

## OBJECTIVE

Design experiments using *D*-optimal design criterion aiming at microbial inactivation kinetic parameter with maximum precision

Range of Temperatures

## INTRODUCTION

- Predictive microbiology is gaining considerably importance in the food processing domain, particularly in the design of efficient and safe inactivation treatments. This terminology designates the use of mathematical models in the description of microbial responses to environmental stressing factors, such as temperature, pH or water activity. Microbial inactivation can be mathematically described by a modified Gompertz model, which includes an initial shoulder (L) followed by a maximum inactivation rate ( $k_{max}$ ) period. The kinetic model parameters are temperature dependent and a Ratkowsky equation or an Arrhenius-type relationship can be used to express such relationship.
- If a mathematical model is properly chosen and the prime objective is to improve parameter estimation, underlying statistical theories can be applied. The criterion aiming at minimisation of parameters' variance, nominated as *D*-optimal design, is an appropriate used approach seeking parameter precision.
- Precision increases with the number of experimental points. But in many situations, when replicates of a number of experimental points equal to the number of model parameters is considered, maximum precision is attained.

If four sampling conditions (i.e. temperature/sampling time) are planned (n=4) the determinant becomes:

$$\Delta = |F^T F| = \begin{vmatrix} \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial k_{ref}}\right)_i^2 & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial k_{ref}} \times \frac{\partial y_{inact}}{\partial E_a}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial k_{ref}} \times \frac{\partial y_{inact}}{\partial C_{Ratk}}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial k_{ref}} \times \frac{\partial y_{inact}}{\partial T_{min}}\right)_i \\ \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial E_a} \times \frac{\partial y_{inact}}{\partial k_{ref}}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial E_a}\right)_i^2 & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial E_a} \times \frac{\partial y_{inact}}{\partial C_{Ratk}}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial E_a} \times \frac{\partial y_{inact}}{\partial T_{min}}\right)_i \\ \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial C_{Ratk}} \times \frac{\partial y_{inact}}{\partial k_{ref}}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial C_{Ratk}} \times \frac{\partial y_{inact}}{\partial E_a}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial C_{Ratk}}\right)_i^2 & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial C_{Ratk}} \times \frac{\partial y_{inact}}{\partial T_{min}}\right)_i \\ \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial T_{min}} \times \frac{\partial y_{inact}}{\partial k_{ref}}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial T_{min}} \times \frac{\partial y_{inact}}{\partial E_a}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial T_{min}} \times \frac{\partial y_{inact}}{\partial C_{Ratk}}\right)_i & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial T_{min}}\right)_i^2 \end{vmatrix}$$

Preliminary estimates of  $k_{ref}$ ,  $E_a$ ,  $C_{Ratk}$  and  $T_{min}$  were assumed to be  $0.29 \text{ min}^{-1}$ ,  $3.34 \times 10^5 \text{ J mol}^{-1}$ ,  $0.38 \text{ K}^{-1} \text{ min}^{-0.5}$  and  $337.1 \text{ K}$ , respectively.

## MATHEMATICAL CONSIDERATIONS

### The model

If one single temperature is chosen from a range, the microbial inactivation model assumed was the one based on modifications of the Gompertz equation:

$$y_{inact}(t) = \log\left(\frac{N}{N_0}\right) = \log\left(\frac{N_{res}}{N_0}\right) \exp\left(-\exp\left(-\frac{k_{max} \exp(1)}{\log\left(\frac{N_{res}}{N_0}\right)} (L - t) + 1\right)\right)$$

$N$  - microbial load at time  $t$ ;  $N_0$  - initial microbial load;  $N_{res}$  - Residual microbial load;  $t$  - time

If a range of temperatures is considered, the Temperature dependence of  $k_{max}$  and  $L$  may be included in the previous equation. Assuming an Arrhenius-type relationship for  $k_{max}$  and a Ratkowsky equation for  $L$ , the model a four-parameter model:

$$y_{inact}(t) = \log\left(\frac{N_{res}}{N_0}\right) \exp\left(-\exp\left(\frac{-k_{ref} \exp\left(-\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_{ref}}\right)\right)}{\log\left(\frac{N_{res}}{N_0}\right)} \left(\frac{C_{Ratk} (T - T_{min})^2 - t}{(C_{Ratk} (T - T_{min})^2 - t) + 1}\right)\right)\right)$$

$k_{ref}$  - Inactivation rate at a finite reference  $T_{ref}$ ;  $E_a$  - Process activation energy;  $C_{Ratk}$  and  $T_{min}$  - Ratkowsky equation parameters;  $R$  - universal gas constant

### D-Optimal experimental design criterion

Precision

Minimisation of parameters' variance

mathematically corresponds to...

Maximisation of the determinant  $|F^T F|$

Minimisation of the determinant of the variance - covariance matrix of parameters  $|F^T F|^{-1}$

For a two - parameter model, the simplest design corresponds to an isothermal experiment, with two samplings at time  $t_1$  and  $t_2$

$$\Delta = |F^T F| = \begin{vmatrix} \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial k_{max}}\right)_{t_i}^2 & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial k_{max}} \times \frac{\partial y_{inact}}{\partial L}\right)_{t_i} \\ \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial L} \times \frac{\partial y_{inact}}{\partial k_{max}}\right)_{t_i} & \sum_{i=1}^n \left(\frac{\partial y_{inact}}{\partial L}\right)_{t_i}^2 \end{vmatrix}$$

The two sampling times that maximise the determinant  $|\Delta|$  were calculated numerically:

- Using analysis tool packages available in Microsoft® Office Excel
- Preliminary estimates of  $k$  and  $L$  required for calculation were the ones presented in Table 1
- Six temperatures, in the range 52.5°C to 65.0°C, were considered and  $\log(N_{res}/N_0)$  was assumed to be -5

## RESULTS AND DISCUSSION

### Single Temperature

- Sampling times ( $t_1$  and  $t_2$ ), that maximise  $|\Delta|$ , were temperature dependent
- $t_1$  corresponds always to 89.09% of inactivation (i.e.  $\log(N/N_0) = -0.96$ ) and  $t_2$  to 99.97% (i.e.  $\log(N/N_0) = -3.52$ )

however...

Variables used in *D*-optimal experimental design definition, and corresponding sampling conditions

Definition of the design			Optimal sampling			
T (°C)	$k_{max}$ ( $\text{min}^{-1}$ )	L (min)	$t_1$ (min)	$\log(N/N_0)$	$t_2$ (min)	$\log(N/N_0)$
52.5	$4.04 \times 10^{-2}$	69.06	91.85	-0.96	162.1	-3.52
55.0	$7.56 \times 10^{-2}$	39.58	51.76	-0.96	89.31	-3.52
57.5	$1.41 \times 10^{-1}$	10.82	17.36	-0.96	37.52	-3.52
60.0	$4.52 \times 10^{-1}$	6.06	8.10	-0.96	14.38	-3.52
62.5	$1.14 \times 10^0$	0.68	1.49	-0.96	3.98	-3.52
65.0	$2.18 \times 10^0$	0.03	0.45	-0.96	1.75	-3.52

### Design efficiency

The *D*-optimal experimental design was compared to a heuristic design in terms of parameters' precision.

- Since  $|\Delta|$  is a measure of parameters' precision, the ratio between  $|\Delta|$  calculated with 10 sampling points equally spaced in time was compared to the one calculated for 5 replicates of each optimal  $t_1$  and  $t_2$ .
  - The efficiency of a heuristic design was 26, 18, 33, 31, 43 and 76% for the experiments conducted at 52.5, 55.0, 57.5, 60.0, 62.5 and 65 °C, respectively.
  - As an example, if *D*-optimal design was chosen, the confidence intervals of  $k$  and  $L$  would decrease **40%** and **59%**, respectively (at 52.5°C), improving precision.

### Range of Temperatures

If a Temperature range is considered, the Gompertz model is a four-parameter model and:

- Optimal experimental design consists of four experiments conducted within the experimental range of temperatures: one at each extreme temperature ( $T_{min}=52.5 \text{ °C}$  and  $T_{max}=65 \text{ °C}$ ), one at the average temperature of the range tested ( $T_{ave}=58.8 \text{ °C}$ ), and the remained one at a temperature 3 % lower than the maximum extreme ( $T_{3\%}<T_{max}=65.0 \text{ °C}$ ).
- At each  $T$ , the sampling times corresponds to 99.95 % ( $T_{min}$ ), 97.49% ( $T_{ave}$ ), 99.92% ( $T_{3\%}<T_{max}$ ) and 99.21 % ( $T_{max}$ ) of inactivation.

### Design efficiency

- The efficiency of a heuristic design was only **1.6 %** (calculated with 18 sampling points equally spaced in time (at each one of the six  $T$ ) and 27 replicates of each one of the four optimal sampling conditions).
- If *D*-optimal design was chosen, the confidence intervals of  $k_{ref}$ ,  $E_a$ ,  $C_{Ratk}$  and  $T_{min}$  would decrease **64**, **88**, **80** and **72 %** respectively, improving precision.

## CONCLUSIONS

Application of *D*-optimal design concept to microbial inactivation processes may considerably improve parameters' precision, when compared to commonly used heuristic designs