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A flow system with in-line blank correction applied to the spectrophotometric determination of total iron and chromium (VI) in wastewaters

Keywords Flow system · Total iron · Chromium (VI) · Blank correction · Wastewaters

Abstract A flow system using the sample as the carrier with a propulsion device located after the detector is presented. This approach allows the correction of the intrinsic color of the sample, as it provides baseline adjustment for each sample. A confluence situated just after the selection valve allows the sample composition to be adjusted for the colorimetric measurement. The developed methodology was applied to the colorimetric determination of total Fe and Cr (VI) in wastewaters at 0.1–6.0 mg L⁻¹ and 0.03–1.0 mg L⁻¹, respectively. RSDs lower than 3% and a sampling rate of approximately 40 h⁻¹ were obtained.

Introduction

The controlled dispersion concept associated with flow injection analysis (FIA), introduced by Ruzicka and Hansen in 1975 [1], provided a considerable advancement in developing simple automatic methods. As an evolution to FIA, Ruzicka and Marshall proposed a methodology named sequential injection analysis (SIA) in 1990 [2], which consists of the sequential aspiration of well-defined sample and reagent zones into a holding coil by means of a multi-position valve. The flow is then reversed and the stacked zones are mixed and directed to the detector. These systems have the advantage of considerably saving reagents, and potentially allow different analysis to be

performed without system reconfiguration. Despite these advantages, the absence of confluence points in SIA results in some difficulties providing an efficient mixing between sample and reagents with different physical characteristics, or assuring a constant concentration along the whole plug [3]. Additionally, as in FIA, when the sample presents an intrinsic signal, a blank run might be necessary, which significantly decreases the sampling-rate and repeatability.

To overcome these difficulties, we propose a flow system with the propulsion device situated after the detector, and using the sample as the carrier. The selection of sample or the reagent into the manifold is carried out by an 8-port selection valve. Therefore, the sample or sample/buffer solutions provide the baseline; the signal increment is due to the reagent intercalation. This system was applied to the determination of total Fe and Cr (VI) in wastewaters. These determinations were previously used in FIA to demonstrate the possibility of carrying out simultaneous determinations using the sandwich technique [4].

Experimental

Reagents and solutions

Deionized water and analytical reagent-grade chemicals were used. Solutions were prepared with previously boiled water and were degassed in an ultrasonic bath prior to their introduction into the system. A 0.02% (w/v) ascorbic acid solution, prepared daily, was obtained by dissolution of the solid in a 3.2 mol L⁻¹ ammonium acetate solution. Fe (III) stock solution was prepared by dissolving (NH₄)₂Fe(SO₄)₂·6 H₂O (1.404 g) in a mixture of concentrated H₂SO₄ (20 mL) and water (50 mL); after dropwise addition of 0.2 mol L⁻¹ KMnO₄ solution (until a persistent pink color was obtained), the solution was diluted to 1 L [5]. Fe (II) stock solution was prepared as previously described without the addition of KMnO₄. Working standard solutions containing Fe (III) or Fe (II) in the range 0.3–6.0 mg L⁻¹ were obtained by dilution of the stock solutions in 1 M HCl. A solution of 0.2% 1,10-phenanthroline was also prepared.

For Cr (VI) determination, a solution of 0.075% 1, 5-diphenyl-carbazide (DPC) was obtained by dissolving the solid in ethanol (5 mL) and diluting to 50 mL with 0.75 M H₂SO₄. A 10 mg L⁻¹ Cr (VI) stock solution was prepared by dissolving previously dried

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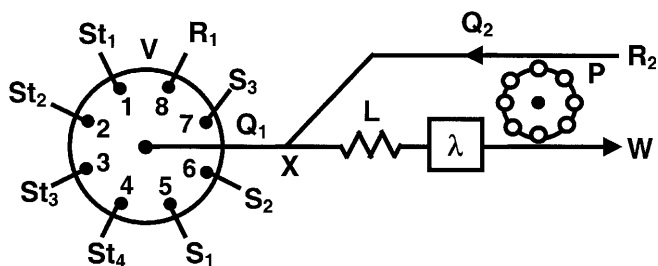


Fig.1 Flow manifold for the determination of total iron and chromium (VI) in wastewaters. *V* selection valve, *P* peristaltic pump, *L* reaction coil (125 cm), *X* confluence, λ spectrophotometer, *W* waste; *S_i* sample, *S_i* standard, *R₁* color reagent, *R₂* 0.02% ascorbic acid in 3.2 M ammonium acetate solution, and sample/standard to total iron and chromium (VI) determinations, respectively, *Q₁* and *Q₂* flow rates

$K_2Cr_2O_7$ in water. Working standards from 0.05 to 1.0 mg L⁻¹ were obtained by dilution of the stock solution.

For Cr (VI) determination, samples were introduced without prior treatment. Regarding total Fe, samples were digested with concentrated HCl and hydroxylamine [5]. Samples or digests that presented large amounts of suspended particles were filtered through a 0.45 μ m membrane.

Apparatus and flow procedure

A Gilson Minipuls 3 peristaltic pump, an 8-port selection valve (Valco VICI C15-3118E), and a Unicam 8625 UV/Vis spectrophotometer with a Hellma 178.710-QS flow-cell were used. All tubing were made of PTFE with 0.8 mm i.d. from Omnifit. A 386 personal computer (Samsung SD700) equipped with an Advantech PCL818L interface card, running homemade software written in QuickBasic 4.5, controlled the selection valve position and the pump rotation speed. Data acquisition was accomplished using the same interface card and a PCLD-8115 wiring terminal board. Signals were also recorded in a Kipp and Zonen BD 111 strip chart recorder.

The manifold developed is depicted in Fig. 1. The flow rates, the timing sequence, and the sample and reagent volumes are listed in Table 1. The sample solutions were used as the carrier, providing a baseline that corresponds to the blank reading. The signal increment, observed when a small amount of reagent is inserted, corresponds to the total Fe or Cr (VI) content. The *R₂* solution was ammonium acetate with ascorbic acid for the total Fe determination and sample for the Cr (VI) methodology. The measurements were taken at fixed time, 18 s for Fe and 13 s for Cr (VI), after the beginning of step 3 of the protocol at 510 nm and 540 nm, respectively. To guarantee constant flow-rates and prevent bubble formation, the propulsion tubes were replaced when a variation of 5% in the flow-rate was observed.

Table 1 Flow system protocol for the determination of total iron and chromium (VI) in wastewater samples

| Step | Valve position | Operation time (s) | Flow rate (mL min ⁻¹) | Volume (μ L) | Description |
|------|----------------|--------------------|-----------------------------------|--------------------|--|
| 1 | 1–7 | 30 | 2.3 | 1095 | Aspirate sample/standard through the detector to create the baseline |
| 2 | 8 | 2/4 ^a | 1.1 | 37/74 ^a | Aspirate color reagent |
| 3 | 1–7 | 40 | 2.3 | 1460 | Aspirate sample/standard through the detector |

^aParameters with different values for total iron and chromium (VI) determination, respectively

Results and discussion

Development of the flow system

Total Fe determination (ferrous and ferric, suspended and dissolved) in wastewaters involves a previous digestion procedure with HCl and hydroxylamine. This treatment also guarantees that possible interfering species such as strong oxidizing agents, cyanide, nitrite, and polyphosphates do not interfere the spectrophotometric determination [5]. After this, the development of a flow system presents two major problems: the color of the samples (requiring a blank reading for each one), and the high acidity of the matrix, leading to a decrease in sensitivity. Additionally, it would be necessary to guarantee no pH differences between samples and standards.

The use of sample as a carrier enabled us to overcome the first of these problems. Regarding acidity, the continuous addition of an ammonium acetate solution to the acidic sample digest at a confluence point provided the proper in-line pH adjustment. After testing different ammonium acetate concentrations, the 3.2 M solution was selected, since lower concentrations led to a decrease in sensitivity. The in-line buffer solution was capable of adjusting the pH of digests with approximately 1 M acidity. This was confirmed by the similar absorbance values obtained when aspirating a 5 mg L⁻¹ standard solution of Fe (III) prepared in 0.8, 1.0, and 1.2 M HCl.

With the length of the tube connecting the selection valve to the confluence point reduced to a minimum, and the length of the reactor (*L*, Fig. 1) pre-set at 125 cm, some optimization procedures were carried out. A 0.2% 1,10-phenanthroline solution was chosen as sensitivity slightly increased up to this level, and then was kept constant. After setting the reagent composition, reagent volumes of 19–76 μ L were tested. A 38 μ L reagent plug was selected as a compromise between sensitivity, repeatability, and reagent consumption.

The ascorbic acid content of the *R₂* solution (Fig. 1) was studied. Although no significant changes of sensitivity between 0.01% and 1.5% (m/v) were noticed, a minimum of 0.02% was chosen to assure that all iron present was in the ferrous state. Absorbance values for the 0.02% solution were registered by using Fe (III) and Fe (II) standard solutions. Results confirmed the absence of differences between both calibrations.

Flow rates of solutions aspirated through the selection valve (*Q₁*) and of the ammonium acetate/ascorbic acid so-

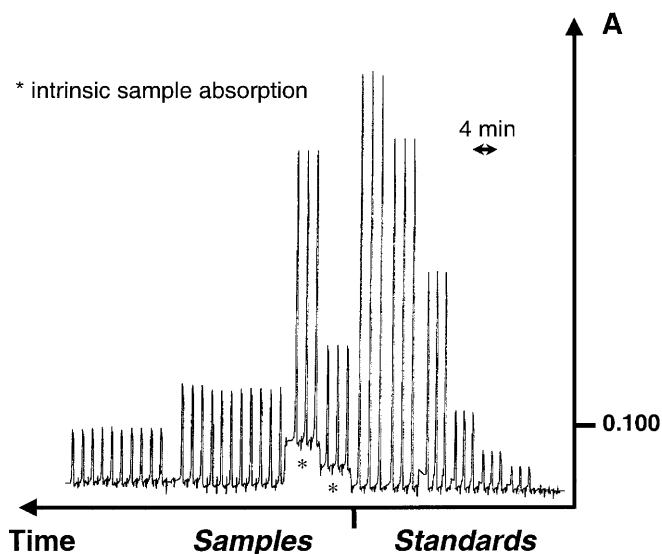


Fig. 2 Recorded output for total iron determination of a set of standards (deionized water, 0.3, 0.5, 1.0, 3.0, 5.0, and 6.0 mg L⁻¹ prepared in 1 M HCl solution) and four different wastewater samples

lution (Q₂) were studied simultaneously. A proportion of two parts of sample solution to one part of ammonium acetate/ascorbic acid solution (R₂) was chosen, as a compromise between sample dilution and pH adjustment, enabling the highest sensitivity. The flow rates adopted were 2.3/1.2 for steps 1 and 3, and 1.1/0.6 mL min⁻¹ for step 2 (Table 1).

Sample aspiration time was also evaluated and set to 30 s for step 1 (Table 1) and 40 s for step 3 to provide a well-defined baseline and a proper return to it (Fig. 2).

When samples with low iron concentration or complex matrix compositions were analyzed, the signal was masked by different refractive indices between solutions (Schlieren effect) [6], and the maximum absorbance did not correspond to the analytical signal. Therefore, an option was taken to perform measurements at a fixed time.

The same system configuration was used for Cr (VI) analysis in water. As there was no need for in-line buffering adjustment, but low detection limits were important, sample was used in both channels (S₁ and R₂ in Fig. 1). The concentration and the volume of the reagent (R₁)

were then optimized. As the reaction occurs under acidic conditions, H₂SO₄ concentrations of 0.25–1 M (in R₁) were studied. The 0.75 M solution was adopted, since higher sensitivity was obtained. Concentrations of 0.025–0.12% of 1,5-DPC were evaluated. Sensitivity increased up to 0.075%, keeping constant afterwards. The reagent volumes of 37–112 μL were tested; 74 μL was finally chosen, as the sensitivity had a significant increase up to this point.

The limit of quantification [7], assessed by ten consecutive injections of the blank solution (1 M HCl for the Fe analysis and water for Cr (VI) determinations) were 0.1 and 0.03 mg L⁻¹, respectively. The calibration curves obtained were: Absorbance=0.105(±0.003)|Fe|+0.001(±0.003); r²=0.9993(±0.0004); Absorbance=0.56(±0.01)|Cr(VI)|-0.001(±0.005); r²=0.9993(±0.0004). The values in parentheses correspond to the standard deviation of seven calibration curves. Possible problems associated with aspirating solutions to the systems, namely variable flow-rates and bubble formation were not significantly observed, as can be perceived by the reproducibility of the calibration curves. For both analyses, the determination rate was approximately 40 h⁻¹.

Application to water samples

Fifteen wastewater samples were analyzed by the proposed flow procedure (C_s) and by the respective reference method (C_r) [5, 8]. For comparison purposes, a linear relationship C_s=C₀+SC_r was established. The equation parameters and the 95% confidence limits are presented in Table 2. These results point out that there is no statistical difference between the two sets of results [9]. Relative standard deviations were lower than 3% (Table 2).

Conclusions

The methodology developed consists of a simple flow system that might be used for different spectrophotometric determinations. For each sample/standard, a blank signal is registered, allowing the correction of the intrinsic color of the sample and the refractive index due to sample matrix composition. This is accomplished using the sample as the carrier stream. Nevertheless, this approach has

Table 2 Parameters of the equation C_s=C₀+SC_r for comparison of the results (mg L⁻¹) obtained by FS (C_s) with those of the reference method (C_r), and the values for relative standard deviation (RSD) corresponding to ten consecutive determinations

| | Equation parameters | | | RSD ^a (%) |
|---------------|-----------------------------|----------------|----------------|------------------------------------|
| | C ₀ ^c | S _c | r ^b | |
| Total iron | -0.02(±0.03) | 1.02(±0.02) | 0.9993 | 2.0 (0.37), 1.4 (1.12), 1.5 (2.62) |
| Chromium (VI) | 0.01(±0.02) | 0.98(±0.03) | 0.9984 | 1.5 (0.40), 1.4 (0.73) |

^aRelative standard deviation measured with five different waters, with the respective concentration (mg L⁻¹) between parentheses. ^bCorrelation coefficient. ^cThe values in parentheses are limits of the 95% confidence intervals

the disadvantage of consuming large amounts of sample, which is not a problem for wastewaters.

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