### CASKS (Computer Analysis of Storage CasKS): A Microcomputer Based Analysis System for Storage Cask Design Review

User's Manual to Version 1b (Including Program Reference)

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# Abstract

CASKS (Computer Analysis of Storage casKS) is a microcomputer-based system of computer programs and databases developed at the Lawrence Livermore National Laboratory (LLNL) for evaluating safety analysis reports on spent-fuel storage casks. The bulk of the complete program and this user's manual are based upon the SCANS (Shipping Cask ANalysis System) program previously developed at LLNL. A number of enhancements and improvements were added to the original SCANS program to meet requirements unique to storage casks. CASKS is an easy-to-use system that calculates global response of storage casks to impact loads, pressure loads and thermal conditions. This provides reviewers with a tool for an independent check on analyses submitted by licensees.

CASKS is based on microcomputers compatible with the IBM-PC family of computers. The system is composed of a series of menus, input programs, cask analysis programs, and output display programs. All data is entered through fill-in-the-blank input screens that contain descriptive data requests.

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## **Executive Summary**

Lawrence Livermore National Laboratory previously developed a microcomputer-based analysis system—SCANS—to assist the Nuclear Regulatory Commission in performing confirmatory analyses for licensing review of radioactive-material shipping cask designs. Because the structure of the shipping cask and the storage cask are similar, we have employed the basic SCANS program to simulate the responses of a storage cask under impact or thermal conditions. A number of enhancements and additions unique to the storage cask were added to the program; however, the overall program layout remains the same. The modified program is named **CASKS**. This volume is the user's manual and program reference which closely follows the format in SCANS Vol. 1—User's Manual to Version 1a. In this volume, we describe the system requirements, installation and operation of **CASKS**, the contents of the **CASKS** distribution diskettes, how **CASKS** is implemented in a DOS environment, and the structure of **CASKS** databases. Theory documents for each analysis module can be found in Volumes 2-5 of SCANS. Appendix G includes the titles and contents for each theory document.

# Introduction

# CASKS (Computer Analysis of Storage $\mbox{CasKS}^*$ ) Based on the SCANS System

The U.S. Nuclear Regulatory Commission previously requested that the Lawrence Livermore National Laboratory develop an integrated software system to conduct confirmatory analyses of *shipping casks*. The analyses were to ensure structural integrity under a series of normal operating loads and hypothetical accident loads as specified in Title 10 of the *Code of Federal Regulations* (1983). As a result, SCANS Version 1a was produced by LLNL in 1988.

SCANS is a microcomputer-based system of computer programs for evaluating safety analysis reports on spent-fuel shipping casks. The system is easy to use and provides an independent check for reviewing the analyses submitted by licensees. SCANS calculates the global response of the shipping casks to impact loads, thermal conditions and pressure loads.

In 1989, the U.S. Nuclear Regulatory Commission requested that LLNL develop a microcomputer-based computer program for evaluating the safety analysis reports on *spent-fuel storage casks* based on the SCANS code. Because the structural designs of the two casks are similar, we used the existing framework in the SCANS program and made a number of enhancements and modifications to accommodate requirements unique to storage casks. The modified program is named CASKS. This user's manual describes the system requirements, installation and operation of CASKS.

### **CASKS System Design**

Structured the same way as SCANS, the CASKS system is composed of a series of menus, input programs, cask-analysis programs and output-display programs. CASKS performs the analysis after the user prepares the input data and chooses an appropriate analysis—impact, thermal (heat transfer), thermally-induced stress, or pressure-induced stress. All data is entered through fill-in-the-blank input screens with descriptive data requests. CASKS provides default values where possible and always evaluates input data for correctness before it is accepted.

To evaluate impact analyses, **CASKS** uses a one-dimensional dynamic beam model. Each node in the beam model has two translational degrees of freedom and one rotational degree of freedom. The impact code uses an explicit time-history integration scheme in which equilibrium is formulated in terms of the global external forces and internal force resultant. This formulation allows the code to track large, rigid-body motion. Thus, **CASKS** can calculate the oblique impact problem from initial impact through essentially rigid-body rotation to secondary impact, and, if required, lateral pressure due to lead-slump.

CASKS allows the user to analyze cask impact on either an unyielding or a yielding surface. A yielding surface is represented as a series of nonlinear force-deflection relationships. To analyze yielding surface cask impact, CASKS first combines the surface force-deflection relationship with the force-deflection relationships of the cask impact limiter prior to the analysis.

<sup>\*</sup> This work was supported by the United States Nuclear Regulatory Commission under a Memorandum of Understanding with the United States Department of Energy.

# Introduction

Most of the storage casks do not require impact limiters. However, CASKS code requires the user to specify the impact limiter force-deflection curve before the code can be executed, even when there are no physical impact limiters on the cask. This requirement can be thought of as the relative 'stiffness' or 'flexibility' of the part of the cask that contacts the target on impact. The 'stiffness' of the cask is derived by entering a 'pseudo' force-deflection curve for the cask.

Based on the general geometry description, CASKS automatically generates appropriate, twodimensional finite-element meshes for thermal, thermal-stress, and pressure-stress analyses. CASKS allows steady-state or transient thermal analyses, which may include phase change, timeand/or temperature-dependent material properties, time and/or temperature boundary conditions, and internal heat generation. Possible thermal boundary conditions include specified temperature, heat flux, convection, radiation, interface contact resistance, and nonlinear heat transfer to a bulk node. Thermal analyses use 4-node elements. Thermal-stress and pressure-stress analyses are performed using a linear-elastic static structural analysis program which allows temperaturedependent material properties. Stress analyses use 9-node elements.

Users can choose to display or print the graphical output. Graphic displays include: impact force, moment and shear time histories; impact animation; thermal/stress geometry outline; thermal/stress element outlines; temperature distributions as iso-contours or profiles; and temperature-time histories.

### Introduction Menu Structure

### **CASKS Menu Structure**

CASKS uses a series of menus to coordinate input programs, cask analysis programs, output programs, data archive programs and databases. Figure 1-1 illustrates the menu structure. The menus are ordered according to the stages of analysis.

CASKS requires only the press of a single key to make menu and subtask selections. CASKS indicates the available selections on each display screen and describes what action CASKS will take. For example, on the Main Menu, CASKS indicates that the appropriate keys to press are 1 23456 and Q (where Q returns you to DOS).

The user enters data through fill-in-the-blank input screens. Full editing features are available (insert, delete, move cursor, overtype, etc.). The system accepts data items when you move the cursor to another data field.



Figure 1-1. CASKS menu structure.

### Introduction Required Hardware and Software

### CASKS Required Hardware

CASKS is designed for microcomputers compatible with the IBM-PC family of computers. The minimum required hardware configuration is an IBM "XT" with the following:

10 Mbyte hard disk drive
360 Kbyte floppy disk
640 Kbyte RAM
CGA Board (Color Graphics Adapter)
Color Graphics Monitor
8087 Math co-processor chip
IBM or EPSON Graphics printer

### **Upgraded Hardware Configuration**

CASKS functions on MS-DOS computers including the 80486 class of machines. A typical upgraded configuration is an IBM IBM PS2 Model 80 (80386 processor) with the following:

40 Mbyte hard disk drive
1.44 Mbyte floppy disk (High Density)
360 Kbyte floppy disk (external)
640 Kbyte RAM
VGA Board (Video Graphics Array)
VGA Color Monitor
80387 Math co-processor chip
HP LaserJet, LaserJet+, or LaserJet Series II printer

### **Required DOS Files**

**CASKS** requires the operating system DOS version 3.1 or later. The DOS command files listed below must be present in the root directory of the *booting* hard disk drive:

#### AUTOEXEC.BAT ANSI.SYS CONFIG.SYS

The following DOS file must be in the root directory of the hard disk drive which will *contain* CASKS:

#### COMMAND.COM

Include the following lines in the CONFIG.SYS\*\* file:

DEVICE=ANSI.SYS BREAK ON FILES=15 BUFFERS=15

<sup>\*\*</sup> The files CONFIG.SYS and AUTOEXEC.BAT and the command PATH are described in the DOS reference manual.

# Introduction

### **Required Hardware and Software**

Include the following path in the AUTOEXEC.BAT<sup>\*\*</sup> file:

PATH x:\ (where x is the hard disk drive which contains CASKS)

### **Required DOS Programs**

The DOS programs listed below must be available through the current PATH.

MODE.COM BACKUP.COM RESTORE.COM

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<sup>\*\*</sup> The files CONFIG.SYS and AUTOEXEC.BAT and the command PATH are described in the DOS reference manual.

### Introduction Installing CASKS

The CASKS release package contains four, 5-1/4-inch double-density distribution diskettes (or two 5-1/4-inch high-density diskettes for 1.2Mb disk drives). The programs and control files on the distribution diskettes occupy approximately 2.6Mb of disk space and must be installed on a hard disk drive. The following instructions will help you install CASKS. The left hand column lists "user input" and the right hand column describes the system response or additional information you might need.

**NOTE:** Press **Q** at any time to abandon installation of **CASKS**. **INSTALL** will ask for verification before terminating the installation.

How to Install CASKS:

- (1) Be sure the DOS file COMMAND.COM is in the root directory of the hard disk drive which will contain CASKS.
- (2) Insert diskette number 1 into drive A: or B:
- (3) If using drive A:, type <u>A:INSTALL</u>

If using drive B:, type **B:INSTALL** 

(4) Press S to select the hard disk drive where CASKS will reside

or

Press Q to QUIT and return to DOS.

(5) Press the indicated letter to select the drive where CASKS will reside

or

Press Q to QUIT and return to DOS.

(6) Insert each diskette as requested into either drive A: or B:. Press A or B as required to install that disk. Repeat for all distribution diskettes. If you press **S**, **INSTALL** displays the available hard disk drives on your system.

INSTALL displays the space remaining on the selected hard disk drive, creates the \CASKS subdirectory, and prompts for CASKS diskette number 1.

### Introduction Installing CASKS

The program **INSTALL** performs the following installation operations:

- **INSTALL** determines how many hard disk drives exist on the system, lists the hard disk drives, and asks for the drive that will contain **CASKS**.
- **INSTALL** checks the selected hard disk drive for enough space. **CASKS** cannot be partially installed. If there is not enough space, either remove files from the hard disk drive to create room or select a different hard disk drive (if available).
- INSTALL creates the subdirectory \CASKS on the selected hard disk. If an older version of CASKS is already installed, \CASKS is renamed to \CASKSnn (where nn is the previous CASKS version number) before \CASKS is created. If the same version of CASKS is already installed, INSTALL asks if you want to reinstall CASKS.
- **INSTALL** copies the program and control files from the distribution diskettes. **INSTALL** asks for each **CASKS** diskette in order.
- **INSTALL** unpacks the sample data set and other packed files. This process takes a few minutes to complete.
- **INSTALL** updates the **CASKS** procedure to identify the selected hard disk.

How to Run the CASKS Program:

typing:

Once installation is complete, start CASKS by CASKS displays the title and disclaimer screen shown in Figure 1-2.

CASKS <then press Enter or Return>



Figure 1-2. Title and disclaimer screen. (Displayed when CASKS is started.)

Press any key to continue.

CASKS automatically initiates the Select Cask process and searches for cask data sets that already exist.

The system displays the number of existing data sets. The screen you see will vary depending on whether no data sets exist, only one data set exists, or more than one data set exists.

Press **Q** to Quit or Press any other key to continue.

If no data sets exist, enter a new CASKID. The CASKID is a four-digit number that

The CASKID is a four-digit number that identifies the cask data set. All four digits are required. For example, to specify a CASKID of 77, enter 0077. Enter Q to QUIT and return to DOS.

or

When only one data set exists, CASKS displays a summary of the data set (Figure 1-3) and offers three choices:

- Press N to select a new CASKID by direct entry
- Press P to Proceed with the indicated CASKID (CASKS displays the Main Menu)
- Press **Q** to QUIT and return to DOS



Figure 1-3. Cask data set summary screen.

or

If more than one data set exists, CASKS displays a list of CASKIDs and several options:

- Press N to select a new CASKID by direct entry
- Press S to select the highlighted CASKID and display data set summary
- Press Q to QUIT and return to DOS
- Press ↑ to highlight the previous CASKID
- Press ↓ to highlight the next CASKID

When S is pressed, the Summary Screen options are:

- Press S to select a different CASKID (return to the CASKID list screen)
- Press P to proceed with the specified CASKID (CASKS displays the Main Menu)
- Press  $\mathbf{Q}$  to QUIT and return to DOS

After you select a CASKID, CASKS displays the Main Menu. The first step for a new data set is to define the basic geometry. Once the geometry definitions exist, CASKS will perform an analysis, display the graphical results (if applicable) and then print the results. You can select each of these operations from the Main Menu.

### Version: 1b 1-11

# Introduction

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### NOTES:

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# Main Menu

The Main Menu (Figure 2-1) is the central hub of CASKS. It provides access to five task menus and the select cask facility. The task menus are connected only through the Main Menu. They cannot call each other directly.

#### PRESS 1 to Select a new CASK ID

The select cask facility is similar to the select cask process when you start CASKS, except that when you press Q, you return to the Main Menu instead of leaving CASKS and returning to DOS.

# PRESS 2 to Create/Modify the CASK geometry model (Geometry Menu)

Select this task first to create a new cask data set. CASKS displays the Geometry Menu which provides tasks for: (1) creating new (or modifying previous) basic geometry definitions and impact limiter force-deflection curves; (2) copying basic geometry or limiter curves from a different cask data set; and (3) creating new (or modifying previous) yielding surface user-input force-deflection curves.

CASKS	MAIN MENU	CASKS	
PRESS	Current CASK ID is 9999		
	To select a new CASK ID		
2	To Create/Modify the CASK geometry model		
3	o Perform CASK analyses		
5	To Print/Review analysis outouts		
6	Fo Archive/Retrieve/Delete CASK data sets		
	Fo QUIT and return to DOS		

Figure 2-1. CASKS Main Menu.

## Main Menu

#### PRESS 3 to Perform CASK analyses (Analysis Menu)

CASK analyses are performed after defining the cask geometry and, if necessary, the impact limiter force-deflection curves. **CASKS** displays the Analysis Menu, which provides tasks to perform analyses involving impact loads, thermal distributions and stresses, and pressure loads.

# PRESS 4 to Display analysis results and/or geometry (Display Menu)

CASKS displays the Display Menu which provides tasks for: (1) plotting dynamic impact time-histories; (2) displaying and printing finite-element meshes used for thermal, thermal-stress and pressure-stress calculations; and (3) plotting thermal distributions as iso-contours, time histories, or thermal profiles. The finite-element meshes can be displayed before any analysis is performed. Results cannot be plotted until the appropriate analysis is performed.

#### PRESS 5 to Print/Review analysis outputs (Print/Review Menu)

**CASKS** displays the Print/Review Menu, which provides tasks for printing or reviewing all printable outputs (analysis results or the cask summary and data check). Printing an output sends it to the printer; reviewing an output displays it on the screen.

# PRESS 6 to Archive/Retrieve/Delete CASK data sets (Archive Menu)

**CASKS** displays the Archive Menu which provides tasks for: (1) archiving cask data sets; (2) retrieving previously archived data sets; and (3) deleting cask data sets (complete data sets or just the output) from the hard disk.

#### PRESS Q to QUIT and return to DOS

CASKS terminates the session and returns to DOS in the root directory of the hard disk which contains CASKS.

# Geometry Menu

The Geometry Menu (Figure 3-1) provides tasks for creating new (or modifying previous) basic geometry definitions: impact limiter force-deflection curves, yielding surface force-deflection curves, and modifying material data set.

#### PRESS 1 to Create/Modify basic geometry

If the basic geometry definition data set exists, editing is initiated. If the basic geometry data does not exist, CASKS creates a new data set with default values, and editing is initiated. When the basic geometry is saved, CASKS automatically performs a data check. Basic geometry definitions must be completed and pass the data check before CASKS will perform an analysis.

#### PRESS 2 to Create/Modify impact limiter F/D curves

If the impact limiter force-deflection curve data set exists, editing is initiated. If the limiter curve data does not exist, CASKS creates a new data set with default values, and editing is initiated. When the limiter curve data is saved, CASKS automatically performs a data check. Limiter forcedeflection curves must be defined and pass the data check before CASKS will perform an impact analysis.

CASKS	GEOMETRY MENU	CASKS
PRESS	Current CASK ID is 9999	
1 To 2 To 3 To 4 To 5 To 6 To M Tc	Create/Modify basic geometry Create/Modify impact limiter F/D curves Create/Modify yielding surface F/D curves Copy basic geometry from different cask Copy limiter data from different cask Modify material data set Return to MAIN MENU	



Version: 1b 3-1

## Geometry Menu

#### PRESS 3 to Create/Modify yielding surface F/D curves

Editing is initiated with previously created cases, if any. A total of nine different surface F/D curves (cases) can be created and/or modified. When the surface curve data is saved, **CASKS** automatically performs a data check before returning to the Geometry Menu.

#### PRESS 4 to Copy basic geometry from different cask

Use this feature to create the basic geometry definition data set by copying it from the existing data set for a different cask. Then, modify the data set to resolve any differences between the casks.

CASKS lists the available basic geometry definition data sets from other casks. Use the cursor keys to highlight the data set to copy, then press S. If a basic geometry data set already exists for the current cask, CASKS asks for confirmation before copying the selected data set over the current one.

#### PRESS 5 to Copy limiter data from different cask

Use this feature to create the impact limiter force-deflection curve data set by copying it from the existing data set for a different cask. Then, modify the data set to resolve any differences between the casks.

CASKS lists the available limiter curve data sets from other casks. Use the cursor keys to highlight the data set to copy, then press S. If a limiter curve data set already exists for the current cask, CASKS asks for confirmation before copying the selected data set over the current one.

#### PRESS 6 to Modify material data set

Use this feature to create/modify a material data set. Locked files may not be edited. A new material data set may be created using the C (copy) option to copy an existing material file then input all necessary data pertaining to this material.

#### PRESS M to Return to MAIN MENU

CASKS returns to the Main Menu display.

### Geometry Menu Using the Editor

**CASKS** uses a general purpose fill-in-the-blank type editor to enter data for the basic geometry definition, the impact limiter and yielding surface force-deflection curve definitions. Appendix A has a complete description of the editor features, displays, and usage. A condensed description of how to use the editor is included here.

The editor title screen indicates the status of the data set. To abandon editing at this point, press **Q** to quit and return to the Geometry Menu. If the data set does not exist, press any other key to create the data set using default values. If the data exists, press **D** to delete the data set and create a new one or press any other key to edit the existing data set. When **D** is selected, **CASKS** asks for confirmation before proceeding.

The editor reads a template which describes the editor screens and, if creating a new data set, identifies each editor page as it is created with the appropriate default values. The editor then displays the first editor page. Each page contains related data, and each data field has a descriptive label indicating what to enter (units are indicated if appropriate).

**IMPORTANT:** All fields displayed in light blue are required inputs. Fields displayed in green have default values which can be changed or accepted as is.

On each page display, in the upper left hand corner, the editor displays the number of pages which must be accessed. These pages have fields that must be filled in before the data set is considered complete. The page list display also identifies these pages. *Be sure to move to each field that is labeled in light blue*. If necessary, enter the appropriate data.

#### Use the following keys to edit a field:

Characters, numbers and special symbols to enter the appropriate data (Typing in the first character position clears the field) Keypad left and right arrow keys to position the cursor DEL and backspace keys to delete characters INS key to toggle between insert and overtype modes

#### Use the following keys to accept a field and go to another:

Keypad up and down arrow keys or ENTER to move to previous or next field on current page.

Keypad PgUp and PgDn to move to first field on previous or next page.

### Geometry Menu Using the Editor

#### Use the following keys for help, redefaulting and special control:

- ESC to display help relating to the current field and a description of all the editing keys.
- F1 to display a list of all the pages in the data set. Use the keypad up and down arrow keys to highlight the desired page and then press F1 again to move to the indicated page. The page list screen indicates which pages have data fields that must be filled in.

F2 saves the data set, terminates the editor, and returns to the current menu.

F3 abandons editing. CASKS asks for confirmation before proceeding.

F4 saves the data set and continues editing.

- F5 prints the displayed page on the printer. Make sure the printer is on-line.
- F6 resets the current field to its default value.
- F7 resets all fields on the current page to their default values.

If the entered data is invalid for the specified field, the editor displays an error message at the bottom of the screen and indicates any restrictions on the data item. Press **ENTER** to clear the error message and return to editing.

See Appendix A for a more complete description of the editor and its features.

### Geometry Menu Defining the Geometry

CASKS uses a simplified cask model comprised of seven components: (1) cask cavity, (2) shell, (3) top end cap, (4) bottom end cap, (5) top impact limiter, (6) bottom impact limiter, and (7) neutron shield and water jacket. The general form of this cask model is shown in Figure 3-2. The shell and end caps can be either solid (single layer) or laminated (two or three layers). The cavity, shell and end caps must be defined for each analysis. Impact limiters are optional but are required for impact calculations. The neutron shield/water jacket is optional and, if included, used only for thermal analyses. Mesh division values are used to generate two-dimensional finite-element meshes for thermal, thermal-stress and pressure-stress analyses. The geometry definition is described in the context of the editor pages that follow.



Figure 3-2. CASKS simplified cask model.

### Geometry Menu Defining the Geometry

#### Basic Geometry PAGE 1 General SAR Information

The SAR title is required. Four fields are provided for other SAR information, three fields are provided for additional information, and three for the submitting company's address. All fields on this page are character type and are not checked for validity.

#### Basic Geometry PAGE 2 Reviewer Information

There is no required data on this page. It is provided to document the persons involved in the cask evaluation. All fields are character type and are not checked for validity.

### Basic Geometry PAGE 3 Cask Cavity/Contents Specifications

The cavity dimensions and the weight specifications are required for all analyses. The maximum heat generation rate is required for thermal and thermal-stress analyses.

Field Name	Description		
Cavity Inner Radius	Required		
	Positive. Must be less than 2000.		
Cavity length (in.)	Required		
	Positive. Must be less than 2000.		
Gross weight of package	Required		
(lbs.)	Positive		
	Includes the cask body, impact limiters, internal structures, and spent-fuel contents.		
Weight of spent-fuel contents	Required		
and internal structures (lbs.)	Positive		
Maximum heat generation	Positive		
rate of the spent fuel contents (Btu/min).	Used for thermal and thermal-stress analyses.		

Basic	Geometry	PAGE	3	Cask	Cavity/Contents	Specifications	(con't.)
-------	----------	------	---	------	-----------------	----------------	----------

Field Name	Description
Temperature defining stress free condition (degrees F).	Must be greater than or equal to -100°F.
	Used for thermal-stress analyses. May be changed during specification of the thermal-stress analysis.
Number of mesh divisions along cavity inner radius and along cavity half length.	Must be even and between 2 and 30.
	Specific mesh divisions along the half length of the cavity, not the full length.
Initial cavity charge pressure (psia) and temperature (degrees F).	Pressure must be positive, and temperature must be greater than or equal to -100°F.
	Used during thermal analyses to estimate the change in internal pressure as a result of thermal loads.
Maximum normal operating pressure (psia).	Must be positive.
	Used as one of the regulatory pressure-stress loading conditions.

### Geometry Menu Defining the Geometry

#### Basic Geometry PAGE 4 Cask Component Configurations

The default cask configuration has a solid shell and solid end caps. It includes top and bottom impact limiters, neutron shield, and water jacket. Enter L to specify a laminated shell or end caps. Enter N to exclude either limiter or the neutron shield and water jacket. Figure 3-3 shows several possible configurations.



Figure 3-3. Sample cask configurations.
Basic Geometry Pages 5a and 5b Cask Shell Specifications

CASKS displays Page 5a for a solid shell and page 5b for a laminated shell.

#### Solid Shell

Field Name	Description
Shell thickness (inches)	Required
	Must be positive and less than 2000.
	Total thickness of the shell.
Shell material name	Select from the displayed list of materials
Number of mesh divisions through shell	Must be even and between 2 and 10.
	Used to generate a two-dimensional finite-element mesh for thermal, thermal-stress and pressure-stress analyses.

#### Laminated Shell

Field Name	Description
Shell inner layer thickness	Required
(inches)	Must be non-negative and less than 2000.
	Set to 0.0 to eliminate the inner layer.
Additional thickness of inner layer in vicinity of the end caps (inches).	Must be non-negative and less than 2000.
	Set to 0.0 if inner shell is not thickened. Used for impact analyses with unbonded lead shielding.
Shell inner layer material name	Select from the displayed list of materials.
Shell shield layer thickness (inches)	Required
	Must be non-negative and less than 2000.
	Set to 0.0 to eliminate the shield layer.

#### Laminated Shell (con't.)

Field Name	Description
Shell shield length (inches)	Required
	Must be non-negative and less than 2000.
	Set to 0.0 to eliminate the shield layer. May be larger than the cavity length but should not exceed the cask body length (cavity length plus thickness of both end caps). Figure 3-4 shows the effects of various shell shield lengths. NOTE: Impact analyses assume shield length is same as cavity length.
Shell shield layer material name.	Select from the displayed list of materials.
Shell outer layer thickness	Required
(inches)	Must be positive and less than 2000.
Additional thickness of outer layer in vicinity of the end caps (inches).	Must be non-negative and less than 2000.
	Set to 0.0 if outer shell is not thickened. Used for impact analyses with unbonded lead shielding.
Shell outer layer material name.	Select from the displayed list of materials.
Number of mesh divisions through inner layer, shield layer and outer layer of the shell.	Must be even and between 2 and 10.
	If inner layer or shield layer is eliminated, number of mesh divisions is ignored.

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#### Basic Geometry Pages 6-7 Cask End Cap Specifications

Page 6a is displayed when a solid top end cap is specified. Page 6b is displayed when a laminated top end cap is specified. Pages 7a and 7b are for solid and laminated bottom end caps; these pages are identical to pages 6a and 6b.

#### Solid End Cap

Field Name	Description
End cap thickness (inches)	Required
	Must be positive and less than 2000.
	Total thickness of the end cap.
End cap material name.	Select from the displayed list of materials.
Number of mesh divisions through end cap.	Must be even and between 2 and 10.

#### Laminated End Cap

Field Name	Description
End cap inner layer thickness	Required
(inches)	Must be non-negative and less than 2000.
	Set to 0.0 to eliminate the inner layer.
End cap inner layer material name.	Select from the displayed list of materials.
End cap shield layer	Required
thickness (inches)	Must be non- negative and less than 2000.
	Set to 0.0 to eliminate the shield layer.
End cap shield radius	Required
(inches)	Must be non-negative and less than 2000.
	Set to 0.0 to eliminate the shield layer. Must be larger than the cavity radius and should not exceed the cask body outer radius (cavity radius plus shell thickness). Figure 3-4 shows the effects of various end cap shield lengths.
End cap shield layer material name.	Select from the displayed list of materials.

#### Laminated End Cap (con't.)

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Field Name	Description
End cap outer layer thickness (inches)	Required
	Must be positive and less than 2000.
End cap outer layer material name.	Select from the displayed list of materials.
Number of mesh divisions through inner layer, shield layer, and outer layer of the end cap.	Must be even and between 2 and 10.
	If inner layer or shield layer is eliminated, number of mesh divisions is ignored.

#### Basic Geometry Page 8 Cask Closure Bolts Information

Field Name	Description
Number of closure bolts	Required
	Must be positive and less than 100.
Diameter of closure bolts (inches)	Required
	Must be positive and less than or equal to 10.
Closure bolt circle radius (inches)	Required
	Must be positive and less than 2000.
	Should be greater than the cavity radius and less than the cask body outer radius (cavity radius plus shell thickness).

#### Basic Geometry Page 9 Cask Neutron Shield / Water Jacket Specifications

The neutron shield and water jacket are not included in impact, thermal-stress and pressurestress analyses. They may be included in thermal analyses if they affect heat transfer.

Field Name	Description
Neutron shield and water jacket length (inches)	Required
	Must be non-negative and less than 2000.
	Should be less than the cavity length. Set to 0.0 to eliminate the neutron shield and water jacket (same as specifying on Page 4 that they are not included).
Neutron shield thickness (inches)	Required
	Must be non-negative and less than 2000.
	Set to 0.0 to eliminate the neutron shield.

Basic Geometry Page 9 Cask Neutron Shield / Water Jacket Specifications (con't.)

Neutron shield material name.	Select from the displayed list of materials.
Water jacket thickness	Must be non-negative and less than 2000.
(inches)	Set to 0.0 to eliminate the water jacket.
Water jacket material name.	Select from the displayed list of materials.
Number of mesh divisions	Must be between 1 and 3.
through neutron shield and	If neutron shield or water jacket is eliminated, number of
water jacket.	mesh divisions is ignored.

#### Basic Geometry Pages 10-11 Cask Impact Limiter Specifications

Page 10 is displayed when a top impact limiter is included in the cask model. Page 11 is displayed when a bottom impact limiter is included\*. Top and bottom impact limiters are specified in a similar manner. Impact limiters are included in impact and thermal analyses. Figure 3-5 shows possible impact limiter configurations.

Field Name	Description
Impact limiter radius (inches)	Required
	Must be positive and less than 2000.
	Should be greater than or equal to the cask body outer radius (cavity radius plus shell thickness).
Impact limiter centerline thickness above the end cap (inches)	Required
	Must be positive and less than 2000.

<sup>\*</sup>Note that most of the storage casks do not require impact limiters. However, CASKS code requires the user to specify the impact limiter force-deflection curve before the code can be executed, even when there are not physical impact limiters on the cask. This requirement can be thought of as the relative 'stiffness' or 'flexibility' of the part of the cask that contacts the target on impact. The 'stiffness' of the cask is derived by entering a 'pseudo' force-deflection curve for the cask.

Basic Geometry Pages 10-11 Cask Impact Limiter Specifications (con't.)

Impact limiter overhang thickness below the end cap (inches)	Required
	Must be non-negative and less than 2000.
	Should be less than or equal to half the cask body length (cavity length plus thickness of both end caps). Set to 0.0 for no overhang. Set greater than half cask body length to surround the cask with the impact limiter. If the impact limiter radius is less than or equal to the cask body outer radius, the overhang thickness is ignored.
Impact limiter material name	Select from the displayed material list.
Number of mesh divisions through limiter centerline thickness and overhang width (impact limiter radius minus cask body outer radius)	Must be between 1 and 10.

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Limiter RADIUS: Equal to cask body

#### Limiter OVERHANG: None





Limiter Radius: Greater than cask body

Limiter OVERHANG: None



RADIUS: Greater than cask body

OVERHANG: Included, exceeds body half length (Limiter surrounds the cask body)



#### Basic Geometry Page 12 Cask Impact Model Specifications

Define these values for impact analyses. They are not used for any other analysis.

Field Name	Description
Number of elements for the one-dimensional beam impact model.	Must be between 3 and 20. Accuracy generally improves with increased number of elements. However, the more elements used, the higher the
	possibility of capturing unnecessary high frequency modes. The integration time step is inversely proportional to the maximum frequency of the model. Thus, high frequencies require small time steps which causes the computation time to lengthen. The number of elements also specifies where force and stress information is output. Set to 3 for output at third points. Set to 4 for output at quarter points. Set to 6 for 1/6th points. Set to 12 for quarter and third points (plus a few more).
Top impact limiter weight (lbs.)	Set to 0.0 to calculate top impact limiter weight based on limiter dimensions and density.
Bottom impact limiter weight (lbs.)	Set to 0.0 to calculate bottom impact limiter weight based on limiter dimensions and density.
Define impact model with user specified properties? [Y/N]. Specify N to use shell, end caps, and impact limiter dimensions for impact analyses. Specify Y to input the following impact model properties directly.	These properties are described in Volume 2, SCANS Impact Analysis Theory Manual, in the section discussing the theory of impact. The weight of the contents and internal structures must be specified on the basic geometry editor page 3 (cask cavity/contents specifications).

The following properties must all be positive:

Shell translational mass (lb-sec\*\*2/inch).
Shell rotational mass (lb-sec\*\*2-inch).
Shell inside length (inches).
Shell E\*I (composite Young's Modulus x Moment of Inertia) (lb-inch\*\*2).
Shell A\*E (composite Young's Modulus x Area) (lbs).
Shell composite Poisson's Ratio.
Top end translational mass (lb-sec\*\*2/inch).
Top end rotational mass (lb-sec\*\*2-inch).
Bottom end translational mass (lb-sec\*\*2/inch).
Bottom end rotational mass (lb-sec\*\*2-inch).
Characteristic cross-section width (inches).

### Geometry Menu Defining the Limiter F/D Curves

CASKS has eight predefined oblique angles for defining force-deflection curves: 0 degrees (side drop); 15; 30; 45; 60; 75; 90 (end-on drop); and CG (center-of-gravity drop). Force-deflection curves are related to the angle of impact because crush forces are based on the contact footprint. Define any or all of the curves; there are eight possible curves for the top impact and eight for the bottom impact. If curves are only defined for one end, CASKS will not allow side drop analyses, secondary impact analyses, or analyses specifying the end without an impact curve as the primary impact end.

Defining the Limiter F/D Curves:

The impact force-deflection data set has 17 editor pages. Page 0 specifies the slope of the unloading path for the impact (Figure 3-6). This slope relates the force unloaded with the amount of elastic recovery of the impact. CASKS allows three choices:

C selects the maximum slope of the force-deflection curve as the unloading slope.

N selects no elastic recovery of the impact (for dynamic stability this is approximated by an unloading slope that is five times the maximum slope of the force-deflection curve).

U selects a user specified unloading slope (in terms of kips of unloading force per inch of elastic recover).

### Geometry Menu Defining the Limiter F/D Curves

Sample Limiter deflection / force data ID:9999 Today is:10/05/88 Impact Limiter Unloading Specification Page 0 of 2h Last chgd:10/02/88	C A S K			
Select the slope of the unloading path for impact limiters C Unloading slope is maximum slope of limiter curve	S			
<ul> <li>N No elastic recovery of impact limiter</li> <li>(Approximated by unloading slope of 5 times max slope of curve)</li> <li>U User specified unloading slope</li> </ul>				
Type of Impact Limiter Unloading[N]				
F1 List Pages F2 Save+END F3 QUIT w/o Save F4 Save+Continue F5 Print Page F6 Redefault Current Field F7 Redefault Entire Page ESCape for HELP				

#### Figure 3-6. Impact limiter unloading specification.

Each of the remaining pages specifies a forcedeflection curve at a specific impact angle. Pages 1a-1h define force-deflection curves for the bottom impact, and pages 2a-2h define curves for the top impact.

The impact end and orientation angle are identified in

the upper left corner of the screen.

- (1) Use the keypad **PgUp** or **PgDn** keys to display the page with the desired limiter and impact angle (or use the page list function key **F1** to select the page).
- (2) Type Y and press ENTER to activate the curve data.
- (3) Fill in up to ten curve points. Enter deflections in inches and forces in kips. NOTE: the first two points are required.

If there are less than ten curve points, leave the remaining curve points 0.0.

### Geometry Menu Defining the Limiter F/D Curves

Data page 1c, which specifies the bottom impact limiter for a 30-degree impact, is shown in Figure 3-7.

ſ	Sample Limiter defle Bottom Impact Limi	action / force da ter for 30 degre	ta ID e impact Pa	:9999 T age 1c of 2h	oday is:10/05/88 Last chgd:10/05	//88	
	Press F10 to copy	Force/Deflection	on data from	another impac	t angle		S K
	Impact angle is defi	ned as follows: E	SIDE impac ND ON impa	t angle is 0. .ct angle is 90.			
	Do you wish to defin	ne a Deflection/	Force curve f	or this angle ?	[Y/N][Y]		
	You n	nust define at le	ast 2 deflecti	on/force pairs			
	Deflection #0	(in) .0		Force #0	(kips) .0		
	Deflection #1	(in)[0.	]	Force #1	(kips)[0.	]	
	Deflection #2	(in)[0.	]	Force #2	(kips)[0.	]	
	Deflection #3	(in)[0.	]	Force #3	(kips)[0.	]	
	Deflection #4	(in)[0.	]	Force #4	(kips)[0.	]	
	Deflection #5	(in)[0.	]	Force #5	(kips)[0.	1	
	Deflection #6	(in)[0.	1	Force #6	(kips)[0.	1	
	Deflection #7	(in)[0.	]	Force #7	(kips)[0.	]	
	Deflection #8	(in) <b>[</b> 0.	]	Force #8	(kips)[0.	]	
	Deflection #9	(in)[0.	]	Force #9	(kips)[0.	]	
	Deflection #10	(in)[0.	]	Force #10	(kips)[0.	]	
F	1 List Pages F2 Sa 6 Redefault Current	ave+END F3 ( Field F7 Re	QUIT w/o Sav default Entire	/e F4 Save+ Page	Continue F5 Pr ESCape for	int Page HELP	

Figure 3-7. Sample impact limiter data page.

(4) Press **F10** to copy curve data from a different impact angle or cask end.

CASKS displays the list of all impact angles.

(5) Use the **UpArrow** and **NC DnArrow** keys to indicate the data to copy from and then press **C** to perform the copy.

**NOTE:** Each force-deflection curve must be single valued and in increasing order. That is, each deflection point must be larger than the previous one.

The impact force-deflection model is described in Volume 2 of SCANS Impact Analysis Theory Manual.

### **Geometry Menu** Defining the Yielding Surface F/D Curves

CASKS allows the user to define how yielding surface behaves under cask impact via the use of yielding surface F/D curves. Yielding surface F/D curves inputs are structured the same way as inputs to the cask limiter F/D curves. User may input up to 9 different surface F/D curves (cases). Each surface force-deflection curve must be input as single valued and in increasing order.

Appendix F provides user with a means to estimate the yielding surface F/D curve for a given concrete slab/subgrade soil combination. Users are encouraged to use a more accurate yielding surface F/D curve whenever possible.

## Geometry Menu

NOTES:

The Analysis Menu (Figure 4-1) provides tasks to perform analyses involving impact loads, thermal distributions and stresses, and pressure loads. The basic geometry model definitions must be completed before CASKS can perform any analysis.

#### PRESS 1 to Perform Impact analysis

**CASKS** determines forces and stresses resulting from impact loads. Impact force-deflection curves must be defined before **CASKS** can perform an impact analysis. Users have the option of selecting cask impact on either an unyielding surface or a yielding surface. The impact condition is specified by drop height, impact type, analysis type, shell/shield interface type, impact end, and impact angle.

#### PRESS 2 to Perform Thermal analysis

CASKS performs any of seven predefined regulatory thermal analyses. These analyses include various ambient temperatures, solar effects, contents heat loads, and fire loads.

CASKS	ANALYSIS MENU	CASKS
	Current CASK ID is 9999	
1To Perfo2To Perfo3To Perfo4To Perfo	orm IMPACT analysis orm THERMAL analysis orm THERMALLY-INDUCED STRESS orm PRESSURE-INDUCED STRESS	S analysis <sup>-</sup> analysis
M To Retu	rn to MAIN MENU	

Figure 4-1. CASKS Analysis Menu

#### PRESS 3 to Perform Thermally-Induced Stress analysis

**CASKS** determines stresses resulting from previously analyzed thermal conditions. After selecting the thermal case, specify the stress-free temperature and, for the transient case, specify the time state.

#### PRESS 4 to Perform Pressure-Induced Stress analysis

CASKS determines stresses resulting from the pressure difference between cavity pressure and external pressures defined by regulations.

#### PRESS M to Return to MAIN MENU

CASKS returns to the Main Menu display.

Select Impact Surface Type

Selecting the Impact Surface Type: CASKS allows the user to choose between cask impact on either an unyielding surface or a yielding surface. When you press 1 to perform See Figure 4-2, below. (1) Impact Analysis, the User Selected CASK Impact Options Screen appears. Select the cask input surface (2) type from the screen. User Selected CASK Impact Options CASK Impacts on Either an Unvielding or a Yielding Surface U for unyielding surface PRESS Y for yieling surface Q to quit the program

Figure 4-2. Select Impact Surface Type Screen

C A S K

### Analysis Menu Select Impact Surface Type

(3) Press U if an unyielding surface impact option is desired.

Press Y if a yielding surface input option is desired.

Press Q to QUIT and return to the Analysis Menu.

When U (unyielding surface option) is selected, CASKS proceeds to perform Impact analysis by displaying the impact analysis parameters input screen as shown in Figure 4-7.

The yielding surface uses a non-linear force-deflection approximation. After a proper yielding surface F/D curve is defined, it then combines with the cask limiter F/D curves before performing an impact analysis.

When Y (yielding surface option) is selected, CASKS then asks whether the user wishes to use the built-in surface force-deflection curves or to input his/her own pair of surface force-deflection values (Figure 4-3).

(4) If **Y** is selected:

Press 1 for built-in curve.

Press 2 for user-defined curve.





Select Impact Surface Type

CASKS does not provide a set of build-in surface F/D curves at this time (this option is reserved for future code expansion).

**IMPORTANT:** User is warned that CASKS will give erroneous impact results if option 1 (build-in curve) is accidently selected.

(5) Select 2 to input a sitespecific surface F/D curve. A screen appears and prompts the user to decide whether to use a previously input case or to input a new case (Figure 4-4).

A total of 9 different surface F/D curves (CASES) may be input through the yielding surface template.

**NOTE:** New cases may ONLY be input using option 3 (to Create/Modify yielding surface F/D curves) under the GEOMETRY MENU.



Figure 4-4. User Input Surface F/D Options

### Analysis Menu Select Impact Surface Type

(6) Press E to use a previous case.

CASKS asks the user to indicate which case to use (Figure 4-5).

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Figure 4-5. Users Specifies Which Previously Defined Surface F/D Curve to Use

### Analysis Menu Select Impact Surface Type

Enter a CASE No. The user will be prompted with a message signaling the completion of combining the surface F/D curves just selected with that of the cask limiter F/D curve. CASKS then performs impact analysis by displaying Figure 4-7.

or

(7) Press N to input a new surface F/D curve.

CASKS will instruct the user to first exit the analysis module and enter the GEOMETRY MENU. New cases can ONLY be entered this way.

Select option 3 (Create/Modify surface F/D curve) to input a new surface F/D curve (Figure 4-6).



Figure 4-6. CASKS Instructs the User on How to Input/Modify a Surface F/D Curve

CASKS assumes beam-column behavior for impact analyses and determines forces and stresses for both primary and secondary impacts. CASKS can perform impact analyses for oblique angles between 0 degrees (side drop) and 90 degrees (end-on drop).

Both the basic geometry and the impact forcedeflection curves must be defined and complete before **CASKS** can perform an impact analysis (see Geometry Menu). The basic geometry must include at least one set of impact force-deflection curves. The Impact Analysis Title Screen indicates any missing information required before an impact analysis can be performed.

(9) From the Select Impact Analysis Parameters Screen, press Q to QUIT and return to the Main Menu, or press any other key to specify the six impact analysis parameters. The six impact analysis parameters are: drop height; impact type; analysis type; shell/shield interface type; primary impact end; and impact angle (Figure 4-7).

SELECT IMPACT ANALYSIS PARAM		
Drop Height (in)[ ]		ĸs
Impact Type [Initial Plus Secondary Impact]	Input CASK drop	
Analysis Type[ Dynamic]	neight in inches	
Shell/Shield Interface[ Bonded]		
Primary Impact End[Bottom]		
Impact Angle (from horizontal)[ ]		
Proce any of the following keys		
P to Perform Analysis 1 to move	to previous field	
Q to Quit ↓ to move	to next field	
		ノ /



CASKS displays the default values for four of the six parameters.

(10) Press P to proceed and perform the analysis with the parameters as displayed, press Q to QUIT and return to the Analysis Menu or modify any of the parameters before performing the analysis.

To modify a parameter, use the keypad up or down arrow keys to highlight the desired field and then press the function key that selects the desired value.

Selecting the Drop Height:

- Input the Drop Height field in (1) inches and press return.
- (2) Input a single digit or a character, then press the return key twice.

The program then asks the user to input either a digit (0-9) or a character (a-z) to uniquely identify this case.

> 4-9 Version: 1b

Selecting the Impact Type:

Two impact types are available: impact of one end (primary impact); and impact of one end followed by rotation of the cask and impact of the other end (secondary impact). Impact limiter geometry and force-deflection curves must be defined for both ends of the cask to perform secondary impact calculations. An impact angle of 0 degrees is always a primary and secondary impact (both ends impact at the same time). Impact angles greater than or equal to the CG angle and unbonded shell/shield interface analyses are always primary impact only.

(1) Highlight the *Impact Type* field and press one of the indicated function keys to change the type of impact:

F1 for initial plus secondary impact

F2 for initial impact only

Selecting the Analysis Type:

Two analysis types can be selected: a dynamic, lumped parameter approach that accounts for the dynamic response of the cask and rigid body motion associated with oblique impact; and a quasi-static approach that treats the cask as a slender rigid bar which does not capture dynamic response. Both types are one-dimensional techniques and assume elastic response.

(1) Highlight the Analysis Type field and press one of the indicated function keys to change the type of analysis:

F1 for a Dynamic analysis

F2 for a Quasi-static analysis

Selecting the Shell-Shield Interface Type:

The default shell/shield interface is bonded. That is, the shield is prevented from slumping. An unbonded interface may be selected if the impact angle is greater than 0 and if the cask has a three-layer laminated shell comprised of STEEL, LEAD, and STEEL. An unbonded interface allows the lead shield to slump and contribute radial forces to the steel shells.

**NOTE:** unbonded shell/shield interface analyses are always primary impact only.

(1) Highlight the *Shell/Shield Interface Type* field and press one of the indicated function keys to change the type of shell/shield interface:

F1 for a bonded interface

F2 for an unbonded interface

.\*

Selecting the Primary Impact End:

character, then press the

return key twice.

(1)	Highlight the <i>Primary Impact</i> <i>End</i> field and press one of the indicated function keys to change the primary impact end.	The primary impact end can only be changed if the alternate end has at least one force-deflection curve defined.
	F1 for primary impact on bottom of cask	
	F2 for primary impact on top of cask	·
Sele	cting the Impact Angle:	

- Input the *Impact Angle* and press return.
   The input angles must be less or equal to 90 degrees. The program then asks the user to input either a digit (0-9) or a character (a-z) to uniquely identify this case.
   Input a single digit or
   A 0-degree angle is a side drop, and a 90-degree
  - A 0-degree angle is a side drop, and a 90-degree impact angle is an end-on drop. Side-drop analyses are always a primary and secondary impact with a bonded shell/shield interface. Impact angles greater than or equal to the CG angle are always primary impact only.

Performing the Analysis:

		After all analysis parameters are selected, CASKS indicates whether a solution exists for this case.
(1)	Press <b>P</b> to perform the analysis.	NOTE: P must NOT be pressed where an input is sought, e.g., Drop Height or Impact Angle. P is accepted in any other field—Impact Type, Analysis Type, Shell/Shield Interface or Primary Impact End. See Fig. 4-7.)
		When the analysis is complete, CASKS displays the maximum impact force and acceleration for both primary impact and secondary impact (if included) and lists two options.
(2)	Press <b>P</b> to perform another impact analysis (with different parameter selections)	During dynamic analyses, <b>CASKS</b> displays the current simulation time, cask orientation, and analysis status.
	NOTE: The user can Press F3 to halt the analysis at any point (results are complete up to the point the analysis is halted).	If the impact angle does not correspond to any of the predefined oblique angles with available F/D curves, <b>CASKS</b> selects the F/D curve that is nearest the next higher impact angle.
or		
	Press <b>Q</b> to QUIT and return to the Analysis Menu	

During primary impact, the analysis status indicates "Calculating PRIMARY impact."

When the primary impact analysis is complete, the status is changed to "Primary impact complete."

When a secondary impact is initiated, the analysis status indicates "Calculating SECONDARY impact" and displays both the cask orientation at secondary impact and the impact force-deflection data set angle used for the secondary impact end.

CASKS selects the F/D curve that is nearest to the actual secondary impact angle.

When the secondary impact analysis is complete, the status is changed to "Secondary impact complete."

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Dynamic impact analyses may indicate one of the error messages listed below:

#### Time limit reached

The analysis could not be completed. Probable cause is a very soft impact limiter that does not absorb all the impact energy.

#### Secondary impact reached, only primary requested

The secondary end of the cask impacts before the primary impact analysis is complete. Message appears only if the impact type was restricted to primary only.

#### Chord rotation in element "i" is too large

Indicates a numerical instability. Probable cause is a geometry or weight error.

Quasi-Static impact analyses may indicate the error message listed below:

Force becomes negative before impact energy can be dissipated The Force/deflection curve defined for this configuration does not absorb all the impact energy. Probable cause is an F/D curve that ends with a negative slope.

### Analysis Menu Generating Finite Element Meshes

Generating Finite-Element Meshes:

	Thermal, thermal-stress, and pressure-stress analyses require two-dimensional finite element meshes. The first time one of these analyses is requested for a cask, <b>CASKS</b> automatically generates the F.E. meshes based on the dimensions and mesh gradings in the geometry definition (see Geometry Menu). The generated F.E. meshes are used automatically until any geometry definition is updated.
	When a pressure-stress or thermal analysis is selected after the geometry definition is updated, CASKS indicates that the F.E. mesh predates the current version of the basic geometry. CASKS displays the date and time for both the geometry definition and F.E. mesh and lists several options:
Press C to Continue (the analysis) with the current F.E. mesh	<b>CASKS</b> displays the thermal and stress meshes after generation is complete. The thermal mesh uses 4-node elements and includes all specified cask components. The stress mesh uses 9-node elements (each 9-node
Press G to Generate a new F.E. mesh based on the current geometry	element is equivalent to four, 4-node elements) and includes only the cask shell and end caps. The impact limiters, neutron shield, and water jacket are low- strength components which do not affect stress
Press $\mathbf{Q}$ to QUIT and return to the analysis menu	distributions. After displaying the meshes, CASKS lists several options.
Press <b>T</b> to print the Thermal mesh as a node/element map	The thermal and stress mesh node/element maps are useful for reviewing results from thermal and stress
Press S to print the Stress mesh as a node/element map	Display Menu.
Press C to Continue with the analysis	NOTE: the video display type and printer type are selected from the Display Menu.
Press <b>Q</b> to QUIT and return to the Analysis Menu (Allows abort if display indicates a potential problem)	

Performing Thermal Analysis:

The basic geometry must be defined and complete before **CASKS** can perform a thermal analysis (see Geometry Menu). The Thermal Analysis Title Screen indicates any missing information required before an analysis can be performed.

(1) Press Q to QUIT and return to the Analysis Menu.

or

Press any other key to display the list of available thermal analysis cases (Figure 4-8).

ſ.	s	ELECT THERMAL	ANALYSIS CASE		
	>>> Cold soak Cold soak Normal cold Normal cold Normal hot Normal hot Fire accident	Contents heat No contents Contents heat No contents Contents heat Contents heat Contents heat	No solar effects No solar effects No solar effects No solar effects No solar effects No solar effects	Solution Exists Solution Exists	
	Press any of the following keys S to select indicated case ↑ to move to previous case Q to QUIT and return to MENU ↓ to move to next case				

Figure 4-8. Select Thermal Analysis Case

The case list also indicates whether a solution exists for each case.

(2) Use the keypad up or down arrow keys to highlight the desired case and press S to select and perform the analysis. The thermal cases are described on the next page. All cases, except the fire accident, include convection and radiation heat transfer to the environment. The fire accident case excludes convection heat transfer during the fire and reinstates it after the fire.

CASKS automatically generates the necessary finite element mesh if one has not been previously generated (see Generating Finite Element Meshes).

Cold Soak, Contents Heat, No Solar Effects Ambient temperature: -40°F Contents Heat: As specified in the geometry definition Solar effects: None Analysis type: Steady State

Cold Soak, No Contents, No Solar Effects Ambient temperature: -40°F Contents Heat: None Solar effects: None Analysis type: Steady State

Normal Cold, Contents Heat, No Solar Effects Ambient temperature: -20°F Contents Heat: As specified in the geometry definition Solar effects: None Analysis type: Steady State

Normal Cold, No Contents, No Solar Effects Ambient temperature: -20°F Contents Heat: None Solar effects: None Analysis type: Steady State

### Perform Thermal Analysis

#### Normal Hot, Contents Heat, Solar Effects Ambient temperature: 100°F Contents Heat: As specified in the geometry definition Solar effects: Included Analysis type: Steady State

#### Normal Hot, Contents Heat, No Solar Effects Ambient temperature: 100°F Contents Heat: As specified in the geometry definition Solar effects: None Analysis type: Steady State NOTE: Required as the initial condition for fire accident

#### Fire Accident, Contents Heat, No Solar Effects

Ambient temperature during fire: 1475°F Ambient temperature after fire: 100°F Contents Heat: As specified in the geometry definition Solar effects: None Analysis type: Transient 360 minutes in duration Duration of fire: 30 minutes NOTE: Requires case Normal Hot, Contents Heat, No Solar Effects as the initial condition before the fire

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All thermal cases, except the fire accident, are steady-state analyses. CASKS initiates steady-state analyses after the case selection is made (and after mesh generation, if necessary) and displays the steady-state thermal analysis status screen (Figure 4-9).



Figure 4-9. Steady State Thermal Analysis Status Screen

Since the analysis is nonlinear, CASKS iterates to converge on the correct solution. The iteration number and convergence achieved are updated on the display after each iteration. Also displayed is the maximum number of iterations that CASKS will perform. When the solution converges, CASKS displays the minimum and maximum temperatures and indicates where they occurred.

(3) To abort the steady state analysis (and delete the output) before convergence is achieved, press F9. CASKS asks for confirmation before aborting the analysis.

- (4) Press F1 to abort the analysis.
- or

Press F9 to continue the analysis.

After the analysis is finished, CASKS lists the following options:

(5) Press P to Perform another thermal analysis (redisplays the case list screen)

The transient fire accident analysis requires the steadystate case Normal Hot, Contents Heat, No Solar Effects as the initial condition. CASKS displays a list of transient analysis with their default values (Figure 4-10).

or

Press Q to QUIT and return to the Analysis Menu



Figure 4-10. Transient Analysis Control Parameters

(6) Press **P** to proceed and perform the analysis with the parameters as displayed To modify a parameter, use the keypad up or down arrow keys to highlight the desired field, and then use the indicated keys to select the desired value.

or

press **Q** to QUIT and return to the Analysis Menu

or

modify any of the parameters before performing the analysis.

(7) When the displayed parameter values are correct, press **P** to perform the transient analysis. CASKS displays a transient analysis status screen that is similar to the steady-state status screen. The transient analysis status screen also includes the current solution time, solution time limit, and minimum and maximum temperature for the previous solution time.
## Analysis Menu Perform Thermal Analysis

(8) To end the transient analysis after the current time step, press F5

**CASKS** asks for confirmation before ending or aborting the analysis.

or

To abort the transient analysis (and delete the output), press **F9**.

(9) Press F1 to end or abort the analysis

After the analysis is finished, CASKS lists several options.

or

Press F9 to continue the analysis.

(10) Press P to Perform another thermal analysis (redisplays the case list screen)

or

Press Q to QUIT and return to the Analysis Menu

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# Analysis Menu

### Perform Thermal Analysis

The following descriptions will help the user work with the Transient Analysis Control Parameters Screen (Figure 4-10).

### Specifying the Printed Output Interval

Highlight the *Printed Output Interval* field. Use the + and - keys to change the time interval between saving thermal states for printing. Printed output can be very long. A printout interval of 30 minutes or longer is recommended.

### Specifying the Plotted Output Interval

Highlight the *Plotted Output Interval* field. Use the + and - keys to change the time interval between saving thermal states for plotting.

### Specifying the Iteration Convergence Tolerance

Highlight the *Iteration Convergence Tolerance* field. Use the + and - keys to change the solution convergence tolerance. Increasing the tolerance reduces the number of iterations (and computation time) for solution convergence, but may result in a less accurate solution.

### Specifying the Iteration Relaxation Parameter

Highlight the *Iteration Relaxation Parameter* field. Use the + and - keys to change the relaxation parameter. The relaxation parameter guides the temperature estimate for the current iteration by using a fraction of the temperature change during the previous iteration. Decrease the relaxation parameter to 0.75 or less to dampen highly oscillatory solutions.

### Specifying the Time Step Type

Highlight the Variable Time Step field. Press Y to use a variable time step or N to use a fixed time step. If a fixed time step is selected, CASKS displays the fixed time step parameter. If a variable time step is selected, CASKS displays maximum allowable time step, maximum allowable temperature change during any time step, and time step modification factor.

### Specifying the Fixed Time Step Parameter

Select N for the Use Variable Time Step parameter and highlight the Fixed Time Step field. Use the + and - keys to change the fixed time step. Small time steps will converge faster, requiring fewer iterations. However, the transient analysis duration will be divided into more time steps.

### Specifying the Maximum Allowable Time Step for Variable Time Step

Select Y for the Use Variable Time Step parameter and highlight the Maximum Allowable Time Step field. Use the + and - keys to change the maximum allowable time step. This places a ceiling on the time step size that CASKS can select during the transient analysis.

## Analysis Menu Perform Thermal Analysis

### Specifying the Maximum Allowable Temperature Change During Any Time Step

Select Y for the Use Variable Time Step parameter and highlight the Maximum Allowable Temperature Change During Any Time Step field. Use the + and - keys to change the maximum allowable temperature change during any time step. CASKS uses the temperature change to determine when it is necessary to change the time step size.

### Specifying the Maximum Allowable Temperature Change During Any Time Step

Select Y for the Use Variable Time Step parameter and highlight the Time Step Modification Factor field. Use the + and - keys to change the modification factor. When the time step is increased, the new time step is the current time step multiplied by the modification factor. When the time step is reduced, the new time step is the current time step divided by the modification factor.

### Analysis Menu Perform Thermally-Induced Stress Analysis

CASKS requires at least one completed thermal analysis to perform thermally-induced stress analyses. The number of thermal analysis solutions is indicated on the Thermal Stress Analysis Title Screen. The module used for stress analyses is based on SAP80 from Computers & Structures, Inc. (used by permission).

### Performing Thermally-Induced Stress Analysis:

(1) Press Q to QUIT and return to the Analysis Menu The case list also indicates whether a solution exists for each case.

or

Press any other key to display the list of available thermal stress cases (Figure 4-11)

ſ	SELECT THERMAL STRESS ANALYSIS CASE	
	>>> Normal hot         Contents heat         Solar effects         Solution Exists           Normal hot         Contents heat         No solar effects         Solution Exists           Fire accident         Contents heat         No solar effects         Solution Exists	
	Press any of the following keys S to select indicated case Q to QUIT and return to MENU to move to next case	

Figure 4-11. Select Thermal Stress Analysis Case

 Use the keypad up or down arrow keys to highlight the desired case, and then press
 S to select the indicated case. CASKS will then display the stress-free temperature as specified in the geometry definition (Figure 4-12)

# Analysis Menu

Perform Thermally-Induced Stress Analysis





- (3) Use the keypad + or keys to change this value (allowable range is -40°F to +400°F).
- (4) Use the keypad up or down arrow keys to select a thermal state.

For the fire accident transient analysis, the thermal stress analysis may be calculated for any thermal state (the states correspond to the temperatures saved at the plotting interval).

CASKS indicates which state contains the maximum temperatures on any cask component.

- (5) Press P to perform the analysis with the displayed stress-free temperature (and indicated thermal state, if applicable)
- (6) When the thermal stress analysis is complete, press P to perform another thermal stress analysis

or

Press Q to QUIT and return to the Analysis Menu.

## Analysis Menu Perform Pressure-Induced Stress Analysis

The external pressure conditions are established by the regulatory guidelines. However, the internal pressure conditions are established by the maximum normal operating pressure (input during geometry definition) or the internal pressure resulting from a thermal analysis. CASKS estimates the change in internal pressure using Ideal Gas Laws, based on the initial cavity charge pressure and temperature (input during geometry definition). The Pressure Stress Analysis Title Screen indicates the number of thermal solutions that exist for the cask. The module used for stress analyses is based on SAP80 from Computers & Structures, Inc. (used by permission).

Performing Pressure-Induced Stress Analysis:

(1) Press Q to QUIT and return to the Analysis Menu

or

Press any other key to display the list of available internal pressure conditions (Figure 4-13)

ſ	SELECT INTERNAL PRESSURE CASE	C A S
	>>>> Maximum Normal Operating Pressure100.0 psiaNormal hotContents heatSolar effects18.9 psiaNormal hotContents heatNo solar effects17.6 psiaFire accidentContents heatNo solar effects20.5 psia	<u> </u>
	Current Pressure case: Internal 100.0 psia External 3.5 psia Solution Exists	$\bullet$
	Press any of the following keys S to Select & get External P Q to QUIT 1 to move to previous P to Proceed with analysis and return to MENU 1 to move to next	•



The internal pressure list consists of the Maximum Normal Operating Pressure and the internal pressures estimated by existing thermal analyses.

## Analysis Menu Perform Pressure-Induced Stress Analysis

ð

(2)	Use the keypad up or down arrow keys to highlight the desired internal pressure. Press $S$ to select the indicated internal pressure and display the list of available external pressure conditions.	These pressure conditions are defined by the regulatory guidelines.
(3)	Use the keypad up or down arrow keys to highlight the desired external pressure.	Below the selection list, <b>CASKS</b> displays the selected internal and external pressures and whether a solution exists for this pressure condition.
(4)	Press <b>P</b> to proceed with the analysis using the indicated internal and external pressure conditions	If <b>P</b> is pressed, wait for the pressure stress analysis to complete, then press <b>P</b> to perform another pressure stress analysis
or		
	Press S to select the indicated external pressure and display the list of available internal pressure conditions	If S is pressed, the Select External Pressure Screen appears (Figure 4-14).
or		

Press Q to QUIT and return to the Analysis Menu.

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## Analysis Menu Perform Pressure-Induced Stress Analysis

$\bigcap$	SELECT I	EXTERNAL PRESSURE	CASE	
	>>>Reduced Pressure Atmospheric Pressure Increased Pressure Accident Immersion Equiv. Pre	əssure (21psig)	3.5 psia 14.7 psia 20.0 psia 35.7 psia	- <u>K</u> s
	Current Pressure case: Inter So	nal 100.0 psia Exter olution Exists	nal 3.5 psia	
S P	Press a to Select & get Internal P to Proceed with analysis a	ny of the following keys Q to QUIT and return to MENU	<ul> <li>↑ to move to previous</li> <li>↓ to move to next</li> </ul>	

Figure 4-14. Select External Pressure Case

The Display Menu (Figure 5-1) provides options for plotting dynamic impact analysis results, displaying and printing finite element meshes, plotting thermal analysis results, and setting video and printer attributes.

### PRESS 1 to Plot Dynamic Impact results

Plot the axial force, shear force, bending moment, position of cask top or bottom, cask orientation, and animation of the cask drop. For casks with an unbonded shell/shield interface, plot lead slump, and shell axial and hoop stresses.

### PRESS 2 to Display/Print finite element meshes

Display the thermal and stress finite element meshes (generated during thermal or pressure stress analyses). Print the meshes as node element maps.

### PRESS 3 to Plot Temperature distributions

Plot temperature distributions as iso-contours, time histories, and thermal profiles.



### Figure 5-1. CASKS Display Menu

### PRESS 4 to Set Attributes for Video/Printer Plots

Select video display (CGA or EGA), printer plot resolution (low or high) and type of printer (IBM/Epson graphics printer or HP LaserJet).

### PRESS M to Return to MAIN MENU

CASKS returns to the Main Menu display.

## Display Menu Plot Dynamic Impact Results

#### Plotting the Dynamic Impact Results:

CASKS displays the Plot Dynamic Impact Results Title Screen indicating the number of dynamic impact solutions.

(1) Press **Q** to QUIT and return to the Display Menu

or

CASKS lists the available dynamic impact solutions and indicates the shell/shield interface, impact type, impact end, drop height, impact angle, date, and time (Figure 5-2).

Press any other key to select the dynamic impact solution to plot.

	SELECT DYNAM	/IC IMPACT	SOLUTIO	N TO PLOT	-		
SHELL/SHIEL INTERFACE	D IMPACT TYPE	IMPACT END	DROP HEIGHT	IMPACT ANGLE	DATE	TIME	S K
Bonded Bonded Unbonded	Primary/Secondary Primary/Secondary Primary	Bottom Bottom Bottom	72.0 72.0 15.0	45 90 45	04-14-91 04-15-91 05-03-91	02:50p 03:46p 10:33a	
	Press an	y of the follo	wing keys	;			
S to se Q to QI	lect indicated solution JIT and return to MENI	J	↑ to mo ↓ to mo	ve to previo ve to next s	ous solution solution		

### Figure 5-2. Select Dynamic Impact Solution to Plot

An unbonded shell/shield interface allows the lead shield to slump.

A primary/secondary impact type includes impact of both ends.

The impact end indicates the end that impacts first. Impact angles are relative to the horizontal (i.e., 0 degrees is a side drop).

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## Display Menu Plot Dynamic Impact Results

(2) Use the keypad up and down arrow keys to highlight the desired case. Press S to select the indicated solution for plotting. CASKS displays the Select Plots and Display Parameters Screen (Figure 5-3) and lists several options.

PLOT DYNAM	IIC IMPACT I	RESULTS	C I
SAR: Sample spent fuel storage cask (demonstr	ation only)		A S
CASE: 15in Drop, Angle=45, Bottom Impact, Unb	onded Shell/	Shield interface	K
	PRESS	TO PLOT	
Select PLOT to PRINT	F1	Axial Force	
Set Lower Time Limit	F2	Shear Force	
Current: .0000 seconds	F3	Bending Moment	
Set Upper Time Limit	EA	Position of Cask Ton	
Current: .0857 seconds	55	Position of Cask Rottom	
Reset Time Limits to Full Range	FS	Position of Oask Bollom	
Lower: .0000 seconds	F6	Cask Orientation	
Upper: .0857 seconds	F7	Animation of Cask Drop	
Select Position Along Cask for	F8	Slump at top of Lead column	
Eerce, Shear and Mamont Plats	F9	Axial Stress in Inner Shell	
Porce, Shear and Moment Plots	F10	Axial Stress in Outer Shell	
Current position: .0 inclus	ALT-F1	Hoop Stress in Inner Shell	
Cask Bottom: .U inches	ALT-F2	Hoop Stress in Outer Shell	
Cask Top: 192.5 inches			
Press anv	of the follow	ing keys	
S to Select a different solution		1 to move to previous	
Q to QUIT and return to MENU		choice	
a to don't dire rotant to metro		010100	

### Figure 5-3. Select Plots and Display Parameters Screen

Press S to Select a different dynamic impact case Press Q to QUIT and return to the Display Menu Press  $\uparrow$  to move to previous choice field Press  $\downarrow$  to move to next choice field

or

Press any of the keys indicated in the options box

### Selecting the Plot to Display or Print

### **Plot Dynamic Impact Results**

Highlight the *Select Plot to Display* field to display plots. Highlight the *Select Plot to Print* field to display and print plots. Press one of the following function keys to display the desired plot.

- **F1** to plot Axial Force (Figure 5-5)
- **F2** to plot Shear Force
- **F3** to plot Bending Moment
- F4 to plot Position of Cask Top
- F5 to plot Position of Cask Bottom (Figure 5-6)
- **F6** to plot Cask Orientation
- **F7** to plot Animation of Cask Drop
- **F8** to plot Lead Slump in the Lead Shield (unbonded only)
- **F9** to plot Axial Stress in the Inner Shell (unbonded only)
- **F10** to plot Axial Stress in the Outer Shell (unbonded only)
- ALT-F1 to plot Hoop Stress in the Inner Shell (unbonded only)
- ALT-F2 to plot Hoop Stress in the Outer Shell (unbonded only) (Figure 5-7)

### **Plot Dynamic Impact Results**

Dynamic impact results are plotted as a function of time. The axial force, shear force, and bending moment are calculated for the total cross section of the cask. Plots of force, bending moment, and stress are at the selected position along the cask. Cask orientation plots are relative to the horizontal (0 degrees). Animation of the cask drop displays the position and orientation of the cask at discrete steps during the impact analysis.

### Selecting the Lower and Upper Time Limits

Adjusting the time limits will zoom in on a portion of the time history. Highlight the Set Lower Time Limit field to change the lower time limit. Highlight the Set Upper Time Limit field to change the upper time limit. Use the + and - keys to change the selected value (times are in seconds). The lower time limit must be greater than or equal to 0. and less than the upper time limit. The upper time limit must be greater than the lower time limit and less than or equal to the maximum time limit.

### Resetting the Time Limits to Full Range

Highlight the *Reset Time Limits to Full Range* field and press F1 to reset the time limits to the full range. Used to display full time histories after time limits have been adjusted.

### Selecting the Position Along Cask for Plotting

Highlight the Select Position Along Cask field and use the + and - keys to change the position along the cask where axial force, shear force, bending moment and stresses are plotted (Figure 5-4). Position 0.0 corresponds to the cask bottom.

## Display Menu Plot Dynamic Impact Results



Figure 5-4. Selecting Position Along Cask for Plotting



Figure 5-5. Axial Force Time History Plot



## Display Menu Plot Dynamic Impact Results



Figure 5-6. Plot of Position of Cask Bottom





## **Display Menu** Display/Print Finite Element Meshes

Display/Print Finite Element Meshes:

CASKS displays the Display/Print Finite Element Mesh title screen and gives the status of the F.E. meshes. Mesh displays are always based on the basic geometry description for the TOP end of the cask and use axisymmetry. Thermal meshes use 4-node elements and include all cask components. Stress meshes use 9-node elements and include only the cask shell and end caps.

(1) Press Q to QUIT and return to the Display Menu

or

Press any other key to display the finite element meshes (Figure 5-8).



Figure 5-8. Display of Thermal and Stress meshes

## Display Menu Display/Print Finite Element Meshes

(2) Press **ENTER** after reviewing the meshes and select one of the following options:

Press T to print the Thermal mesh as a node/element map (Figure 5-9).

Press S to print the Stress mesh as a node/element map

Press **D** to Display the meshes again Press **Q** to QUIT and return to the Display Menu

## **Display Menu** Display/Print Finite Element Meshes

CASK ID: 9999 NODE/ELEMENT map of THERMAL MESH SCANS Version 2a Generated on 5/09/91 at 6:57:55 SAR: Sample spent fuel shipping cask (demonstration only) N O T T O S C A L E NOTE -- Mesh is axisymmetric model for TOP half of cask

Material numbers ... (printed in corner of each element)

l= Inner Shell	4= End cap inner layer	7= Neutron Shield
2= Shell shield	5= End cap shield layer	8= Water Jacket
3= Outer Shell	6= End cap outer layer	9= Impact Limiter

139.8	196	197	198	199	2002	201	202i	203	204	2052	2062	2072	20()	2092	510	2112	212	213
	226	227 #19	228	229 #7	230	231	232	233	234	235	236	237	238	239	240	241	242	
127.8	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	
115.8	246	247	248	249	50	251	252	253	254	255	56	257	256	59	260	261	262	215
103.8	8	195 19	20	215	190 #9	3	190 190		200	201 #9	202 #9	203 #9	204 89	205 #7	206	207	208	216
	151	152	153 #0	154 #0	155 #0	156 mó	157 #6	158 86	159 #6	160 #0	161 805	162 50	163 50	164 #6	189	190 #9	191 #7	
102.5	137	138	139	140	141	142	143	166	145	146	147	148	149	150	186	187	188	217
101.3	68	69	70	71	72	73	74	75	76	77	78	79	80	81	····	40	er7 241	18
100.0	54	55	123 80 56	120 80	127 #6 58	126 80 59	60	130 61	62	132 #0 63	155 80 66	134 86 65	135 #6	136 #6 67	183 #9 55	184 #9 38	185	219
<b>68 8</b>	109	110 mo	111 #6	112 60	113 	114	115 	116	117 80	118 #6	119 80	120 120	121 #0	122	180 #7	181 #9	182 #7	
Y0.8	95	96	97	98	99	100	101	102	103	104	105	106	107	108	177	178	179	20
97.5	26	27	28	29	30	31	32	33	34	35	36	37	38	39	37	34	235	21
96.3	86		#6	<b>F</b> 0	e0	<b>1</b> 0	<b>1</b> 0	#6 19	20	21	22	23	875 24	25	<b>9</b>	32	33	22
							19 m1	20 1	57 #2	58 #2	59 #2	60 62	79 =3	80 R3	171	172	173	
0.0							17	18	53	54	55	56	π	78	165	169	170	
75.3 ···						,		16	06 40	07	08	69	10	11	0	28	229;	24
64.8							m1 0	m1 86	<b>a</b> 2	e2 00	#2 01	52 02	03 •3	#3 04	1	±9	#9 226	25
55.5							13 =1	14 @1	45	46 82	47 #2	48 82	73 83	74 3	,			
							11	12	41	42	43	4	71	72	Î			
46.3							22	10	37	38	39	8( 40	9 69	0 70	3			
37.0							#1 3;	e1 7	<b>5</b> 2	#2 9	e2	m2	هئ 2	83 35	4			
27.8							7 =1	8 #1	33 2	34	35 #2	36 #2	- 67 • 33	68 83	s			
							S m1	6 m1	29 #2	30 #2	31 #2	32 #2	45 83	66 83				
18.5						1	3	4	25	26	27	28	a	64				
<b>9.3</b>							m1	<b>m1</b>	7	8	#2 9	 	•3 1	2	l7 1			
.0							, al	2 m1	21 #2	22 #2	23	22 m2	61 m3	62 83	Į.			

x 1.0 L.3 d.5 12.8 17.1 21.4 25.6 20.1 26.6 27.6 28.6 29.5 30.5 31.6 32.8 41.8 50.9 00.0

Figure 5-9. Thermal Node/Element Map

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Plotting Temperature Distributions:

CASKS displays the Plot Thermal Analysis Results Title Screen and indicates the number of thermal solutions.

(1) Press **Q** to QUIT and return to the Display Menu, or press any other key to select the thermal solution to plot.

CASKS lists the available thermal solutions and displays the thermal case description, contents heat, date, and time for each solution (Figure 5-10).

THERMAL SOLUTIONS								
THER	VAL CASE DESCR	PTION	CONTENTS HEAT	DATE	TIME	ĞК S		
Normal hot Normal hot Fire accident	Contents heat Contents heat Contents heat	Solar effects No solar effects No solar effects	500.00 500.00 500.00	10-02-88 10-13-88 10-13-88	3:19p 1:51p 1:58p	Ó		
S to Sel Q to QU	Pre ect indicated case IT and return to MB	ss any of the follov ENU	ving keys ↑ to move to previ ↓ to move to next	ous case case		•		



The case description indicates the external temperature condition and the status of contents heat and solar effects. The applied contents heat is in Btu/min.

(2) Use the keypad up or down arrow keys to highlight the desired case and press S to select the indicated solution for plotting.
After the case is selected, CASKS displays the Select Plots and Display Parameters Screen (Figure 5-11) and lists several options.

Press  $\mathbf{S}$  to select a different thermal case

Press  $\mathbf{Q}$  to QUIT and return to the Display Menu

Press ↑ to move to previous choice field

Press  $\downarrow$  to move to next choice field

or

Press any of the keys indicated in the options box



### Figure 5-11. Select Plots and Display Parameters Screen

**NOTE:** Enter values in the same manner as entering values when editing the geometry or impact limiter curves (see Appendix A).

### Selecting the Plot to Display or Print

Highlight the Select Plot to Display field to display plots. Highlight the Select Plot to Print field to display and print plots. Press one of the following function keys to display the desired plot.

- F1 to plot Thermal Iso-contours (Figure 5-16)
- F2 to plot Temperature along a Profile (Figure 5-17) (only if Line for Profile Plot is defined)
- F3 to plot Time History of Nodes (or Elements) (Figure 5-18) (only if Items for Time History Plots are defined)
- F4 to plot Material Outline (Figure 5-19)
- F5 to plot Finite Element (F.E.) Mesh
- F6 to plot F.E. Mesh with Material Numbers
- F7 to plot F.E. Mesh with Element Numbers
- F8 to plot F.E. Mesh with Node Numbers
- **F9** to plot Geometry showing Profile Line (Figure 5-20) (only if Line for Profile Plot is defined)

### **Plot Temperature Distributions**

Thermal iso-contours are lines of constant temperature plotted on the geometry material outline. Plots of temperature along a profile are: (1) the temperature profile along a line cutting the geometry (the line may be defined by XY coordinates or nodes numbers); or (2) temperature plotted for specified nodes as a function of distance between the nodes. Time history plots of nodal temperatures or averaged element temperatures are only available for the transient fire case. Up to six time histories per plot are allowed. Cask components are represented as different materials. Material outline plots are composed of outlines for each component selected for display. The finite element mesh can be plotted showing the mesh only, the mesh with material numbers, the mesh with element numbers, and the mesh with node numbers. Use the ZOOM option to isolate portions of the mesh when element or node numbers overlay one another. When a temperature profile line has been defined, the line can be plotted on the cask material outline to verify its location.

### Selecting the Time for Iso-contour and Profile Plots

Highlight the *Time for Iso-contour and Profile Plots* field and use the + and - keys to change the time state for plotting. If the case is a steady state solution (all cases except transient fire) the time cannot be changed.

### Setting the Zoom for plots with geometry

Highlight the *Set Zoom* field and press one of the indicated function keys to change the zoom for geometry displays. Zoom on small portions of the geometry for more detailed views (Figure 5-21). This is helpful when displaying the finite element mesh with node or element numbers.

- F1 to Automatically center and display the full geometry
- **F2** to ZOOM on specified coordinates
- **F3** to ZOOM on a specified node

For zoom on specified coordinates (Figure 5-12), enter the X and Y coordinates which define the center of the plot and the width of the geometry to plot around the plot center. For zoom on a specified node, enter the number of the node which defines the center of the plot instead of X Y coordinates. After specifying the zoom conditions, press one of the following keys:

- Press D when DONE entering values
- Press A to revert to Automatic centering and display full geometry
- Press Q to QUIT and return to the Display Menu



Figure 5-12. ZOOM on Specified Coordinates

### Selecting the Symmetry Displays

Highlight the *Select Symmetry Displays* field and press one of the indicated function keys. **CASKS** uses an axisymmetric model of the TOP end of the cask to represent the thermal geometry. Reflect about the Y axis to simulate the geometry full width. Reflect about the X axis to simulate the geometry full length. Reflect about both the X and Y axes to simulate the full cask geometry.

- F1 for NO symmetry reflections
- F2 to reflect about the Y axis (Figure 5-22)
- **F3** to reflect about the X axis
- F4 to reflect about the X and Y axes

### Selecting the Materials to Include for Geometry and Iso-contour Plots

Highlight the *Select the Materials to Include* field and press one of the indicated function keys. CASKS represents each cask component as a different material. Use this option to isolate cask components for iso-contour and outline plots.

- F1 to Include ALL Materials in the Plots
- F2 to Select Materials for Plots

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Figure 5-13. Select Materials for Plotting

When selecting materials, CASKS displays a list of all cask components indicating the material number, component name, and whether the component is included or omitted for iso-contour and outline plots (Figure 5-13). Press the indicated function keys to include specific components or press ALT and the function key to omit components. To complete material selections, press one of the following:

- Press **D** when DONE selecting materials
- Press A to include ALL materials
- Press **Q** to QUIT and return to the Display Menu

### Specifying the Iso-contour Plot Limits

Highlight the *Specify the Iso-contour Plot Limits* field and press one of the indicated function keys to specify the contour range. Use the + and - keys to change the number of evenly spaced contour lines.

- F1 to set to Automatic ranging
- **F**·2 to specify the contour range
- + to increase the number of contour lines (maximum is 8)
- to decrease the number of contour lines (minimum is 2)

### **Plot Temperature Distributions**

Automatic ranging sets the contour range based on the minimum and maximum temperatures of the components included for display. For a specified contour range, enter values for the FIRST and LAST contour lines. The remaining contour lines are evenly spaced in between. Enter values in the same manner as entering values when editing the geometry or impact limiter curves. NOTE: The value of the FIRST contour line must be less than the value for the LAST contour line. After specifying the contour range, press one of the following:

- Press **D** when DONE entering values
- Press A to revert to Automatic ranging
- Press Q to QUIT and return to the Display Menu

### Defining a Line for a Profile Plot

Highlight the *Define Line for Profile Plot* field and press one of the indicated function keys to define one of the three types of temperature profile lines. Profile lines defined between XY coordinates or between two nodes produce plots of the temperature profile along the defined line where it crosses the geometry. Profile lines defined as a series of nodes produce plots of temperature for the specified nodes as a function of the distance between the nodes. The temperature profiles between successive nodes in the series are drawn as a straight lines and do not reflect the actual temperature profiles between nodes.

- F1 to Define a Line Between XY Coordinates
- F2 to Define a Line Between Two Nodes (Figure 5-14)
- **F3** to Define a Line as a Series of Nodes

When defining a profile line between XY coordinates, enter X and Y coordinates for both ends of the line. NOTE: The line must have a finite length (the coordinates of the first point must not equal the coordinates of the second point). When defining a profile line between two nodes, enter a node number for each end. NOTE: the first node must not equal the second node. When defining a profile line as a series of nodes, enter node numbers for each node in the series. If the series has less than 12 nodes, terminate the list with a node number of zero. After defining the profile line, press one of the following keys:

- Press  $\mathbf{D}$  when DONE entering values
- Press A to ABANDON line definition
- Press  $\mathbf{Q}$  to QUIT and return to the Display Menu

Define Temperature Profile Line Between Two Nodes	C A S K
Fill in the HIGHLIGHTED fields with the appropriate values NOTE: 1st Node must not equal 2nd Node	
Range of Available Node Numbers: 1 to 282	
Number of 1st Node[1 ]	
Number of 2nd Node[213 ]	
Press any of the following keys	
D when DONE defining line       ↑ to move to previous field         A to ABANDON line definition       ↑ to move to previous field         Q to QUIT and return to MENU       ↓ to move to next field	∫●

Figure 5-14. Define Profile Line Between Two Nodes

### Specifying Profile Plot Limits

Highlight the *Specify Profile Plot Limits* field and press one of the indicated function keys to specify the temperature range for the temperature profile plots.

- F1 to set to Automatic ranging
- F2 to specify the Temperature range

Automatic ranging sets the temperature range based on the minimum and maximum temperatures along the profile line. For a specified temperature range, enter values for the LOWER and UPPER temperature limits. NOTE: The value of the LOWER temperature limit must be less than the value for the UPPER temperature limit. After specifying the profile temperature range, press one of the following:

- Press **D** when DONE entering values
- Press A to revert to Automatic ranging
- Press **Q** to QUIT and return to the Display Menu

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### **Plot Temperature Distributions**

### Defining Items for Time History Plots

Highlight the *Define Items for Time History Plots* field and press one of the indicated function keys to select the nodes or elements for time history plots. Up to six nodes or elements may be plotted on a single time history plot. Element temperatures are calculated as the average of the temperatures of the nodes defining the element. Time history plots are only available for transient fire case solutions.

- F1 to Specify NODES for Time History Plots (Figure 5-15)
- F2 to Specify ELEMENTS for Time History Plots

Enter up to six node or element numbers. If the list has less than six node or element numbers, terminate the list with a node or element number of zero. After specifying items for time history plots, press one of the following keys:

- Press **D** when DONE selecting items
- Press A to ABANDON selections
- Press  $\mathbf{Q}$  to QUIT and return to the Display Menu

### Specifying Time History Plot Limits

Highlight the *Specify Time History Plot Limits* field and press one of the indicated function keys to specify the temperature range for time history plots.

- F1 to set to Automatic ranging
- F2 to specify the Temperature range

Automatic ranging sets the temperature range based on the minimum and maximum temperatures of the nodes or element for the full time history. For a specified temperature range, enter values for the LOWER and UPPER temperature limits. NOTE: The value of the LOWER temperature limit must be less than the value for the UPPER temperature limit. After specifying the time history temperature range, press one of the following:

- Press D when DONE entering values
- Press A to revert to Automatic ranging
- Press Q to QUIT and return to the Display Menu



### Figure 5-15. Select NODES for Time History Plots







Figure 5-17. Plot of Temperature Along Profile Between Nodes 1 and 213 Profile line is shown in Figure 5-20











Figure 5-20. Plot of Geometry Showing Profile Line

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Figure 5-22. Iso-contour Plot with Y Axis Reflection

CASKS displays the Set Attributes for Video/Printer Plots Screen shown in Figure 5-23. Select the desired attributes for display type, printer plot resolution, and printer type. Then press Q to QUIT and return to the Display Menu.

### Selecting the Display Type

Press C for Color Graphics Adapter (one color, 640 x 200 pixels)

Press E for Enhanced Graphics Adapter (three colors, 640 x 350 pixels)

#### Selecting the Printer Plot Resolution

Press **H** for HIGH resolution printer plots Press **L** for LOW resolution printer plots

Printer plots are for graphics displays and require a printer that supports graphics. High resolution plots take up to 10 times longer to print than low resolution plots.

### Hint:

Use low resolution plots until report-quality plots are required. Switch to high resolution for report-quality plots, then return to low resolution.



Figure 5-23. Set Video/Printer Plot Attributes

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### Selecting the Printer Type

Press J for Hewlett Packard LaserJet printer Press I for IBM/Epson graphics type dot matrix printer

CASKS can utilize any dot matrix printer that uses the same graphics commands as the IBM Proprinter and Epson FX-85.

CASKS uses the three Hewlett Packard LaserJet printer models in a limited fashion. Node/element mesh maps are printed using the standard Courier font (10 characters per inch) and the Line Printer font (16.66 characters per inch). LOW resolution plots are drawn using 150 dpi (dots per inch) graphics mode; HIGH resolution plots are drawn using 300 dpi graphics mode. Each LaserJet model is described below with its particular limitations and possible remedies.

### LaserJet

- (1) The Line printer font is not an internal font. Provide a font cartridge which contains the Line Printer font for mesh maps.
- (2) The maximum graphics mode resolution is 75 dpi. Both LOW and HIGH resolution printer plots are printed piecemeal on several pages. If the LaserJet upgrade is installed, printer plots are printed on one page.

### LaserJet+

(1) The maximum graphics mode resolution is 150 dpi. LOW resolution printer plots are printed on one page and HIGH resolution plots are printed piecemeal on several pages. If the LaserJet+ upgrade is installed, HIGH resolution plots are printed on one page.

### LaserJet Series II

(1) The maximum graphics mode resolution is 150 dpi. LOW resolution printer plots are printed on one page and HIGH resolution plots are printed piecemeal on several pages. If a 1 Mbyte memory board is installed, HIGH resolution plots are printed on one page.

## **Print/Review Menu**

The Print/Review Menu (Figure 6-1) provides options for printing and reviewing the Cask Summary/Data Check and outputs from Impact, Thermal, Thermal Stress, and Pressure Stress analyses. Output for Thermal, Thermal Stress, and Pressure Stress can also be printed as an abbreviated output summary. The review function displays the output on the screen. The outputs are discussed in Appendix C.

### PRESS 1 to Print/Review Impact Output

Print or Review Dynamic or Quasi-Static Impact analysis output.

### PRESS 2 to Print/Review Thermal Output

Print or Review Thermal output. Abbreviated prints skip the summary of input, printing the temperature output with flux balances.

### PRESS 3 to Print/Review Thermal Stress Output

Print or Review Thermal stress output. Abbreviated prints skip nodal displacements and element stresses, printing the summary of maximum stresses and stresses corresponding to Impact nodal locations.



Figure 6-1. CASKS Print/Review Menu

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## **Print/Review Menu**

### PRESS 4 to Print/Review Pressure Stress output

Print or Review Pressure stress output. The abbreviated print skips the nodal displacements and element stresses and includes a table of maximum stresses and the stresses corresponding to Impact nodal locations.

### PRESS 5 to Print/Review Cask Summary and Data Check

Print or Review the geometry summary / data check for basic geometry and impact limiter force/deflection curve data.

### PRESS M to Return to Menu

CASKS returns to the Main Menu display.
Selecting the Output to Print/Review

#### Selecting the Output to Print/Review:

(1) Press the appropriate Menu key to select the output type.

CASKS displays the Print/Review Title Screen indicating the number of outputs available for printing or review.

(2) Press **Q** to QUIT and return to the Print/Review Menu, or press any other key to select a particular output case to print or review. CASKS lists the available outputs and displays a description, date, and time for each output (Figure 6-2).

		IMPACT	SOLUTIO	NS				
ANALYSIS TYPE	SHELL/SHIELD	IMPACT TYPE	IMPACT END	DROP HEIGHT	IMPACT ANGLE	DATE	TIME	
Dynamic Dynamic Dynamic Quasi-static Quasi-static	Bonded Bonded Bonded Bonded	Primary/Secondary Primary/Secondary Primary Primary/Secondary Primary/Secondary	Bottom Bottom Bottom Bottom	72.0 72.0 15.0 72.0 72.0	45 90 45 45 90	04-15-91 04-15-91 05-03-91 04-15-91 04-15-91	02:50p 02:46p 10:33a 02:51p 02:51p	٩
Press any of the following keys								
S to Select indicated solution   ↑ to move to previous solution     Q to QUIT and return to MENU   ↓ to move to next solution								

Figure 6-2. Select Solution to Print/Review

Selecting the Output to Print/Review

Output Type	Description
Impact	The case descriptions indicate the analysis type, shell/shield interface, impact type, impact end, drop height, and impact angle. An unbonded shell/shield interface allows the lead shield to slump. A primary/secondary impact type includes impact of both ends. The impact end indicates the end that impacts first. Impact angles are relative to the horizontal (i.e., 0 degrees is a side drop).
Thermal and Thermal stress	The case descriptions indicate the external temperature condition, the status of the applied contents heat, and the status of solar effects. The applied contents heat is in Btu/min.
Pressure stress	The case descriptions indicate the internal and external pressures. The internal pressure is the maximum normal operating temperature (input during geometry definition) or the internal pressure resulting from a thermal analysis. The external pressure is established by regulatory guidelines.
Summary / Data Checks	The description indicates the basic geometry specifications or impact limiter force/deflection curves.

Use the keypad up or down arrow keys to highlight the desired case.
Press S to select the indicated solution to print or review.

After the output is selected, CASKS displays an Output Summary Screen indicating the number of pages in the output, if abbreviated output is available, and the output header (Figure 6-3).

Selecting the Output to Print/Review

	l C
OUTPUT has 7 pages	A S K S
OUTPUT HEADER	
DYNAMIC IMPACT OUTPUT FOR CASK 9999 GENERATED ON 04/15/91 AT 14:46:45 CASKS VERSION: 1a SAR: Sample spent fuel storage cask (demonstration only) 72.0 in drop on cask bottom - primary and secondary impact Angle of primary impact is 45 degrees - shield/shell interace is bonded	
P to Print the OUTPUT	
R to Review the OUTPUT on the screen	
S to Select a different OUTPUT to Print/Review	
Q to QUIT and return to MENU	

Figure 6-3. Output Summary Screen

The output header indicates the type of analysis, date and time the output was generated, and a brief description of the parameters defining the output. CASKS then lists several options.

Press P to Print the OUTPUT

Press  $\mathbf{R}$  to Review the OUTPUT on the screen

Press S to Select a different OUTPUT to Print/Review

Press  $\mathbf{Q}$  to QUIT and return to the Print/Review Menu

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### Printing the Output

If you press **P** at the Output Summary Screen, **CASKS** displays a reminder to make sure the printer is ON-LINE and set to the TOP-OF-PAGE. Press one of the following keys:

- Press **P** to Print the complete output
- Press A to print the Abbreviated output (if available)
- Press Q to QUIT and return to the Print/Review Menu

As the output is printed, CASKS indicates the current page being printed. Press any key to suspend printing. When printing is halted, CASKS lists the following options:

Press C to Continue Press Q to QUIT and return to the Print/Review Menu

After printing is finished, CASKS lists the following options:

Press **P** to Print/Review another case (redisplays the case list screen for current output type) Press **Q** to QUIT and return to the Print/Review Menu

**Reviewing the Output** 

After pressing  $\mathbf{R}$  on the Output Summary Screen, CASKS displays the first 20 lines of the full output on the screen (Figure 6-4). CASKS can review up to 4000 lines of output (the entire output can be printed). The review control options are:

Press	S	to print the 20 lines displayed on the screen
Press	ESC	to exit (end review)
Press	Р	to print the output (see Printing the Output)
Press	î	to scroll screen down, displaying previous line at top
Press	$\downarrow$	to scroll screen up, displaying next line at bottom
Press	Home	to display first 20 lines of output
Press	End	to display last 20 lines of output
Press	PgUp	to display previous 20 lines of output
Press	PgDn	to display next 20 lines of output

The symbol **<FF>** represents form feeds used to paginate the output. Press **ESC** to terminate reviewing the output. **CASKS** lists the following options:

Press	P	to Print/Review another case
		(redisplays the case list screen for current output type)
Press	Q	to QUIT and return to the Print/Review Menu

(	Press any of the fol	lowing keys		
S to print Screen	ESC to exit		P to Print output	A
↑ for previous line	Home for first so	creen	PgUp for previous screen	κ.
↓ for next line	End for last scre	en	PgDn for next screen	S
	IMPACT SU	MMARY		
PRIMARY IMPACT (Cask	Bottom)			
Impact Velocity	=	235.9	in/sec	
Impact Angle	=	45.0	degrees	
CG Over Corner Angle		74.4	degrees	
Maximum Limiter Crush	=	11.3	inches	
Maximum Rigid Body Acc	elerations			
Vertical Acceleration	=	9.4	g's	
Horizontal Acceleration	=	-1.4	g's	
Rotational Acceleration	· <b>=</b>	-45.0	rad/sec**2	
Maximum Impact Forces				
Axial Force In Cask	=	-1009.3	kips	
	Position in output	: 13%		



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NOTES:

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The Archive Menu (Figure 7-1) provides options for archiving cask data sets to diskettes, retrieving archived cask data sets, and deleting cask data sets from the hard disk.

#### PRESS 1 to Archive CASK data set on diskettes

Creates a compressed data set archive containing the basic geometry, impact limiter force-deflection curve data, finite-element meshes and all analysis output for the selected cask. Then writes the data set archive to diskettes.

#### PRESS 2 to Retrieve CASK data set from diskettes

Retrieves a compressed data set archive from diskettes and uncompress, restoring the data set to the hard disk.

#### PRESS 3 to Delete CASK data set from hard disk

Deletes either a complete data set or analysis output for the selected cask.

#### PRESS M to Return to MAIN MENU

CASKS returns to the Main Menu display.

CASKS PRESS 1 To Arcl 2 To Ret 3 To Dela	ARCHIVE MENU Current CASK ID is 9999 nive CASK data set on diskettes rieve CASK data set from diskettes ete CASK data set from hard disk	CASKS	C <sub>A</sub> s K <sub>S</sub>
M To Ret	urn to MAIN MENU		0
	-		

#### Figure 7-1. CASKS Archive Menu.

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## Archive Menu Archiving Data Sets

#### Archiving Data Sets:

CASKS archives data sets by creating a compressed data set archive and then writing the archive to a diskette. If the archive is larger than a single diskette, CASKS automatically uses the DOS utility *BACKUP* to save the archive on more than one diskette. The module used to create the compressed archive is adapted from ARC version 5.1 from System Enhancement Associates (used by permission). All existing data sets can be archived from the Archive Menu. The number of existing data sets is indicated on the Archive Data Sets Title Screen.

(1) Press **Q** to QUIT and return to the Archive Menu

If more than one data set exists, **CASKS** displays a list of CASKIDs and several options.

or

Press any other key to select the data set to archive.

Press S to Select the highlighted CASKID and display summary

Press  $\mathbf{Q}$  to QUIT and return to the Archive Menu

Press ↑ to highlight the previous CASKID

Press  $\downarrow$  to highlight the next CASKID

If only one data set exists, CASKS selects that data set. The data set summary screen is shown in Figure 7-2.

Archiving Data Sets



Figure 7-2. Summary of data set for Archive

If S is selected, the Summary Screen options are:

Press A to Archive the summarized data set

Press S to select a different CASKID (return to the CASKID list screen—only if more than one data set exists)

Press  ${\bf Q}$  to QUIT and return to the Archive Menu

Press A to Select DRIVE A:

Press B to Select DRIVE B:

Press  $\mathbf{Q}$  to QUIT and return to the Archive Menu

CASKS starts the archive process by creating a compressed data set archive. This process can take up to 30 minutes if the data set is large and the PC is slow (ATs are much faster). The resulting compressed archive requires only 15 to 30 percent of the space the complete data requires. After the compressed archive is created, CASKS asks for a formatted diskette in drive A: or B:. Because of potential drive/diskette incompatibility, do not use a 360Kb diskette in a 1.2Mb drive.

**CASKS** checks the selected drive and compares the space requirements for the archive with the available space on the diskette.

The error conditions that can occur are listed in Table 7-1. Archiving will not proceed until all error conditions are satisfied.

## Archive Menu Archiving Data Sets

If the compressed archive will fit on a single diskette, CASKS will use *COPY* to write the archive to the diskette. If the archive will not fit on a single diskette, CASKS will use *BACKUP* to write the archive to multiple diskettes (CASKS indicates how many formatted diskettes of similar density are required). If the archive exists on the diskette, CASKS displays the date and time of the hard disk version and diskette version of the archive.

Press the appropriate key to continue with archiving:

Press ENTER to write the Archive to diskette

(using *COPY* if the archive will fit on one diskette)

(using *BACKUP* if the archive will not fit on one diskette)

**NOTE:** If archive exists on diskette, it is pre-deleted

or

Press S to Select different Diskette or Drive

or

Press  $\mathbf{Q}$  to QUIT and return to the Archive Menu

Press C to Continue (to select other data sets to archive)

Press **D** to DELETE cask data set (from the hard disk)

Press F1 to delete the data set

or

Press **F9** to continue without deleting.

BACKUP will request necessary number of diskettes to complete the BACKUP process. Be sure to label the diskettes with the order in which they were processed. RESTORE will request BACKUP diskettes in the order they were written.

When **CASKS** finishes writing the archive to diskettes, the following options are presented.

CASKS asks for confirmation before deleting any data set.

After archiving the data set is complete, CASKS displays the number of data sets remaining on the hard disk that may potentially be archived.

Archiving Data Sets

If no data sets remain on disk, press **ENTER** to return to the Archive Menu.

or

If one or more data sets remain on disk, press A to archive additional data sets.

or

Press **Q** to QUIT and return to the Archive Menu.

### Archiving Data Sets

#### Table 7-1. Possible Error Messages during Archiving

#### There is NO diskette in drive X:

Possible causes: wrong drive selected, or drive door is not closed. Make sure a diskette is in drive A: or B: and that the drive door is closed.

# Diskette is UNFORMATTED or a 1.2Mb diskette is in a 360K drive

Possible causes: diskette is unformatted, diskette is damaged and unreadable, or 1.2Mb diskette is in a 360K drive. Make sure the diskette is formatted and of the correct density.

#### General ERROR on drive X:

Possible causes: diskette is reversed, diskette is damaged and unreadable, or drive is malfunctioning. Try a different drive and/or diskette.

#### Not enough space on the diskette

The compressed archive will fit on the diskette if other data is not on the diskette. Either remove data from the diskette or provide a diskette that has more space.

Diskette is a BACKUP diskette, ARCHIVE will fit on one diskette CASKS will use COPY to write the archive on a single diskette. Existing data on the diskette was written by BACKUP. Use a non-BACKUP diskette.

#### Diskette is a BACKUP diskette NOT for this ARCHIVE

**CASKS** will use *BACKUP* to write the archive on multiple diskettes. Existing data on the diskette was written by *BACKUP* for data other than this archive. Use a different diskette.

## **Retrieving Data Sets**

Retrieving Data Sets:

		<b>CASKS</b> retrieves compressed data sets from diskettes and then unpacks the archive, restoring the data set to the hard disk. The module used to unpack the compressed archive is adapted from ARC version 5.1 from System Enhancement Associates (used by permission). <b>CASKS</b> lists two options on the Retrieve Data Sets title screen:
or	Press $\mathbf{Q}$ to QUIT and return to the Archive Menu	Place the diskette containing the compressed data set archive (or the first <i>BACKUP</i> diskette for the archive) in either drive A: or B:
0,	Press any other key to start retrieval	
	of data set	
Pre	ess one of the following keys:	CASKS checks the selected drive and searches for archived data sets. The error conditions that can occur
	Press A to find data sets on diskette in Drive A:	are listed in Table 7-2. Retrieval will not proceed until all error conditions are satisfied.
	Press <b>B</b> to find data sets on diskette in Drive <b>B</b> :	
	Press <b>Q</b> to QUIT and return to the Archive Menu	
		If the diskette contains only one archived data set, CASKS selects that data set for retrieval. If the diskette contains more than one archived data set, CASKS displays a list of CASKIDs for the archived data sets and lists several options:
	Press S to Select the highlighted CASKID for retrieval	<b>CASKS</b> displays the date and time of the selected archive on the diskette and warns if this data set will replace an existing data set on the hard disk. <b>CASKS</b>
	Press <b>Q</b> to QUIT and return to the Archive Menu	lists the following options
	Press ↑ to highlight the previous CASKID	
	Press↓ to highlight the next CASKID	

### **Retrieving Data Sets**

Press ENTER to retrieve the Archive

(using COPY if the archive was saved with COPY)

(using *RESTORE* if the archive was saved with *BACKUP*)

or

Press S to Select different Diskette or Drive

or

Press Q to QUIT and return to the Archive Menu

Press F1 to delete the data set from the hard disk, or press F9 to QUIT and return to the Archive Menu.

CASKS asks for confirmation before deleting the existing data set.

After deleting the data set (if necessary), CASKS starts retrieving the archived data set.

If the archive was saved using *BACKUP*, **CASKS** uses *RESTORE* for retrieval. *RESTORE* will request the archive *BACKUP* diskettes in the order they were written.

After the archive is retrieved from the diskette, CASKS unpacks the data from the archive. Be patient, this process may take a little while.

When unpacking is complete, press  $\mathbf{R}$  to retrieve additional data sets or press  $\mathbf{Q}$  to QUIT and return to the Archive Menu.

#### Table 7-2. Possible Error Messages during Retrieving

#### There is NO diskette in drive X:

Possible causes: selected the wrong drive; drive door is not closed. Make sure a diskette is in drive A: or B: and that the drive door is closed.

## Diskette is UNFORMATTED or a 1.2Mb diskette is in a 360K drive

Possible causes: diskette is unformatted; diskette is damaged and unreadable; 1.2Mb diskette is in a 360K drive. Make sure the diskette is formatted and of the correct density.

#### General ERROR on drive X:

Possible causes: diskette is reversed; diskette is damaged and unreadable; drive is malfunctioning. Try a different drive and/or diskette.

#### NO Archives on diskette

Diskette does not contain any compressed data set archives. Archive names have the form xxxxDATA.ARC, where xxxx is the four digit CASKID. Try a different diskette.

## Archive Menu Retrieving Data Sets

**Deleting Data Sets:** Data sets consist of basic geometry descriptions, impact limiter force-deflection curves, and analysis outputs. CASKS has two options for deleting data sets: (1) delete the complete data set, or (2) delete just the analysis outputs. All existing data sets can be deleted from this menu. CASKS indicates the number of existing data sets and lists two choices: If only one data set exists, CASKS selects that data Press Q to QUIT and return to the set and displays a summary of the data set. If more Archive Menu than one data set exists, CASKS displays a list of CASKIDs and indicates several options. or Press any other key to select the data set to delete After the data set is selected, CASKS displays a Press S to Select the highlighted summary of the data set. The data set summary screen CASKID and display data set displays several options: summary Press Q to QUIT and return to the Archive Menu Press 1 to highlight the previous CASKID Press  $\downarrow$  to highlight the next CASKID Press C to delete COMPLETE data set Press O to delete OUTPUT for the data set Press S to select a different data set (available only if more than one data set is on disk) Press Q to QUIT and return to the Archive Menu

### **Retrieving Data Sets**

Press F1 to delete the data set or output

CASKS asks for confirmation before deleting the data set or output as shown in Figure 7-3.

or

Press F9 to QUIT and return to the Archive Menu without deleting

or

If no data sets remain on disk, press **ENTER** to return to the Archive Menu.

Press **D** to Delete additional data sets

(redisplays the data set list screen)

Press  $\mathbf{Q}$  to QUIT and return to the Archive Menu

When CASKS has completed deleting the data set or output, if one or more data sets remain on disk, CASKS lists several options.

#### CAUTION!!

Once a data set or its output is deleted, it is not recoverable unless it was archived on diskettes. Be careful when deleting data sets or data set outputs.

#### HINT:

Consider deleting data set outputs before archiving. CASKS can reproduce analysis outputs based on the basic geometry descriptions and impact limiter force/deflection curves. Archiving just the basic geometry and limiter curves is much faster than archiving a data set with numerous outputs.

### **Retrieving Data Sets**



Figure 7-3. Confirm decision to DELETE screen

**CASKS** uses a general purpose fill-in-the-blank type editor to enter data for the basic geometry definition, impact limiter force-deflection curve definitions, and yielding surface force-deflection curve definitions. The editor title screen indicates the status of the data set. If the data set does not exist, **CASKS** lists the following options:

Press **Q** to QUIT and return to the Menu Press any other key to proceed with editing (creates a new data set)

If the data set already exists CASKS lists the following options:

Press **Q** to QUIT and return to the Menu Press **D** to delete current data set and create a new data set Press any other key to proceed with editing (edit the current data set)

Delete the data set to start with a fresh data set with all data set to default values. CASKS asks for confirmation before deleting the existing data set:

Press	<b>F1</b>	to delete the data set and create a new data set			
		(edit the new data set)			
Press	Q	to QUIT and return to th	e Menu		
Press	F2	to proceed with editing	(edit the current data set)		

CASKS reads a template which describes the editor pages and how data values are saved in the data set. If creating a new data set, CASKS displays a status screen which indicates each editor page as it is created. As pages are created, all values are set to appropriate defaults. CASKS then displays the first editor page.

#### **Description of Editor Pages**

Each data set is divided into pages of related items. For example, all the items necessary to define the cask shell are on the same editor page. All pages have the same format (Figure A-1). The top line indicates the name of the data set [A], the CASK ID [B], and the current date [C]. The second line indicates the name of the editor page [D], the current page number of how many [E], and the date any item on the page was last changed [F]. The third line is a double green bar the full width of the screen. This line also indicates how many pages remain which must be accessed [G] and Insert Mode (if applicable) [H]. Below the second double green bar is a list of available function keys and their application [I].

Between the double green bars are the item requests [J]. Each item request has a descriptive label indicating what to enter (units are included if appropriate) [K], and an item field delimited by square brackets [L]. Item descriptions displayed in *light blue* require an entry, while item descriptions displayed in *green* have default values which can be accepted as is. The count of pages remaining which must be accessed indicates pages which have items requiring an entry. Once entries are made on a page for ALL items requiring an entry, the page need not be accessed.

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ſ	ABasic Geometry Specifications D Cask Cavity/Contents Specifications G 7 Pages remain which must be accessed	B <sub>ID:9999</sub> E <sup>Page 3</sup> of 1	Foday is:10/20/8 12 Last chgd:10/20/ INSERT	BB F A S MODE
	Cavity inner radius (in.) Cavity length (in.)	[25.625 [192.5		
	K Gross weight of package (lbs) Weight of contents / internals (lbs)	[180000. [56065.	1	
	Maximum heat generation rate of contents (Btu/min)	[500.	1	
	Initial cavity charge pressure (psia) Initial cavity charge temperature (deg.F) Maximum normal operating pressure (psia)	[14.7 [70. [100.	] ] ]	J
	Temperature defining stress free condition (deg.F)	[70.	1	
	(Include the following to define 2-D finite-element mesh) (Mesh divisions must be even)			
	Number of mesh divisions along cavity inner radius Number of mesh divisions along cavity half length	[6 ] [10]		
I	F1 List Pages F2 Save+END F3 QUIT w/o Save F6 Redefault Current Field F7 Redefault Entire Pag	F4 Save+Continue	F5 Print Page Cape for HELP	

Figure A-1. CASKS Editor Page Layout

### Getting Help

Press the ESC key to display the *HELP* screens. The first screen indicates the current item type and restrictions placed on the item and describes the use of the function keys. The second *HELP* screen indicates the data entry and editing keys. The third *HELP* screen indicates the keys used to move between item fields and editor pages.

#### Saving the Edits

Save the changes made during the editing session using the following keys. The value in the current item field must be a valid item before **CASKS** will save the edits.

F2 (function key)

Save the data set as is, end the editing session and return to the current menu.

F4 (function key)

Save the data set as is and redisplay the current page to continue editing. Use this feature to save the edits periodically during a protracted editing session. CASKS will lose all edits not saved if a power failure interrupts the operation of the PC.

#### Ending the Edit Session

End the editing session by pressing one of the following function keys:

F2 (function key)

Save the data set as is, end the editing session, and return to the current menu.

F3 (function key)

Abandon all edits during this session (or since the previous save), end the editing session and return to the current menu. CASKS asks for confirmation before proceeding: press F1 to QUIT, abandoning the edits; or press F9 to return to editing.

#### **Moving Around**

The blinking solid cursor identifies the current item field expecting an entry. The entry in the item field is checked for validity when the cursor is moved from this field to another. The entry must be valid before **CASKS** will allow the cursor to leave the current item field. Use the following keys to accept the current entry and move to another item field:

**UP** Arrow (on the keypad)

Move to the previous item field on the current page. If the current item field is the FIRST on the page, move to the LAST item field.

DOWN Arrow (on the keypad) or ENTER

Move to the next item field on the current page. If the current item field is the LAST on the page, move to the FIRST item field.

- **PgUp** (on the keypad) Move to the FIRST item field on the previous page. If the current page is the FIRST editor page, move to the FIRST item field on the current page.
- PgDn (on the keypad)

Move to the FIRST item field on the next page. If the current page is the LAST editor page, move to the FIRST item field on the current page.

#### F1 (function key)

Display list of all pages in the data set. Use the keypad UP Arrow and **DOWN** Arrow keys to highlight the desired page, and then press F1 to move to the FIRST item field on the indicated page. The page list indicates which pages have items requiring an entry.

# Appendix A

The Editor

#### Entering a Value

Enter values by typing in the item field (typing in the first character position clears the field). Enter character string type items using letters, numeric digits and special character (\$,%,#, etc.). Enter integer number type items using the form **nnn**. The sign is optional; **n** is any numeric digit (0-9). Enter real number type items using either the form **nn.mmm** or **nn.mmmEjj** (scientific notation). The sign, decimal point and exponent are optional; **n**, **m**, and **j** are any numeric digit (0-9). Use the following keys to assist editing values in the item field.

#### LEFT Arrow (on the keypad)

Accept the character under the cursor and move the cursor to the left one character (can move as far left as the first character position).

**RIGHT Arrow** (on the keypad)

Accept the character under the cursor and move the cursor to the right one character (can move as far right as the last character position).

**DEL** (on the keypad)

Delete the character under the cursor and shift the remaining characters to the left.

#### BACKSPACE (above ENTER)

Delete the character to the left of the cursor and shift the remaining characters to the left.

INS (on the keypad)

Toggle insert mode on and off. When insert mode is on, **INSERT** appears in the upper right corner of the screen on the double green bar. All new characters are inserted at the cursor, shifting the remaining characters to the right. When insert modes is off, new characters are inserted at the cursor, and they write over previous characters.

F6 (function key)

Set the current item to the CASKS default (NOT the previous saved value).

F7 (function key)

Set all items on the current page to the CASKS defaults (NOT the previous saved values).

#### Making Selections From a List

Certain items are restricted to values presented in a list (Figure A-2). Use the following keys to change the selection indicated in the item field:

- N or n Move blinking highlight cursor to the NEXT list item.
- **P** or **p** Move blinking highlight cursor to the *PREVIOUS* list item.
- S or s Select the item indicated by the blinking highlight cursor.



Figure A-2. Select Item From a List

#### Copying Data From Another Editor Page

If the item requests displayed on the current editor page are the same as those on another editor page, press F10 to copy data from another page. CASKS displays a list of all pages that are appropriate for copying and indicates the current page. Use the UpArrow and DnArrow keys to indicate the page to copy from, and then press C to perform the copy. Press R to return without performing a copy.

#### Printing an Editor Page

Press the F5 function key to print a copy of the current page. Make sure the printer is online and ready before printing the page.

#### **Handling Errors**

If an entry is invalid for the specified item, CASKS displays an error message at the bottom of the screen and indicates any restrictions on the item. Press ENTER to clear the error message and return to editing.

NOTES:

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The material sets used in CASKS contain all the information required to perform Impact, Thermal, Thermal-Stress, and Pressure-Stress analyses. These materials marked "LOCKED" are material properties built into CASKS and cannot be modified. CASKS also provides the ability to let the user input and/or modify the material sets.

Impact analyses use dynamic Young's Modulus, Poisson's Ratio, and material density (used for component weight calculations). Thermal analyses use temperature dependent properties for thermal conductivity and specific heat capacity. Thermal stress analyses use temperature dependent properties for Young's Modulus, Poisson's Ratio and coefficient of thermal expansion. Pressure stress analyses use the thermal stress properties at 70 degrees F.

### Material

Cuth 1 Contraction

References

Structural and Water Jacket Materials	
Borated SS 304	5, 6, 7, 8
Carbon Steel	1, 2
Ductile cast iron	5, 6, 7, 8
Stainless Steel 304	1, 2, 8
Stainless Steel 310	5, 6, 7, 8
Stainless Steel 316	5, 6, 7, 8
Stainless Steel 347	5, 6, 7, 8
Copper (Water Jacket Only)	5, 6, 7, 8
Shielding Materials	
Lead	1, 2, 10
Impact Limiter Materials	
Polyfoam	9
Polyurethane	2
Balsa Cross-Grained	2
Redwood Cross-Grained	4
Neutron Shield Materials	
Air Convection	3
Water Convection	3

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**D** 1

## Structural and Water Jacket Materials

#### Borated/Stainless Steel 304 (1.1% Boron)

Set name: BSS304

Impact Young's Modulus:3.194E+07 psiImpact Poisson's ratio:0.2990Density:0.2900 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/lbm°F)	Young's Modulus (psi)	Poisson's Ratio	Coefficient of Thermal Expansion (in./in.°F)
	011050	1000			0.0705.00
-28.	.011250	.1200	3.2/3E+0/	.2990	9.070E-06
68.	.011400	.1230	3.194E+07	.2990	9.070E-06
212.	.012083	.1238	3.110E+07	.3060	9.070E-06
392.	.012083	.1275	2.997E+07	.3060	9.360E-06
572.	.013056	.1312	2.884E+07	.3060	9.580E-06
752.	.013889	.1350	2.693E+07	.3060	9.810E-06
1112.	.015278	.1425	2.535E+07	.3060	9.930E-06
1472.	.018056	.1500	2.535E+07	.3060	9.930E-06

#### Carbon Steel

Set name: CARBNSTL

Impact Young's Modulus:	2.800E+07 psi
Impact Poisson's ratio: 🕠	0.2900
Density:	0.2820 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/lbm°F)	Young's Modulus (psi)	Poisson's Ratio	of Thermal Expansion (in./in.°F)
-100.	.035000	.1130	2.900E+07	.2900	6.600E-06
68.	.034700	.1130	2.790E+07	.2900	6.639E-06
200.	.034700	.1130	2.770E+07	.2900	6.670E-06
300.	.034000	.1130	2.740E+07	.2900	6.870E-06
400.	.033300	.1130	2.700E+07	.2900	7.070E-06
500.	.032600	.1130	2.640E+07	.2900	7.250E-06
600.	.031500	.1130	2.570E+07	.2900	7.420E-06
700.	.029600	.1130	2.480E+07	.2900	7.590E-06

## Structural and Water Jacket Materials (continued)

Set name: DUCSTION **Ductile Cast Iron** 

> Impact Young's Modulus: 2.450E+07 psi Impact Poisson's ratio: 0.2900 0.2840 lb/cu.inch Density:

70031944 .1100 2.450E+07 .2900 6.	230E-06
390029860 .1100 2.450E+07 .2900 6.	780E-06
570027080 .1180 2.450E+07 .2900 7.	120E-06
750025280 .1210 2.450E+07 .2900 7.	.340E-06
930023610 .1230 2.450E+07 .2900 7.	510E-06
1110022920 .1280 2.450E+07 .2900 7.	620E-06
1290022640 .1440 2.450E+07 .2900 7.	.670E-06
1400021940 .1440 2.450E+07 .2900 8.	230E-06

### **Stainless Steel 304**

Set name: SS304

Impact Young's Modulus:	3.194E+07 psi
Impact Poisson's ratio:	0.2990
Density:	0.2900 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/lbm°F)	Young's Modulus (psi)	Poisson's Ratio	of Thermal Expansion (in./in.°F)
					\ <b>_</b>
-58.	.011250	.1200	3.273E+07	.2990	9.070E-06
68.	.011400	.1230	3.194E+07	.2990	9.070E-06
212.	.012083	.1238	3.110E+07	.3060	9.070E-06
392.	.012083	.1275	2.997E+07	.3060	9.360E-06
572.	.013056	.1312	2.884E+07	.3060	9.580E-06
752.	.013889	.1350	2.693E+07	.3060	9.810E-06
1112.	.015278	.1425	2.535E+07	.3060	9.930E-06
1472.	.018056	.1500	2.535E+07	.3060	9.930E-06

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### Structural and Water Jacket Materials (continued)

Stainless Steel 310 Set name: SS310

Impact Young's Modulus:2.820E+07 psiImpact Poisson's ratio:0.2900Density:0.2870 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/Ibm°F)	Young's Modulus • (psi)	Poisson's Ratio	of Thermal Expansion (in./in.°F)
		<u></u>			<del></del>
-50.	.010400	.0880	2.820E+07	.2900	7.576E-06
68.	.010600	.0880	2.820E+07	.2900	8.056E-06
300.	.012200	.0880	2.820E+07	.2900	9.001E-06
600.	.014800	.1055	2.820E+07	.2900	9.159E-06
900.	.017700	.1200	2.820E+07	.2900	9.175E-06
1200.	.021100	.1300	2.820E+07	.2900	9.230E-06
1600.	.025400	.1310	2.820E+07	.2900	9.531E-06
2000.	.025400	.1310	2.820E+07	.2900	9.889E-06

#### Stainless Steel 316

Set name: SS316

Impact Young's Modulus:	2.810E+07 psi
Impact Poisson's ratio:	0.2900
Density:	0.2870 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/lbm°F)	Young's Modulus (psi)	Poisson's Ratio	Coefficient of Thermal Expansion (in./in.°F)
		_ <u>~~~~~</u> ~~~~~~~			
-50.	.010100	.0980	2.810E+07	.2900	7.997E-06
68.	.010900	.1080	2.810E+07	.2900	8.321E-06
300.	.012600	.1170	2.810E+07	.2900	8.958E-06
600.	.015200	.1310	2.810E+07	.2900	9.605E-06
900.	.016700	.1360	2.810E+07	.2900	9.921E-06
1200.	.019200	.1400	2.810E+07	.2900	1.028E-05
1600.	.021600	.1550	2.810E+07	.2900	1.051E-05
2000.	.021600	.1620	2.810E+07	.2900	1.173E-05

## Structural and Water Jacket Materials (continued)

#### Stainless Steel 347 Set name: SS347

Impact Young's Modulus:2.820E+07 psiImpact Poisson's ratio:0.2900Density:0.2860 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/lbm°F)	Young's Modulus (psi)	Poisson's Ratio	Coefficient of Thermal Expansion (in./in.°F)
		- <u></u>		<u></u>	••••••••••••••••••••••••••••••••••••••
-50.	.011400	.0980	2.820E+07	.2900	8.502E-06
68.	.011900	.1080	2.820E+07	.2900	8.786E-06
300.	.012700	.1200	2.820E+07	.2900	9.345E-06
600.	.015100	.1310	2.820E+07	.2900	9.831E-06
900.	.016700	.1370	2.820E+07	.2900	1.019E-05
1200.	.018800	.1440	2.820E+07	.2900	1.044E-05
1600.	.020500	.1590	2.820E+07	.2900	1.086E-05
2000.	.020500	.1640	2.820E+07	.2900	1.229E-05

#### Copper

Set name: COPPER

(Water Jacket Only)

Density: 0.3240 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/Ibm°F)
<del></del>		
-100.	.331900	.0851
68.	.320800	.0917
260.	.313900	.0951
440.	.311100	.0974
620.	.306900	.0998
800.	.302800	.1020
1160.	.291700	.1067
1340.	.286100	.1091

## Shielding Materials

#### Cast Lead Set name: LEAD

Impact Young's Modulus:	2.775E+04 psi
Impact Poisson's ratio:	0.4200
Impact Yield Stress:	4.300E+03 psi
Impact Plastic Modulus:	2.400E+03 psi
Density:	0.4110 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/lbm°F)	Young's Modulus (psi)	Poisson's Ratio	Coefficient of Thermal Expansion (in./in.°F)
<u></u>		·		•	·····
-58.	.028888	.0300	2.000E+06	.4200	1.600E-05
68.	.028000	.0307	2.000E+06	.4200	1.600E-05
212.	.026800	.0315	2.000E+06	.4200	1.600E-05
392.	.025278	.0326	2.000E+06	.4200	1.600E-05
572.	.023889	.0337	2.000E+06	.4200	1.600E-05
630.	.016806	.0340	2.000E+06	.4200	1.600E-05
717.	.013472	.0339	2.000E+06	.4200	1.600E-05
1276.	.012028	.0337	2.000E+06	.4200	1.600E-05

## Impact Limiter Materials

### Polyfoam Set name: POLYFOAM

Density: 0.0116 lb/cu.inch

	Thermal	Specific	
Temp	Conductivity	Heat Capacity	
(°F)	(BTU/in.min°F)	nin°F) (BTU/lbm°F)	
<u> </u>			
-58.	.000278	.3000	
68.	.000278	.3000	
1300.	.000278	.3000	

## Impact Limiter Materials (continued)

#### Polyurethane Set name: PURETHAN

Density: 0.0021 lb/cu.inch

Temp	Thermal Conductivity	Specific Heat Capacity	
(°F)	(BTU/in.min <sup>o</sup> F)	(BTU/lbm°F)	
-58.	.000034	.4200	
68.	.000034	.4200	
1300.	.000034	.4200	

#### Balsa Cross-Grained Set name: BALSAXGR

Density: 0.0162 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/lbm°F)
		<u></u>
-58.	.000067	.5500
68.	.000067	.5500
1300.	.000067	.5500

#### Redwood Cross-Grained Set name: REDWDXGR

Density: 0.0150 lb/cu.inch

	Thermal	Specific
Temp	Conductivity (BTU/in min <sup>o</sup> F)	Heat Capacity (BTU/lbm°F)
-58.	.000088	.6900
68.	.000088	.6900
1300.	.000088	.6900

## Neutron Shield Materials

#### Air Convection Set name: AIRCONV

Density: 0.0000 lb/cu.inch

	Thermal	Specific	
Temp	Conductivity	Heat Capacity	
(°F)	(BTU/in.min°F)	(BTU/lbm°F)	
	<u> </u>	<u></u>	
	000100	2400	
-38.	.000139	.2400	
68.	.000139	.2401	
263.	.000139	.2421	
533.	.000139	.2482	
803.	.000139	.2568	
983.	.000139	.2621	
1253.	.000139	.2704	
1523.	.000139	.2770	

#### Water Convection

Set name: H2OCONV

Density: 0.0347 lb/cu.inch

Temp (°F)	Thermal Conductivity (BTU/in.min°F)	Specific Heat Capacity (BTU/Ibm°F)
-58.	.000182	.4100
68.	.001200	.9990
150.	.020500	1.0000
200.	.024100	1.0050
300.	.028900	1.0300
400.	.032400	1.0760
500.	.035500	1.1820
600.	.038500	1.3700

### Material References

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## Appendix C Sample Cask and Description of Output

#### **Description of Sample Cask**

This sample spent fuel storage cask is included in the CASKS release. The CASKID is 9999. The cask geometry includes a long cylindrical cask body, top and bottom end caps, and top and bottom impact limiters. The cask body has an inner shell layer of Stainless Steel 304, a Lead shielding layer, and an outer shell layer of Stainless Steel 304. Both end caps are solid Stainless Steel 304. The impact limiters overhang the cask body and are constructed of Polyfoam. This sample cask does not include a neutron shield and water jacket. Cask dimensions are shown in Figure C-1. Component weights, closure bolt information, and impact limiter force-deflection data are listed below:

Weights (in pounds)

Gross package:	180000
Contents/internals:	56065
Top impact limiter:	10000
Bottom impact limiter:	10000

Closure Bolts (for Top End Cap)

Number of bolts:	32	
Bolt diameter:	1.5	inches
Bolt circle radius:	29.5	inches

#### **Impact Limiter Force-Deflection Data**

NOTE: The following data is for Top and Bottom limiters for all impact angles.

Force (kips)
250.
1700.
4000.
6000.
10000.

## Appendix C Sample Cask and Description of Output



Figure C-1. Sample Cask Geometry and Dimensions

**C-2** 

# Appendix C

### Sample Cask and Description of Output

### Geometry Data Summary Output

This output is produced during the data check performed when the basic geometry is saved (Geometry Menu). It is a complete summary of all specifications for the cask. Warning and error messages appear when specified weights differ from calculated weights and when geometry dimensions are inconsistent. This output does not have any warning messages. The output format follows.

#### (1) Header

Indicates Geometry Data Summary, page number of how many, date and time the output was generated, and CASKS version number. The header shown in Figure C-2 is printed at the top of every page of output.

#### (2) Data Set Status

Indicates whether the Basic Geometry data set is *COMPLETE* (Figure C-2). The data set has items requiring an entry if the status indicates *INCOMPLETE*.

#### (3) General Information

Lists general SAR information, general cask and contents specifications, and cask component weights (Figure C-2). The general SAR information includes the SAR title, report information, additional information, licensee's address, and names of review team members.

#### (4) Component Specifications

Summary of geometry specifications for each cask component (Figure C-3).

#### (5) Closure Bolts

Lists the number of bolts, bolt diameter, and bolt circle radius (Figure C-4).

#### (6) Finite Element Mesh Grading

Lists the number of mesh divisions through each cask component (Figure C-4). The output also indicates the status and size of the meshes. The Finite Element meshes are used for 2-D Thermal and Stress analyses.

#### (7) Material Properties

Tables listing properties for each material (Figure C-4). The output also indicates the components using the material.

#### (8) Impact Model Description

Lists the geometry of the simplified Impact model (Figure C-5).
01		lo
	GEOMETRY DATA SUMMARY FOR CASK 9999 Page 1 of 8 GENERATED ON 11/16/88 AT 8:20:00 CASKS VERSION: 1a	lo
		1
01		10
01	Basic geometry data set is COMPLETE	lo
01		10
1	GENERAL SAR INFORMATION	1
Ĩ		1
0 l 1	SAR: Sample spent fuel storage cask (demonstration only)	10 1
01	Papart number: 123 Volume 1	lo 1
0	Report date: 4/15/91	lo
.!	Docket number: 9999	
° I	DOCKET STATE DATE: 4/15/91	1
01		lo
01		lo
l°	CASK GENERAL DIMENSIONS AND SPECIFICATIONS	I
01	Country inner radius 25.625 inchas	lo
01	Cavity length: 192.500 inches	io
	Cask hady outer radius, 22,750 instea	
	Cask body length: 207.500 inches	1
01	Ton impact limiter is included in model	lo 1
0	Bottom impact limiter is included in model	Io
1	Neutron shield is not included in model Water issket is not included in model	
ľ	Watti jarrer 15 nor illenden in model	I
01	Contents maximum heat generation rate: 500.00 Btu/minute	
1		1
01	Temperature defining stress free condition: 70. degrees F	lo I
01	Initial cavity charge pressure: 14.70 psia	lo
0	Initial cavity charge temperature: 70.00 degrees P Maximum normal operating pressure: 100.00 psia	lo
1		
	CASK WEIGHTS (By component)	1
01		io 1
0	Gross package: 180000. lbs	, Io
	Contents/internals: 56065. lbs Ten import limiter 2004 lbs (Colouleted)	
<b>P</b>	Bottom impact limiter: 8294. lbs (Calculated)	1
01	Cask shell / end caps: 103935. lbs Gross wt - (Contents+Limiters) lo	1
01	Bottom end cap: 7497. lbs	10
1	Shell: 92353. lbs	1
l° ¦		10

Figure C-2. Cask Geometry Summary Output -- General Information

							1
0							Io
	CASK SHELL DESCRI	PTION					l lo
01 1	Laver	Material Name	Thickness Inches	Inner Radius Inches	Outer Radius Inches	X-section Area Sq Inches	  0 
0	 Immor Shall		1.000				lo 1
0	Shield Outer Shell	LEAD SS304	3.875 2.250	26.625 30.500	30.500 32.750	695.421 47.088	lo I
01	То	tal Thickness	7.125		Total Area	lo 1306.657	l Io
01	Inner Shell a Outer Shell a	dditional thick additional thick	ness at end mess at end	cap interface: cap interface:	.000 inches .000 inches		l lo
01	Shield height	:	19	4.500 inches			l lo l
01							lo I
01	TOP END CAP DESCI	RIPTION					lo I
01							lo I
0	-	Material	Thickr	less			lo
01	Layer	Name	Inch	es 			lo
 0	End cap	SS304	7.50	00			l lo l
0	BOTTOM END CAP I	DESCRIPTION					lo
01		•					lo
01	Layer	Material Name	Thick: Inch	iess es			l lo l
01	Endcap	SS304	7.50	00			lo I
10	IMPACT LIMITERS						lo I Io
01	TOP Impact	Limiter					l Io
0	Material Radius:	: POLYFOAM	6	0.000 inches			lo
   0	Thickne Overhar	ss above end ig along cask i	cap: 30 body: 39	5.000 inches 9.000 inches			l lo
0	BOTTOM Im	pact Limiter					lo
01	Material Radius:	POLIFOAM	6	0.000 inches			lo
01	Thickne Overhar	ss above end ng along cask	cap: 3 body: 3	5.000 inches 9.000 inches			lo
01							lo
0	NEUTRON SHIELD						l lo
01	Neutron Shie	ld is NOT inc	luded in mod	lei			l lo
01	WATER JACKET						lo I
01	Water Jacket	is NOT inclu	ded in model				lo I Io
ľ'i							1

Figure C-3. Cask Geometry Summary Output -- Component Specifications

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		1
lo i		lo
Li.	CLOSURE BOLTS	1
loi		lo
ľi		1
lai.	Number of bolts: 32	10
ľ	Bolt diameter: 1 500	1
	Bolt circle radius: 29 500	lo l
l"i		1
		in
l"	EINITE EI EMENT MESH OPADING (Applies to 2-D Thermal and Stress calculations)	ĩ
	FIGHE ELEMENT WISH ORADING (Applies to 2-5 Thema and Suces calculations)	in
1° ;		ĩ
	Consister	in
l°¦	Number of mech divisions along inner radius:	i
	Number of mask divisions along county half length 10	in
l°:	Shall of mesh divisions along cavity han rengul.	
	Shell	
l°!	Number of mesh divisions through miler layer. 2	
	Number of mesh divisions though since layer.	
lo !	The Decision of the set of the se	
	Top End Cap	6
l°!	Parton End Con	. 10
	Down Elle Cap	10
101	Ton Impact Limiter	1
	Number of most divisions through contacting thickness:	1
	Number of mesh divisions through center-line throughs	~~
	Relief of limitar divisions divogit overhaig width.	
1.	Number of mesh divisions through center line thickness:	ĩ
	Number of mesh divisions through cuterbane width:	in
	Number of mesh divisions through overhang which.	ĩ
	Einite element methes were generated on 10.02-28 at 3:17n	10
ľ.	Time clonent meshes were generated on 10-02-00 at 5.17p	ĩ
	Thermal mech has 282 nodes and 245	4.
Inode	elemente io	
1	Stress mesh has 195 nodes and 41 9-node elements	1
		lo
ľ		i
	MATERIAL PROPERTIES	lo
ľ		i i
lai.		lo
ľ.	This model uses 3 different materials	1
la i		lo
ľ.	SS 304 (SS 304 )	i
lai.		Io
ľ.	. Lised in	1
	Social Million and Martin	10
ľ.	The end can	1
	Rottom end can	
1° i		i.
	Impact Young's Modulus: 2,830E+07 psi	Jo
ľ	Impact Poisson's ratio:2900	I.
loi		10
1 i	Density: .2841 lb/cu.inch	1
01	Coefficient	lo
1 i	Thermal Specific Young's Poisson's of Thermal	1
01	Temp Conductivity Heat Capacity Modulus	
Rati	Expansion lo	
1	F BTU/in min F BTU/lbm F psi in/in F	1
01	·····	lo
11	-58011250 .1200 2.910E+07 .2900 8.700E-06	1
01	68011400 .1230 2.840E+07 .2900 .000	lo
1	212012083 .1238 2.760E+07 .2900 8.700E-06	1
01		lo
1	·	1
01		lo
1 1		1



01							0
1!							1
01							10
1.1	IMPACT MODEL D	ESCRIPTION					I In
10 !		-					10
							1
l° ¦	Model morees	and shall at	iffnage Naluas				10
	NOUAI IIIASSES	and shell st	IIIIess values				1
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ľ	Number	inches	lb-sec**2/in	lb-sec**2-in	lbs	lb-in**2	ĩ
lai							Io
Fi	1 BOT	0.	74.	39578.			1
loi	2	48.	58.	24756.	1.730E+10	7.922E+12	lo
Γi	3	96.	58.	24756.	1.730E+10	7.922E+12	L
01	4	144.	58.	24756.	1.730E+10	7.922E+12	10
1	5 TOP	193.	74.	39578.			1
01							lo
1							ł
01	Shell areas an	d inertias fo	r nodes 2 through	. 4			lo
1							I
01			Area	Moment of Inertia			lo
11	Layer		in**2	in**4			1
01							10
	Inner Shell		164.15	56037.			- I -
0	Shield		695.42	284973.			0
Lł	Outer Shell		447.09	223858.			1
10!							10
4 1							1

Figure C-5. Cask Geometry Summary Output -- Impact Model Description

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#### Limiter Curve Summary Output

This output is produced during the data check performed when the impact limiter force/deflection data set is saved (Geometry Menu). It is a complete summary of all specifications for the cask. Error messages appear when impact limiter force-deflection curve definitions are incorrectly specified. The output format follows.

#### (1) Header

Indicates Limiter Curve Summary, page number of how many, date and time the output was generated, and CASKS version number. The header shown in Figure C-6 is printed at the top of every page of output.

#### (2) Data Set Status

Indicates whether the Limiter F/D data set is COMPLETE (Figure C-6). The data set has items requiring an entry if the status indicates INCOMPLETE.

#### (3) Impact Limiter Force/Deflection Curves

Lists the impact limiter force-deflection curve specifications (Figure C-6). The limiter curves are specified individually for each end of the cask and for various impact orientations.

10 01 Page 1 of 2 LIMITER CURVE SUMMARY FOR CASK 9999 1 1 CASKS VERSION: 1a GENERATED ON 11/16/88 AT 8:22:00 10 οl 1 lo 01 J. 1 lo 01 Limiter F/D data set is COMPLETE 1 1 io 01 1 - 1 lo 01 L 1 IMPACT LIMITER FORCE/DEFLECTION CURVES In 01 I. - 1 lo οl L 1 01 Bottom Limiter ío 1 1 Side Impact ( 0 degrees) 10 01 L 1 Slope Deflection Force 10 o 1 inches Kips Kips/inch 1 - 1 lo 01 ----------0 0 1 500.00 .500 250.00 lo οl 116.00 13.000 1700.00 1 26.500 4000.00 170.37 lo 01 571.43 30.000 6000.00 1 33.500 10000.00 1142.86 lo 01 1 10 . . . ٤ . . . lo 01 . . . 1



#### **Impact Analysis Output**

This sample Impact analysis is based on a 30-foot hypothetical accident drop on the cask bottom on an unyielding surface at an initial impact angle of 45 degrees. Primary and secondary impacts are included in the analysis, and the shield/shell interface is bonded (the lead shield is not allowed to slump). The discussion of the output format includes a detailed description of output for a Dynamic Analysis. Quasi-static output is in the same format. Differences in output for an unbonded lead shield analysis are also noted.

#### (1) Header

Indicates the type of analysis, page number of how many, date and time the output was generated, CASKS version number, and a brief description of the parameters defining the analysis case. The header shown in Figure C-7 is printed at the top of every page of output.

#### (2) Impact Summary

Lists the impact velocity, impact angle, CG (center-of-gravity) over corner angle, limiter crush, rigid body accelerations, maximum cask axial and shear forces, and maximum impact moment about the cask center line for both primary and secondary impacts (**Figure C-7**). For an unbonded lead shield analysis, **CASKS** lists the permanent lead slump. For secondary impacts, **CASKS** lists the secondary impact angle and the impact limiter data used (the force-deflection curve for the angle closest to the actual secondary impact angle).

#### (3) Maximum Force and Moment Results

Tables for maximum axial force, maximum shear force, and maximum bending moment are printed for each node location along the cask body and at the cask ends (Figure C-8). These forces and moments are beam-type values for the composite cross-section of the cask.

#### (4) Impact Stress Intensity Results

Tables for maximum stress intensity are printed for each shell layer at each node location along the cask body. Stress intensity is the absolute value of the maximum difference between the principal stresses. Principal stresses are calculated from axial, bending, shear, hoop, and radial stresses. For bonded shell/shield interface analyses the hoop stress is assumed to be zero. Axial and shear forces and bending moments are applied to the composite cross-section of the cask in order to calculate axial, bending, and shear stresses for each shell layer based on its individual stiffness. CASKS prints the stress intensity for the three maximum stress conditions listed below (Figure C-9).

A. Maximum Tension. Based on the maximum sum of the axial stress and bending stress at the extreme fiber. Shear stress is zero for this condition. This stress is the first principal stress. The second principal stress is the hoop stress.

# Appendix C

#### Sample Cask and Description of Output

- B. Maximum Compression. Based on the maximum difference of the axial stress and bending stress. Shear stress is zero for this condition. This stress is the first principal stress. The second principal stress is the hoop stress.
- C. Maximum Shear. Based on the axial stress, maximum shear stress, hoop stress and radial stress, occurring at the neutral axis. The principal stresses are calculated using Mohr's circle.

#### (5) Interface Force and Moment Results (unbonded lead shield analysis only)

Tables for edge moments and shear forces are printed for the inner and outer shell at the bottom end cap and top closure interfaces (Figure C-11). A positive moment results in compression in the outermost fiber of the shell, and a positive shear force is directed radially inward.

#### (6) End Cap Stresses

Lists the bending and shear stresses in the end caps (Figure C-10). The end caps are treated as circular plates with fixed boundary conditions for the bottom end cap and pinned boundary conditions for the top end cap. The inertial forces are evenly distributed across the end caps, and the impact limiters contribute no bending resistance. The shear stress is calculated as a maximum at the indicated radius.

#### (7) Top Closure Bolt Stresses

Indicates bolt axial and shear stresses (Figure C-12). Bolt axial stresses are calculated only when the bolts are in tension.

01						
1	DYNAMIC IMPACT OUTPUT FOR CASK 99	99	•		Page 1 of 7	1
01	GENERATED ON 4/15/91 AT 14:46:47				CASKS VERSION: 1a	lo
	SAR: Sample spent fuel storage cask (demo	nstrat	ion only)	•	I	14
	Angle of primary impact is 45 degrees - shi	ry ∝ ield/si	secondary imp hell interface i	act	t	10
01	ANALYSIS INCLUDES USER DEFINED MATER	IALS		000000	•	lo
<b>I</b> 1						I
0	IMPACT SI	IMI	MARY		•	lo
10						
						1
°¦	PRIMARY IMPACI (Cask Bottom)					10
01						Io
1	Impact Velocity	=	235.9	in/sec		ł
01	Impact Angle	=	45.0	degrees		lo
	CG Over Corner Angle	=	74.4	degrees		
ľí	Maximum Limiter Crush	=	11.3	inches		i
oi						·
lo						
1.!	Maximum Rigid Body Accelerations		0.4	-1-		1
°¦	Vertical Acceleration Horizontal Acceleration	=	9.4 _1.4	gs o's		10
oi	Rotational Acceleration	=	-45.0	rad/sec**2		lo
						I
0	Maximum Impact Forces		1000 0	1-t		lo
	Axiai Force in Cask Shear Force In Cask	=	-1009.3	kips		1
ľ.	Shoa Toroo hi Case	-	1115.0	кірэ		ĩ
01	Maximum Impact Moment (C.L.)	=	-21025.2	in-kips		lo
			•			1
10						
1	SECONDARY IMPACT (Cask Top)					L
0						lo
	Impact Velocity	=	406.8	in/sec		I In
ľi	Impact Angle	=	1.1	degrees		Ĩ
01	Limiter Angle Used	=	.0	degrees		lo
				• •		I
0	Maximum Limiter Crush	=	14.2	inches		10
6	Maximum Rigid Body Accelerations					Io
l i	Vertical Acceleration	=	9.9	g's		I
01	Horizontal Acceleration	=	2.2	g's		lo
	Rotational Acceleration	=	81.5	rad/sec**2		I
10	·					
Ĩ	Maximum Impact Forces					L
01	Axial Force In Cask	=	54.0	kips		lo
	Shear Force In Cask	=	-1905.1	kips		1
					•	
Ĩĭ	Maximum Impact Moment (C.L.)	=	12722.8	in-kips		L
01	•					lo
						1
° ¦	Run Time For Dynamic Analysis	=	358 6	seconds		10
0	The shirt of Synamic Fillingsis		220.0			i
0						
LE		_				1

Figure C-7. Dynamic Impact Output -- Header and Impact Summary

Version: 2a C-11

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	M A 	XIMUM FORCE	S AND MOMENT	r s Io	
NOTE: Node 1 i	is at Cavity BOTTO	OM, Node 5 is at Cav	ity TOP		
	ACT (on each both	(m)			
		0.11)			
Node Number	Axial Position	Max Axial Force	Max Shear Force	Max Moment	
(Location)	(Inches)	(Kips)	(Kips)	(In-Kips)	
			10	-	
Cask Bottom		-1009.3	1115.0	-21025.2	
1	.0	-842.5	558.8	23844.8	
2	48.1	-744.1	362.2	3844.0	
3	96.3	-554.5	71.9	11273.1	
4	144.4	-344.5	-91.7	7639.5	
5	192.5	-262.3	-126.5	2689.8	
Cask Top		.0	.0	.0	
SECONDARY I	MPACT (on cask	top)			
				N/ N/	
Node Number	Axial Position	Max Axial Force	Max Shear Force	Max Moment	
(Location)	(Inches)	(Kips)	(Kips)	(in-Kips)	
Cask Bottom		.0	.0	.0.	
1	.0	83.0	449.6	4427.8	
2	48.1	96.7	409.4	26849.6	
3	96.3	116.6	199.5	45819.1	
4	144.4	100.0	-396.6	44832.3	
5	192.5	-96.3	-740.0	10186.2	
Cask Top		-54.0	-1905.1	12722.8	

Figure C-8. Dynamic Impact Output -- Maximum Forces and Moments

						1
1			STRESS INTENS	SITY		10 
0					lo	
0	NOTE: SI is bas	ed on maximum con	nbined axial & bending	stress		lo
I	or maxin	num shear stress	Ŭ			1
0	NOTE: Node 1 is		Nodo E is a Casim T	<b>O</b> D		lo
י הו	NOTE: Node 1 is	at Cavity BOTTOM	, Node 5 is at Cavity I	OP		1
Ĭ						ĩ
o	PRIMARY IMPA	CT (on cask bottom)				lo
ן 1 ה	********		SUD	ESS INTENSITY BASED	ON	
ĩ	Node Number	Axial Position	Max (P/A+Mc/I)	Max (P/A-Mc/I)	Max Shear	10
0	(Location)	(Inches)	(psi)	(psi)	(psi)	lo
1				****		1
9 I 1	1	.0	1673.	4405	4275	10
, i c	2	48.1	1237	1757	2885	10
1	3	96.3	733.	2294.	903.	10
o İ	4	144.4	601.	1537.	829.	Io
ī	5	192.5	438.	708.	1000.	1
ьİ	Outer Shell					lo
1	1	.0	1859.	4588.	4275.	I
51	2	48.1	1232.	1785.	2885.	lo
1	3	96.3	818.	2381.	903.	Í
51	4	144.4	657.	1596.	829.	lo
1	5	192.5	438.	728.	1000.	L
1						lo
1						
1	SECONDARY IN	PACT (on cask top)			•	10
i		······				lo
1		_	STR	ESS INTENSITY BASED	ON	E
1	Node Number	Axial Position	Max (P/A+Mc/I)	Max (P/A-Mc/I)	Max Shear	lo
1	(Location)	(Inches)	(psi)	(psi)	(psi)	1
	Inner Shell					lo
5 İ	1	.0	611.	525	3232	10
ï	2	48.1	3428.	3341.	2943.	1
۰ ۱	3	96.3	5803.	5818.	1441.	lo
Ì	4	144.4	5646.	5771.	2851.	1
51	5	192.5	1286.	1404.	5320.	10
1	Outer Shell					t
51	1	.0	646.	559.	3232.	lo
l	2	48.1	3638.	3551.	2943.	L
51	3	96.3	6162.	6174.	1441.	lo
I	4	144.4	5994.	6122.	2851.	l
1 0	5	192.5	1362.	1484.	5320.	lo
1						I
D [						lo

Figure C-9. Dynamic Impact Output -- Stress Intensity

Т			
0   	END CAP STRESSES		lo I
0			lo I
، ۱ د	NOTE: Limiters contribute no bending stiffness to the end caps Inertial forces are evenly distributed across the end caps		lo l
o I i	All stresses are in PSI		10
0   	PRIMARY IMPACT (on cask bottom)		10 
0   			lo I
0	BOTTOM END CAP (based on inertia of end cap and contents)		io I
01	Solid End Cap		lo 1
0 I	Maximum Bending Stresses		lo 1
0   	At center of end cap     2228.4       At edge near inner shell     -3454.8		lo I Io
0	Average Shear Stresses 674.1		I lo
0	At radius = 25.6 inches		I I
0	I TOP END CAP (based on inertia of end cap)		I I
0	I I Solid End Cap		I
٥	Maximum Bending Stresses		10
٥	At center of end cap 312.8		lo I
0	Average Shear Stresses     37.1       At radius = 25.6 inches		lo 1 lo
°			l lo
°	i SECONDARY IMPACT (on cask top)	la	1
°	1	10	1
°	BOTTOM END CAP (based on inertia of end cap)		10
٥	Solid End Cap		10 1
0			10 1
0	At center of end cap 43.2		lo
	At edge near inner shell -67.0		lo
ľ	Average Shear Stresses 13.1 At radius = 25.6 inches		l lo
ľ			l lo
ľ	TOP END CAP (based on inertia of end cap and contents)	lo	1
°	Solid End Cap	10	1
٥	Maximum Bending Stresses		1
0	At center of end cap -6756.8		lo I
0	Average Shear Stresses 696.2		lo 1
0	AL radius = 27.5  menes		lo

Figure C-10. Dynamic Impact Output -- End Cap Stresses

<u> </u>		1
0		lo
11	MAXIMUM CASK SHELL / END CAP	I
01		lo
	INTERFACE FORCES AND MOMENTS	I
01	lo	
		1
01	A positive moment results in compression in the outermost fiber of shell.	
l i	A positive shear force is directed radially inward.	
lo i		
F i		
	Edge moment of inner shell at bottom and can $-$ 4.057 in kinetin	1
	Edge moment of milet shell at bottom end eag $= -4.57$ m-kips/m.	10
	Edge moment of other shell at bottom end cap $=$ 14.500 in-kips/in.	1
0		lo
	Edge shear of inner shell at bottom end cap $= -2.521$ kips/in.	1
0	Edge shear of outer shell at bottom end cap $= 4.500$ kips/in.	lo
E E		1
01		io
	Edge moment of inner shell at top closure =993 in-kips/in.	I I
01	Edge moment of outer shell at top closure = 3.326 in-kips/in.	lo
1		1
01	Edge shear of inner shell at top closure =466 kips/in.	lo
L i	Edge shear of outer shell at top closure $= .917$ kinsin	1
loi		in in
ľ.		

Figure C-11. Dynamic Impact Output -- Interface Forces and Moments Note: Results based on unbonded shell/shield interface for primary impact only

   	TOP CLOSU:	RE BOLT STRESS	ES .	i Io I
01			lo	1
0				10
1	Bolt Shear Stress (psi)	PRIMARY IMPACT	SECONDARY IMPACT	1
0			lo	
				ł
01	Applied to ALL bolts equally	2238.	13086.	lo
				1
Ĩ	Bolt Axial Tensile Stress (psi)	PRIMARY IMPACT	SECONDARY IMPACT	1
01			lo	•
1				I
0	Case 1: Applied to ALL bolts equally	0.	17079.	lo
i	Case 2: Maximum stress based on bolt	0.	226.87	1
01	position relative to impacting		220107	lo
1	edge of the cask			I
01				lo
	NOTE 1 Anist load is due to make of the sec			1
01	NOIE: 1. AXIAI load is due to mass of the con	ntents and top end cap		10
0	3. Case 2 is best case when impact and	le is less than C.G. angle	lo	1
I	b) and b is see end when where	10 10 1000 anal 0.01	10	Т
01				lo

Figure C-12. Dynamic Impact Output -- Closure Bolt Stresses

Version: 2a C-15

#### Thermal Analysis Output

This Thermal analysis is based on the thermal case Normal Hot, Contents Heat, Solar Effects. The ambient temperature is 100°F, contents heat load is 500 Btu/min, and solar effects are included. The Thermal Analysis output format is typical for a Finite Element analysis program and is described below.

لشصب

#### (1) Header

Indicates the type of analysis, page number of how many, date and time the output was generated, CASKS version number, and a brief description of the parameters defining the analysis case. The header shown in Figure C-13 is printed at the top of every page of output.

#### (2) Control Data

Lists the parameters controlling the analysis. Typical control parameters are: number of materials, nodes, and elements; type of geometry; number and type of boundary and initial conditions; and non-linear solution convergence controls. A partial summary of control parameters is shown in Figure C-13.

#### (3) Summary of Nodal Data

Table of nodes for the Finite Element mesh, indicating the coordinates. The mesh is an axisymmetric representation of the TOP end of the cask. A partial summary of node data is shown in Figure C-14.

#### (4) Summary of Element Data

Table of elements for the Finite Element mesh, indicating the nodes which define the element, material number, and element volume. A partial summary of element data is shown in Figure C-14.

#### (5) Summary of Material Data

Table for each material used in the analysis, indicating the material name, cask component, material number for reference by element data, and material properties. A summary of Material 1 is shown in Figure C-14.

#### (6) Summary of Temperature Initial Conditions

Table of initial temperatures applied to nodes. A partial summary of initial temperatures is shown in Figure C-15.

#### (7) Summary of Flux Boundary Conditions

Table of flux boundary conditions applied to boundary segments. Each segment is defined by two nodes. Flux boundary conditions are applied to (1) the cavity surface to represent the contents heat and (2) the outer surface to represent solar effects. A partial summary of flux boundary conditions is shown in Figure C-15.

#### (8) Summary of Convection Boundary Conditions

Table of convection boundary conditions applied to boundary segments. Each segment is defined by two nodes. Convection boundary conditions are applied to the outer surface to transfer heat between the cask and the ambient environment. A partial summary of convection boundary conditions is shown in Figure C-15.

#### (9) Summary of Radiation Boundary Conditions

Table of radiation boundary conditions applied to boundary segments. Each segment is defined by two nodes. Radiation boundary conditions are applied to the outer surface to transfer heat between the cask and the ambient environment. Radiation boundary conditions are also used to represent fire conditions. A partial summary of radiation boundary conditions is shown in Figure C-15.

#### (10) Bandwidth Minimization Information

Summary of results of bandwidth minimization, used internally for improved calculational speed.

#### (11) Summary of Output

Table of nodal temperatures, indicating the location and magnitude of the minimum and maximum temperatures and the cavity pressure and temperature. The cavity temperature is the average cavity surface temperature. The cavity pressure is calculated using the ideal gas law. **CASKS** also prints the energy transferred across each boundary condition segment, permitting an energy balance check. For the transient Fire Accident case, temperature and energy results are printed for each time specified by the printing interval. A partial summary of temperature and energy results are shown in **Figure C-16**.

#### (12) Termination Message

Indicates the total clock time in seconds for the analysis and indicates the status of the analysis (Figure C-16). *Normal Termination* indicates the analysis was completed. *Error Termination* indicates the analysis was either terminated early by the user or because of an internal error condition (e.g., unable to extract values from function curves). When the analysis ends with an error termination, the resulting output can be printed but cannot be plotted.

н l lo οi THERMAL OUTPUT FOR CASK 9999 Page 1 of 34 L 1 CASKS VERSION: 1a GENERATED ON 11/16/88 AT 8:50:00 οl lo SAR: Sample spent fuel shipping cask (demonstration only) 1 1 THERMAL CASE: Normal hot Contents heat Solar effects lo ٥l 500.00 BTU/MIN 1 Maximum contents heat generation: L οI lo L 1 0 | using the TOPAZ version compiled -8/23/88 lo Т reference - Gary L. Johnson ph: 415-422-9323 o l lo I. o 1 lo \*\*\*\*\*\* \*\*\*\*\*\* \*\*\*\*\*\* \*\*\*\* \*\*\*\*\*\* 10 01 т lo 0 L 1 01 ĺο L lo 01 1 lo 0 [ 1 0 | lo SUMMARY OF INPUT 1 1 0 lo \*\*\* control data\*\*\* L o 1 lo t 0 lo number of materials 9 £ lo 01 number of nodes = 282 Т lo 0 number of elements = 245 Ł - 1 lo 01 temperature units 3 L - 1 = eq.1: dimensionless 01 lo eq.2: centigrade 1 eq.3: Fahrenheit 01 lo eq.4: kelvin 1 eq.5: rankine lo οl t -1 type of geometry 1 ío 0 | eq.1: axisymmetric 1 1 o i eq.2: plane lo Ł bandwidth minimization 01 1 lo eq.0: no minimization Т eq.1: minimization 01 lo eq.2: minimization - nodal destination L vector read from input file lo i lo ł - 1 lo 0

Figure C-13. Thermal Output -- Header and Control Data

									I.
ľ	· ·			***	nodal	d a t a ***			lo I
0									lo
0	node nu	mber	x1-coord	inate	x2-co	ordinate	temperatu	re (deg. f)	lo
	1		.00000		96	5.250	00	000	I Io
	2		4.2708		96	5.250	.00	000	i
	3		8.5417 12.813		96 96	5.250 5.250	.00	000	lo
0	5		17.083		96	5.250	.00	000	lo
0	6		21.354		96	5.250	.00	000	l : lo :
				•••					1
ľi				•••	•				10
01				*** e	lement	data ***			lo I
0									lo I
0	elem. no.	i	j	k	1	matl. no.	matl. angle	volume	lo
	1	17	49	56	56	1	.00000	877.24	l lo
1	2	49	50	57	56	1	.00000	894.19	I
0	3	16	56	63	15	1	.00000	877.24	lo
۱.¦	4	20 15	57 63	64 70	63 14	1	.00000	894.19	
ľi	.5	63	64	71	70	1	00000	94.19	10
01	Ŭ	05	04		70	*		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	lo
				•••					1
0				••	•				lo
0									l lo
				***	materi	al data*	***		i In
ľ									I
0	SS 304	Used	in the INNE	R SHELL			•		lo I
0 [							_		lo
0	m	aterial numbe	ſ			-	1		l lo
	m	aterial type				=	3		1
ľi	de	nsity				=	28414		10
01	th	ermal generat	ion rate c	urve nun	ıber	=	0		lo 1
0	th	ermal generat	ion rate m	ultiplier		= .(	00000		lo I
01	m	aterial angle		-		= .(	00000		lo I
01		tem	perature		CV	Ŀ	1		lo
01		com							lo
		-:	58.00 58.00		.1200	1.125	0E-02 0F-02		10
Ľi		21	2.0		.1238	1.208	33E-02		1
01		39	2.0		.1275	1.208	33E-02		lo
		57	2.0		.1312	1.305	6E-02		1
0		75	2.0		1425	1.388	9E-02		lo
6		147	2.		.1425	. 1.805	6E-02		10
l i						1.000			ĩ
01					,				ło



17.7

Version: 2a C-19

 0									1
1			*** t e m p	erature ini	tial cond	ditions*	**	l	1
1	tempera	ature units =	= (deg. f)						i
	node	temp	nod	e temp	node	temp	nc	ode temp	, I
	1	100.0	72	100.0	143	100.0	2	14 100.0	i
01	2	100.0	73	100.0	144	100.0	2	15 100.	0 1
	3	100.0	74	100.0	145	100.0	2		ו ט
01	4	100.0	15	100.0	140	100.0	2	18 100.	י מ
lo i	5	100.0	,,,		14.	100.0	-		Ĭ
1				•••					I
01				•••					
									1
1			*** f	lux bounda	ry condi	tion ***			1
01		node i	node i	curve no.	i-m	ultiplier	j-multi	plier	
01							,	•	
1		1	2	0	-1.4	2371E-02	-1.423	71E-02	
0		2	3	0	-1.4	2371E-02	-1.423	71E-02	
01		3	4	0	-1.42	23715-02	-1.423	71E-02	
1		5	6	0	-1.4	2371E-02	-1.423	71E-02	
01		-	-						
I				•••					
01				• • •					
01									
0			*** con \	vection bou	ndary co	ndition	***		
Ĵ	node	node	h	h	free conv	t	temp i	temp j	
0  	i	j	curve	multiplier	exponent	curve	multiplier	multiplier	
٥İ	196	197	0	2.1990E-05	.3333	0	100.0	100.0	
1	197	198	0	2.1990E-05	.3333	0	100.0	100.0	
01	198	199	0	2.1990E-05	.3333	0	100.0	100.0	
0	200	200	0	2.1990E-05	.3333	0	100.0	100.0	
1	200	201	v			v	200.0	100.0	
01				•••			•		
1				•••					
0									
0			*** ra	diation bou	ndary co	ndition	***		
0	node	node	f	f	temp	lemp	i	temp i	
i	i	j	curve #	multiplier	curve #	multip	lier	multiplier	
01		•					·		
1	196	197	0	1.001E-13	0	100	).	100.	
0	197	198	0	1.001E-13	0	100	). )	100.	
0	198	200	0	1.001E-13	0	100	).	100.	
Ĩ	200	201	õ	1.001E-13	õ	100	).	100.	
01			-	•••	-				
1									
01				•••					
01									



<u> </u>	and the state of the state of the state of the state of the state of the state of the state of the state of the					
0						l lo
01	SUMMARY OF OUTP	UT				10
0	Steauy State Solution	100 0 5				lo
0	Minimum temperature Maximum temperature	= 157.7 F = 348.6 F	at node at node	228 1		lo
0	Cavity pressure	= 20.1 psia				l lo
01	Cavity temperature	= 265.1 deg F				l lo
 	node temperature	node	temperature	node	temperature	l lo
0	1 348.6 2 347.8	95 96	264.1 263.3	189 190	322.2 321.6	l lo
0	3 345.9	97	261.1	191	320.6	l lo
						1
	internal energy is 0. at the init	ial state	outward not	mat vector		
	positivo non non lo in oncon	franc	for rote	heat transfe	Total heat	1
	tume sea # are	this	step	this step	transferred	
	type seg # alea		rgy/umej	[energy/sic	pj [energy]	10
	Ilux I 57.50		1582			10
	a					lo
01	flux TOTAL	-85	)8.03			lo I
10	conv 1 57.30	.3	4631			lo I
01		••				lo I
01	conv TOTAL		50.13			lo I
0   						lo I
0   	rad 1 57.30	3.3 	2472			lo I
0   		····				10 1
o    0	rad TOTAL			44	.0.96	
 	heat	t gen. total	heat	change in	internal	l lo
 0	this mat # [en:	step gene ergy] [ene	ration rey]	int. energy [energy]	energy [energy]	l lo
1	1	.0	0000		[8]]	I I
1						I Io
0	TOTAL					l Io
0	execution ended on 10/02/8	8 at 15:19:20				l Io
0	execution time = 1	04 sec				i I
1	*** normal termination ***					I Io
Ì						1

Figure C-16. Thermal Output -- Temperature Output and Energy Balance

#### Thermal and Pressure Stress Analysis Output

Thermal Stress and Pressure Stress analyses have the same output format. The sample output shown in Figures C-17, C-18, and C-19 is for a Thermal Stress analysis. The analysis is based on the thermal case Normal Hot, Contents Heat, Solar Effects. The ambient temperature is 100°F, contents heat load is 500 Btu/min, solar effects are included, and the stress free temperature is 70°F. The output format is as follows:

#### (1) Header

Indicates the type of analysis, page number of how many, date and time the output was generated, CASKS version number, and a brief description of the parameters defining the analysis case. The header shown in Figure C-17 is printed at the top of every page of output.

#### (2) Nodal Results

Table of coordinates and displacements for each node in the Finite Element mesh. The mesh is an axisymmetric representation of the TOP end of the cask. The results for the first ten nodes are shown in Figure C-17.

#### (3) Element Stress results

Table of stresses for each element in the mesh. Stresses are calculated at element integration points. These stress are extrapolated to the nodes which define the element and printed in the output. Stresses are not calculated for nodes which lie on the axis of symmetry. The stresses for the first two elements are shown in Figure C-18. The stress components are defined as follows:

Srr	Radial stress
Szz	Axial Stress
Stt	Hoop Stress
Srz	Shear stress in the axial cutting plane
S(MAX)	Maximum Principal Stress
S(MIN)	Minimum Principal Stress
ANGLE	Orientation of the principal stresses

#### (4) Summary of Output

Table of maximum and minimum stresses (radial, axial, hoop, shear), indicating the elements where they occur; table of stresses at locations corresponding to Impact model node locations. Stresses are printed for the outer radius of each shell layer along the cask body. Stresses are interpolated to the Impact node locations when necessary. The stresses at the outer radius of the Shell Inner Layer corresponding to Impact node locations are shown in **Figure C-19**.

o       I       STRESS OUTPUT FOR CASK 9999         o       I       GENERATED ON 11/16/88 AT 8:55:00       C         I       TITLE: Sample spent fuel shipping cask (demonstration only)       C         o       I       THERMAL CASE: Normal hot Contents heat Solar effects       Maximum contents heat generation: 500.00 BTU/MIN         o       I       Stress Free Temp= 70. Thermal State 2 at Time S.S.						Page 1 of 19 CASKS VERSION: 1a I	  0  0  0  1  0
6	NODAL RES	SULTS					io
[ i							ĩ
01							lo
1	NODE	COOL	RDINATES	DISPLAC	EMENTS		ł
01	NUMBER	х	Y	DX	DY		lo
							1
01	1	.000	96.250	.000000	.173338		lo
1	2	4.271	96.250	.009740	.173180		1
01	3	8.542	96.250	.019431	.172724		lo
1	. 4	12.813	96.250	.029021	.171950		1
01	5	17.083	96.250	.038461	.170854		lo
F	6	21.354	96.250	.047802	.169543		1
01	7	25.625	96.250	.056273	.168131		lo
1	8	25.625	88.375	.046712	.148118		1
01	9	25.625	80.500	.046414	.130258		lo
	10	25.625	72.625	.044109	.114609		1
01							lo
							1

Figure C-17. Thermal Stress Output -- Header and Nodal Results

										1
10!										lo
	ELEMEN	IT STRESS	RESULTS							1
10!	Y						3			10
	integrati	on point	suesses a	re extrapol	ated to the	element no	aes			1
	Flore	Mada	S	Saa	<b>C</b> ++	S	004430	COMPANY	ANCT	10
	Numb	Numb	511	322	ou	512	S(MAA)	S(MIN)	ANGLE	1
	Numo	Numb	psi	psi	psi	psi	psi	SI I	eg.	10
0	1-	17	-3.	1447.	-3151.	15.	1448.	-3.	89.40	lo
1		49	-59.	1612.	-2906.	11.	1612.	-59.	89.62	1
01		50	-113.	1771.	-2670.	7.	1771.	-113.	89.78	lo
1		16	3.	1547.	-3153.	-10.	547.	3.	-89.64	L
01		56	-51.	1709.	-2908.	-14.	1709.	-51.	-89.54	lo
1		57	-103.	1864.	-2672.	-18.	1864.	-104.	-89.46	1
01		15	10.	1647.	-3155.	-35.	1647.	9.	-88.78	lo
1		63	-43.	1805.	-2910.	-40.	1806.	-44.	-88.78	1
01		64	-93.	1957.	-2674.	-44.	1958.	-94.	-88.77	lo
	2 -		*****					1		
01		15	-21.	1591.	-3174.	13.	1591.	-21.	89.54	lo
		63	-85.	1725.	-2940.	-1.	725.	-85.	-89.95	1
01		64	-147.	1854.	-2714.	-15.	1854.	-147.	-89.56	lo
		14	-24.	1891.	-3164.	-54.	1892.	-25.	-88.40	1
01		70	-69.	2008.	-2929.	-69.	2010.	-71.	-88.11	lo
11		71	-113.	2121.	-2702.	-83.	2124.	-116.	-87.87	1
01		13	-26.	2191.	-3154.	-120.	2197.	-32.	-86.91	lo
		77	-53.	2291.	-2918.	-136.	2299.	-61.	-86.69	1
01		78	-79.	2387.	-2690.	-151.	2396.	-88.	-86.51	lo
1										1
01										lo

Figure C-18. Thermal Stress Output -- Typical Element Stresses

2.3

Version: 2a

C-23

Т lo 01 SUMMARY OF OUTPUT E 01 I٥ I. 01 Elements with minimum and maximum stress values lo 1 0 | Srr minimum of -12843. psi occurs in element 14 at node 122 lo 45558. 26 at node 124 maximum of psi occurs in element 1 1 οl lo Szz minimum of -14372. psi occurs in element 14 at node 120 I. 124 0 maximum of 24511. psi occurs in element 26 at node 10 οl Stt minimum of -15114. psi occurs in element 14 at node 120 10 1 maximum of 24232. psi occurs in element 26 at node 124 Т οI lo -24557. 124 psi 26 at node Srz minimum of occurs in element 1 01 maximum of 21143. psi occurs in element 25 at node 120 lo Т ٥l lo t Stresses along Cask body at radius of each SHELL layer 01 10 Stresses are interpolated to IMPACT node positions position is .0 inches οI Cask bottom end: Impact node is 1, lo 192.5 inches 1 Cask top end: Impact node is 5, position is t 01 lo . SHELL INNER LAYER outer radius= 26.625 inches 0 lo Ł οl Impact In Model Pos. Srr Szz Stt Srz S(MAX) S(MIN) ANGLE L 1 psi psi psi deg. 01 Node inch psi psi psi 10 - 1 ---------------------\_\_\_\_\_ --------------1 o l 1 .0 -3536. 12020. 1683. 6011. 14072. -5588. 71.15 lo -2710. 7.9 -2024. 4505. 4765. 1329. -2284. 78.93 1 1 ٥l 15.8 461. 452. -5228 458. 914. -1. 44.71 lo 1 23.6 665. 2989. -3111. 2531. 4612. -957. 57.33 1 79.77 01 31.5 -20. 2057. -2896. 388. 2127. -90. lo 42.3 -65. 2159. -2816. 2159. 89.69 12. -65. Т 48.1 2 -103. 2251. -2754. -89.42 -24. 2251. -104. 01 10 1 53.1 -136. 2328. -2701. -55. 2329. -137. -88.73 1 63.9 2121. -2702. 2124. o I -113. -83. -116. -87.87 10 74.7 -120. -30. 1906. 1 1906. -2694. -120. -89.16 Т ٥l 85.5 -103. 1864. -2672. -18. 1864 -104. -89.46 lo 3 96.3 1771. -2670. 7. 1771. 89.78 -113. -113. 1 1 107.0 01 -103. 1864. -2672. -18. 1864. -104. -89.46 lo -120. 1906. -2694. 1906. 117.8 -30. -120. -89.16 1 1 128.6 -2702. -83. οl -113. 2121. 2124. -116. -87.87 10 139.4 -136. 2328. -2701. -55. 2329. -137. -88.73 1 4 144.4 -103. 2251. -2754. -24. 2251. -89.42 -104. 01 lo 1 150.2 -65. 2159. -2816. 12. 2159. -65. 89.69 1 -20. 2057. -2896. 2127. 79.77 οl 161.0 388. -90. lo 2989. -3111. -957. 1 168.9 665. 2531. 4612. 57.33 1 οl 176.8 461. 452. -5228. 458. 914. 44.71 -1. lo -2024. 4505. -2710. 4765. -2284. 78.93 184.6 1329. J 1 οI 5 192.5 -3536. 12020. 1683. 6011. 14072. -5588. 71.15 lo 1 1 0 10

Figure C-19. Thermal Stress Output -- Summary of Stresses

# Appendix D

#### Thermal Analysis Boundary Conditions

CASKS uses heat flux, convection, and radiation boundary conditions to define the thermal analysis conditions. Following is a list of the boundary condition values used for each CASKS thermal analysis.

NOTE: Refer to Volume 4, SCANS Thermal Analysis Theory Manual for a more complete description of the following terms and equations.

> Convection Equation:  $\dot{q}'' = h (T - T_{\infty})^a (T - T_{\infty})$ Where: **q**" = Surface heat flux due to convection h = Convection coefficient= Free convection exponent а = Surface temperature T  $T_{m}$  = Convection flow temperature Radiation Equation:  $\hat{q}'' = f(T + T_{\infty}) (T^2 + T_{\infty}^2) (T - T_{\infty})$  $f = \sigma F$ and Where: • q" = Surface heat flux due to radiation

σ = Stefan-Boltzmann constant

F = characteristic exchange factor (includes effects of geometry, emissivity and reflectivity)

T = Surface temperature

= Radiation source temperature

#### Cold Soak, Contents Heat, No Solar Effects

All boundary conditions are constant

```
Heat Flux
         Cavity: Contents heat as specified in the geometry definition
         Outer Surfaces (solar): None
Convection
         Flat surfaces
              h = .00002199 \text{ Btu} / \text{in.}^2 \text{min} \,^\circ \text{F}
               a
                    = .3333
              T_{m} = -40 \,^{\circ}F
         Cylindrical surfaces
                   = .00002083 Btu / in.<sup>2</sup> min °F
              h
                    = .3333
               a
              T_{m} = -40 \,^{\circ}F
Radiation
                    = 1.001E-13 Btu / in.<sup>2</sup> min °F<sup>4</sup>
                    = -40 \,^{\circ}\mathrm{F}
```

# Appendix D Thermal Analysis Boundary Conditions

Cold Soak, No Contents, No Solar Effects

Ĩ.• •

All boundary conditions are constant

```
Heat Flux

Cavity: None

Outer Surfaces (solar): None

Convection

Flat surfaces

h = .00002199 Btu / in.<sup>2</sup> min °F

a = .3333

T_{\infty} = .40 °F

Cylindrical surfaces

h = .00002083 Btu / in.<sup>2</sup> min °F

a = .3333

T_{\infty} = .40 °F

Radiation

f = 1.001E-13 Btu / in.<sup>2</sup> min °F<sup>4</sup>

T_{\infty} = .40 °F
```

#### Normal Cold, Contents Heat, No Solar Effects

All boundary conditions are constant

```
Heat Flux

Cavity: Contents heat as specified in the geometry definition

Outer Surfaces (solar): None

Convection

Flat surfaces

h = .00002199 \text{ Btu / in.}^2 \min {}^\circ\text{F}

a = .3333

T_{\infty} = .20 \, {}^\circ\text{F}

Cylindrical surfaces

h = .00002083 \text{ Btu / in.}^2 \min {}^\circ\text{F}

a = .3333

T_{\infty} = .20 \, {}^\circ\text{F}

Radiation

f = 1.001\text{E-}13 \text{ Btu / in.}^2 \min {}^\circ\text{F}^4

T_{\infty} = .20 \, {}^\circ\text{F}
```

# Appendix D

Thermal Analysis Boundary Conditions

#### Normal Cold, No Contents, No Solar Effects

All boundary conditions are constant

Heat Flux Cavity: None Outer Surfaces (solar): None Convection Flat surfaces  $h = .00002199 \text{ Btu / in.}^2 \min {}^\circ F$ a = .3333  $T_{-} = -20 \,^{\circ}F$ Cylindrical surfaces  $h = .00002083 \text{ Btu} / \text{in.}^2 \text{min}^\circ \text{F}$ = .3333 a  $T_{m} = -20 \,^{\circ}F$ Radiation = 1.001E-13 Btu / in.<sup>2</sup> min °F<sup>4</sup> f  $T_{m} = -20 \,^{\circ}F$ 

#### Normal Hot, Contents Heat, Solar Effects

All boundary conditions are constant

```
Heat Flux
         Cavity: Contents heat as specified in the geometry definition
        Outer Surfaces (solar): .01065 Btu / in.<sup>2</sup> min
Convection
        Flat surfaces
                  = .00002199 Btu / in.<sup>2</sup> min °F
              h
                   = .3333
              a
              T_{m} = 100 \,^{\circ}\text{F}
         Cylindrical surfaces
                        .00002083 Btu / in.2 min °F
              h
                  =
                        .3333
              а
                   =
              T_{\infty} = 100 \,^{\circ}\text{F}
Radiation
                   = 1.001E-13 Btu / in.<sup>2</sup> min °F<sup>4</sup>
              f
              T_{-} = 100 \,^{\circ}F
```

Version: 1b D-3

# Appendix D Thermal Analysis Boundary Conditions

#### Normal Hot, Contents Heat, No Solar Effects

All boundary conditions are constant

Heat Flux

Cavity: Contents heat as specified in the geometry definition Outer Surfaces (solar): None Convection Flat surfaces  $h = .00002199 \text{ Btu} / \text{in.}^2 \text{min}^\circ \text{F}$ = .3333  $T_{m} = 100 \,^{\circ}F$ Cylindrical surfaces  $h = .00002083 \text{ Btu} / \text{in.}^2 \text{min }^\circ \text{F}$ = .3333 а  $T_{m} = 100 \,^{\circ} F$ Radiation = 1.001E-13 Btu / in.<sup>2</sup> min °F<sup>4</sup> f 100 °F Τ\_ =

#### Fire Accident, Contents Heat, No Solar Effects

All boundary conditions are time dependent

```
Heat Flux Applied for complete analysis
        Cavity: Contents heat as specified in the geometry definition
        Outer Surfaces (solar): None
Convection Applied after fire (30-360 minutes)
        Flat surfaces
             h = .00002199 \text{ Btu / in.}^2 \min {}^\circ \text{F}
                  = .3333
             a
             T_{m} = 100 \,^{\circ}\text{F}
        Cylindrical surfaces
             h = .00002083 \text{ Btu} / \text{in.}^2 \text{min} \,^\circ \text{F}
              a = .3333
             T_{\infty} = 100 \,^{\circ}\text{F}
Radiation Applied during fire (0-30 minutes)
             f = 1.47087E-13 Btu / in.^2 min °F^4
             T_{m} = 1475 \,^{\circ}F
Radiation Applied after fire (30-360 minutes)
             f = 1.6016E-13 Btu / in.^2 min °F^4
              T_{m} = 100 \,^{\circ}\text{F}
```

# **Contents of Distribution Diskettes**

The CASKS release package contains four 5<sup>--</sup>-inch double-density (360Kb) distribution diskettes, listed below. Each file is identified and its function explained.

DISK 1 (5 files)	
File Name	Function
CASKSV1B.D1	CASKS Disk 1 Identification File
CASKS.VER	CASKS Version File
INSTALL.EXE	Program to Install CASKS on the PC
SAMPLE.EXE	Packed Sample Cask Data Set
D1.EXE	Packed File. Install process will unpack the file and produce following files:
PLTDYN.EXE	Program to Plot Dynamic Impact Analysis Results
LIMITER.EDT	Editor Template File for Limiter Force-Deflection Curves
EDITOR EXE	Program to Edit Geometry and Limiter Data Files
TOPAZ.EDT	Editor Template for Creating Thermal Analysis Input
DISK 2 (2 files)	
<u>File Name</u>	Function
CASKSV1B D2	CASKS Disk 2 Identification File
D2 FXF	Packed File Install process will unnack the file and produce following files:
TOPA7 FXF	Program to Perform Thermal Analysis
MSHDSP FXF	Program to Display Finite Element Meshes
POSTP7 FXF	Program to Plot Thermal Analysis Results
INPACT EXE	Program to Perform Impact Analysis
CASKS BAT	CASKS Main Control Batch File
GEOMETRY EDT	Editor Template File for Basic Geometry
SURFACE EDT	Editor Template File for Yielding Surface Force-Deflection Curves
TTRGTPT	Thermal Analysis B C File
MATERIALEDT	Editor Template for Creating/Modifying materials
DISK 3, (2 files)	
File Name	Function
CASKSV1B D3	CASKS Disk 3 Identification File
D3 FXF	Packed File Install process will uppack the file and produce following files:
DATACK FXF	Program to Create Cask Summary and Data Check
SAPPHIRE EXE	Program for Thermal/Pressure Analysis module
SAPRESS EXE	Program to Create Pressure Analysis Input
SAVER EXE	Program to Archive/Retrieve/Delete Data Sets
ASOLIDEEXE	Program for Thermal/Pressure Analysis module
PRETOPAZEXE	Program to Select Thermal Case and Control Thermal Analysis
ASOLIDEXE	Program for Thermal/Pressure Analysis module
CASKSDM COM	CASKS Display Menu
VIDEO VGA	Flag File for Video Display Type
CASKSEM COM	CASKS Archive Menu
CASKSGM COM	CASKS Geometry Menu
CASKSMM COM	CASKS Main Menn
CASKSDM COM	CASKS Print Menu
CASKSAM COM	CASKS Analysis Menu
BSG304 STM	Shell/End Can Material File, Borated Steel 304
DUCSTION STM	Shell/End Cap Material File, Ductile Cast/Iron

Version: 1b E-1

DISK 4 (2 files)	
File Name	Function
CASKSV1B.D4	CASKS Disk 4 Identification File
D4.EXE	Packed File. Install process will unpack the file and produce following files:
GETID.EXE	Program to Select CASK ID
DISCLAIM.EXE	Program to Display Disclaimer
ALLDONE.EXE	Program for Termination Message
SOLVE2.EXE	Program for Thermal/Pressure Analysis module
EDGLP.EXE	Program to Initialize Editor
PRINTIT.EXE	Program to Print and Review Outputs
SAPINPT.EXE	Program to Create Thermal Stress Analysis Input
COPYFL.EXE	Program to Copy Geometry/Limiter Data Files
MATCK.EXE	Program to Check Material Data Files
SOLVE1.EXE	Program for Thermal/Pressure Analysis module
ARCSCANS.EXE	Program to Compress/Expand Data Sets for Archive
EDMAT.EXE	Program to Edit Material Data Files
T1RGTPZI	Thermal Analysis B.C. File
T2RGTPZI	Thermal Analysis B.C. File
T3RGTPZI	Thermal Analysis B.C. File
T4RGTPZI	Thermal Analysis B.C. File
T5RGTPZI	Thermal Analysis B.C. File
T6RGTPZI	Thermal Analysis B.C. File
SS304.STM	Shell/End Cap Material File, Stainless Steel 304
SS304.WJM	Water Jacket Material File, Stainless Steel 304
SS310.STM	Shell/End Cap Material File, Stainless Steel 310
SS310.WJM	Water Jacket Material File, Stainless Steel 310
SS316.STM	Shell/End Cap Material File, Stainless Steel 316
SS316.WJM	Water Jacket Material File, Stainless Steel 316
SS347.STM	Shell/End Cap Material File, Stainless Steel 347
SS347.WJM	Water Jacket Material File, Stainless Steel 347
AIRCONV.NSM	Neutron Shield Material File, Air Convection
BALSAXGR.ILM	Impact Limiter Material File, Balsa wood cross-grained
CARBNSTL.STM	Shell/End Cap Material File, Carbon Steel
CARBNSTL.WJM	Water Jacket Material File, Carbon Steel
COPPER.WJM	Water Jacket Material File, Copper
H2OCONV.NSM	Neutron Shield Material File, Water Convection
LEAD.SHM	Shield Material File, Lead
POLYFOAM.ILM	Impact Limiter Material File, Polyfoam
PLOTRES.LOW	Flag File for Printer Plot Resolution
PRINTER.EPS	Flag File for Printer Type
PURETHAN.ILM	Impact Limiter Material File, Polyurethane
REDWDXGR.ILM	Impact Limiter Material File, Redwood cross-grained
DOT2.COM	Program for Thermal/Pressure Stress Analysis Module
PRINTER.LJT	Program to Control Laser Jet Printer
SURFACE.EDT	Editor Template for Yielding Surface Force-Deflection Curves
DOT1 COM	Program for Thermal/Pressure Stress Analysis Module

### System Details

**CASKS** uses a DOS *BATCH* command file to coordinate the menus, input programs, cask analysis programs, output programs, data archive programs and databases. A *BATCH* file is a file containing commands that DOS executes one at a time. The CASKS *BATCH* file is controlled using menu programs. Each menu program displays a list of options and waits until one of the indicated keys is pressed. After accepting the key, the menu program sets the DOS ERRORLEVEL to indicate which key was pressed. The *BATCH* file branches based on ERRORLEVEL, to perform the selected task.

CASKS has six menu programs. Each menu program is written in Assembly Language, making it small, fast, and flexible. All other programs in CASKS are written in FORTRAN. The FORTRAN programs use a set of FORTRAN callable Assembly Language routines to provide access to DOS and BIOS functions. These functions include manipulating the video screen, sending data to the printer, managing disk files, and obtaining disk space and directory information.

The CASKS BATCH file is listed below with comments identifying the flow of control.

C:	Switch to hard disk continuing CASKS
PROMPT \$e[1:37:40m	Clear prompt, set white text over black background
ECHO OFF	Turn off echo feature of batch file
MODE CO80	Set video mode to CGA with 80 columns of text
REM ***** TEST FOR COMMAND.COM O	N CASKS DRIVE *****

#### IF EXIST\COMMAND.COM GOTO CHNGDIR

ECHO ECHO ECHO ECHO ERROR -- CANNOT INITIALIZE CASKS ECHO ECHO ECHO DRIVE WHICH CONTAINS CASKS ECHO ECHO

PROMPT \$P\$G GOTO END2

:CHNGDIR CD\CASKS DISCLAIM GETID IF NOT EXIST CASK.ID GOTO END

Change to CASKS subdirectory Display CASKS disclaimer Select CASK ID If no CASK ID selected, go to end CASKS

:MAIN CASKSMM IF ERRORLEVEL 7 GOTO END IF ERRORLEVEL 6 GOTO SAVE

Display MAIN MENU Check ERRORLEVEL and branch

Version: 1b E-3

# Appendix E

**Program Reference** IF ERRORLEVEL 5 GOTO PRINTER IF ERRORLEVEL 4 GOTO DISPLAY IF ERRORLEVEL 3 GOTO ANALYZE **IF ERRORLEVEL 2 GOTO GEOMETRY** :INIT Select CASK ID GETID and return to MAIN MENU GOTO MAIN :GEOMETRY Delete EDITOR control file IF EXIST EDITOR.EDM DEL EDITOR.EDM Display GEOMETRY MENU CASKSGM Check ERRORLEVEL and branch **IF ERRORLEVEL 7 GOTO MAIN** Check ERRORLEVEL and branch IF ERRORLEVEL 6 GOTO EDITM IF ERRORLEVEL 5 GOTO COPYLM IF ERRORLEVEL 4 GOTO COPYBG IF ERRORLEVEL 3 GOTO EDITS IF ERRORLEVEL 2 GOTO EDITL EDITG EDIT THE BASIC GEOMETRY DATA FILE AND PERFORM DATA CHECK Setup to edit GEOMETRY EDGLP G IF NOT EXIST EDITOR.EDM GOTO GEOMETRY If control file missing, return to GEOMETRY MENU Edit GEOMETRY EDITOR If not doing data check, return to GEOMETRY MENU IF NOT EXIST DATACHCK GOTO GEOMETRY DATACK G Perform data check on basic geometry and return to GEOMETRY MENU GOTO GEOMETRY EDITL EDIT THE IMPACT LIMITER DATA FILE AND PERFORM DATA CHECK Setup to edit LIMITER EDGLPL

EDGLP L IF NOT EXIST EDITOR.EDM GOTO GEOMETRY EDITOR IF NOT EXIST DATACHCK GOTO GEOMETRY DATACK L GOTO GEOMETRY

If control file missing, return to GEOMETRY MENU
Edit LIMITER
If not doing data check, return to GEOMETRY MENU
Perform data check on limiter F/D curves
and return to GEOMETRY MENU

Setup to edit SURFACE

:EDITS EDGLP S IF NOT EXIST EDITOR.EDM GOTO GEOMETRY EDITOR DATACK S GOTO GEOMETRY'

:COPYBG COPY BASIC GEOMETRY FROM DIFFERENT CASK COPYFL B | Copy GEOMETRY from different data set GOTO GEOMETRY | and return to GEOMETRY MENU

:COPYLM COPY LIMITER DATA FROM DIFFERENT CASK COPYFL L | Copy LIMITER from different data set GOTO GEOMETRY | and return to GEOMETRY MENU

:EDITM EDMAT S IF NOT EXIST EDITOR.EDM GOTO GEOMETRY EDITOR IF NOT DATACHCK TOTO GEOMETRY MATCK GOTO GEOMETRY

:ANALYZE PERFORM ANALYSIS CASKSAM IF ERRORLEVEL 5 GOTO MAIN

IF ERRORLEVEL 4 GOTO PSTRESS IF ERRORLEVEL 3 GOTO TSTRESS IF ERRORLEVEL 2 GOTO THERMAL

:IMPACTIT PERFORM IMPACT ANALYSIS IMPACT GOTO ANALYZE

:THERMAL PERFORM THERMAL ANALYSIS PRETOPAZ IF NOT EXIST TOPAZ.CMD GOTO ANALYZE TOPAZ IF EXIST CONTINUE.TPZ GOTO THERMAL GOTO ANALYZE

:PSTRESS SAPRESS IF NOT EXIST TEMPCASK GOTO ANALYZE SAPPHIRE ASOLID DOT1 SOLVE1 >TEMPCASK.JNK DOT2 SOLVE2 >>TEMPCASK.JNK ASOLIDF DEL TEMPCASK.\* DEL SYSTEM IF EXIST CONTINUE.TSO GOTO PSTRESS GOTO ANALYZE | Display ANALYSIS MENU | Check ERRORLEVEL and branch

Perform IMPACT analysis and return to ANALYSIS MENU

Perform THERMAL analysis

and return to ANALYSIS MENU

Select case for PRESSURE STRESS analysis If no case selected, return to ANALYSIS MENU Perform PRESSURE STRESS analysis

Delete temporary files

If performing another, go to select case else return to ANALYSIS MENU

# Appendix **E**

### **Program Reference**

:TSTRESS SAPINPT IF NOT EXIST TEMPCASK GOTO ANALYZE SAPPHIRE ASOLID DOT1 SOLVE1 >TEMPCASK.JNK DOT2 SOLVE2 >>TEMPCASK.JNK ASOLIDF DEL TEMPCASK.\* DEL SYSTEM IF EXIST CONTINUE.TSO GOTO TSTRESS GOTO ANALYZE

:DISPLAY CASKSDM IF ERRORLEVEL 5 GOTO MAIN IF ERRORLEVEL 4 GOTO ATTRIB IF ERRORLEVEL 3 GOTO PLOTT IF ERRORLEVEL 2 GOTO PMESH

:PLOTI PLOT IMPACT RESULTS PLTDYN GOTO DISPLAY

:PMESH PLOT FINITE ELEMENT MESHES MSHDSP D GOTO DISPLAY

:PLOTT PLOT THERMAL DISTRIBUTIONS POSTPZ GOTO DISPLAY

:ATTRIB SET VIDEO ATTRIBUTES SETVIDEO GOTO DISPLAY

:PRINTER CASKSPM IF ERRORLEVEL 6 GOTO MAIN IF ERRORLEVEL 5 GOTO PRINTD IF ERRORLEVEL 4 GOTO PRINTP IF ERRORLEVEL 3 GOTO PRINTS IF ERRORLEVEL 2 GOTO PRINTT Select case for THERMAL STRESS analysis
 If no case selected, return to ANALYSIS MENU
 Perform THERMAL STRESS analysis

Delete temporary files

If performing another, go to select case else return to ANALYSIS MENU

Display DISPLAY MENU Check ERRORLEVEL and branch

Plot DYNAMIC IMPACT ANALYSIS results and return to DISPLAY MENU

Display FINITE ELEMENT meshes and return to DISPLAY MENU

Plot THERMAL ANALYSIS results and return to DISPLAY MENU

Select Video/Printer type and plot resolution and return to DISPLAY MENU

Display PRINT/REVIEW MENU Check ERRORLEVEL and branch

#### Appendix $-\mathbf{E}$ **Program Reference**

PRINTI PRINT IMPACT RESULTS PRINTIT I GOTO PRINTER PRINTT PRINT THERMAL RESULTS PRINTIT T GOTO PRINTER

:PRINTS PRINT THERMAL STRESS RESULTS PRINTIT S GOTO PRINTER

PRINTP PRINT PRESSURE STRESS RESULTS PRINTIT P GOTO PRINTER

PRINTD PRINT CASK SUMMARY AND DATA CHECK PRINTIT D GOTO PRINTER

:SAVE CASKSFM IF ERRORLEVEL 4 GOTO MAIN IF ERRORLEVEL 3 GOTO DELETE **IF ERRORLEVEL 2 GOTO GET** 

:PUT ARCHIVE CASK DATA SET SAVER A **GOTO SAVE** 

:GET RETRIEVE CASK DATA SET SAVER R **GOTO SAVE** 

:DELETE DELETE CASK DATA SET SAVER D **GOTO SAVE** 

:END \*\*\*\*\* END OF THE CASKS PROCESS IF EXIST CASK.ID DEL CASK.ID PROMPT \$p \$g ALLDONE :END2 CD/ ECHO ON

Print IMPACT ANALYSIS results and return to PRINT/REVIEW MENU

Print THERMAL ANALYSIS results and return to PRINT/REVIEW MENU

Print THERMAL STRESS ANALYSIS results and return to PRINT/REVIEW MENU

Print PRESSURE STRESS ANALYSIS results and return to PRINT/REVIEW MENU

Print CASK SUMMARY/DATA CHECK and return to PRINT/REVIEW MENU

Display ARCHIVE MENU Check ERRORLEVEL and branch

ARCHIVE data sets and return to ARCHIVE MENU

RETRIEVE data sets and return to ARCHIVE MENU

DELETE data sets and return to ARCHIVE MENU

Terminate CASKS Delete CASK ID identification file Set prompt to display drive and path Display termination message

Change to root directory Restore ECHO

Version: 1b E-7

### **Description** of Databases

**CASKS** uses integrated databases to pass information between various programs. These databases describe the cask geometry, impact limiter force-deflection curves, material properties, boundary conditions for Thermal analyses, analysis results for plotting, and analysis results for printing. All databases, with the exception of printable output, are *random access* files with fixed record lengths. Thus, each program that utilizes the database has access to individual elements in the data base, identified by record number. Following is a description of each *random access* database.

#### Basic Geometry Database

Purpose:	Contains all geometry specifications for the cask.
Used by:	IMPACT, DATACK, PRETOPAZ, SAPINPT, SAPRESS, MSHDSP
Created by:	EDITOR
Modified by:	EDITOR, PRETOPAZ
Record Length:	12

NOTE: Record types are as follows:

Real = Real Number Int = Integer Number Char = Character string List = Single Character which must match specific choices Name = Value is selected from a file name list

#### <u>Header</u>

Record	Description	Туре	Length	Comments
1	Casks Id			Must be Scans ger
2١				
31				•
4	Database name	Char	60	
51				
6/				
8	File creation date	Char	8	Form 'mm/dd/yy'
9	File creation time	Char	8	Form 'hh:mm:ss'
10	Editor code name	Char	8	Editor
11	Editor version no.	Char	3	2.1
12	Editor compile date	Char	8	Form 'mm/dd/yy'
13	Geometry template file name	Char	12	Geometry.edt
14	Unused at this time			
15	Data file status	Char	12	'Complete' or 'Incomplete'
16	Page 1 mod date, PGACC, PGREO	Char	811	Form 'mm/dd/yy AR'
17	Page 2 mod date, PGACC, PGREO	Char	811	Form 'mm/dd/yy AR'
1				

. NOTE: See TEMPLATE for definition of PGACC & PGREQ

	•			
45	Page 45 mod date, PGACC, PGREQ	Char	811	Form 'mm/dd/yy AR'

#### General SAR Information and Reviewer Information

Record Description	Туре	Length	Restrictions	Default
46 \				
47   48   SAR title	Char	54		(blank)
49	0	5.		(onumy
50 /				
51 SAR report number	Char	12		(blank)
52 SAR report date	Char	8		(blank)
53 SAR docket number	Char	7		(blank)
54 SAR docket start date	Char	8		(blank)
55 \				
561	C.	~ ^		<i>.</i>
57 I Additional SAR into Line 1	Char	54		(blank)
50 /				
597				
61		•		
62 I Additional SAR info Line 2	Char	54		(blank)
63	•••••	•		()
64 /				
65 \				
66 I				
67 I Additional SAR info Line 3	Char	54		(blank)
68 1				
69 /				
70 \				
71   72   Submitters address I ine 1	Char	54		(blank)
72   Submitter's address Emic 1	Cha	54		(utank)
74 /				
75 \				
76				
77 I Submitters address Line 2	Char	54		(blank)
78				
79 /				
80 \				
	Ohan	54		0.1
82 I Submitters address Line 3	Cnar	54		(blank)
84 /				
85 Cask review leader name	Char	24		(blank)
86 (cont'd)	0	2.		(0)
87 Thermal analyst's name	Char	24		(blank)
88 (cont'd)				
89 Structural analyst's name	Char	24		(blank)
90 (cont'd)				
91 Nucleonics analyst's name	Char	24		(blank)
92 (cont'd)				

Unused at this time 93-99

Version: 1b E-9

### Cask Cavity/Contents Specifications

Record	Description	Туре	Length	Restrictions	Default
100	Gross weight of package (lbs)	Real	12	Positive	0.
101	Cavity radius (inches)	Real	12	$.001 \le X \le 2000$	0.
102	Cavity radius mesh divisions	Int	2	Even $2 \le I \le 20$	6
103	Cavity length (inches)	Real	12	$.001 \le \mathrm{X} \le 2000$	0.
104	Half length mesh divisions	Int	2	Even $2 \le I \le 40$	8
105	Weight of contents (lbs)	Real	12	Positive	0
106	Max contents heat (btu/min)	Real	12	0 ≤ X	0
107	Initial cavity pressure (psia)	Real	12	$0 \le X \le 500$	14.7
108	Initial cavity temperature (°F)	Real	12	$-100 \le X \le 300$	70
109	Maximum Normal Operating Pressure (psia)	Real	12	$0 \le X \le 2000$	14.7
110	Stress free temperature (°F)	Real	12	$-100 \le X \le 300$	70

#### Cask Component Configurations

Record	d Description	Type L	length	Restrictions	Default
111	Shell configuration	List	1	S or L	S
112	Top end cap configuration	List	1	S or L	S
113	Bottom end cap configuration	List	1	S or L	S
114	Top limiter present?	List	1	Y or N	Y
115	Bottom limiter present?	List	1	Y or N	Y
116	Neutron shield/water jacket?	List	1	Y or N	Y

117-120 Unused at this time

#### **Cask Shell Specifications**

Record	Description	Туре	Length	Restrictions	Default
The follo	wing 3 records are for Solid Shells (1 layer)				
121	Shell thickness (in.)	Real	12	$.001 \le X \le 2000$	0.
122	Shell material	Name	8	List from *.STM	SS304
123	Shell mesh divisions	Int	2	Even $2 \le I \le 10$	4
The follo	owing 12 records are for Laminated Shells (1-3 layo	ers)			
124	Shell inner layer thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
125	Shell inner layer material	Name	8	List from *.STM	SS304
126	Shell inner layer mesh divisions	Int	2	Even $2 \le I \le 10$	2
127	Shell shield thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
128	Shell shield length (in.)	Real	12	0. ≤ X ≤ 2000	0.
129	Shell shield material	Name	8	List from *.SHM	LEAD
130	Shell shield mesh divisions	Int	2	Even $2 \le I \le 10$	4
131	Shell outer layer thickness (in.)	Real	12	$.001 \le X \le 2000$	0.
132	Shell outer layer material	Name	8	List from *.STM	SS304
133	Shell outer layer mesh divisions	Int	2	Even $2 \le I \le 10$	2
134	Inner Shell additional thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
135	Outer Shell additional thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.

#### Cask Top End Cap Specifications

Record	Description	Туре	Length	Restrictions	Default
The follo	owing 3 records are for Solid Top End Caps (1 laye	r)			
136	Top End Cap thickness (in.)	Real	12	$.001 \le X \le 2000$	0.
137	Top End Cap material	Name	8	List from *.STM	SS304
138	Top End Cap mesh divisions	Int	2	Even $2 \le I \le 10$	4
The follo	owing 10 records are for Laminated Top End Caps (	1-3 layer	s)		
139	Top End Cap inner layer thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
140	Top End Cap inner layer material	Name	8	List from *.STM	SS304
141	Top End Cap inner layer mesh divisions	Int	2	Even $2 \le I \le 10$	2
142	Top End Cap shield thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
143	Top End Cap shield length (in.)	Real	12	0. ≤ X ≤ 2000	0.
144	Top End Cap shield material	Name	8	List from *.SHM	LEAD
145	Top End Cap shield mesh divisions	Int	2	Even $2 \le I \le 10$	4
146	Top End Cap outer layer thickness (in.)	Real	12	$.001 \le X \le 2000$	0.
147	Top End Cap outer layer material	Name	8	List from *.STM	SS304
148	Top End Cap outer layer mesh divisions	Int	2	Even $2 \le I \le 10$	2

149-150 Unused at this time

### Cask Bottom End Cap Specifications

Record	Description	Туре	Length	Restrictions	Default
The foll	owing 3 records are for Solid Bottom End Caps (	1 layer)			
151	Bottom End Cap thickness (in.)	Real	12	$.001 \le X \le 2000$	0.
152	Bottom End Cap material	Name	8	List from *.STM	SS304
153	Bottom End Cap mesh divisions	Int	2	Even $2 \le I \le 10$	4
The foll	owing 10 records are for Laminated Bottom End	Caps (1-3 la	iyers)		
154	Bottom End Cap inner layer thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
155	Bottom End Cap inner layer material	Name	8	List from *.STM	SS304
156	Bottom End Cap inner layer mesh divisions	Int	2	Even $2 \le I \le 10$	2
157	Bottom End Cap shield thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
158	Bottom End Cap shield length (in.)	Real	12	0. ≤ X ≤ 2000	0.
159	Bottom End Cap shield material	Name	8	List from *.SHM	LEAD
160	Bottom End Cap shield mesh divisions	Int	2	Even $2 \le I \le 10$	4
161	Bottom End Cap outer layer thickness (in.)	Real	12	$.001 \le X \le 2000$	0.
162	Bottom End Cap outer layer material	Name	8	List from *.STM	SS304
163	Bottom End Cap outer layer mesh divisions	Int	2	Even $2 \le I \le 10$	2

164-167 Unused at this time

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E-11 Version: 1b
### Appendix E

### Program Reference

### Cask Closure Bolts Information

Record	Description	Туре	Length	Restrictions	Default
168	Closure bolt circle radius (in.)	Real	12	$.001 \le X \le 2000$	0.
169	Number of closure bolts	Int	2	1 ≤ I ≤ 99	0
170	Diameter of closure bolts (in.)	Real	12	$.001 \le \mathrm{X} \le 10$	0.

171-175 Unused at this time

### Cask Neutron Shield / Water Jacket Specifications

Record	Description	Туре I	Length	Restrictions	Default
176	Neutron shield / Water Jacket length (in.)	Real	12	0. ≤ X ≤ 2000	0.
177	Neutron shield thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
178	Neutron shield material	Name	8	List from *.NSM	H2OCONV
179	Neutron shield mesh divisions	Int	2	2 ≤ I ≤ 9	1
180	Water jacket thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
181	Water jacket material	Name	8	List from *.WJM	SS304
182	Water jacket mesh divisions	Int	2	2≤I≤9	1

183-185 Unused at this time

### Cask Top Impact Limiter Specifications

Record	Description	Туре	Length	Restrictions	Default
186	Top limiter outer radius	Real	12	$.001 \le \mathrm{X} \le 2000$	0.
187	Top limiter centerline thickness (in.)	Real	12	$.001 \le X \le 2000$	0.
188	Top limiter centerline mesh divisions	Int	2	$2 \le I \le 10$	4
189	Top limiter overhang thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
190	Top limiter overhang mesh divisions	Int	2	$2 \le I \le 10$	3
191	Top limiter material	Name	8	List from *.ILM	POLYFOAM

192-195 Unused at this time

### Cask Bottom Impact Limiter Specifications

Record	Description	Туре	Length	Restrictions	Default
196	Bottom limiter outer radius	Real	12	$.001 \le \mathrm{X} \le 2000$	0.
197	Bottom limiter centerline thickness (in.)	Real	12	$.001 \le \mathrm{X} \le 2000$	0.
198	Bottom limiter centerline mesh divisions	Int	2	$2 \le I \le 10$	4
199	Bottom limiter overhang thickness (in.)	Real	12	0. ≤ X ≤ 2000	0.
200	Bottom limiter overhang mesh divisions	Int	2	$2 \le I \le 10$	3
201	Bottom limiter material	Name	8	List from *.ILM	POLYFOAM

202-205 Unused at this time

### **Cask Impact Model Specifications**

Record	Description	Туре	Length	Restrictions	Default
206	Number of elements for 1d model	Int	2	$3 \le I \le 20$	4
207	Top limiter weight (lbs)	Real	12	$0 \leq X$	0.
208	Bottom limiter weight (lbs)	Real	12	0 ≤ X.	0.
209	Define model with user properties ?	List	1	Y or N	N
210	Shell translational mass (lb-sec**2/in.)	Real	12	POSITIVE	0.
211	Shell rotational mass (lb-sec**2-in.)	Real	12	POSITIVE	0.
212	Shell inside length (in.)	Real	12	POSITIVE	0.
213	Shell composite E*I (lb-in.**2)	Real	12	POSITIVE	0.
214	Shell composite A*E (lb)	Real	12	POSITIVE	0.
215	Top End translational mass (lb-sec**2/in.)	Real	12	POSITIVE	0.
216	Top End rotational mass (lb-sec**2-in.)	Real	12	POSITIVE	0.
217	Bottom End translational mass (lb-sec**2/in.)	Real	12	POSITIVE	0.
218	Bottom End rotational mass (lb-sec**2/in.)	Real	12	POSITIVE	0.
219	Characteristic cross-section (in.)	Real	12	POSITIVE	0.

220 Unused at this time

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### **Thermal Transient Analysis Control Parameters**

NOTE: These parameters cannot be modified using the EDITOR

Record	Record Description		Length	Restrictions	Default	
221	Allow phase change ?	List	1	Y or N	N	
222	Print output interval (min)	Real	12	$10 \le X \le 3603$	0.	
223	Plot output interval (min)	Real	12	$2 \le X \le 30$	5.	
224	Use variable time step?	List	1	Y or N	N	
225	Iteration convergence tolerance	Real	12	$.001 \le X \le .1$	.001	
226	Iteration relaxation parameter	Real	12	.3 ≤ X ≤ 1.	1.	
227	Maximum allowable time step (min)	Real	12	$5 \le X \le 30$	30.	
228	Maximum allowable temperature change (°F)	Real	12	$25 \le X \le 50$	100.	
229	Time step modification factor	Real	12	2≤X≤6	2.	
230	Fixed time step size (min)	Real	12	.25 ≤ X ≤ 5	.5	

### Impact Limiter Force-Deflection Curves Database

Purpose:Contains all limiter force-deflection curve specificationsUsed by:IMPACT, DATACKCreated by:EDITORModified by:EDITORRecord Length:12

NOTE: Record types are as follows:

- Real = Real Number
- Int = Integer Number
- Char = Character string
- List = Single Character which must match specific choices
- Name = Value is selected from a file name list

### <u>Header</u>

Record 1 2 \	Description Casks Id	Туре	Length	<b>Comments</b> Must be 'Scans lmi'
31				
4	Database name	Char	60	
51				
6/			-	
8	File creation date	Char	8	Form 'mm/dd/yy'
9	File creation time	Char	8	Form 'hh:mm:ss'
10	Editor code name	Char	8	Editor
11	Editor version no.	Char	3	2.1
12	Editor compile date	Char	8	Form 'mm/dd/yy'
13	Limiter template file name	Char	12	Limiter.edt
14	Unused at this time			
15	Data file status	Char	12	'Complete' or 'Incomplete'
16	Page 1 mod date, PGACC, PGREQ	Char	811	Form 'mm/dd/yy AR'
17	Page 2 mod date, PGACC, PGREQ	Char	811	Form 'mm/dd/yy AR'

. NOTE: See TEMPLATE for definition of PGACC & PGREQ

	-			
45	Page 45 mod date, PGACC, PGREQ	Char	811	Form 'mm/dd/yy AR'

### **Impact Limiter Unloading Specification**

Record	Description	Type	Length	Restrictions	Default
48	Type of limiter unloading	List	1	N or U or C	N
49	User unloading slope (kips/in.)	Real	12	POSITIVE	0.

### Bottom Impact Limiter Curve for a 0-Degree Impact

Record	Descript	ion		Type 1	Length	Restrictions	Default
50	Is this limite	r defin	ned?	List	1	Y or N	N
51	Deflection #	1 (in.)	•	Real	12	POSITIVE	0.
52	Force	#1	(kips)	Real	12	POSITIVE	0.
53	Deflection	#2	(in.)	Real	12	POSITIVE	0.
54	Force	#2	(kips)	Real	12	POSITIVE	0.
55	Deflection	#3	(in.)	Real	12	0, ≤ X	0.
56	Force	#3	(kips)	Real	12	0. ≤ X	0.
57	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
58	Force	#4	(kips)	Real	12	0. ≤ X	0.
59	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
60	Force	#5	(kips)	Real	12	0. ≤ X	0.
61	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
62	Force	#6	(kips)	Real	12	0. ≤ X	0.
63	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
64	Force	#7	(kips)	Real	12	0. ≤ X	0.
65	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
66	Force	#8	(kips)	Real	12	0. ≤ X	0.
67	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
68	Force	#9	(kips)	Real	12	0. ≤ X	0.
69	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
70	Force	#10	(kips)	Real	12	0. ≤ X	0.
71-74	Unused a	t this i	ime				

### Bottom Impact Limiter Curve for a 15-Degree Impact

L. L. B. Straw Markey Com

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Record	Descripti	ion		Туре	Length	Restrictions	Default
75	Is this limite	r defi	ned?	List	1	Y or N	Ν
76	Deflection	#1	(in.) .	Real	12	POSITIVE	0.
77	Force	#1	(kips)	Real	12	POSITIVE	0.
78	Deflection	#2	(in.) ·	Real	12	POSITIVE	0.
79	Force	#2	(kips)	Real	12	POSITIVE	0.
80	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
81	Force	#3	(kips)	Real	12	0. ≤ X	0.
82	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
83	Force	#4	(kips)	Real	12	0. ≤ X	0.
84	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
85	Force	#5	(kips)	Real	12	0. ≤ X	0.
86	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
87	Force	#6	(kips)	Real	12	0. ≤ X	0.
88	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
89	Force	#7	(kips)	Real	12	0. ≤ X	0.
90	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
91	Force	#8	(kips)	Real	12	0. ≤ X	0.
92	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
93	Force	#9	(kips)	Real	12	0. ≤ X	0.
94	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
95	Force	#10	(kips)	Real	12	0. ≤ X	0.
96-99	Unused at	this	time				

### Appendix E

### Program Reference

### Bottom Impact Limiter Curve for a 30-Degree Impact

Record	Descripti	ion		Туре	Length	Restrictions	Default
100	Is this limiter	r defir	ied?	List	1	Y or N	Ν
101	Deflection	#1	(in.)	Real	12	POSITIVE	0.
102	Force	#1	(kips)	Real	12	POSITIVE	0.
103	Deflection	#2	(in.)	Real	12	POSITIVE	0.
104	Force	#2	(kips)	Real	12	POSITIVE0.	
105	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
106	Force	#3	(kips)	Real	12	0. ≤ X	0.
107	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
108	Force	#4	(kips)	Real	12	0. ≤ X	0.
109	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
110	Force	#5	(kips)	Real	12	0. ≤ X	0.
111	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
112	Force	#6	(kips)	Real	12	0. ≤ X	0.
113	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
114	Force	#7	(kips)	Real	12	0. ≤ X	0.
115	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
116	Force	#8	(kips)	Real	12	0. ≤ X	0.
117	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
118	Force	#9	(kips)	Real	12	0. ≤ X	0.
119	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
120	Force	#10	(kips)	Real	12	0. ≤ X	0.
121-124	Unused at	this ti	ime				

### Bottom Impact Limiter Curve for a 45-Degree Impact

Record	Descript	ion		Туре	Length	Restrictions	Default
125	Is this limite	r defin	ned?	List	1	Y or N	Ν
126	Deflection	#1	(in.)	Real	12	POSITIVE	0.
127	Force	#1	(kips)	Real	12	POSITIVE	0.
128	Deflection	#2	(in.)	Real	12	POSITIVE	0.
129	Force	#2	(kips)	Real	12	POSITIVE	0.
130	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
131	Force	#3	(kips)	Real	12	0. ≤ X	0.
132	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
133	Force	#4	(kips)	Real	12	0. ≤ X	0.
134	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
135	Force	#5	(kips)	Real	12	0. ≤ X	0.
136	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
137	Force	#6	(kips)	Real	12	0. ≤ X	0.
138	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
139	Force	#7	(kips)	Real	12	0. ≤ X	0.
130	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
141	Force	#8	(kips)	Real	12	0, ≤ X	0.
142	Deflection	#9	(in.)	Real	12	0, ≤ X	0.
143	Force	#9	(kips)	Real	12	0. ≤ X	0.
144	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
145	Force	#10	(kips)	Real	12	0. ≤ X	0.
146-149	Unused at	this ti	ime				

### Bottom Impact Limiter Curve for a 60-Degree Impact

Record	Descript	ion		Type.	Length	Restrictions	Default
150	Is this limite	r defin	ned?	List	1	Y or N	N
151	Deflection	#1	(in.)	Real	12	POSITIVE	0.
152	Force	#1	(kips)	Real	12	POSITIVE	0.
153	Deflection	#2	(in.)	Real	12	POSITIVE	0.
154	Force	#2	(kips)	Real	12	POSITIVE	0.
155	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
156	Force	#3	(kips)	Real	12	0. ≤ X	0.
157	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
158	Force	#4	(kips)	Real	12	0. ≤ X	0.
159	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
160	Force	#5	(kips)	Real	12	0. ≤ X	0.
161	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
162	Force	#6	(kips)	Real	12	0. ≤ X	0.
163	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
164	Force	#7	(kips)	Real	12	0. ≤ X	0.
165	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
166	Force	#8	(kips)	Real	12	0. ≤ X	0.
167	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
168	Force	#9	(kips)	Real	12	0. ≤ X	0.
169	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
170	Force	#10	(kips)	Real	12	0. ≤ X	0.
171-174	Unused at	this t	ime				

### Bottom Impact Limiter Curve for a 75-Degree Impact

Record Description Type Length Restrictions Default										
175	Is this limite	r defi	ned?	List	1	Y or N	N			
176	Deflection	#1	(in.)	Real	12	POSITIVE	0.			
177	Force	#1	(kips)	Real	12	POSITIVE	0.			
178	Deflection	#2	(in.)	Real	12	POSITIVE	0.			
179	Force	#2	(kips)	Real	12	POSITIVE .	0.			
180	Deflection	#3	(in.)	Real	12	0. ≤ X	0.			
181	Force	#3	(kips)	Real	12 -	0. ≤ X	0.			
182	Deflection	#4	(in.)	Real	12	0. ≤ X	0.			
183	Force	#4	(kips)	Real	12	0. ≤ X	0.			
184	Deflection	#5	(in.)	Real	12	0. ≤ X	0.			
185	Force	#5	(kips)	Real	12	0. ≤ X	0.			
186	Deflection	#6	(in.)	Real	12	0. ≤ X	0.			
187	Force	#6	(kips)	Real	12	0. ≤ X	0.			
188	Deflection	#7	(in.)	Real	12	0. ≤ X	0.			
189	Force	#7	(kips)	Real	12	0. ≤ X	0.			
190	Deflection	#8	(in.)	Real	12	0. ≤ X	0.			
191	Force	#8	(kips)	Real	12	0. ≤ X	0.			
192	Deflection	#9	(in.)	Real	12	0. ≤ X	0.			
193	Force	#9	(kips)	Real	12	0. ≤ X	0.			
194	Deflection	#10	(in.)	Real	12	0. ≤ X	0.			
195	Force	#10	(kips)	Real	12	0. ≤ X	0.			
196-199	96-199 Unused at this time									

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### Bottom Impact Limiter Curve for a 90-Degree Impact

Record	Descripti	on		Туре	Length	Restrictions	Default
200	Is this limiter	defir	ied?	List	1	Y or N	Ν
201	Deflection	#1	(in.)	Real	12	POSITIVE	0.
202	Force	#1	(kips)	Real	12	POSITIVE	0.
203	Deflection#2		(in.)	Real	12	POSITIVE	0.
204	Force	#2	(kips)	Real	12	POSITIVE	0.
205	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
206	Force	#3	(kips)	Real	12	0. ≤ X	0.
207	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
208	Force	#4	(kips)	Real	12	0. ≤ X	0.
209	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
210	Force	#5	(kips)	Real	12	0. ≤ X	0.
211	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
212	Force	#6	(kips)	Real	12	0. ≤ X	0.
213	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
214	Force	#7	(kips)	Real	12	0. ≤ X	0.
215	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
216	Force	#8	(kips)	Real	12	0. ≤ X	0.
217	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
218	Force	#9	(kips)	Real	12	0. ≤ X	0.
219	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
220	Force	#10	(kips)	Real	12	0, ≤ X	0.
221-224	Unused at	this ti	ime				

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### Bottom Impact Limiter Curve for a C.G. Degree Impact

Record	Descript	ion		Туре	Length	Restrictions	Default
225	Is this limite	r defii	ned?	List	1	Y or N	N
226	Deflection	#1	(in.)	Real	12	POSITIVE	0.
227	Force	#1	(kips)	Real	12	POSITIVE	0.
228	Deflection	#2	(in.)	Real	12	POSITIVE	0.
229	Force	#2	(kips)	Real	12	POSITIVE	0.
230	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
231	Force	#3	(kips)	Real	12	0. ≤ X	0.
232	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
233	Force	#4	(kips)	Real	12	0. ≤ X	0.
234	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
235	Force	#5	(kips)	Real	12	0. ≤ X	0.
236	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
237	Force	#6	(kips)	Real	12	0. ≤ X	0.
238	Deflection	#7	(in.)	Real	12	0. ≤ X	0. <sup>.</sup>
239	Force	#7	(kips)	Real	12	0. ≤ X	0.
230	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
241	Force	#8	(kips)	Real	12	0. ≤ X	0.
242	Deflection	#9	(in.)	Real	12	. ≤ X .	0.
243	Force	#9	(kips)	Real	12	0. ≤ X	0.
244	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
245	Force	#10	(kips)	Real	12	0. ≤ X	0.
246-249	Unused at	this t	ime				



### Top Impact Limiter Curve for a 0-Degree Impact

Record	Descript	ion		Туре	Length	Restrictions	Default
250	Is this limite	r defii	ned?	List	1	Y or N	N
251	Deflection	#1	(in.)	Real	12	POSITIVE	0.
252	Force	#1	(kips)	Real	12	POSITIVE	0.
253	Deflection	#2	(in.)	Real	12	POSITIVE	0.
254	Force	#2	(kips)	Real	12	POSITIVE	0.
255	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
256	Force	#3	(kips)	Real	12	0. ≤ X	0.
257	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
258	Force	#4	(kips)	Real	12	0. ≤ X	0.
259	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
260	Force	#5	(kips)	Real	12	0. ≤ X	0.
261	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
262	Force	#6	(kips)	Real	12	0. ≤ X	0.
263	Deflection	<b>#7</b>	(in.)	Real	12	0. ≤ X	0.
264	Force	#7	(kips)	Real	12	0. ≤ X	0.
265	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
266	Force	#8	(kips)	Real	12	0. ≤ X	0.
267	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
268	Force	#9	(kips)	Real	12	0. ≤ X	0.
269	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
270	Force	#10	(kips)	Real	12	0. ≤ X	0.
271-274	Unused at	this t	ime			•	

### Top Impact Limiter Curve for a 15-Degree Impact

Record	Descripti	ion		Туре	Length	Restrictions	Default
275	Is this limite	r defir	ned?	List	1	Y or N	Ν
276	Deflection	#1	(in.)	Real	12	POSITIVE	0.
277	Force	#1	(kips)	Real	12	POSITIVE	0.
278	Deflection	#2	(in.)	Real	12	POSITIVE	0.
279	Force	#2	(kips)	Real	12	POSITIVE	0.
280	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
281	Force	#3	(kips)	Real	12	0. ≤ X	0.
282	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
283	Force	#4	(kips)	Real	12	0. ≤ X	0.
284	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
285	Force	#5	(kips)	Real	12	0. ≤ X	0.
286	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
287	Force	#6	(kips)	Real	12	0. ≤ X	0.
288	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
289	Force	#7	(kips)	Real	12	0. ≤ X	0.
290	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
291	Force	#8	(kips)	Real	12	0. ≤ X	0.
292	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
293	Force	#9	(kips)	Real	12	0. ≤ X	0.
294	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
295	Force	#10	(kips)	Real	12	0. ≤ X	0.
296-299	Unused at	this ti	me				

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### Top Impact Limiter Curve for a 30-Degree Impact

Record	Descript	ion		Type	Length	Restrictions	Default
300	Is this limite	r defir	ned?	List	1	Y or N	Ν
301	Deflection	#1	(in.)	Real	12	POSITIVE	0.
302	Force	#1	(kips)	Real	12	POSITIVE	0.
303	Deflection	#2	(in.)	Real	12	POSITIVE	0.
304	Force	#2	(kips)	Real	12	POSITIVE0.	
305	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
306	Force	#3	(kips)	Real	12	0. ≤ X	0.
307	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
308	Force	#4	(kips)	Real	12	0. ≤ X	0.
309	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
310	Force	#5	(kips)	Real	12	0. ≤ X	0.
311	Deflection	#6	(in.)	Real	12 ,	0. ≤ X	0.
312	Force	#6	(kips)	Real	12	0. ≤ X	0.
313	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
314	Force	#7	(kips)	Real	12	0. ≤ X	0.
315	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
316	Force	#8	(kips)	Real	12	0. ≤ X	0.
317	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
318	Force	#9	(kips)	Real	12	0. ≤ X	0.
319	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
320	Force	#10	(kips)	Real	12	0. ≤ X	0.
321-324	I Inused at	this t	ime				

### Top Impact Limiter Curve for a 45-Degree Impact

Record	Descripti	ion		Туре	Length	Restrictions	Default
325	Is this limiter	r defir	ned?	List	1	Y or N	N
326	Deflection	#1	(in.)	Real	12	POSITIVE	0.
327	Force	#1	(kips)	Real	12	POSITIVE	0.
328	Deflection	#2	(in.)	Real	12	POSITIVE	0.
329	Force	#2	(kips)	Real	12	POSITIVE .	0.
330	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
331	Force	#3	(kips)	Real	12	0. ≤ X	0.
332	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
333	Force	#4	(kips)	Real	12	0. ≤ X	0.
334	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
335	Force	#5	(kips)	Real	12	0. ≤ X	0.
336	Deflection	#6	(in.)-	Real	12	0. ≤ X	0.
337	Force	#6	(kips)	Real	12	0. ≤ X	0.
338	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
339	Force	#7	(kips)	Real	12	0. ≤ X	0.
330	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
341	Force	#8	(kips)	Real	12	0. ≤ X	0.
342	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
343	Force	#9	(kips)	Real	12	0. ≤ X	0.
344	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
345	Force	#10	(kips)	Real	12	0. ≤ X	0.
346-349	Unused at	this ti	ime				

E-20

### Top Impact Limiter Curve for a 60-Degree Impact

Record	Descript	ion		Type I	ength	Restrictions	Default
350	Is this limite	r defii	ned?	List	1	Y or N	N
351	Deflection	#1	(in.)	Real	12 ·	POSITIVE	0.
352	Force	#1	(kips)	Real	12	POSITIVE	0.
353	Deflection	#2	(in.)	Real	12	POSITIVE	0.
354	Force	#2	(kips)	Real	12	POSITIVE	0.
355	Deflection	#3	(in.)	Real	12	0. ≤ X.	0.
356	Force	#3	(kips)	Real	12	0. ≤ X.	0.
357	Deflection	#4	(in.)	Real	12	0. ≤ X.	0.
358	Force	#4	(kips)	Real	12	0. ≤ X.	0.
359	Deflection	#5	(in.)	Real	12	0. ≤ X.	0.
360	Force	#5	(kips)	Real	12	0. ≤ X.	0.
361	Deflection	#6	(in.)	Real	12	0. ≤ X.	0.
362	Force	#6	(kips)	Real	12	0. ≤ X	0.
363	Deflection	<b>#7</b>	(in.)	Real	12	0. ≤ X	0.
364	Force	#7	(kips)	Real	12	0. ≤ X	0.
365	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
366	Force	#8	(kips)	Real	12	0. ≤ X	0.
367	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
368	Force	#9	(kips)	Real	12	0. ≤ X	0.
369	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
370	Force	#10	(kips)	Real	12	0. ≤ X	0.
371-374	Unused at	this ti	ime				

### Top Impact Limiter Curve for a 75-Degree Impact

Record	Descript	tion		Туре	Length	Restrictions	Default
375	Is this limit	er defi	ined?	List	1	Y or N	N
376	Deflection	#1	(in.)	Real	12	POSITIVE	0.
377	Force	#1	(kips)	Real	12	POSITIVE	0.
378	Deflection	#2	(in.)	Real	12	POSITIVE	0.
379	Force	#2	(kips)	Real	12	POSITIVE	0.
380	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
381	Force	#3	(kips)	Real	12	0. ≤ X	0.
382	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
383	Force	#4	(kips)	Real	12	0. ≤ X	0.
384	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
385	Force	#5	(kips)	Real	12	0. ≤ X	0.
386	Deflection	#6	(in.)	Real	12	•0. ≤ X	0.
387	Force	#6	(kips)	Real	12	0. ≤ X	0.
388	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
389	Force	#7	(kips)	Real	12	0. ≤ X	0.
390	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
391	Force	#8	(kips)	Real	12	0. ≤ X	0.
392	Deflection	#9	(in.)	Real	12	$0. \leq X$	0.
393	Force	#9	(kips)	Real	12	0. ≤ X.	0.
394	Deflection	#10	(in.)	Real	12	$0. \leq X$	0.
395	Force	#10	(kips)	Real.	12	$0. \leq X.$	0.
396-399	Unused a	t this	time				

Version: 1b

### Top Impact Limiter Curve for a 90-Degree Impact

Record	Descrip	tion		Туре	Length	Restrictions	Default
400	Is this limit	er def	ined?	List	ī	Y or N	N
401	Deflection	#1	(in.)	Real	12	POSITIVE	0.
402	Force	#1	(kips)	Real	12	POSITIVE	0.
403	Deflection	#2	(in.)	Real	12	POSITIVE	0.
404	Force	#2	(kips)	Real	12	POSITIVE	0.
405	Deflection	#3	(in.)	Real	12	0. ≤ X	0.
406	Force	#3	(kips)	Real	12	0. ≤ X	0.
407	Deflection	#4	(in.)	Real	12	0. ≤ X	0.
408	Force	#4	(kips)	Real	12	0. ≤ X	0.
409	Deflection	#5	(in.)	Real	12	0. ≤ X	0.
410	Force	#5	(kips)	Real	12	0. ≤ X	0.
411	Deflection	#6	(in.)	Real	12	0. ≤ X	0.
412	Force	#6	(kips)	Real	12	0. ≤ X	0.
413	Deflection	#7	(in.)	Real	12	0. ≤ X	0.
414	Force	#7	(kips)	Real	12	0. ≤ X	0.
415	Deflection	#8	(in.)	Real	12	0. ≤ X	0.
416	Force	#8	(kips)	Real	12	0. ≤ X	0.
417	Deflection	#9	(in.)	Real	12	0. ≤ X	0.
418	Force	#9	(kips)	Real	12	0. ≤ X	0.
419	Deflection	#10	(in.)	Real	12	0. ≤ X	0.
420	Force	#10	(kips)	Real	12	0. ≤ X	0.
421-424	Unused a	t this	time				

### Top Impact Limiter Curve for a C.G. Degree Impact

Record	Descrip	tion		Туре І	Length	Restrictions	Default
425	Is this limit	er defi	ined?	List	1	Y or N	N
426	Deflection	#1	(in.)	Real	12 P	OSITIVE	0.
427	Force	#1	(kips)	Real	12 P	OSITIVE	0.
428	Deflection	#2	(in.)	Real	12 P	OSITIVE	0.
429	Force	#2	(kips)	Real	12 P	OSITIVE	0.
430	Deflection	#3	(in.)	Real	12 0	), ≤ X	0.
431	Force	#3	(kips)	Real	12 0	. ≤ X	0.
432	Deflection	#4	(in.)	Real	12 0	), ≤ X	0.
433	Force	#4	(kips)	Real	12 0	). ≤ X	0.
434	Deflection	#5	(in.)	Real	12 0	). ≤ X	0.
435	Force	#5	(kips)	Real	12 0	). ≤ X	0.
436	Deflection	#6	(in.)	Real	12 0	). ≤ X	0.
437	Force	#6	(kips)	Real	12 0	). ≤ X	0.
438	Deflection	#7	(in.)	Real	12 0	). ≤ X	0.
439	Force	#7	(kips)	Real	12 0	). ≤ X	0.
430	Deflection	#8	(in.)	Real	12 0	. ≤ X	0.
441	Force	#8	(kips)	Real	12 0	. ≤ X	0.
442	Deflection	#9	(in.)	Real	12 0	). ≤ X	0.
443	Force	#9	(kips)	Real	12 0	). ≤ X	0.
444	Deflection	#10	(in.)	Real	12 0	. ≤ X	0.
445	Force	#10	(kips)	Real	12 0	). ≤ X	0.
446-450	Unused a	t this	time				

E-22

Version: 1b

### Finite Element Mesh Node Database

Purpose:Contains all Finite Element mesh nodes, all boundary specificationsUsed by:TOPAZ, SAPRESSCreated by:MSHDSPRecord Length:65

### NOTES:

- 1. Node/element lists are defined by number of first node/element, number of additional nodes/elements, and increment between nodes/elements.
- 2. Surface segment lists are defined by first node pair, number of additional segments and increment between node pairs.
- 3. Slideline surfaces defined by first node, last node, and increment between node identified by positive length of list. Slideline surfaces defined by list of nodes, separated by commas identified by negative length of list.
- 4. FORTRAN read/write format for each data item follows the description.

### <u>Header</u>

Record	Description [format]	
1	Casks Id. 'Scans geo'	[9a1]
2	Title	[65a1]
3	Date of Mesh Generation	[9a1]
4	Time of Mesh Generation	[9a1]
5	Geometry DB Basic Dimensions Filename	[12a1]

6-10 Unused at this time

### Node Control Data

Record	<b>Description</b> [format]	
11	Number of Nodes (thermal)	[ <i>i6</i> ]
12	Number of Nodes (stress)	[i6]

13-21 Unused at this time

### Appendix E

Program Reference

### Slide Line Control Data Data

Record	Description [format]	
22	Number of Slidelines	[i6]
23	Total Number of Slave Nodes	[i6]
24	Total Number of Master Nodes	[i6]
25	Number of Slave Nodes in Slideline 1	[i6]
26	Number of Master Nodes in Slideline 1	[i6]
26	Number of Slave Nodes in Slideline 2	[i6]
28	Number of Master Nodes in Slideline 2	[i6]

29 Unused at this time

### Boundary and Initial Conditions Control Data Data

Record	Description [format]	
30	Number of Elements with Heat Generation	[i6]
31	Number of Nodes with Non-Zero Temperature Initial Conditions	[i6]
32	Number of Nodes with Temperature Boundary Conditions	[i6]
33	Number of Cavity Boundary Segments	[ <i>i6</i> ]
34	Number of Outer Boundary Segments (Sections 2,3,4-Limiter)	[i6]
35	Number of Outer Boundary Segments (Section 2-Limiter Top )	[i6]
36	Number of Outer Boundary Segments (Section 3-Limiter Side)	[i6]
37	Number of Outer Boundary Segments (Section 4-Limiter Bot.)	[i6]
38	Number of Outer Boundary Segments (Section 5-H2OJkt. Side)	[i6]
39	Number of Outer Boundary Segments (Section 6-Limiter Bot. to shell)	[i6]
40	Number of Outer Boundary Segments (Sections 1->10-All Surf)	[i6]
41	Number of Outer Boundary Segments (Sections 2->10-Conv Surf)	[i6]
42	Number of Outer Boundary Segments (Sections 2->10-Rad Surf)	[i6]
43	Number of Outer Boundary Segments (Section 7-Limiter side to cask)	[ <i>i6</i> ]
44	Number of Outer Boundary Segments (Section 8-NS/WJ top to shell)	[i6]
45	Number of Outer Boundary Segments (Sections 9-NS/WJ top)	[ <i>i6</i> ]
46	Number of Outer Boundary Segments (Sections 10-Cask side)	[16]

47-50 Unused at this time

### Slideline No. 1 Node Description

Record	<b>Description</b> [format]	
51	First Slave Node	[i6]
52	Last Slave Node	[ <i>i6</i> ]
53	Increment between Slave Nodes	[ <i>i6</i> ]
54	List of Slave Nodes separated by commas	[65a]]
55	First Master Node	[ <i>i6</i> ]
56	Last Slave Node	[ <i>i6</i> ]
57	Increment between Master Nodes	[i6]
58	List of Master Nodes separated by commas	[65a1]

### Slideline No. 2 Node Description

59 First Slave Node	. [ <i>i6</i> ]
60 Last Slave Node	[i6]
61 Increment between Slave Nodes	[i6]
62 List of Slave Nodes separated by commas	[65a1]
63 First Master Node	[i6]
64 Last Slave Node	[i6]
65 Increment between Master Nodes	[i6]
66 List of Master Nodes separated by commas	[65a1]

### List of Elements With Heat Generation

Record	Description [format]	
67	First element	[i6]
68	Number of additional element	[i6]
69	Increment between elements	[i6]

### List of Nodes With Non-Zero Temperature Initial Conditions

Record	<b>Description</b> [format]	
70	First node	[ <i>i6</i> ]
71	Number of additional nodes	[ <i>i6</i> ]
72	Increment between nodes	[ <i>i6</i> ]

### List of Nodes Temperature Boundary Conditions

Record	<b>Description</b> [format]	
73	First node	[ <i>i6</i> ]
74	Number of additional nodes	[i6]
75	Increment between nodes	[i6]

### **Cavity Boundary Surface Segments**

, **-** -

Record	<b>Description</b> [format]	
76	Node A of First Surface Segment	[i6]
77	Node B of First Surface Segment	[i6]
78	Number additional segments defined	[i6]
79	Nodal increment between Node Pairs	[i6]

### Appendix E

### **Program Reference**

### Outer Boundary Surface Segments (Sections 2,3,4-Limiter)

Record	Description [format]	
80	Node A of First Surface Segment	[i6]
81	Node B of First Surface Segment	[i6]
82	Number additional segments defined	[i6]
83	Nodal increment between Node Pairs	[ <i>i6</i> ]

### Outer Boundary Surface Segments (Section 2-Limiter Top)

Record	Description [format]	
84	Node A of First Surface Segment	[i6]
85	Node B of First Surface Segment	[i6]
86	Number additional segments defined	[i6]
87	Nodal increment between Node Pairs	[i6]

### Outer Boundary Surface Segments (Section 3-Limiter Side)

Record	<b>Description</b> [format]	
88	Node A of First Surface Segment	[i6]
89	Node B of First Surface Segment	[ <i>i6</i> ]
90	Number additional segments defined	[i6]
91	Nodal increment between Node Pairs	[ <i>i6</i> ]

### Outer Boundary Surface Segments (Section 4-Limiter Bottom)

Record	<b>Description</b> [format]	
92	Node A of First Surface Segment	[ <i>i6</i> ]
93	Node B of First Surface Segment	[ <i>i6</i> ]
94	Number additional segments defined	[ <i>i6</i> ]
95	Nodal increment between Node Pairs	[ <i>i6</i> ]

### Outer Boundary Surface Segments (Section 5-Water Jacket Side)

Record	<b>Description</b> [format]	
96	Node A of First Surface Segment	[i6]
97	Node B of First Surface Segment	[i6]
98	Number additional segments defined	[ <i>i6</i> ]
99	Nodal increment between Node Pairs	[ <i>i6</i> ]

### Outer Boundary Surface Segments (Section 6-Limiter Bot. to shell)

Record	<b>Description</b> [format]	
100	Two nodes separated by a comma	[i3, 1x, i3]

### List of Inner Boundary Nodes With Pressure Conditions

Record	<b>Description</b> [format]	
101	First node	[i6]
102	Number of additional nodes	[i6]
103	Increment between nodes	[i6]

### List of Outer Boundary Nodes With Pressure Conditions

Record	<b>Description</b> [format]	
104	First node	[i6]
105	Number of additional nodes	[i6]
106	Increment between nodes	[ <i>i6</i> ]

### Outer Boundary Surface Segments (Section 7-Limiter Side to Cask Top)

Record	<b>Description</b> [format]	
107	Two nodes separated by a comma	[i3, 1x, i3]

### Outer Boundary Surface Segments (Section 8-NS/W.J Top to Shell)

Record	<b>Description</b> [format]	
108	Two nodes separated by a comma	[i3, 1x, i3]

### Outer Boundary Surface Segments (Section 9-NS/WJ Top)

Record	<b>Description</b> [format]	
109	Node A of First Surface Segment	[i6]
110	Node B of First Surface Segment	[i6]
111	Number additional segments defined	[i6]
112	Nodal increment between Node Pairs	[i6]

### Outer Boundary Surface Segments (Section 10-Exposed Cask Side)

Record	Description [format]	
113	Node A of First Surface Segment	[i6]
114	Node B of First Surface Segment	[i6]
115	Number additional segments defined	[i6]
116	Nodal increment between Node Pairs	[i6]
117-120	Unused	

### Nodal Description

Section Section

RecordDescription[format]121Node Coordinates (2 nodes per record for remainder of file)

i x(i) y(i) i+1 x(i+1) y(i+1) (each record) format [ ( i4, 1p2e14.7, 1x, i4, 2e14.7 ) ]

### Appendix E

Program Reference

### Finite Element Mesh Element Database

Purpose:Contains all Finite Element mesh elements for Thermal and Stress analyses, and<br/>contains names of materials for each cask componentUsed by:TOPAZ, SAPRESSCreated by:MSHDSPRecord Length:65

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### NOTES:

1. FORTRAN read/write format for each data item follows the description.

### <u>Header</u>

Record	Description [format]	
1	Casks Id. 'Scans geo'	[9a1]
2	Title	[65al]
3	Date of Mesh Generation	[9a1]
4	Time of Mesh Generation	[9a1]
5	Geometry DB Basic Dimensions Filename	[12a1]

6-10 Unused at this time

### Node Control Data

Record	Description [format]	
11	Number of Elements (stress) NELS	[i6]
12	Number of Elements (thermal) NELT	[i6]
13	Number of Materials	[i6]
14	Material No. 1 ID Shell inner layer	[8a1]
15	Material No. 2 ID Shell shield layer	[8a1]
16	Material No. 3 ID Shell outer layer	[8a1]
17	Material No. 4 ID End cap inner layer	[8a1]
18	Material No. 5 ID End cap shield layer	[8a1]
19	Material No. 6 ID End cap outer layer	[8al]
20	Material No. 7 ID Neutron shield	[8a1]
21	Material No. 8 ID Water jacket	[8al]
22	Material No. 9 ID Impact limiter	[8a1]

23-30 Unused at this time

### 4-Node Elements For Thermal Analyses

<b>Description</b> [format] 4-Node elements (2 per record)	[6i5,5x,6i5]
••	
	<b>Description</b> [format] 4-Node elements (2 per record)

en(n) m(n) i(n) j(n) k(n) l(n) en(n+1) m(n+1) i(n+1) j(n+1) k(n+1) l(n+1)

### 9-Node Elements For Stress Analyses

Record	<b>Description</b> [format]	
ii	9-Node elements (1 per record)	[11:5]

en(n) m(n) n1(n) n2(n) n3(n) n4(n) n5(n) n6(n) n7(n) n8(n) n9(n)

The start of 9-node elements (ii) is calculated as follows

ii = 31 + (NELT+1)/2

### Appendix E

### **Program Reference**

### Impact Analysis Plot Database

Purpose:Contains time history results for Impact AnalysisUsed by:PLTDYNCreated by:IMPACTRecord Length:36

### NOTES:

1. FORTRAN read/write format for each data item follows the description.

Maximum number of nodal variables (NVAR) is 8.
 If NVAR=3, variables are:

 (1) FORCE, (2) SHEAR, (3) MOMENT
 If NVAR=8, variables are:

 (1) FORCE, (2) SHEAR, (3) MOMENT, (4) PERM. LEAD SLUMP
 (5) AXIAL STRESS (inner shell), (6) AXIAL STRESS (outer shell)
 (7) HOOP STRESS (inner shell), (8) HOOP STRESS (outer shell)

### <u>Header</u>

Record	<b>Description</b> [format]	
1	Casks Id. 'Scans Imp'	[9a1]
2	Title	[36a1]
3	Title (continued)	[29a1]

### **Control Data**

Record	Description [format]	
4	Number of time states (NTS)	[2i5,f10.0,i5]
	Number of nodes (NNODE)	
	Length of Cask (CLEN)	
	Number of nodal variables per node (NVAR)	

### <u>Plot Variable Data</u> (repeat for each time state)

Record	<b>Description</b> [format]	
ii	Time, X(bottom),Y(bottom)	[ <i>3f</i> 12.0]
ii+1	Angle, X(top), Y(top)	[ <i>3f12.0</i> ]
ii+2	Node 1 Variables	[ <i>(3f12.0)</i> ]
jj	Node i Variables	[ <i>(3f12.0)</i> ]
	• • •	
kk	Node NNODE Variables	[ <i>(3f12.0)</i> ]

Start of time history for any node N: jj = 7 + (N-1)\*((NVAR+2)/3)Increment between time states for node: inc = 2 + NNODES\*((NVAR+2)/3)

### Thermal Analysis Plot Database

 Purpose:
 Contains Finite Element mesh elements for Thermal and Stress analyses. Also contains Thermal Analysis results (nodal temperatures)

 Used by:
 POSTPZ, SAPINPT

 Created by:
 TOPAZ

 Record Length:
 65

### NOTES:

- 1. FORTRAN read/write format for each data item follows the description.
- 2. Number of states is 2 for steady state and is greater than 2 for transient.
- 3. Maximum number of model global variables is 5.
- 4. Maximum number of material global variables is 5 for each material.
- 5. Maximum number of nodal distribution variables is 5.
- 6. Global variables can be maximums, minimums, averages, etc.

### <u>Header</u>

Record	d Description [format]	
1	Casks Id. 'Scans tpp'	[9a1]
2	Title	[65al]
3	Date of Analysis	[9a1]
4	Time of Analysis	[9a1]
5	Geometry DB Basic dimensions filename	[ <i>12a1</i> ]
6-10	Unused at this time	

### Control\_Data

Record	Description [format]	
11	Number of Nodes (thermal)	[ <i>i6</i> ] NODT
12	Number of Nodes (stress)	[ <i>i6</i> ] NODS
13	Number of Elements (thermal)	[ <i>i6</i> ] NELT
14	Number of Elements (stress)	[ <i>i6</i> ] NELS
15	Number of Materials	[ <i>i6</i> ] NMAT
16	Material No. 1 ID Shell inner layer	[ <i>a</i> 8]
17	Material No. 2 ID Shell shield layer	[ <i>a</i> 8]
18	Material No. 3 ID Shell outer layer	[ <i>a</i> 8]
19	Material No. 4 ID End cap inner layer	[a8]
20	Material No. 5 ID End cap shield layer	[ <i>a</i> 8]
21	Material No. 6 ID End cap outer layer	[ <i>a</i> 8]
22	Material No. 7 ID Neutron shield	[a8]
23	Material No. 8 ID Water jacket	[ <i>a</i> 8]
24	Material No. 9 ID Impact limiter	[ <i>a</i> 8]

### <u>Control Data</u> (continued)

Kecord	Description [formal]	
25	Unused at this time	
26	Number of Time States	[ <i>i6</i> ] NTS
27	Maximum time of analysis	[f12.0]
28	Maximum temperature, state number, time	[f12.0,i6,f12.0]
29	Minimum pressure, state number, time	
	Maximum pressure, state number, time	[2(f12.0,i6,f12.0)]
30	Number of Model Global Variables	[ <i>i6</i> ] NUMGV
31	Number of Material Global Variables	[ <i>i6</i> ] NUMMV
32	Number of Nodal Distribution Variables	[ <i>i6</i> ] NUMNV
33	Unused at this time	

### Variable Descriptors

Record	<b>Description</b> [format]	
34	Time Descriptor and units	[2a12]
35	Length Descriptor and units	[2a12]
36	Model Global Var 1 Descriptor/units	[2a12]
37	Model Global Var 2 Descriptor/units	[2a12]
38	Model Global Var 3 Descriptor/units	[2a12]
39	Model Global Var 4 Descriptor/units	[2a12]
40	Model Global Var 5 Descriptor/units	[2a12]
41	Material Global Var 1 Descriptor/units	[2a12]
42	Material Global Var 2 Descriptor/units	[2a12]
43	Material Global Var 3 Descriptor/units	[2a12]
44	Material Global Var 4 Descriptor/units	[2a12]
45	Material Global Var 5 Descriptor/units	[2a12]
46	Nodal Variable 1 Descriptor/units	[2a12]
47	Nodal Variable 2 Descriptor/units	[2a12]
48	Nodal Variable 3 Descriptor/units	[2a12]
49	Nodal Variable 4 Descriptor/units	[2a12]
50	Nodal Variable 5 Descriptor/units	[2a12]

### Nodal Description

Record	Description [format]	
51	Node Coordinates (2 nodes per record)	
	i x(i) y(i) i+1 x(i+1) y(i+1) (each record)	

### [*i*4,2*f*14.0,1*x*,*i*4,2*f*14.0]

### 4-Node Elements for Thermal Analyses

RecordDescription [format]ii4-Node elements (2 per record)[6i5,5x,6i5]en(n) m(n) i(n) j(n) k(n) l(n)<br/>en(n+1) m(n+1) i(n+1) j(n+1) k(n+1) l(n+1)The start of 4-node elements (ii) is calculated as follows:<br/>ii = 51 + (NODT+1)/2

### 9-Node Elements for Thermal Stress Analyses

RecordDescription [format]jj9-Node elements 1 element per record [11i5]en(n) m(n) n1(n) n2(n) n3(n) n4(n) n5(n) n6(n) n7(n) n8(n) n9(n)

The start of 9-node elements (jj) is calculated as follows: jj = ii + (NELT+1)/2

<u>Plot Variable Data</u> (repeat for each time state)

Record kk	Description Time for state	[format] [f12.0]
·	The start of state dat kk = jj + N	a is calculated as follows: ELS
11	NUMGV model glol Model Variable Model Variable	val variables 1 per record $[f/2.0]$ 1 = Maximum temperature 2 = Maximum pressure
	The start of model g ll = kk + 1	lobal variables is calculated as follows:
' mm	NUMMV material g Each material v Number of reco	lobal variables [5f12.0] ariable is entered for all materials rds for each variable is (NMAT+4)/5
	The start of material mm = kk +	global variables is calculated as follows: 1 + NUMGV
nn	NUMNV nodal varia Nodal Variable Nodal Variable Nodal Variable	bles 5 nodes per record [5f12.0] 1 = Nodal temperature 2 = Nodal flux in global X direction 3 = Nodal flux in global Y direction
	The start of a nodal $nn = kk + 1$ where N	variable is calculated as follows: + NUMGV + NUMMV*(NMAT+4)/5 + (NV-1)*(NODT+4)/5 / is the nodal variable number
Length	of state is calculated as	s follows:

LEN = 1 + NUMGV + NUMMV\*(NMAT+4)/5 + NUMNV\*(NODT+4)/5

### **Description of Editor Templates**

.

The CASKS editor uses a *template* to describe the editor pages and how data values are saved in the data sets. The *template* is a *random access* ASCII file. It is divided into three sections: control information, page headers, and descriptions of each editor page. The record length for the *template* is 150. The format of the *template* and the function of *template* parameters are described below.

### **Control Information**

Record	Description	[format]
1	Casks Id 'Scans edt'	[9a1]
2	Name of the Templat	te [65a1]
3	Date of last modifica	tion [20a1]
4	RECTOT, PAGTOT	, TRECL, MAXREC, RECLN [5i6]
	where RECTOT	= Number of records in the template file
	PAGTOT	= Number of editor pages
	TRECL	= Template file record length (unused)
	MAXREC	= Number of records to create in data file
	RECLN	= Data file record length
5	FORTRAN read forr	mat for body of template [al27]

### Page Headers

Record	Variable	Columns	Format	Comments
6	HDPGNO	1-3	I3	Sequential page number (unused)
	PAGNUM	5-7	A3	Page number displayed with editor page
	PGNAME	9-53	A45	Page identification line (end with ))
	NPRECS	55-57	13	Number of records used to describe this page (If NPRECS<0, then this editor page is a copy of page IABS(NPRECS))
	PGACC	70	A1	Page access flag (reported in data file header) (Y=page always on, otherwise toggle A=on, N=off)
	PGREQ	72	A1	Required access flag (reported in data file) (R=page must be accessed, O=optional access)
	CBYPGN	74-75	12	Page which has data which controls this page $(0=this page not controlled by another)$
	CBYRCN	77-78	12	Record on page CBYPGN which controls this page
	CPON	80	A1	Character which defines page accessibility if record CBYRCN is character type and data is CPON
	IPON	82-83	12	Number which defines page accessibility if record CBYRCN is integer type and data $\geq$ IPON
	GRCOFF	85-87	13	Global record offset in data file added to the data global record if page is copy (NPRECS<0)
	FL10FF	89-91	13	1st default file data offset for copy pages
	FL1EXT	93-95	A3	1st default file extension to use FL10FF
	FL2OFF	89-91	13	2nd default file data offset for copy pages
	FL2EXT	93-95	A3	2nd default file extension to use FL2OFF

Repeat record 6 for each editor page (PAGTOT)

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### Description of Editor Pages

Record	Variable	Columns 1	Format	Comments
ii	NPG	1-2	12	Page number (reference only)
	NLINE	4-5	12	Description line number (reference only)
	GRBASE	6-9	I3	Global record in data file for data item
				(0=description line on screen is comment,
				GRCOFF is added to GRBASE if page is copy)
	REODAT	11	A1	Is this required data? (must be filled in)
				(Y=ves, display cyan; N=no, display green)
	CNTRL	13	A1	Control flag for displaying rest of page
	-			If CNTRL=blank and DTYPE=C or L, then if
				data item matches CNTRL rest of rage is avail.
	LROW	15-16	12	Row to display description (3 to 21)
	LCOL	18-19	12	Column to display description (0 to 65)
	LABEL	21-94	A74	Data item description (must end with ))
	DTYPE	96	A1	Data item type
				''(blank) = comment, not a data item
				'c' = Character string
				n' = Data item selected from name list
				I' = Single character which must match list
				'i' = Integer number
				'r' = Real number
	DLEN	98-99	12	Length of data item field
	DROW	101-102	12	Row for data item field (0=use LROW) (3-21)
	DCOL	104-105	12	Column for data item field (0-70)
	NUMCHK	107-108	A2	Numeric data item validation requirement
				' ' (blank) = No checking
				'NC' = No checking
				'GT' = must be greater than NUM1
				'LT' = must be less than NUM1
				GE' = must be greater than or equal to NUM1
				'LE' = must be less than or equal to NUM1
				'RG' = must be in range NUM1 to NUM2 inclusive
				'PS' = must be positive
				'ER' = must be even and in range NUM1 to NUM2
				NOTE: NUM1 and NUM2 are contained in CHK
	CHK	110-130	var	For DTYPE='l' list of appropriate characters
				(end list with a blank character)
				For DTYPE='i' or 'r' NUM1 and NUM2 are in CHK
				READ ( CHK, 'f10.0,1x,f10.0' ) NUM1,NUM2
				For DTYPE='n' mask for file names (i.e. '*.mat')
	DFLT	131-145	var	For DTYPE='c', 'l' or 'n' default characters
				For DTYPE='i' or 'r' numeric default is in CHK
				READ (CHK, 'f10.0') RDVAL
	DFLTRC	147-150	I4	Record in default data file to find default value
				0 = default is specified as DFLT in template
				>0 = default data file name is in DFLT and
				DFLTRC is record number in default data file

Repeat record ii for each line describing the editor page (NPRECS) Repeat the set of records for each editor page (PAGTOT)

Scans get											
Template for	SCANS basic geometry										
06/23/88 at	1:12pm by Hichael A. Gerhard										
143 16	163 230 12										
(bn,5x,14,2(1	x,a1),2(1x,i2),1x,a74,1x,a1,3(1x,i2),1x	,82,1x,821,1x,	a14,1x,	, 14)	)						
11 Gene	ral SAR Information	\ 11	YR	0	0						
22 Revi	ewer Information	\ 4	ΥO	0	0						
3 3 Cask	Cavity/Contents Specifications	13	YR	0	0						
4 4 Cask	Component Configurations	\ 9	YO	0	0						
5 5a Cask	Shell Specifications (SOLID)	5	H R	4	1 S						
6 5b Cask	Shell Specifications (LAHIHATED)	14	NR	4	1 L						
76a Cask	Top End Cap Specifications (SOLID)	6	YNR	4	3 S						
8 6b Cask	Top End Cap Specifications (LAMINATED)	13	YNR	4	3 L						
9 7a Cask	Bottom End Cap Specifications (SOLID)	•7	YNR	4	5 S	15					
10 7b Cask	Bottom End Cap Specs (LAMINATED)	-8	YNR	4	5 L	15					
11 8 Cask	Closure Bolts Information	3	YR	0	0						
12 9 CASK	Neutron Shield / Water Jacket Specs	. 8	NR	4	9 Y						
13 10 CASK	Top Impact Limiter Specifications	. 8	YNR	4	74						
14 11 CASK	Bottom Impact Limiter Specifications	-13	THR	4	81	10					
15 12 Cask	Impact Hodel Specifications	18	YO	0	0						
16 12 Ther	T a control params	10	ЮК	U	U						
1 1 40 K	S U SAR TITLE						C 24	14			
1 2 53	5 U SAR docket number						c /	5 29			
1 3 51	5 40 SAR report number						c 12	5 65			
1 4 54	7 0 SAR docket start date						c 8	7 29			
1 5 52	7 40 SAR report date\						c 8	7 65			
1 6 55	9 0 Add. info						c 54	14			
1 7 60	11 0 Add. info						c 54	14			
1 8 65	13 0 Add. info\						c 54	14			
1 9 70	15 0 Comp addr\						c 54	14			
1 10 75	17 0 Comp addr\						c 54	14			
1 11 80	19 0 Comp addr\						c 54	14			
2 1 85	3 O Cask review leader name\						c 24	35			
2 2 87	5 O Thermal analyst name\						c 24	35			
2 3 89	7 O Structural analyst name\						c 24	35			
2 4 91	9 O Nucleonics analyst name\						c 24	35			
3 1 101 R	3 O Cavity inner radius (in.)\						r 12	58 RG .001	2000.	0.0	
3 2 103 R	4 O Cavity length (in.)\						r 12	58 RG .001	2000.	0.0	
3 3 100 R	6 O Gross weight of package (lbs)						r 12	58 PS		0.0	
3 4 105 R	7 O Weight of contents / internals (l	bs)\					r 12	58 PS		0.0	
3 5 106	9 O Maximum heat generation rate of c	contents (Btu/n	nin)\				r 12	50 GE U.	500	14.7	
3 6 107	11 O Initial cavity charge pressure (p						r 12	50 KU U.	300.	70	
3 7 108	12 0 Initial cavity charge temperature	(deg.F)\					r 14	- JO KG - 100.	500.		

**Basic Geometry Template** 

3 8 109	13 O Maximum normal operating pressure	(psia)	r 12	58 RG O.	2000.	14.7	0
3 9 110	15 0 Temperature defining stress free	condition (deg.F)\	r 12	58 RG -100.	300.	70.	0
3 10 0	17 0 (Include the following to define a	2-D finite-element mesh)\					0
3 11 0	18 0 (Hesh divisions must	be even)\					0
3 12 102	20 O Number of mesh divisions along ca	vity inner radius\	i 2	58 ER 2.	20.	6.	0
3 13 104	21 O Number of mesh divisions along ca	vity half length\	12	58 ER 2.	40.	8.	0
4 1 111	3 0 Shell configuration\		ι 1	36 SL		S	0
420	4 0 [S=solid, L=laminated]\						0
4 3 112	6 0 Top end cap configuration\		ι 1	36 SL		S	0
440	7 0 [S=solid, L=laminated]\						0
4 5 1 1 3	9 0 Bottom end cap configuration\		ι 1	36 SL		S	0
460	10 0 [S=solid, L=laminated]\						0
4 7 114	13 O is Top impact limiter present?	[Y/H] \	11	55 YN		Y	0
4 8 115	15 0 Is Bottom impact limiter present?	[Y/H] \	ι 1	55 YN		Y	0
4 9 116	17 O is Neutron shield / water jacket p	present? [Y/H]\	L 1	55 YN		Y	0
5 1 121 R	3 0 Shell thickness (in.)		r 12	32 RG .001	2000.	0.	0
5 2 122	5 0 Shell material name\		n 8	32 •.stm		SS304	0
530	10 0 (Include the following to define 2	-D finite-element mesh)\					0
540	11 0 (Hesh divisions must b	e even)\					0
5 5 123	13 O Number of mesh divisions through s	hell\	i 2	46 ER 2.	10.	4.	0
6 1 124 R	3 O Shell inner layer thickness (in.)	۸	r 12	52 RG 0.	2000.	0.	0
6 2 134	4 0 Additional thickness at end cap i	nterface (in.)\	r 12	52 RG 0.	2000.	0.	0
6 3 125	5 O Shell inner layer material name\		n 8	52 *.stm		SS304	0
6 4 127 R	7 0 Shell shield layer thickness (in.)	۸	r 12	52 RG 0.	2000.	0.	0
6 5 128 R	8 0 Shell shield length (in.)\		r 12	52 RG O.	2000.	0.	0
6 6 129	9 O Shell shield layer material name\		n 8	52 *.shm		LEAD	0
6 7 131 R	11 O Shell outer layer thickness (in.)	۸ · ·	r 12	52 RG .001	2000.	0.	0
6 8 135	12 O Additional thickness at end cap is	nterface (in.)\	r 12	52 RG O.	2000.	0.	0
6 9 132	13 O Shell outer layer material name\		n 8	52 *.stm		SS304	0
6 10 0	16 0 (Include the following to define 2	-D finite-element mesh)\					0
6 11 0	17 0 (Hesh divisions must b	e even)\					0
6 12 126	19 O Number of mesh divisions through si	hell inner tøyer\	í 2	62 ER 2.	10.	2.	0
6 13 130	20 O Number of mesh divisions through s	hell shield layer\	12	62 ER 2.	10.	4.	0
6 14 133	21 O Number of mesh divisions through s	hell outer layer\	12	62 ER 2.	t0.	2.	0
7 1 136 R	3 0 End cap thickness (in.)\		r 12	31 RG .001	2000.	0.	0
7 2 137	5 O End cap material name\		n 8	31 *.stm		SS304	0
730	10 O (Include the following to define 2	-D finite-element mesh)\					0
740	11 0 (Hesh divisions must b	e even)\					0
7 5 138	13 O Number of mesh divisions through end	nd cap\	i 2	45 ER 2.	10.	4.	0
760	19 0 Press F10 to copy data from othe	r end cap (if it is SOLID)\					0
8 1 139 R	3 0 End cap inner layer thickness (in)	N	r 12	44 RG 0.	2000.	0.	0
8 2 140	4 0 End cap inner layer material name\		n 8	44 *.stm		SS304	0
8 3 142 R	6 0 End cap shield layer thickness (in	.)\	г 12	44 RG 0.	2000.	0.	0
8 4 143 R	7 O End cap shield layer radius (in.)		r 12	44 RG 0.	2000.	0.	0
8 5 144	8 0 End cap shield layer material name	Ν	n 8	44 <b>".</b> shm		LEAD	U

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Basic Geometry Template continued

Appendix E Program Reference

Version: 1b E-37

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8 6 146 R	10 0 End cap outer layer thickness (in.)\	r 12 44 RG .001	2000. 0.	0
8 7 147	11 0 End cap outer layer material name\	n 8 44 *.stm	\$\$ <b>3</b> 04	0
880	13 0 (Include the following to define 2-D finite-element mesh)			0
890	14 0 (Hesh divisions must be even)			0
8 10 141	16 O Number of mesh divisions through end cap inner layer\	i 2 61 ER 2.	10. 2.	0
8 11 145	17 O Number of mesh divisions through end cap shield layer\	i 2 61 ER 2.	10, 4,	0
8 12 148	18 O Number of mesh divisions through end cap outer layer\	i 2 61 ER 2.	10. 2.	0
8 13 0	21 0 Press F10 to copy data from other end cap (if it is LAHINATED) $\$			0
11 1 169 R	3 O Number of closure bolts\	i 2 50 RG 1.	99. 0.	0
11 2 170 R	5 0 Diameter of closure bolts (in.)\	r 12 50 RG .001	10. 0.	0
11 3 168 R	7 O Closure bolt circle radius (in.)	r 12 50 RG .001	2000. 0.	0
12 1 176 R	3 O Heutron shield/waterjacket length (in.)\	r 12 52 RG 0.	2000. 0.	0
12 2 177 R	5 0 Heutron shield thickness (in.)	r 12 52 RG D.	2000. 0.	0
12 3 178	6 O Neutron shield material name	n 8 52 *.nsm	HZOCONV	0
12 4 180 R	8 O Water jacket thickness (in.)	r 12 52 RG 0.	2000. 0.	0
12 5 181	9 O Water jacket material name	n 8 52 *.µjm	\$\$304	0
12 6 0	14 O (Include the following to define 2-D finite-element mesh)			0
12 7 179	16 O Humber of mesh divisions through neutron shield	i 2 55 RG 1.	9. 1.	0
12 8 182	17 O Humber of mesh divisions through water jacket	i 2 55 RG 1.	9. 1.	0
13 1 186 R	3 0 Impact limiter radius (in.)	r 12 50 RG .001	2000. 0.	0
13 2 187 R	5 0 Impact limiter center line thickness (in.)	r 12 50 RG .001	2000. 0.	Ο,
13 3 189 R	7 0 Impact limiter overhang thickness (in.)	r 12 50 RG 0.	2000. 0.	0
13 4 191	9 0 Impact limiter material name\	n 8 50 *.ilm	POLYFOAH	ı 0
13 5 0	12 0 (Include the following to define 2-D finite-element mesh)			0
13 6 188	14 O Humber of mesh divisions through limiter CL thickness\	i 2 63 RG 1.	10. 4.	0 🕨
13 7 190	16 O Number of mesh divisions through limiter overhang width\	1 2 63 RG 1.	10. 3.	0
13 8 0	20 O Press F10 to copy data from other impact limiter\			0
15 1 206	3 O Number of elements for 1-D impact model\	i 2 47 RG 3.	20. 4.	0
15 2 207	4 G TOP Impact limiter weight (lbs)	r 12 47 GE 0.	0.	0
15 3 208	5 0 BOTTOH Impact limiter weight (lbs)\	r 12 47 GE O.	0.	0
15 4 0	6 0 (If omitted, weights are calculated based on volume and density)			0
15 5 209 Y	8 O Define impact model with user specified properties? [Y/H]\	L1 65 YH	н	0
15 6 0	9 0 NOTE - Weight of contents must be defined (Page 3)\			0
15 7 0	0 0 No stress recovery is available for user defined casks\			0
15 8 210 R	1 5 Shell translational mass (lb-sec**2/in)\	r 12 57 PS	0.	0
15 9 211 R	2 5 Shell rotational mass (lb-sec**2-in)\	r 12 57 PS	0.	0
15 10 212 R	3 5 Shell inside length (in.)	r 12 57 PS	0.	0
15 11 213 R	14 5 Shell E*1 (lb-in**2)\	r 12 57 PS	0.	0
15 12 214 R	15 5 Shell A*E (lb)\	r 12 57 PS	0.	0
15 13 220 R	6 5 Shell composite Poisson's Ratio\	r 12 57 PS	0.	0
15 14 215 R	<pre>i7 S Top end translational mass (lb-sec**2/in)\</pre>	r 12 57 PS	0.	0
15 15 216 R	18 5 Top end rotational mass (ib-sec**2-in)\	r 12 57 PS	0.	0
15 16 217 R	9 5 Bottom end translational mass (lb-sec**2/in)\	r 12 57 PS	0.	0
15 17 218 R	20 5 Bottom end rotational mass (lb-sec**2-in)\	r 12 57 PS	0.	0
15 18 219 R	21 5 Characteristic cross-section width (in)\	r 12 57 PS	0.	0

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Basic Geometry Template continued

E-38 Version: 1b

16 1 221	3 O Allow phase change? [Y/H]\	L 1 57 YN		R
16 2 222	5 0 Time between printed output (min.)	r 12 57 RG 10.	360.	30.
16 3 223	6 0 Time between plotted output (min.)\	r 12 57 RG 2.	30.	5.
16 4 224	8 O Use variable time step? [Y/H]\	L 1 57 YH		۲
16 5 225	10 0 Iteration convergence tolerance\	r 12 57 RG .001	.1	.001
16 6 226	11 0 Iteration relaxation parameter	r 12 57 RG .3	1.	1.
16 7 227	13 O Maximum allowable time step for variable TS (min.)\	r 12 57 RG 5.	30.	30.
16 8 228	14 O Haximum temperature change per time step (F)\	r 12 57 RG 25.	100.	100.
16 9 229	15 O Time step modification factor for variable TS\	r 12 57 RG 2.	6.	2.
16 10 230	17 O Fixed time step size for fixed TS (min.)	r 12 57 RG .25	5.	.5

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Scans lmt Template file for LIMITER editor 05/05/88 at 4:47pm by Hichael Gerhard 56 17 150 450 12 (bn,5x,i4,2(1x,a1),2(1x,i2),1x,a74,1x,a1,3(1x,i2),1x,a2,1x,a21,1x,a14,1x,i4) 1 0 Impact Limiter Unloading Specification \ 8 Y C 2 1a Bottom Impact Limiter for 0 degree impact \ 26 Y Y C 0 3 1b Bottom Impact Limiter for 15 degree impact \ -2 Y Y C 25 4 1c Bottom Impact Limiter for 30 degree impact \ -2 Y Y C 50 5 1d Bottom Impact Limiter for 45 degree impact \ -2 Y Y C 75 4 1c Bottom Impact Limiter for 645 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 69 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 degree impact \ -2 Y Y C 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bottom Impact Limiter for 75 5 1d Bott				Impact	Appendix Program Referen
7 IfBottom Impact Limiter for 75 degree impact \ -2Y Y C1258 1gBottom Impact Limiter for 70 degree impact \ -2Y Y C1509 1hBottom Impact Limiter for C.G. impact \ -2Y Y C17510 2aTop Impact Limiter for 0 degree impact \ -2Y Y C20011 2bTop Impact Limiter for 15 degree impact \ -2Y Y C22512 2cTop Impact Limiter for 30 degree impact \ -2Y Y C22512 2cTop Impact Limiter for 45 degree impact \ -2Y Y C25013 2dTop Impact Limiter for 60 degree impact \ -2Y Y C27514 2eTop Impact Limiter for 75 degree impact \ -2Y Y C30015 2fTop Impact Limiter for 76 degree impact \ -2Y Y C32516 2gTop Impact Limiter for 90 degree impact \ -2Y Y C35017 2hTop Impact Limiter for C.G. impact \ -2Y Y C35017 2hTop Impact Limiter for C.G. impact \ -2Y Y C3750 142Select the slope of the unloading path for impact Limiters\0 264CUloading slope is maximum slope of Limiter \0 374NNo elastic recovery of impact Limiter\				Limiter Force-Deflectio	ice E
<ul> <li>6 4 8 4 (Approximated by Unloading slope of 5 times max slope of curve)</li> <li>7 49 8 13 Type of Impact Limiter Unloading slope</li> <li>6 48 U 11 3 Type of Impact Limiter Unloading No</li> <li>7 49 8 13 3 User specified unloading slope (kips/inch)</li> <li>8 15 4 Unloading slope is KIPS of unloading per inches elastic recovery</li> <li>1 3 0 Press F10 to copy Force/Deflection data from another impact angle</li> <li>2 5 0 Impact angle is defined as follows: SIDE impact angle is 0.\</li> <li>1 3 6 0 END ON impact angle is 90.\</li> <li>1 4 50 Y 8 0 Do you wish to define a Deflection/Force curve for this angle 7 (Y/N)</li> <li>1 5 10 13 You must define at least 2 deflection/force pairs\</li> <li>1 4 0 eflection #0 (in) .0 Force #0 (kips) .0</li> </ul>	l 1 r 12 l 1	50 UNC 50 PS 77 YN	N O. N	n Curves Templa	
1       6       11       4       Deflection #0 (th)       10       Force #0 (kips)         1       7       51 R       12       4       Deflection #1 (in)\         1       8       52 R       12       45       Force #1 (kips)\         1       9       53 R       13       4       Deflection #2 (in)\         1       10       54 R       13       45       Force #2 (kips)\         1       11       55       14       4       Deflection #3 (in)\         1       12       56       14       45       Force #3 (kips)\         1       13       57       15       4       Deflection #4 (in)\	r 12 r 12 r 12 r 12 r 12 r 12 r 12 r 12	27 PS 65 PS 27 PS 65 PS 27 GE 0. 65 GE 0. 27 GE 0.	0. 0. 0. 0. 0. 0.	o o o o o o	

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1 14	58	15 45 Force #4 (kips)\	r 12	65 GE 0.	0.	٥
1 15	59	16 4 Deflection #5 (in)\	r 12	27 GE 0.	0.	0
1 16	60	16 45 Force #S (klps)\	r 12	65 GE 0.	0.	ň
1 17	61	17 4 Deflection #6 (in)\	r 12	27 GE 0.	0.	0
1 18	62	17 45 Force #6 (kips)\	r 12	65 GE 0.	0.	ů
1 19	63	18 4 Deflection #7 (in)\	r 12	27 GE 0.	0.	0
1 20	64	18 45 Force #7 (kips)\	r 12	65 GE 0.	0.	n n
1 21	65	19 4 Deflection #8 (in)\	r 12	27 GE 0.	0.	0
1 22	66	19 45 Force #8 (kips)\	r 12	65 GE 0.	0.	ů
1 23	67	20 4 Deflection #9 (in)	· r 12	27 GE 0.	0.	n n
1 24	68	20 45 Force #9 (kips)\	r 12	65 GE 0.	0.	0
1 25	69	21 4 Deflection #10 (in)\	r 12	27 GE 0.	0.	ů
1 26	70	21 45 Force #10 (kips)\	r 12	65 GE 0.	0.	0
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Appendix E Program Reference

Impact Limiter Force-Deflection Curves Template continued

Version: 1b E=41

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Scans (ce				
Template file for SURFACE editor				
10/20/92 at 4:40pm by T. F. Chen				
56 17 150 450 12				
(bn, 5x, i4, 2(1x, a1), 2(1x, i2), 1x, a74, 1x, a1, 3(1x, i2), 1x, a2, 1x, a21, 1x, a14, 1x, i4)				
1 0 Impact Surface Unloading Specification \ 8 Y C				Y
2 1a User Input Impact Surface F/D Curve CASE 1 \ 26 Y Y C 0				e
3 1b User Input Impact Surface F/D Curve CASE 2 \ -2 YYC 25				Id
4 1c User Input Impact Surface F/D Curve CASE 3 \ -2 Y Y C 50				· 🚡
5 1d User Input Impact Surface F/D Curve CASE 4 \ -2 YYC 75				an c
6 le User Input Impact Surface F/D Curvo CASE 5 \ -2 YYC 100				• 1
7 1f User Input Impact Surface F/D Curve CASE 6 \ -2 Y Y C 125				S
8 1g User Input Imapct Surface F/D Curve CASE 7 \ -2 Y Y C 150				
9 1h User Input Impact Surface F/D Curve CASE 8 \ -2 YYC 175				÷
10 2a User Input Impact Surface F/D Curve CASE 9 \ -2 YYC 200				36
11 2b This CASE reserved for future use \ -2 YYC 225				ē
12 2c This CASE reserved for future use \ -2 YYC 250				H-1
13 2d This CASE reserved for future use \ -2 YYC 275				õ
14 2e This CASE reserved for future use \ -2 YYC 300				7
15 2f This CASE reserved for future use \ -2 YYC 325				ce
16 2g This CASE reserved for future use \ -2 YYC 350				
17 2h This CASE reserved for future use \ -2 YYC 375				$\sim$
0 1 4 2 Select the slope of the unloading path for impact surface \				°Ě
0 2 6 4 C Unloading slope is maximum slope of F/D curve				• e
0 3 7 4 N No elastic recovery of F/D curves \				• <del>C</del>
0 4 8 4 (Approximated by unloading slope of 5 times max slope of curve)				° 0
0 5 9 4 U User specified unloading slope				° 5
0 6 48 U 11 3 Type of Impact surface Unloading	1 1	50 UNC	N	0
0 7 49 R 13 3 User specified unloading slope (kips/inch)\	r 12	50 PS	0.	ο <u>Ω</u>
0 8 15 4 Unloading slope is KIPS of unloading per inches elastic recovery				• 1
1 1 3 0 Press F10 to copy Force/Deflection data from another impact CASE \				• 4
1 2 5 0				° 63
1 3 6 0				0
1 4 50 Y 8 0 Do you wish to define a Deflection/Force curve for this CASE 7 $(Y/N)$	1 1	77 YN	N	• 1
1 5 10 13 You must define at least 2 deflection/force pairs\				· · · · · ·
1 6 11 4 Deflection #0 (in) .0 Force #0 (kips) .0\				° D
1 7 51 R 12 4 Deflection #1 (in)	r 12	27 PS	0.	° pi
1 8 52 R 12 45 Force #1 (kips)\	r 12	65 PS	0.	ଂ ମୁ
1 9 53 R 13 4 Deflection #2 (in)	r 12	27 PS	0.	° e
1 10 54 R 13 45 Force #2 (kips)\	r 12	65 PS	0.	0
1 11 55 14 4 Deflection #3 (in)\	r 12	27 GE 0.	0.	0
1 12 56 14 45 Force #3 (kips)\	r 12	65 GE 0.	0.	0
1 13 57 15 4 Deflection #4 (in)	r 12	27 GE 0.	0.	0

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1 14	58	15 45 Force #4 (kips)\	r 12	65 GE 0.	0.
1 15	59	16 4 Deflection #5 (in)\	r 12	27 GE 0.	0.
1 16	60	16 45 Force #5 (kips)\	r 12	65 GE 0.	0.
1 17	61	17 4 Deflection #6 (in)	r 12	27 GE 0.	0.
1 18	62	17 45 Force #6 (kips)\ .	r 12	65 GE 0.	0.
1 19	63	18 4 Deflection #7 (in)	r 12	27 GE 0.	0.
1 20	64	18 45 Force #7 (kips)\	r 12	65 GE 0.	0.
1 21	65	19 4 Deflection #8 (in)	r 12	27 GE 0.	0.
1 22	66	19 45 Force #8 (kips)\	r 12	65 GE 0.	0.
1 23	67	20 4 Deflection #9 (in)\	r 12	27 GE 0.	0.
1 24	68	20 45 Force #9 (kips)\	r 12	65 GE 0.	0.
1 25	69	21 4 Deflection #10 (in)	r 12	27 GE 0.	0.
1 26	70	21 45 Force #10 (kips)\	r 12	65 GE 0.	0.

Yielding Surface Force-Deflection Curves Template continued

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4.4a Temperature 1 Properties \ 6	HR 3 1 1							re 🗙
5 4b Temperature 2 Properties \ -4	NR 3 1 2 10							n
6 4c Temperature 3 Properties V -4	NR 3 1 3 20							e j
7 4d Temperature 4 Properties \ -4	HR 3 1 4 30						7	
8 4e Temperature 5 Properties \ -4	NR 3 1 5 40						A	-
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12 4h Dummy page for hidden properties \ 11	NOOO						<u> </u>	
1 1 46 R 4 U Material name		c 24	45			0	Р	
1 2 51 R 6 0 Density (10m/in.**3)		r 12	45 PS		.1	0	ro	
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2 $2$ $3$ $3$ $3$ $3$ $1$ impact Poisson's Ratio	ine and buckling)	r 12	45 KG .001	.499	.3	0	er	
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2 6 56 11 0 Ultimate stress (psi)		r 12	45 GE 0.		0.0	0	. 1	
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2 8 14 0 to and m define the stress-strain relation a	t stress levels\					0	Ë	
2 9 15 0 above the proportional stress limit accordin	g to 1 = 10 • Y**m\					0	di di	•
2 10 57 17 0 Proportional stress limit (psi)		r 12	45 GE 0.		0.0	0	la	
2 11 58 18 0 lo (psi)\		r 12	45 GE 0.		0.0	0	te	
2 12 59 19 0 m		г 12	45 GE 0.		0.0	0		
3 1 66 R 4 O Number of temperature sets (max is 8)\		i 1	45 RG 1.	8.	1.	0		
3 2 65 6 O Material type (Only type 3 is available)\		F 1	45 RG 3.	3.	3.	0		
4 1 71 R 4 O Temperature (F)\		r 12	45 GE -459.		0.0	0		
4 2 72 R 6 0 Young's Modulus (psi)\		r 12	45 PS		1.	0		
4 3 73 R 7 O Poisson's Ratio\		r 12	45 RG .001	.499	.3	0		
4 4 74 8 O Coefficient of thermal expansion (in./in.F)		r 12	45		0.	0		
4 5 75 10 O Thermal conductivity (Btu/in.min F)\		r 12	45 PS		1.	0		
4 6 76 11 O Specific heat capacity (Btu/lbm F)\		r 12	45 PS		1.	0		
12 1 61 4 O Helt Temperature (F)\		r 12	45 GE -459.		10000.	0		
12 2 62 5 O Heat of Fusion (Btu/lbm)\		r 12	45 PS		1.	0		
12 3 63 6 0 Internal heat generation (Btu/in.**3 min)\		r 12	45 GE O.		0.	0		
12 4 77 7 0 Thermal emissivity for radiation\ temp 1		r 12	45 RG O.	۱.	1.	0		

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12	5	87	8	0	Thermal	emissivity	for	radiation\	temp 2
12	6	97	9	0	Thermal	emissivity	for	radiation\	temp 3
12	7	107	10	0	Thermal	emissivity	for	radiation\	temp 4
12	8	117	11	0	Thermal	emissivity	for	radiation\	temp 5
12	9	127	12	0	Thermal	emissivity	for	radiation\	temp 6
12	10	137	13	0	Thermal	emissivity	for	radiation\	temp 7
12	11	147	14	0	Thermal	emissivity	for	radiation\	temp 8

r 12	45 RG O.	1.	1.	0
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r 12	45 RG 0.	1.	1.	0
r 12	45 RG 0.	1.	1.	0
r 12	45 RG 0.	1.	1.	0

# Material Properties Template continued

Appendix E Program Reference

### **Data Set File Naming Conventions**

CASKS data set files have 12 character names which specify the CASK ID, the analysis case, and the file type. File names are of the form:

IIIICCCCC·TTT File Type \* Analysis Case (or data name) \* CASKID

### Data Files

CCCC.TTT identifies the data type database:

BASE.GEI	=	Basic Geometry Database
BASE.CHK	=	Basic Geometry Data Check Output
LMTR.LMI	=	Limiter Force-Deflection Curves Database
LMTR.CHK	=	Limiter Force-Deflection Curves Data Check Output
YLDS. FCE	=	Yielding Surface Force-Deflection Curve Database
YLDS.CHK	=	Yielding Surface Force-Deflection Curve Data Check Output
DATA.FLG	=	Data Check Flags for Basic Geometry and Limiter Databases
NODE.GEO	=	Finite Element Mesh Node Database
ELEM.GEO	=	Finite Element Mesh Element Database

### **Impact Analysis Files**

CCCC.TTT identifies the analysis parameters and type and is of the form

### $\mathbf{H} \mathbf{E} \mathbf{T} \mathbf{D} \cdot \mathbf{A} \mathbf{A} \mathbf{O}$



where the individual parameters are

Drop Height user input digit or character	Impact End T=Top B=Bottom	Impact Type P=Primary only S=Primary with Secondary	Impact Angle user input digit or character	Analysis Type QB=Quasi-Static (bonded) QU=Quasi-Static (unbonded) IB=Dynamic (bonded)	Output Type O=Printable P=Plot file
				IU=Dynamic (unbon	ded)

### Thermal Analysis Files

CCCC identifies the analysis case:

T1RG = Cold Soak, Contents Heat, No Solar Effects

T2RG = Cold Soak, No Contents Heat, No Solar Effects

T3RG = Normal Cold, Contents Heat, No Solar Effects

T4RG = Normal Cold, No Contents Heat, No Solar Effects

T5RG = Normal Hot, Contents Heat, Solar Effects

T6RG = Normal Hot, Contents Heat, No Solar Effects

**T7RG** = Fire Accident, Contents Heat, No Solar Effects

TTT identifies the output type: TPO = Printable outputTPP = Plot file for POSTPZ

### Thermal Stress Analysis Files

CCCC identifies the analysis case:

T1RG = Cold Soak, Contents Heat, No Solar Effects

T2RG = Cold Soak, No Contents Heat, No Solar Effects

T3RG = Normal Cold, Contents Heat, No Solar Effects

T4RG = Normal Cold, No Contents Heat, No Solar Effects

T5RG = Normal Hot, Contents Heat, Solar Effects

T6RG = Normal Hot, Contents Heat, No Solar Effects

T7RG = Fire Accident, Contents Heat, No Solar Effects

TTT identifies the output type: TSO = Drinteble output

TSO = Printable output

### Pressure Stress Analysis Files

CCCC identifies the internal and external pressure conditions and is of the form:

### IIEE

External Pressure
 Internal Pressure

Where the internal and external pressures are identified as follows:

Internal Pressure	External Pressure		
MX=Maximum Normal Operating Pressure	RP=Reduced pressure	(3.5 psia)	
Tn=Pressure from Thermal case n	AP=Atmospheric pressure	(14.7 psia)	
	IP=Increased Pressure	(20.0 psia)	
	IM=Accident Immersion	(35.7 psia)	

TTT identifies the output type: PSO = Printable output

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**CASKS** provides the user with a companion software. This software can be used to estimate and generate a yielding surface force-deformation curve for a given concrete slab/soil subgrade combination. The theoretical background is contained in the Deformable Foundation Theory Report (Appendix G).

The software is divided into five programs. *model.bat* is a batch file that controls the other four programs. *dsep.exe* is a data input routine that splits the main input data file, *model.in*, into a file called *mcurve.in* containing reinforced concrete parameters, and a file called *mater.dat* containing finite-element mesh parameters. *mcurve.exe* inputs the reinforced concrete parameters from *mcurve. in* and generates five coordinates to represent the approximate moment-curvature relationship. These coordinates are output to the file *mcurve.out*. *meshgen.exe* inputs data from *mcurve.out* and *matr.dat*, and generates the final input file, *plate.in*, for the nonlinear finite-element code. *nlrmplate.exe* is the nonlinear finite element code that generates force-deformation data for a centrally loaded reinforced concrete slab on engineered fill. General data is output to a file called *plate.out*. Force-deformation data is output to a file called *plate.plt*.

All operations are carried out automatically. The user need only generate the main input file, *model.in*. NOTE: All output files are overwritten with each program execution. Therefore, data files should be renamed and stored before each program execution if they are to be kept.

The codes may either be run directly from the appropriate directory, or may be copied to a directory on a hard drive. To run the code, the main input file, *model.in*, must first be generated. This may be done using any text editor. Depending on the version of MS-DOS that the machine is running, *edlin.com* or *edit.com* may be used to generate the input file. Once *model.in* has been generated, the program may be executed by typing *MODEL* and then *ENTER*. The program must be run from the same directory that contains all data files and all executable files. Again, old versions of the output files will be overwritten each time the program is run.

The codes require approximately 570 KB of usable memory to execute. Make sure the required memory is available before you execute the code. To free the extra memory, temporarily shift and/or delete some memory–resident programs.

#### Format for model.in

The main input file is called *model.in*. This file is the only user-generated input file. It has the following format:

First Line:  $d_v$  $A_{sy} A'_{sx} A'_{sy} d'_{x}$ dx A<sub>sx</sub> d'<sub>v</sub> Second Line:  $\varepsilon_{\max,x}$  $\varepsilon_{max,y}$ Third Line: h  $E_s$  f'<sub>c</sub> f<sub>v</sub> Ks Gp Fourth Line shape atype x<sub>a</sub> y<sub>a</sub> x<sub>b</sub> Уb r

where:  $d_x$  is the distance from the top of the slab to the centroid of the tension steel in the X-direction

 $d_y$  is the distance from the top of the slab to the centroid of the tension steel in the Y-direction

 $A_{sx}$  and  $A_{sy}$  are the areas of the tension steel per unit width in the X and Y directions.

 $A'_{sx}$  and  $A'_{sy}$  are the areas of the compression steel per unit width in the X and Y directions.

 $d'_x$  and  $d'_y$  are distances from the top of the slab to the centroid of the compression steel in the X and Y directions.

 $\varepsilon_{\max,x}$  and  $\varepsilon_{\max,y}$  are the maximum compressive strains in the X and Y directions.

h is the thickness of the slab.

 $E_{\rm S}$  is Young's Modulus for steel.

 $f'_{c}$  is the maximum compressive strength of the concrete.

 $f_{\rm y}$  is the yield strength of the steel.

 $K_{\rm S}$  is the soil subgrade modulus.

 $G_{\rm p}$  is the soil shear modulus.

 $X_a$  and  $Y_a$  are the width and depth of a rectangular loading pattern in the X and Y directions.

 $X_b$  and  $Y_b$  are the width and depth of a rectangular slab in the X and Y directions.

r is the radius of a circular loading area.

shape is a flag indicating the shape of the loading area (1 = Rectangular, 2 = Circular).

*atype* is a flag representing the type of analysis to be performed (1 = Nonlinear, 2 = Linear).

All units are in kips and inches.

#### Examples

Two examples follow. Example 1 creates a nonlinear model of slab A-1b from Elstner and Hognestad (1956) on a 6" subgrade of clay subjected to a 10" square shaped loading pattern. Example 2 creates a nonlinear model of the same slab subjected to a circular loading pattern of 5" radius. All examples utilize a two-parameter model of the soil.

#### Example 1

Slab A-1b from Elstner and Hognestad (1956) is modeled on a 6" subgrade of clay. The following table lists slab parameters as reported by Elstner and Hognestad.

			Longitudinal Reinforcement					
			Tension Mat			Compression Mat		
			Spacings			Spacings		
Slab	f' c (ksi)	f <sub>y</sub> (ksi)	Bar#	Bot. (in)	Top (in)	Bar #	Bot. (in)	Top (in)
A-1b	3.66	48.2	6	9	7.5	4	7	8

 Table F.1

 Slab Parameters from Elstner and Hognestad (1956)

Taking the X-direction to correspond to the top steel in the tension and compression mats, and the Y-direction to correspond to the bottom steel in the tension and compression mats, the following additional data may be derived from Elstner and Hognestad (1956):

dx = 5.0 d'x = 1.5 dy = 4.25d'y = 1.0

The values of  $A_{sx}$ ,  $A'_{sx}$ ,  $A_{sy}$ , and  $A'_{sy}$  may be derived by dividing the cross sectional area of the appropriate steel bar by its spacing. For example, the bottom layer of the tension mat has #6 bars at nine-inch spacing. Each #6 bar has a cross sectional area of 0.44 in<sup>2</sup>. Therefore,

$$A_{\rm sx} = \frac{0.44inch^2}{9inch} = 4.889E - 2$$

Similarly,  $A'_{sx} = 2.857E-2$ ,  $A_{sy} = 5.867E-2$ , and  $A'_{sy} = 0.025$ .

We will take  $\varepsilon_{\max,x}$  and  $\varepsilon_{\max,y}$  to be 0.0035. The slab is six inches thick, so h = 6.0. We take  $E_s$  to be 29.0E3.  $f'_C$  is given as 3.66.  $f_y$  is given as 48.2.  $K_s$  and  $G_p$  are estimated to be  $K_s = 2.374$ , and  $G_p = 9.402$ .

The loading pattern is 10" X 10" square. Therefore,  $x_a = 10.0$ ,  $y_a = 10.0$ , and *shape* = 1. The slab is 72" X 72", so  $x_b = 72.0$ , and  $y_b = 72.0$ . Any value may be assigned to r for this example. We will perform a nonlinear analysis, so *atype* = 1.

The following input file, *model.in*, is appropriate for this example:

5.0 4.25 4.889E-2 5.867E-2 2.857E-2 0.025 1.5 1.0 0.0035 0.0035 6.0 29.0E3 3.66 48.2 2.374 9.402 10.0 10.0 72.0 72.0 0.0 1 1

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### Example 2

All parameters here are the same as for Example 1, with the following exceptions. The loading pattern is now circular with a radius of 5". Therefore, r = 5.0, and shape = 2.  $x_a$  and  $y_a$  may hold any value for this example:

:

The following input file is appropriate for this example:

5.0 4.25 4.889E-2 5.867E-2 2.857E-2 0.025 1.5 1.0 0.0035 0.0035 6.0 29.0E3 3.66 48.2 2.374 9.402 0.0 0.0 72.0 72.0 5.0 2 1

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U.S. NUCLEAR REGULATORY COMMISSION U.S. NUCLEAR REGULATORY COMMISSION BIBLIOGRAPHIC DATA SHEET (See instructions on the reverse) 2. TITLE AND SUBTITLE CASKS (Computer <u>A</u> nalysis of <u>S</u> torage Cas <u>KS</u> ) A Microcomputer Based Analysis System for Storage Cask Design Review: User's Manual to Version 1b (Including Program Reference) 5. AUTHOR(S) T. F. Chen, M. A. Gerhard, D. J. Trummer, G. L. Johnson, G. C. Mok	1. REPORT NUMBER (Assigned by NRC, Add Vol., Supp., Rev., and Addendum Numbers, if any.) NUREG/CR-6242 UCRL-ID-117418 3. DATE REPORT PUBLISHED MONTH YEAR February 1995 4. FIN OR GRANT NUMBER L1615 6. TYPE OF REPORT 7. PERIOD COVERED (Inclusive Dates)			
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10. SUPPLEMENTARY NOTES 11. ABSTRACT (200 words or test) CASKS ( <u>C</u> omputer <u>A</u> nalysis of <u>S</u> torage Cas <u>KS</u> ) is a microcomputer-based system of computer programs and databases developed at the Lawrence Livermore National Laboratory (LLNL) for evaluating safety analysis reports on spent-fuel storage casks. The bulk of the complete program and this user's manual are based upon the SCANS ( <u>S</u> hipping <u>C</u> ask <u>AN</u> alysis <u>S</u> ystem) program previously developed at LLNL. A number of enhancements and improvements were added to the original SCANS program to meet requirements unique to storage casks. CASKS is an easy-to-use system that calculates global response of storage casks to impact loads, pressure loads and thermal conditions. This provides reviewers with a tool for an independent check on analyses submitted by licensees. CASKS is based on microcomputers compatible with the IBM-PC family of computers. The system is composed of a series of menus, input programs, cask analysis programs, and output display programs. All data is entered through fill-in-the-blank input screens that contain descriptive data requests.				
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