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DESIGN OF A DIAGNOSTIC AREA-TYPE BEAM POSITION MONITOR FOR X-RAY BEAMLINES AT THE NATIONAL SYNCHROTRON LIGHT SOURCE

NATIONAL SYNCHROTRON LIGHT SOURCE

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DESIGN OF A DIAGNOSTIC AREA-TYPE BEAM POSITION MONITOR FOR X-RAY BEAMLINES AT THE NATIONAL SYNCHROTRON LIGHT SOURCE

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ABSTRACT

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We have built a prototype area-type beam position monitor for use as a diagnostic tool at the National Synchrotron Light Source. The device is compact and fits into a vacuum cross. We completed range and resolution tests of the device at beamline X-19A at the NSLS and concluded that such a monitor can be placed in the confines of the vacuum cross.

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I. INTRODUCTION:

In many cases, the stability of a photon beam provided by a synchrotron is of utmost importance in order that experimenters may take advantage of the transverse dimensions of a photon beam. For this reason, efforts must be made to keep such beam deviation to within a fraction of the beam's transverse dimensions. [1]

To counter this problem, the NSLS is currently developing a family of photon beam position monitors for use on the beamlines as feedback and diagnostic elements in hopes that a device which is sufficiently general in design and relatively inexpensive will gain acceptance from both users and accelerator physicists. Such devices exploit the photo-electric effect and all should also have sensitivity on the order of microns. [1]

The following paper presents our design for an "area-type" beam position monitor (BPM) which is actually a split ionization-chamber as described by Tischler et al. [2]. We have designed it such that it has a generic design in that it can fit into a vacuum cross and with minor modifications can double as a normal ion-chamber, and it was inexpensive.



II. THEORY

The split ion-chamber differs from a conventional ion chamber in that the low potential side of the chamber consists of two triangular plates (splitters) instead of one (fig. 1), and associated with each of these splitters is a current dependent upon the

potential between it and the full plate yet independent of the other splitter.

In essence, the incident beam passes over the first splitter and ionizes the gas residing in the chamber via the photo-electric effect. Electrons resulting from the collisions of photons and gas particles seek the low potential split plates while their counterpart ions go to the the high potential. This results in a current later defined as I_T registered at the top splitter.





Continuing on its flight, the photon beam passes over the bottom plate and photons within the beam collide with gas particles resulting in current I_B at the bottom plate.

Assuming the photon beam to be a Gaussian, one may show that the top and bottom currents are respectively,

$$I_{\tau} = \frac{I_{o}(t)}{\sigma\sqrt{2\pi}} \tan\theta \int_{-\frac{h}{2}}^{\frac{h}{2}} (\delta + \frac{h}{2}) \exp\left[\frac{-z^{2}}{2\sigma^{2}}\right] dz$$

and

$$I_{B} = \frac{I_{o}(t)}{\sigma\sqrt{2\pi}} \tan\theta \int_{-\frac{h}{2}}^{\frac{h}{2}} (\frac{h}{2} - \delta) \exp\left[\frac{-z^{2}}{2\sigma^{2}}\right] dz$$

where height h of the nested plates, the pitch angle θ and the beam height σ are defined in fig. 2.

In and of themselves the currents I_T and I_B tell us nothing about beam position.

However, the difference over the sum of the two currents yields the beam displacement δ from the center of the monitor, or

$$\mathsf{P}(\delta) = \frac{\mathsf{I}_{\mathsf{T}} - \mathsf{I}_{\mathsf{B}}}{\mathsf{I}_{\mathsf{T}} + \mathsf{I}_{\mathsf{B}}}$$

thus allowing for a 1:1 mapping from electronic to spacial quantities [1].

Figure 3. A Vacuum Cross



III. DESIGN

We have designed half of an area-type beam position monitor which fits into a stainless steel vacuum cross (fig. 3). The completed device would consist of two such vacuum crosses placed in a line and each containing monitors oriented perpendicular to one another.

In designing our prototype BPM, we have constrained ourselves to the parameters of low-cost, simplicity of design, and the dimensions of a vacuum cross. To such an end, we built this BPM with a limit on specialized machining and focused on drawing ready-made components from available stock thus optimizing the cost and simplicity of the device.

In essence, an Aluminum channel connected on one end by a conflat flange with a round hole in the center slides into the vacuum cross. The high-voltage plate connects to one side of the Al channel while the two splitters connect to the other side to form a rectangle. All such plates have been tapped and connect to the channel via nylon screws. Appendix A contains a photograph of our BPM while Appendix B contains the a scale assembly diagram and Appendix C the blueprints used in designing the device.

IV. EXPERIMENTAL

We carried out preliminary testing of our half-BPM on NSLS beamline X-19A with a 1mm high monochromatic, 7 keV x-ray beam in an open air environment. We placed a 300V potential between the plates and oriented the device such that the plates were perpendicular to the experimental floor.



We simulated beam motion by mounting the BPM on a stepping motor stage which would scan the BPM in the the horizontal and vertical dimensions. Using a laser position finder and burns on x-ray sensitive paper, we roughly positioned the beam near the center of the BPM. Keithley preamplifiers boosted the incoming signal, and countrate vs. postion data was recorded by the in-house ACE program [3]. Figure 4. represents a schematic of our experimental setup.

V. RESULTS

Appendix D contains the raw data collected during our experiment. We

completed data analysis with the XMGR program.

Figure 5a represents a vertical scan within the limits of the BPM while the beam is centered on the horizontal We have defined the signal starting in the upper left hand corner as I_1 and the bottom left to be I_2 . Notice as I_1 registers a high count rate, I_2 registers a much lower count rate. As the beam (or in our case the motor) approaches the horizontal origin, the signal I_1 decreases as I_2 increases. The intersection of the I_1 and I_2 represent the geometric vertical center where both splitters will register similar currents (that is $I_1 = I_2$).

Note also in figure 5a. that if the beam had been properly centered, the intersection of I_1 and I_2 would occur at zero-point on the Vertical Position (mm) axis. We will touch upon this more fully in the discussion.

Figure 5b. represents the difference over the sum of the signals I_1 and I_2 . Here it is important to note that the difference over the sum be a straight line, and in this case it nearly is straight.

Figure 6a. represents another vertical scan but the beam has been displaced 4mm from the horizontal. We feel that the "electron deficiency" in the top left of the l_1 signal occurs because the l_1 splitter resides in close proximity to the AI channel wall which "robs" photo-electrons originally in-bound for the l_1 splitter. Perhaps the cause of this problem is due to the electrical edge effects on the side of the plate.

Dips also occur in both I_1 and I_2 at this position. We can provide no satisfactory explanation to this problem

Figure 6b. shows us the difference over the sum of the signals I_1 and I_2 from figure 6a. It is apparent that the electron deficiency is of no consequence. However the central dip in the difference over the sum shows that the device cannot provide adequate resolution at 4mm from the horizontal.

VI. DISCUSSION OF RESULTS

It is apparent from figure 5a that we did not center the beam properly. To exploit the difference over the sum as a mapping tool it is helpful that the beam be centered inside the high and low voltage plates during calibration. Although this is not necessary, it is far easier to center the beam and get an absolute result as opposed to not centering the beam and having to make further necessary calculations.

We have proposed a modification to the initial beam positioning procedure which should be implemented in the future. Using a laser position finder and x-ray burns one

Figure 5a.



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Figure 5b.



Figure 6a.

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Figure 6b.



can roughly postion the beam in the center of the device as we have. The next step, the one we neglected to implement, is to set up a cross-hair across the face of the device, the intersection of which is centered across the high and low voltage plates. At this point one must produce more burns while moving the motor stage such that the device centers itself on the beam.

It appears that the electron deficiency seen in I_1 of figure 6a. is of no consequence because there is no trace of it in the difference over sum (fig. 6b.). However, it would be ecclectically pleasing to get rid of this behavior and thus we propose a solution of milling a 3/4" slot down the channel wall such that electrons which normally would go there, are incapable because of the greater distance between the channel wall and the splitter. A second and more common solution would be to place buffer plates close to but not touching the ends of the two splitters. Each of these plates would maintain a potential equal to that of one of the plates.

Regarding the central dips in figure 6a., we suggest milling a slot down the center of the splitter mounting wall. Like the slot above, it would allow the individuals splitters to attract their photo-electrons without the interference of the lower potential channel wall.

VII. CONCLUSIONS

This paper has discussed the design and performance of a low-cost and inexpensive area-type beam postition monitor built almost exclusively of NSLS stock materials. The next stage in development of this BPM is to build a second prototype with modifications as discussed in section VI. Assuming success, a duplicate will be placed in line with the existing half-BPM such that the two will allow an x-ray beam to pass unmolested. Following such, we will seal our BPM and run free-flowing helium through the monitor and test the completed monitor with potentials higher than 300V.

Though our BPM cannot provide adequate resolution for current needs, our project has been a success in that we have designed a low-cost BPM of sufficiently general design to build the majority of components from existing materials. We feel that further generations of this device will provide the necessary resolution as well as the existing features previously discussed.

VIII. ACKNOWLEDGEMENTS

We thank R. Thomas and the the DOE Science and Engineering Research Semester Program for funding this project. One of us (D.C.) thanks the NSLS R&D machinists R. Green and G. Nintzel for suggestions and help during the developmental stages. Likewise, D.C. thanks G. Vanderlaske for his timeless patience in teaching machine skills and shop safety at the NSLS User Machine Shop. D.C. also thanks E. Fontes for taking time to proof this paper. Special thanks go to D.C.'s advisor L. Berman for his guidance, generosity, and friendship.

IX. REFERENCES

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[3] S.K. Feng-Berman, D.P. Siddons, and L.E. Berman, Nucl. Instrum Methods Phys. Research Sect. A, <u>347</u>, 603-606 (1994)

APPENDIX A: PHOTOGRAPH OF BPM



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| 51 | 4.7500 | 100001 | 34658 | 16493 | 9479 |
| 52 | 5.0000 | 100001 | 34630 | 16726 | 923Ġ |
| 53 | 5.2500 | 100002 | 34658 | 16989 | 9001 |
| 54 | 5.5000 | 100002 | 34642 | 17228 | 8742 |
| 55 | 5.7500 | 100001 | 34651 | 17487 | 8482 |
| 56 | 6.0000 | 100001 | 34636 | 17736 | 8216 |
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scan pv -8 6.25 at 4mm (horiz position) *.* . -: