

Effect of the axial jet on the optimal response in Batchelor vortex

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Introduction

Wing-tip vortices are circular patterns of rotating air left behind a wing as it generates lift.

Instabilities:

Non-modal stability analysis ($t \sim 0$)

- Response to initial conditions (Optimal perturbation)
- Transient growth (Mao2012)

- Response to external forcing (**Optimal response**)

Time-harmonic forcing (Guo2011)

Stochastic forcing (Fontane2008)

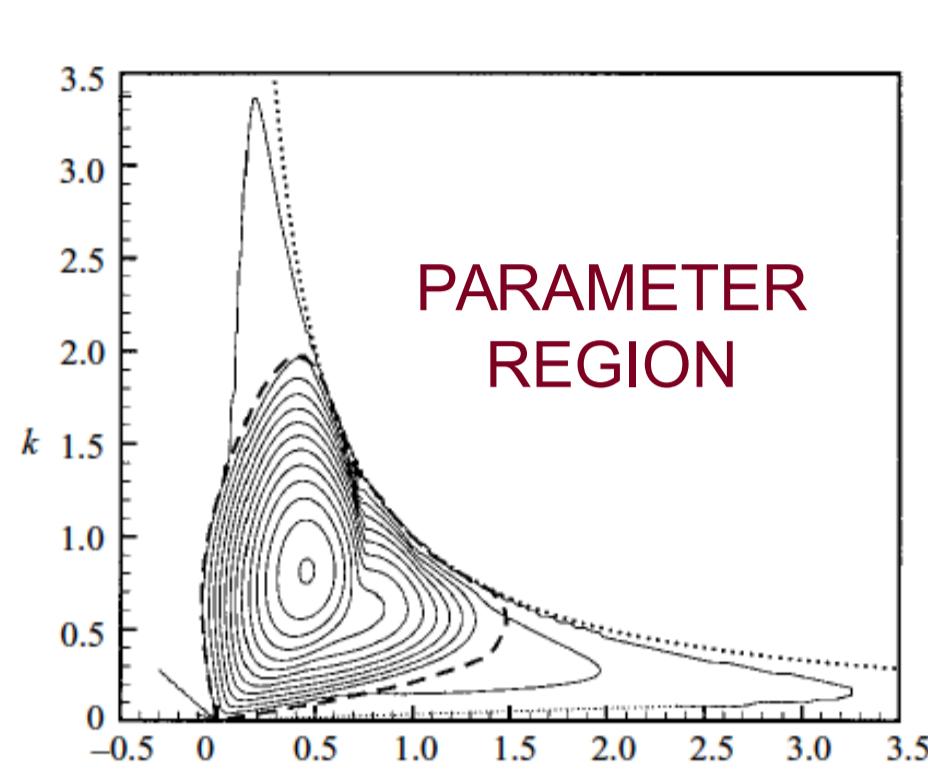
Normal mode stability analysis ($t \sim \infty$)

- Strong inviscid helical instability (Heaton2007)

- Weak viscous instabilities (Khorrami1991)

- Weak viscous centre instabilities (Fabre2004)

- Cooperative instability (Hattori2009)



Applications: → **Aeronautics:** Optimization of airport traffic decreasing the current spacing between aircrafts in complete safety

→ **Wind energy:** Increase the performance in wind farms of turbines since the functionality of one rotor depends on the incident flow given by the precedent one

Objective: Characterize numerically the response of a time-harmonically force in LNS with a Batchelor vortex as a base flow

Why?

Because the Batchelor vortex is widely adopted in aeronautics

Study the effect of swirl parameter q on the optimal response

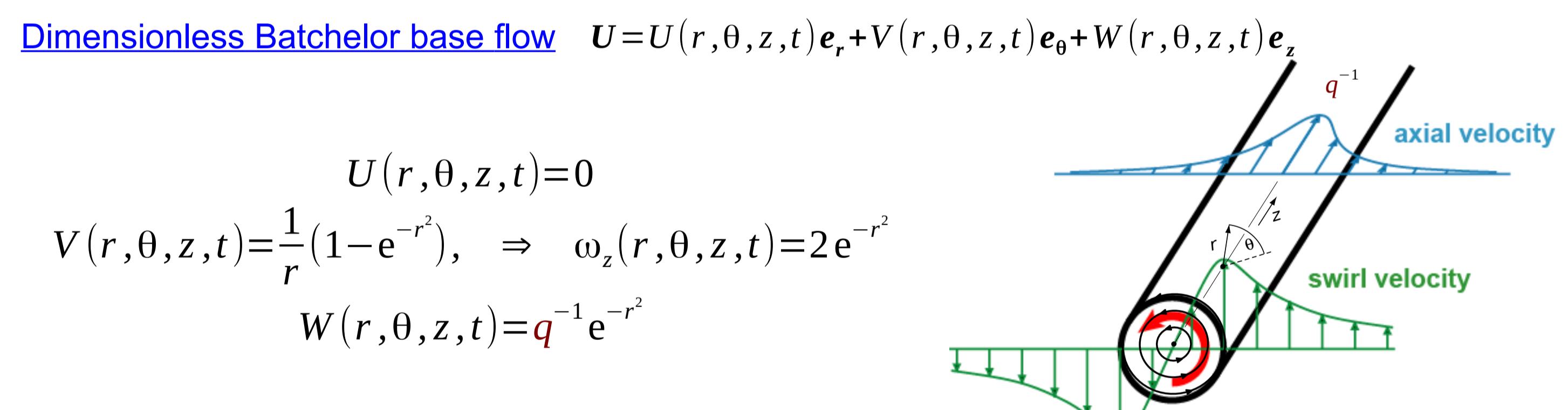
THUS Numerical validation (DNS) of the theoretical response and flow structures using a spectral Fourier-based numerical method

[Mao2012] X. Mao and S.J. Sherwin, **697**, *J. Fluid Mech.*, (2012) [Guo2011] Z.-W Guo and D.-J. Sun, **375**, *Phys. Letters A*, (2011) [Fontane2008] Fontane et al., **613**, *J. Fluid Mech.*, (2008) [Heaton2007] C.J. Heaton, **576**, *J. Fluid Mech.*, (2007) [Khorrami1991] M.R. Khorrami, **225**, *J. Fluid Mech.*, (1991) [Fabre2004] D. Fabre and L. Jacquin, **500**, *J. Fluid Mech.*, (2004) [Hattori2009] Y. Hattori and Y. Fukumoto, **21**, *Phys. Fluids*, (2009)

Governing equations. Stability analysis

Incompressible forced Navier-Stokes equations $\mathbf{u} = u(r, \theta, z, t)\mathbf{e}_r + v(r, \theta, z, t)\mathbf{e}_\theta + w(r, \theta, z, t)\mathbf{e}_z$

$$\partial_t \mathbf{u} = -(\mathbf{u} \cdot \nabla) \mathbf{u} - \nabla p + \frac{1}{Re} \nabla^2 \mathbf{u} + \mathbf{f} e^{i\omega t}, \quad \nabla \cdot \mathbf{u} = 0$$



Linearized Navier-Stokes equations $\mathbf{u}' = \mathbf{U} + \mathbf{u}'$

$$\partial_t \mathbf{u}' = -(\mathbf{U} \cdot \nabla) \mathbf{u}' - (\mathbf{u}' \cdot \nabla) \mathbf{U} - \nabla p' + \frac{1}{Re} \nabla^2 \mathbf{u}' + \mathbf{f} e^{i\omega t}, \quad \nabla \cdot \mathbf{u}' = 0$$

Perturbation ansatz

$$(\mathbf{u}', p') = (u', v', w', p') = [u'(r, t), v'(r, t), w'(r, t), p'(r, t)] e^{ikz + i\omega t} \quad k \in \mathbb{R}, \quad n \in \mathbb{N}$$

Optimal response analysis

Evolution equation $\dot{\delta} = [u'(r, t), v'(r, t)]$

$$\partial_t [\mathbf{L}] \delta = ([M] + \frac{1}{Re} [N]) \delta + [H]^A \mathbf{f} e^{i\omega t}, \quad \mathbf{u}' = [H] \delta, \quad [H] = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ \frac{i}{k} \left(\frac{d}{dr} + \frac{1}{r} \right) & -m \frac{k}{r} \end{bmatrix}$$

$$\partial_t \delta = [A] \delta + [B] \mathbf{f} e^{i\omega t}, \quad \delta(t=0) = \delta_0$$

Eigenvalue decomposition $\delta \sim e^{\lambda t}$

$$[A] = [Q][\lambda][Q]^{-1}, \quad \Re(\lambda) < 0 \Rightarrow \text{Normal-mode STABLE}$$

General solution

$$\mathbf{u}'_{out} = [H](\delta_h + \delta_p) = [H][Q]e^{[\lambda]t}[Q]^{-1}\delta_0 + [H][Q](i\omega - [\lambda])^{-1}[Q]^{-1}[B]\mathbf{f} e^{i\omega t}$$

Based-kinetic energy norm

Cholesky decomposition

$$2E = \|\delta\|_e^2 = \int_0^\infty (u'^2 + v'^2 + w'^2) r dr \approx \mathbf{u}'^T [W] \mathbf{u}' = \| [M] \mathbf{u}' \|_2^2 \Rightarrow [W] = [M]^A [M]$$

Optimal response

$$R(\omega) = \max_f \frac{\|\mathbf{u}'_{out}\|_e^2}{\|\mathbf{f} e^{i\omega t}\|_e^2} = \max_f \frac{\|[H](i\omega - [A])^{-1}[B][M]\|_2^2}{\|\mathbf{f} e^{i\omega t}\|_e^2} = \|[H](i\omega - [A])^{-1}[B]\|_e^2$$

Singular value decomposition

$$R(\omega; Re, q, m, k) = \|[M]^{-1}[H](i\omega - [A])^{-1}[B][M]\|_2^2 = \|[P]\|_2^2$$

$$R_{max}(\hat{\omega}; Re, q, n, k) = s_1$$

$$[P][V] = [S][U] \Rightarrow [P]v_1 = s_1 \mathbf{u}_1$$

$$\mathbf{f} = [M]^{-1} \mathbf{v}_1, \quad \mathbf{u}'_{out} = [M]^{-1} \mathbf{u}_1$$

DNS

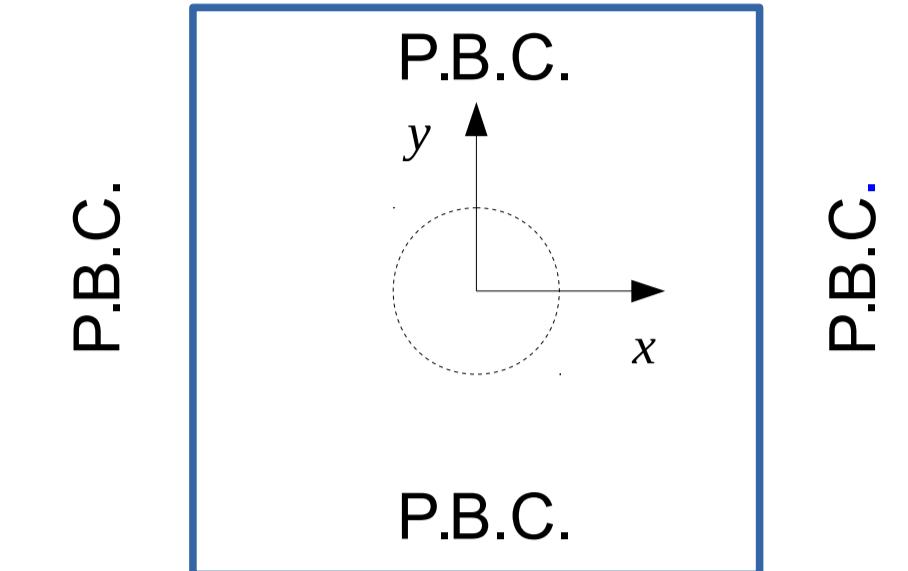
Base flow in cartesian coordinates

$$U = U_x(x, y, z, t)\mathbf{e}_x + U_y(x, y, z, t)\mathbf{e}_y + U_z(x, y, z, t)\mathbf{e}_z$$

$$U_x(x, y, z, t) = -\frac{y}{\sqrt{x^2 + y^2}} V(x, y, z, t), \quad U_y(x, y, z, t) = \frac{x}{\sqrt{x^2 + y^2}} V(x, y, z, t), \quad U_z(x, y, z, t) = q^{-1} e^{-(x^2 + y^2)}$$

Fourier spectral method $k = k_x \mathbf{e}_x + k_y \mathbf{e}_y + k_z \mathbf{e}_z$

$$\mathbf{u}(x, y, k_z, t) = \iint \hat{\mathbf{u}}(k_x, k_y, k_z, t) e^{i(k_x x + k_y y)} dk_x dk_y$$



Adams-Basforth time-integration scheme (Delbende1998)

$$\hat{\mathbf{u}}^{n+1} = e^{\frac{k^2 \delta t}{Re}} \hat{\mathbf{u}}^n + \frac{\delta t}{2} \left[3 e^{\frac{k^2 \delta t}{Re}} \mathbf{N}(\mathbf{u}^n, \mathbf{f}^n, S_{fringe}) + e^{\frac{2k^2 \delta t}{Re}} \mathbf{N}(\mathbf{u}^{n-1}, \mathbf{f}^{n-1}, S_{fringe}) \right]$$

Fringe region (Nordström1999)

$$S_{fringe}(r) = S_{max} \left[S \left| \frac{r - r_{start}}{\delta_{rise}} \right| - S \left| \frac{r - r_{end}}{\delta_{fall}} \right| \right],$$

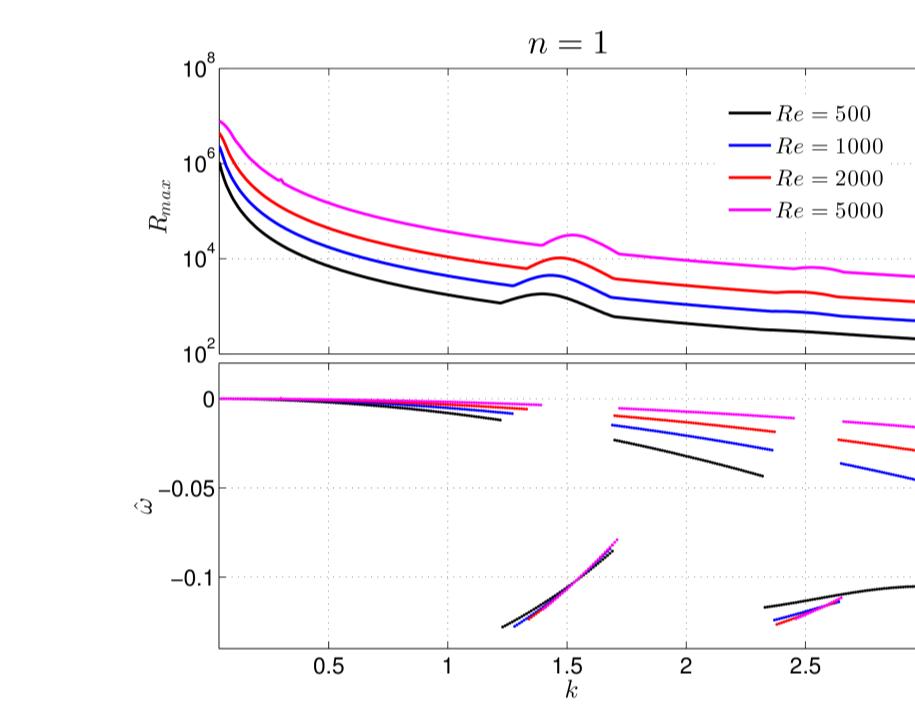
$$S(r) = \begin{cases} 0 & r \leq 0 \\ \frac{1}{1 + e^{\frac{1}{r - 1}}} & 0 < r < 1 \\ 1 & r \geq 1 \end{cases}$$

[Delbende1998] I. Delbende et al., **355**, *J. Fluid Mech.*, (1998)

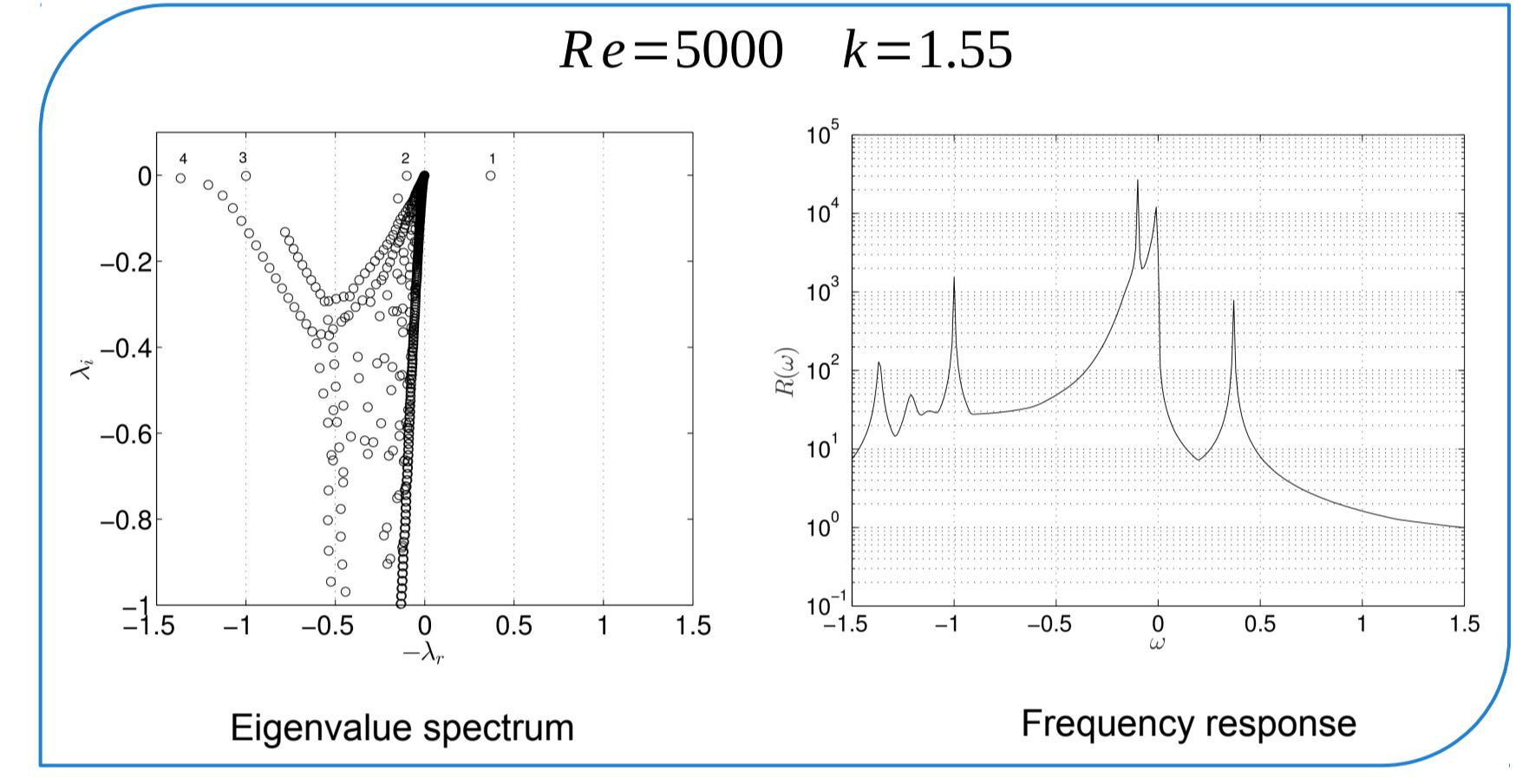
[Nordström1999] J. Nordström et al., **20**, *SIAM J. Sci. Comput.*, (1999)

Results

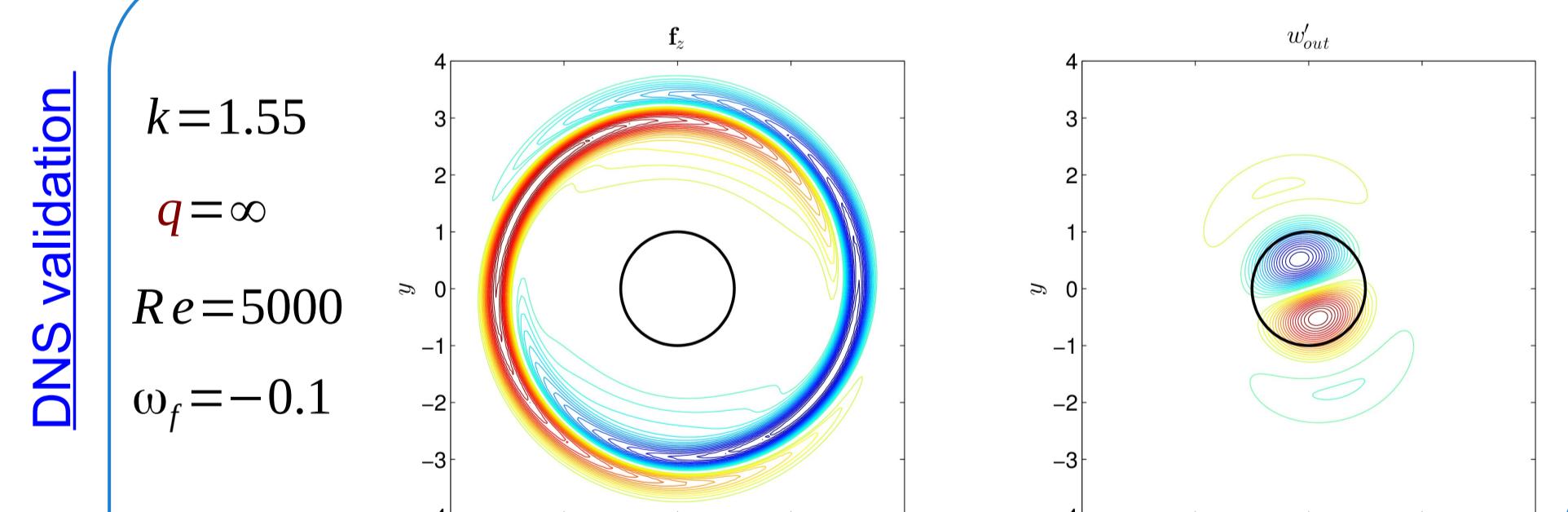
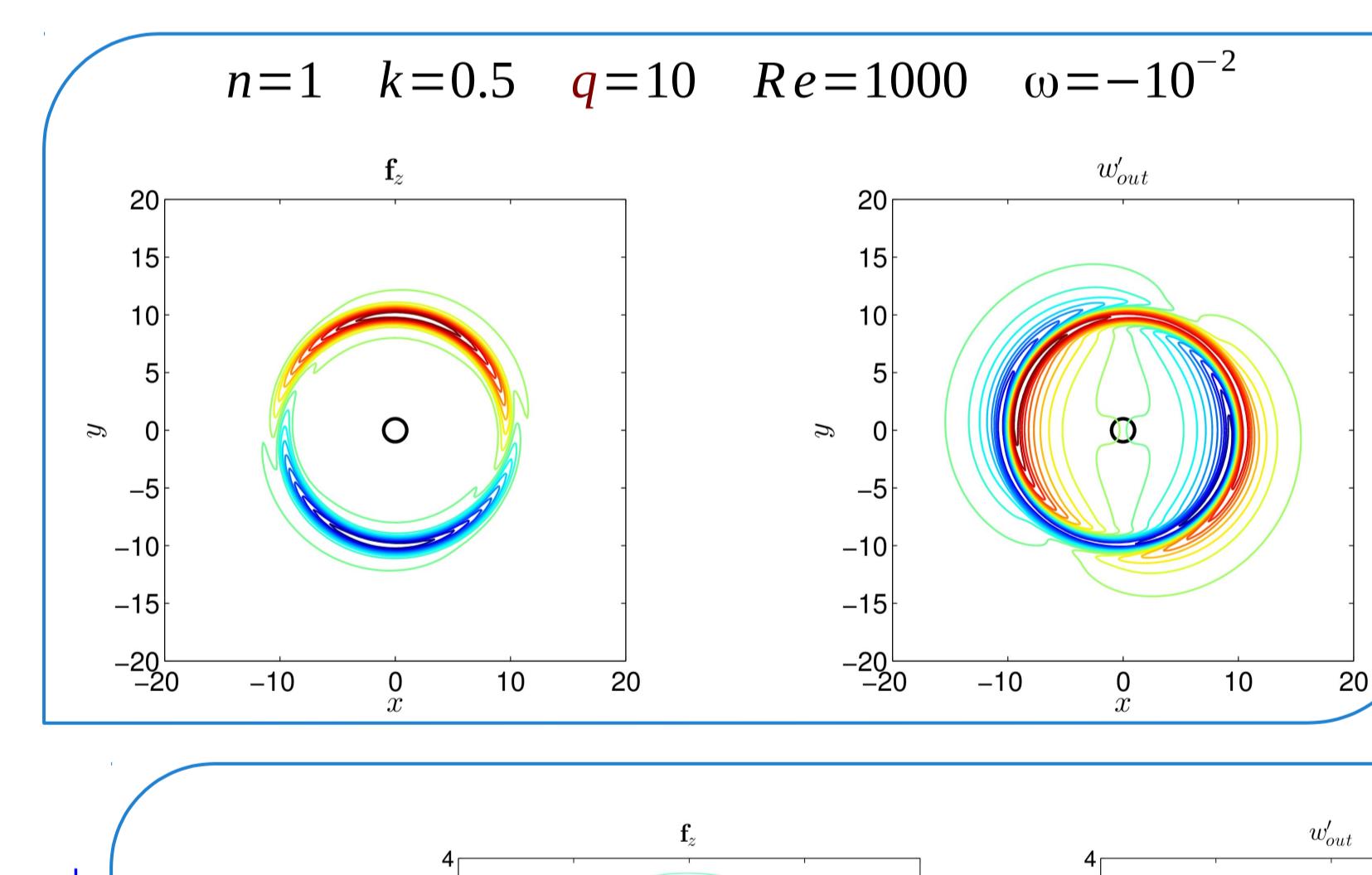
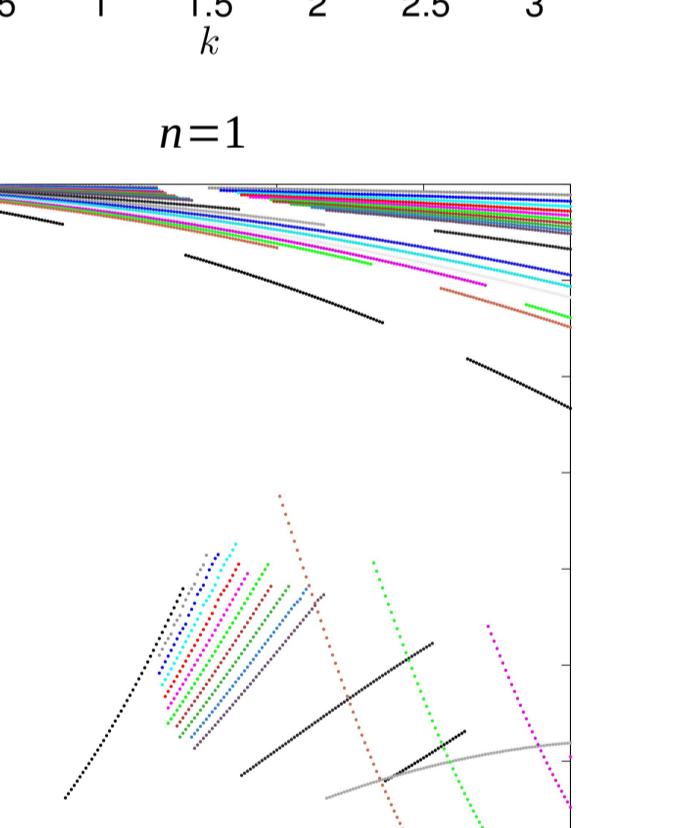
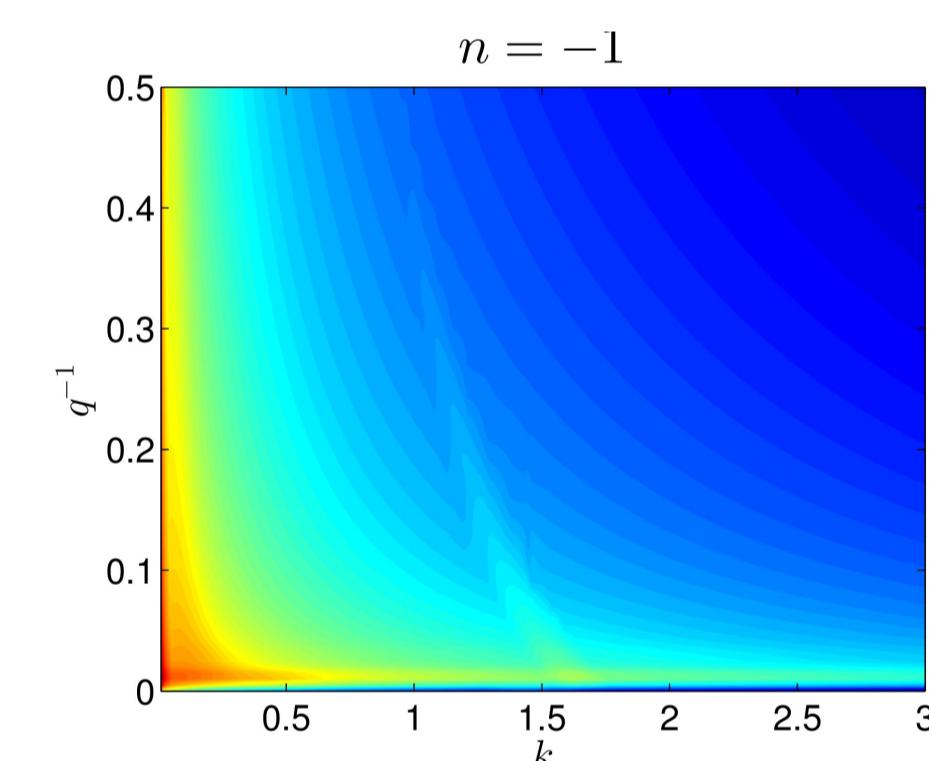
Lamb-Oseen vortex $n=1$



Re=5000 $k=1.55$



Batchelor vortex $Re=1000$



Conclusions and perspectives

- Effect of the axial flow on the optimal response of a Batchelor vortex has been investigated.
 - Lamb-Oseen vortex published results have been recovered.
 - Several integration parameter paths have been tested.
 - Axysimmetric and helical modes have been simulated for Batchelor vortices:
 - Axysymmetric:** Maximum gain does not depend on swirl parameter. Stationary optimal forcing.
 - Helical:** $q-k$ resonant gain maps have been built. Differents branches for $\hat{\omega}$ have been detected.
 - Optimal forcing structure is so complicated that it is not possible to reproduce experimentally. Understanding the mechanism will provide an insight of where to act.
- Spectral Fourier-based DNS method (Fringe region) validates the theoretical results.

Acknowledgments

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