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ANL/ET/CP -- 89105RECEIVED STRENGTH AND FLEXIBILITY OF BULK NOV 1 ? 1996 HIGH-T_c SUPERCONDUCTORS* OSTI

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MFA-3

Strength and Flexibility of Bulk High-T_c Superconductors

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Abstract—Strength, fracture toughness, and elastic modulus data have been gathered for bulk high-temperature superconductors, commercial 99.9% Ag, and a 1.2 at.% Mg/Ag alloy. These data have been used to calculate fracture strains for bulk conductors. The calculations indicate that the superconducting cores of clad tapes should begin to fracture at strains below 0.2%. In addition, residual strains in Ag-clad (Bi,Pb)₂Sr₂Ca₂Cu₃O_x tapes have been measured by neutron diffraction. An explanation is offered for why many tapes appear to be able to tolerate large strains before exhibiting a reduction in current transport.

I. INTRODUCTION

Although engineering critical current density remains the primary consideration for high-temperature superconductor wires, strength and flexibility are also important [1,2]. Large bodies of mechanical-property data have been published for bulk YBa₂Cu₃O_x (Y-123), Bi₂Sr₂CaCu₂O_x (Bi-2212) and (Bi,Pb)₂Sr₂Ca₂Cu₃O_x (Bi-2223), but not TI-based superconductors. Relevant data for each system will be presented and discussed. Literature values will be used for Y-123, Bi-2212, Bi-2223, Tl₂Ba₂Ca₂Cu₃O_x (TI-2223), Ag, and a 1.2 at.% Mg/Ag alloy. New data will be presented for Tl₂Ba₂CaCu₂O_x (TI-2212), and residual-stress data obtained by neutron diffraction will be presented for a Bi-2223/Ag composite tape [2,3].

The goal of this work is to reconcile bulk strength and stiffness data with strain-tolerance reports for Ag-clad tapes [4-8]. It has generally been found that apparent strain tolerances are much higher than would be expected for conductors containing hard brittle cores.

II. EXPERIMENTAL DETAILS

Data for fracture strength, toughness, and elastic modulus were gathered for several superconductors and two Ag alloys.

A. Materials

Two types of Y-123 specimens were used. Strength data were obtained on extruded wires ≈ 0.85 mm in diameter

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[9,10]. Other data were obtained from sintered pellets [10,11]. All Y-123 samples were virtually phase pure, with nearly randomly oriented grains less than $\approx 10 \,\mu$ m in size.

All of the mechanical-property data for Bi-2212 and Bi-2223 were obtained from hot-forged bars. Such materials are highly phase pure, exhibit very strong c-axis textures, and are > 95% dense [12-17]. Data for Bi-2223 composites containing MgO and Ag will also be discussed [18]. Monofilament Ag-clad Bi-2223 tapes [2] for residual strain measurements were fabricated by American Superconductor Corporation (Westborough, MA).

The TI-2212 and TI-2223 compounds were chosen for fabrication and characterization because of their stability relative to other TI-based superconductors [19,20]. Although the TIBa₂Ca₂Cu₃O_x phase is probably of more interest for bulk applications, we were unable to produce dense specimens of good phase purity [21]. The TI-2212 was synthesized in highly phase pure form from hydroxide precursors [22,23]. Details of the TI-2223 have been published [20]. Dense specimens were prepared by wrapping powder compacts in Ag foil and forging at ~835°C in air. Final stresses were 30-40 MPa. The resultant bars were $\approx 90\%$ dense.

The 99.9% Ag alloy was purchased from Johnson-Matthey (Ward Hill, MA) and the 1.2 at.% Mg alloy (referred to henceforth as AgMg) from Vacuumschmeltze (Hanau, Germany). Chemical analysis and microstructural details have been published [24,25].

B. Characterization

Microstructures were examined by X-ray diffraction and scanning electron microscopy (SEM). Both fractured and polished surfaces were examined.

Strength (σ) and fracture toughness (K_{IC}) values were measured in three- or four-point bending [26]. Details have been published [10,12-15]. Elastic modulus was measured ultrasonically [16,27,28].

New data were obtained for yielding of the two Ag alloys. Specimens were tested in compression in an Instron universal tester Model 4505 (Canton, MA). Alloys were tested in the soft-annealed state, after having been work hardened \approx 70%, and for the AgMg, after having been heat treated in O₂ at 900°C to induce precipitation hardening through formation of MgO [25].

For the residual strains, a bundle was packed from tape sections 100 μ m thick and 20 mm long. The bundle filled a volume =10 mm in diameter and 20 mm in length. Strains were measured in a direction perpendicular to the long axis of each tape. The diffraction peaks for a variety of crystallographic direction were very sharp. Bi-2223 powder and 99.9% Ag strip were used as references. The error in the average strain measurements was about $\pm 0.01\%$ [3].

III. RESULTS AND DISCUSSION

The microstructures of the Y-123 specimens were nearly randomly oriented. Because they were hot forged, the other specimens exhibited c-axis textures. Textures for the TI-2212 and TI-2223 specimens were moderate, those for the Bi-2212 and Bi-2223 specimens were strong. Individual grains for the Y-123, TI-2212, and TI-2223 specimens had aspect ratios generally < 3; the Bi-2212 and Bi-2223 specimens had grain aspect ratios > 10 (Fig. 1).

The microstructures of the Bi-based specimens are similar to those obtained in powder-in-tube tapes or thick films [1]. They are conducive to good current transport. It would be best if all of the specimens tested had similar microstructures. Bi-2212 and Bi-2223 grains are by nature more platelike than other high-temperature superconductor grains, however, and only they could be aligned effectively by hot forging.



Fig. 1. SEM photomicrographs of fracture surfaces of (a) TI-2212 test specimen and (b) Bi-2212 test specimen. The grains of the Bi-2212 are much more elongated and strongly textured.

Basic mechanical-property data for these specimens are shown in Table I. The individual grains of all hightemperature superconductors have highly anisotropic properties [16,29-32], and thus comparisons of the data shown in Table I must be made with caution. We have not found any strengths reported that are more than =15% higher than those listed in Table I. It is noted that the microstructures shown in Fig. 1 are rather good for strength. Large-grained melt-textured materials exhibit significantly lower strengths [33]. Furthermore, additions of Ag particles or ceramic particles or whiskers provide at best only moderate improvements to strength of stiffness [14,18]. By Hooke's law for elastic materials, one can see that none of the superconductors is likely to exhibit a strain to failure >0.2%.

The Ag data are of interest because in Ag/superconductor composites the alloy sheath will carry some any applied stress and the sheath may impart a residual stress to the superconductor core because of differences in the coefficients of thermal expansion.

The residual stresses for Ag/Bi-2212 or Bi-2223 tapes are particularly complicated because of the configuration and crystal anisotropy. The thermal expansion of Ag [34] is $19-23 \times 10^{-6}$. The thermal expansion of Bi-2223 varies from 14 to 24 x 10^{-6} , with the larger expansion being in the c-axis direction [29]. It is difficult to predict, even the sign, of the residual stresses in the Ag or superconductor core. Neutron diffraction measurements at the Intense Pulsed Neutron Source at Argonne National Laboratory yielded the average strains in the Ag sheath and Bi-2223 core in various crystallographic directions. It was found that the Ag had an average compressive strain of 0.062% and the Bi-2223 had an average tensile strain of 0.034%.

If one approximates the residual stress by Hooke's law, the residual stresses in both components are 40–50 MPa, which is a large fraction of the fracture stress for monolithic superconductors. The stress sate is favorable, as the superconductor core is in compression. A further residualstress advantage might be realized if stronger and stiffer alloy sheaths were to be used. Larger favorable stresses might be generated [24].



Fig. 2. Schematic diagram of current transport path in an Ag/Bi-2223 tape.

Material	Density (g/cm ³)	E (GPa)	σ (MPa)	K _{IC} (MPa√m)
Ag - annealed	10.6	76	65	
AgMg - annealed AgMg - cold worked	10.5	74 74	48 220	
AgMg – oxidized Y–123	10.5 6.3	85 148*	385 230	1.5-2.0
Bi-2212 Bi-2223	6.5 6.4	118, 44** 82*	145 145	2.9 2.9
T1–2212	6.4		120	2.6
T1-2223	6.0	101*		1.2

TABLE I
SUMMARY OF MECHANICAL-PROPERTY DATA AND APPROXIMATE DENSITIES

*Average value.

****Values for a-b plane and c-direction for highly textured specimens.**

All of the data indicate that even within a metallic sheath, a superconductor core should not be able to withstand a strain of more than about 0.2% before cracking. Yet strains to 0.5–1.0% without apparent degradation of superconducting properties are often cited for Ag-clad Bi-2223 conductors. This discrepancy has been convincingly explained recently. Current can flow around cracks by shunting through the metallic sheath, as shown schematically in Fig. 2. So long as there are sufficiently few cracks and they are sufficiently sharp, the critical current density measured with a 1 μ V/cm criterion will not be affected. Details of this analysis can be found in Refs. 35 and 36.

IV CONCLUSION

Mechanical-property data for monolithic high-temperature superconductors and residual-strain date for Ag/Bi-2223 tapes indicate that superconductor cores should crack at strains no greater than $\approx 0.2\%$. The apparent larger strain tolerances of clad conductors is due to current shunting around the crack and passing through the metallic sheath.

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