



A multicommutated flow injection system with a multi-channel propulsion unit: spectrophotometric determination of N-NH_4^+

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Introduction

Separation processes in flow analysis

➤ Objectives

- Avoid matrix problems
- Enhance selectivity
- Pre-concentrate/dilute

➤ Limitations

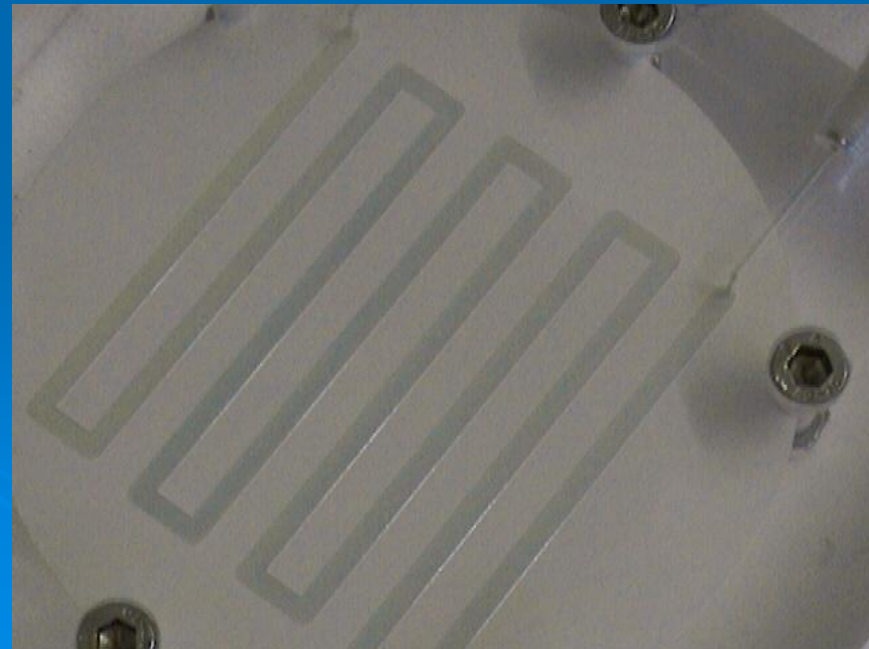
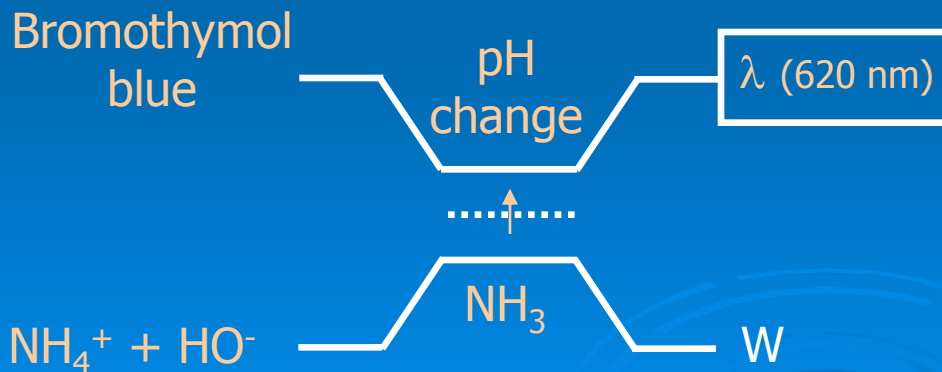
- Overpressure conditioning
 - Propulsion process
 - Manifold configuration
 - Flow technique
- Mostly used in FIA systems
 - High reagents consumption and waste generation

Introduction

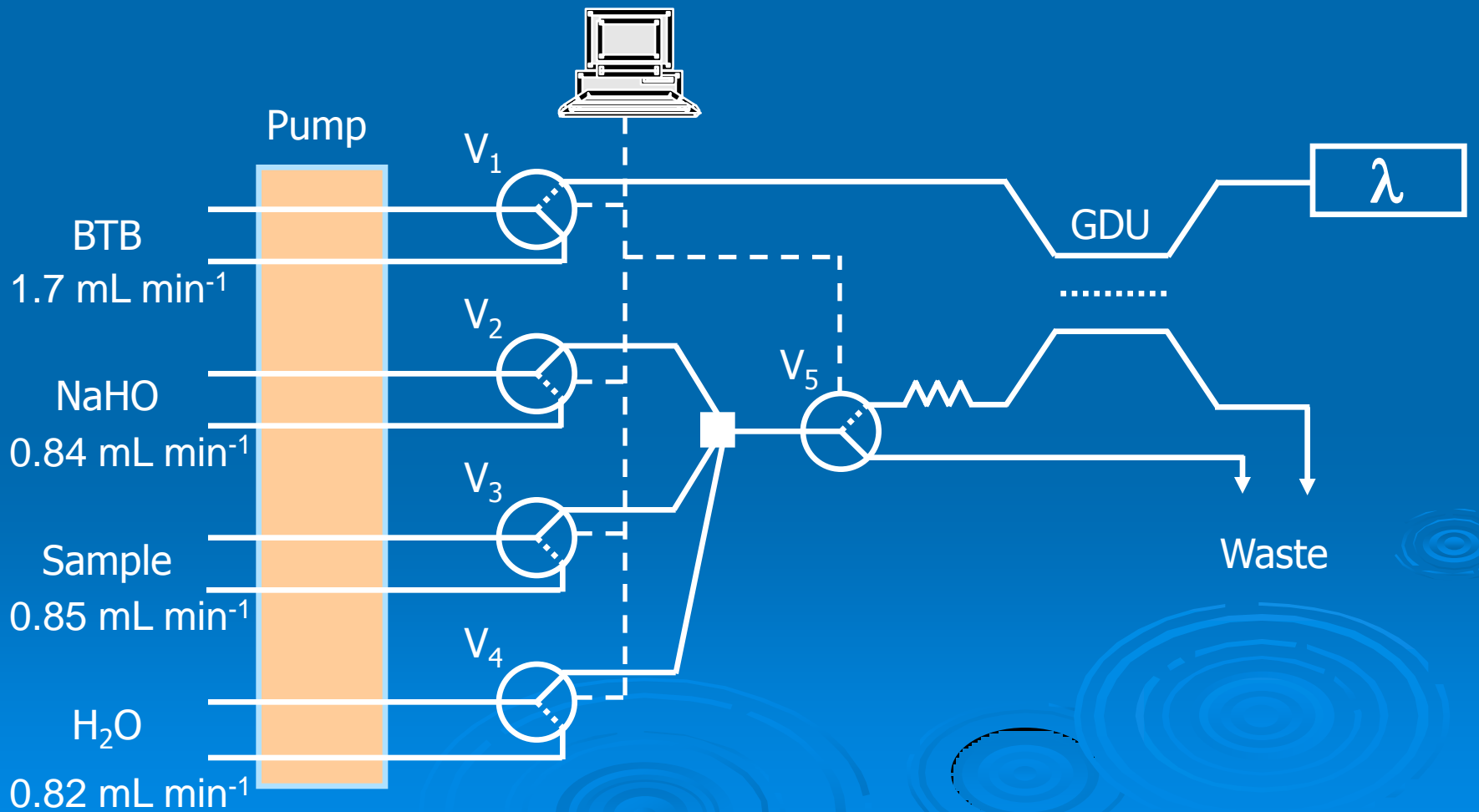
- Multicommutation system with the pumping device placed before the solenoid valves
 - Minimisation of the formation of unwanted air bubbles
 - Easy adaptation of a separation device to the manifold
 - Minimisation of reagent consumption and waste generation
 - Propulsion of the solutions into the flow network or recirculation to their own vessel
 - Possibility of reagent recycling

Introduction

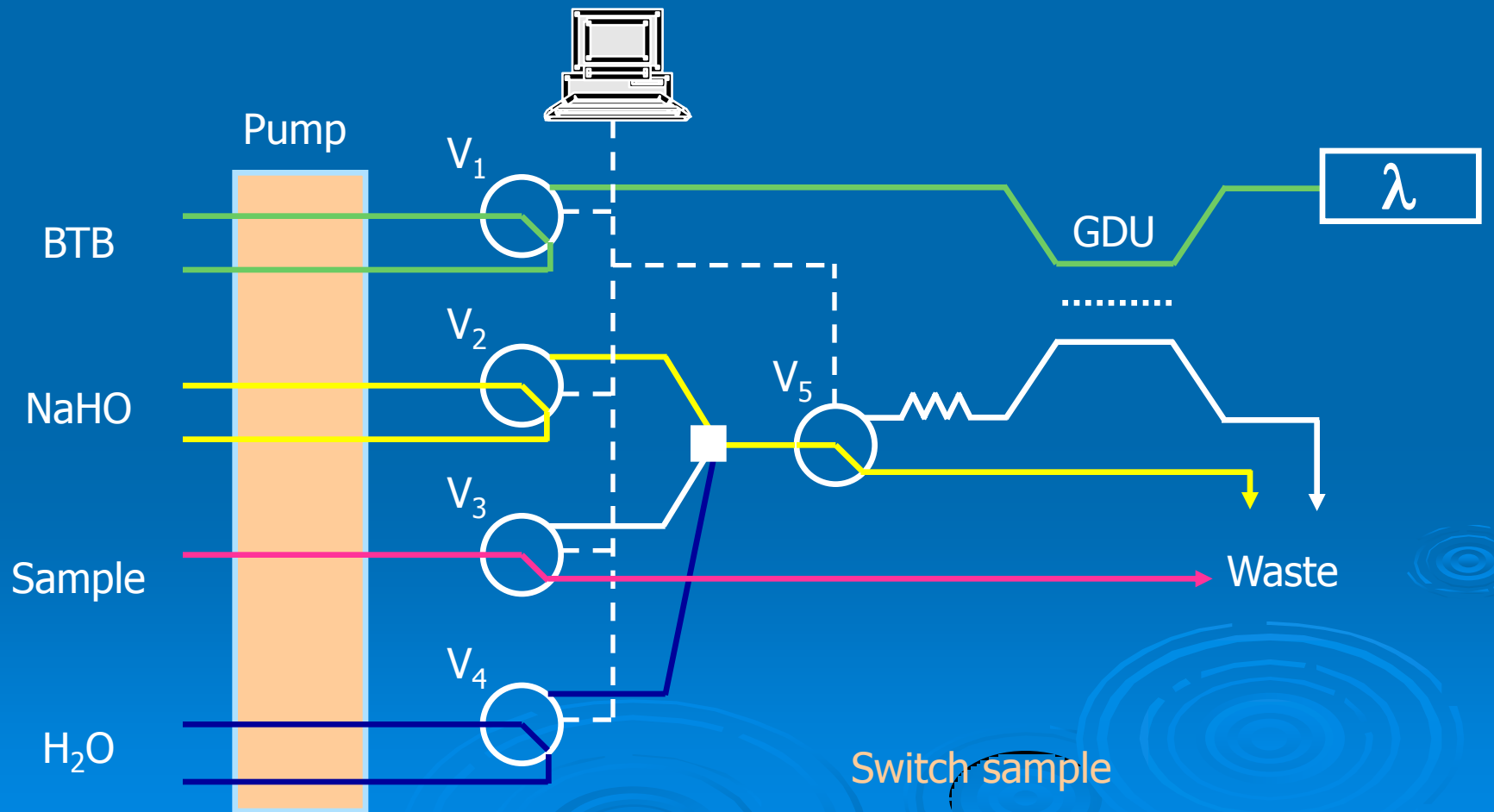
- Application of the system to a reaction with low selectivity
 - Spectrophotometric determination of ammonium nitrogen using an acid-base indicator
- Incorporation of a gas diffusion unit
 - Transfer the analyte from a donor stream (sample) to an acceptor solution (detector)



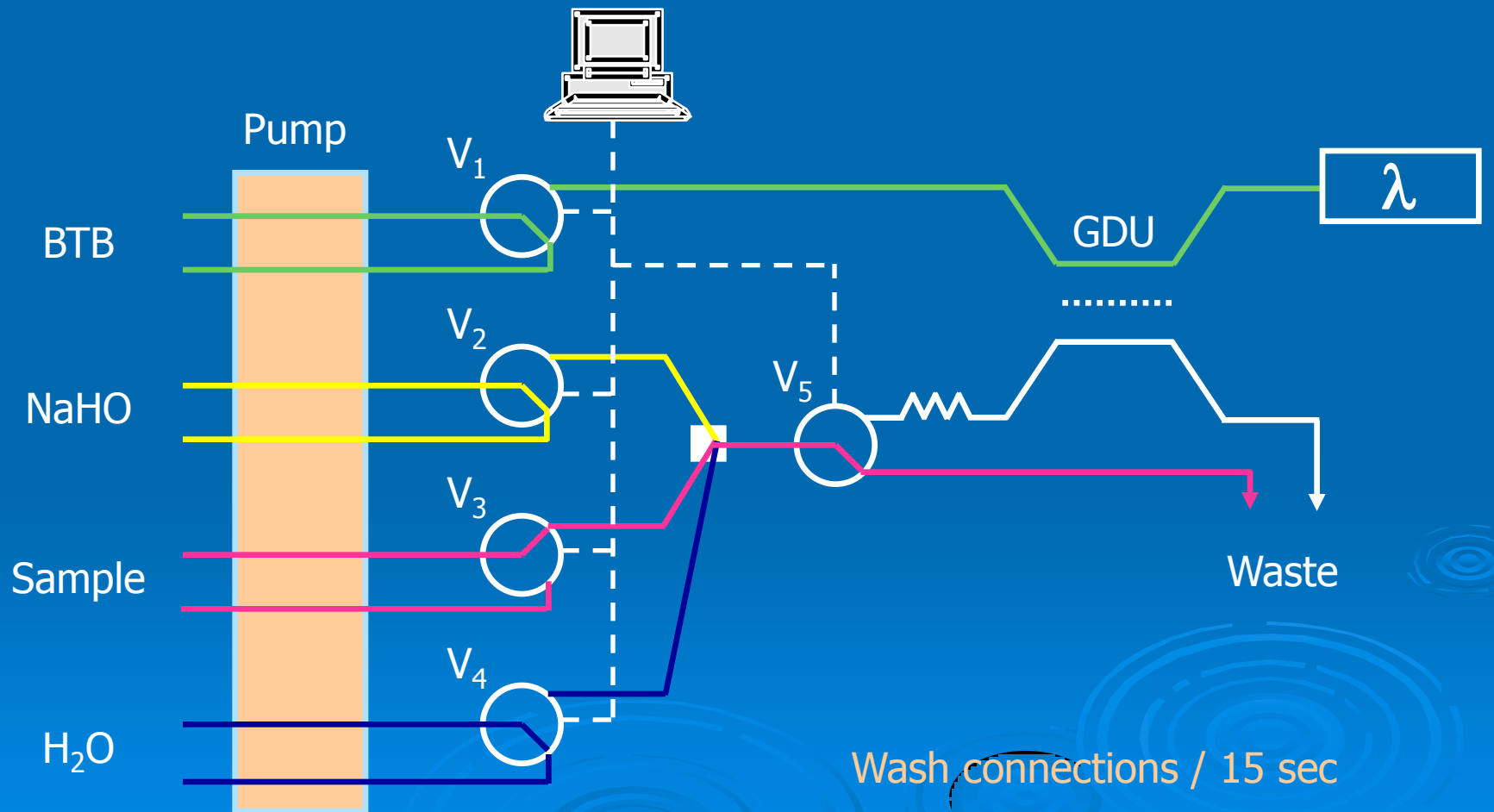
Multicommutated manifold



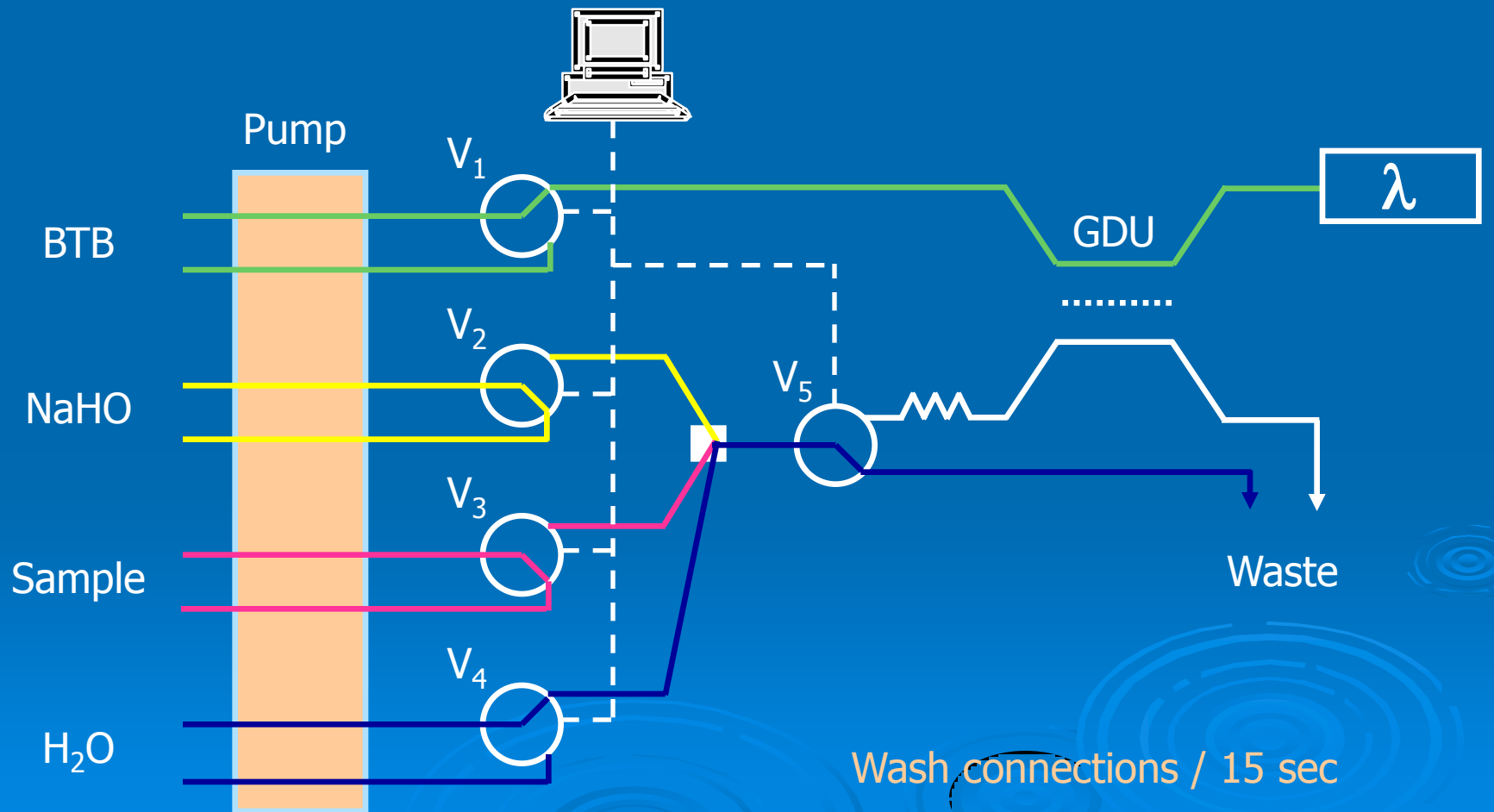
Analytical sequence



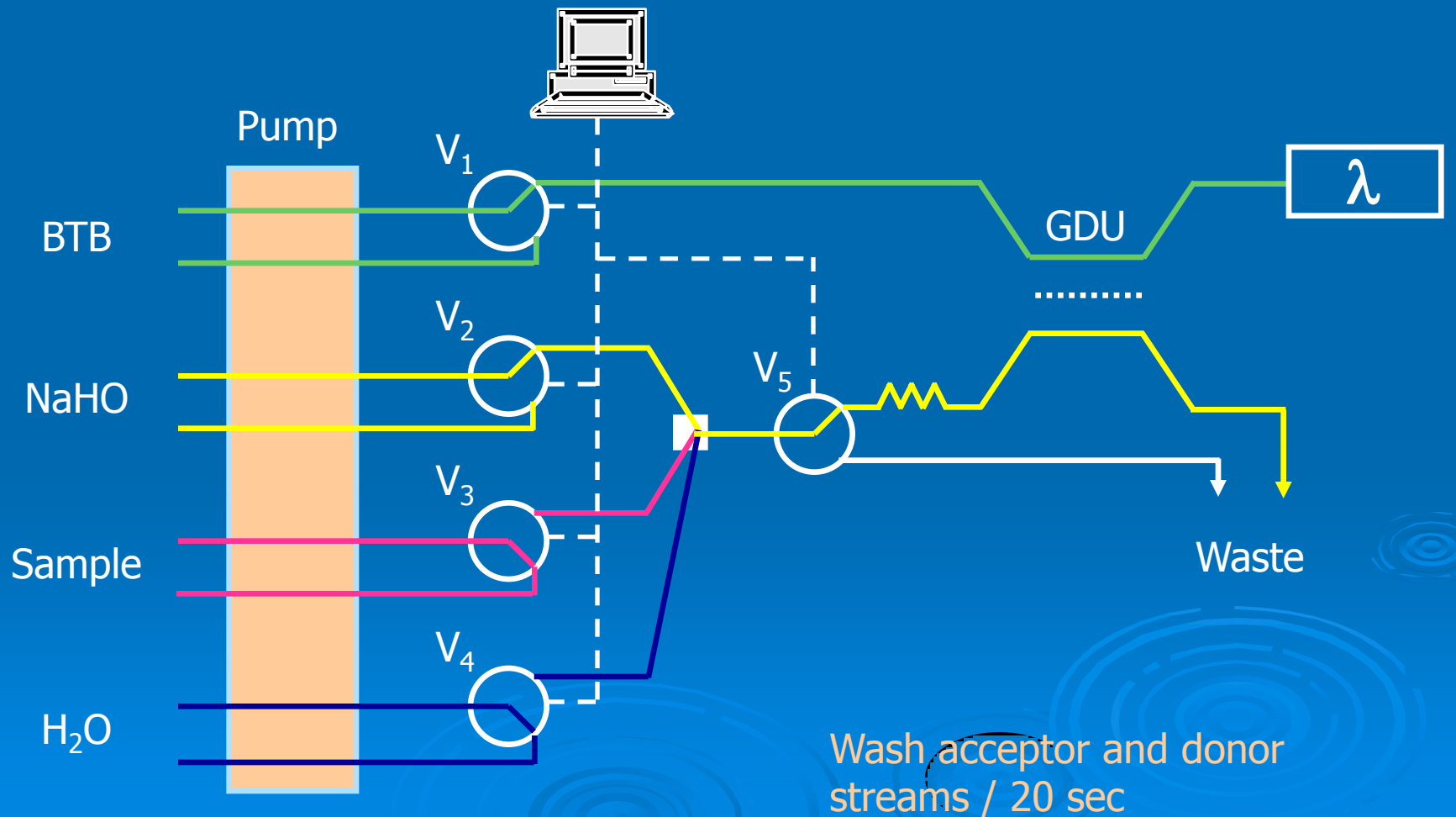
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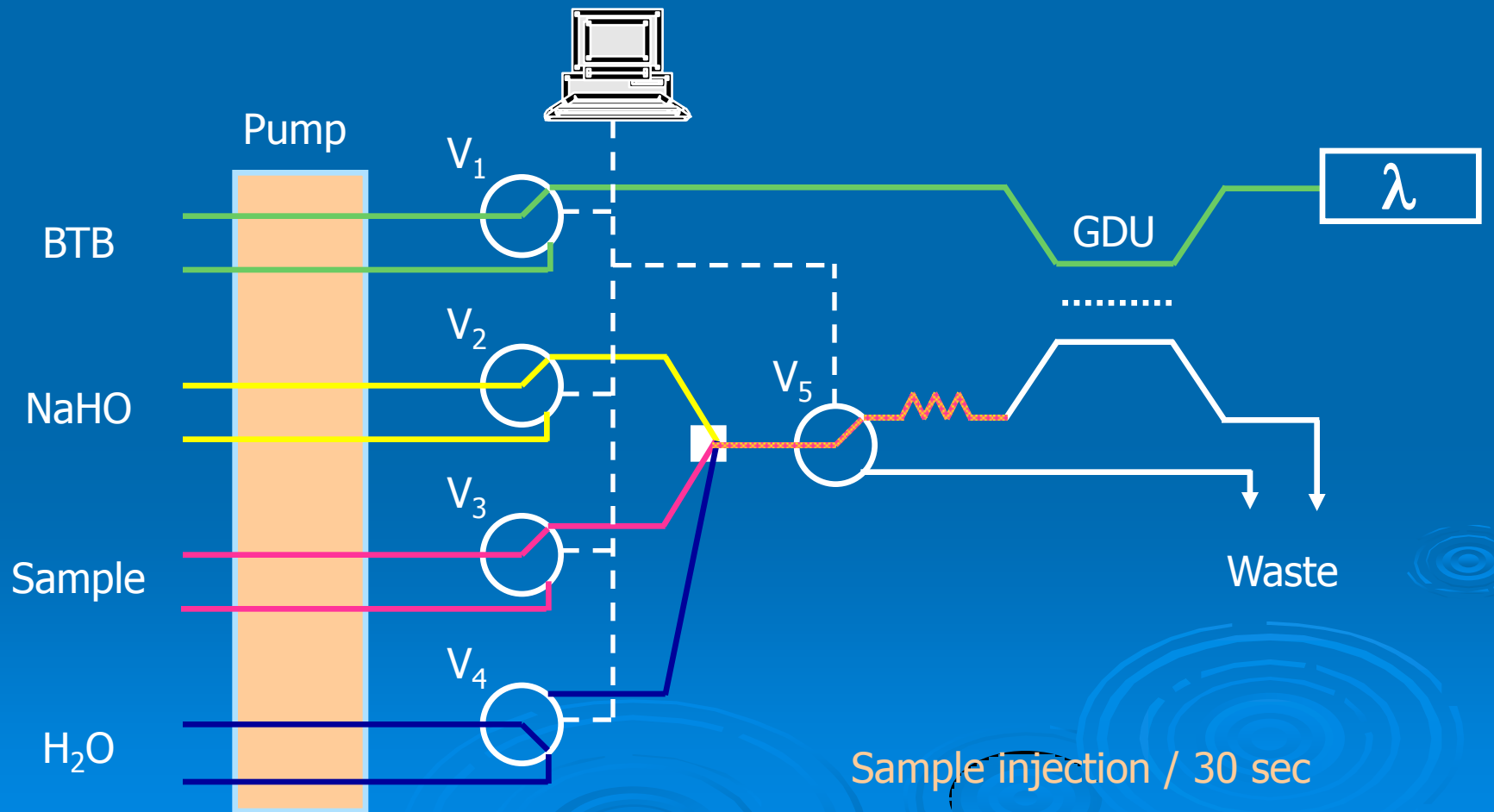
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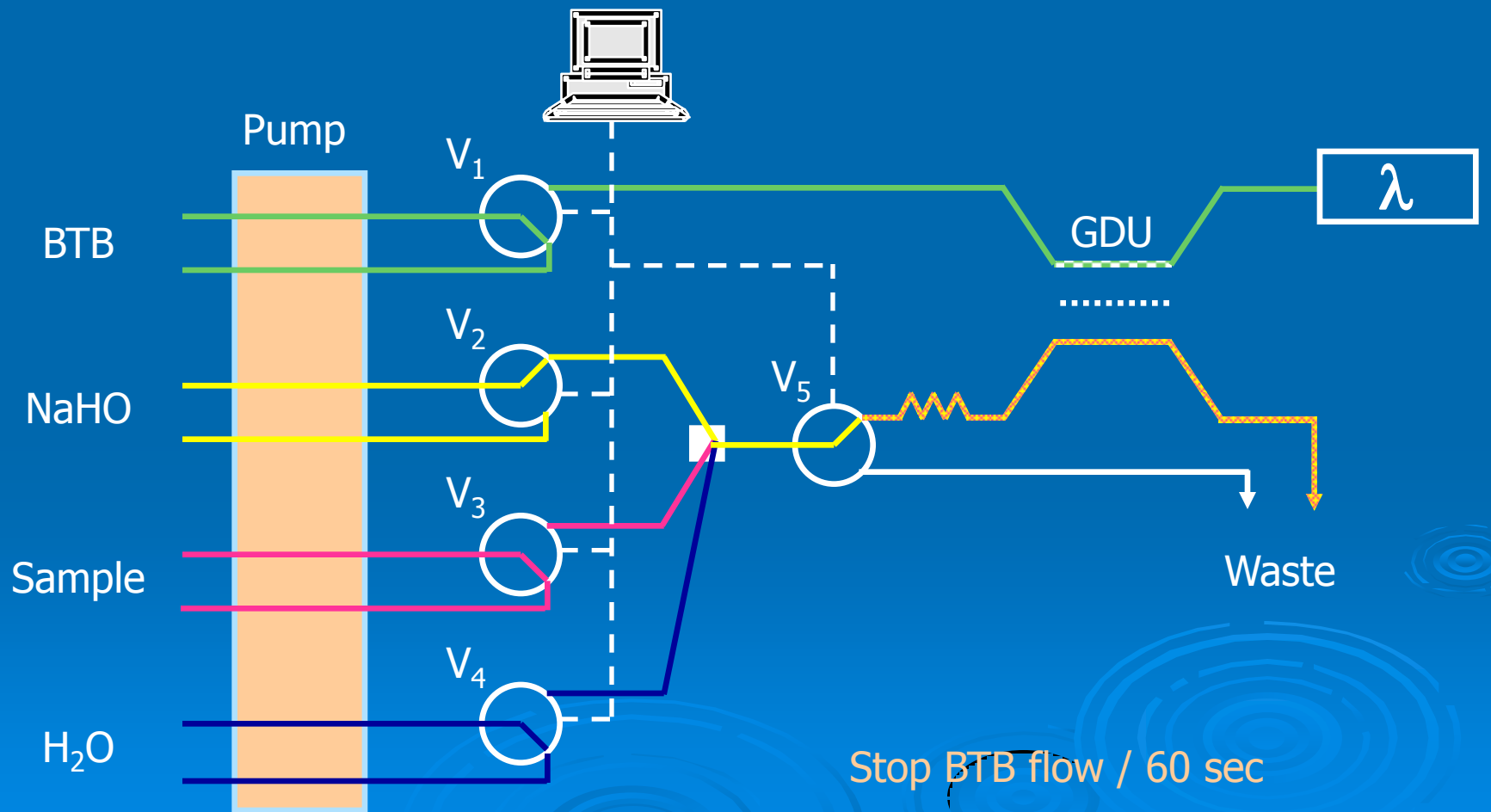
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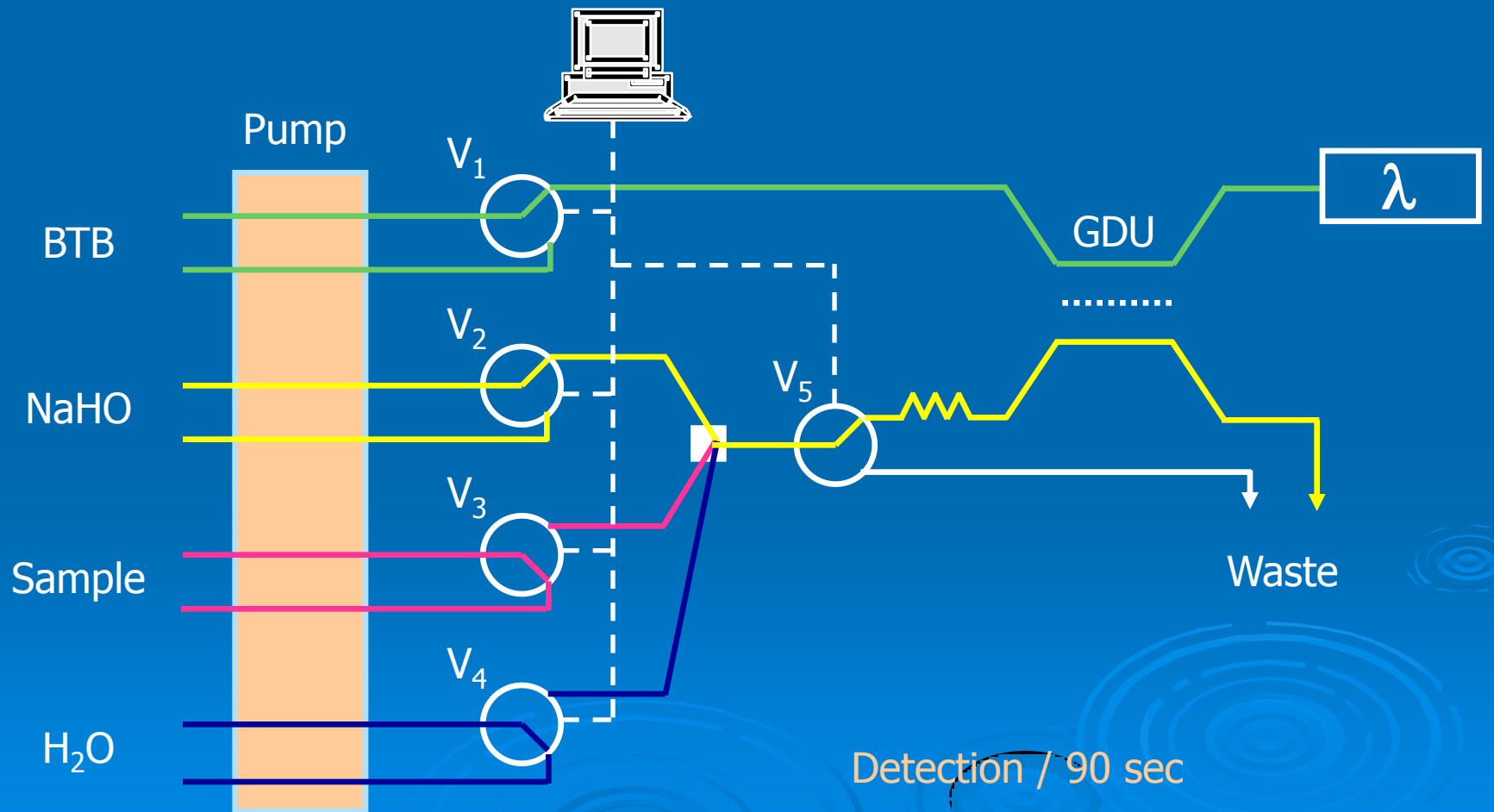
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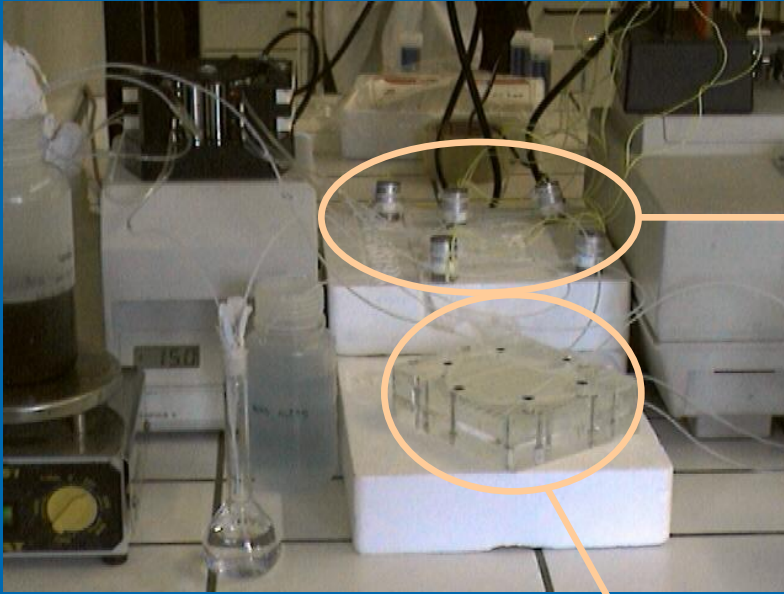
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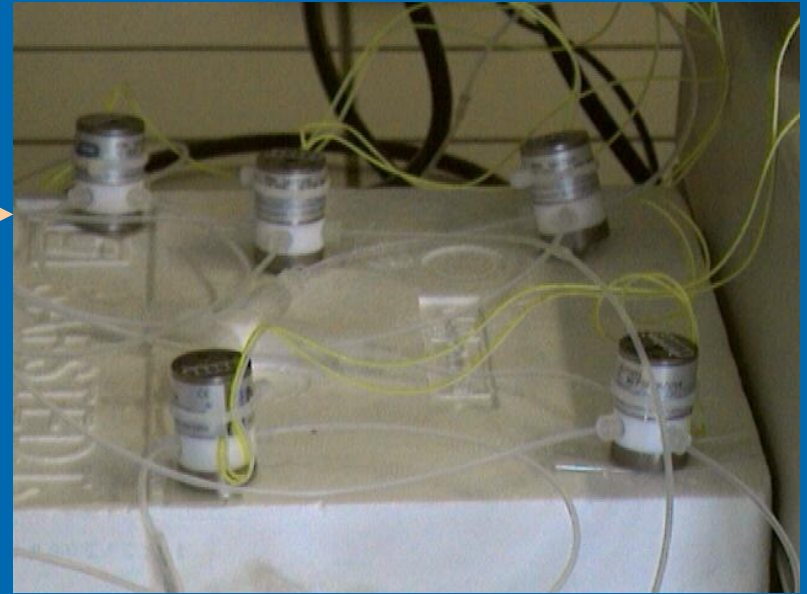
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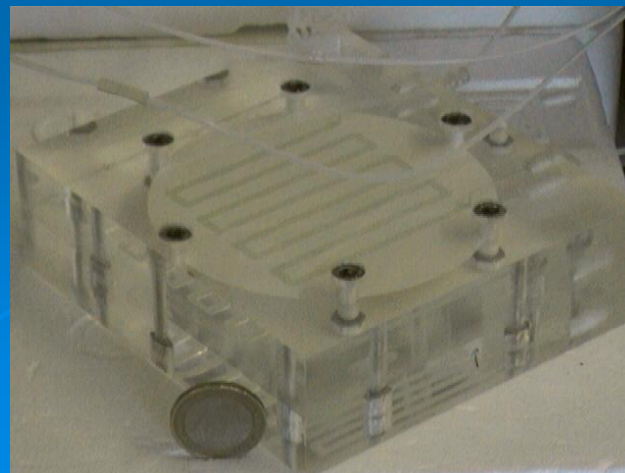
In the laboratory



Flow manifold



Network of solenoid valves



Gas diffusion device

Development of the flow system

Variable studied	Range	Chosen Value
Temperature (donor solution)	25 – 80°C	25°C
Ultrasonic treatment	Yes / No	No
Flow cell optical path	10 mm / 20 mm	10 mm
BTB pH	5.8 – 7.6	6.8
Acceptor flow rate	1.1 – 2.3 mL min ⁻¹	1.7 mL min ⁻¹
Donor flow rate	1.1 – 2.0 mL min ⁻¹	1.7 mL min ⁻¹
Sample volume	208 – 553 μL	415 μL
Stop period of BTB solution	0 – 80 s	60 s
NaHO concentration	0.01 – 0.5 mol L ⁻¹	0.1 mol L ⁻¹
BTB concentration	0.02 – 0.1 mmol L ⁻¹	0.06 mmol L ⁻¹

Development of the flow system

➤ Configuration and area of the gas diffusion device



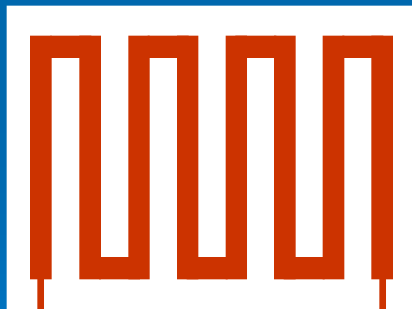
$$A = 108 \text{ mm}^2$$

$$s = 0.0165 \text{ AU mg}^{-1} \text{ L}$$



$$A = 142 \text{ mm}^2$$

$$s = 0.0177 \text{ AU mg}^{-1} \text{ L}$$



GDU chosen

$$A = 1524 \text{ mm}^2$$

$$s = 0.0804 \text{ AU mg}^{-1} \text{ L}$$



$$A = 146 \text{ mm}^2$$

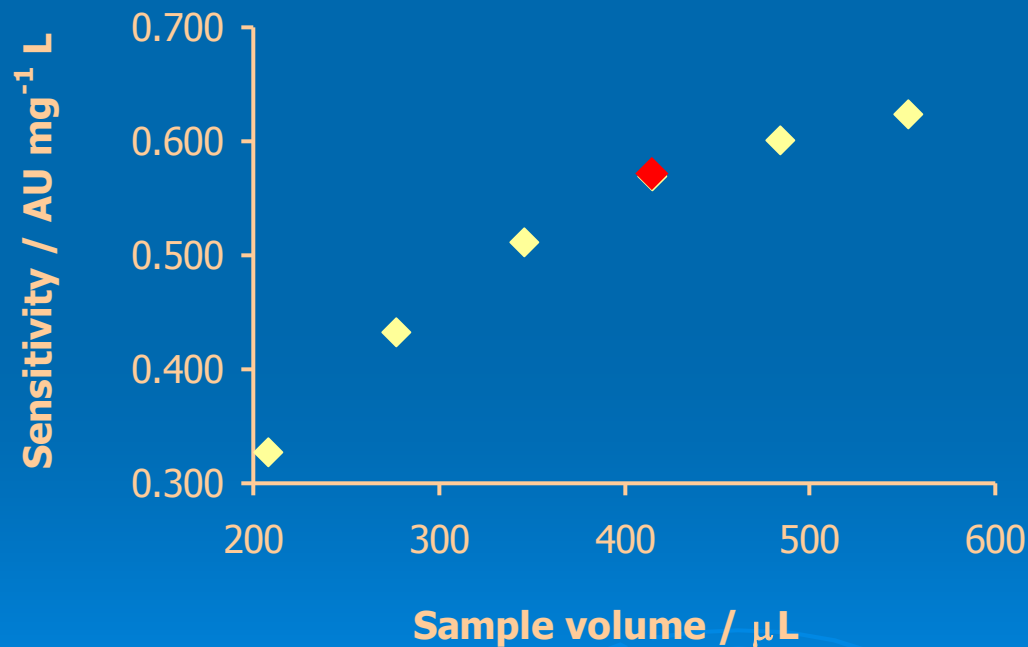
$$s = 0.0553 \text{ AU mg}^{-1} \text{ L}$$

s = sensitivity

Experiments done with a FIA system; NH_4^+ concentration range = 1 – 20 mg L^{-1}

Development of the flow system

➤ Sample volume

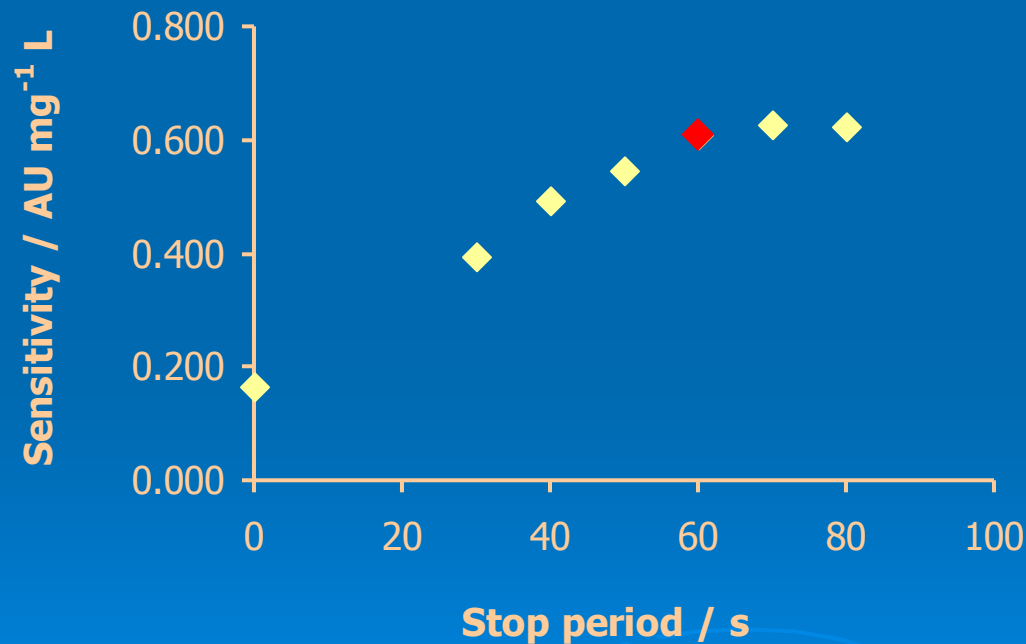


A sample volume of 415 μL corresponded to 96% of the sensitivity relative to the maximum volume tested

NH₄⁺ concentration range = 50 – 1000 μg L⁻¹

Development of the flow system

➤ Stop period of the BTB solution

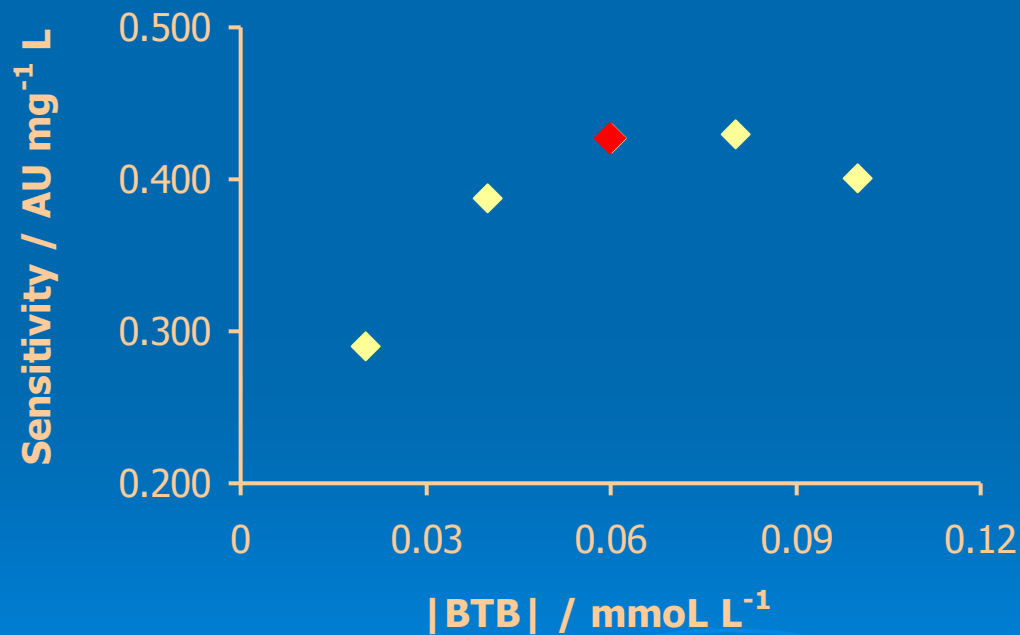


The flow of the acceptor stream was stopped for a period of 60 seconds

NH_4^+ concentration range = 50 – 1000 $\mu\text{g L}^{-1}$

Development of the flow system

➤ Acceptor solution concentration



A concentration of 0.06 mmol L⁻¹ of BTB was selected for further work

NH₄⁺ concentration range = 50 – 1000 μg L⁻¹

Development of the flow system

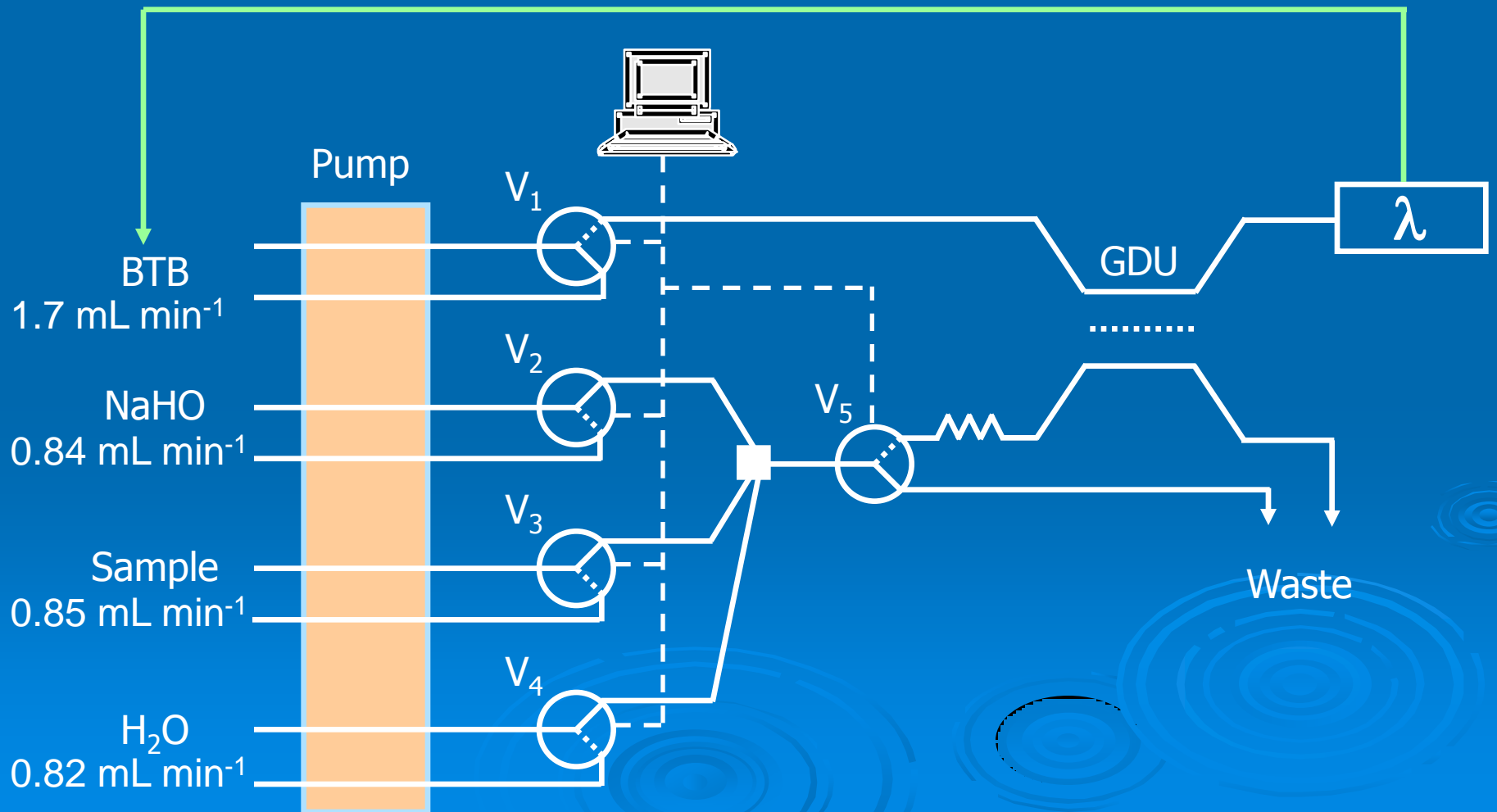
➤ Interferences

Interfering ion	Concentration tested	Relative deviation / %
Cu^{2+}	$200 \mu\text{g L}^{-1}$	-0.61
Zn^{2+}	$200 \mu\text{g L}^{-1}$	-3.64
Fe^{2+}	$200 \mu\text{g L}^{-1}$	4.5
Ca^{2+}	$200 \mu\text{g L}^{-1}$	-4.15
Mg^{2+}	$200 \mu\text{g L}^{-1}$	-4.15
Al^{3+}	$200 \mu\text{g L}^{-1}$	2.75
HCO_3^-	10mg L^{-1}	-2.47

NH_4^+ concentration = $100 \mu\text{g L}^{-1}$

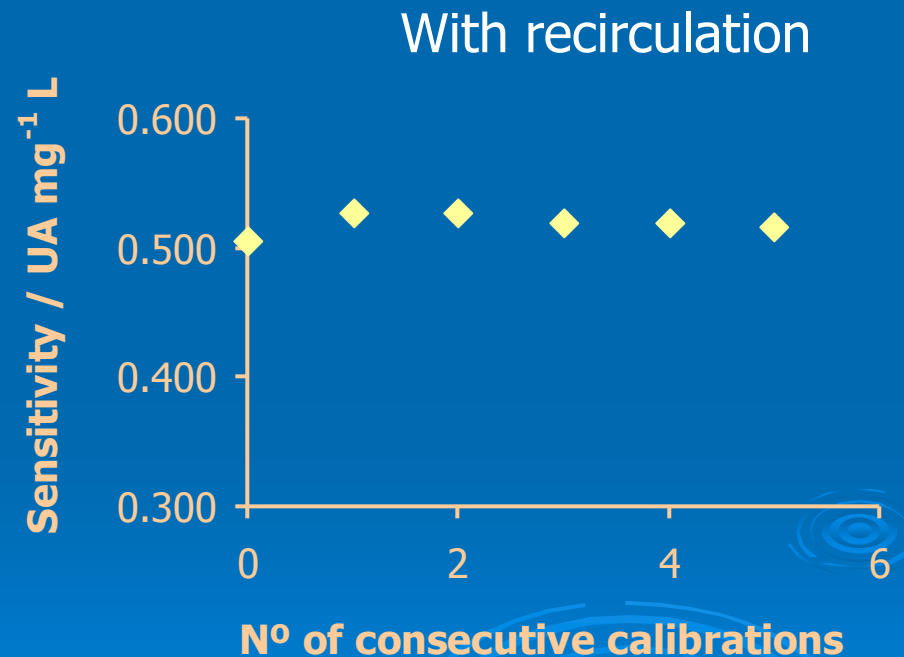
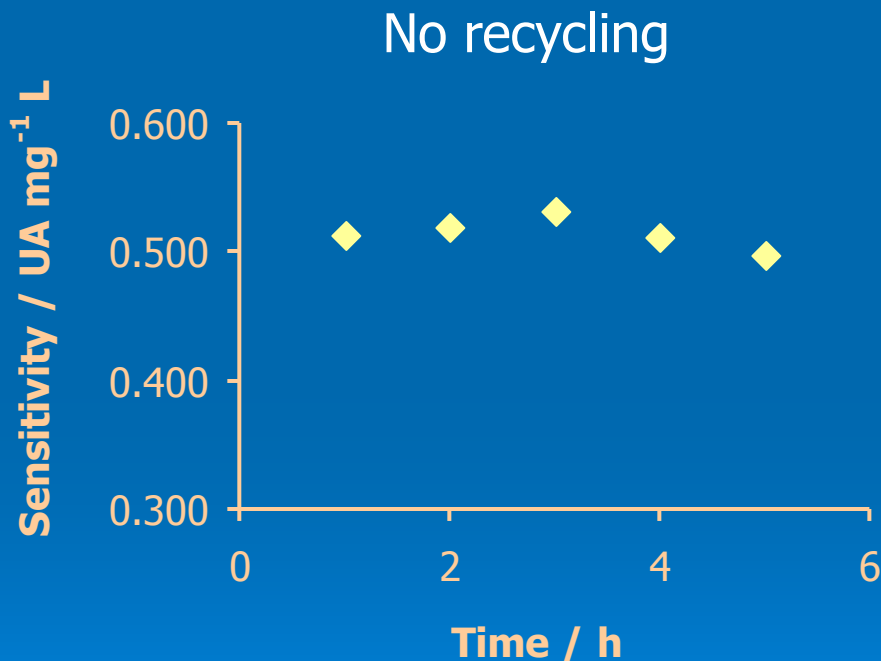
Development of the flow system

➤ Multicommutated manifold with BTB recirculation



Development of the flow system

➤ Possibility of BTB recycling



There is no statistical difference between both graphs
t- test: $|t|_{\text{calculated}} = 0.77 < t_{\text{critical}} = 2.26$

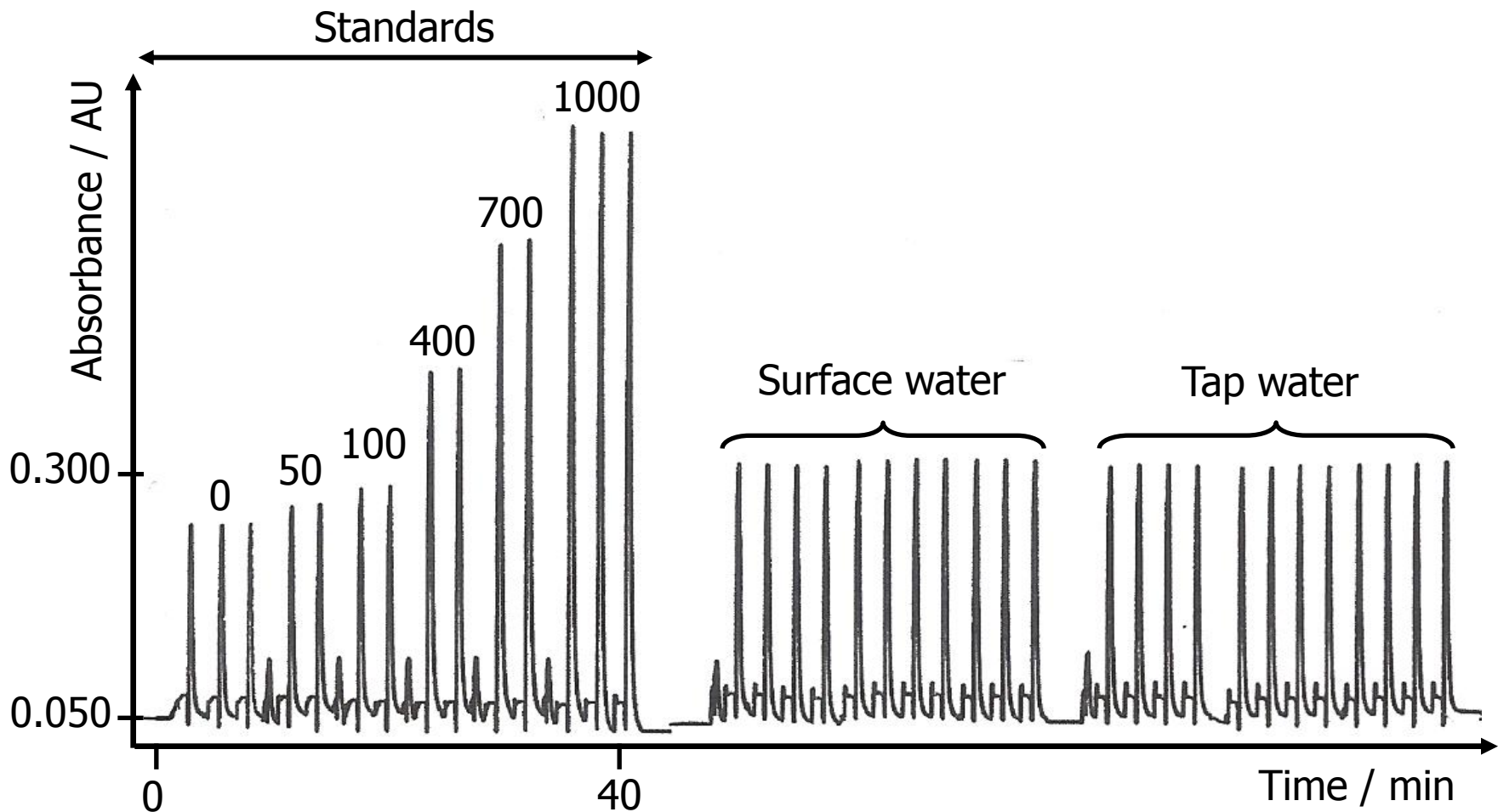
Development of the flow system

➤ Figures of merit

Concentration range / $\mu\text{g L}^{-1}$	50 – 1000
Sensitivity / $\text{AU mg}^{-1} \text{L}$	0.519 ± 0.008
Quantification limit / $\mu\text{g L}^{-1}$	42
Detection limit / $\mu\text{g L}^{-1}$	27
Relative standard deviation / % (n = 10)	<1.6
Determination rate / h^{-1}	20
Effluent volume per determination / mL	3.2

Development of the flow system

➤ Calibration curve ($|\text{NH}_4^+|$ expressed in $\mu\text{g L}^{-1}$)



Application to water samples

➤ Recovery studies

NH ₄ ⁺ added / μg L ⁻¹	Recovery %		
	Surface water 1	Surface water 2	Tap water
0	-----	-----	-----
50	120 _{±13}	99.0 _{±3.2}	98.3 _{±2.2}
200	102 _{±2}	95.1 _{±1.3}	100 _{±1}
500	99.2 _{±0.8}	97.5 _{±1.9}	99.0 _{±0.7}
800	102 _{±2}	99.3 _{±1.7}	100 _{±1}

n = 9

Application to water samples

➤ Certified sample (VKI QC RW1)

	$ N / \mu\text{g L}^{-1}$	SD	Concentration range
Certified values	100.9	1.26	100.2 – 101.5

	$ N / \mu\text{g L}^{-1}$	SD	RSD / %	
Certified sample prepared in	Deionised water	100.3	1.0	0.96
	Surface water	100.5	1.6	1.5
	Tap water	101.0	1.2	1.2
	Sea water	100.6	1.2	1.1

n = 10

Conclusions

- The proposed system configuration allowed easy manipulation of the flow procedure
 - Sample volume/analyte concentration
 - Efficiency of the diffusion process
 - Reagents recirculation
- Ammonium determination in waters
 - Certified sample results and recovery tests indicate good accuracy
 - Successful application of the system to the determination of low levels of N-NH_4^+ in several types of water
 - BTB recirculation reduces reagent consumption and effluent generation

Acknowledgements

Sara Oliveira and Ildikó Tóth thank Fundação para a Ciência e a Tecnologia (FCT) and FSE (III Quadro Comunitário) for the grants SFRH/BD/23782/2005 and SFRH/BPD/5631/2001, respectively



Porto

Thank you all for your kind attention