San Jose State University SJSU ScholarWorks

Master's Theses

Master's Theses and Graduate Research

Fall 2014

The Role of Lithology in Glacial Valley Cross-Sectional Shape in Sierra Nevada, California

Kaai Jensen San Jose State University

Follow this and additional works at: https://scholarworks.sjsu.edu/etd theses

Recommended Citation

Jensen, Kaai, "The Role of Lithology in Glacial Valley Cross-Sectional Shape in Sierra Nevada, California" (2014). *Master's Theses*. 4497.

DOI: https://doi.org/10.31979/etd.pkkt-wf95 https://scholarworks.sjsu.edu/etd_theses/4497

This Thesis is brought to you for free and open access by the Master's Theses and Graduate Research at SJSU ScholarWorks. It has been accepted for inclusion in Master's Theses by an authorized administrator of SJSU ScholarWorks. For more information, please contact scholarworks@sjsu.edu.

THE ROLE OF LITHOLOGY IN GLACIAL VALLEY CROSS-SECTIONAL SHAPE IN SIERRA NEVADA, CALIFORNIA

A Thesis

Presented to

The Faculty of the Department of Geology

San Jose State University

In Partial Fulfillment

of the Requirements for the Degree

Master of Science

by

Ka'ai Jensen

December 2014

© 2014

Ka'ai Jensen

ALL RIGHTS RESERVED

The Designated Thesis Committee Approves the Thesis Titled THE ROLE OF LITHOLOGY IN GLACIAL VALLEY CROSS-SECTIONAL PROFILE IN SIERRA NEVADA, CALIFORNIA

by

Ka'ai Jensen

APPROVED FOR THE DEPARTMENT OF GEOLOGY SAN JOSE STATE UNIVERSITY

December 2014

Dr. Emmanuel Gabet Department of Geology

Dr. Jonathan Miller Department of Geology

Dr. Paula Messina Department of Geology

Dr. Luis Bonachea Department of Biology

ABSTRACT

THE ROLE OF LITHOLOGY IN GLACIAL VALLEY CROSS-SECTIONAL PROFILE IN SIERRA NEVADA, CALIFORNIA

It is commonly inferred that alpine glaciers transform fluvial valleys from V to Ushaped. It has been suggested that, under certain circumstances, glaciers are unable to modify V-shaped valleys and that lithology may play an important role in a glacier's ability to effectively erode bedrock. To test this hypothesis, six glaciated valleys with both U and V-shaped cross sections were chosen in the Sierra Nevada (CA) to examine how lithological properties might affect patterns of glacial erosion: Tenaya Canyon, Tuolumne River, Little Yosemite Valley, the San Joaquin River, the north fork of the King River, and Deadman Canyon. Valley profiles were fitted with the power law, $y = ax^b$, where the exponent b represents the shape of the cross section. Rock mass strength (RMS) values for these sites were determined by field inspection. No clear relationship was found between RMS and valley shape. Although, there was a weak association between measured joint orientation and valley axis in Little Yosemite Valley, the North Fork of the King River, and the San Joaquin, the two variables appear unrelated in Tenaya Creek, Tuolumne River, and Deadman Canyon. These results propose that in the Sierra Nevada granitic batholith, patterns of glacial erosion in granitic rock are not dependent on rock mass strength (as typically measured), while joint orientation may play a minor role.

ACKNOWLEDGMENTS

This project has had many contributors in the last two and a half years, each devoting their time and knowledge to the completion of a venture that has been a long time coming. I would like to first acknowledge my advisor, Manny Gabet, who was the inspiration behind the subject matter, my heartfelt thanks for his continued support, encouragement, insight, and patience. I will treasure his firm belief in the usage of a thesaurus when writing. Behind any good writer is a good editor, and I would like to recognize Tim Carlson and Manny Gabet for their continued efforts in reading and improving this work.

I would also like to recognize the assistance of my committee and the contribution of their knowledge in the writing of this paper. I am indebted, as always, to my mom and brother who have continued to faithfully support me in all of my endeavors. Lastly, my sincere appreciation to all of my resolute field assistants: Tim and Dave Carlson, Gregg Armstrong, and Robert Neusel for braving an often difficult, yet rewarding, field season.

Table of Contents

Introduction	1
Materials and Methods	4
Field Site	4
Methodology	6
Fieldwork	7
GIS Analysis	8
Results	11
Discussion	13
Error Analysis	14
Future Studies	17
Conclusion	2.1

List of Figures

Figure 1. Cross sectional transect of Tuolumne River Valley, Yosemite National Park, CA	22
Figure 2. Map of California showing the locations of the six field sites	23
Figure 3. Ten meter DEM of Tuolumne River Valley, Yosemite National Park, CA	24
Figure 4. Ten meter DEM of Tenaya Canyon, Yosemite National Park, CA	25
Figure 5. Ten meter DEM of Little Yosemite Valley, Yosemite National Park, CA	26
Figure 6. Ten meter DEM of the San Joaquin River, Sequoia National Forest, CA	27
Figure 7. Ten meter DEM of the North Fork King River, Sequoia National Forest, CA	28
Figure 8. Ten meter DEM of Deadman Canyon, Kings Canyon National Park, CA	29
Figure 9. Example of a U and a V-shaped valley from Tuolumne River Valley	30
Figure 10. Illustration of sampling area	31
Figure 11.Matlab curve fit for half a U-shaped transect from Tuolumne River Valley	32
Figure 12. Google image of large scale jointing	33
Figure 13. Graphs showing relationship between RMS and valley shape for all six field sites	34
Figure 14. Graph showing median joint spacing for all six Sierra Nevada valleys	35
Figure 15. Equal area projection stereonets for all six field areas	36
Figure 16. Photo illustrating joint bounded blocks from Tenaya Canyon	37
Figure 17. Plot showing the mode of the delta strike vs. average <i>b</i> for 19 reaches from the six valleys surveyed	38
Figure 18. Percent frequency histogram for the mode of delta strike orientations	39
Figure 19. Photo of perpendicular microfractures from Tenaya Canyon	40
Figure 20. Photo illustrating in situ blocks with fracture spacing greater than 1 meter	41

List of Tables

Table 1. Previous g	glaciations from	the last 3 r	million years	from the Sierra	Nevada42
Table 2. Rock mas	s classification	chart from	Selby (1980)		43

Introduction

Horton (1945) was one of the first to examine the erosional development of fluvial systems from a geomorphologic perspective utilizing the idea that river systems develop V-shaped valleys. V-shaped valley morphology has been used to determine the fluvial origin of river valleys in Alberta, Canada (Smith and Fisher, 1993). Numerous geomorphological studies of Martian valleys have also used Vshaped cross-sections as evidence for the existence of surface water processes on another planet (e.g. Brakenridge et al., 1985; Gulick and Baker, 1990; Baker, 2001). The idea that U-shaped cross-sectional profiles represent a typical glacial valley was introduced by Matthes (1930). This morphology has continued to be considered the classic indicator for glacially carved valleys (e.g. Potter, 1976; Harbor, 1995; MacGregor et al., 2000) and Yosemite Valley in the Sierra Nevada, California, is recognized as one of the iconic symbols representing this classic glacial U-shape. Large alpine glaciers last occupied the Sierra Nevada mountain range approximately 18,000 years ago (Birkland, 1964; Bateman and Wahrhaftig, 1966; James, 2003; Gillespie and Zehfuss, 2004). Matthes (1930) was the first to make a thorough inspection of the extent and morphology of presumed glacial erosion in the central and southern Sierra Nevada. Matthes' initial field work began in Yosemite Valley and expanded to the San Joaquin, Kern, and Kaweah river basins (Matthes 1960, 1965). Although Matthes classified much of Yosemite Valley as U-shaped, he noted areas above Bridal Veil Falls and sections along the Tuolumne River valley as being

V-shaped (Figure 1) and suggested that lithological characteristics, such as the extent of jointing, may play an important role in a glacier's ability to effectively erode bedrock.

Boulton (1979) was one of the earliest works to compare the formation of erosional landforms in two different lithologies: lithified and unlithified sediment. By examining the erosional processes that formed these landforms beneath active glaciers, Boulton (1979) suggested that quarrying was the dominant erosional process in lithified sediment and abrasion was the principal process in eroding unlithified sediment. Research into bedrock control on the subglacial formation of rock steps in Camp Glacier, Oksfjordjokelen (Norway) found that the basal shear stress produced by a flowing glacier was sufficient to remove any joint-bounded bedrock blocks, indicating that glacial erosion by quarrying is an important process in fractured rock (Rea, 1994). Hay (1943) speculated that the Pennine valley in northern England was both V and U-shaped based on the distribution of joint spacing in the rock. He believed that closer joint spacing resulted in more Ushaped valleys. A comparison of glacial valleys in highly jointed metamorphic rocks and non-jointed plutonic rocks in the Southern Alps, New Zealand concluded that the presence of joints and their spacing, orientation, and width contributed to the formation of broader, flatter glacial troughs (Augustinus, 1992). Augustinus (1995) expanded on his 1992 study and examined how rock mass strength (RMS) and a rock's in situ stress-field controlled the direction and extent of slope

modification in glacial valleys. He concluded that broader, shallower valleys developed in areas with low RMS on valley slopes. Brook et al. (2004) compared cross-sectional profiles of glacial valleys in igneous and metamorphic rocks with RMS and rock intact strength in the Scottish Highlands and NW Iceland. Brook et al.'s (2004) study concluded that rock intact strength had a negligible effect on valley morphology and that joint spacing, joint orientation, and joint width were the most effective at explaining cross-section profile morphology in glacial valleys.

Krabbendam and Glasser (2011) analyzed the formation of glacial features, (e.g. whale backs) through the processes of quarrying and abrasion between intact versus fractured sandstone and quartzite in northwest Scotland. They concluded that quarrying is the dominant erosional method in hard rock with dense joint spacing, while softer rocks with greater joint spacing are eroded by abrasion. Cosmogenic radionuclide (CRN) concentrations in bedrock were measured to determine past glacial erosion rates within the Tuolumne River basin in Yosemite National Park and compared with joint density for two units of the Tuolumne Intrusive Series and compared to past erosion rates (Duhnforth et al., 2010). Duhnforth et al. (2010) concluded that when fracture spacing is less than 1 m, quarrying of the bedrock is the dominant process, whereas in less fractured bedrock, abrasion dominates. In a survey of an Alaskan glacial lake, Loso et al. (2004) discovered that coarse material carried as bedload is often underrepresented in most estimates of total sediment yield. Their measurements showed that bedload material comprised 80 – 85% of

the total load backing the interpretation that quarrying is an important process in glacial erosion. Experiments by Sklar and Dietrich (2001) showed that, under fluvial conditions, granite is more resistant to abrasion than most other rock lithologies, supporting the idea that fractures are necessary for efficient erosion of granitic rock.

I hypothesized that rock hardness, joint density, and joint orientation strongly influence the cross-sectional shape of glacially eroded valleys in the Sierra Nevada batholith. Duhnforth et al. (2010) showed that where abrasion is the dominant process, erosion rates are slow, and in valleys where quarrying is the dominant process, erosion rates are much faster. Therefore, regions with abrasion-dominant erosion should experience less valley modification and exhibit a V-shaped cross-sectional profile, while regions with quarrying-dominant erosion should display U-shaped profiles.

Materials and Methods

Field Site

The Sierra Nevada mountain range with its varied glaciated-valley cross-sections presents a unique opportunity to study the effects of lithology on glacial erosional processes. Seven major glacial advances in the Sierra Nevada over the last ~3 million years are recognized by Gillespie and Zehfuss, (2004) (Table 1). Based on glacial maps from Moore and Mack (2008), Alpha et al. (1987), and Matthes (1960, 1965), six previously glaciated regions composed of granitoids within the

Sierra Nevada were selected for this study: the Tuolumne River Canyon, Tenaya Canyon, Little Yosemite Valley, the San Joaquin River Canyon, the Canyon of the North Fork of the Kings River and Deadman Canyon (Figure 2). The Sierra Nevada batholith, comprised of Mesozoic-aged plutonic rocks, forms the majority of the Sierra Nevada mountain range (Bateman and Wahrhaftig, 1966). The Tuolumne River site is the most heterogeneous of the six sites consisting of Cretaceous leucogranite of Ten Lakes, equigranular facies of the Half Dome granodiorite, the Johnson granite porphyry, the coarse grained Mount Hoffman granodiorite, and a Tertiary trachybasalt plug (Bateman et al., 1983). Tenaya Canyon is formed principally of the medium grained Cretaceous equigranular facies of the Half Dome granodiorite (Bateman et al., 1983). Half Dome quartz monzonite and medium grained equigranular facies of Half Dome granodiorite constitutes the majority of Little Yosemite Valley (Bateman et al., 1983). The Mount Givens granodiorite forms the bulk of the Middle Fork of the San Joaquin River valley (Bateman et al., 1971; Huber and Rinehart, 1965). The North Fork of the King River valley runs primarily through Mount Given granodiorite with patches of Finger Peak felsic quartz monzonite at its eastern end (Bateman, 1965). Deadman Canyon is made up entirely of Sugarloaf granodiorite with the exception of small pockets of Quaternary alluvium scattered throughout (Moore and Sisson, 1978).

Methodology

Using 10 m DEMs (digital elevation models) (Figures 3-8) in ArcGIS, I visually confirmed that each valley has profiles that span the range from V to U-shape (Figures 9A and 9B). The valleys were divided into transects which extended from the base of the valley to the upper limits of glacial erosion (~200 m) or the top of the valley, making sure that each transect was drawn perpendicular to elevation contours. The maximum elevation over which effective glacial erosion occurred was selected at two hundred meters (Matthes, 1930; Moscicki, et al., 2006). Each transect was then divided into a series of circles with a radius of ~1.3 m. The circles continued from the base of the valley proceeding up the valley slope perpendicular to glacial flow with subsequent circles located ~10 m above the previous one (Figure 10). Measurements of rock intact strength, rock weathering, joint orientation, joint spacing, joint width, joint continuity, and outflow of groundwater were taken within the area of each circle. This procedure was repeated for approximately 10 transects along each of the longitudinal profiles of Tuolumne River valley, Tenaya Canyon, Little Yosemite Valley, the San Joaquin River valley, the North Fork of the King River Valley and Deadman Canyon. An attempt was made to use transects from valley walls that were directly opposite each other in order to delineate the cross-sectional shape, but due to accessibility problems in many areas, this was often not feasible.

Fieldwork

An N-type Schmidt hammer was used to determine the rock intact strength. This instrument is extremely sensitive to discontinuities in a rock and so should not be used on rock that is fissile, laminated or closely foliated. Goudie (2006) recommends that the Schmidt hammer be used on large blocks of rock weighing more than 25 kg avoiding surface irregularities as they may influence the results and so tests should be done on a rock surface that is as free from defects as possible. The effectiveness of the Schmidt hammer is also improved when it is used parallel to the force of gravity (Goudie, 2006), although in instances where measurements cannot be taken perpendicular to the rock face a correction can be made using the Schmidt hammer manual.

Following Selby's (1980) RMS classification chart, each of the measured parameters was assigned a range of values that were grouped into five classes. This range of values was then assigned an "r" rating reflecting the strength of the rock. For example, an average spacing between measured joints of 0.6 m falls within the range of 0.3-1 m and so was given an "r" rating of 21, indicating a rock of moderate strength (Table 2). The "r" rating number for rock intact strength, rock weathering, joint orientation, joint spacing, joint width, joint continuity, and outflow of groundwater were then summed to determine the total RMS value ranging from 1 to 100. A very weak rock has an RMS value of < 26 and a very strong rock has an RMS value of 91-100.

For the purpose of this research, a joint is defined as all discontinuities throughout the bedrock (Selby, 1980; Palmstrom, 2005). The orientation of the fracture is the attitude of the joint in space as defined by its strike and dip direction (Gumede and Stacey, 2007). Spacing is the perpendicular distance between two joints (Palmstrom, 2005), and joint width is the width of the aperture between two adjacent joint walls (Selby, 1980). Any joint that terminates at another joint is considered discontinuous (Palmstrom, 1995), all others are continuous. Joint infill is any material that is of dissimilar composition to that of the rock type in which the joint is found (Selby, 1980). Following Palmstrom (2005) and Selby (1980) joints less than 5mm in length (microjoints) were not considered as they do not contribute significantly to the weakening of rock.

GIS Analysis

A quantitative analysis of valley cross-sectional morphology adopted by some (e.g., Brook et al., 2004; Yingkui et al., 2001; Augustinus 1995; Hirano and Aniya, 1988; Graf, 1970) uses the power law,

$$y = ax^b \tag{1}$$

where *x* is the horizontal distance (in meters) measured from the center of valley, *y* is the height (in meters) from the center to that point, and *a* and *b* are constants with increases in *b* toward 2.0 reflecting a broader U-shaped valley. A *b* value of 1.0 indicates a narrow V- shaped valley (Brook et al. 2004; Yingkui et al. 2001). A MATLAB (2012) program was used to calculate the value of *b* from a best curve fit

from Eqn. 1 with b values \leq 1.5 defined as a V-shape and b values > 1.5 as U-shaped. For example, Figure 11 shows a b value of 1.78 demonstrating a U-shaped cross-sectional profile.

The form ratio (F_r) was used by Hirano and Aniya (1988) in order to better understand where on the spectrum between V and U-shape the cross section of glacial valleys fell. The form ratio is equal to D/W, with D defined as the valley depth and W as the valley width. Hirano and Aniya (1988) defined two regimes based on their findings; the Rocky Mountain regime where b values rise with increasing F_r and the Patagonia and Antarctica regimes where larger b values are associated with decreasing F_r . They indicated that the form ratio could be used independently of any other valley shape analysis. Several other studies such as (Brook et al., 2004) have followed this example, however, there is disagreement over the proper usage of the form ratio Harbor (1992) suggested that the form ratio should only be used in conjunction with the power law, stating it has no merit on its own due to the fact that two valleys could have the same form ratio but two very different profile shapes. Based on these arguments, the form ratio as proposed by Hirano and Aniya (1988) was not used in this study.

There is some error associated with determining *b* values. James (1996) compared the usefulness of the power law (Eqn. 1) and the quadratic equation for determining the cross-sectional shape of glacial valleys,

$$y = mx^2 + nx + p \tag{2}$$

where y is elevation above sea level, x is the lateral distance from the valley's axis; m, n, and p are constants with m representing valley form. After examining three valleys from the northwestern Sierra Nevada James (1996) concluded that the value of b can differ depending on operational decisions of where to begin each curve fit analysis. The parameter b can be sensitive to valley bottom morphology and so, in areas where processes such as fluvial action or rock fall debris have modified the valley floor, b can misrepresent the true valley shape. Values of b can also be significantly altered based on the terminating height chosen for the curve fits. For example, a curve fit analysis of a transect in Little Yosemite Valley at a height of 200 m produces a b value of 1.35, but a height of 50 m produces a b value of 1.97, two very distinct representations of valley cross-sectional shape. It is also essential that all transects be drawn perpendicular to topography as any deviation can again result in a b value that is not truly representative of valley form.

James (1996) concluded that a quadratic equation was less sensitive to valley bottom morphology errors although convexity, asymmetry, and polymorphism in the valley cross-sectional profile made the usage of the quadratic equation inappropriate. Due to the high amount of visual complexity observed within many of the valleys selected for field studies and widespread acceptance, the power law was selected as the most representative equation of valley form for this study. Mitigation of the various issues mentioned above was attempted through the selection of transects dominated by exposed bedrock with little or no signs of other

processes having operated on the area, limiting the curve fit height to a maximum glacial elevation of 200 m, and taking all transects perpendicular to the valley axis.

Large scale joints (>0.5 km) measured from aerial photographs were also incorporated into the analysis. Each of the six valleys was divided into 5 km² areas extending along the length of the valley where measurements had been taken in the field. The strike of glacial flow and all visible joints were measured using the ruler tool in Google Earth® at an eye altitude of ~10,920 m (Figure 12). The difference in orientation between the large scale joints and valley trend, the delta strike, was also calculated.

Results

An independent sample t-test was run on the RMS and b values from the six river valleys. The average RMS value for U-shaped glacial valleys (78.13 \pm 9.19 1σ) was not significantly different (α = 0.05) than the average RMS value for V-shaped glacial valleys (75.25 \pm 9.40 1σ) (independent samples t-test: n = 42, p = 0.476). There was no apparent correlation between b and RMS (Figure 13), suggesting that valley profiles are not dependent on rock mass strength.

Despite this lack of correlation, there are several points worth noting. Each valley, with the exception of Deadman Canyon, has cross-sectional profiles that range from strongly V-shaped to distinctly U-shaped. Although the *b* values from Deadman Canyon imply that it is predominantly U-shaped, it too has a spectrum of profiles from barely U- shaped to highly U-shaped. Interestingly, Deadman

Canyon was the only valley to have a slight negative linear relationship between RMS and *b* (Figure 13). In addition, all the valleys except Deadman Canyon have at least one profile with two halves of the transect with different *b* values. For example, Tenaya Canyon has a profile with a *b* value of 1.9 for the left side and 1.2 for the right side.

Because it has been suggested that the distance between joints plays a role in valley profile shape (Duhnforth, et al. 2010), a plot of joint spacing vs. b was created to determine if such a relationship could be identified from the current study's field data (Figure 14). Joint spacing values extended from 0.3 - 20 m with the majority of spacing falling between 0.4 - 2.5 m. Values for b ranged from 3.4 - 1.0 with no discernible correlation with joint spacing.

In order to investigate the role of joint orientation, poles to the plane for the strike and dip of each of the smaller scale joints were plotted on an equal area lower- hemisphere stereonet. All of the valleys have a significant grouping of shallowly dipping joints with clusters of vertical to sub-vertically dipping joints (Figure 15), indicating the presence of two distinct perpendicular joint sets which can form fractured rock blocks of sufficient size for quarrying (Figure 16).

A plot of b vs. the mode of the delta strike (Figure 17) suggests a clustering of joint direction between 25° and 45° indicating that the majority of the jointing is obliquely oriented to the valley trend and glacial flow direction. A percent frequency histogram (Figure 18) exhibits a similar tendency in that the delta strike

values with the two highest percentages are 45° and 25°. The delta strike with the third highest percentage is 5° which appears to deviate from figure seventeen's results.

Discussion

Former glacial valleys that have retained their presumed original fluvial shape in Scotland and Iceland were documented by Brook et al. (2004). Their study focused on how bedrock properties in five morphologically and lithologically distinct terrains influenced valley morphology away from continent-continent collision zones. The power law, form ratio, and quadratic equation were used as measures of glacial valley cross- profile shape that were then compared to rock mass strength. Their results showed that while valleys with lower rock mass strength values have a distinct U-shape and valleys with higher rock mass strength values tend to be deeper with a considerably less pronounced U-shape profile, the rock mass strength properties that are most important in valley morphology are joint width, spacing, and orientation.

Augustinus (1992) also conducted a similar study in the Southern Alps of New Zealand using a slightly modified version of Selby's (1980) RMS classification and intact strength based on Schmidt hammer measurements. Augustinus (1992) used the form ratio, the shape factor, glaciated valley joint density, and the coefficients a, b and c from the quadratic formula to quantify valley morphology in granite, gneiss, greywacke, and schist. A lack of relationship was found between the rock

intact strength properties and morphometric variables such as the form ratio, valley cross-sectional shape, and the shape factor, but a positive relationship was shown when plotting valley profile against rock mass strength, indicating steeper slopes and narrower valleys in regions with higher rock mass strength.

Error Analysis

A comparison of average rock mass strength (RMS) and valley shape (*b* from Eqn. 1) from Brook et al.'s (2004) data and the current study was done to corroborate the experimental techniques of the present study. Brook et al.'s (2004) average RMS value of 78.75 and average *b* value of 1.48 in granite agree reasonably well with the current study's average RMS of 78.91 and average *b* value of 1.42, confirming that my experimental techniques of the present study are acceptable. A comparison of *b* values could not be made with Augustinus' (1992) data as he did not use the power law, but his average RMS value of 82.5 is not significantly greater than 78.7 or 78.9.

Despite demonstrating a lack of correlation between rock mass strength and valley shape, this study shows that there are both V and U-shaped profiles throughout formerly glaciated valleys within the central and southern Sierra Nevada. This brings forth the question of how these two morphologies can exist simultaneously in an area of such extensive glaciation. The idea that rivers are capable of carving U-shaped valleys and that the cross-sectional profiles within the Sierra Nevada range were set by pre-glacial fluvial processes was suggested by Schaffer (1997). This concept is illustrated with Zion Canyon in Zion National

Park, Utah. It has a broad, flat floor that gradually merges with walls whose heights rival that of Yosemite Valley to form a wide U-shaped valley (Grater, 1947). Zion Canyon consists predominantly of the Navajo sandstone which can be as resistant to abrasion as granite (Sklar and Dietrich, 2001). There are two factors that undermine the strength of this particular type of sandstone. The first is a weaker cement, making it less resistant to the sapping processes which are known to form broad, flat-floored U-shaped profiles (Kochel and Piper, 1986; Gulick and Baker, 1990). The second is the presence of closely spaced joints and joints of various lengths, which lowers the rock's resistance to erosion even further (Bahat et al., 1995). These two factors, combined with extensive biannual flooding events, have led to the U-shaped profile of Zion Canyon, an area that has never been previously glaciated (Grater, 1947). If Schaffer's (1997) interpretation is correct, similar processes to the ones operating in Zion Canyon can be applied to the Sierra Nevada valleys during their formation.

That the Sierra Nevada mountain range was formed during the Cretaceous is not a new concept (e.g. Wahrhaftig, 1965). A recent review of the numerous studies supporting this concept (Gabet, 2014) indicates that there is sufficient evidence to justify an origination of the Sierra Nevada during the Cretaceous. Instead of the current warm temperate climate (Kottek et al., 2006) with seasonal rains, western California was wet and tropical during the early Cretaceous through the mid-Eocene (Minnich, 2007). A warmer and wetter climate leads to increased chemical

weathering of the felsic minerals within granitic rocks, leaving the more resistant minerals such as quartz and feldspar to a loose material called gruss (White, 1945; Hall et al., 1989). The presence of joints increases the surface area available for weathering which, coupled with a tropical environment, increases granite erosion rates (White, 1945). This weakening of a normally resistant rock may have led to increased fluvial erosion within the Sierra Nevada during the Cretaceous/Paleogene and created morphologies similar to that of Zion Canyon today.

Two separate processes in an open system leading to the same result are known as equifinality (Grezov and Drazin, 1997). Equifinality is an idea that has been used extensively in psychology, biology, medicine, and a variety of other fields. Recently, it has been applied to the field of geological sciences including aspects such as the modeling of hydrologic and geomorphic systems (e.g., Beven, 1996; Phillips, 1997; Beven, 2006), paleoenvironmental reconstruction of alluvial fans in New Zealand (Nicholas and Quine, 2010), and comparison of erosional processes in the formation of shore platforms (Cruslock et al., 2010). Campbell and Twidale (1995) reviewed distinct landforms associated with granite and their development through specific mechanisms and demonstrated that multiple processes are able to produce the same topographic feature. This idea of equifinality can be applied to the formation of Sierra Nevada valleys. In his investigation of Yosemite Valley, Matthes (1930) acknowledged that up to 300 m of the valley's depth could have

been due to fluvial erosion, supporting the interpretation that rivers may have contributed a much greater proportion of valley development than originally thought.

Future studies

The development of joints within the Sierra Nevada presents the most problematic aspect in understanding their role in glacial erosion and valley morphogenesis. The presence of exfoliation jointing, shallowly dipping fractures parallel to the surface on which they form, was noted by Bergbauer and Martel (1999) and Martel (2006) at Olmstead Point in Yosemite National Park. In addition to these shallowly dipping breaks in the rock, vertical and sub-vertical jointing is also recognized in the Sierra Nevada (Segall, 1984), yet little is known about their formation relative to glaciation and their temporal distribution. Based on an age of ~80 mya from K/Ar dating of chlorite and epidote K/Ar within fractures in the Sierra Nevada, Segall et al. (1990) put initial joint formation at shortly after the intrusion of the pluton. This implies that some jointing within the Sierra Nevada is pre-glacial, but the rate at which new joints form is unknown. Many microfractures were observed in the field (Figure 20); presumably, these will evolve into joints large enough and deep enough for the next glacier to quarry. If the time-span for the development of these microfractures into extensive jointing is longer than the time between glaciations, the bedrock may not be sufficiently fractured to induce quarrying, thus reducing the effectiveness of glacial erosion. A quantification of the timescales over which jointing is sufficient for glaciers to quarry rock is, thus, essential in order to better constrain the rates of glacial erosion.

Studies into fracture mechanics have concluded that the stresses generated during glaciation have the potential to contribute to the acceleration of jointing within the bedrock (Leith, et al., 2011; Hallet 1995; Morland and Boulton, 1975). Under glaciers, high stresses sufficient to form fractures, can occur along the edges of rock steps (Hallet, 1995; Iverson, 1991; Morland and Boulton, 1979). Harbor (1995) has emphasized the importance of these sub-glacial joints as weaknesses that can then be exploited for further erosion by future glacial events. While it is possible that sub-glacial stress induced fracturing may be the principal method through which granite is sufficiently weakened, spatial constraints on joint propagation must also be understood.

Anderson (2014) investigated seasonal variations on the subglacier hydrologic system and progression of surface irregularities in bedrock over thousands of years. A model of glacial erosion supported the importance of subglacial joint formation and block size in the quarrying of rock. If a block is too large, a glacier will be unable to transport it through quarrying and abrasion becomes the primary form of rock removal, reducing the rate of erosion. Field observations from the current study not only noted the occurrence of joint bounded blocks (Figure 16) at varying heights up the valley walls in each of the six sites visited, but several of the valley

blocks were found with glacial polish on their upper surfaces (Figure 19). Many of the observed blocks also have joint spacing within the 1-3 m range noted by Duhnforth et al. (2010). This observation along with other models of quarrying processes (Iverson, 1991; Cohen et al., 2006; Hooyer, et al., 2012; Iverson, 2012), suggest that there was insufficient fracturing of the blocks during glaciation for effective quarrying.

Although many studies agree that closely spaced joints are the key to effective glacial quarrying, one element that has not yet been closely examined is the vertical propagation of joint growth. In order for the formation of the stepped topography that is needed to promote quarrying (Cohen, 2006; Hooyer, 2012; Iverson, 2012), perpendicular joint sets must either be continuously formed through sub-glacial stresses or be present at depth. Jahns (1945) observed that some exfoliation joints can extend up to ~100 m at depth. Ziegler et al. (2013), attempted to date exfoliation joints in the Central Alps by mapping their distribution above and below ground and correlating it to various fluvial and glacial erosion patterns within valleys. Their results indicate that exfoliation joints can occur at depths up to 240 m, that they are most established in massive granitic or gneissic rocks away from faulting, and that there were four distinct episodes in which exfoliation joints were generated (lower Pleistocene, middle Pleistocene, upper Pleistocene, and Late Glacial to Holocene).

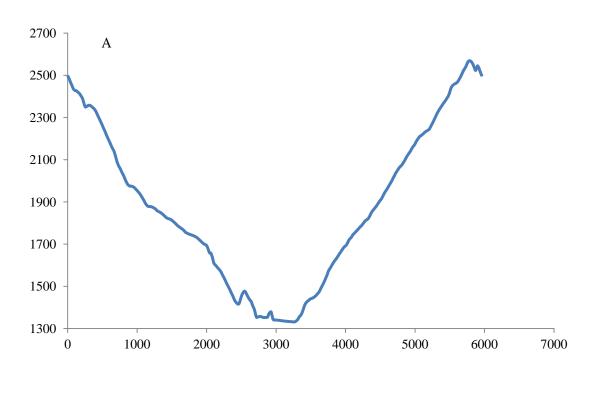
While it is acknowledged that joint orientation is an important aspect controlling

rock mass strength (e.g. Augustinus, 1995), very little research has been done to understand its relationship with quarrying. Moore et al. (2009) studied the relationship of rock mass strength properties to rock falls in the north-central Sierra Nevada. They found that although higher rock mass strength did correlate to fewer rock falls, the most important factor in controlling rock fall rate was the orientation of the jointing. Rock wall with joints dipping into the faces were less prone to rock falls than areas with joints dipping out of the rock face. Similarly, recognizing the spatial patterns of jointing and how they affect the mechanism of glacial quarrying is key to being able to fully interpret glacial erosion rates and their ability to alter the landscape. This is particularly important in the Sierra Nevada with its diverse jointing patterns.

Augustinus (1992) and Harbor (1995) have argued that in addition to comparisons such as rock mass strength versus valley cross-sectional profile; the age, mode, and rate of rock slope development should be taken into consideration when evaluating valley morphogenesis. Rock falls have been documented in the granitic cliffs of Yosemite National Park that are associated with exfoliation jointing (Stock et al., 2011). The existence of rock falls throughout this region of the Sierra Nevada is indicative of active erosional processes other than glacial and fluvial which in the area. The extent to which rock falls have contributed to the evolution of valley morphology is a final area of research that should be further explored.

Conclusion

Many studies have shown that V-shaped valleys tend to develop in strong rocks and U-shaped valleys are form in weak rock. Data collected for this study matched closely with the average rock mass strength and b values of previous studies but did not find an association between rock mass strength and valley cross-sectional profile. A better comprehension of subaerial processes such as rock falls and their role in glacial valley morphogenesis is needed before rock mass strength can be linked to valley morphology. A more thorough understanding of the temporal constraints on joint formation in granite and its relationship to glacial cycles will also help to clarify glacial erosion rates in the Sierra Nevada. Rock is an anisotropic material which tends not to conform to idealized models of glacial erosion. The Sierra Nevada is a complex system with an equally complicated geologic history, and the evolution of the valleys within this system may involve considerably more determinants than that of simply abrasion and quarrying. It is likely that the erosional processes which shape valleys are not dominated by a single process but that multiple interactions are occurring at the subglacial interface, and that the idea of equifinality can be applied to the formation of the Sierra Nevada valleys.



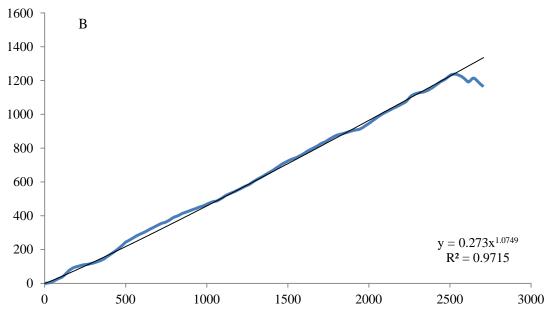


Figure 1. Transect from Tuolumne River valley, Yosemite National Park, California (A). A *b* value of 1.07 indicates a linear profile or V-shaped valley (B).

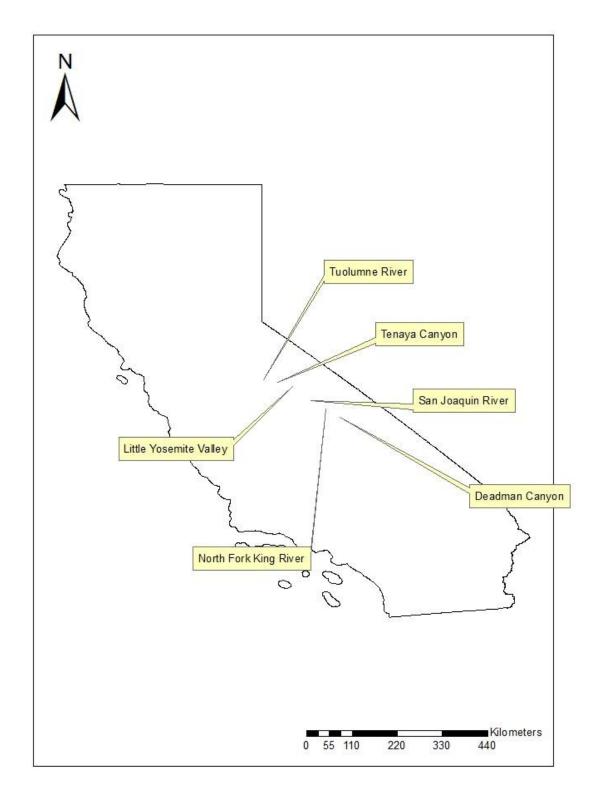


Figure 2. Map of California showing the locations of the six field sites.

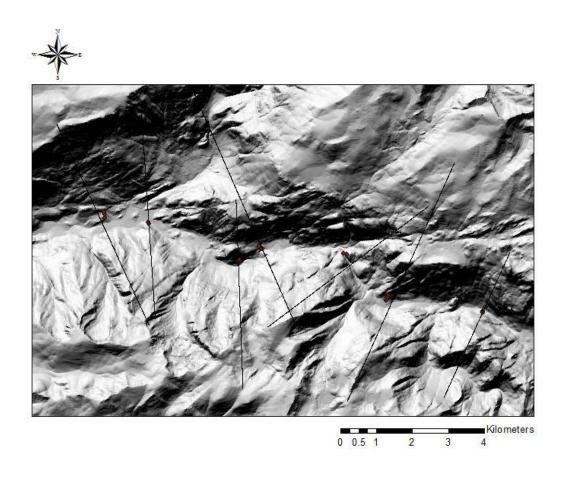


Figure 3. Ten meter DEM of Tuolumne River valley, Yosemite National Park, California. Dots indicate locations of measurements taken along transect (black lines).

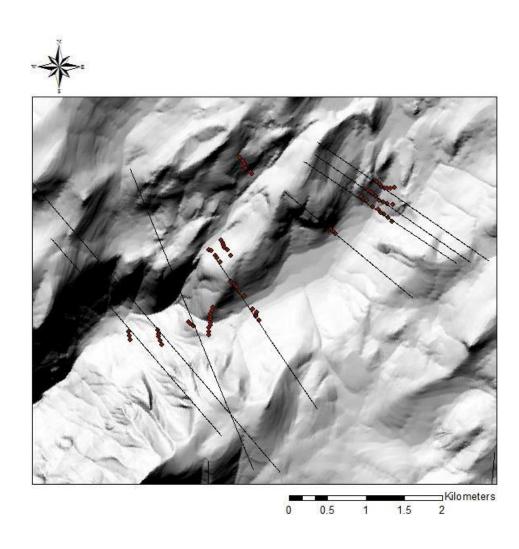


Figure 4. Ten meter DEM of Tenaya Canyon, Yosemite National Park, California. Dots indicate locations of measurements taken along transects (black lines)

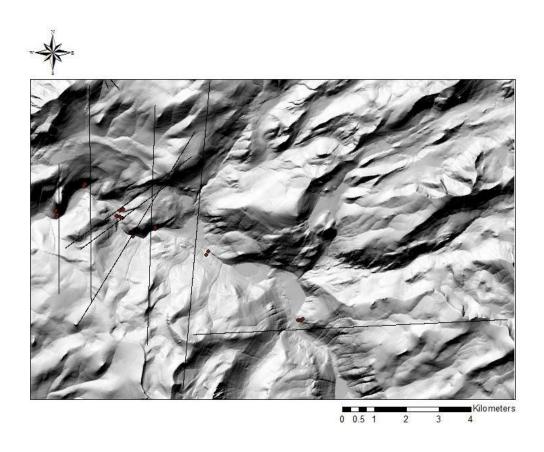


Figure 5. Ten meter DEM of Little Yosemite Valley, Yosemite National Park, California. Dots indicate locations of measurements taken along transect (black lines).

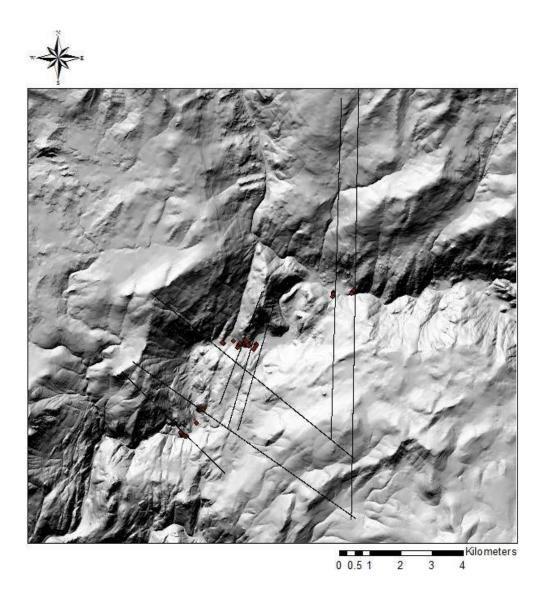


Figure 6. Ten meter DEM of San Joaquin River, Sequoia National Forest, California. Dots indicate locations of measurements taken along transect (black lines).

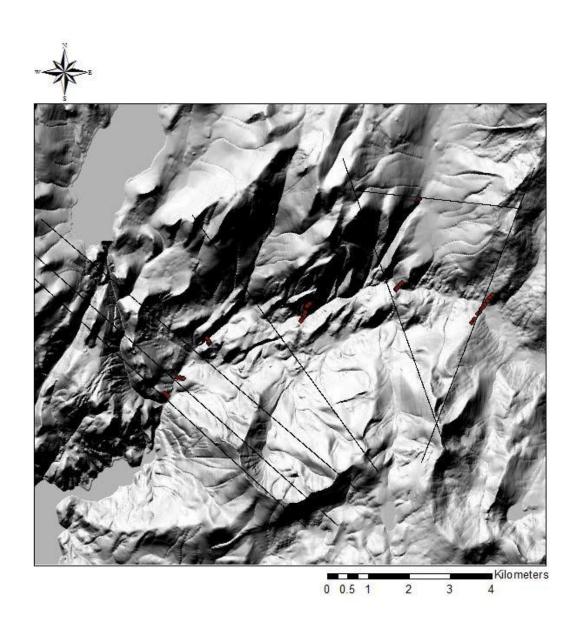


Figure 7. Ten meter DEM of North Fork King River, Sequoia National Forest, California. Dots indicate locations of measurements taken along transect (black lines).



Figure 8. Ten meter DEM of Deadman Canyon, Kings Canyon National Park, California. Dots indicate locations of measurements taken along transect (black lines).

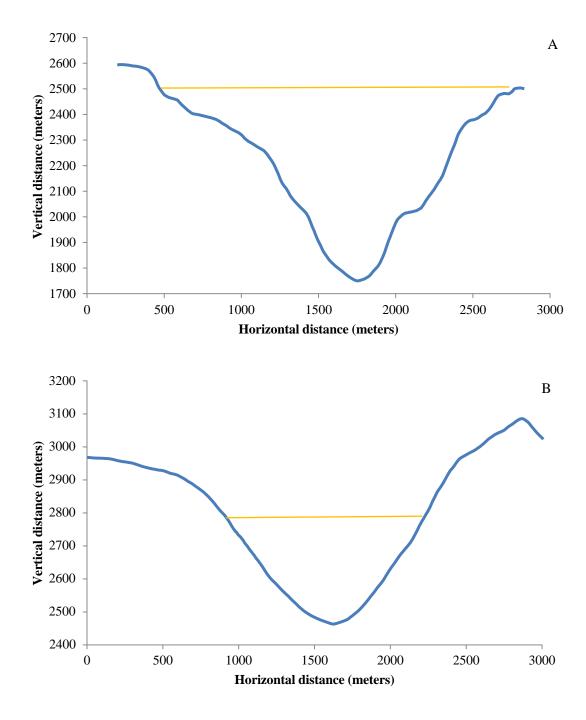


Figure 9. Example of a V-shaped valley (A) and a U-shaped valley from Tuolumne River valley, Yosemite National Park, California (B). The grey lines show the approximate height of the glaciers taken from Matthes (1930) map.

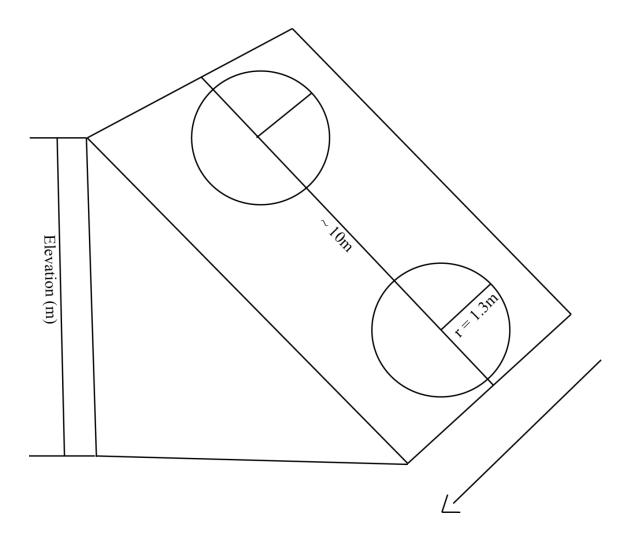


Figure 10. Illustration of one half of a glacial valley with circles indicating an area of $\sim 5 \text{ m}^2$ in which all field measurements were taken. Areas are spaced $\sim 10 \text{ m}$ apart. Arrow shows down valley direction.

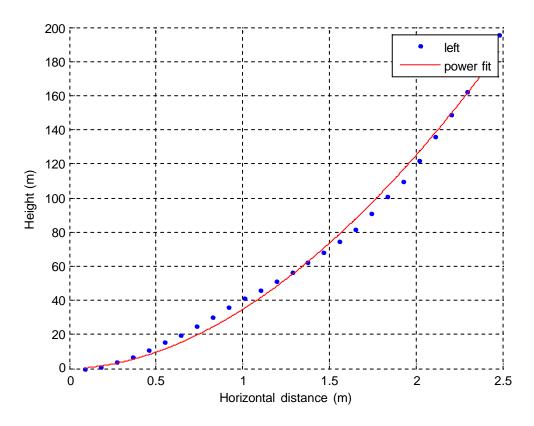


Figure 11. Matlab curve fit for the left half of a transect in Tuolumne River valley with a *b* value of 1.8 indicating a U-shape.

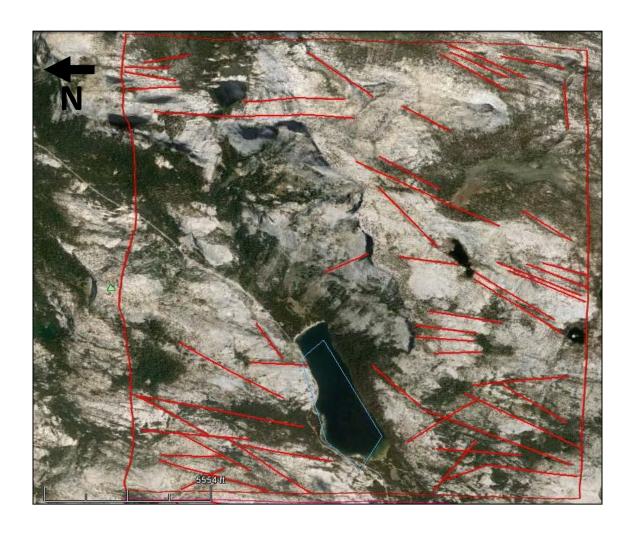


Figure 12. Google Earth image of large scale jointing (> 0.5 km) in a 5 km² area near Tenaya Lake, Yosemite National Park, California with an eye altitude of $\sim 10,920 \text{ m}$.

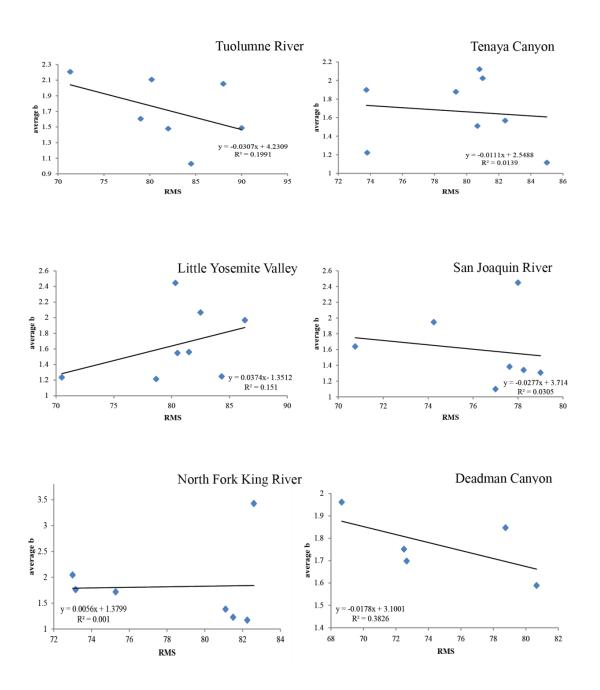


Figure 13. Graphs showing valley shape (b) and rock mass strength (RMS) for each of the six sites surveyed. All six show no correlation between b and RMS with the highest R^2 value being 0.38 for Deadman Canyon.

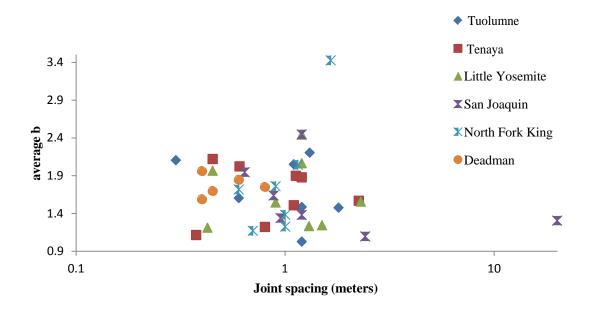


Figure 14. Median joint spacing for the six Sierra Nevada valleys plotted against the average valley cross-sectional shape (b). Although there is no relationship between joint spacing and b the majority of the spacing values fall between 0.3 m and 2.4 m, roughly the ideal distance for glacial quarrying. Note logarithmic scale on x-axis.

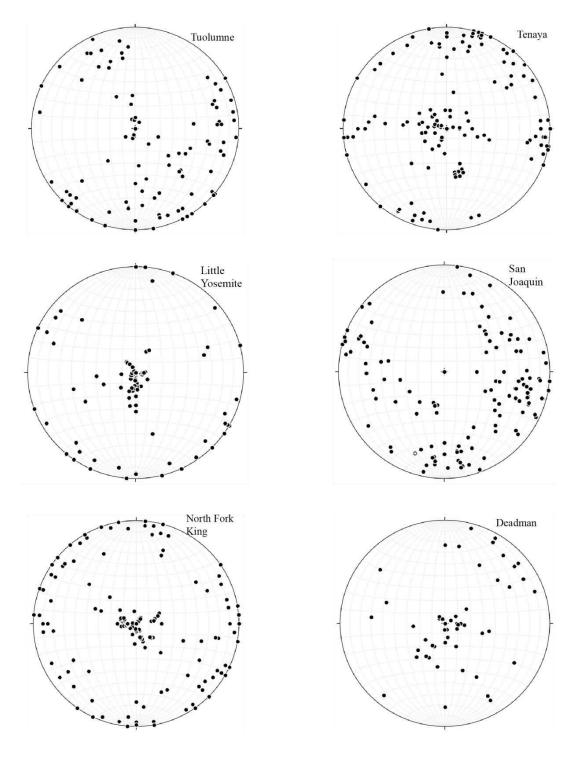


Figure 15. Equal area projection stereonets of the six field sites. All six stereonets show a distribution of shallowly dipping joints as well as sub-vertical to vertically dipping joints. Each valley exhibits a number of perpendicular joints which form fracture bounded blocks, an ideal geometry for glacial quarrying.



Figure 16. Photo of joint bounded blocks in Tenaya Canyon with < 1 m joint spacing and stepped topography, an ideal situation for glacial quarrying. Brunton compass for scale.

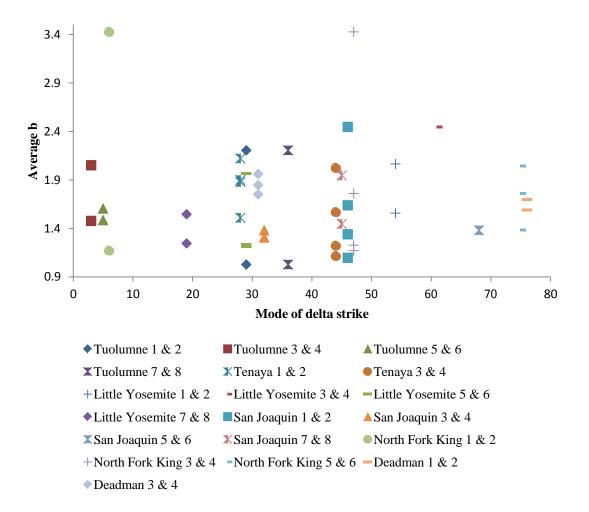


Figure 17. Mode of the delta strike vs. average b for 19 reaches from the six valleys surveyed. The clustering of the joints implies that the majority of the large scale joint orientation is $20^{\circ} - 45^{\circ}$, obliquely oriented to the longitudinal axis of the valley, although no correlation between delta strike and b values is evident.

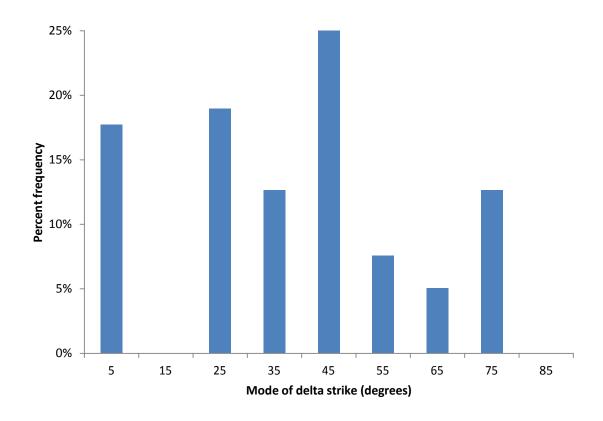


Figure 18. Percent frequency histogram of the mode of delta strike orientations. Note the lack of jointing at $5^{\circ} - 25^{\circ}$ and above 75° .



Figure 19. Photo of perpendicular microfractures from Tenaya Canyon.



Figure 20. Photo illustrating *in situ* blocks with joint spacing < 1 m with glacial polish on their surfaces indicating they were either not moved during glaciation or joints formed post-glacial.

Table 1. Previous glaciations from the last ~3 million years within the Sierra Nevada mountains, California (Gillespie and Zehfuss, 2004.

Glaciation	Mean age (ka)
Recess Peak	14.2-13.1
Tioga (retreat)	15-14
Tioga (start)	21-20
Tenaya	31
Tahoe	50-42
Sherwin	c. 820
McGee	2,700-1,500

Table 2. Rock mass strength (RMS) classification chart from Selby (1980).

	1	2	3	4	5
Parameter	Very strong	Strong	Moderate	Weak	Very weak
Intact rock strength (N- type Schmidt	100 – 60	59 – 50	49 – 40	39 – 35	34 – 10
Hammer 'R')	R:20	R:18	R:14	R:10	R:5
Weathering	Unweathered	Slightly weathered	Moderately weathered	Highly weathered	Completely weathered
	R:10	R:9	R:7	R:5	R:3
Spacing of joints	> 3 m	3 -1 m	0.99 – 0.3 m	299 – 50 mm	< 50 mm
	R:30	R:28	R:21	R:15	R:8
Joint orientations	Very favorable. Steep dips into slope, cross joints interlock. R:20	Favorable. Moderate dips into slope. R:18	Fair. Horizontal dips, or nearly vertical (hard rocks only) R:14	Unfavorable. Moderate dips out of slope. R:9	Very unfavorable. Steep dips out of slope. R:5
Width of joints	< 0.1 mm R:7	0.1 – 1 mm R:6	0.99 – 5 mm R:5	4.9 – 20 mm R:4	> 20 mm R:2
Continuity of	None	Few	Continuous,	Continuous,	Continuous,
joints	continuous	continuous	no infill	thin infill	thick infill
	R:7	R:6	R:5	R:4	R:1
Outflow of groundwater	None	Trace	Slight < 25 l/min/10 m2 R:4	Moderate 25 – 125 1/min/10 m2	Great > 125 1/min/10 m2 R:1
Total rating	100-91	90-71	70-51	50-26	<26
10tai ratilig	100-71	70-71	10-31	30-20	\ZU

References

Allmendinger, R., 2014, Stereonet 9, http://www.geo.cornell.edu/geology/faculty/RWA/programs/stereonet.html.

Alpha, Tau R., Wahrhaftig, Clyde, and Huber, N.K., 1987, Oblique map showing maximum extent of 20,000-year-old (Tioga) glaciers, Yosemite National Park, Central Sierra Nevada, California, scale varies with direction, 1 sheet.

Augustinus, P. C. 1995, Glacial valley cross-profile development: the influence of in situ rock stress and rock mass strength, with examples from the Southern Alps, New Zealand: Geomorphology, v. 14, p. 87-97.

Augustinus, P. C., 1992, The influence of rock mass strength on glacial valley cross-profile morphometry: A case study from the Southern Alps, New Zealand: Earth Surface Processes and Landforms, v. 17, p. 39-51.

Bahat, D., Grossenbaker, K., and Karasaki K. 1995, Investigation of Exfoliation Joints in Navajo Sandstone at the Zion National Park and in Granite at the Yosemite National Park by Tectonofractographic Techniques: Lawrence Berkeley Laboratory, University of California, Earth Sciences Division, p. 1-70.

Baker, V.R. 2001, Water and the Martian landscape: Nature, v. 412, p. 228-236.

Bateman, P.C. 1992, Plutonism in the Central Part of the Sierra Nevada Batholith, California: U.S. Geological Survey Paper 1483, p. 1-194.

Bateman, P.C., Kistler, R.W., Peck, D.L., and Busacca, A. 1983, Geologic map of the Tuolumne Meadows quadrangle, Yosemite National Park, California: U.S. Geological Survey, Geologic Quadrangle Map GQ-1570, scale 1:62,000, 1 sheet.

Bateman, P.C., Lockwood, J.P., and Lydon, P.A. 1971, Geologic map of the Kaiser Peak quadrangle, central Sierra Nevada, California: U.S. Geological Survey, Geologic Quadrangle Map GQ-894, scale 1:62,500, 1 sheet.

Bateman, P.C. and Wahrhaftig, C. 1966, Geology of the Sierra Nevada: Geology of northern California: California Division of Mines and Geology Bulletin, 190, p. 107-172.

Bateman, P.C., 1965, Geologic map of the Blackcap Mountain quadrangle, Fresno County, California: U.S. Geological Survey, Geologic Quadrangle Map GQ-428, scale 1:62,500, 1 sheet.

Bergbauer, S. and Martel, S.J. 1999, Formation of joints in cooling plutons: Journal of Structural Geology, v. 21, p. 821-835.

Beven, K., 1996, Equifinality and Uncertainty in Geomorphological Modeling, *in* eds. Rhoads, B.L. and Thorn, C.E., The Scientific Nature of Geomorphology: Proceedings of the 27th Binghamton Symposium in Geomorphology held 27-29 September 1996, p. 291-313.

Beven, K., 2006, A manifesto for the equifinality thesis: Journal of Hydrology, v. 320, p.18-36.

Birkland, P.W. 1964, Pleistocene glaciation of the northern Sierra Nevada, north of Lake Tahoe, California: The Journal of Geology, v. 72, p. 810-825.

Brakenridge, G.R., Hewsom, H.E., and Baker, V.R., 1985, Ancient hot springs on Mars: Origins and paleoenvironmental significance of small Martian valleys: Geology, v. 13, p. 859-862.

Brook, M.S., Kirkbride, M.P., and Brock, B. W. 2004, Rock strength and development of glacial valley morphology in the Scottish Highlands and northwest Iceland: Geografiska Annaler, v. 86, p. 225-234.

Boulton, G.S., 1979, Process of Glacier Erosion on Different Substrata: Journal of Glaciology, v. 23, p. 15-38.

Cohen, D., Hooyer, T.S., Iverson, N.R., Thomason, J.F., and Jackson, M. 2006, Role of transient water pressure in quarrying: a subglacial experiment using acoustic emissions: Journal of Geophysical Research, v. 111. DOI: 10.1029/2005JF000439.

Cruslock, E.M., Naylor, L.A., Foote, Y.L., and Swantesson, J.O.H., 2010, Geomorphic equifinality: A comparison between shore platforms in Hoga Kusten and Faro, Sweden and the Vale of Glamorgan, South Wales, UK: Geomorphology, v. 114, p. 78-88.

Duhnforth, M., Anderson, R.S., Ward, D. and Stock G.M., 2010, Bedrock fracture control of glacial erosion processes and rates: Geology, v. 38, p. 423-426.

Gabet, E., 2014, Late Cenozoic uplift of the Sierra Nevada, California? A critical analysis of the geomorphic evidence: American Journal of Science, v. 314, p. 1224-1257.

Gillespie, A.R. and Zehfuss, P.H., 2004, Glaciations of the Sierra Nevada, California, USA, *in* Ehlers, J. and Gibbard, P.L., eds., Quaternary Glaciations – Extent and Chronology, Part II: New York, Elsevier B.V., p. 51-62.

Goudie, A.S. 2006, The Schmidt hammer in geomorphological research. Progress in Physical Geography 30, 6. 703-713. DOI: 10.1177/3039133306071954.

Graf, W.L. 1970, The geomorphology of the glacial valley cross section: Arctic and Alpine Research, v. 2, p. 303-312.

Grater, R.K., 1947, A Geologic and Geographic Sketch of Zion National Park: Zion-Bryce Museum Bulletin No. 3 National Park Service, Zion Natural History Museum, 18 p.

Grezov, C. and Drazin, R., 1997, Equifinality: Functional Equivalence in Organizational Design: Academy of Management Review, v. 22, p. 403-428.

Gulick, V.C. and Baker, V.R. 1990, Origin and evolution of valleys on Martian volcanoes: Journal of Geophysical Research: Solid Earth (1978-2012) v. 95, p. 14325-14344.

Gumede, H. and Stacey, T.R. 2007, Measurement of typical joint characteristics in South African gold mines and the use of these characteristics in the prediction of rock falls: The Journal of The Southern African Institute of Mining and Metallurgy, v. 107, p. 335-344.

Hall, A.M., Mellnor, A, and Wilson, M.J., 1989, The clay mineralogy and age of deeply weathered rock in north-east Scotland: Zeitschrift fur Geomorphologie N.F. Supplemental Bulletin, v. 72, p. 97-108.

Harbor, J.M. 1995, Development of glacial-valley cross sections under conditions of spatially variable resistance to erosion: Geomorphology, v. 14, p. 99-107.

Harbor, J.M. 1992, Numerical modeling of the development of U-shaped valleys by glacial erosion: Geological Society Bulletin, v. 104, p. 1364-1375.

Hallet, B. 1995, Glacial quarrying: a simple theoretical model: Annals of Glaciology, v. 22, p. 1-8.

Hay, T. 1943, Notes on Glacial Erosion and Stone Stripes: The Geographical Journal, v.102, p.13-20.

Hirano, M. and Aniya, M., 1988, A rational explanation of cross-profile morphology for glacial valleys and of glacial valley development: Earth Surface and Processes, v. 13, p. 707-716.

Hooyer, T.S, Cohen, D. and Iverson, N.R, 2012, Control of glacial quarrying by bedrock joints: Geomorphology, v.153-154, p. 91-101.

Horton, R.E., 1945, Erosional development of streams and their drainage basins; hydrophysical approach to quantitative morphology: Geological society of America bulletin, v. 56, p. 275-370.

Huber, N.K. and Rinehart, C.D., 1965, Geologic map of the Devils Postpile quadrangle, Sierra Nevada, California: U.S. Geological Survey, Geologic Quadrangle Map GQ-437, scale 1:62,500, 1 sheet.

Iverson, N.R. 2012, A theory of glacial quarrying for landscape evolution models: Geology, v.40, p. 679-682.

Iverson, N.R. 1991, Potential effects of subglacial water pressure fluctuations on quarrying: Journal of Glaciology, v.36, p. 304-314.

James, L.A., 1996, Polynomial and Power Functions for Glacial Valley Cross-section Morphology: Earth Surface Processes and Landforms, v. 21, p. 413-432.

James, L.A. 2003b, Glacial erosion and geomorphology in the northwest Sierra Nevada, CA: Geomorphology, v.55, p. 283-303.

Krabbendam, M. and Glasser, N. 2011, Glacial erosion and bedrock properties in NW Scotland: Abrasion and quarrying, hardness and joint spacing: Geomorphology, v. 130, p. 374-383.

Kochel, R.C., and Piper, J.F. 1986, Morphology of large valleys on Hawaii: Evidence for groundwater sapping and comparisons with Martian valleys: Journal of Geophysical Research: Solid Earth (1978-2012), v. 91, p. E175-E192.

Kottek, M., Grieser, J., Beck, C., Rudolf, B., and Rubel, F., 2006. World Map of the Koppen-Geiger climate classification updated: Meteorologische Zeitschrift, v. 15, p. 259-263.

Leith, K., Moore, J., Amann, F., and Loew, S. 2011, Effect of glacial ice cover on fracturing in critically stressed bedrock: Geophysical Research Abstracts, EGU General Assembly, v. 13, EGU2011-12825-2.

Loso, M.G., Anderson, R.S., Anderson, S.P., and Reimer, P.J., 2006, A 1500-year record of temperature and glacial response inferred from varved Iceberg Lake, southcentral Alaska: Quaternary Research, v.66, p. 12-24.

Li, Y., Liu, G., and Cui, Z. 2001, Glacial valley cross-profile morphology, Tian Shan Mountains, China: Geomorphology, v.38, p. 153-166.

MacGregor, K.R., Anderson, R.S., Anderson, S.P., and Waddington, E.D. 2000, Numerical simulations of glacial-valley longitudinal profile evolution: Geology, v. 28, p. 1031-1034.

Martel, S.J. 2006, Effect of topographic curvature on near-surface stresses and application to sheeting joints: Geophysical Research Letters, v.33, p. 1-5.

Matlab 8.3, Natick, Massachusetts, The Mathworks Inc., 2012.

Matthes, F.E. 1965, Glacial Reconnaissance of Sequoia National Park California: U.S. Geologic Survey Professional Paper 504-A, 164 pp.

Matthes, F.E. 1960, Reconnaissance of the Geomorphology and Glacial Geology of the San Joaquin Basin, Sierra Nevada California: U.S. Geologic Survey Professional Paper 329, 62 pp.

Matthes, F.E. 1930, Geologic History of the Yosemite Valley: U.S. Geologic Survey Professional Paper 160, 131 pp.

Minnich, R.A. 2007, Climate, Paleoclimate and Paleovegetation *in* Barbour, M.G., Keeler-Wolf, T, and Schoenherr, A.S. eds., Terrestrial Vegetation of California: University of California Press, p. 43-70.

Moore, J. G., and Mack, G.S., 2008, Map Showing Limits of Tahoe Glaciation in Sequoia and Kings Canyon National Parks, California, scale 1:25,000, 1 sheet.

Moore, J.G., and Sisson, T.W., 1978, Geologic map of the Triple Divide Peak quadrangle, Tulare County, California: U.S. Geological Survey, Geologic Quadrangle Map GQ-1636, scale 1:62,500, 1 sheet.

Moore, J.R., Sanders, J.W., Dietrich, W.E., and Glasser, S.D., 2009, Influence of rock mass strength on the erosion rate of alpine cliffs: Earth Surface Processes and Landforms.

Morland, L.W., and Boulton, G.S. 1975, Stress in an elastic hump: the effects of glacier flow over elastic bedrock: Proceedings of the Royal Society of London Series A, v. 344, p.157-73.

Moscicki, J., Kotara, A., and Kedzia, S., 2006. Glacial erosion in the Abisko Mountains: Karevagge and Vassivagge, Northern Sweden: Geografiska Annaler, v. 88, p. 151-163.

Nicholas, A.P., and Quine, T.A., 2010, Quantitative assessment of landform equifinality and paleoenvironmental reconstruction using geomorphic models, Geomorphology, v. 121, p. 167-183.

Palmstrom, A. 2005, Measurements of and Correlations between Block Size and Rock Quality Designation (RQD): Tunnel and Underground Space Technology, v. 20, p. 362-377.

Palmstrom, A. 1995, RMi – a rock mass characterization system for rock engineering purposes, PhD thesis, Oslo University, Norway, 400p.

Phillips, J., 1997, Simplexity and the reinvention of equifinality: Geographical Analysis, v. 29, p. 1-15.

Potter, E.C. 1976, Pleistocene glaciation in Ethiopia: new evidence: Journal of Glaciology, v. 17, p. 148-150.

Rea, B.R. 1994, Joint Control in the Formation of Rock Steps in the Subglacial Environment, *in* Robinson, D.A. and Williams, R.G., eds., Rock Weathering and Landform Evolution: John Wiley & Sons Ltd., p. 473-486.

Schaffer, J. 1997, The Geomorphic Evolution of the Yosemite Valley and Sierra Nevada Landscapes: Solving the Riddles in the Rocks: Berkeley, California, Wilderness Press, 388 p.

Segall, P., 1984, Formation and growth of extensional fracture sets: Geological Society of America Bulletin, v. 95, p. 454-462.

Segall, P., McKee, H., Martel, S.J., and Turrin, B.D., 1990, Late Cretaceous age of fractures in the Sierra Nevada batholith, California: Geology, v. 18, p. 1248-1251.

Selby, M.J. 1980, A rock mass strength classification for geomorphic purposes: with tests from Antarctica and New Zealand: Zeitschrift Geomorphologie, v. 24, p. 31-51.

Smith D.G. and Fisher T.G. 1993, Glacial Lake Agassiz: The northwestern outlet and paleoflood: Geology, v. 21, p. 9-12.

Sklar, L.S. and Dietrich, W.E. 2001, Sediment and rock strength controls on river incision into bedrock; Geology, v. 29, p. 1087-1090.

Stock, GM., Martel, S.J., Collins, B.D., and Harp E.L., 2011, Progressive failure of sheeted rock slopes: the 2009-2010 Rhombus Wall rock falls in Yosemite Valley, California, USA: Earth Surface Processes and Landforms, v. 37, p. 546-561.

Yingkui, L., Gengnian L., and Zhijiu, C. 2001, Longitudinal variations in cross-section morphology along a glacier valley: a case-study from the Tien Shan, China: Journal of Glaciology, v. 47, p. 243-250.

White, W.A., 1945, Origin of Granite Domes in the Southeastern Piedmont: The Journal of Geology, v. 53, p. 276-282.

Ziegler, M., Loew, S., and Moore, J.R., 2013, Distribution and inferred ago of exfoliation joints in the Aar Granite of the central Swiss Alps and relationship to Quaternary landscape evolution: Geomorphology, v. 201, p. 344-362.

APPENDIX A

Tuolumne	River	valler						
Waypoint	MAGI	v aneg	, 	1				1
92 (T7)				Joint	Joint	Joint		
	Elev.			spacing	length	width	Joint strike	
Lat/Long	(m)	SH	Alpha		(m)	(mm)	and dip	Continuity
37.93520	(111)	511	rupiia	(111)	(111)	(11111)	and dip	Continuity
119.4889	1758	60	-45	r=28	3.5 (1)	na	15	r=6
117.1007	1750	64	15	7-20	5 (2)	na	15	7-0
		48			1.5 (3)	na	125,88	
		68			1 (4)	0.5	90,90	
		60			5 (5)	0.5	90,45	
		60			3 (3)	r=7	r=18	
		48				7 - 7	7-10	
		68						
		64						
		63						
		65						
		55						
		63						
		63						
		63						
		55						
		63						
		61						
		1						
Waypoint 93								
27 02506								
37.93506 119.48881	1777	70.7	15	0.8	2.5 (1)	0.5	6	
119.40001	1///	70 (65	r-45	0.8		0.5	6	r=5
		66		0.3	3 (2) > 5 (3)	1	125,89 10	
		69		3	> 5 (3)	na	68	
		73		2	2 (5)	na 2.5	75,60 (flake	<u> </u>
		68		0.6	2 (3)	r=4	r=9	<i>)</i>
		64		0.0		<i>i –4</i>	1-3	
		71		r=21				
		/ I		1-41				

, DUILLE								
Waypoint						1		
		71						
	-	70				-		
		73						
		68						
	<u> </u>	74						
		64						
	<u> </u>	74						
		72						
		70						
		74				r=4	r=18	r=6
		71		r=28	6 (8)	3.5	263,7(?)	
		73		2	>5 (7)	4	247,55	
		70		3	3 (6)	2	240,60	
		73		2		2-Jan	260,60	
		70		1.5	2 (4)	3	68	
		72		2.5		face	65	
		72		2	3 (2)	na	4	
37.93491 119.48875	1781	72(P	-45	1	1.5 (1)		357,68	
94	-						1	
Waypoint								
		68						
		72						
		71						
		68		1		<u> </u>		
		66						+
	-	64						
		64						
		69						
		69 70						

		40		0.9	1.5 (3)	face	15,73	
		60		1	>5 (4)	60	140,10	
		58		0.3	3 (5)	20	107,90	
		64		0.6	2 (6)	60	170	
		58		2		r=2	r=9	
		59		0.9				
		59		r=21				
		37						
		50						
		47						
		58						
		54						
		59						
		54						
		52						
		54						
Waypoint 96								
37.93616								
119.48857	1798	50	-90	0.3			90,90	r=5
		58		0.3	0.5 (2)	face	60,90	
		54		0.6	2 (3)	face	80,90	
		54		0.5	0.5 (4)	4	57	
		52		0.4		r=7	r=14	
		56		r=21				
		54						
		54						
		56						
		58						
		56						
		51						
		50						
		60						
		58						
		58						
		61						
		61 54 55						

Waypoint 97 (T6)							
25 02005							
37.93097				> 5m			
119.51716	1684	56 -90	r=28	(1)	na	32	r=7
		58		1 (2)	na	40	
		56		5 (3)	na	27	
		52		2.5 (4)	na	135	
		64		2 (5)	na	135	
				> 5m			
		64		(6)	na	27	
		66			r=7	r=20	
		50					
		61					
		66					
		63					
		63					
		65					
		61					
		66					
		68					
		72					
		62					
Waypoint							
98							
37.93122							
119.51714	1695	72 (P-90	r=28	2.5 (1)	na	60	r=7
		72		2(2)	na	60	
		70		4 (3)	na	10	
		75		>4 (4)	na	10	
		72			r=7	r=20	
		71					
		76					
		68					
		72					
		72					
		73					
		70					

	1	70	I	I				
		70		1				
		75						
		72						
		72						
		68						
		72						
Waypoint 99								
37.93180								
119.51706	1720	52	-90		2(1)	30	55	r=5
		64			0.5 (2)	5	50	
		66			0.5 (3)	5	130	
		65			>4 (4)	10	110	
		55			3-4 (5)	15	169	
		58			3 (6)	20	5	
		66			2 (7)	30	55	
		62			3.5 (8)	60	115	
		58					r=14	
		58		r=21		r=2		
		63						
		63						
		65						
		64						
		52						
		64						
		58						
		61						
Waypoint 100								
37.931217								
	1766	68(P	-90		5.5 (1)	3mm	347	r=6
		66			2 (2)	face	350,85	
		70			>5 (3)	1mm	76	
		64			>4 (4)	na	62	

		68			3 (5)	na	145	
		62		r=21		r=5	r=18	
		66						
		70						
		62						
		66						
		64						
		64						
		67						
		68						
		63						
		60						
		62						
		65						
Waypoint 101 (T5)								
37.93867								
119.53250	1619	55	-90		>5 (1)	4mm	135,90	1
		55			0.5 (2)	1mm	40,34	1
		66			0.5 (3)	na	78,42	
		62			1 (4)	1mm	48,40	
		58			0.5 (5)	na	85,30	
					>10 (6)			
					& 5			
		60			(10)	5mm	63,90	
		66			1 (7)	1mm	27,45	
		68			>6 (8)	na	343,86	
		59		r=28		r=6	r=14	r=6
		61						
		64						
		58						
		65						
		64						
		61						
		65						
		63						
		62						

Waypoint 102								
102								
37.93851					0.6 (set			
119.53333	1583	56	0	0.2	1)	na	130,90	
117.55555	1303	30	O	0.2	7 (vein	iiu	130,70	
		58		2	1)	2	90	
					0.5 (set		70	
		49		0.6	2)	1.5	70,57	
					3			
					(veins			
		58		1	2)	2mm	65	
		56		2	>3 (3)	3.5mm	140	
		58		1	>3 (4)	9mm	15	
					1.6			
					(vein			
		58		r=28	3)	1	72	
					>3.5			
		59			(5)	na	80,90	
					1.8 (6)			
					Flake(?			
		65)	1mm	130,86	
					>4			
		66			(vein4)	3	130(?),34	
		60				r=6	r=9	r=5
		50						
		52						
		56						
		56						
		62						
		64						
		58						
Waypoint								
103 (T4)								
37.93404								
119.55695	1489	54	-90	0.4	0.5 (1)	3mm	134,80	r=5
117.33093	1407	52	-30	0.4	1.5 (2)	na	55	1-3
		46		0.6	0.5 (3)	na	137,80	
	<u> </u>	40		0.0	0.5 (3)	1114	137,00	<u> </u>

		1		_		T		
					1.5 (4)			
					2nd //			
					joint			
		46		0.9	1m.	2	220,85	
					>2 (5)			
					Four //			
					joints ~			
		54			1m	1	134	
		55			1 (6)	2	5,87	
					2 (7)			
					2nd //			
					joint			
		54			10cm.	4	235	
		51		0.6		r=4		
		46		r=21			r=9	
		51						
		50						
		46						
		44						
		48						
		50						
		48						
		50						
Waypoint								
104								
37.93425					3 (Set			
	1507	60	-90	0.3	1)	127	84,52	r=5
			7.0		1 (Set		1,0 =	
		54		0.3	2)	150	342,67	
		†		1	>3.5	123	2.2,07	
		53		0.6	(Set3)	55	85,65	
		46		0.9	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	r=2	r=14	
		48		0.45			, , ,	
		63		r=21				
		65		†				
		54						
		50		1	+			
		48		+				
		TO						

		-	Ī	I				
		56						
		58						
		58						
		66						
		62						
		60						
		54						
		56						
XX7								
Waypoint 105								
37.93434								
119.55788	1509	69	-90		>4 (1)	na	17,78	r=5
		72			>3 (2)	na	60	
		70			0.5 (3)	na	320	
		66			0.5 (4)	na	305	
		68			1.5 (5)	20	290	
		68			2 (6)	50	330,90	
		68			2.5 (7)	20	50	
		71			>2 (8)	30	320	
		68			1 (9)	25	30,40	
		70				r=2	r=14	
		70		r=28				
		70						
		68						
		68						
		70						
		68						
		67						
		69						
Waypoint 106 (T3)								
37.92962								
119.56202	1459	58	-90		2(1)	1mm	40,90	r=5
		61			2.5 (2)	1.5mm	41,90	
		62			2.5 (3)	1mm	40,90	
		62			3 (4)	1.5mm	40,86	

		63			1.5 (5)	na	280	
		62			>3 (6)	1mm	40,90	
		53		r=28	>3 (7)	na	357,72	
		66			2 (8)	na	355,70	
		61			3 (9)	na	281	
					0.5			
		54			(10)	na	350	
		60			1 (11)	2mm	75,77	
					1.5			
		58			(12)	2mm	75,80	
					0.5			
		64			(13)	1mm	60,90	
					1.8			
		58			(14)	1mm	60,90	
					0.5			
		64			(15)	1mm	95,67	
					0.5			
		65			(16)	1mm	95,68	
					0.8			
		52			(17)	2mm	40	
					0.8			
		60			(18)	2mm	40	
					1 (19)	na	90,80	
					1 (20)	na	70,80	
					0.8			
					(21)	na	60,80	
					>3 (22)	6mm	355,85	
					4 (23)	na	352	
					>4 (24)	face	30,73	
						r=5	r=14	
Waypoint								
107								
37.92984								
119.56216	1477	54(P	-90	r=28	>4 (1)	na	45,50	r=7
		66			>2 (2)	na	46,55	
		65			>3 (3)	na	43,50	

		66			0.3 (4)	na	320	
		00			2 (vein	114	320	
		69			5)	2	355	
		07			>2 (2	333	
		68			vein 6)	4mm	290	
		66			1 (7)	1	170	
		65			1 (/)	r=7	r=20	
		66				7 – 7	1-20	
		68						
		70						
		72						
		74						
		73						
		75						
		75		1				
		70						
		69						
Waypoint								
108								
37.93003								
119.56244	1488	40	0	r=28	>7 (1)	face	48,90	r=6
		50			1 (2)	2mm	130,78	
		64			? (3)	Look at p		
		63				r=5	r=18	
		58						
		56						
		54						
		54						
		60						
		59						
		61						
		50						
		_	1					
		51						
		51 64						
		_						
		64						
		64 64						

1333	56	-45		3 (1)	face	190,83	r=6
	68			1.5 (2)	vein	68	
	52			2 (3)	vein	24	
	58			3 (4)	na	330,78	
	59			3 (5)	na	247,73	
	64		r=21	2 (6)	na	238,77	
	60			>3 (7)	1mm	307	
	54			1.5 (8)	na	240,75	
	64			2.5 (9)	face	324,75	
	62			2 (10)	na	260,20	
	50				r=6	r=18	
	60						
	56						
	60						
	53						
	61						
	62						
	59						
1373	51	0	r=28	>4 (1)	face	97,62	r=6
	56			1.5 (2)	15		
	66				2		
	60						
					1		
	62						
			1			_	
			1				
				(-)			
	_			1			1
				1			1
	58		1	1			
	1373	68 52 58 59 64 60 54 60 60 56 60 56 60 56 60 56 60 56 60 56 60 56 60 59 60 60 59 60 60 60 60 60 60 60 6	68 52 58 59 64 60 56 60 56 60 56 60 56 60 56 60 56 60 56 60 56 60 56 60 56 60 56 60 55 60 60	68 52 58 59 64 60 54 64 62 50 60 53 61 62 59 1373 51 0 r=28 56 60 56 60 60 60 60 60 60 60 60 60 60 60 60 60	68 1.5 (2) 52 2 (3) 58 3 (4) 59 3 (5) 64 r=21 2 (6) 60 >3 (7) 54 1.5 (8) 64 2.5 (9) 62 2 (10) 50 60 56 60 53 61 62 59 56 1.5 (2) 66 1.5 (3) 60 >4 (4) 56 55 (5) 62 0.5 (6) 60 1.5 (7) 63 0.5 (8) 52 0.1 (9) 60 0.1 (9)	68 1.5 (2) vein 52 2 (3) vein 58 3 (4) na 59 3 (5) na 64 r=21 2 (6) na 60 >3 (7) Imm 54 1.5 (8) na 64 2.5 (9) face 62 2 (10) na 50 r=6 60 r=6 60 r=6 60 r=6 53 r=6 61 r=6 59 r=28 54 1,5 (2) 55 1,5 (2) 15 15 66 1,5 (2) 15 15 66 1,5 (2) 15 3 60 >4 (4) 1mm 56 55 3mm 62 0.5 (6) 3mm 60 1,5 (7) 10 63 0.1 (9) 60 r=4 59 0	68 1.5 (2) vein 68 52 2 (3) vein 24 58 3 (4) na 330,78 59 3 (5) na 247,73 64 r=21 2 (6) na 238,77 60 >3 (7) 1mm 307 54 1.5 (8) na 240,75 64 2.5 (9) face 324,75 62 2 (10) na 260,20 50 r=6 r=18 60 r=6 r=18 60 r=6 r=18 61 r=6 r=18 62 r=7,62 r=18 61 r=7,62 r=18 62 r=1,5 (2) r=15 r=24,87 66 r=1,5 (2) r=15 r=18 66 r=1,5 (2) r=15 r=18 66 r=1,5 (3) r=135,62 r=16 60 r=1,5 (3) r=135,62 r=16 61 r=1,5 (3) r=135,62 r=16 62 r=

		63						
		50		1				
		57						
		58						
		58						
Waypoint 111 (T1)								
37.93018								
119.60405	1371	54	-90		0.5 (1)	3	355,47	r=6
		48			2(2)	na	15	
		56			>4 (3)	na	35	
		54			1.5 (4)	25	12,62	
					>3.5			
		61		r=15	(5)	25	10,60	
		60			0.5 (6)	1	14	
		62			3 (7)	1.5	350	
		64			3.5 (8)	20	9,75	
		64			1.5 (9)	15	95	
		63			4 (10)	face	223,60	
		63			2 (11)	na	235	
		59			>2 (12)	20	107,75	
		64				r=2	r=18	
		60						
		57						
		66						
		64						
		60						

Waypoint 112								
37.93072					1 (Set			
119.60443	1376	64	-90	r=15	1)	2	147,86	r=5
		62			2 (Set 2)	1	57,90	
				1	1.5		ĺ	1
		66			(Set 3)	1	15,74	

	T		ı	I	1	1 -	1	
		70				r=2	r=14	
		68						
		44						
		64						
		66						
		70						
		68						
		66						
		66						
		60						
		74						
		64						
		70						
		71						
		65						
Waypoint								
113								
37.93131								
119.60491	1377	64	0	r=21	2(1)	40	340,70	r=5
117,00 171	1377	66	Ü		0.5 (2)	face	260,77	1-0
		66			0.6 (3)	50	345,70	
		64			2 (4)	30	335,80	
		68			3 (5)	120	250,60	
		68			2.5 (6)	150	240,30	
		00			>3.5	130	240,30	
		67			(7)	60	265,70	
		in /			1 > /1 (X)	IUII		
Ī		62 68			>4 (8)	90 r-2	260,65 r-14	
		68			>4 (8)	r=2	r=14	
		68 66			>4 (8)			
		68 66 62			>4 (8)			
		68 66 62 63			>4 (8)			
		68 66 62 63 68			>4 (8)			
		68 66 62 63 68 61			>4 (8)			
		68 66 62 63 68 61 66			>4 (8)			
		68 66 62 63 68 61 66 67			>4 (8)			
		68 66 62 63 68 61 66			>4 (8)			

Tenaya Ca	nyon							
Waypoint ? (TN8)								
	Elev.	CIT		Joint length	Joint width	Joint strike and		
Lat/Long	(m)	SH	Alpha	(m)	(mm)	dip	(m)	Continuity
37.80755								
119.47040		60	-90	>10	100	185,65	3.5	r=6
		52		3.5	10	105,82	0.75	
		58			40	r=9	1.25	
		48			50		1	
		50			15		0.4	
		40			40		0.3	
		54			100		0.4	
		50			40		2	
		56			r=2		0.875	
		54					r=21	
		52						
		50						
		55						
		40						
		52						
		43						
		54						
		51						
Waypoint 204		63						
37.80739								
119.47012		60	-90		10	210,25	1.4	r=6
		58			5	150,20	0.9	
		58			10	r=9	5	
		64			r=4		4.5	
		64					2.95	
		58					r=28	
		58			1			
		58			1			
		59			1			
		60			+			

		E 1						
		54		<u> </u>				
		58		 			1	
		57						
		62						
		58						
		55						
		59						
Waypoint 205								
37.80740								
119.46991	2348	49	-90		20	245,80	1	r=6
		50			35	325,65	1.7	
		52			30	220,15	0.5	
		53		<u> </u>	50	325,60	0.45	
		50			r=2	230,20	2.1	
		50				105,75	1.2	
		55				320	1.1	
		50				185	r=28	
		50				r=9		
		50						
		51						
		50						
		48						
		56						
		40						
		52						
		50						
Waypoint 206								
37.80723				1				
119.46945	2422	52	-90		50	285	1.5	r=6
117.40743	<i>L</i> 4 <i>LL</i>	50	-90	+	10	200,10	1.3	1-0
		52		 	5	290		
		52 47		 	40	190,10	0.3	
		_						
		50		1	25	290,90	0.9	
		45		1	r=2	295,90	1.2	
		51		1		330	2	
		46				335	1.2	

		52			r=9	r=28	
	†	44					
	†	48					
		49					
		47					
		48					
		51					
		51					
		45					
		49					
Waypoint							
207							
37.80704							
119.46905	2410	58	-90	25	200,7	11	r=6
		60		152	20,15	0.3	
		58		30	305,85	0.1	
		45		10	210,90	6	
		61		27.5	295	0.2	
		50		r=2	210,90	0.3	
		58			290	0.6	
		53			r=14	0.3	
		52				r=15	
		55					
		62					
		59					
		60					
		56					
		58					
		49					
		54					
		56					
Waypoint 208							
37.80695							
119.46856	2407	74	-90	10	290,85	0.3	r=6
		67		30	10,90	0.2	
		68		35	0,20 (F)	0.3	
		69		20	285,84	0.8	

	1				1.0	202 =0	0.0	
		66			10	292,79	0.3	
		64			32	288,86	0.5	
		68			25	285,90	0.25	
		70			r=2	10,88	1	
		68				15,86	3	
		70				12,90	2	
		68				290,88	1	
		70				289,86	1.5	
		70					0.65	
		70					r=15	
		74						
		74						
		70						
		72						
		72						
		70						
Waypoint 209								
37.80706								
119.46826	2420	48	-45		10	105,90	0.8	r=6
		67			8	345	3.6	
		53			40	125	1.8	
		66			30	110,80	2.4	
		65			15	10,82	2.1	
		58			20	0,90	0.9	
		64			25	0,10 (F)	0.9	
		53			20	145,85	1.8	
		63			r=2	280,83	r=28	
		52				,		
		54						
		56						
		60						
		63						
		64			<u> </u>			
		53						
		59			<u> </u>			
					†			
Waypoint								
210								
				_1	1		_1	

37.80716							
119.46779	2432	70	-90	38	75,80	r=28	r=7
		65		5	285,87		
		58		5	r=14		
		70		10			
		69		7.5			
		70		r=4			
		70					
		68					
		74					
		66					
		72					
		67					
		70					
		70					
		66					
		70					
		75					
		69					
Waypoint 211							
37.80735							
119.46729	2454	68	-90	100	5,75	0.6	r=5
		58		20	265,70	0.3	
		68		10		0.3	
		66		25	8,70	0.5	
		62		10	5,85	0.7	
		60		8	270,80	0.9	
		54		115	265,73	1.2	
		66		150	r=14	0.3	
		52		200		0.15	
		52		25		0.2	
		63		 30		0.2	
		58		 25		0.9	
		66		r=2		1.2	
		54				0.5	
		64				r=15	
		58					

		54					
		60	1				
		1					
Waypoint			1				
212 (TN5)							
37.80617							
119.47073	2431	68	-90	203	355,88	0.3	7
		64		10	250	0.6	
		55		30	275	0.15	
		67		20	280	0.6	
		67		15	260	0.5	
		68		10	100,82	0.9	
		68		12	325,80	0.9	
		65		20	335	0.4	
		68		30	320	0.2	
		69		15	320,70	0.3	
		58		25	·	0.3	
		59		30		1.2	
		57		150		0.45	
		70		120			
		60		30			
		70		40			
		58		100			
		64		30			
Waypoint 213							
No lat and							
long data.							
Next point							
up.	2419	65	-90	50	325,65	1.8	5
		56		30	325	4	
		64		10	15	0.2	
					230,15		
		56		20	(F)	2.1	
		60		25		1.2	
		58				1.8	
		54					
		57					
		60					

		_					
		57					
		64					
		57					
		54					
		57					
		55					
		64					
		62					
		59					
Waypoint 214							
37.80592				1			
119.46994	2403	65	-90	10	310,90	0.6	6
115(1055)	2.02	60	70	40	308,84	0.3	
		64		30	310,75	0.25	
		52		8	05,86	0.9	
		56		5	310 (V)	0.2	
		57		10	10 (V)	0.3	
		61			320,88	1.2	
		60			220,00	0.9	
		65				0.2	
		64				1.2	
		58				0.15	
		66				0.3	
		60					
		55					
		55		1			
		64					
		60		1			
		60					
Waypoint							
215							
37.80576							
119.46944	2386	62	-45	0	195	>3	R=7
		58		R=7	191	R=30	
		48			196		
		56			195		

					195,20		
		54			(F,3)		
		44			R=20		
		54					
		57					
		56					
		51					
		55					
		46					
		55					
		62					
		59					
		49					
		56					
		54					
Waypoint							
216 (TN7)							
37.80552							
119.46883	2371	58	-90	0	N/A	>3	R=7
				t			
		55		R=7	r=20	r=30	
		59		R=7			
		59 61		R=7			
		59 61 57		R=7			
		59 61 57 55		R=7			
		59 61 57 55 51		R=7			
		59 61 57 55 51 64		R=7			
		59 61 57 55 51 64 61		R=7			
		59 61 57 55 51 64 61 58		R=7			
		59 61 57 55 51 64 61 58 60		R=7			
		59 61 57 55 51 64 61 58 60		R=7			
		59 61 57 55 51 64 61 58 60 56		R=7			
		59 61 57 55 51 64 61 58 60 56 50 63		R=7			
		59 61 57 55 51 64 61 58 60 56 50 63 58		R=7			
		59 61 57 55 51 64 61 58 60 56 50 63 58		R=7			
		59 61 57 55 51 64 61 58 60 56 50 63 58 59 61		R=7			
		59 61 57 55 51 64 61 58 60 56 50 63 58		R=7			
Waynaint		59 61 57 55 51 64 61 58 60 56 50 63 58 59 61		R=7			
Waypoint 217		59 61 57 55 51 64 61 58 60 56 50 63 58 59 61		R=7			

37.80544					340,18		
119.46828	2384	64	-90	5	(F,2)		R=7
		66		r=5	100 (V)	r=28	
		65			160 (V)		
		56			r=18		
		58					
		57					
		59					
		56					
		58					
		57					
		65					
		62					
		63					
		58					
		58					
		58					
		59					
		60					
Waypoint 218							
37.80536							
119.46762	2399	54	-90	20	115	0.6	r=6
		60		100	225	1.8	
		61		10	103	0.25	
		47		30	r=14	0.3	
		58		5		1.4	
		54		10		5.3	
		57		15		1	
		54		r=4			
		55					
		58					
		49					
		65					
		53					
		60					
		58					
		62					
		57					

		1					
Waypoint 219							
37.80547							
119.46684	2439	54	-90	30	285,73	0.45	r=7
		60		40	05,80	0.25	
		44		0.5	25	0.3	
		58		1	285,68	0.4	
		58		0.3	130,90	0.15	
		60		20	100	0.9	
		54		2	r=9	0.35	
		63		2		r=15	
		61		r=5			
		50					
		61					
		57					
		48					
		60					
		63					
		61					
		60					
		57					
Waypoint							
220 (TN2)							
37.78882							
119.48655	2342	59	-90	10	340,80	1.5	r=5
		61		15	10,30 (F)	0.9	
		58		5	8	1	
		50		2	335	0.45	
		53		10	10,68	1.2	
		52		1	5	0.45	
		55		 20	90	0.76	
		42		 1	350	1	
		53		 30	335	0.3	
		48		 1	350	0.1	
		51		 2	355	0.2	
		54		1.5	185,50	0.1	
		48		15	185,35	0.61	

		47		5	185	r=21	
		48		r=4	r=9		
		54					
		51					
		52					
		1					
Waypoint							
221							
37.78848		1					
	2347	64	-90	30	355	0.3	r=6
		61		15	255	1	
		53		10	180,68	0.2	
		1			280,15		
		52		10	(F,4)	0.6	
		61		35	270,75	0.3	
		51		5	r=9	0.9	
		59		15		1.2	
		61		25		0.6	
		60		20		r=21	
		63		15			
		54		r=4			
		60					
		51					
		59					
		55					
		65					
		63					
		58					
Waypoint		1	 				
222							
37.78806		1	1 1				
119.48665	2333	60	-90	0	N/A	>3	7
		60	† †	r=7	r=20	r=30	
		60	† †				
		56	† †				
		53	† †				
		64					
		60	1 1				
		55	† †				

	1	T_ :	T	1	1			
		54						
		57						
		61						
		58						
		60						
		67						
		64						
		63						
		60						
		60						
Waypoint	+							
223								
37.78775						115,35		
119.48654	2314	63	-90		15	(F)	0.3	R=6
		61			10	265,45	0.1	
		63			5	330	0.8	
		61			20	165,90	0.05	
		59			30	330,85	0.1	
		57			40	170-190, 20-30 (F, 10)	0.05	
		61			5	R=9	0.05	
		51				N=9		
					10		0.1	
		56			15		0.4	
		61			10		0.2	
		55	1		100		0.15	
		56	1		30		0.3	
		60	1		10		0.2	
		57			15		0.1	
		54			20		0.15	
		56			5		0.2	
		55			65		0.1	
		58			5		0.1	
	1	<u> </u>			8		0.2	
					45		0.25	
		1			200		0.3	
		<u> </u>			35		0.1	
	<u> </u>		<u> </u>		30		1.5	

				15		0.15	
				R=4		R=15	
Waypoint							
225	1						
37.78715	2201		0.0	0	DT / A	2	
119.48634	2291	57	-90	0	N/A	>3	
	1	51		r=7	r=20	r=30	r=7
		53					
	ļ	50					
		54					
		59					
		55					
		54					
		57					
		55					
		58					
		52					
		56					
		60					
		53					
		48					
		55					
		55					
	1						
Waypoint 226 (TN3)							
37.78688					95,20 (F,		
119.48624	2302	65	-90	3	12)	0.9	r=4
		58		5	0,10 (F)	1.8	
		61		10	235,80	1.4	
		64		8	120	0.3	
		57		15	55	0.25	
	1	65		10	r=9	0.5	
		64		20		0.3	
		56		5		0.1	
		66		20		0.4	
		58		2		r=21	
		65		1			
	+	57		15			
		51		1.5			

		60	1 1	120			
		60		30			
		60		60			
		60		10			
		62		r=4			
		63					
		61					
Waypoint							
227							
37.78662					75,40		
119.48627	2314	60	-45	20	(F,8)	1	r=5
		48		15	225,80	0.6	
		60		10	185,90	0.4	
		52		30	250,86	0.2	
		58		10	95,20	0.3	
		58		35	160	0.25	
		52		15	265,15	0.6	
		60		10	r=9	0.1	
		54		5		0.9	
		55		15		0.05	
		60		r=4		0.35	
		58				r=21	
		55				7 21	
		55					
	1	61					
		59					
		61					
		57					
		31					
Waypoint							
228							
37.78614	2246	60		15	175 00	0.2	
119.48608	2346	68	-90	15	175,80	0.3	r=6
		65	1	5	120,84	1.2	
		66	 	20	165,90	0.45	
		59		15	45	0.2	
		63		10	115	0.1	
		66		20	135,40	0.2	
		64		5	315,55	0.35	
		64		20	345,5	0.5	

					1	To =	0.15	
		65			15	95	0.15	
		64			120	285	0.1	
		67			40	325,80	0.2	
		64			30	320,20	0.1	
		65			17.5	290	0.9	
		64			r=4	115,8 (F)	0.6	
		63				120,86	0.15	
						Flakes		
						striking		
						roughly		
		67				east/NE	0.5	
		68				r=9	1	
		65					0.2	
							0.15	
							0.6	
							0.25	
							r=15	
Waypoint 229								
37.78581								
119.48599	2364	65	-90		130	270,60	0.6	r=6
		67			140	175,86	1.2	
		68			30	315,80	1.2	
		70			20	350	0.6	
		66			110	280	0.9	
		55			10	180,75	1.5	
		58			25	r=14	0.2	
		60			40		1.4	
		69			35		1.05	
		66			r=2		r=28	
		58						
		65						
		67						
		58						
		68						
		57						
		68						
		64						
	<u> </u>	•		<u> </u>	I		1	

			\Box		T		
Waypoint 230 (TN1)							
37.78648							
119.48923	2266	64	-45	60	280,76	1	r=6
		65		15	195,5	0.6	
		65		30	265	1.2	
		61	1 1	80	260,75	0.6	
		69		20	r=9	1.5	
		71	1 1	75		0.5	
		66		25		0.8	
		58		10		r=21	
		65		27.5			
		57	† †	r=2			
		67					
		69					
		66					
		65					
		56					
		69					
		67					
		65					
Waypoint							
231							
37.78637							
119.48890	2281	60	-90	10	270,84	0.6	r=7
		60		15	105	0.3	
		48		5	115,70	0.6	
		57		6	95	1	
		50		5	70,80	0.9	
			1 1		160,10		
		54		2	(F)	0.4	
		53		20	15,25 (F)	0.9	
		54	† †	1	20,76	0.6	
		53	† †	3	275,68	r=21	
		50	† †	5	r=18		
		56	† †	r=4			
		64	† †				
		64					

		60			T		
			1				
		58	1	 			
		55	<u> </u>				
		64					
	ļ	62					
		56					
	ļ						
Waypoint							
232							
37.78619							
119.48843	2303	59	-90	1	125,20	2.4	<i>r=7</i>
		62		25	115	0.9	
		54		30	120,81	1.4	
		56		5	110,86	0.3	
		61		2	95,90	0.4	
					280,30		
		56		3	(F)	1.8	
		52		10	r=14	1.15	
		58		30		r=28	
		61		7.5			
		61		r=4			
		62					
		59					
		53					
		60					
		52					
		52					
		62					
		58	1				
	1		1				
Waypoint			1				
233 (TN6)							
37.80428							
119.46809	2363	63	-90	2	260,90	1.2	r=7
		52		5	r=14	r=21	
		63		3.5			
		65		r=5			
		53					
		58					
		57					

		55					
		56	+	1			
		58	1				
		60	1	+			
		55	1				
		54	1				
	1	60	+				
		60					
			1				
		56	<u> </u>				
		58	1				
		58					+
Waypoint				1			
234							
37.80416							
119.46764	2380	60	-90	40	Set 290	0.3	r=7
		54		200	285,10	0.6	
		58		100	r=9	0.8	
		57		75		0.2	
		54	†	10		1.2	
		57	†	304		0.5	
		47		87.5		0.2	
		48		r=2		0.5	
		48		 		r=21	
		58				7 21	
		48					
		57					
		56	 				
		50	 				
		58	 				
		48	 				
		54					
W							
Waypoint 235							
37.80393							
119.46699	2412	64	-45	1	355, 80	>3	r=7
		63		r=7	r=14	r=30	
		54					
		64					

		65					
		62					
		63					
		51					
		64					
		60					
		58					
		54					
		57					
		58					
		62					
		57					
		52					
		59					
Waypoint 236							
37.80368			1		+		
	2440	66	-90	1	5,83	0.9	r=6
117110022	2	62	70	2	360, 80	1.8	. •
		-		<i>_</i>	355,10	1.0	
		58		2	(F)	2.74	
		65		1	30	0.3	
	1	66	1	5	45	1	
	1	56	1	4	265,85	0.3	
	1	66	1	10	270	1.2	
		62		6	r=9	1	
		62	1	12		r=21	
		64	<u> </u>	10			
	1	60	†	40			
	1	58	†	5			
	1	57	†	r=5			
		66	1				
		66	1				
		60	1				
	1	56	†				
	1	62			1		
		t					
	1	1	†				

2359	60	-90		0	150	>3	<i>r</i> =7
	58			r=7	r=20	r=30	
	58						
	64						
	60						
	64						
	60						
	57						
	61						
	50						
	48						
	52						
	60						
	60						
	55						
	58						
	58						
	58						
2355	60	-90		r=7	r=20	r=30	r=7
1							
ī		!	}	+	+	1	1
	60						
	60 57						
	2359	58 58 64 60 64 60 57 61 50 48 52 60 60 55 58 58 58 58 58 58 58 59 62 54 54	58 58 64 60 64 60 57 61 50 48 52 60 60 55 58 58 58 58 58 58 50 54 60 60 60 60 59 62 58 61 54	58 58 64 60 64 60 57 61 50 48 52 60 60 60 55 58 58 58 58 58 54 60 60 60 60 60 60 65 59 62 58 61 54 61 54 61 54 61	58 r=7 58 r=7 64 60 64 60 57 61 50 48 52 60 60 60 55 58 58 58 58 7 54 7 60 60 60 60 60 60 60 60 60 60 65 59 62 58 61 54	58 r=7 r=20 58 r=7 r=20 64 r=7 r=20 60 r=7 r=20 61 r=7 r=20 60 r=7 r=20 58 r=7 r=20 54 r=7 r=20 54 r=7 r=20 55 r=7 r=20 54 r=7 r=20 55 r=7 r=7 r=20 7 r=2	58 r=7 r=20 r=30 58 r=7 r=20 r=30 64 r=6 r=7 r=20 r=30 60 r=7 r=7 r=7 r=30 50 r=7 r=20 r=30 2355 r=7 r=20 r=30 2355 r=7 r=20 r=30 54 r=7 r=20 r=30 60 r=7 r=30 r=30 7 r=7 r=20 r=30 8 r=7 r=30 r=30 9 r=7 r=20 r=30 9 r=7 r=20 r=30 9

		64			T		
		60					
		59					
		39					
Waypoint?							
Not marked							
in GPS	?	58	-90	15	350 (5)	r=21	r=5
		60		1	190 (2)		
		51		501	r=14		
		59		25			
		48		10			
		51		5			
		52		10			
		52		203			
		56		45			
		55		150			
		54		10			
		60		503			
		50		20			
		60		130			
		58		40			
		54		25			
		62		r=2			
		55					
Waypoint 239							
37.80506							
119.47041	2371	61	-90	30	280	0.6	r=5
		58		1	350	0.9	
		58		50	300	1.2	
		50		15	360	0.3	
		60		20	355	0.4	
		52		15	100	0.6	
		56		40	190,60	0.5	
		56		45	85	0.6	
		60		25	185	0.3	
		60		20	190	1.6	

		1	1	1	1	T	П	
		60			35	95	1	
		50			30	70	0.4	
		61			60	175,90	0.5	
		54			50	r=9	0.4	
		54			10		0.3	
		61			2		0.2	
		60			27.5		0.5	
		57			r=2		r=21	
Waypoint 240								
37.80532								
	2390	64	-90		40	290	1.5	r=6
		63			20	265 (F)	1	
		63			15	r=14	2.7	
		64			20		0.2	
		68			r=4		0.3	
		66					1	
		67					r=28	
		66						
		68						
		63						
		68						
		65						
		67						
		70	1					
		69	1					
		68						+
		66	+					
		66						
								_
Waypoint		†	†					
241 (TN4)								
37.80061		1	+					
119.47329	2341	55	-90		r=7	r=20	r=30	r=7
117.11347	2371	54	70		- /	1-20	1-30	<u> </u>
		56	+					
		66						
		57						
		56						-
		50						

	1	1	1	1	1	1	1	
		59						
		66						
		66						
		56						
		63						
		66						
		63						
		65						
		56						
		58						
		58						
		60						
Waypoint								
242								
37.80074								
119.47375	2352	57	-90		5	120,8	0.23	r=6
		48			8	115,10	0.6	
		56			38	115,15	1.7	
		54			127	220,10	1.5	
		56			50	210,5	0.6	
		60			10	110	0.3	
		55			5	120	0.6	
		52			20	125	r=21	
		60			15	220,80		
		50			r=4	0		
		48				r=9		
		56						
		60						
		58						
		53						
		60						
		51						
	1	55	1					
		t		1	1		1	
Waypoint 243								
37.80085		1		1			1	
119.47417	2370	66	-90		30	340	0.2	r=7
		67	<u> </u>	<u> </u>	5	335	0.1	

	64	3	340	0.3
(52	1	200	0.9
(52	5	330	0.5
	50	50	190,32	0.9
	65	25	195	0.6
	52	80	165	0.2
	51	10	280	0.1
(54	10	185	0.4
(52	5	180	0.3
4	57	100	145	0.6
	50	2	140	0.9
4.5	58	40	r=9	0.3
	56	5		0.25
4	55	10		0.15
(54	r=4		0.15
	62			0.3
				r=15

Little Yose	mite V	alley						
Waypoint								
166 (LY7)								
				Joint	Joint	Joint	Joint	
	Elev.			length	width	strike and	spacing	
Lat/Long	(m)	SH	Alpha		(mm)	dip	(m)	Continuity
37.73994								
119.42727	2170	66	-90	>5 (1)	na	220	0.3	r=6
		48		3-4.5 (2)	0.1	170	1.2	
		68		2 (3)	0.1	170	1.5	
		72		2.5 (4)	na	210	0.6	
		65		2 (5)	0.1	181	0.9	
				>3, >15				
		66		(6)	na	215	0.6	
		66			r=7	r=20	2	
		72					4	
		72					0.9	
		66					1.33	
		72					0.9	
		72					r=21	
		71						
		64						
		68						
		70						
		69						
		67						
Waypoint								
167								
37.73887								
119.42755	2202	51	-90	>20 (1)	0.5	200	1.2	r=6
		48		4(2)	1	170	0.6	
		62		3.5 (3)	5	220	0.3	
		55		3.5 (4)	na	215	5	
		47		4 (5)	na	170	0.2	

	1	1	1	1	1	1	1	
				>10 (V1)				
				Very				
		52		fractured	15	120	4	
		57		>6 (V2)	10	150	0.9	
		55		0.9 (6)	r=4	r=14	r=21	
		54						
		61						
		63						
		62						
		56						
		51						
		56						
		54						
		60						
		56						
Waypoint								
168 (LY8)								
37.72949								
119.39222	2238	54	-90	3.5 (1)	5	55	1.2	r=6
		50		10 (2)	75	345,90	0.3	-
		52		1.5 (3)	2	110	0.6	
		53		1.5 (F1)	150	325	0.3	
		48		1 (F2)	5	35	0.1	
		54		- ()	5	r=9	0.2	
		52			r=4		0.5	
		50					0.2	
		56					0.4	
		57					0.6	
		52					1.5	
		54					0.4	
		52					r=21	
		53						
		50						
		52						
		52						
						+		
1	1	1	I					

Waypoint								
169								
37.72964								
119.39174	2263	56	-45	>20 (1)	na	60	2	r=6
		56		>5 (2)	0.2	55	1.2	
		58		2 (3)	1	10	3	
		53		>10 (4)	0.1	60	1.5	
				, ,				
		60		>15 (V1)	0.1	135	2	
		58		10 (V2)	0.3	130	2.5	
		57		>10 (V3)	na	135	2.03	
		55			r=7	r=20	2	
		48					r=28	
		62						
		62						
		56						
		54						
		56						
		52						
		53						
		64						
		56						
Waypoint								
170	2279	50	-90	2(1)	1	60	3	r=5
37.72975								
119.39133		58		4(2)	130	65,90	0.3	
		48		2 (3)	10	45,90	1.2	
		61		1 (4)	20	160,.90	2	
		57		4 (5)	5	90,84	0.9	
		51		6 (F1)	130	70	2	
		61		2 (F2)	5	175,30	1	
		66		1 (F3)	1	165,50	0.2	
		64		2.5 (F4)	na	225,60	0.9	
		56			7.5	r=9	1	
		52			r=4		r=28	
		58				1		
		53						
		60						

		T						1
		52						
		55						
		53						
		57			<u> </u>			
Waypoint 171								
37.73012								
119.39083	2313	55	-90	>10	1	70	0.9	r=6
		54		>3 (2)	0.5	60	1	
		60		2 (3)	0.1	90	3	
		54		1.5 (F1)	0.2	60	2	
		56		5 (2)	0.5	40	1.73	
		58		>8 (1)	r=6	r=18	1.5	
		58		>0 (1)	7-0	7-10	r=28	
		53					7-20	
		57						
		_						
		55						
		52						
		50			-			
		51						
		54						
		60						
		54						
		56						
		55						1
Waypoint 172 (LY6)								
37.74175								
119.44622	2143	52	-45	>10 (1)	face	280,77	2	r=6
		54		2.5 (2)	1	205,80	0.9	
		58		3.5 (3)	100	270,90	1.5	
		54		2 (4)	30.5	205,90	1.2	
		48		>15 (5)	60	275,90	4	
						,		
		54		>10 (V1)	100	15	0.6	
		56		(- /	r=2	r=18	1.35	
		56	1				r=28	1
		55			 			
		55		1	<u> </u>			

			1				T	,
		48						
		52						
		47						
		50						
		51						
		53						
		54						
		51						
		56						
		60						
		58						
		53						
Waypoint								
173		<u> </u>						
37.74169								
119.44644	2151	54	-45	2(1)	2.5	150,85	0.3	r=6
		54		1 (Set 1)		225,80	0.2	
		57		2.5 (F1)	5	10	0.2	
		58		3 (2)	20	310	0.3	
		62		>5 (V1)	10	355	0.5	
		58		>4 (V2)	30.5	355	4	
		60		>4 (V3)	122	0	3.5	
		56			r=4	r=9	2.5	
		62					2	
		64					3	
		52					1.65	
		54					1.25	
		58					r=28	
		62						
		56						
		62						
		62						
		58						
		1						
Waypoint 174								
37.73779								
119.45259								
	•	•		•		•	•	

Waypoint								
175 (LY5)								
37.74176								
119.45863	2032	55	-90	>9, 4 (1)	1	30,86	0.3	r=6
		55		0.5-2 (2)	17.5	65	0.9	
		47		1.75 (3)	14	85	2	
		60		> 9 (4)	5	55	3	
		53		9 (5)	face	110	1.55	
		54		9 (6)	25.5	30,90	1.45	
		54		1.75 (7)	na	165	r=28	
		58			r=4	r=18		
		50						
		53						
		50						
		56						
		56						
		54						
		56						
		58						
		56						
		54						
Waypoint								
176								
37.74168								
119.45834	2054	52	-90	3 (1)	10	45	0.6	r=5
		56		>5 (2)	10	30,88	0.3	
		46		4.5 (3)	30	125,90	0.2	
		56		2.5 (4)	50	45,80	0.3	
		53		1.75 (5)	130	115,90	0.1	
		55		? (6)	15	15,86	1	
		49		2 (F1)	30	295	2	
		54			r=2	r=14	2	
		56					0.45	
		57					r=21	
		54						
		53						
		58						
		50						

20 0.1 r=6
140 0.01
50 0.3
180 0.02
110 0.01
0.2
140 0.3
50 0.3
115 0.3
130,90 0.6
30,85 0.6
125,80 0.1
25,80 0.01
75 0.6
80 0.2
85 0.24
25 0.2
165 r=15
r=18
!
35 1.2 r=6
e 320,85 4
30 3.5
315 or
220,80 as
joint. 5

r=6

Waypoint								
180								
37.74396								
119.45820	2041	55	-45	3 (1)	6	75,50	r=21	r=5
		56	1	5.5 (2)	face	75,90		
		54		3.5 (3)	1.5	55,87		
		52		1 (4)	2	75		
		58		5 (F1)	10	140		
		54			4	r=14		
		57			r=5			
		56						
		58						
		58						
		54						
		56						
		55						
		57						
		54						
		55						
		52						
		55						
Waypoint								
181 (LY4)								
						95,90 or		
37.74186						175		
119.45962	2035	54	-45	3.5	25	(flake)	0.1	r=5
						35,90 or		
						300		
		56		2.5	10	(flake)	0.1	
		55		0.7 (1)	10	345,55	0.2	
		51		0.5 (2)	15	285	0.3	
		52		1 (3)	75	195	0.15	
						measure		
				0.7.40	10	from	0.6	
		52		0.7 (4)	10	photos	0.6	
		54		3 (5)	10	340,60	0.2	
					100			
		54		> 3 (V1)	100	255	0.3	
		58			10	r=9	0.1	

	ı		1	T	T .		T _a	1
		58			r=4		2	
		51					0.6	
		54					0.6	
		52					0.25	
		48					r=15	
		54						
		50						
		55						
		53						
Waypoint 182								
37.74182								
119.45968	2044	60	-90	>8 (1)	2.5	220,80	0.3	r=6
		56		2 (2)	na	130,75	0.5	
		59		3.5 (3)	face	150,45	1	
		51		4 (4)	na	115,80	0.6	
		62		2 (5)	1	215,80	2	
		56		3.5 (6)	2.5	255	0.6	
		59		3 (F1)	3	190	2	
		57		, ,	r=5	r=14	0.6	
		56					r=21	
		63						
		60						
		52						
		52						
		55						
		62					†	
		56			1	†	†	
		56			1	+	+	
								+
		57						
Waypoint 183 (LY2)								
183 (LY2)								
183 (LY2) 37.74653	1935	57	-45?	> 5 (1)	20	200.70	0.3	r=5
183 (LY2)	1935	57 54	-45?	> 5 (1) 2 (2)	20	200,70	0.3	r=5
183 (LY2) 37.74653	1935	54 54	-45?	2 (2)	0.1	35	0.1	r=5
183 (LY2) 37.74653	1935	57 54	-45?					r=5

	1	50			1		12	
		52			r=4		2	
		51					2	<u> </u>
		52					1.5	
		58					1.2	
		53					r=21	
		52						
		55						
		54						
		54						
		59						
		58						
		53						
		55						
Waypoint								
184								
37.74741								
119.47275	1997	60	-90	3 (1)	1	315	0.6	r=6
		58		>3.5 (2)	2	70,80	0.9	
		55		3 (3)	1	20	0.6	
		56		2.5 (4)	1	295	2.5	
		52		>4 (5)	1	260	4	
		61		>10 (6)	r=6	275	2	
		60		7 10 (0)		r=20	1.2	1
		52					1.2	1
		58					r=28	1
		54					7-20	
		64			1			
		62						+
		64						+
	-	52						
		62				+		
		55				1		
	-	56				+		
	-	58			-	+		
		30						
XX 7. • 4					-	1		
Waypoint								
185 (LY1)								

				No				
37.73752				visible				
119.47859	1964	53	-90	joints.	r=7	r=20	r=30	r=7
		56						
		66						
		54						
		56						
		60						
		58						
		60						
		56						
		64						
		54						
		52						
		56						
		58						
		54						
		59						
		52						
		57						
Waypoint								
186								
37.73841								
119.47932	2018	54	-90	5 (F1)	100	90	0.3	r=6
						250 or		
				1.75 (F2		045,90 as		
		53		?)	25	joint	0.6	
		49		1.5 (F2)	50	330	0.9	
		53		2 (F3)	50	115	4	
		55		2 (F4)	60	230	3	
		57		0.5 (1)	5	220	0.9	
		53		2.5 (2)	2.5	165	0.6	
		55		>3 (3)	30	90,85	0.9	
		50		>8 (V1)	150	70	r=21	
				1.75				
		54		(V2)	4	105		
		56		>4 (V3)	100	225		
		50			40	r=9		
		52			r=2			

		58						
		54						
		56						
		55						
		54						
Waypoint 187								
37.73683								
119.47863	1959	50	-90	2(1)	2	355	0.6	r=6
		54		>3 (2)	na	100,80	1.5	
		54		1.5 (3)	na	45	1.2	
		56		4 (4)	4	270	2	
		56		>3.5 (5)	3	350	1	
		52		3 (F1)	1	290	1.2	
		57			r=6	r=20	r=28	
		58						
		53						
		53						
		54						
		56						
		52						
		56						
		57						
		55						
		58						
		55						

San Joaqui	n River	valle	ey					
Waypoint								
58 (SJ4)								
· · · · · ·				Joint	Joint	Spacing		
	Elev.			length	width	between	Joint strike	
Lat/Long	(m)	SH	Alpha		(mm)	joints (m)	and dip	Continuity
				No				
37.51050				visible				
119.19923	1402	36	-90	joints.	r=7	r=30	r=20	r=7
		62		,				
		56						
		42						
		42						
	1	65						
		64						
		33						
		57						
		57						
		63						
		59						
		60						
		42						
		46						
		61						
		58						
		53						
Waypoint								
59								
				No				
37.51066				visible				
119.19910	1404	44	-90	jointing.	r=7	r=30	r=20	r=7
		62	1	J ~ G ·	-			-
	†	66						
	†	68						
	†	50						
	+	64				†		
	+	53						
	1	44				1		

	1	1	T	1	-	1	- T	
		62						
		56						
		64						
		41						
		58						
		53						
		59						
		68						
		58						
		57						
Waypoint 60								
37.51073								
119.19906	1405	52	-90	10	2	0.50	206, 82	r=6
		64		0.5	10	0.30	306,76	
		44		0.3	50.8	0.60	r=14	
		58		1	25	0.47		
		34		1.3	21.95	r=21		
		56		1	17.5			
		48		0.1	r=7			
		50						
		50						
		64						
		38						
		39						
		40						
		41						
		36						
		49						
		54						
		48						
Wownsint								
Waypoint 61								
37.51076								
119.19904	1410	50	-90	1.5	na	0.25	359,63	r=5
		38		0.8	na	0.15	6	
		49		1	150	0.90	19	
		33		2.4	50	0.50	r=9	

		42		2.5	r=5	0.90		
		60		2		0.54		
		38		1.75		0.50		
		54		0.18		r=21		
		38						
		56						
		58						
		52						
		44						
		62						
		42						
		52						
		40						
		48						
Waypoint 62								
37.51082							169,85/165	
119.19893	1420	63	-90	0.4	76	0.20	,64	r=5
		69		0.5	76	1.50	205,85	
		59		3.5	0.1	0.15	195,84	
		56		3	0.1	0.62	97,89	
		64		1	0.1	0.20	19,90	
		62		1.5	30.46	r=15	r=14	
		61		1.3	0.1			
		45		2	r=6			
		52		1.4				
		55		0.14				
		62						
		57						
		42						
		39						
		48						
		50						
		65						
		53						
		56						
	•	•	•	•	•	•	•	

	ı	ı	1		1		1	
Waypoint								
63								
37.51093								
119.19892	1416	52	-90	1	neg	1.80	15,90	r=6
		66		2	neg	0.30	10,100	
		34		2.5	20	0.60	21,76	
		58		10	r=4	0.90	r=9	
		45		2.25		0.60		
		59		0.225		r=21		
		59						
		54						
		54						
		52						
		32						
		48						
		54						
		52						
		42						
		54						
		48			1			
		51						
Waypoint					1			
64								
37.51105								
119.19889	1422	51	-45	20 (1)	10	0.30	17,88	
		52		15 (2)	20	0.15	23,75	
		42			15	0.50	r=14	r=5
		45			r=4	0.32		
		39				0.31		
		46				r=15		
		32						
		52						
		52	1					
		41	1		1			
		54	1		1			
		54						
	1	44	†					
	1	29	†					
		37	†					
		51	<u> </u>					

	1	1	1	1		ī	1	1
		54						
		45						
		45						
Waypoint								
65 (SJ3)								
37.51120								
119.20140	1363	42	-90	25	10	0.20	0	r=5
		51		15	100	1.20	191,72	
		32		10	20	1.80	99	
		48		1	15	1.07	r=14	
		42		1.5	50	1.20		
		54		1.5	39	r=28		
		37		5.75	20			
		62		1	r=4			
		45						
		38						
		35						
		48						
		38						
		40						
		30						
		38						
		51						
		43						
Waypoint 66								
00							350,35	
							(joint set	
							roughly	
37.50979							equivalent)	
119.20454	1388	40	-90	6	152	0.15	equivalent)	r=5
119.20434	1300		-90	6		0.15	r=14	1-3
		50 41	-	0.3	30 20	0.30	r=14	
		44	-	0.3		1.80		
			1	0.3 0.03	40	1.50		
		30		0.03	60.5 35	0.90		
	-	40 30	-		r=5	0.93		
			1		r=3	0.90		
		28				r=21		

		52						
		43		2	r=6	r=30	r=18	
119.20475	1398	33	-90	20	5	>30	185,63	r=6
37.50988								
Waypoint 68								
***	1							
		53						
		40						
		47						
		58						
		49						
		38						
		43						
		55						
		59						
		51						
		64						
		44						
		64						
		63						
		52						
		60						
		62		0	r=7	r=30	r=20	
119.20474	1391	54	-45		joints.	>30		r=7
37.50982					visible			
· · ·	1				No			
Waypoint 67								
		39						
		38						
		48						
		30						
		31						
		35						
		48						
		42						
		42						
		44						

1	1		ī	ı
58				
52				
54				
60				
62				
48				
44				
50				
54				
68				
42				
45				
42				
38				
50				
68				
(P)				
70				
70				
68				
66				
68				
68				
64				
68				
72				
71				
69				
74				
74				
74				
67				
70				
70				
1 1				
1 1				
1 1	 1	<u> </u>	l	

Waypoint								
69								
37.50995				>20				
119.20486	1405	34	-90	(closed)		>30	205,35	r=6
		42		0	r=5	r=30	r=18	
		43						
		53						
		54						
		56						
		52						
		55						
		33						
		46						
		33						
		35						
		48						
		52						
		35						
		49						
		52						
		45						
Waypoint								
70 (SJ4)								
27.51004							201.70	
37.51024 119.199528	1392	60	00	_	25	2.00	281,78	- -
119.199328	1392	60	-90	6	35	2.00	(lower)	r=5
		62			76	0.20	193,58	
		02		2	76	0.20	(left)	
		60		0.2	1	0.20	38,89	
		60		0.2	1	0.30	(right)	+
		61		0.2		0.20	277,69	
		64		0.3	2	0.30	(upper)	+
		60		1.15	152	0.50	r=14	+
		63		0.115	53.2	1.50		+
		64			35	0.05	1	1
		70			r=2	0.07	1	1
		60				0.05	1	1
		58				0.07	1	

		50				0.07			
		66				0.07			
		65				0.05			
		65				0.06			
		61				0.05			
		60				0.07			
		64				0.34			
		62				0.07			
						r=15			
Waypoint 71									
37.51012									
119.19937	1405	52	-90	2	76	0.07	201,74		5
		52		2	250	0.50	304,79		
							roughly		
							parallel to		
		36		1.5	100	1.20	joint 1	r=5	
		66		1.2	100	1.20	r=14		
		48		1.5	250	1.20			
		65		25	20	1.00			
		52		1.75	10	1.00			
		65		0.175	10	0.15			
		70			15	0.15			
		44			0.5	0.20			
		64			0.5	0.20			
		56			75.64	0.30			
		66			47.82	1.50			
		54			r=4	1.30			
		66				0.71			
		55				0.75			
		52				r=21			
		57							
Waypoint 72									
37.50989		1							
119.19945	1426	58	-90	25	300	0.15	304,39	r=6	
		60	<u></u>	4	127	2.00	105,83		

	1	T	T T	Т.	1	1		
		47		4	20	0.60	r=14	
		50		0.5	10	3.50		
		50		1	20	1.20		
		60		4	100	0.30		
		50		0.4	30	1.50		
		56			87	1.50		
		50			30	0.30		
		56			r=2	1.23		
		58				1.20		
		54				r=21		
		52						
		64						
		45						
		38						
		50						
		53						
Waypoint								
73								
37.50974								
119.19944	1440	54	-90	20	64	0.50	281,32	r=5
		55		1.5	20	0.60	10,84	
		55		1	10	1.80	12,80	
		48		2	20	2.50	290,25	
		56		2.5	100	1.80	r=14	
		59		2.5	150	1.50		
		42		1.8	80	0.60		
		54		2	100	1.40		
		58		2	30	2.00		
		60		1.5	20	1.41		
		50		2	10	1.50		
		60		0.2	55	r=28		
		53			30			
		64			r=2			
		48						
		52						
		63	1					
		55		1				
				1				
Ī	I							1

Wormsin4								1
Waypoint								
smoking								
crack								
(Double								
check all								
previous								
waypoints)								
	1450	45	-45	3.5 (1)	5	1.50	353,48	r-6
		44		> 9 (2)	17.8	1.50	11,45	
		53		3 (3)	6	2.00	35,na	
		55		> 20 (4)		1.00	6,64	
		40		1 (5)	4	1.00	110,67	
		52			8.56	3.00	r=21	
		46			6	1.67		
		52			r=4	1.50		
		58				r=28		
		64						
		40						
		48						
		38						
		45						
		54						
		24						
		42						
		47						
Waypoint 74 (SJ2)								
37.49036								
119.20627	1343	49	-90	2.5	100	0.75	135,45	r=5
		56	-	1	50	0.50	242,49	
		52		1.5	150	0.90	r=9	
		41		2	100	1.00		
		56		1.75	100	0.75		
		54		0.175	100	1.00		
		50			r=2	0.82		
		44			_	0.83		
		48				r=21		
		45				. —		
<u> </u>		TJ	l		<u> </u>	<u> </u>	<u> </u>	

						_		
		58						
		34						
		58						
		56						
		58						
		47						
		62						
		51						
Waypoint 75								
37.49047								
119.20604	1363	61	-45	20	1	5.00	276,74	r=6
		62		20	2	0.30	331,31	
		56		5	0.1	0.30	261,73	
		68		1	0.5	4.00	260,75	
		44		4	4	20.00	r=14	
		53		5	10	10.00		
		30		5	1	0.90		
		51		0.5	2.66	5.79		
		38			1	4.00		
		62			r=6	r=30		
		52						
		63						
		61						
		64						
		61						
		64						
		57						
		56						
Waypoint 76								
37.49050				>20				
119.20582	1369	48	-90	(closed)	10	>30	261,64	r=7
117.20302	1309	46	-50	0	r=7	r=30	r=9	
		52	1	0	/ - /	1-30	1-7	
		50	+	+	1			
		29	+	+	1			
		29						

	_			•		_	1	
		48						
		56						
		49						
		52						
		67						
		54						
		60						
		50						
		57						
		56						
		56						
		45						
		51						
Waypoint								
77								
				No				
37.49066				visible				
119.20564	1383	49	-90	jointing	r=7	r=30	r=20	<i>r=7</i>
117,12000.	1000	52	70	0				
		58						
		62						
		44						
		38						
		54						
		69						
		52						
		52						
		55						
		63						
		53						
		66						
		60						
		64						
		40						
		55						
L								

l l

		44		2.5				
		42		0.25				
		40						
		38						
		38						
		44						
		38						
Waypoint 80								
37.49085								
119.20469	1439	62	-90	3	40	0.50	104,65	r=6
		70		3.5	0	0.30	42,85	
		50		3.5	127	0.30	110	
		54		3	25	0.90	310,30	
		46		3	20	1.20	220,80	
		62		3.5	53	0.30	r=14	
		58		1	32.5	1.50		
		64		0.8	r=2	1.00		
		44		1		0.75		
		44		0.9		0.70		
		36		0.8		r=21		
		58		3				
		48		2				
		42		3				
		56		2.5				
		34		3				
		36		3				
		51		0.3				
Waypoint 81								
37.48689				1				
119.20548								
				1				
Waypoint 82 (SJ1)								
37.4823								
119.20902	1377	36	-90	3.5	0	1.00	276,76	r=6
		24		1	0	3.50	9,51	

		41		0.9	0	2.50	159,75	
		53		0.5	r=6	1.50	r=18	
		56		2		1.00		
		52		1		1.80		
		54				2.00		
		58				1.80		
		41				1.89		
		54				1.80		
		65				r=28		
		65						
		53						
		60						
		55						
		61						
		44						
		51						
Waypoint 83								
37.48283								
119.20913	1380	63	-90	1 (1)	0	0.30	258,65	r=6
119.20918	1500	61		3.5 (2)	0	5.00	295	
		01		3.3 (2)	Ů.	3.00	275	
		52		> 20 (3)	0	3.00	261	
		68		7 20 (3)	r=7	2.77	r=20	
		49		0		r=28	7 20	
		38		0		7-20		
		52						
		60						
		45						
		60						
		42						
		55						
		52						
		48	 					
		32						
		51	 					
		52						
		52	1					
		34						
					<u> </u>			

	-	1	1	1	1	Ī		Ī
Waypoint								
84								
37.48288								
119.20919	1389	66	-90	9	76	0.20	259,79	r=6
		68		0.3	20	0.70	261,65	
		68		0.2	25	1.20	278,70	
		66		1.2	30	1.30	r=14	
		72		1.5	40	1.50		
		70		1.2	100	0.60		
		70		0.12	150	0.92		
		69			63	0.95		
		68			40	r=21		
		66			r=4			
		71						
		66						
		70						
		70						
		71						
		72						
		65						
		69						
Waypoint								
85								
37.48298								
119.20928	1395	46	-90	2.5	150	0.20	34,72	r=6
		47		12	120	0.60	164,60	
		43		12	100	1.20	329,45	
		42		1	face(?)	1.00	23,90	
		42		2	face(?)	1.20	282,85	
		44		4	face(?)	1.00	138,44	
		41		1.5	100	0.87	346,59	
		60		10	25	1.00	251	
		40		3.25	200	r=21	339,59	
	†	56	1	0.325	116		r=14	
	†	43	1		110			
		41	†		r=2			
		38				1		
	1	58	1					
		46	†					
		70				<u> </u>		

		50						1
		39		_				
		46				1		
Waynaint						+		
Waypoint 86								
37.48306								
119.20940	1395	42	-90	2	15	1.00	201,65	r=6
		52		3	300	1.80	300	
		45		1	30	2.00	354	
							18, 66 &	
		52		1.5	20	0.60	20,70	
		33		0.3	10	0.80	280,60	
		51		1.5	face	0.60	r=14	
		32		0.15	face	0.90		
		38			75	1.10		
		59			20	0.90		
		48			r=4	r=21		
		52						
		61						
		63						
		49						
		46						
		48						
		58						
		49						
Waypoint 87								
37.48319								
119.20947	1399	47	-90	8	200	1.80	184,79	r=5
		58		3	50	2.10	245,78	
		38		1	25	1.20	325,77	
		61		10	100	0.90	r=14	
		46		5.5	93.75	0.30		
		60		0.55	75	1.26		
		37	 		r=2	1.20		
		46	1			r=28		
		36	1			1 20		
		49				1		
		^T /	1					

	1	т -	1	1	1	1	1	1
		43						
		36						
		41						
		36						
		56						
		44						
		48						
		46						
Waypoint 88								
37.48331								
119.21954	1398	59	-90	10	180	0.25	270,56	r=5
		62	1	3.5	30	0.61	258	
		43		2	face(?)	1.00	154,58	
		52		2	face(?)	1.20	289	
		43		2	30	0.50	196,71	
		53		1	20	0.20	89,64	
		61		1.5	20	0.30	78	
		67		2	r=2	1.50	r=14	
		36		0.2		1.50		
		55		1		1.20		
		53				0.83		
		63				0.81		
		48				r=21		
		64						
		45						
		46						
		51						
		53						
				†		 	<u> </u>	1
Waypoint				1				1
90								
37.48277	1001				1.26		110.01	
119.20753	1331	36	-90	3	130	0.25	118,81	r=5
		34		1	face	0.90	180,47	1
		28		2.5	100	0.30	NE block	
		48		4	20	0.30	r=14	
		39		1.5	50	0.60		
		56		2.5	60	1.50		<u> </u>

	_		1		_			
		36		0.25	150	1.20		
		39			>20	1.80		
		33			r=2	0.90		
		43				1.80		
		50				0.45		
		50				0.20		
		54				0.90		
		40				1.50		
		33				0.90		
		37				0.90		
		34				r=21		
		41						

Waypoint 188								
37.53322								
119.16740	1560	44	-90	3	40	0.30	185,80	r=5
		44		3	50	0.30	194,70	
		52		3	20	0.15	187,60	
		44		2	30	0.20	259,60	
		52		1.5	25	0.30	175	
				3.5				
				(Flake				
		58		1)	25	0.50	239	
		54		3	>20	0.30	r=14	
		61		0.3	r=2	0.40		
		61				1.00		
		60				0.90		
		52				0.15		
		56				0.20		
		50				0.75		
		49				0.42		
		57				0.30		
		60				r=15		
		59						
		54						
L			1		1			

***	ı	1	1			1	<u> </u>	
Waypoint								
189	1	<u> </u>	<u> </u>					
37.53342		- 0						_
119.16719	1580	60	-90	3	1	0.40	250,65	r=5
		57		3.25	2	1.00	189,65	
		49		1	2.5	1.50	141,69	
		60		1	5	0.30	229,63	
		64		3.3	2	0.15	145	
		49		2.5	7.5	0.20	270,66	
		59		2	5	0.40	131	
		55		4	30.5	1.00	195,86	
		63		1	4	1.20	146,55	
		62		2.5	6.61	0.90	r=14	
		64		0.25	4	0.60		
		50			r=5	0.30		
		52				0.66		
		54				0.50		
		58				r=21		
		50						
		51						
		56						
Waypoint								
190								
37.53392	1 100			• •		2.70	105	_
119.16698	1609	68	-90	20	25	2.50	195	r=5
		65		1.5	50	1.50	239	
		66		3	30	0.30	197	
		68		3	75	1.00	134	
		68		3.5	40	1.20	179,67	
		67		1.5	30	2.00	130	
		67		4	50	2.00	190,41	
		66		1	30	3.50		
		68		20	41.25	0.90	193,59	
		67		3.5	35	1.66	282,26	
		69		1.5	r=2	1.50	190,44	
		71		3		r=28	r=9	
		65		0.3				
		68		İ				
								

	1	1		1	1	1	1	1
		69						
		62						
		67						
Waynaint								
Waypoint 191								
37.53276								
119.16733	1544	48	-90	4	50	1.50	195,85	r=5
		50		3	200	1.00	110	
		47		10	200	0.30	218,56	
		50		2	75	0.20	134	
		50		1.5	25	0.20	190	
		54		1	40	0.30	221	
		51		2.5	>20	0.15	r=9	
		51		0.25	r=2	1.00		
		48				1.20		
		50				0.20		
		44				0.30		
		47				0.15		
		46				2.00		
		53				0.65		
		52				0.30		
		45				r=21		
		57						
		50						
TT 7 • 4								
Waypoint 192 (SJ 7)								
37.53170								
119.17341	1506	73(P	-90	15	60	1.00	200,55	r=6
		72		1.5	>20	1.50	r=9	
		74			r=2	0.30		
		71				1.50		
		75				1.08		
		68				1.25		
		73				r=28		
		73						
		72						
		71						
		73						

	T	5 0	ı			1	
		70					
		74					
		74					
		72					
		70					
		70					
		72					
		58					
		58					
		53					
		60					
		65					
		58					
		56					
		50					
		56					
		57					
		55					
	†	63					
	†	57					
		48					
	1	51					
	1	55					
	 	60	1				
	1	56					
		30					
Waypoint							
193							
37.53152	1						
119.17330	1513	60 (P-90	1	25	0.10	197,71	r=5
117.1730	1313	66	2	25	0.10	135	1-3
	+	56	10	10	7.10	200,61	
		60	1.5	20	0.30	r=9	
		56	1.3	30	1.00	- /	
		50	1.5	50	0.90		
	+	62	0.15	40	0.50		
	+	68	0.13	12	_		
	+				1.00		
		63		>20	0.60		
		64		r=4	0.45		

	T	60				Io 15		
<u> </u>		60				0.15		
		62				1.00		
		66				1.11		
		64				0.55		
		68				r=21		
		64						
		63						
		62						
		72						
		72						
		65						
		72						
		71						
		70						
	1	70				1		
		65						
		72						
		72						
		72						
		72						
		62						
		68						
		64						
		62						
		68						
		69						
		07						
Waypoint								
194								
37.53120								
119.17322	1517	64	-90	10	30-75	2.50	205,84	r=5
	1	64		2	30	2.00	187	
	†	64		7 (F1)	90	2.00	147	
	+	65		20	>20	2.40	r=14	
	+	67		10	r=2	0.25		
		66		1	† -	0.10		
		66		1		0.20		
	+	66				0.20		
		56				3.00		
		JU				5.00		

	ľ		ľ			4 44		
		62				1.42		
		58				2.00		
		68				r=28		
		70						
		67						
		68						
		68						
		68						
		65						
Waypoint								
194 A								
No lat and								
long. Next								
step up from								
waypoint								
194	na	63	-90	3.5	50,70	1.20	189	r=6
		65		15	25	1.00	210,50	
		60		1	25	10.00	175,86	
		56		0.75	40	0.30	209,45	
		60		3.5	50	0.20	286,27	
		65		1	30	0.75	194	
		66		30	>20	1.00	r=14	
		66		3.5	r=2	0.25	, 1,	
		65		0.35	- <u>-</u>	0.50		
		64		0.55		0.15		
		66				1.00		
		60				2.00		+
		58	1			1.53		+
		58	1			0.88		+
		63				r=21		+
		58				1-21		+
		68				+		+
		62						+
		UZ						+
		1				+		
		1				+		+
		-				-		
			<u> </u>			1		

	1	T .	1	1	1			
Waypoint								
195				1				
37.53037								
119.17336	1562	56	-90	2 (1a)	127	1.00	190,90	r=5
		64		2.5 (1b)	100	0.15	207,72	
		58		0.3	75	0.15	240	
		57		2	60	0.15	210	
		66		7.5	30	0.30	184,70	
		63		0.3	25	0.75	217,50	
		60		1.15	>20	0.40	r=14	
		55		0.115	r=2	0.41		
		61				0.30		
		66				r=15		
		56						
		63						
		62						
		62						
		64						
		54						
		60						
		60						
Waypoint								
196 (SJ6)								
37.51215								
119.19344	1412	52	-90	0.5	15	0.30	199	r=5
	1	50	70	0.7	10	0.70	187	
		52		1	35	0.50	128,45	
		56		1	75	0.90	246	
		50		0.7	25	0.90	234	
		57		1.5	200	0.80	250,87	
		58		2	130	0.80	187	+
	1	52		1.5	200	0.60	255,79	+
		52		1.3	230	0.20	129,56	+
		50		3.5	103	0.30	129,50	
		53		3.5	130	0.60	268,79	+
		55		0.35	>20	0.30	r=14	+
		53		0.33	r=2	0.30		+
	1	53		+	1 –2	0.13		+
		JJ		1	<u> </u>	0.90		

		50				1.00		1
		52				1.00		
		57	<u> </u>			0.90		
		50				0.80		
		53				0.63		
						0.70		
						r=21		
Waypoint 197								
37.51190								
119.19352	1423	52	-90	0.8	10	1.20	200,74	r=5
		54		3.5	20	0.45	110 or 290	
		54		1.5	180	0.15	260,80	
		50	†	1	50	0.90	190,68	
		54	1	2	25	0.25	165	
		58		1	25	0.50	156,65	
		56		2	30	0.90	164	
		52		2	100	0.20	226,59	
		51		3	150	0.80	189	
		55		1.5	200	0.90	250,55	
		54		3	10	0.30	110	
		56		2.5	305	0.60	208	
		53		1	50	0.20	259	
		54		2	50	0.15	195	
		58		1	15	0.60	219,76	
		45		2	>20	0.15	r=14	
		55		0.2	r=2	0.20		
		54				0.30		
						0.49		
						0.38		
						r=21		
Waypoint								
198								
37.51131								
119.19362	1451	60	-90	10	1525	1-3m	201,39	r=6
		62		0.7	5	r=28	143	
		66		10	155		223	
		62		10	30		195	
		58		1.5	25		238	
		55		10	150		205	

p.								
		60		1.5	5		137	
		55		2	1		245	
		68		6	1		255	
		60		0.6	210.78		r=14	
		58			25			
		60			r=2			
		52						
		58						
		60						
		55						
		59						
Waypoint 199								
37.51059	+					1		
119.19399	1476	62	-90	4	5.3	1-3m	206	r=6
117.17377	1170	64	70	1	25	r=28	209	7-0
		60		0.6	5	7-20	290,110	
		55		4	10	1	179	
		64		3.5	25	1	199	
		68		3.5	1	+	r=14	
		64		0.35	2	†	,-1,	
		56		0.33	30	†		
		60			10	1		
		61			20			
		61			40	1		
		64			1			
		60			1			
	+	58			2	1		
	1	68			3			
	+	53			1			
	+	64			10			
		61			11.25			
					5.3			
					r=4			
						•	•	

Waypoint 200 (SJ 5)								
37.51109								
119.19582	1439	70(P	-90	2	1	1.75	186	r=5
		71		2	25	3.00	155,36	
		72		1	face	1.75	200	
		72		0.5	100	0.60	146,43	
		74		1	115	0.50	276,73	
		74		0.5	100	0.60	214	
		71		1.5	100	0.30	185,90	
		73		0.9	50	0.15	266	
		70		1	r=2	1.20	r=14	
		72		0.1		0.30		
		72				0.60		
		74				0.90		
		72				0.60		
		70				0.90		
		74				0.94		
		73				0.60		
						r=21		
		68						
		72						
		65						
		70						
		68						
		66						
		66						
		70						
		68						
		63						
		60						
		64						
		64						
		67						
		67						
		68						
		66						
		67						

337	1	1	I					
Waypoint								
201	1							
37.51139 119.19610	1452	61	-90	4	50	2.50	199	r=5
119.19010	1453	64	-90	4		3.50		<i>r=</i> 3
		56		2	15	1.00	225	
	1	63		1.5	25	3.50	149	
		70		1.5	3	0.50	184	
		67		3	50	1.20	285	
		57		4.5	20	0.30	210	
		64		2	10	0.60	195	
		52		2	1	0.90	290 or 110	
		55		1	12	1.20	130	
		59		0.5	5	1.00	188	
		65		3.5	7	1.50	216	
		55		1	2	1.38	285 or 105	
		59		2	6	1.00	283	
		57		2	r=4	r=21	r=9	
		70		0.2				
		52						
		64						
		61						
Waypoint 202								
37.51197	1			3.5 (Set				
119.19695	1502	58	-90	1)	na	0.30	194	r=5
		54		3 (2)	2	1.20	120	
		50		1 (3)	150	0.45	145	
		61		1.5 (4)	100	0.60	190	
		56		3.5 (5)	2	1.50	166	
		58		0.5 (6)	na	0.60	155,45	
		64		2 (7)	100	0.30	225	
		56		4 (8)	30	0.20	193	
		58		3.5 (9)	na	1.80	229	
		42		1 (10)	25	2.00	171	
		52		>4 (11)	100	0.75	143	
				` ´				
		_			ï			
		50 48		>5 (12) 3 (13)	face 25	2.40 0.60	184,70 279	

		55	1		r=2	0.80	r=9	
		57			1-2	0.86	1-2	
		46				0.68		
		56				r=21		
		54				1-21		
		34						
Waypoint								
203								
37.51249								
119.19790	1524	52	-90	>1.5 (1)	50	0.20	219	r=5
117.17770	1324	54	-50	0.7 (2)	75	0.20	265	7-3
		34		1.6 (Set	13	0.30	203	
		57			100	0.60	278	
				3)	50			
		56 57		2.5 (4)	100	0.30	232 148	
		59		2 (5)			161	
				1.2 (6)	50	0.50		
		55		1.2 (7)	20	0.20	218	
		59		2.5 (8)	150	0.75	171	
		59		1 (9)	25	0.45	272	
		65		1.5 (10)	10	0.45	133	
		60		0.5 (11)	5	0.50	203	
		62		0.5 (11)	57.73		r=9	
		63			50	0.60	1-9	
						0.60		
		60			r=2	0.45		
		64				0.60		
		60				0.45		
	1	65	<u> </u>			0.45		
	<u> </u>	59		1		0.90		
		-				1.75		
		-				1.75		
						1.75		
		<u> </u>	1			0.90		
	1	<u> </u>				1.60		
						1.60		
						0.20		
						1.75		
			<u> </u>			1.60		
						0.81		

			0.60	
			r=21	

North Fork	King	River	valley					
Waypoint								
128 (K3)								
				Joint	Joint	Joint	Spacing	
	Elev.			length	width	strike and	between	
Lat/Long	(m)	SH	Alpha	(m)	(mm)	dip	joints (m)	Continuity
37.06516								
118.93773	2174	60	-90	no visible	r=7	r=20	r=30	r=7
		50						
		54						
		60						
		58						
		62						
		58						
		40						
		50						
		60						
		45						
		50						
		54						
		55						
		60						
		62						
		58						
		55.1						
Waypoint 129								
37.06528								
118.93782	2162	72(P)	-90	>5 (1)	25	220	1-3m	r=6
		70		>10 (2)	0	220,80	r=28	
		70			152	r=18		
		70			10			
		66			46.75			
		69			17.5			
		64			r=4			
		72						
		70						
		70						

	I	60	Ī					
	1	68						1
		70			1			
		68						
		72						
		68						
		66						
		70						
		68.9						
Waypoint								
130								
37.06538								
118.93806	2138	60	-90	>2 (1)	20	110	0.8	r=6
		58		3.5 (2)	15	65,60	0.6	
		55		>4 (3)	20	90,65	0.3	
		54		3 (4)	25	145,70	0.3	
		60			10	r=18	0.3	
		55			15		1	
		54			12		1	
		54			13		0.2	
		64			5		1.2	
		58			75		0.63	
		58			25		0.6	
		54			21.36		r=21	
		60			15			
		60			r=4			
		58						
	1	62						
		57.8						
Waypoint								
131			<u></u>					
37.06548								
118.93810	2128	54	-90	4 (1)	100	275,85	1.2	r=6
		59		3 (2)	100	230	1	
		65		0.75 (3)	50	135,75	0.3	
		60		2 (4)	75	125,90	0.5	
		50		>4 (5)	75	25,90	0.3	
		53		>4.5 (6)	50	30,85	0.3	
	1	57		>2.5 (7)	2	45,80	0.8	

			I	0.7.(0)	L	207.00	lo 5	т —
		60		0.5 (8)	1	285,80	0.7	
		64		1 (9)	5	170	1.5	
		61		2 (10)	10	30	1	
		60		>4 (11)	25	40,76	1.2	
		63			44.82	r=9	0.8	
		55			50		0.8	
		62			r=2		r=21	
		55						
		52						
		52						
		57.8						
Waypoint								+
132								
37.06582								
118.9875	2113	57	-90	>4 (1)	1	30,80	0.6	r=6
		53		>4 (2)	1	150	0.3	
		50		3 (3)	3	185,90	1	
		50		>4.5 (4)	2	180	0.2	
		50		1.5 (5)	3	225,30 (?)	0.3	
		54		1 (F1)	5	45	0.2	
		55			1	r=14	0.2	
		51			1		0.3	
		55			1		0.25	
		52			50		0.25	
		51			10		0.6	
		58			5		1.2	
		50			5		1	
		56			2		0.9	
		52			10		0.52	
		52			5		0.3	
		57			50		r=21	
		53.1			9.12			
					3			
	-						L	

Waypoint								
133 (K2)					r=5			
37.05265					1-3			
118.94520	2116	70(P)	-90	>5 (1)	50	230,90	0.6	r=5
110.74320	2110	65	70	>2 (2)	90	90,85	0.25	1-3
		68		1.5 (3)	2	190	1.2	
		66		2 (4)	100	325,60	0.6	
		68		2.5 (5)	150	30,60	1.8	
		68		>5 (V1)	150	315	0.3	
		68		2 (V2)	25	210	1.8	
		71		_ (, _)	81	r=9	0.94	
		66			90	1 -	0.6	
		68			r=2	1	r=21	
		64						
		70						
		68						
		67						
		63						
		68						
		69						
		67.3						
		62						
		60						
		66						
		66						
		56						
		54						
		56						
		44						
		50						
		60						
		52						
		64						
		51						
		60						
		61						
		48						
		53						
		56.6						

Waypoint								
134								
37.05265								
118.94478	2099	68(P)	-90	>5 (1)	25	180	0.3	r=6
		69		5	0.1	r=18	0.3	
		71		0.5	2		1.5	
		70			2		1.8	
		70			0.01		1.8	
		72			5.82		1.14	
		69			2		1.5	
		66			r=5		r=28	
		74						
		70						
		66						
		69						
		69						
		68						
		68						
		72						
		72						
		69.7						
		61						
		40						
		45						
		40						
		60						
		58						
		54						
		62						
		52						
		60						
		44						
		60						
		56						
		58						
		62						
		68						
		54						
		54.9						

Waypoint							
134 A							
No lat and							
long.	72(P)	-90	3 (1)	20	220	0.3	r=6
	71		>3.5 (2)	10	335,20	1	
	69		1.5 (3)	10	170	0.6	
	63		2 (4)	5	170	0.3	
	73		1.5 (5)	na	290,60	1	
	63		2.5 (6)	10	290,65	2.5	
	67		0.5 (7)	na	170	1.2	
	68		3 (8)	30	290	0.5	
	72		3 (9)	15	225	0.25	
	63		3 (10)	40	55,85	0.8	
	65		4 (11)	100	10	1.8	
	64		1 (12)	2	220	1.4	
	69		>3 (13)	180	200,30	1.4	
	62		>3 (14)	100	200,30	0.2	
	63		>5 (15)	200	200,35	6	
	64			55.54	r=18	1.28	
	64			20		1	
	66.3			r=5		r=28	
	60	-90					
	63						
	54						
	57						
	58						
	56						
	51						
	49						
	61						
	52						
	44						
	60						
	70						
	58						
	54						
	54						
	52						
	56.1						

Waypoint								
135								
37.05229								
118.94422	2070	70(P)	-90	>5 (1)	60	180,80	0.6	r=6
		66		>5 (2)	305	170	1.8	
		68		2 (3)	75	260	3	
		58		1 (4)	100	295	1	
		68		3 (5)	75	265,82	1.2	
		70		4 (6)	20	220,90	0.8	
		72			10	r=18	1	
		70			30		0.15	
		65			84.38		0.3	
		72			67.5		1.09	
		60			r=2		1	
		70					r=21	
		72						
		65						
		72						
		60						
		72						
		67.5						
		60						
		62						
		50						
		52						
		62						
		56						
		52						
		56						
		62						
		58						
		60						
		51						
		60						
		48						
		55						
	1	65						
		55						
		56.7						

Waypoint					Ī			
136 (K1)					<u></u>			
37.05656								
118.94321	2058	72(P)	-90	>10 (1)	1	325	1.2	r=6
		68		>10 (2)	2	355	1.5	
		70		4 (3)	1	235,85	1.8	
		72			3	r=20	2.5	
		74			1		3	
		72			1.6		2	
		75			1		1.8	
		71			r=6		r=28	
		72						
		69						
		72						
		70						
		68						
		66						
		72						
		71						
		69						
		70.7						
		54						
		44						
		60						
		52						
		50						
		56						
		40						
		54						
		55						
		48						
		56						
		52						
		45						
		52						
		47						
		58						
		61						
		52						

Waypoint								
137								
37.05655								
118.94260	2065	70(P)	-90	2-2.5	50	35 (as flak	0.3	r=5
110.5 1200	2003	74	70	>10 (2)	100		0.5	7-3
		68		>7 (3)	90		0.25	
		70		1.5 (4)	10		0.25	
		72		1.5 (+)	r=2	r=9	0.5	
		72			1-2	1-7	0.3	
		70					0.45	
		69					0.43	
		66					0.6	
		70					1.8	
		72					1	
		68					1	
		72					1.2	
		70					1	
		70					1.2	
		64					1	
		71					1	
		69.9					1.2	
		50					2.5	
		52					0.86	
		48					1	
		56					r=21	
		60						
		58						
		60						
		52						
		54						
		42						
		59						
		52						
		61						
		43						
		60						
		62						
		60						
		54.6						

2083	71(P)	-90	1.5 (1)	20	330.82	r-30	r=6
2003		70				1-30	7-0
			3.3 (4)				
				7-0			
2097	74	-45	15 (1)	10	350,90	0.9	r=6
	74			na	55	0.6	
	71		3.5 (F1)	1	150	1.8	
	70			0.1	140	1.5	
	70			2	155	2.1	
	69			1.5	r=14	1.38	
	72			r=5		1.5	
	71					r=28	
	70						
	67						
	70						
1	50	ì	1				
	72						
	72 72						
	2083	66 68 70 71 68 72 68 70 73 70 69 72 70 72 71 68 69.9 2097 74 74 71 70 69 72 71 70 69 72 71 68	666 688 70 71 688 72 688 70 73 70 73 70 69 72 71 68 69.9 2097 74 -45 74 71 70 70 69 72 71 70 70 70 69 72 71 70 70 70 70 70 70 70 70 70 70 70 70 70	66	66	66	66

		69						
		70.8						
Waypoint								
140								
37.05666								
118.94155								
(very poor								
satellite								
reception.)	2212	61	-45	2-2.5	50	50,30	0.6	r-6
		58		2 (2)	1	350	0.25	
		56		0.5-1.5	1	335,80	0.2	
		52			2	r=14	0.15	
		43			1		0.15	
		58			4		0.25	
		60			2		0.2	
		44			3		0.15	
		61			2		0.9	
		47			100		0.8	
		60			51		0.15	
		48			25		0.6	
		61			50		0.3	1
		56			10		0.36	
		50			150		0.25	
		52			10		r=15	1
		61			20			
		54.6			200			
					100			
					41.16			
					10			
					r=4			
Waypoint								1
141 (K5)								
37.08646								
118.89583	2379	52	-90	>4 (1)	75	175,70	0.5	r=5
		60		>4 (2)	90	220	1	
		61		1.75 (3)	1	145	0.15	
		50		1 (4)	5	150,60	0.9	
		54		1 (5)	1	290	1.8	
		52		2 (6)	2	220,50	1	1

		50	1	I	20	0	0.6	1
		50			29	r=9	0.6	
		56			3.5		0.15	
		50			r=6		1	
		50					1.5	
		58					0.86	
		52					0.95	
		58					r=21	
		63						
		56						
		58						
		59						
		55.2						
Waynaint	1							
Waypoint 142								
37.08659								
118.89581	2374	55	-45	>20 (1)	150	210,85	1.8	r=5
		60		1 (2)	10	260,90	2.4	
		58		2.5 (3)	na	305	2.75	
		56		3 (4)	0	200	0.3	
		57		4.5 (F1)	75	115	0.6	
		50		3 (F2)	15	120	0.15	
		58		>15 (V1)		195	2.4	
		49			50	125	0.2	
		41		>10 (V3)		120	0.15	
		61		, ,	1	r=14	0.6	
	†	60			1		0.3	+
	1	53			2		0.6	
	1	60			10		1	
	1	42			20		1.02	
		59			50		0.6	+
	1	54			1		r=21	
		58			48.67			
		54.8			15			
					r=4			
	1							
		ı	L	1	ı	1	_1	

Waypoint	I							
143								
37.08673						+		
118.89556	2360	53	-45	3 (1)	4	190	0.75	r=6
110.0000	2500	58	1.0	3 (2)	face	70,60	0.3	-0
		61		3.5 (F3)	120	150	0.15	
		48		2 (F4)	50	205	0.15	
		56		2 (5)	face	210,80	0.45	
		60		2 (F6)	50	275	0.45	
		44		2.5 (7)	face	200	0.5	
		52		>3 (8)	75	r=9	0.2	
		58		73 (0)	r=2	, ->	0.3	
		61			7-2		0.15	
		54				+	0.3	
		47					0.3	
		56				+	0.15	
		58				+	0.25	
		46				+	0.2	
		52					0.3	
		54					0.4	
		54					0.25	
		54				+	0.23	
							0.3	
							r=15	
						+	7-13	
Waypoint 144								
37.08733		4.0			1.50			
118.89536	2370	48	-90	1.5 (1)	150	0,20	1.2	r-5
		56		>4 (2)	face	95,80	0.3	
		60		>4.5 (3)	75	15,55	0.45	
		49		3.5 (4)	10	115	1.2	
		50		>3 (5)	10	40	1.5	
		58		1 (6)	30	35	1	
		56		1 (7)	10	60	1	
		52		>2 (8)	0	140	1.2	
		53		3 (9)	0	20	1.8	
		55			35.63	r=9	1.07	
		57			10		1.2	
		58			r=4		r=28	

146	<u> </u>							
Waypoint								
	1				r=4		r=21	
					20		0.6	
					36.59		0.91	
	<u> </u>	53.6			10		3	
	†	62			20		0.45	
	†	48			100		0.3	
	†	60			30		0.3	
	<u> </u>	58			20		1.2	
	†	53			40		1	
	<u> </u>	60			60	- 1	0.45	
		45		- (-)	10	r=9	0.6	
	†	53		2 (9)	5	90	1	
	<u> </u>	61		0.3 (F8)	100	55	1.2	
		42		1.5 (7)	2	0,90	0.45	
	†	57	1	>5 (6)	130	30,80	0.45	
	1	54		0.5-2.5 (S		135,55	0.6	
	1	43		3 (F4)	20	285	0.3	
	+	57		1 (3)	0.001	65(J), 160		
110.07310	2300	50	-70	4 (2)	0.001	25	1.8	1-3
118.89510	2388	55	-90	>10 (1)	25	45,75	0.3	r=5
37.08774	-							
Waypoint 145								
337 • .	1							
	1	54	ļ					
	1	55						
		44						
		52						
		60						
		55						

		42		>3 (6)	100	325		
		60		()	105	r=14		
		58			115			
		52			r=2			
		60						
		54						
		61						
		56						
		50						
		52						
		60						
		58						
		54.7						
Waypoint 147 (K4)								
37.07589								
118.91648	2196	60	-90	>5 (1)	100	20	1-3m	r=6
		51		>4 (2)	100	180,75	r=28	
		42		1 (3)	na	320		
		54		>5 (4)	150	10,70		
		50		3 (5)	na	355,90		
		40		3 (?) (F1)	0.001	115		
		50			1	r=18		
		60			1			
		56			2			
		55			0.001			
		61			44.25			
		42			1.5			
		58			r=5			
		50						
		58						
		54						
		60						
		53						

Waypoint								
147								
37.07623	 							
118.91647	2211	40	-90	4-10(Set)	75	10,90	1	r=5
		57			10	290,80	1.2	
		51		3 (3)	60	280	1.5	
		59		2.5 (4)	75	255,86	1.2	
		46		2 (5)	na	350	1.8	
		57		3.5 (6)	125	85,70	3	
		53		1.5 (F1)	25	15	0.6	
		60		1 (F2)	10	280,77	1	
		54		, ,	r=2	r=14	0.9	
		48					2.5	
		52					0.6	
		55					2.5	
		56					1	
		62					0.9	
		54					1.41	
		47					1.1	
		56					r=28	
		53.4						
Waypoint 149								
37.07677								
118.91641	2227	63	-45	3 (1)	200	80,86	0.3	r=5
110001011	1227	54		>6 (2)	300	30,90	0.45	1-0
	 	58		1.5 (3)	120	5,85	0.6	
		50		1.5 (4)	100	35,90	0.3	
		57		>5 (5)	60	355,90	0.2	
		46		4 (6)	na	105	0.3	
		52		0.3 (Set 1		r=14	0.9	
	†	56		0.2 (Set 2			0.75	
	<u> </u>	58		- (~ CC Z			1.2	
		54					1.2	
	†	43					1.5	
	<u> </u>	54					2	
		58					2	
	1	48	1		1		1	1
		4 8					11	

		56		Ī		I	1	
		61		+		+	1.2	
	1	54.7					0.93	
	1	34.7					0.9	
							r=21	
Waypoint							1-21	
150								
37.07800								
118.91647	2269	57	-90	8 (1)	0.5	5	>3m	r=6
		46		3 (2)	0.001	5	r=30	
		63		5 (3)	1	45,90		
		60		4 (F1)	1	20		
		53		2.5 (F2)	1	40		
		44			0.1	r=9		
		54			0.5			
		62			0.59			
		52			0.5			
		55			r=6			
		60						
		50						
		43						
		62						
		50						
		56						
		54.2						
Waypoint								
151								
37.07874				• • • • • • • • • • • • • • • • • • • •		0.00		
118.91603	2311	57	-90	>20 (1)	75	0,90	0.3	r=6
		52		1.8 (2)	1	218,80	0.15	
		62		2.5 (3)	face	110,86	0.2	
		48		2 (4) F? (255	0.6	
		58		3 (F1)	150	250	1.5	1
		52		>3 (F2)	face	215,90	0.3	1
		61		1.5 (F3)	75	0,80	0.6	
		44		2.5 (F4)	1	30	0.5	
		50		1.2 (F5)	2	350	0.3	
		56		1 (F6)	2	350	0.6	
		50			30	r=9	0.3	

					т		ī	
		41			20		0.15	
		58			10		0.1	
		52			5		1.2	
		52			10		1.5	
		54			1		0.45	
		43			50		6	
		52.4			40		0.3	
					100		1.2	
					35.41		1.5	
					20		0.2	
					r=2		0.85	
							0.45	
							r=21	
Waypoint								
152								
37.07517								
118.91678	2205	54	-90	2(1)	2	165	0.6	r=5
		60		>10 (F1)(100	90,88	0.15	
		51		> 10 (V1)	75	250	0.1	
		48		4.5 (V2)	200	180	0.1	
		62		>5 (V3)	25	220	0.1	
		51			r=2	r=9	0.3	
		56					2.1	
		43					0.3	
		54					2.4	
		58					1.2	
		48					1	
		52					1.5	
		53					0.9	
		60					0.3	
		46					0.2	
		59					0.75	1
		53.4					0.3	1
							r=15	1
								1
								1
								1
								1
L	1	1		1	1	1	I	

Waypoint								
153								
37.07484								
118.91695	2231	54	-45	>4 (1)	1	350,80	1.2	r=6
		62		1 (2)	10	80,90		
		41		1.5 (F1)	1	210	1.5	
		53		2 (F2)	3	50	0.2	
		60		2.5 (F3)	20	155		
		54		`	20	r=9		
		42			0.5		0.6	
		63			0.5		0.5	
		55			1		1	
		46			20		0.9	
		64			10		0.84	
		44			7.91		0.9	
		62			3		r=21	
		56			r=5			
		60						
		56						
		66						
		55.2						
Waypoint								
154								
37.08761								
118.87350	2410	50	-90	1(1)	face	60,86	0.75	r=5
		60		4.5 (2)	200	280	1	
		53		4.5 (Flak	75	200	1.4	
		60		+	.1	200,90	3	
		50		2 (Flake	3	15	2.5	
		58		·	69.75	r=9	1.2	
		63			39		1.64	
		58			r=2		1.4	
		44					r=28	
		60						
		52						
		53						
		60						
		61						
		61			İ			

	1	50	I		I			
		50						
		52						
		55.6						
Waypoint								
155								
37.08686								
118.87364	2459	70(P)	-90	1.75 (1)	1	215	0.45	r=6
		70		>5 (2)	1	220	0.45	
		70		1 (3)	2	245	0.3	
		72		>5 (V1)	1000	210	0.6	
		68			251	r=14	0.45	
		62			1.5		0.45	
		65			r=5		r=21	
		64						
		70						
		71						
		69						
		64						
		64						
		66						
		62						
		62						
		64						
		66.6						
		00.0						
Waypoint								
156								
37.08634								
118.87386	2478	55	-90	5-7 (Set 1	1		0.75	r=6
		45		5 (2)	X	10,67 (19		
		60		1.5 (3)	150	175,80	1.5	
		52		1.5 (4)	100	245,64	0.3	
		46		1 (5)	1	200	0.45	
		58		1.5 (6)	na	240	0.9	
		59		0.2 (7)	na	185	0.15	
		60		4.5 (V1)	180	240	0.45	
		65			r=4	r=14	1.5	
		71					0.2	
		60					3	

		_						
		69					0.3	
		72					0.6	
		70					5	
		63					1.2	
		61					0.3	
		68					1.8	
		60.8					3	
							1.26	
							0.83	
							r=21	
Waypoint 157								
37.08514								
118.87444	2503	64	-45	4(1)	1	115	1.8	r=6
		58		1.5 (2)	0.5	205	1.5	
		56		1.5 (3)	na	175	0.6	
		74		3 (4)	na	245	0.6	
		66		7 (V1)	305	305	0.6	
		52		0.5 (V2)	75	200	4.5	
		46			r=6	r=20	1.5	
		70					1.8	
		66					0.3	
		62					1.2	
		49					1.44	
		56					1.35	
		56					r=28	
		62						
		58						
		70						
		58						
		60.2						
				1				
				1				
				1				
	†	1						
L	1	<u> </u>	<u> </u>	ı	I			

Waypoint						Τ		
158								
37.08435								
118.87475	2536	42	-90	>4 (1)	20	200	1-3m	r=6
		60		> 4 (2)	10	95,90	r=28	
		58		1 (3)	0.01	150		
		48		5 (4)	0.5	95		
		59		,	30	r=18		
		54			15			
		55			12.59			
		58			12.5			
		56			r=5			
		54						
		53						
		44						
		57						
		56						
		56						
		53						
		58						
		54.2						
Waypoint 159 (K6)								
37.08803						†		
118.87320	2453	60	-90	>4 (Flake	75	115	0.15	r=5
		52		2.5 (Flak		145	0.1	
		44		1 (Flake	10	65	0.2	
		58		1.5 (1)	50	240,86	0.3	
		66		1 (2)	50	115,90	0.3	
		56		1.3 (3)	25	125,90	0.15	
		46		1 (4)	15	195,75	0.3	
		65			100	r=14	0.25	
		60			60		0.2	
		58			20		0.25	
		50			10		0.4	
		58			60		0.01	
		62			r=2		0.9	
		55					0.75	
		48					0.30	

		60					0.25	
		57					r=15	
		56.2						
Waypoint								
160								
37.08861								
118.87283	2464	59	-90	3-4 (Set 1	10	20	0.3	r=6
		62		>3.5 (2)	10	285,90	0.4	
		47		2 (Flake	2	315	0.2	
		58		(200	r=9	4.5	
		61			100		1.7	
		64			200		2.4	
		56	1		50		1	
		49			81.714		1.5	
		54			50		1	1
		60			r=2		r=28	1
		51			,-2		7-20	
		57						
		46						
		56						
		56						
		63						
	1	60						1
		56.4						
		50.4						
XX : - 4								
Waypoint 161								
37.08941								
	2483	<i>5 5</i>	00	10 (Cat	20	200.96	0.2	
118.87242	2483	55	-90	>10 (Set		200,86	0.3	r=6
		52		2.5 (Set 2		100,86	0.6	
		63		0.4 (3)	3	330	0.3	
		48	-		50	r=14	0.8	
		52	-		100		0.3	
		54			10		0.45	
		50			10		0.3	
		55			10		0.9	
		50			200		1.2	
		50			100		0.2	
		54			60		0.15	

		52			5		0.3	
		56			3		0.45	+
		56			1		0.43	+
		60			2		0.3	+
							_	+
		58			10		1.2	
		55			100		1.5	
		54.1			48.47		2	_
					10		0.65	
					r=4		0.45	_
							r=21	
Waypoint 162								
37.09029								
118.87216	2515	63	-90	~3 (1)	na	15	>3m	r=6
		70		>3.5 (V1)	150	345	r=30	
		58		3 (V2)	40	260		1
		71			r=7	r=20		
		68						1
		64						1
		61						1
		70						1
		68						1
		64						1
		64						1
		72						
		74						
		72						1
		72						1
		68						1
		74						1
		63						1
								1
								1
								1
								1
								+
						1		+
				<u> </u>	l			

Waypoint								
163								
37.09109							1	
118.87156	2541	49	-90	>10 (1)	10	185,84	1-3m	r=6
110101100	25 11	60	70	1.5 (Flak	1	70	r=28	
		58			20	50	. 20	
		55		1 (Flake	1	50		
		55		>15 (V1)		355	1	
		56		710 (11)	r=4	r=18		
		44				7 20	1	
		62						
		64						
		58						
		48			1		1	
		60						
		56		1		1	1	
		56						
		48						
		55						
		54						
		55.2						
Waypoint								
164 (K7)								
37.10564								
118.89648	2451	52	-90	3 (1)	75	155,80	1-3m	r=5
		52		4(2)	75	230	r=21	
		59		1.8 (3)	100	120,75		
		54		>4 (4)	50	260		
		58		>3 (5)	100	240,90		
		56		1 (6)	100	280,86		
		64		1.5 (7)	100	275,90		
		62		1.5 (8)	250	250,90		
		50		1.5 (9)	250	335,65		
		55		, ,	r=2	r=14		
		50						
		58						
	1	62						
		02						
		54						

		52						
		60						
		56.4						
Waypoint								
165								
37.10569								
118.89684	2472	60	-90	1 (V1)	130	275	0.2	r=5
		52		>3 (Set 1	180	275	0.3	
		48		0.5 (Set 2	50	345,80	0.2	
		58		4 (3)	25	260,90	0.6	
		51			r=2	r=14	0.15	
		56					0.15	
		52					0.45	
		56					1.2	
		61					0.9	
		62					1.5	
		56					0.6	
		50					0.5	
		50					0.6	
		60					0.45	
		54					0.5	
		62					0.6	
		62					0.3	
		55.9					0.6	
							0.54	
							0.5	
							r=21	

Deadman (Canyon	1						
Waypoint								
114 (D5)								
				Joint	Joint	Spacing		
	Elev.			length	width	of joints	Joint strike	
Lat/Long	(m)	SH	Alpha	(m)	(mm)	(m)	and dip	Continuity
36.68356								
118.57772	2404	35	-90	2(1)	10	0.30	320 (?), 52	r=5
		45		1.2(2)	9	0.50	330,60	
		36		0.6(3)	10	0.60	320,75	
		48		1 (4)	2	1.00	175	
		30		1 (5)	3	0.60	170	
		38		2.5 (6)	2	0.55	175	
		44		0.3 (7)	2.5	r=21	310,85	
		60		0.6(8)	1		330	
		42		1.5 (9)	3		330,75	
		58		2 (10)	2.5		155	
		52		3 (11)	18		340,80	
				> 1.5				
		37		(12)	3		200,50	
		11		0.5 (12)	1.5		0	
		44		0.5 (13)	1.5		r=9	
		46		0.5 (14)	1			
		56		, ,	4.89			
		34			2.75			
		52			r=2			
		45						
Waypoint 115								
							1	
36.68367	2400	26	00	2 (1)	1	0.20	200.95	
118.57719	2488	36 42	-90	3 (1)	1	0.20	300,85	r=6
				1.8 (2)	na	1.00	160	
		42		2 (3)	na	1.20	220	
		50		1 (4)	na	0.30	140	
		46		3.5 (5)	face	0.50	325,10	
				> 4 (6) (Set)				
		66		2.5 & 2	2.25	0.15	220.70	
		66		2.3 & Z	2.23	0.13	220,70	

	1	l	I	1 (7)	ı		T	I
				1 (7)				
				(Set)				
		43		All 1m.		0.40	130	
		48		1.5 (8)	2.5	r=21	230	
		49		4 (9)	5		350	
		60			2.55		r=20	
		40			2.25			
		52			r=6			
		44						
		62						
		38						
		48						
		44						
		48						
Waypoint								
116								
36.68356				3.5 (Set				
118.57685	2499	42	-45	1)	2-0.1	0.76	75,5	r=6
				3 (Set			, .	
		60		2)	0.2-0.1	0.15	130,35	
				1.5 (Set	0.2 0.1	0.10	100,00	
		45		3)	0.4-0.1	0.20	90,70	
		43		2)	0.86	0.07	r=14	
		61			r=4	0.60	1	
		62			-	1.20	1	
		62				0.02	1	
		44				0.20		
		43				r=21		
		38				. –21		
		48				 		
		39						
		45						
					-			
		1/16					1	I
		46						
		41						
		41 48						
		41 48 30						
		41 48						

Waypoint								
117 (D1)								
36.64120								
118.58739	2693	46	-90	2(1)	5	1.40	200	r=5
110.00703	2075	34	70	4(2)	10	0.50	175	1-0
		31		1 (3)	10	0.50	175	
		40		(Set)	12	0.10	285,85	
		44		3.5 (4)	5	0.15	185	
				(1)	top	0.10	100	
		35		> 5 (5)	edge	0.30	170	
		52		(-)	8	0.60	r=9	
		40			7.5	1.80		
		54			r=5	0.69		
		46				0.50		
		42				r=21		
		50						
		62						
		52						
		41						
		43						
		55						
		38						
		46						
Waypoint								
118								
36.64114				2-2.5				
118.58816	2724	42	-90	(Set 1)	4	1.80	195	r=6
				1 (Set				
		46		2)	3	0.30	120,20	
		53		3 (3)	5	0.70	155	
		43		4 (4)	4	2.50	25	
				1-1.5				
		37		(5) (Set)	2	1.00	90,15	
				152				
		34		(6)	1	0.10	25,10	
		43		2 (7)	2	0.60	235	
		32		1 (8)	1	0.02	315	
		43			2.75	0.15	r=9	

			1	1	r	T	
		52			2.5	0.20	
		56			r=5	0.45	
		42				r=21	
		40					
		54					
		50					
		43					
		41					
		44					
Waypoint							
119				> 1 (C-4			
36.64113	2754	24	00	> 4 (Set		0.25	Striles into E
118.5887	2754	34	-90	1)	1	0.25	Strike into f r=6
		10		0.6 (Set		0.20	20
	+	42		2)	4	0.30	20
					1 for		
				5 (8	most.		
				> 5 (Set			
		41		3)	largest.	0.60	280,65
				0.5-1			
		39		(Set 4)	na	0.30	05, dip into face
		50			r=2	0.90	r=14
		34				0.60	
		33				0.45	
		45				r=21	
		37					
		45					
		50					
		36					
		34					
		52					
		44					
		41					
		40					
		41					
		43					
•	•	•	•	•		•	

Waypoint 120 (D2)								
36.66020				3.5 (Set				
118.58072	2672	35	-90	1)	2-4 cm	0.60	270,65	
				> 4 (Set				
		62		2)	15	0.05	45	r=6
		50			r=4	0.30	r=14	
		61				0.20		
		46				1.20		
		44				0.50		
		48				0.90		
		50				0.50		
		58				r=21		
		46						
		48						
		50						
		54						
		57						
		54						
		54						
		54						
		51						
Waypoint 121								
36.66047				1.8 (Set				
118.58121	2695	51	-90	1)	4	0.30	320,80	r=5
		45		2.5 (2)	5	0.20	190	
		53		1 (3)	1	0.90	270	
		52		2 (4)	3.5	0.15	300,55	
		58			r=2	0.60	r=14	
		42				0.30		
		49				r=21		
		42						
		44						
		54						
		48						
		57						
		47						
		48						

	T	T .	r	ı	1	1	
	53						
	44						
	50						
			No				
2640	69(D)	15		r-7	r-30	r-20	r=7
2040	. ,	-43	9	/ - /	1-30	1-20	1-7
			U				
	68						
	62						
	66						
	69						
	68						
	68						
	67						
	-						
	UI.						
2665	(0/P)	4.5	. 4 (1)	2.5	1 20	0.10	
2665		-45					r=5
						5,15	
	66			na			
	68		3.5 (7)	2	r=21		
	64		3 (8)	2		7	
	0 1		0 (0)			<u> </u>	
	2640	44 50 50 50 66 66 66 65 55 66 68 68 68 68 68 67 58 68 68 67 58 68 67 58 68 67 58 68 67 58 68 67 58 68 67 55 66 68 65 55 66 66 66 66 66 65 55 66	53 44 50 50 50 50 50 50 50	53	53 44 50 50 50 50 50 50 50	53	53

		62		2.5 (10)	2		6	
		66		1 (11)	na		160	
		69		2 (12)	na		160	
		68		, ,	r=5		r=14	
		68						
		67						
		58						
		68						
		61						
Waypoint 124								
36.66010								
118.57553	2725	58	-90	2(1)	1	0.30	120,30	r=6
		52		3.5 (2)	1.5	0.90	100,35	
		60		3 (3)	1	1.50	200	
		57		>4 (4)	1	0.25	200	
		56		>4 (5)	2	0.30	245	
					12.5			
		64		3.5 (6)	(flake)	0.15	140	
		58		1.5 (7)	1.5	0.80	140	
		58		1 (8)	2.5	2.00	265	
		60		>4 (9)	15	0.55	175,25	
		64		>5 (10)	10	r=21	250	
		58		1.5 (11)	1		140,20	
		53		1.5 (12)			200	
		59			2		200	
	†	59		>4 (14)	2		260	
	†	66		(11)	3		r=14	
		66			r=5		-	†
		62						†
		59						†
	†							†
	†							†
								1

Waypoint								
125 (D4)								
36.6819				1.5-2.5				
118.57624	2515	43	-90	(Set 1)	9	0.60	60,50	r=6
				1-1.5				
		60		(Set 2)	0.5	1.20	300,80	
				0.3 (Set				
		47		3)	7.5	0.30	45	
				1.5 (Set				
		44		4)	15	1.50	60,75	
		41		2.5 (5)	10	0.25	30,65	
		52		0.6 (6)	7.5	0.60	120	
		44			r=4	r=21	r=18	
		44						
		48						
		54						
		48						
		50						
		47						
		48						
		50						
		50						
		50						
		48						
Waypoint 126								
36.68018				>4 (Set				
118.57571	2549	54 (P)	-90	1)	15-20	0.60	77	r=5
		62		1 (2)	1	0.25	140	
		64		>2 (3)	1	1.20	135	
		62		2 (4)	9	0.30	140	
		64		>5 (5)	7	1.80	140	
				~ 5				
				(Flake				
		52		1)	13	0.60	See Photos.	
		68		ĺ	6.2	r=21	r=14	
		66			7			
		68			r=5			
		56				1		1

		1.5						
		65						
		62						
		70						
		66						
		66						
		65						
		64						
		57						
Waypoint 127								
36.68022				0.4-0.5				
118.57536	2579	70	-90	(Set 1)	13	1.00	55	r=5
				3-3.5	10 &			
		66		(Set 2)	na	0.60	325,20	
				3 (Set				
		58		3)	1 to 2	1.50	135,30	
		64		2 (4)	2.5	0.90	65,20	
		74		4 (5)	7	0.95	130,80	
		68		2 (6)	20	r=21	60,70	
		63		>4 (7)	4		320	
		56		0.5 (8)	face		70,40	
		58			r=4		r=18	
		63						
		64						
		67						
		64						
		58						
		68						
		69						
		65						
		64						