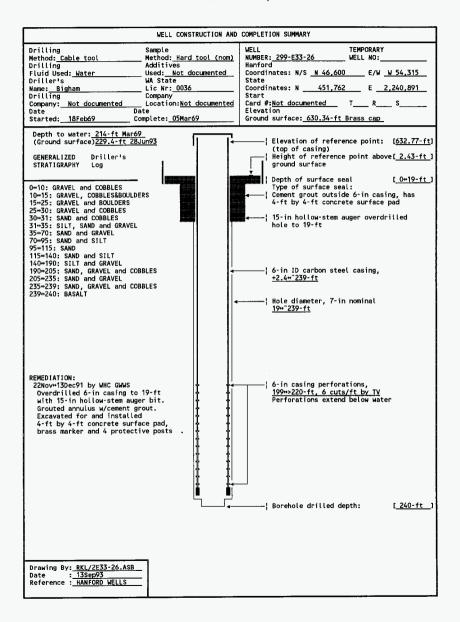
NOT APPLICABLE
FILLD INSPECTION, 06Feb90,
Fill carbon steel casing. Capped and locked, no posts.
No pad. Not in radiation zone.

OTHER: AVAILABLE LOGS Driller

Not applicable TV SCAN COMMENTS Not applicable DATE EVALUATED EVAL RECOMMENDATION : Not applicable

LISTED USE Water levels measured, 04Feb86+31Mar88 :

None documented CURRENT USER PUMP TYPE None documented



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WELL DESIGNATION 299-E33-26 • RCRA FACILITY Not applicable

200 Aggregate Area Management Study (200-BP-1) CERCLA UNIT

HANFORD COORDINATES : N 46,600 W 54,315

N 451,762 E 2,240,891 [HANCONV] LAMBERT COORDINATES :

DATE DRILLED Mar69

DEPTH DRILLED (GS) : 240-ft MEASURED DEPTH (GS) : 241-ft Aug90 TV DEPTH TO WATER (GS) :

214-ft, Mar69; 229.4-ft, 28Jun93 6-in, carbon steel, +2.43+~239-ft 632.77-ft, [25Feb92-NGVC CASING DIAMETER [25Feb92-NGVD | 291 ELEV TOP OF CASING : ELEV GROUND SURFACE : 630.34-ft. Brass cap [25Feb92-NGVD 29]

PERFORATED INTERVAL :

199+Not documented-ft Not applicable SCREENED INTERVAL

FIELD INSPECTION, 06Feb90, COMMENTS

Carbon steel casing. Capped and locked, no posts.

Carbon Steet cashs. Capped and tooked, no posts.

2-ft round pad, identification stamped on brass cap in pad.

FIELD INSPECTION, 150ct92,

6-in carbon steel casing, capped and locked.

4-ft by 4-ft concrete pad with identification stamped on marker, 4 protective posts

OTHER: Driller

AVAILABLE LOGS

TV SCAN COMMENTS

Depths referenced to ground surface; 02Nov89:

Depth to bottom: 237-ft; Bottom of casing: Not detected; Depth to water: 226-ft

Vadose zone casing: corrosion/scale present. The perforations started at 199-ft. Found 6 perforations per rd/ft extending down to "220-ft.

Perforations couldn't be distinguished below the water level. Submerged casing: The casing is corroded and scaled over and requires scrubbing prior to use. Following scrubbing the well should be redeveloped.

Depth to bottom: 241-ft, gravel; Depth to water: 229-ft, floating debris Vadose zone casing was clean. Perforations started at 199-ft, 6 rd/ft.

Submerged casing clean. Some perfs visible. Water clear, some suspended debris,

probably algae. 13Nov90

DATE EVALUATED

1. Remove 2-ft collar and install a 2-in void grout surface seal outside EVAL RECOMMENDATION :

8-in casing to approximately 18-ft, OR;
2. Perforate 3+18-ft and install a 4-in liner with cement basket to approximately

20-ft. Pressure grout to 40-psi.

3. Install protective posts and concrete pad per WAC 173-160-510 and field

conditions.

Survey to water level measurement standards.

200BP-1 monthly water level measurement, 04Feb86+28Jun93, LISTED USE

CURRENT USER

WHC ES&M w/l monitoring, WHC ER characterization,

PNL sitewide sampling 93

Hydrostar, intake at 234.9-ft, (top-of-casing). PUMP TYPE MAINTENANCE 120ct89; Removed electric submersible pump.

02Nov89; TV camera survey. 28Nov89; Installed suibmersible pump.

14May90; Pulled pump, scrubbed casing, bailed debris and fill.

15&16Aug90; Bailed and developed with pump to <5 NTU.

27Aug90; TV camera survey. 28Aug90; Installed hydrostar pump. 22Nov91; Removed concrete pad.

REMEDIATION

02Dec91; Overdrilled 6-in casing to 19-ft w/15-in auger.

Grouted annulus w/cement grout (Al powder added).

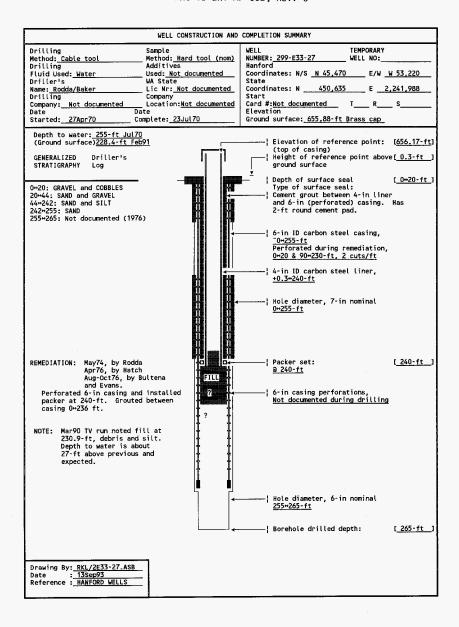
O5Dec91; Excavated for surface pad and protective posts.

06Dec91; Installed concrete pad, brass marker and 4 protective posts.

09Dec91; Repaired casing, stamped number on brass cap.

Did not extend casing.

12+13Dec91; Primed and painted cap, casing and posts.



WELL DESIGNATION : 299-E33-27

RCRA FACILITY SST-241-BX-Farm -

200 Aggregate Area Management Study (200-BP-5) N 45,470.5 W 53,219.3 [17Sep90-200E] N 450,635 E 2,241,989 [HANCONV] CERCLA UNIT

HANFORD COORDINATES :

LAMBERT COORDINATES :

Jul 70 DATE DRILLED : DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 265-ft 231-ft

DEPTH TO WATER (GS) : 255-ft, Jul70; 228.4-ft, 01Feb91

228.4-rt, 01Feb91
6-in, carbon steel, \*0-255-ft.
4-in, carbon steel, \*0.3-240-ft
656.17-ft, [175ep90-200E]
655.88-ft, Brass cap [175ep90-200E]
0riginal 6-in not documented; remediation 0+20 & 90+230-ft, 2 cuts/rd. CASING DIAMETER ELEV TOP CASING

ELEV GROUND SURFACE : PERFORATED INTERVAL :

Not applicable SCREENED INTERVAL :

COMMENTS

FIELD INSPECTION, 270ct89, Carbon steel casing, capped, not locked.

2-ft round pad, no posts. Well number marked on brass cap. No pump. In surface radiation zone.

OTHER; AVAILABLE LOGS Driller : 28Mar90: TV SCAN COMMENTS

:

Depth to bottom: 230.9-ft, debris and silt.

Depth to water: 227.6-ft, may be of outside origin.

Depth should be about 255-ft.

Vadose zone casing: Some rust.

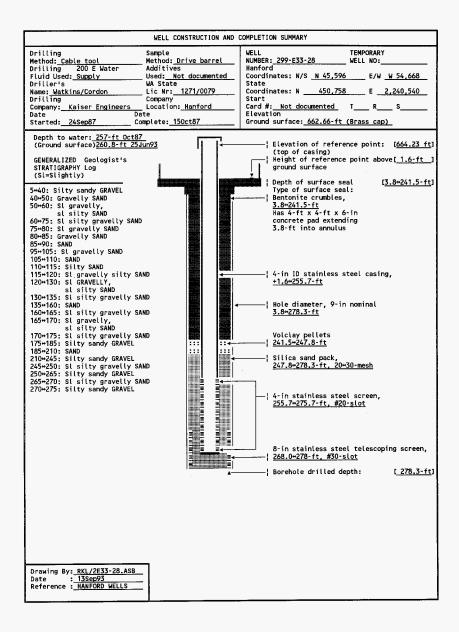
Camera did not get out of 4-in casing. Well has apparently filled in.

DATE EVALUATED Not applicable EVAL RECOMMENDATION :

Not applicable
Water levels measured 29May90+01Feb91 LISTED USE :

WHC TWRS radiation monitoring CURRENT USER

PUMP TYPE : None documented



WELL DESIGNATION 299-E33-28 .

Low Level Burial Grounds - WMA-1 RCRA FACILITY

200 Aggregate Area Management Study (200-BP-1) CERCLA UNIT

HANFORD COORDINATES : N 45,596 W 54,668 [07Dec87-200E] N 450,758 E 2,240,540 [HANCONV]

LAMBERT COORDINATES : DATE DRILLED Nov87

DEPTH DRILLED (GS) : 278-ft 275-ft, Nov89 TV 257-ft, Oct87; 260.8-ft, 25Jun93 MEASURED DEPTH (GS) : DEPTH TO WATER (GS) :

4-in, stainless steel, +1.6+255.7-ft CASING DIAMETER ELEV TOP OF CASING : 664.23-ft, [07Dec87-200E]

662.66, Brass cap [07Dec87-200E] PERFORATED INTERVAL :

boc.bo, brass cap torbetor-255.7 Not applicable 255.7\*275.7-ft, 4-in, #20-slot stainless steel FIELD INSPECTION, 06Feb90 SCREENED INTERVAL

COMMENTS

4-in stainless steel casing. 4x4-ft concrete pad. 4 posts.

Well identification stamped on brass cap in pad.

Not in radiation zone.

OTHER: AVAILABLE LOGS Geologist

19Nov89, depths referenced to ground surface; TV SCAN COMMENTS

Depth to bottom: 275-ft Bottom of casing: 275-ft Depth to water: 259.9-ft Screen: 256+275-ft

Clean, ready for sampling. 13Nov90 DATE EVALUATED

EVAL RECOMMENDATION : No remediation required. Surface seal is 3 3/4-ft, not >18-ft per WAC 173-160.

LLBG monthly water level measurement, O2Dec87+25Jun93; WHC ES&M w/l monitoring and RCRA sampling, LISTED USE :

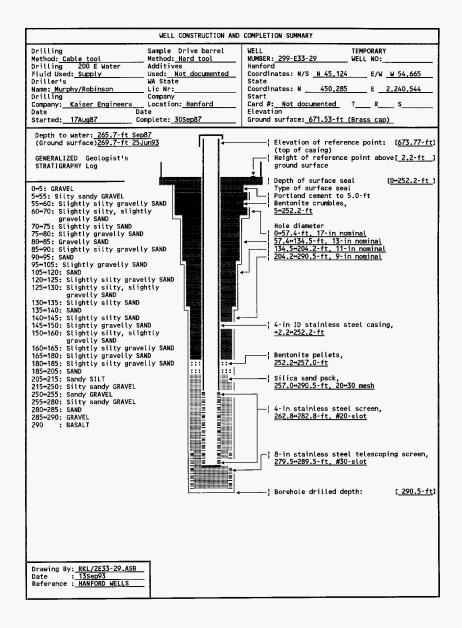
CURRENT USER

WHC ER monitoring PLIMP TYPE

Hydrostar, intake at 274.9-ft, (top-of-casing). 120ct89; Removed hydrostar pump for camera survey. MAINTENANCE

190ct89; TV camera survey. 02Nov89; TV camera survey.

28Nov89; Reinstalled hydrostar pump.



299-E33-29 WELL DESIGNATION

RCRA FACILITY Low Level Burial Grounds, 218-E-10

CERCLA UNIT

200 Aggregate Area Management Study (200-BP-5) N 45,124 W 54,665 [07Dec87] N 450,285 E 2,240,544 [HANCONV] HANFORD COORDINATES : LAMBERT COORDINATES :

Sep87 DATE DRILLED

DEPTH DRILLED (GS) : 290.0-ft MEASURED DEPTH (GS) : Not documented 265.7-ft, Sep87, 269.7-ft, 25Jun93 DEPTH TO WATER (GS) :

4-in, stainless steel, +2.2\*262.8-ft. 673.77-ft, [07Dec87] 671.53-ft, Brass cap [07Dec87] CASING DIAMETER

ELEV TOP CASING

ELEV GROUND SURFACE :

PERFORATED INTERVAL : Not applicable SCREENED INTERVAL :

Not applicable 4-in, 262.8+282.8-ft; 8-in, 279.5+289.5-ft FIELD INSPECTION, 02Jun90, COMMENTS

4-in stainless steel casing, no protective casing. Capped and locked.

4-ft by 4-ft concrete pad, 4 posts, brass marker with stamped ID.

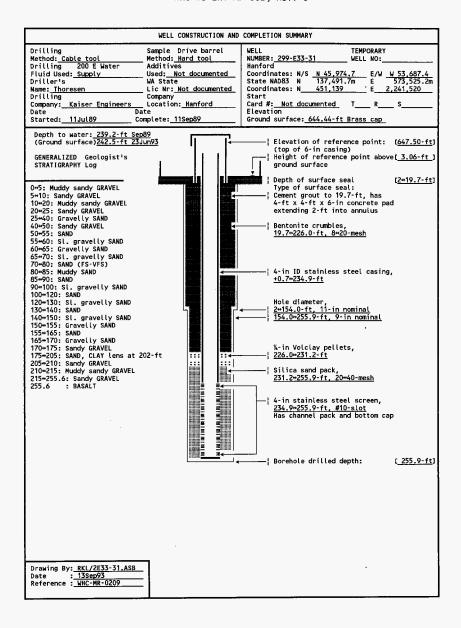
OTHER;

AVAILABLE LOGS Geologist, Driller TV SCAN COMMENTS Not applicable DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

LLBG monthly water level measurement, 01Dec87\*25Jun93; WHC ES&M w/l monitoring and RCRA sampling, LISTED USE •

CURRENT USER

WHC ER characterization PUMP TYPE Hydrostar :



299-E33-31 WELL DESIGNATION

RCRA FACILITY

299'-53-53 Single Shell Tanks, 241-B-BX-BY Farms 200 Aggregate Area Management Study (200-BP-5) N 45,794.7 W 53,687.4 [04Jan90-200E] N 451,139 E 2,241,520 [NAMCOW1] N 137,491.7m E 573,525,2m [04Jan90-NAD83] CERCLA UNIT HANFORD COORDINATES : LAMBERT COORDINATES :

Sep89 255.9-ft DATE DRILLED

DEPTH DRILLED (GS): MEASURED DEPTH (GS): Not documented DEPTH TO WATER (GS) :

239.2-ft, Sep89, 242.5-ft, 23Jun93 4-in, stainless steel, +0.7-234.9-ft. CASING DIAMETER 6-in, stainless steel, +3.06\*\*0.5-ft 647.50-ft, [26Feb92-NGVD'29] 644.44-ft, Brass cap [26Feb92-NGVD'29] ELEV TOP CASING ELEV GROUND SURFACE :

Not applicable PERFORATED INTERVAL :

4-in stainless steel with channel pack, 234.9+255.9-ft SCREENED INTERVAL

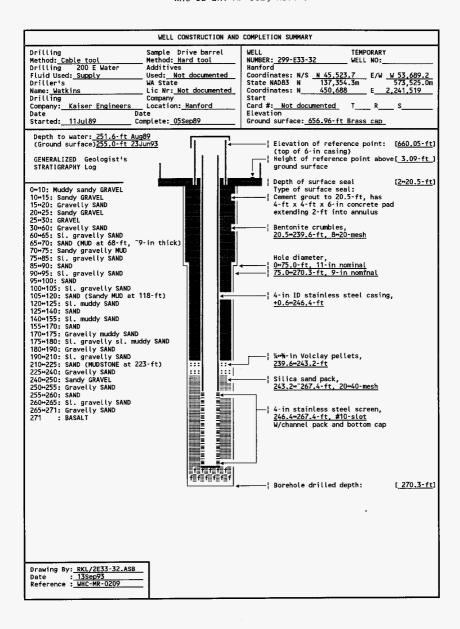
COMMENTS FIELD INSPECTION, OTHER;

Geologist, Driller AVAILABLE LOGS : TV SCAN COMMENTS Not applicable DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

SST monthly water level measurement, 01Dec89+23Jun93; LISTED USF :

CURRENT USER : WHC ES&M w/l monitoring and RCRA sampling,

WHC ER characterization Hydrostar PUMP TYPE :



WELL DESIGNATION 299-E33-32 :

RCRA FACILITY

299-E35-52 Single Shell Tanks, 241-B-BX-BY Farms 200 Aggregate Area Management Study (200-BP-5) N 45,523.7 W 53,689.2 [04Jan90-200E] N 450,688 E 2,241,519 [HANCONY] N 137,354.3m E 573,525.0m [04Jan90-NAD83] CERCLA UNIT HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Sep89

DEPTH DRILLED (GS): MEASURED DEPTH (GS): 270.3-ft Not documented 251.6-ft, Aug89 DEPTH TO WATER (GS) : 255.0-ft, 23Jun93

4-in, stainless steel, +0.6+246.4-ft. 6-in, stainless steel, +3.09+0.5-ft 660.05-ft, (26Feb92-NGVD'29) 656.96-ft, Brass cap [26Feb92-NGVD'29] CASING DIAMETER ELEV TOP CASING ELEV GROUND SURFACE :

PERFORATED INTERVAL : Not applicable

SCREENED INTERVAL : 4-in stainless steel with channel pack, 246.4+267.4-ft

FIELD INSPECTION, 05Feb90; COMMENTS

6-in stainless steel casing. 4-ft by 4-ft concrete pad, 4 posts, 1 removable

capped and locked, brass cap in pad with well ID.

Not in radiation zone.

OTHER;

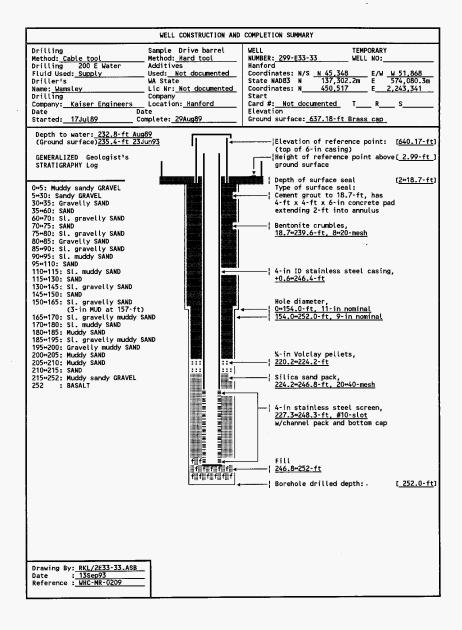
AVAILABLE LOGS Geologist, Driller TV SCAN COMMENTS Not applicable DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

LISTED USE SST monthly water level measurement, 01Dec89+23Jun93;

CURRENT USER WHC ES&M w/l monitoring and RCRA sampling.

WHC ER characterization

DUMP TYPE Hydrostar



WELL DESIGNATION 299-E33-33

RCRA FACILITY

CERCLA UNIT HANFORD COORDINATES :

297-23-33 Single Shell Tanks, 241-B-BX-BY Farms 200 Aggregate Area Management Study (200-BP-5) N 45,348 W 51,868 [OBDec89-200E] N 450,517 E 2,243,341 [HANCONV] N 137,302m E 574,080.3m [OBDec89-NAD83] LAMBERT COORDINATES :

Aug89 DATE DRILLED

DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 252.0-ft

Not documented DEPTH TO WATER (GS) :

Not accumented 232.8-ft, Aug89, 235.4-ft, 23Jun93 4-in, stainless steel, +0.5+227.3-ft, 6-in, stainless steel, +3.0+0.5-ft 640.39-ft, [26Feb92-NGVD'29] 637.40-ft, Brass cap [26Feb92-NGVD'29] Not applicable CASING DIAMETER

ELEV TOP CASING ELEV GROUND SURFACE :

PERFORATED INTERVAL :

4-in stainless steel with channel pack, 227.3+248.3-ft SCREENED INTERVAL

COMMENTS FIELD INSPECTION, 06Feb90;

6-in stainless steel casing. 4-ft by 4-ft concrete pad, 4 posts, 1 removable

capped and locked, brass cap in pad with well ID.

Not in radiation zone.

OTHER; AVAILABLE LOGS Geologist, Driller

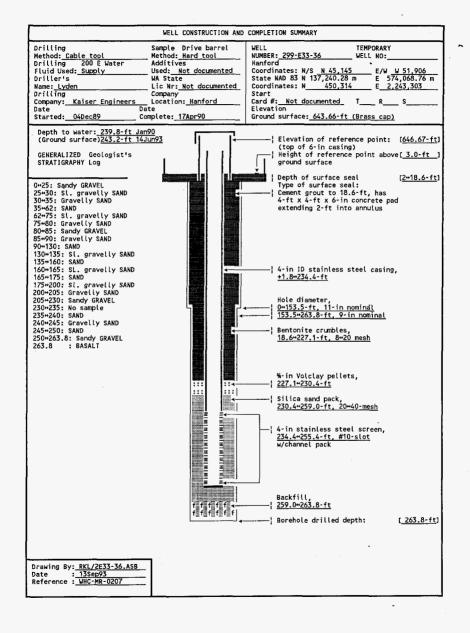
TV SCAN COMMENTS Not applicable DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

SST monthly water level measurement, OBDec89+23Jun93; WHC ES&M w/l monitoring and RCRA sampling, LISTED USE :

CURRENT USER :

WHC ER characterization, PNL sitewide w/l monitoring 93

PUMP TYPE Hydrostar •



WELL DESIGNATION RCRA FACILITY 216-B-63 Trench •

CERCLA UNIT

200 Aggregate Area Management Study (200-BP-5) N 45, 145 W 51,906 (19Apr90-200E) N 450,314 E 2,243,303 (HANCONY) N 137,240.28m E 574,068.76m (19Apr90-NAD83) HANFORD COORDINATES : LAMBERT COORDINATES :

Apr90 DATE DRILLED

DEPTH DRILLED (GS):
MEASURED DEPTH (GS):
DEPTH TO WATER (GS):

264.0-ft
Not documented
239.8-ft, Dec89,
243.2-ft, 14Jun93
4-in, stainless steel, +1.8\*234.4-ft.
6-in, stainless steel, +3.0\*\*0.5-ft
(19Apr90-200E] CASING DIAMETER ELEV TOP CASING

ELEV GROUND SURFACE : 643.66-ft, Brass cap [19Apr90-200E] PERFORATED INTERVAL : Not applicable

SCREENED INTERVAL : 234.4+255.4-ft, 4-in stainless steel with channel pack

FIELD INSPECTION, 10Aug93; 4 and 6-in stainless steel casing. COMMENTS

4-ft by 4-ft concrete pad, 4 posts, 1 removable. Capped and locked, brass cap in pad with well ID.

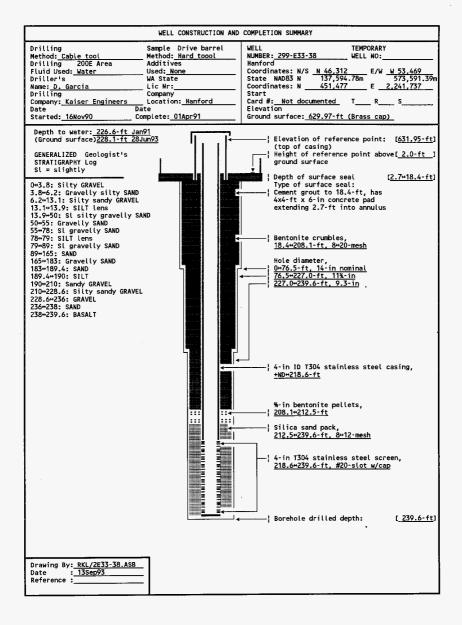
Not in radiation zone. OTHER;

AVAILABLE LOGS Geologist, Driller TV SCAN COMMENTS Not applicable DATE EVALUATED Not applicable : EVAL RECOMMENDATION :

Not applicable B-63 Trench quarterly water level measurement, 01Jan91+14Jun93; LISTED USE :

WHC ES&M w/l monitoring and RCRA sampling, CURRENT USER

PNL sitewide sampling 93 PUMP TYPE Hydrostar



299-E33-38 WELL DESIGNATION RCRA FACILITY

Not applicable 200 BP-1 (200 Aggregate Area Management Study) N 46,312 W 53,469 [20Mar91-200E] N 451,477 E 2,241,737 [HANCONY] N 137,594.78m E 573,591.39m [20Mar91-NAD83] CERCLA UNIT HANFORD COORDINATES :

LAMBERT COORDINATES :

DATE DRILLED

Apr91 239.6-ft DEPTH DRILLED (GS) : MEASURED DEPTH (GS) :

Not documented DEPTH TO WATER (GS) :

226.6-ft, 10Jan91; 228.1-ft, 28Jun93 6-in, stainless steel, +2.0+0.5-ft; 4-in, stainless steel, +ND+218.6-ft 631.95-ft [20Mar91-NGV) 291 CASING DIAMETER ELEV TOP CASING ELEV GROUND SURFACE : 629.97-ft, Brass cap [20Mar91-NGVD'29]

PERFORATED INTERVAL :

Not applicable 218.6+239.6-ft, 4-in stainless steel, #20-slot SCREENED INTERVAL - :

COMMENTS FIELD INSPECTION, 24Mar91;

6-in stainless steel casing. 4-ft by 4-ft concrete pad, 4 posts, 1 removable capped and locked, brass cap in pad with well ID.

Not in radiation zone.

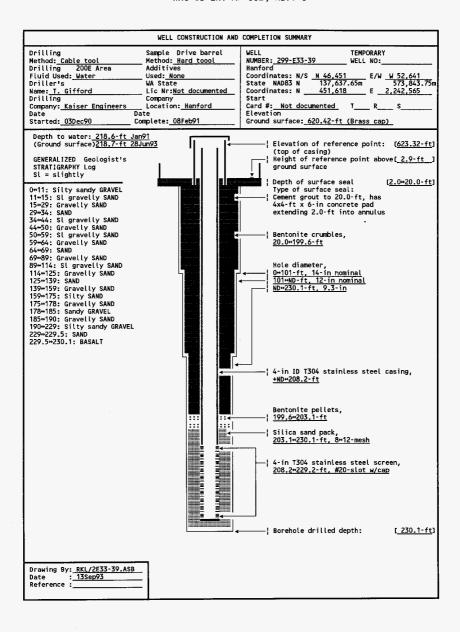
AVAILABLE LOGS Geologist TV SCAN COMMENTS Not applicable

DATE EVALUATED Not applicable EVAL RECOMMENDATION :

Not applicable 200-BP-1 monthly water level measurement, 01Mar91↔28Jun93; LISTED USE

CURRENT USER WHC ES&M w/l monitoring and RCRA sampling,

WHC ER characterization PUMP TYPE Hydrostar



WELL DESIGNATION 299-E33-39

RCRA FACILITY Single Shell Tanks, WMA-B-BX-BY

200 BP-1 (200 Aggregate Area Management Study) N 46,451 W 52,641 (20Mar91-200E) N 451,618 E 2,242,565 (HANCONY) N 137,637.65m E 573,843.75m (20Mar91-NAD83) CERCLA UNIT HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Feb91 230.1-ft

DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : 229.8-ft, 13May91 218.6-ft, 17Jan91; 218.7-ft, 28Jun93 DEPTH TO WATER (GS) :

6-in, stainless steel, +2.9~0.5-ft; 4-in, stainless steel, +ND+208.2-ft 623.32-ft [20Mar91-NGVD'29] CASING DIAMETER ELEV TOP CASING ELEV GROUND SURFACE : 620.42-ft, Brass cap [20Mar91-NGVD'29]

PERFORATED INTERVAL : Not applicable 208.24229.2-ft, 4-in stainless steel, #20-slot SCREENED INTERVAL

FIELD INSPECTION, 1Mayo1;
6-in stainless steel casing. 4-ft by 4-ft concrete pad, 4 posts, 1 removable capped and locked, phass cap in pad with well ID.

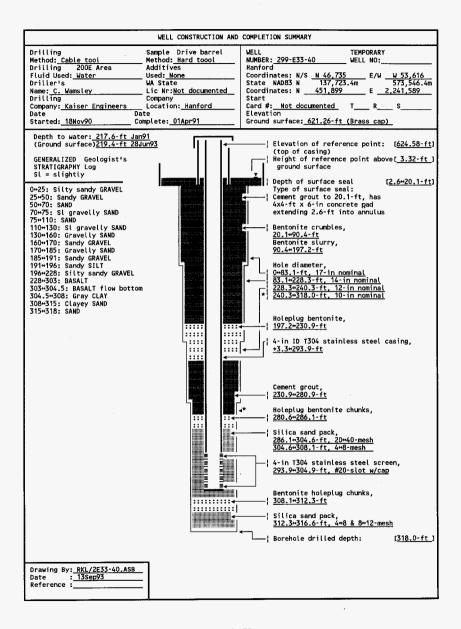
In underground radiation zone. DTW 220.2-ft, DTB 232.7-ft Top of pump support. AVAILABLE LOGS Geologist

TV SCAN COMMENTS Not applicable : DATE EVALUATED Not applicable EVAL RECOMMENDATION :

Not applicable 200-BP-1 monthly water level measurement, 01Mar91+28Jun93: LISTED USE

CURRENT USER WHC ES&M w/l monitoring and RCRA sampling, WHC ER characterization

PLIMP TYPE Hydrostan



299-E33-40 WELL DESIGNATION

RCRA FACILITY

Not applicable
200 BP-1 (200 Aggregate Area Management Study)
N 46,735 W 53,616 [30Jul91-200E]
N 451,899 E 2,241,589 [HANCONV]
N 137,723.38m E 573,546.44m [30Jul91-NAD83] CERCLA UNIT HANFORD COORDINATES : LAMBERT COORDINATES :

Apr91 DATE DRILLED 318.0-ft

DEPTH DRILLED (GS) : MEASURED DEPTH (GS) : Not documented DEPTH TO WATER (GS) :

217.6-ft, 02Jan91; 219.4-ft, 28Jun93 6-in, stainless steel, 7+3.0+70.5-ft; 4-in, stainless steel, +3.32+293.9-ft 624.58-ft [30Jul91-NCV)\*291 CASING DIAMETER ELEV TOP CASING 621.26-ft, Brass cap [30Jul91-NGVD 29] ELEV GROUND SURFACE :

Not applicable PERFORATED INTERVAL : 293.9+304.9-ft, 4-in stainless steel, #20-slot SCREENED INTERVAL

COMMENTS .

FIELD INSPECTION, 13May91; 6-in stainless steel casing. 4-ft by 4-ft concrete pad, 4 posts, 1 removable capped and locked, phass cap in pad with well ID.

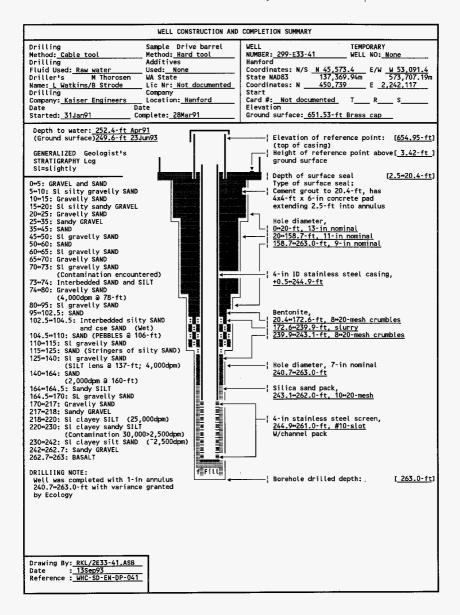
In underground radiation zone. AVAILABLE LOGS

Geologist Not applicable TV SCAN COMMENTS DATE EVALUATED Not applicable EVAL RECOMMENDATION : Not applicable

200-BP-1 monthly water level measurement, 01May91+28Jun93; LISTED USE

CURRENT USER WHC ES&M w/l monitoring, WHC ER characterization

PUMP TYPE Hydrostar



WELL DESIGNATION 299-E33-41 :

CERCLA UNIT 200 Aggregate Area Management Study

RCRA FACILITY Single Shell Tanks

N 45,773.4 W 53,091.4 [200E-11Jul91] N 450,739 E 2,242,117 [HANCONV] N 137,369.94m E 573,707.19m [NAD83-11Jul91] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Apr91 263.0-ft

DEPTH DRILLED (GS): MEASURED DEPTH (GS): Not documented 252.4-ft, 29Apr91; 249.6-ft, 23Jun93 DEPTH TO WATER (GS) :

4-in stainless steel, +0.5+279.2-ft; 6-in stainless steel, +3.4+~0.5-ft 654.95-ft, [NGVD 29-11Jul 91] CASING DIAMETER ELEV TOP CASING

654.95-ft, [NGVD'29-11Jul91] 651.53-ft, Brass cap [NGVD'29-11Jul91] ELEV GROUND SURFACE : PERFORATED INTERVAL :

Not applicable 244.9+261.0-ft, 4-in #10-slot stainless steel, with channel pack SCREENED INTERVAL

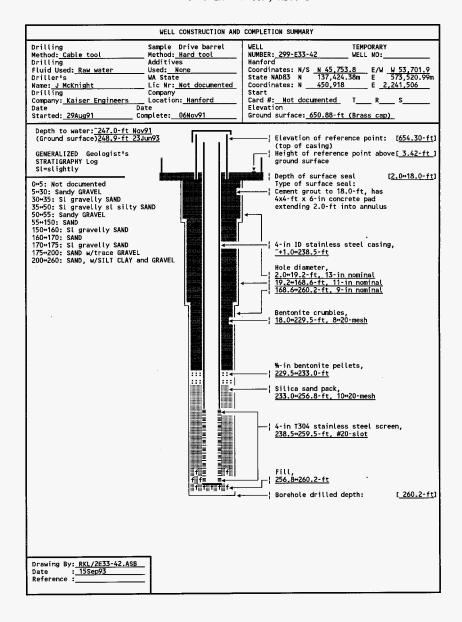
COMMENTS OTHER:

AVAILABLE LOGS Geologist, driller . Not applicable TV SCAN COMMENTS Not applicable DATE EVALUATED EVAL RECOMMENDATION : Not applicable

LISTED USE SST monthly water level measurement, 01Jun91+23Jun93, . .

WHC ES&M w/l monitoring and RCRA sampling, CURRENT USER

PUMP TYPE Hydrostar



299-E33-42 WELL DESIGNATION :

CERCLA UNIT 200 Aggregate Area Management Study :

RCRA FACILITY SST/BX-BY Tank Farm

N 45,753.8 W 53,701.9 [200E-12Dec91] N 451,649 E 2,238,486 [HANCONV] N 137,424.38m E 573,520.99m [NAD83-12Dec91] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Nov91

DEPTH DRILLED (GS):
MEASURED DEPTH (GS):
DEPTH TO WATER (GS): 260.2-ft Not documented 247.0-ft, 04Nov91

247.0-ft, 04Nov; 248.9-ft, 23Jun93 4-in stainless steel, 71.0#238.5-ft; 6-in stainless steel, 43.42#0.5-ft [NGVD'29-12bec91] CASING DIAMETER ELEV TOP CASING

654.30-ft, [NGVD'29-12Dec91] 650.88-ft, Brass cap [NGVD'29-12Dec91] ELEV GROUND SURFACE : Not applicable 238.5+259.5-ft, 4-in #20-slot stainless steel; PERFORATED INTERVAL :

SCREENED INTERVAL COMMENTS FIELD INSPECTION, 19May93;

4 and 6-in stainless steel casing.

4-ft by 4-ft concrete pad, 4 posts, 1 removable. Capped and locked, brass cap in pad with well ID.

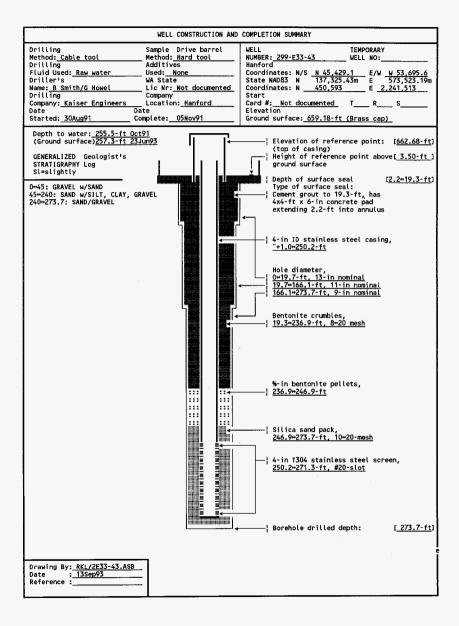
Not in radiation zone. OTHER:

AVAILABLE LOGS Geologist TV SCAN COMMENTS Not applicable : Not applicable DATE EVALUATED EVAL RECOMMENDATION : Not applicable

LISTED USE SST monthly water level measurement, 31Dec91+23Jun93,

CURRENT USER WHC ES&M w/l monitoring and RCRA sampling, Hydrostar, intake @ 254.0-ft

PUMP TYPE MAINTENANCE



200-F33-43 WELL DESIGNATION :

200 Aggregate Area Management Study CERCLA UNIT

RCRA FACILITY SST/BX Tank Farm

[200E-12Dec91] N 45,459.1 W 53,695.6 [200E-12Dec91] N 450,593 E 2,241,513 [HANCONV] N 137,325.43m E 573,523.19m [NAD83-12Dec91] HANFORD COORDINATES : LAMBERT COORDINATES :

DATE DRILLED Nov91

DEPTH DRILLED (GS):
MEASURED DEPTH (GS):
DEPTH TO WATER (GS): 273.7-ft Not documented 255.5-ft, 01Nov91;

257.3-ft, 23Jun93 CASING DIAMETER

257.3-ft, 25Juny5 4-in stainless steel, "+1.0\*250.2-ft; 6-in stainless steel, +3.50\*70.5-ft 662.68-ft, [NGVD'29-12Dec91] 659.18-ft, Brass cap [NGVD'29-12Dec91] ELEV TOP CASING ELEV GROUND SURFACE : Not applicable 250.2\*271.3-ft, 4-in #20-slot stainless steel; FIELD INSPECTION, 19May93; 4 and 6-in stainless steel casing. PERFORATED INTERVAL :

SCREENED INTERVAL : COMMENTS

4-ft by 4-ft concrete pad, 4 posts, 1 removable. Capped and locked, brass cap in pad with well ID.

Not in radiation zone. OTHER:

AVAILABLE LOGS Geologist TV SCAN COMMENTS Not applicable : Not applicable DATE EVALUATED : EVAL RECOMMENDATION : Not applicable

LISTED USE SST monthly water level measurement, 31Dec91+23Jun93, :

CURRENT USER WHC ES&M w/l monitoring and RCRA sampling Hydrostar, intake @ 268.5-ft

PUMP TYPE MAINTENANCE

DISTRIBUTION SHEET					
То	From	Page 1 of 1			
Distribution	J. A. Caggiano	Date September 25, 1996			
Project Title/Work Order		EDT No. 610766			
Assessment Groundwater Monitoring Plan for Single Shell Tank Waste Management Area B-BX-BY		ECN No. N/A			

Name	MSIN	Text With All Attach.	Text Only	Attach./ Appendix Only	EDT/ECN Only
D. Alison	R1-51	Х			
J. A. Caggiano	H6-06	X			
C. J. Chou	H6-06	X			
A. J. DiLiberto	H6-10	Х			
D. B. Engelman	L6-37	Х			
M. J. Furman	H0-12	Х			
L. A. Garner	R2-36	X			
M. J. Hartman	H6-06	X			
D. G. Horton	H6-06	Х			
D. F. Iwatate	H5-68	Х			
V. G. Johnson	H6-06	Х			
R. K. Price	N1-55	Х			
K. M. Thompson	H0-12	Х			
B. A. Williams	H6-06	X			
J. D. Williams	B2-35	Х			
Central Files	A3-88	Х			