

JUL 01 1997

21

ENGINEERING DATA TRANSMITTAL

1. EDT

Page 1 of 2  
621292

Station 34

2. To: (Receiving Organization) Distribution	3. From: (Originating Organization) Criticality and Shielding	4. Related EDT No.: 621292
5. Proj./Prog./Dept./Div.: SNF	6. Design Authority/ Design Agent/Cog. Engr.: K. N. Schwinkendorf	7. Purchase Order No.: NA
8. Originator Remarks: This calculation note documents the criticality analysis of a recent design change in the MCO scrap basket.		9. Equip./Component No.: NA
		10. System/Bldg./Facility:

11. Receiver Remarks:	11A. Design Baseline Document? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	12. Major Assm. Dwg. No.: NA
		13. Permit/Permit Application No.: NA
		14. Required Response Date:

15. DATA TRANSMITTED								
(A) Item No.	(B) Document/Drawing No.	(C) Sheet No.	(D) Rev. No.	(E) Title or Description of Data Transmitted	(F) Approval Designator	(G) Reason for Transmittal	(H) Originator Disposition	(I) Receiver Disposition
1	HNF-SD-SNF-CN-025		0	Results for Case A for Task Order 041-001	<del>8</del> N/A KN	3		

16. KEY					
Approval Designator (F)		Reason for Transmittal (G)		Disposition (H) & (I)	
E, S, Q, D or N/A (see WHC-CM-3-5, Sec.12.7)	1. Approval 2. Release 3. Information	4. Review 5. Post-Review 6. Dist. (Receipt Acknow. Required)	1. Approved 2. Approved w/comment 3. Disapproved w/comment	4. Reviewed no/comment 5. Reviewed w/comment 6. Receipt acknowledged	

17. SIGNATURE/DISTRIBUTION (See Approval Designator for required signatures)											
(G) Reason	(H) Disp.	(J) Name	(K) Signature	(L) Date	(M) MSIN	(G) Reason	(H) Disp.	(J) Name	(K) Signature	(L) Date	(M) MSIN
		Design Authority	L. W. Goldmann	R3-86		(See page 2 for signature)					
		Design Agent									
1		Cog. Eng.	K. N. Schwinkendorf	6/17/97	30-35						
1		Cog. Mgr.	J. Greenberg	6/19/97	35						
		QA									
		Safety									
		Env.									

18. K. N. Schwinkendorf Signature of EDT Originator 6/17/97	19. Authorized Representative Date for Receiving Organization	20. Greenberg Signature 6/19/97 Design Authority/Significant Manager Date	21. DOE APPROVAL (if required) Ctrl. No. <input type="checkbox"/> Approved <input type="checkbox"/> Approved w/comments <input type="checkbox"/> Disapproved w/comments
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**ENGINEERING DATA TRANSMITTAL**

Page 2 of 2  
621292  
1. EDT

2. To: (Receiving Organization) <b>Distribution</b>		3. From: (Originating Organization) <b>Criticality and Shielding</b>		4. Related EDT No.: <b>621292</b>	
5. Proj./Prog./Dept./Div.: <b>SNF</b>		6. Design Authority/ Design Agent/Cos. Engr.: <b>K. N. Schwinkendorf</b>		7. Purchase Order No.: <b>NA</b>	
8. Originator Remarks: <b>This calculation note documents the criticality analysis of a recent design change in the MCO scrap basket.</b>				9. Equip./Component No.: <b>NA</b>	
				10. System/Bldg./Facility:	
11. Receiver Remarks: 11A. Design Baseline Document? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No				12. Major Assm. Dwg. No.: <b>NA</b>	
<b>ENGINEERING DATA TRANSMITTAL</b>				13. Permit/Permit Application No.: <b>NA</b>	
				14. Required Response Date:	

15. DATA TRANSMITTED								
(A) Item No.	(B) Document/Drawing No.	(C) Sheet No.	(D) Rev. No.	(E) Title or Description of Data Transmitted	(F) Approval Designator	(G) Reason for Transmittal	(H) Originator Disposition	(I) Receiver Disposition
1	HNF-SD-SNF-CN-025		0	Results for Case A for Task Order 041-001	<i>S</i> <i>N/A</i>	3		

16. KEY					
Approval Designator (A)	Reason for Transmittal (G)			Disposition (H) & (I)	
E, S, C, D or N/A (See WHC-CN-3-5, Sec.12.7)	1. Approval	4. Review	5. Post-Review	1. Approved	4. Reviewed ns/comment
	2. Release	6. Dist. (Receipt Acknow. Required)		2. Approved w/comment	5. Reviewed w/comment
	3. Information			3. Disapproved w/comment	6. Receipt acknowledged

17. SIGNATURE/DISTRIBUTION (See Approval Designator for required signatures)											
(G) Reason	(H) Disp.	(J) Name	(K) Signature	(L) Date	(M) MSIN	(G) Reason	(H) Disp.	(J) Name	(K) Signature	(L) Date	(M) MSIN
1	1	Design Authority	<i>John Goldman</i>	7/1/97							
		Design Agent									
1		Cos. Engr. K. N. Schwinkendorf	<i>K. N. Schwinkendorf</i>	6/19/97							
1		Cos. Mgr. J. Greenberg	<i>J. Greenberg</i>	6/19/97							
		QA									
		Safety									
		Env.									

FAX TO  
Karen Noland  
373-3804  
from Lou - thales

18. K. N. Schwinkendorf <i>K. N. Schwinkendorf</i> Signature of EDT Date <i>6/19/97</i> Originator		19.  Authorized Representative Date for Receiving Organization		20. <i>Greenberg</i> <i>J. Greenberg</i> Signature Manager Date <i>6/19/97</i>		21. DOE APPROVAL (if required) Cert. No. <input type="checkbox"/> Approved <input type="checkbox"/> Approved w/comments <input type="checkbox"/> Disapproved w/comments	
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Louis H. Goldman R3-86

# Results for Case A for Task Order 041-001

**K. N. Schwinkendorf**

Fluor Daniel Northwest, Inc., Richland, WA 99352  
 U.S. Department of Energy Contract DE-AC06-96RL13200

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 Org Code: 403 Charge Code: E55480  
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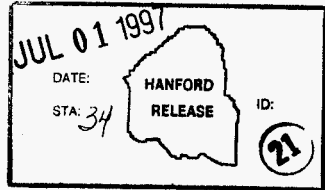
Key Words: Spent Nuclear Fuel, MCO, MCNP

**Abstract:** A design change in the Multicanister Overpack (MCO) container scrap basket has required a reevaluation for criticality safety. The bounding case, the drop accident case for MarkIV-loaded MCOs, was reanalyzed with less mass in the baseplate of the upper scrap basket. The reduction in mass was from 50 lb to 27lb. No statistically significant difference between the two cases was found. The original analysis is therefore considered valid and no additional analysis is required.

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Karen H. Roland 7/1/97  
 Release Approval Date

Release Stamp

**Approved for Public Release**

**CHECKLIST FOR INDEPENDENT REVIEW**

Document Reviewed: Results for CASEA for Task Order 041-001

Author: K. N. Schwinkendorf

Yes No N/A

- Problem completely defined.
- Necessary assumptions explicitly stated and supported.
- Computer codes and data files documented.
- Data checked for consistency with original source information as applicable.
- Mathematical derivations checked including dimensional consistency of results.
- Models appropriate and used within range of validity or use outside range of established validity justified.
- Hand calculations checked for errors.
- Code run streams correct and consistent with analysis documentation.
- Code output consistent with input and with results reported in analysis documentation.
- Acceptability limits on analytical results applicable and supported. Limits checked against sources.
- Safety margins consistent with good engineering practices.
- Conclusions consistent with analytical results and applicable limits.
- Results and conclusions address all points required in the problem statement.
- Have all reasonable accidents been considered?
- Has low density water (steam) been evaluated as a moderator?
- Is the fuel and other hardware composition correct?
- Are the cases considered conservative? Too conservative?
- Do the computer models adequately reflect the actual geometry? Have cross sectional cuts of the geometry been made and do they show the desired geometry?
- Has the analysis been reviewed by Safety? This may not be required in a preliminary design.
- Has the reviewer completed the Criticality Safety Course for Managers and Engineers?

Reviewed by: Victor Roetman Date 6/18/97

NOTE: Any hand calculations, notes, or summaries generated as part of this review should be signed, dated, and attached to this checklist. Materials should be labeled and recorded so that it is intelligible to a technically-qualified third party.

## RESULTS FOR CASE A FOR TASK ORDER 041-001

**Methodology**

The Monte Carlo N-Particle (MCNP) (Breismeister 1993) computer code was used to perform the calculation documented in this report. MCNP was used to perform a Monte Carlo simulation of the transport of neutrons through a model of the Multicanister Overpack (MCO) container to obtain a statistical estimate of the effective neutron multiplication factor,  $k_{\text{eff}}$ .

**Assumptions**

MCNP calculation CASE4 (Schwinkendorf 1997) was based on an assumption of 3/8-inch stainless steel baseplates forming the bottom of the scrap baskets. These baseplates are assumed in the MCNP input model to be solid (the holes are not explicitly modeled). Given the diameter of the baseplate, this model includes nearly 50 lbs of steel. The current scrap basket design calls for 27.13 lb instead of the 50 lbs assumed in the reference. This calculation was therefore modified by reducing the material density of the scrap basket baseplate so that the weight is reduced to 27.13 lb.

CASE4 is the Mark IV-loaded MCO after the drop accident, where all the intact fuel in the central three fuel baskets are assumed to fragment, and pack together into an optimal configuration with a packing fraction of 0.4 (the scrap baskets in the top and bottom locations remain loaded with optimal 0.95 wt% enriched uranium metal scrap).

**Input Data**

The input file for this calculation may be found in filename case4\_nu.inp, located on the workstation server disk under the directory: /home\_area/h56712/mcnp This data file is also appended to this calculation note.

**Calculations**

This calculation was performed using 50 neutron generations of 1,000 neutron histories per generation, and 10 generations were skipped before statistical information was included in the result. The calculation was performed on the sg1 Silicon Graphics workstation.

**Results**

The results are as follows:

CASE4 from the Schwinkendorf reference:

$$k_{\text{eff}} = 0.9341 \pm 0.0028, 95\% \text{ upper bound estimate} = 0.9398$$

Modified CASE4 with the reduced-density scrap basket baseplate:

$$k_{\text{eff}} = 0.9329 \pm 0.0027, 95\% \text{ upper bound estimate} = 0.9382$$

## Conclusions

The removal of neutron-absorbing material (reduced steel density in the scrap basket baseplate) from the MCNP model should have increased the  $k_{\text{eff}}$  of the system. However, this change in the model is so slight that MCNP was not able to discern a statistically-significant difference in the neutron multiplication constants between the two cases. The difference between the two  $k_{\text{eff}}$  values is only one-third of the 1-sigma statistical error in the two cases. The conclusion is that, within the statistical uncertainty in the Monte Carlo results, there is no statistically significant difference between how the scrap basket baseplates were modeled in the reference and the modified design. It is felt that no further analysis is required.

## References

- Breismeister, J. F., Editor, 1993, *MCNP — A General Monte Carlo N-Particle Transport Code, Version 4A*, LA-12625, Los Alamos National Laboratory, Los Alamos, New Mexico.
- Schwinkendorf, K. N., 1997, *Criticality Safety Evaluation Report for Spent Nuclear Fuel Processing and Storage Facilities*, HNF-SD-SNF-CSER-005 Revision 3, Fluor Daniel Northwest, Richland, Washington.

## MCNP input file

The following is a listing of the input file used to perform this calculation:

message:

```

multiple canister over-pack - RUN 4 - MKIV Drop Case
1 1 -18.82 -1 u=1 imp:n=1 $ MKIV fuel scrap
2 2 -6.55 1 -2 u=1 imp:n=1 $ fuel clad
3 4 -1.00 2 u=1 imp:n=1 $ lattice water
4 0 -5 6 -9 8 -7 10 lat=2 u=2 fill=1 imp:n=1
5 1 -18.82 -3 u=3 imp:n=1 $ MKIV fuel rubble
6 2 -6.55 3 -4 u=3 imp:n=1 $ fuel clad
7 4 -1.00 4 u=3 imp:n=1 $ lattice water
8 0 -11 12 -15 14 -13 16 lat=2 u=4 fill=3 imp:n=1
9 4 -1.00 -20 21 -19 imp:n=1 $ top water reflector
10 4 -1.00 -21 22 -17 imp:n=1 $ water in gap #1
11 0 -17 -22 23 fill=2 imp:n=1 $ scrap in basket #1
12 3 -4.717 -23 24 -17 imp:n=1 $ ss plate #1
13 0 -17 -24 25 fill=4 imp:n=1 $ MKIV rubble #2
14 3 -8.03 -25 26 -17 imp:n=1 $ ss plate #2
15 0 -17 -26 27 fill=4 imp:n=1 $ MKIV rubble #3
16 3 -8.03 -27 28 -17 imp:n=1 $ ss plate #3
17 0 -17 -28 29 fill=4 imp:n=1 $ MKIV rubble #4
18 3 -8.03 -29 30 -17 imp:n=1 $ ss plate #4
19 0 -17 -30 31 fill=2 imp:n=1 $ scrap in basket #5
20 3 -8.03 -31 32 -17 imp:n=1 $ ss plate #5
21 3 -8.03 -32 33 -18 imp:n=1 $ ss mco bottom end cap
22 3 -8.03 36 -18 -21 32 imp:n=1 $ steel on side of mco
23 4 -1.00 -19 18 -21 33 imp:n=1 $ water surrounding mco
24 4 -1.00 -33 34 -19 imp:n=1 $ water below ss end cap
25 3 -8.03 17 -35 32 -21 imp:n=1 $ mco liner
26 4 -1.00 35 -36 32 -21 imp:n=1 $ water gap
27 0 20: -34: 19 imp:n=0 $ outside world

1 cz 0.9 $ optimum scrap radius

```

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2	cz	0.96444					\$ scrap token clad radius
3	cz	1.5					\$ optimum rubble radius
4	cz	1.60741					\$ rubble token clad radius
5	px	1.51418					\$ lattice hexagon planes for scrap
6	px	-1.51418					
7	p	-0.57735	1.0	0.0	1.74842		
8	p	0.57735	1.0	0.0	-1.74842		
9	p	0.57735	1.0	0.0	1.74842		
10	p	-0.57735	1.0	0.0	-1.74842		
11	px	2.25861					\$ lattice hexagon planes for rubble
12	px	-2.25861					
13	p	-0.57735	1.0	0.0	2.60802		
14	p	0.57735	1.0	0.0	-2.60802		
15	p	0.57735	1.0	0.0	2.60802		
16	p	-0.57735	1.0	0.0	-2.60802		
17	cz	29.5275					\$ basket diameter 23.25"
18	cz	50.8					\$ outer steel radius 20"
19	cz	81.28					\$ water outside mco
20	pz	209.48565					\$ top of water reflector
21	pz	179.00565					\$ top of water gap #1
22	pz	161.03685					\$ top of scrap #1
23	pz	93.79035					\$ top of ss plate #1
24	pz	92.83785					\$ top of MKIV rubble #2
25	pz	31.58095					\$ top of ss plate #2
26	pz	30.62845					\$ top of MKIV rubble #3
27	pz	-30.62845					\$ top of ss plate #3
28	pz	-31.58095					\$ top of MKIV rubble #4
29	pz	-92.83785					\$ top of ss plate #4
30	pz	-93.79035					\$ top of scrap #5
31	pz	-161.03685					\$ top of ss plate #5
32	pz	-161.98935					\$ top of ss end cap
33	pz	-181.03935					\$ bottom of ss end cap
34	pz	-211.51935					\$ water below ss end cap
35	cz	30.7975					\$ mco liner
36	cz	31.75					\$ water gap
mode n							
kc	code	1000	1.0	10	50		
ks	rc	12.11344	0.0			122.89155	
		-12.11344	0.0			122.89155	
		9.03444	0.0			59.1947	
		-9.03444	0.0			59.1947	
		9.03444	0.0			0.0	
		-9.03444	0.0			0.0	
		9.03444	0.0			-59.1947	
		-9.03444	0.0			-59.1947	
		12.11344	0.0			-122.89155	
		-12.11344	0.0			-122.89155	\$ 10 source points
m1		92235.50c	-0.009471	92238.50c	-0.990529		\$ mkiv inners
m2		40000.50c	-1.000				\$ zr clad
m3		6000.50c	-0.0004				\$ stainless steel 304
		25055.50c	-0.0200				\$ (8.03 g/cc)
		14000.50c	-0.0100				
		24000.50c	-0.1900				
		28000.50c	-0.0925				
		26000.55c	-0.6871				
m4		1001.50c	-0.1119	8016.50c	-0.8881		\$ water
mt4		lwtr.01t					
m5		6000.50c	-0.000396				\$ borated stainless steel 304
		25055.50c	-0.0198				\$ (8.03 g/cc)
		14000.50c	-0.0099				
		24000.50c	-0.1881				
		28000.50c	-0.091575				
		26000.55c	-0.680229				
		5010.50c	-0.00199				
		5011.55c	-0.00801				
m6		92235.50c	-0.009471	92238.50c	-0.990529		\$ mkiv outers

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## DISTRIBUTION SHEET

To Distribution	From Criticality and Shielding	Page 1 of 1
Project Title/Work Order Results for Case A for Task Order 041-001		Date June 17, 1997
		EDT No. 621292
		ECN No.

Name	MSIN	Text With All Attach.	Text Only	Attach./ Appendix Only	EDT/ECN Only
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P. J. Bedell	S0-04	X			
J. Greenborg	H0-35	X			
K. N. Schwinkendorf	H0-35	X			
K. M. Walterskirchen	G3-17	X			
J. L. Wise	X3-85	X			
Central Files (1 + Original)	A3-88	X			
<i>KN</i> L. H. Goldman	R3-86	X			