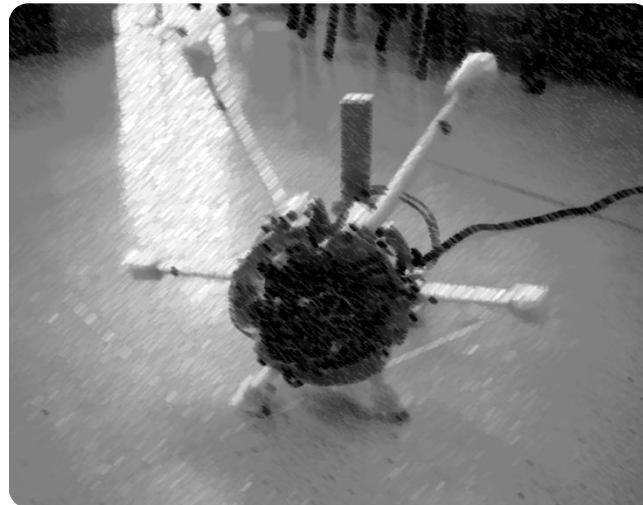




Design of a driving module for a hybrid locomotion robot

J. J. CASTILLO, J. A. CABRERA, M. JAIMEZ, F. VIDAL AND A. SIMÓN.

DEPARTMENT OF MECHANICAL ENGINEERING. UNIVERSITY OF MÁLAGA.





Script



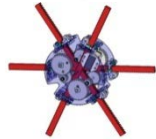
I. Introduction



Script



I. Introduction



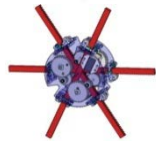
II. Mechanical Design



Script



I. Introduction



II. Mechanical Design

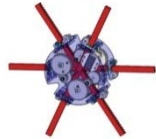


III. Electronics and Sensing

Script



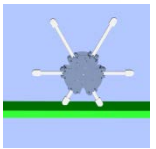
I. Introduction



II. Mechanical Design



III. Electronics and Sensing

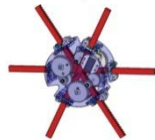


IV. Module Modeling

Script



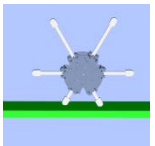
I. Introduction



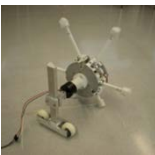
II. Mechanical Design



III. Electronics and Sensing



IV. Module Modeling

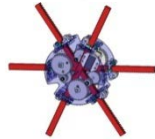


V. **Experimental Results**

Script



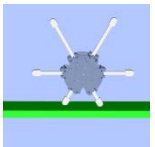
I. Introduction



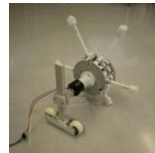
II. Mechanical Design



III. Electronics and Sensing



IV. Module Modeling



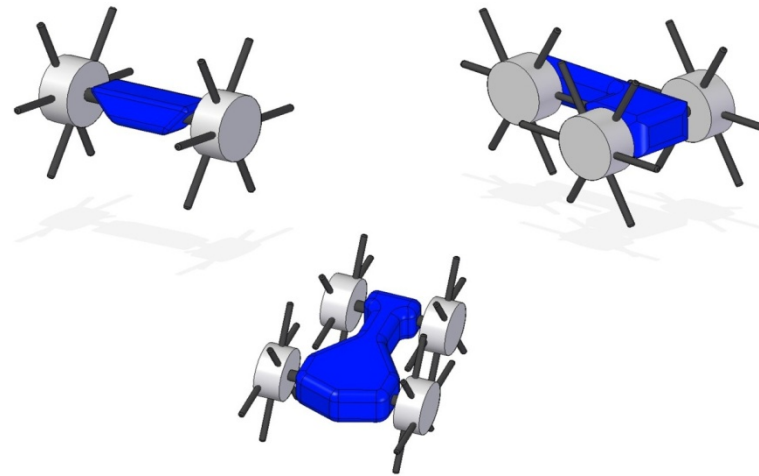
V. Experimental Results



VI. Conclusions



Introduction





Introduction

Robotics challenges

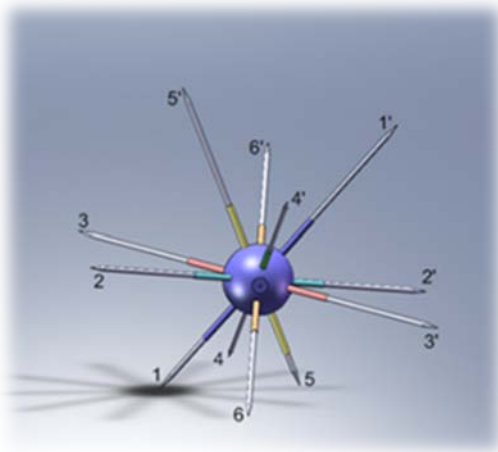
- ❖ Energy autonomy
- ❖ Computational capability
- ❖ Artificial intelligence
- ❖ Sensing capabilities
- ❖ Locomotion systems

Mobile robotics

Introduction

Evolution

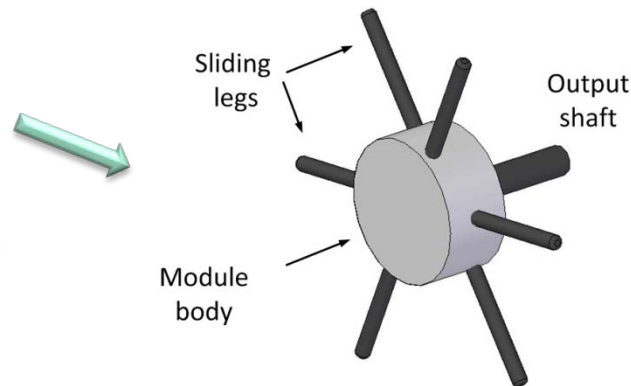
Inspiration



Spherical robot with sliding legs

V. Gheorghe et al
(2008)

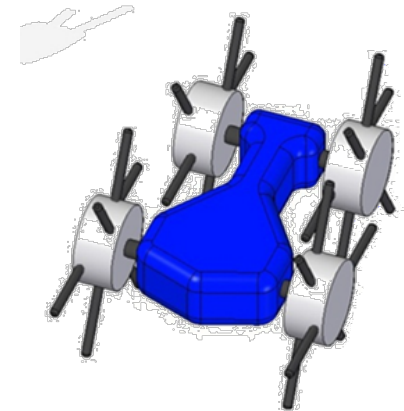
Adaptation



Cilindrical module with sliding legs

Castillo et al ?
(2014)

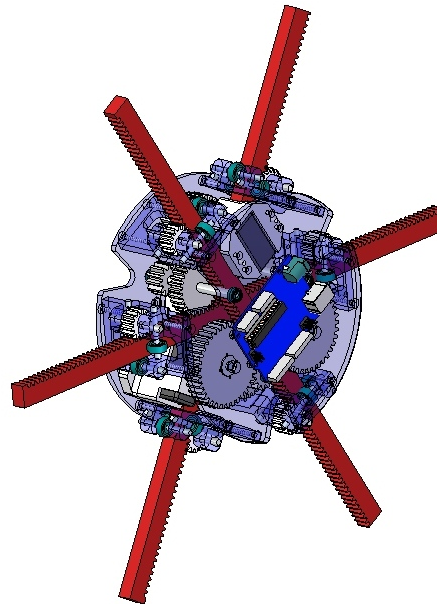
Objetive



Robot with sliding legs modules



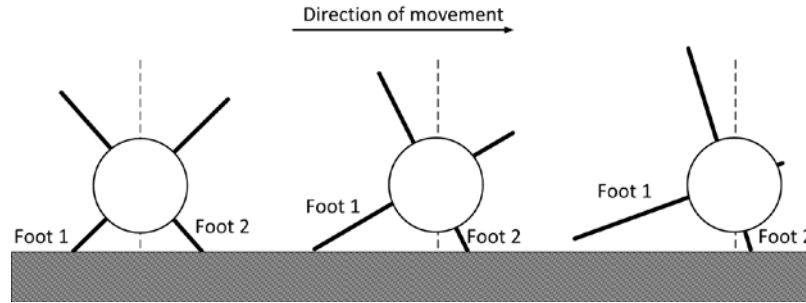
Mechanical Design



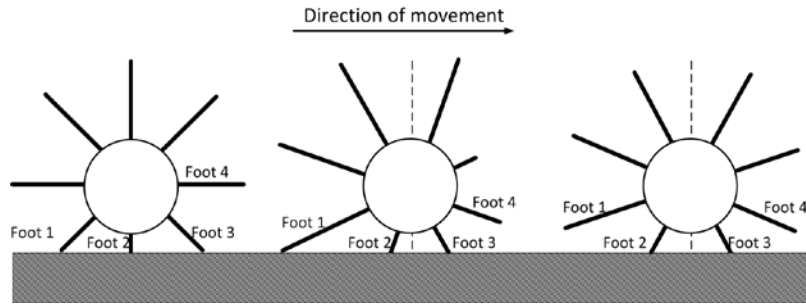


Mechanical Design

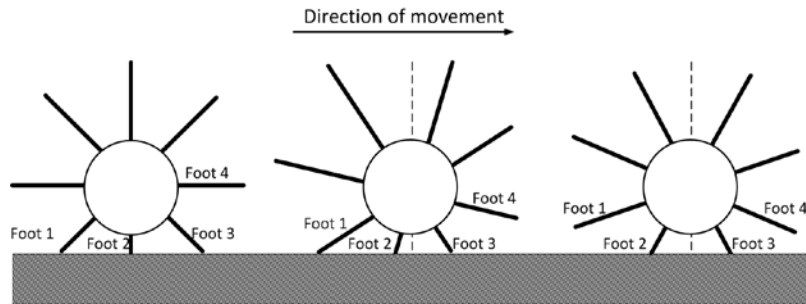
4 Feet



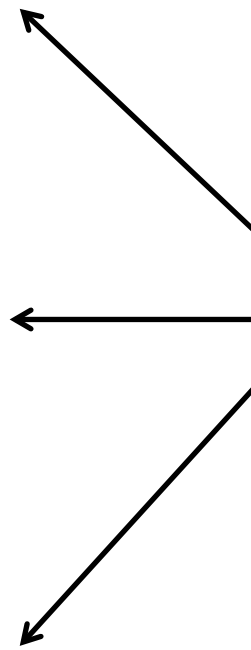
6 Feet



8 Feet

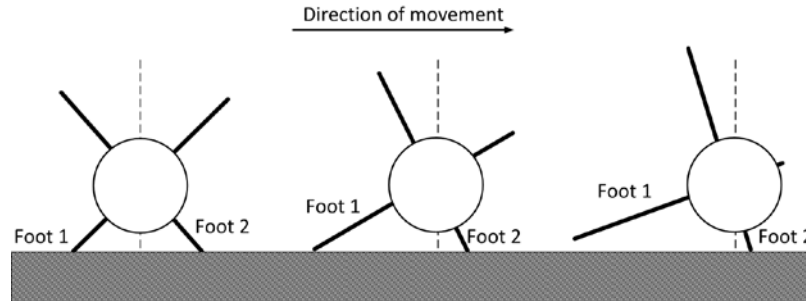


Triple support required

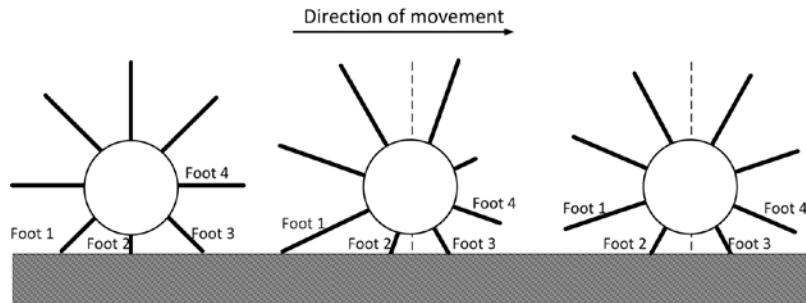


Mechanical Design

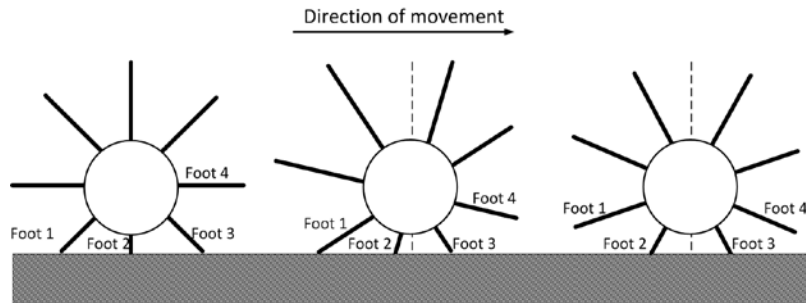
4 Foot




6 Feet



8 Feet

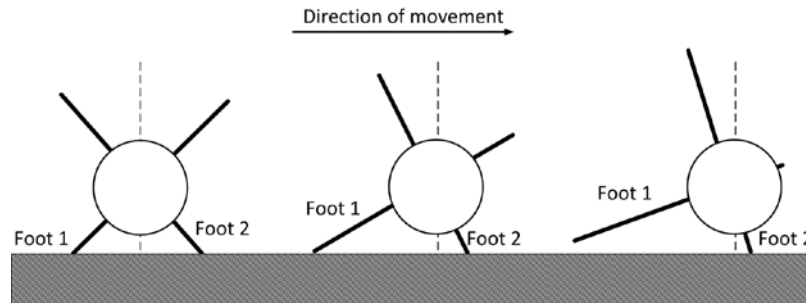


 Complete rotation not possible

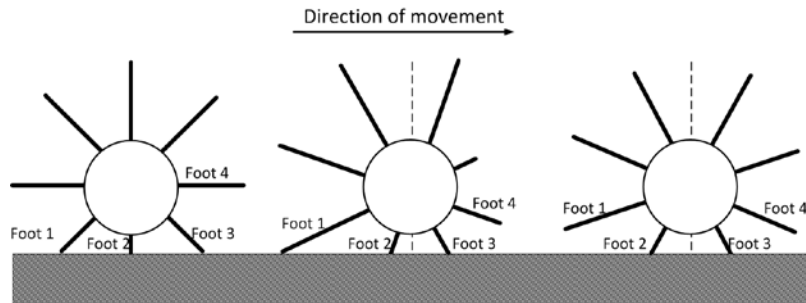
Triple support required

Mechanical Design

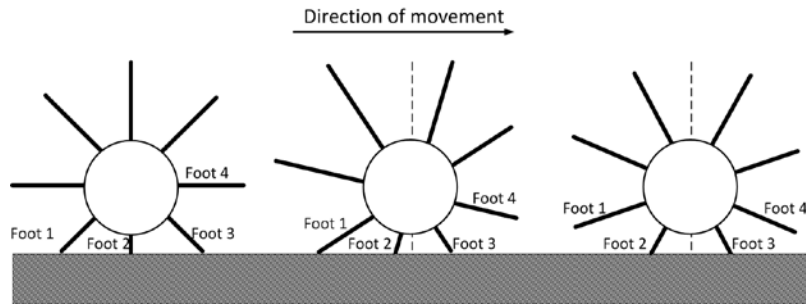
4 Foot



6 Feet



8 Feet



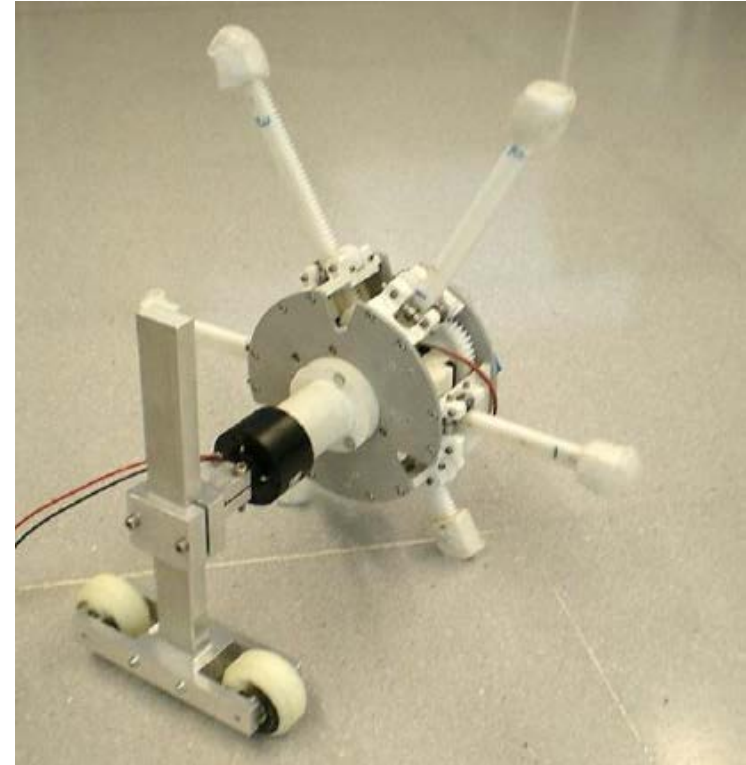
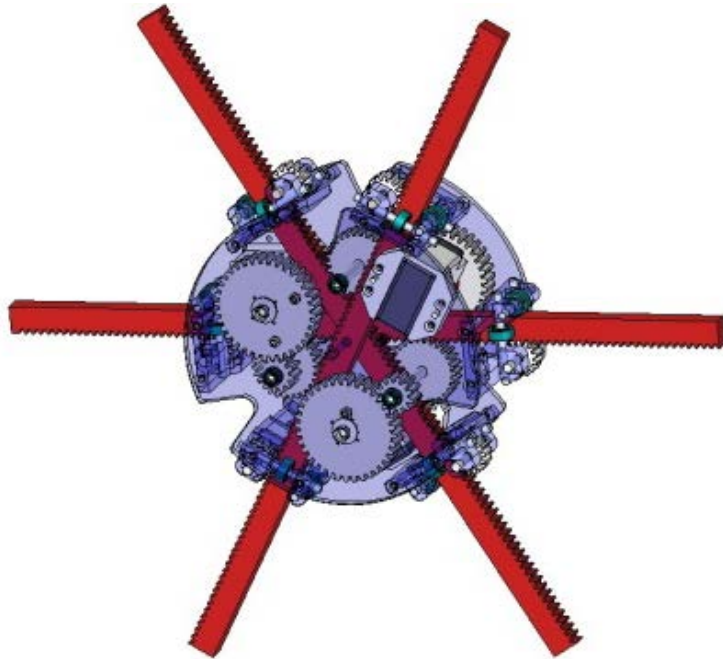
Complete rotation not possible

Triple support required

Complex



Mechanical Design



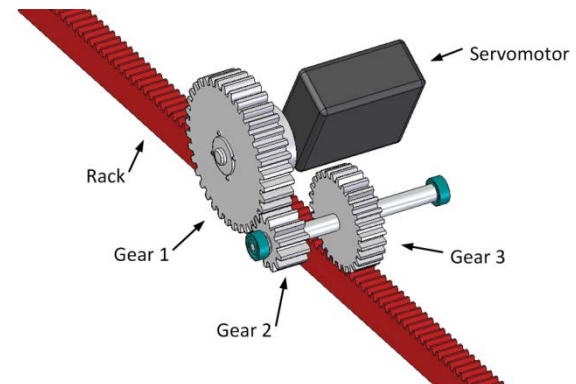
Servomotors

Mass – 60 grams
Maximum Torque – 16 kg cm
Maximum speed – 333°/ s

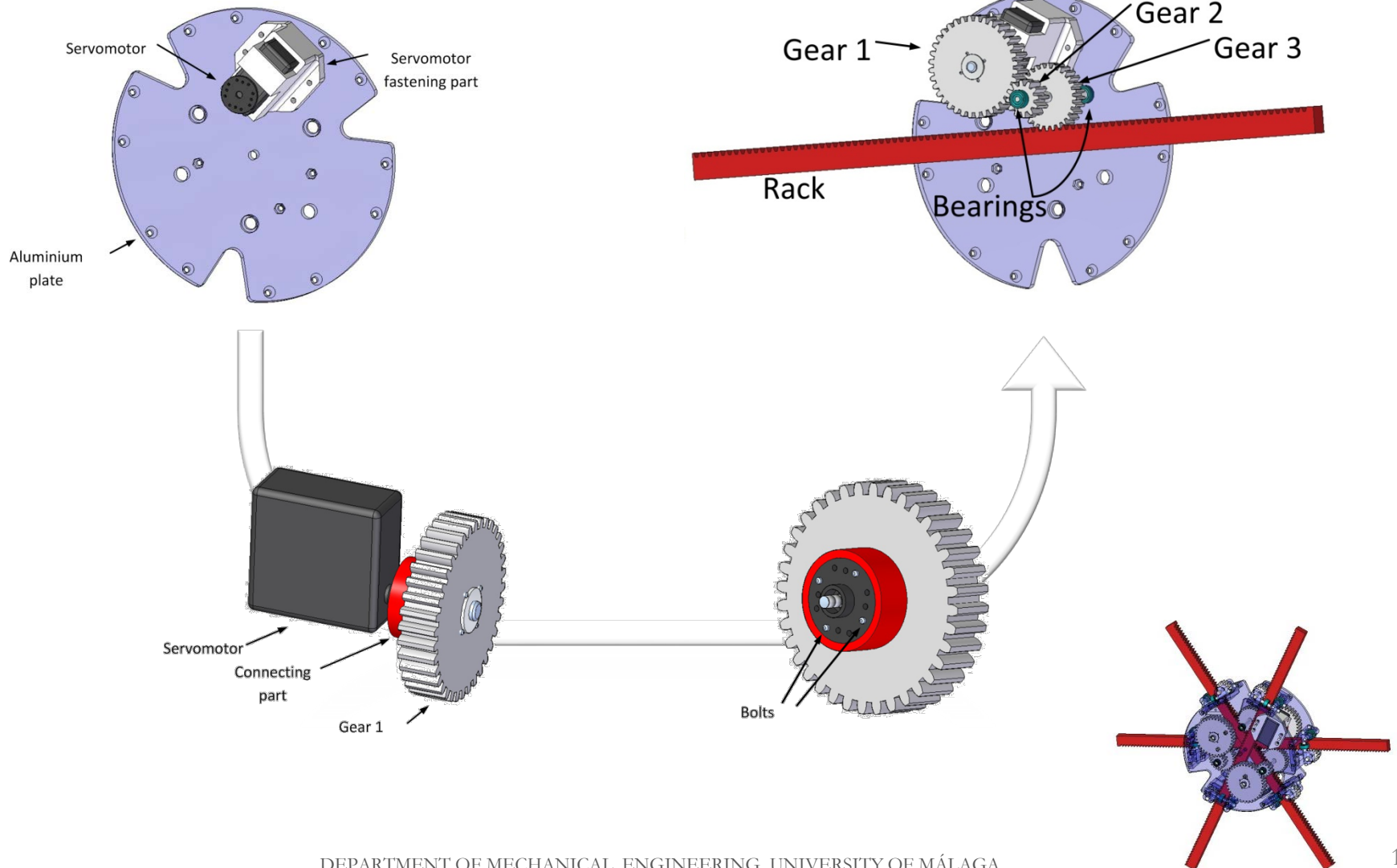


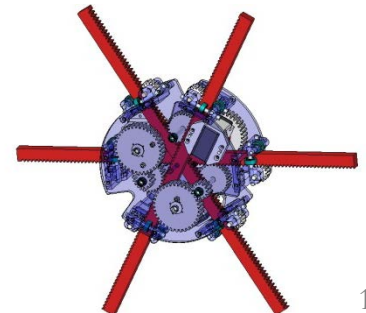
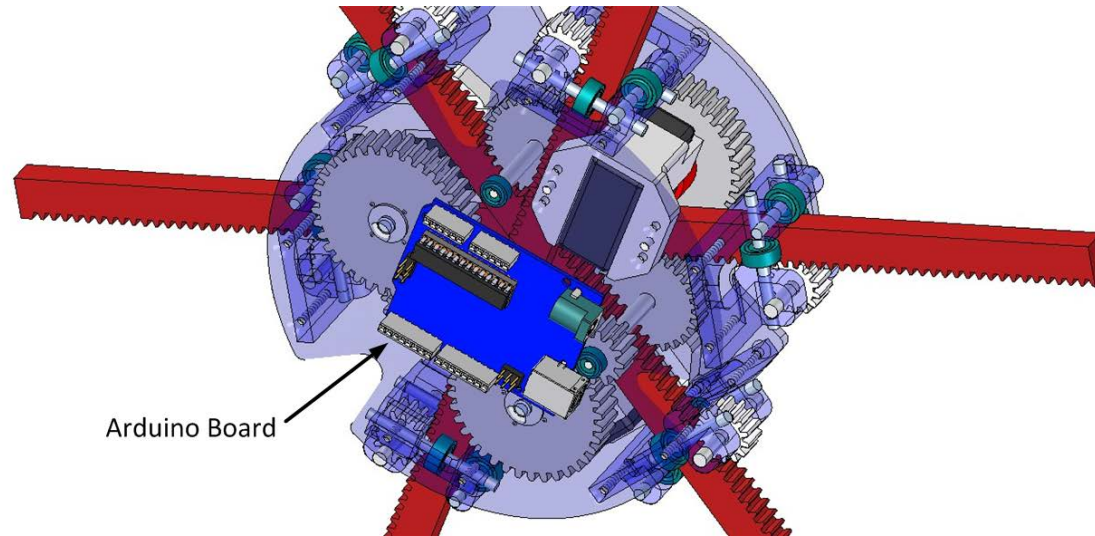
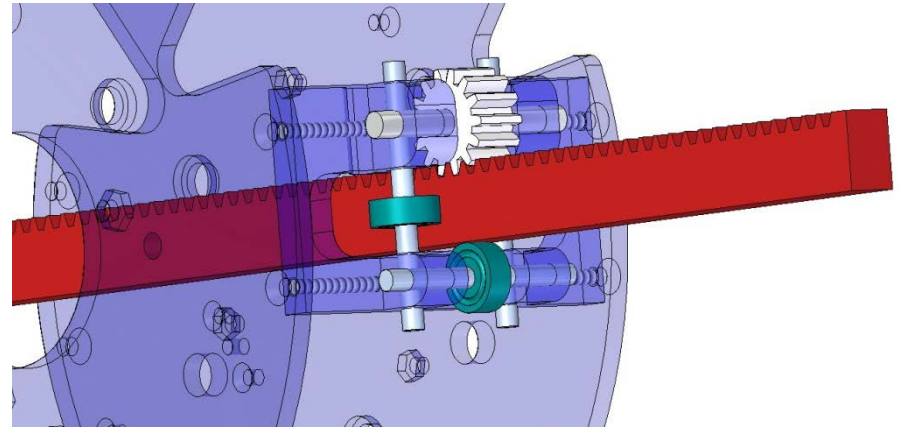
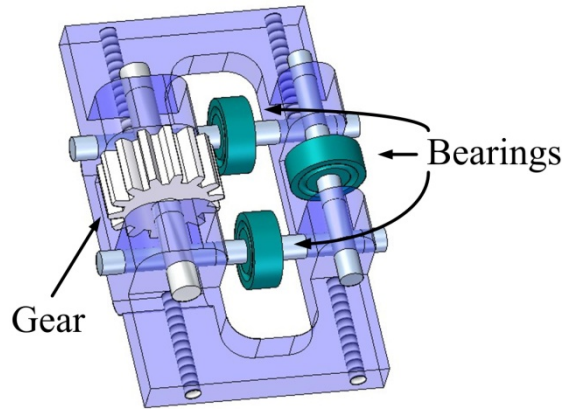
Mechanical Transmission

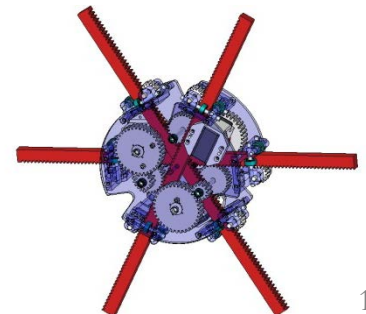
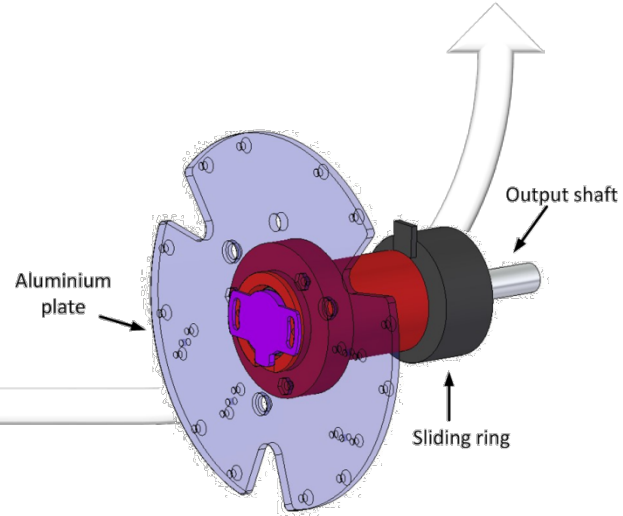
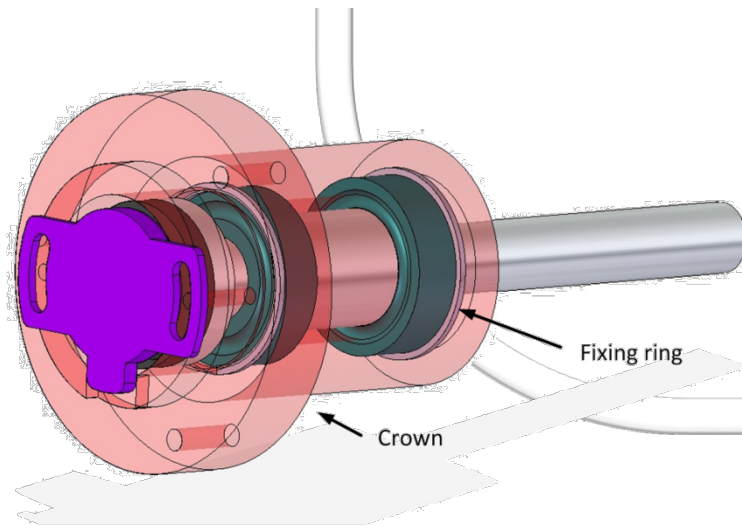
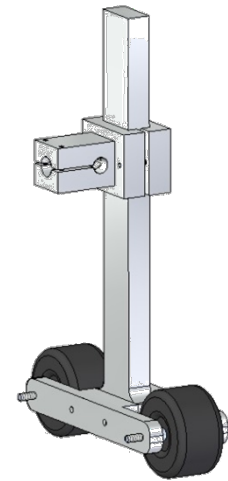
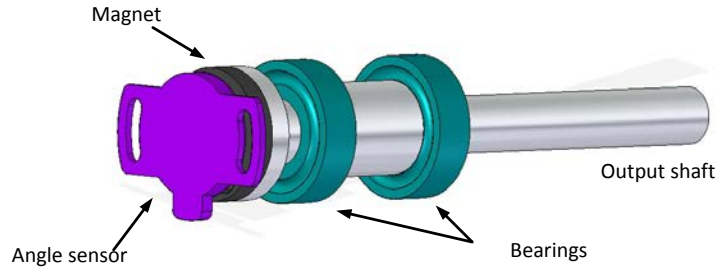
- Rotation 180°
- Sliding distance > 12.8 cm
- Maximum force = 30 N
- Low inertia



Mechanical Design







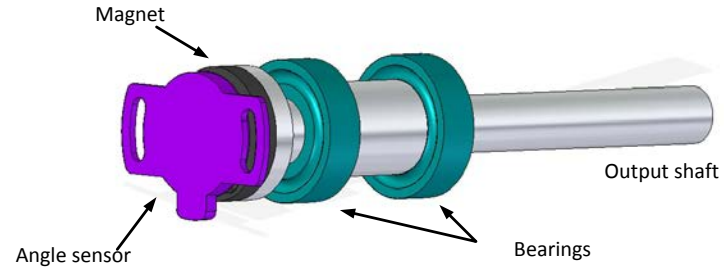
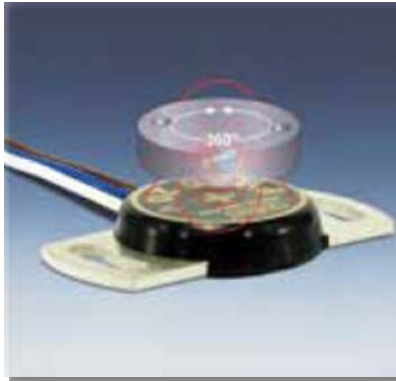


Electronics and Sensing

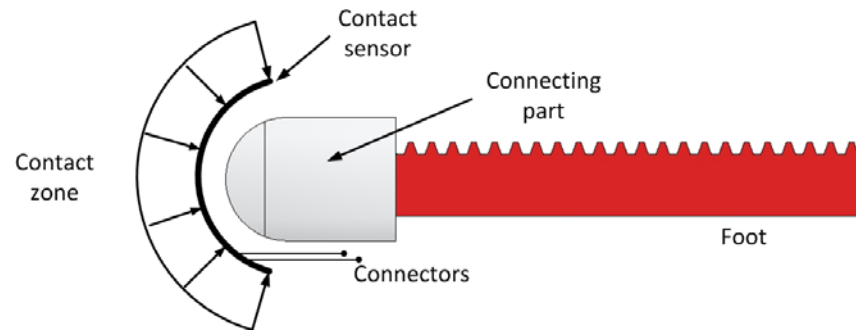
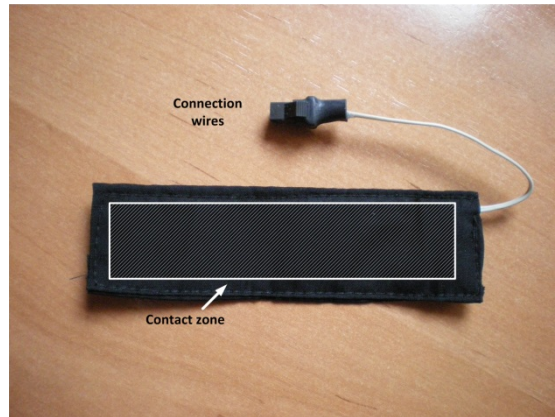


Sensors

Angular sensor

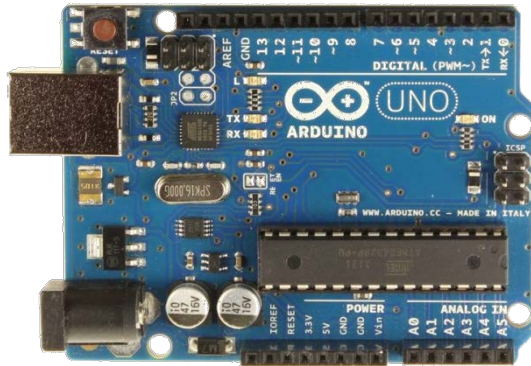


Contact sensor



Programming

Arduino UNO

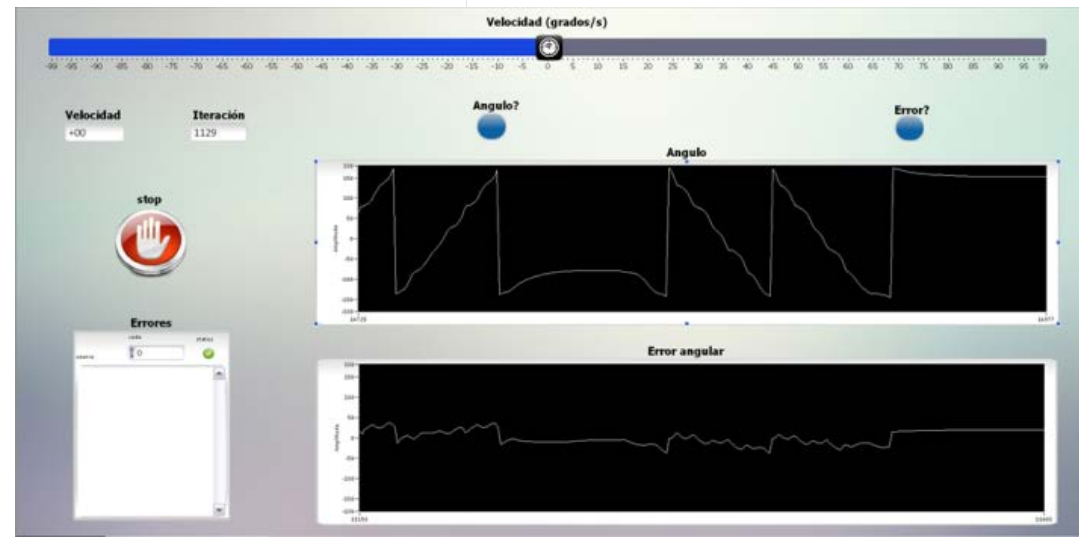


ZigBee module



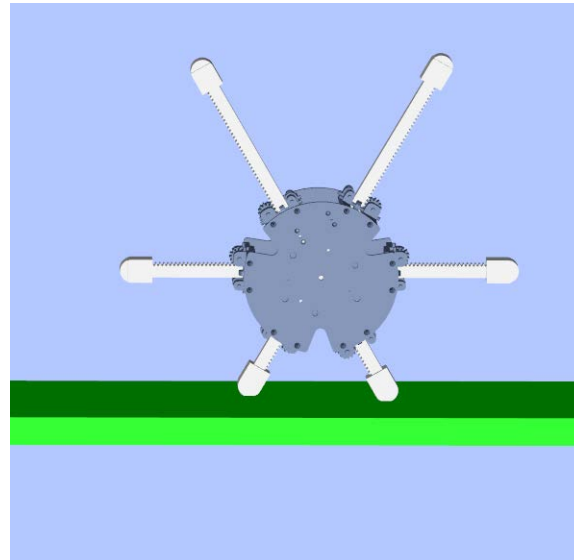
C++ (programming) ✓

LabVIEW Interface ✓

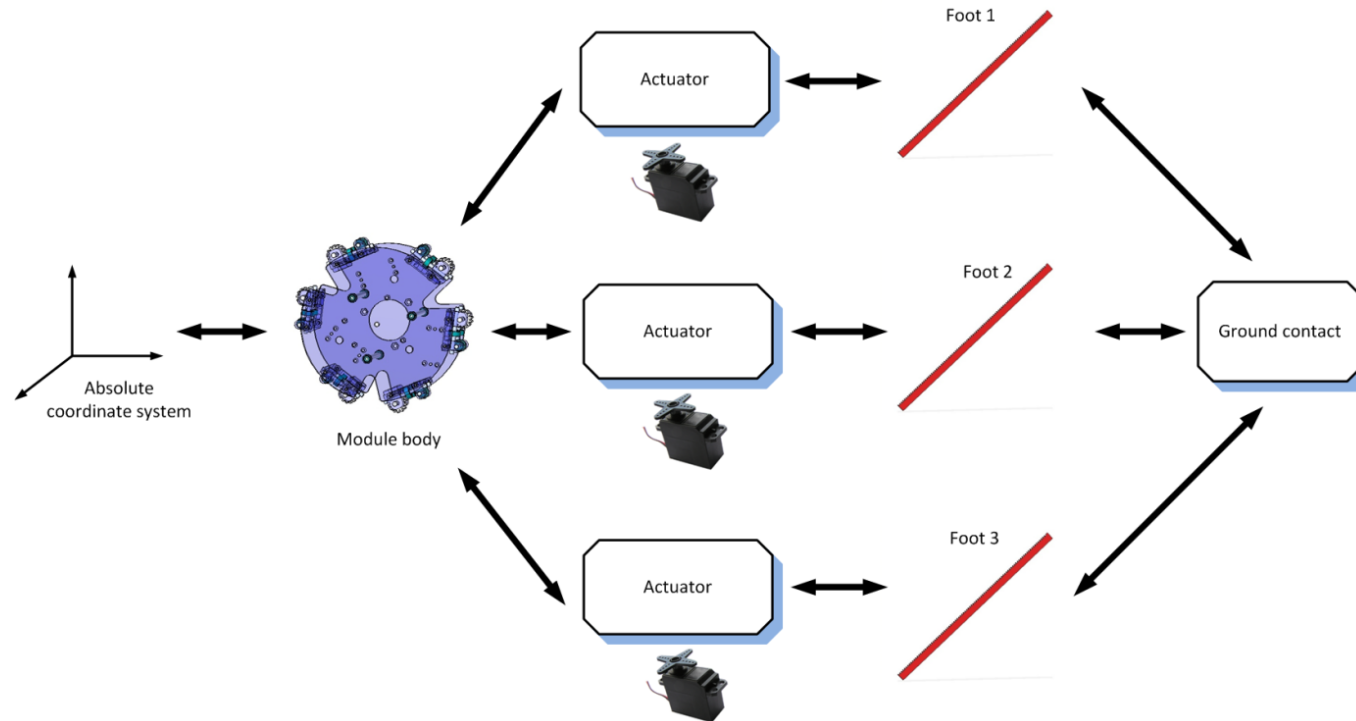




Module Modeling



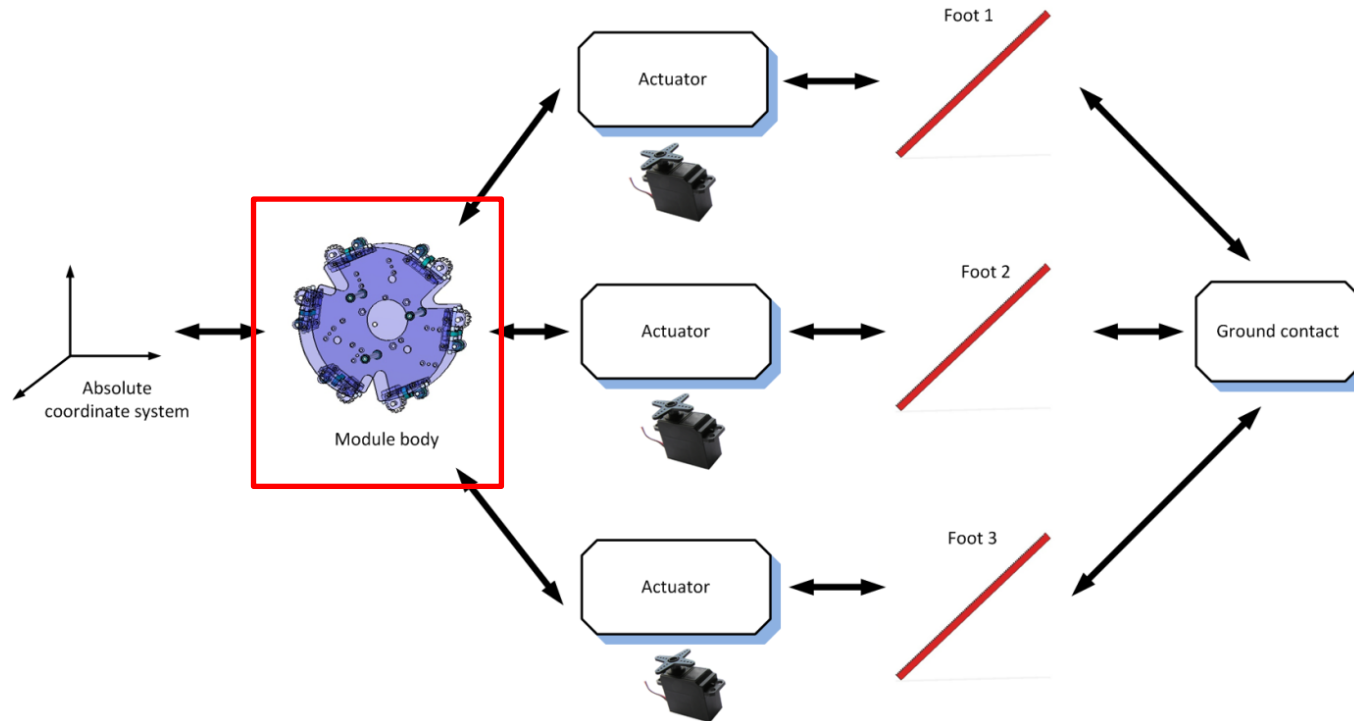
Module Modeling



Assumptions

- ❖ Bidimensional model
- ❖ Ground friction is considered
- ❖ Flat and smooth surface

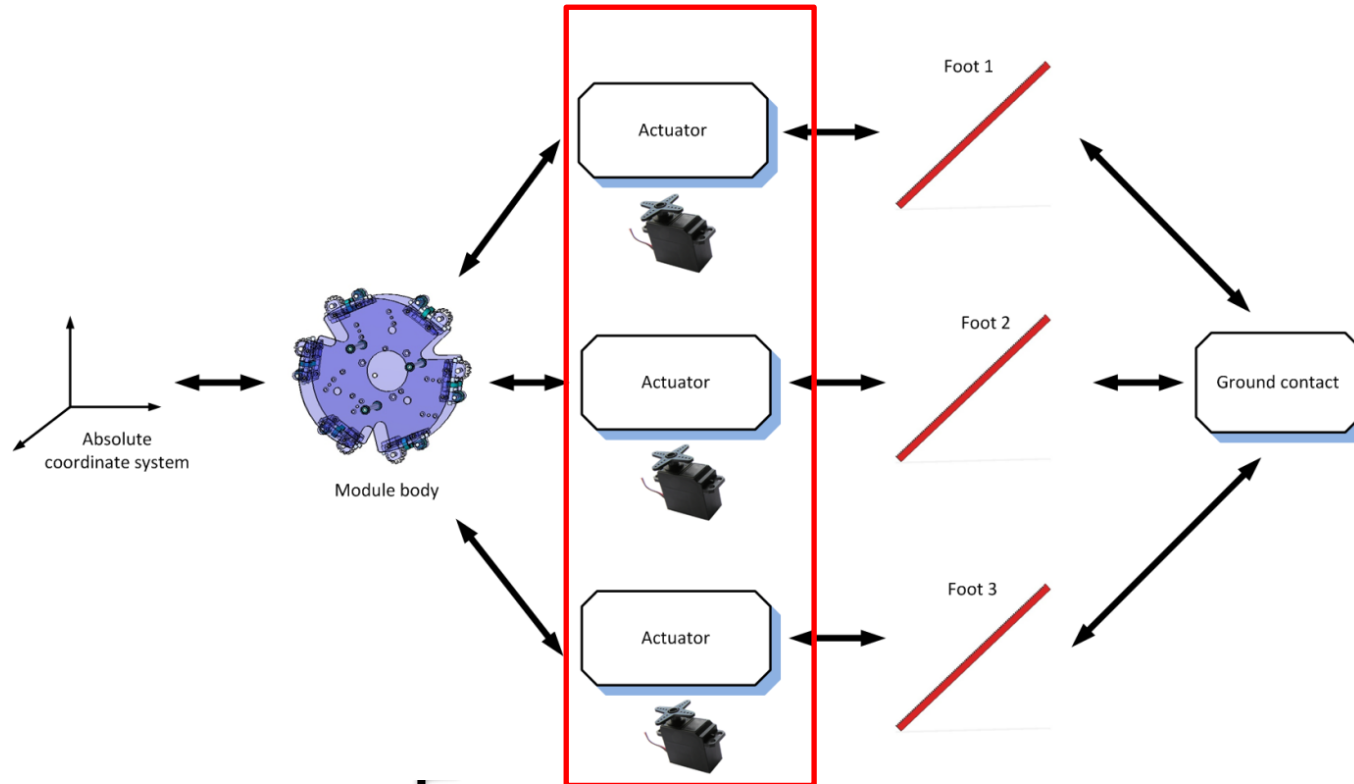
Module Modeling



Assumptions

- ❖ Bidimensional model
- ❖ Ground friction is considered
- ❖ Flat and smooth surface

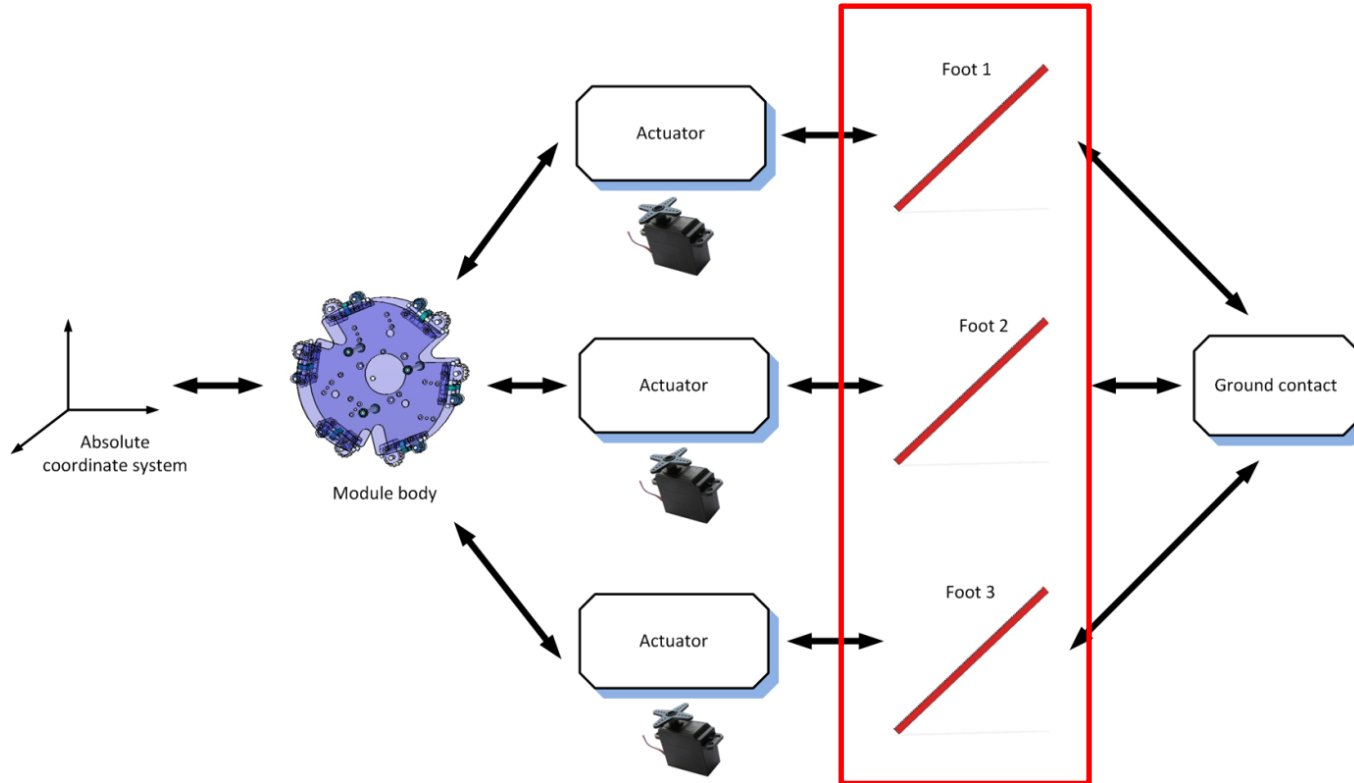
Module Modeling



Assumptions

- ❖ Bidimensional model
- ❖ Ground friction is considered
- ❖ Flat and smooth surface

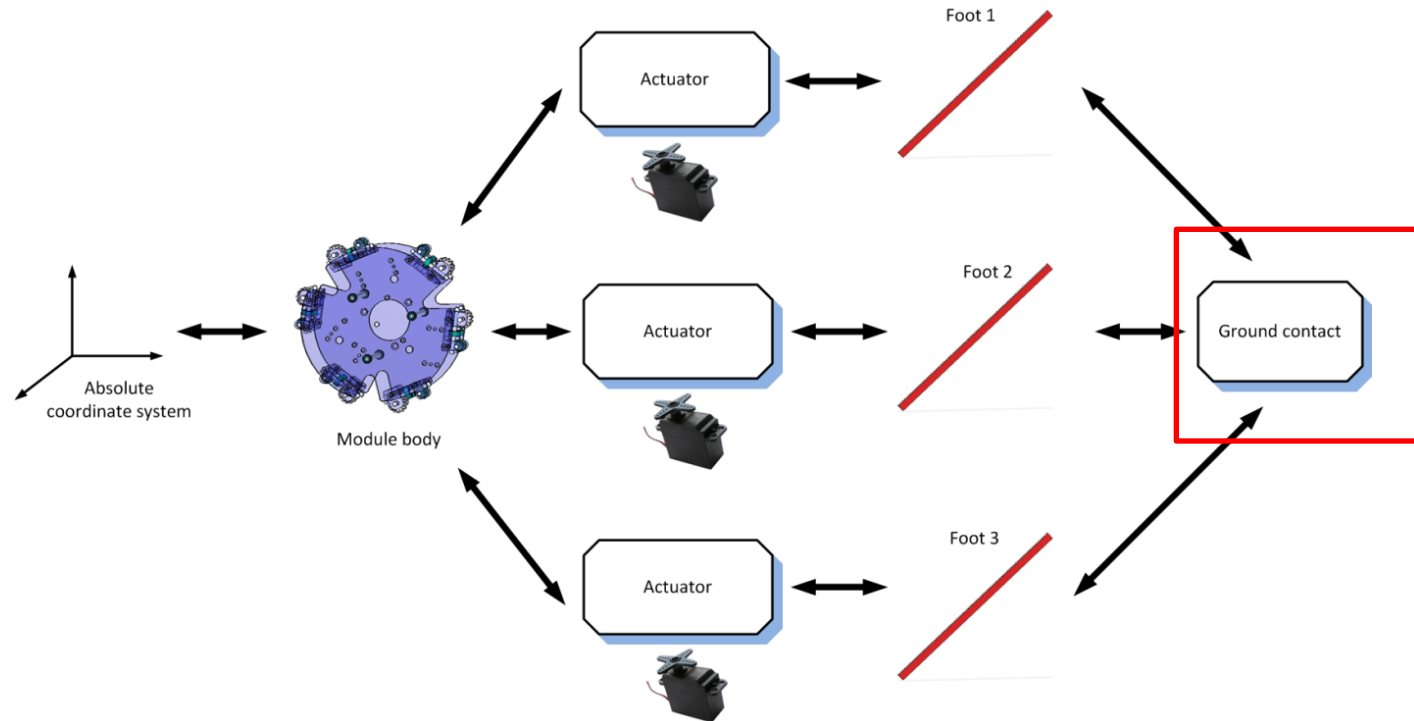
Module Modeling



Assumptions

- ❖ Bidimensional model
- ❖ Ground friction is considered
- ❖ Flat and smooth surface

Module Modeling

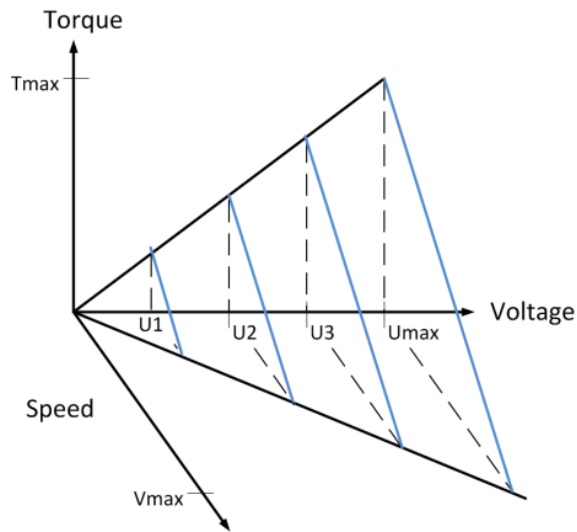


Assumptions

- ❖ Bidimensional model
- ❖ Ground friction is considered
- ❖ Flat and smooth surface

Motors modeling

Torque & Speed vs voltage

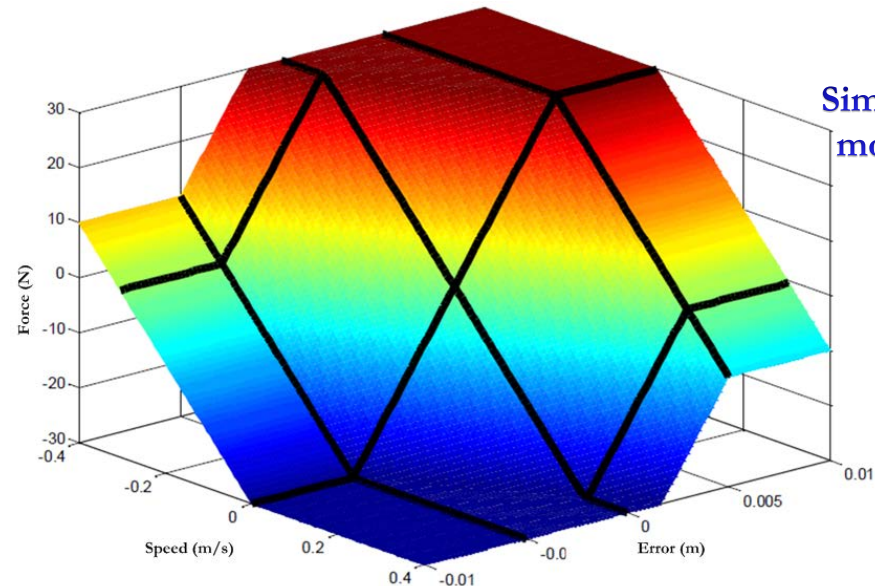


Linear actuator force

$$F(e, v) = \begin{cases} \frac{F_{max}}{e_c} e - \frac{F_{max}}{v_{max}} v & |e| < e_c \\ \text{sign}(e)F_{max} - \frac{F_{max}}{v_{max}} v & |e| \geq e_c \end{cases}$$

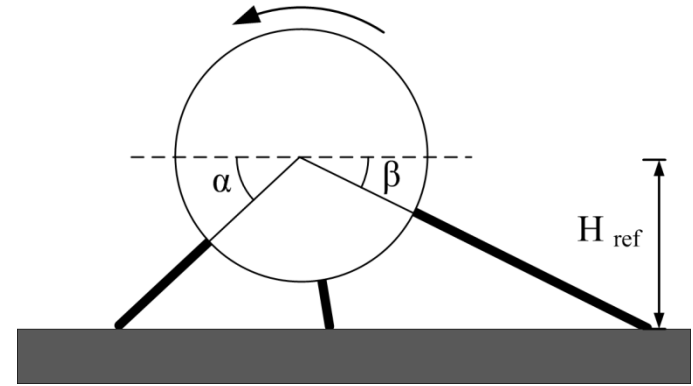
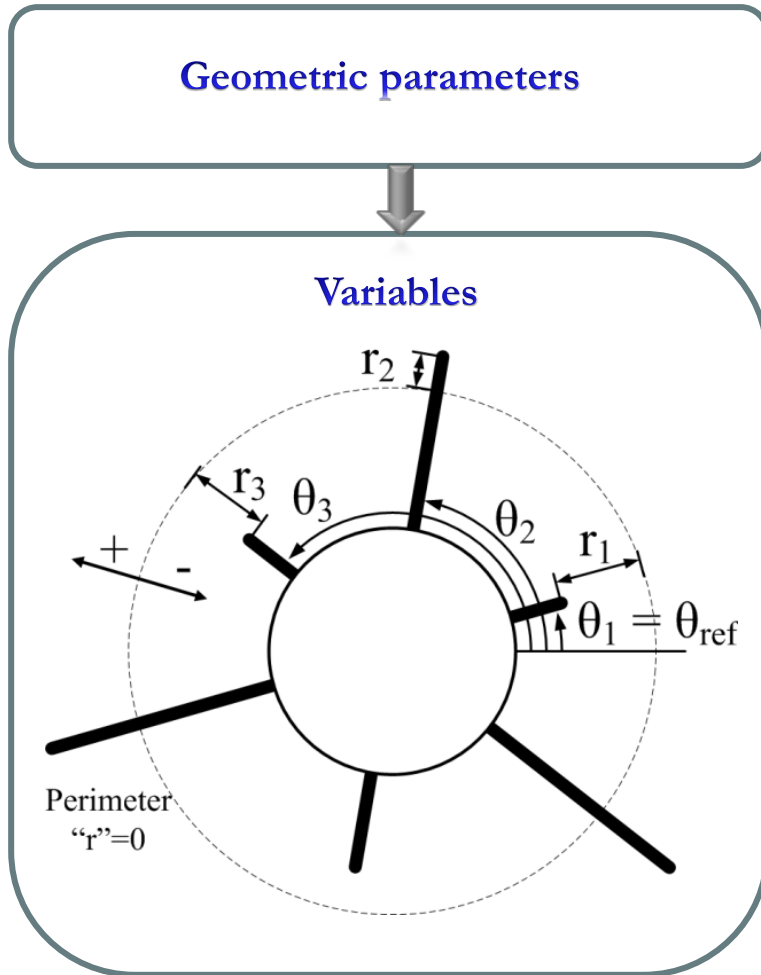
$e_c = \text{Maximum acceptable error}$

$$\text{Voltage} = \begin{cases} \frac{U_{max}}{e_c} e & \text{si } e < e_c \\ U_{max} & \text{si } e \geq e_c \end{cases}$$



SimMechanics
motor model

Feet movement control. Low level control.

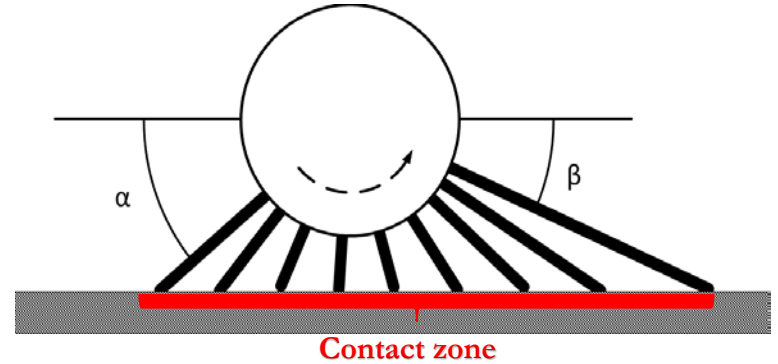


H_{ref} : desired height during operation

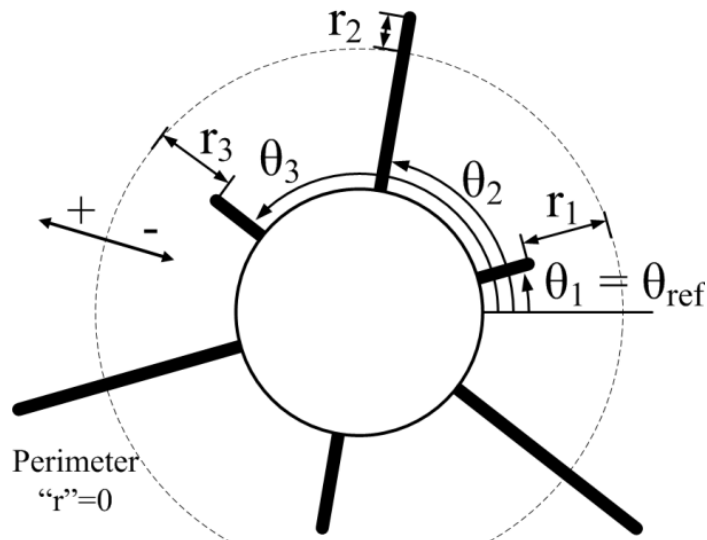
Θ : angular reference of the module

Feet movement control. Low level control.

Geometric parameters



Variables

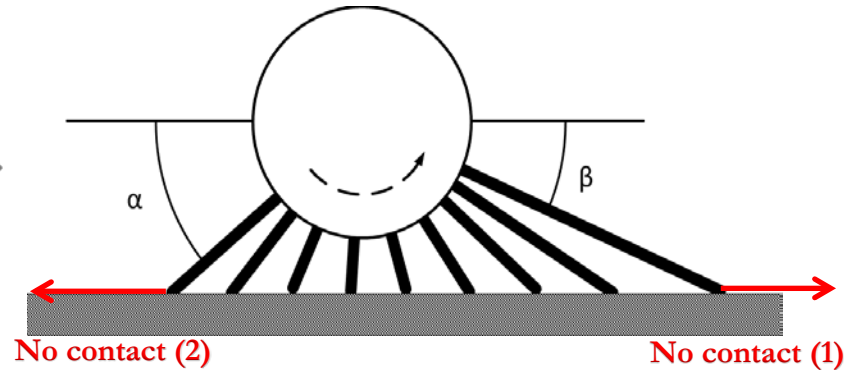


Control equations

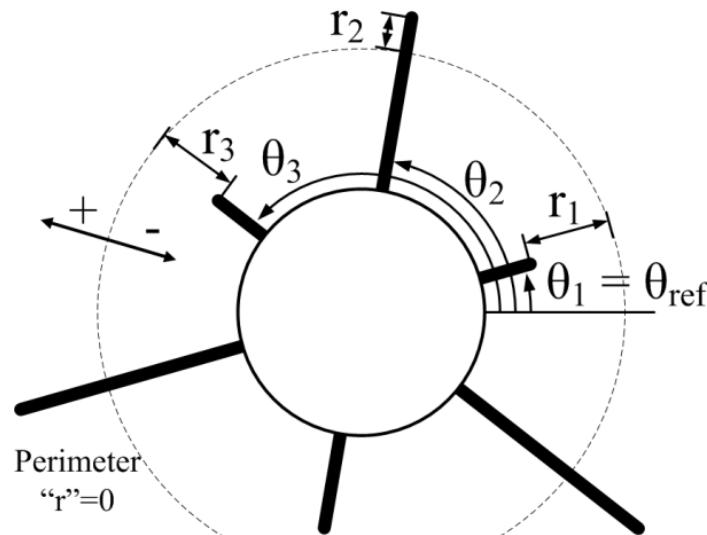
$$r_i^{ref} = \text{signo}(\sin(-\theta_i)) \left(\left| \frac{H_{ref}}{\sin(-\theta_i)} \right| - \frac{l}{2} \right)$$

Feet movement control. Low level control.

Geometric parameters



Variables



Control equations

$$r_i^{ref} = \text{signo}(\sin(-\theta_i)) \left(\left| \frac{H_{ref}}{\sin(-\theta_i)} \right| - \frac{l}{2} \right)$$

$$(1) \quad r_i^{ref} = - \left(\left| \frac{H_{ref}}{\sin(\beta)} \right| - \frac{l}{2} \right) \frac{\sin(\theta_i)}{\sin(\beta)}$$

$$(2) \quad r_i^{ref} = - \left(\left| \frac{H_{ref}}{\sin(\alpha)} \right| - \frac{l}{2} \right) \frac{\sin(\theta_i)}{\sin(\alpha)}$$

Ground contact model

Feet



Rigid solid

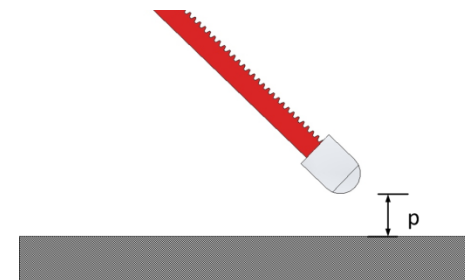
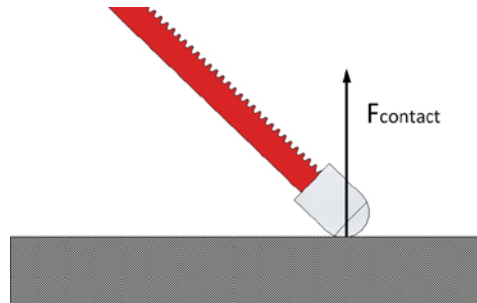
Ground



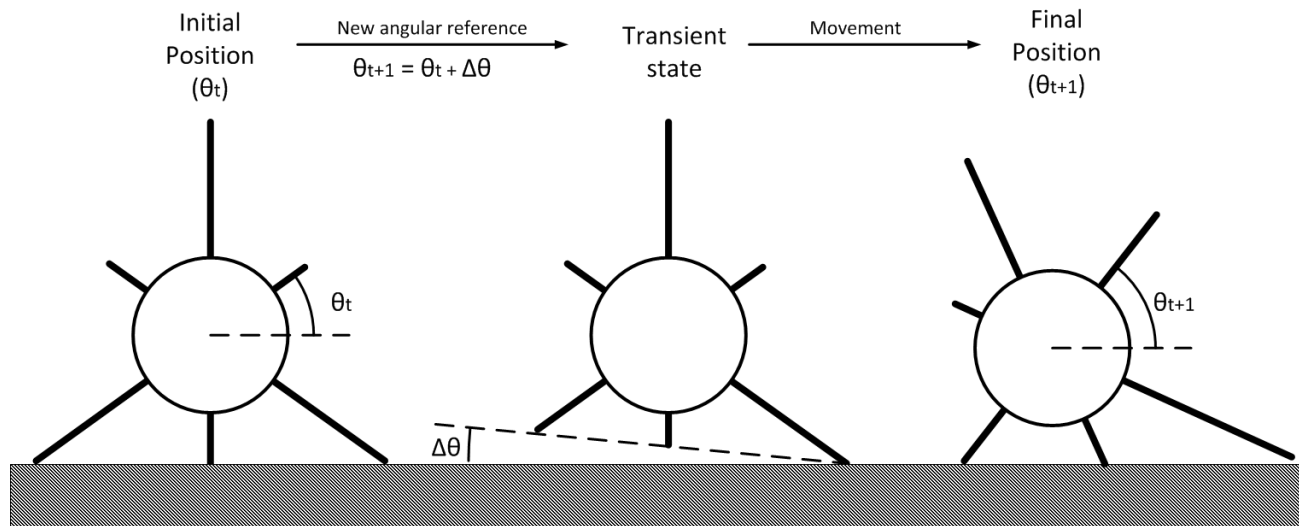
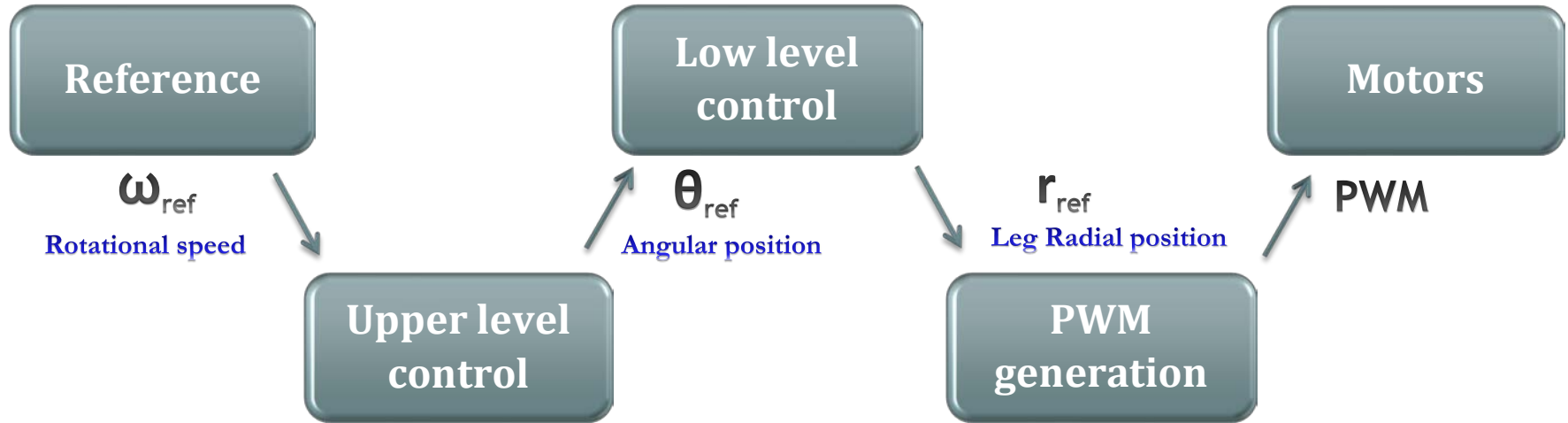
Soft solid (high elastic constant, k_e , + dissipation constant, k_d)

Normal force equation:

$$F_{contact} = \begin{cases} 0 & \text{si } p > 0 \text{ o } \left(-k_e p - k_d \frac{dp}{dt} \right) < 0 \\ -k_e p - k_d \frac{dp}{dt} & \text{si } p \leq 0 \text{ y } \left(-k_e p - k_d \frac{dp}{dt} \right) \geq 0 \end{cases}$$



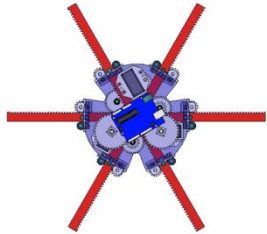
Module Modeling



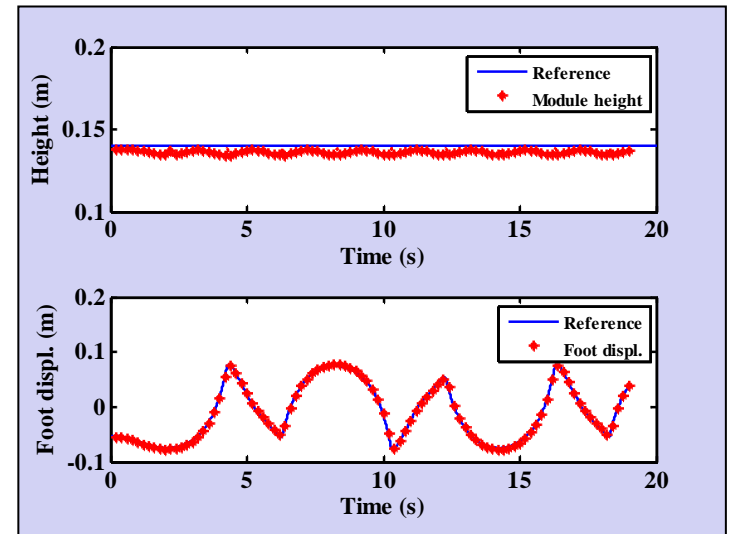
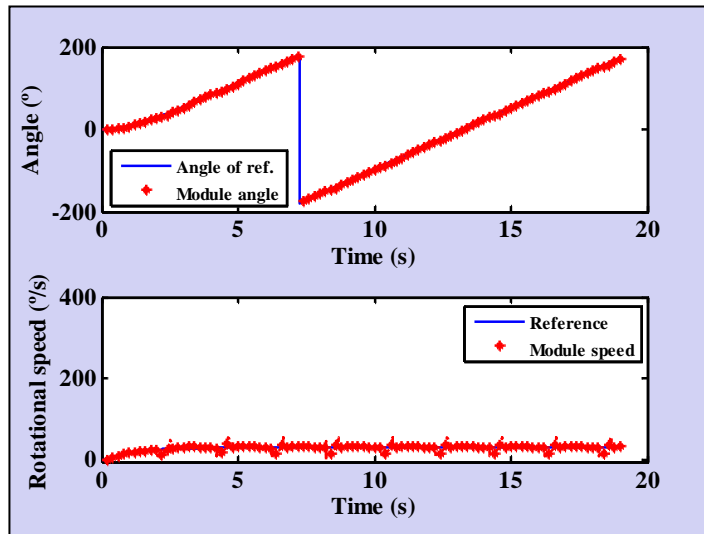
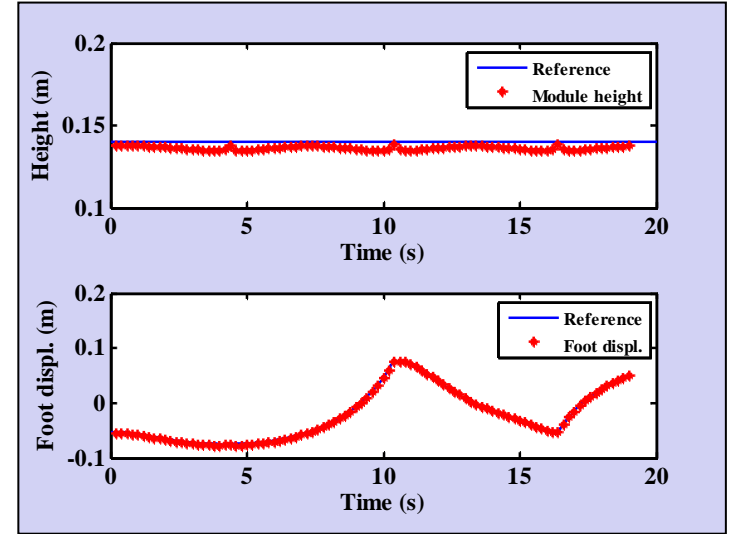
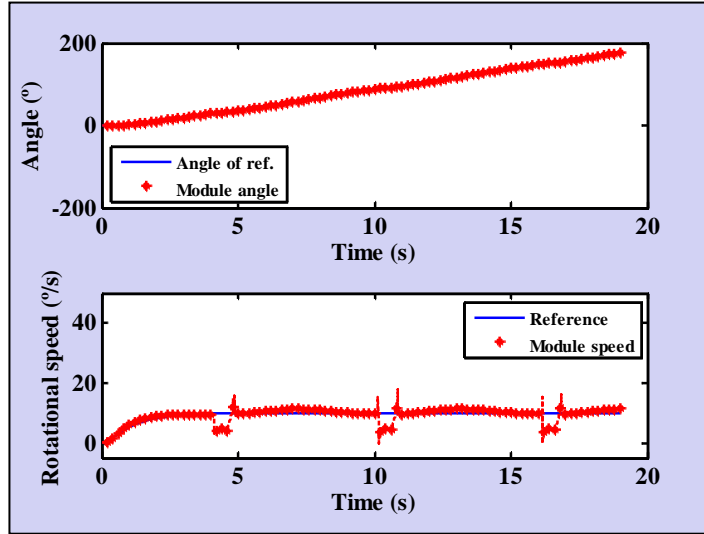
Module Modeling

Simulations

$$\omega_{ref}^1 = 10^\circ/s$$



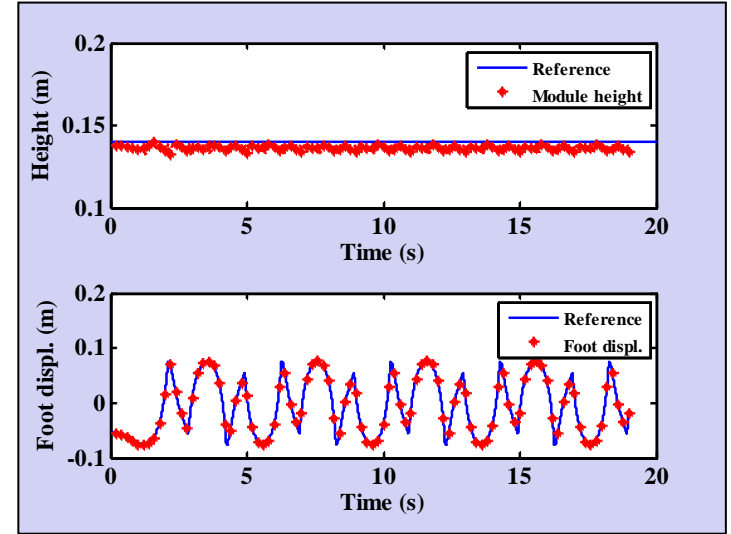
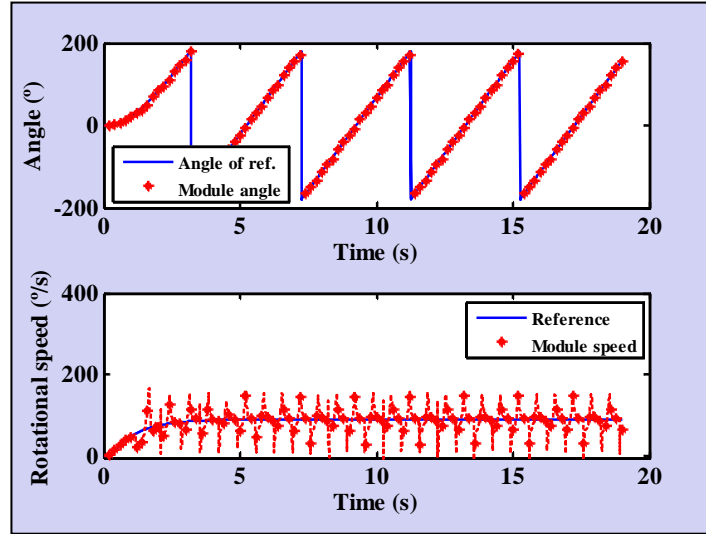
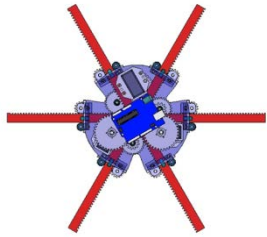
$$\omega_{ref}^1 = 30^\circ/s$$



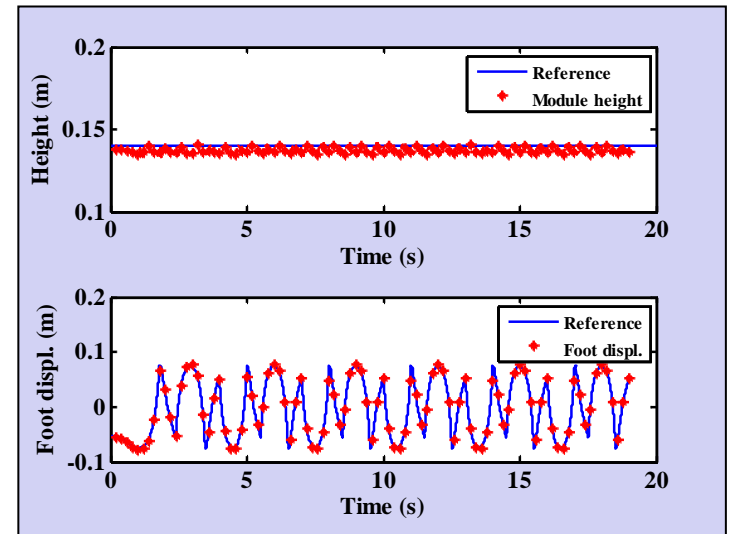
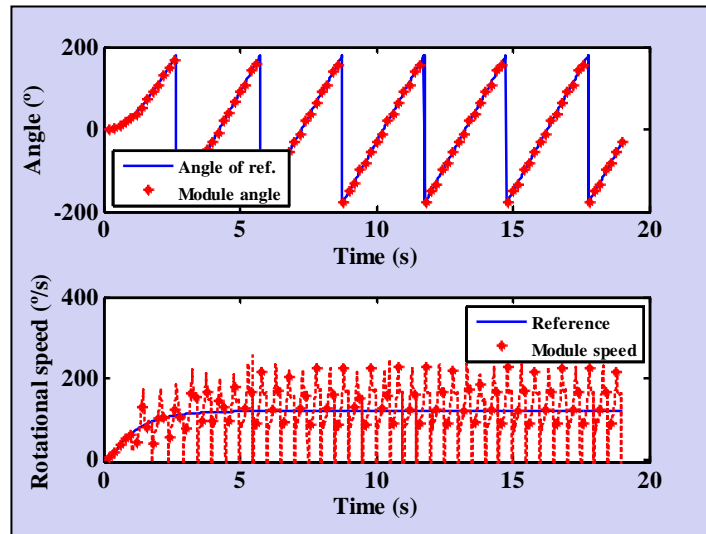
Module Modeling

Simulations

$$\omega_{ref}^1 = 90^\circ/s$$

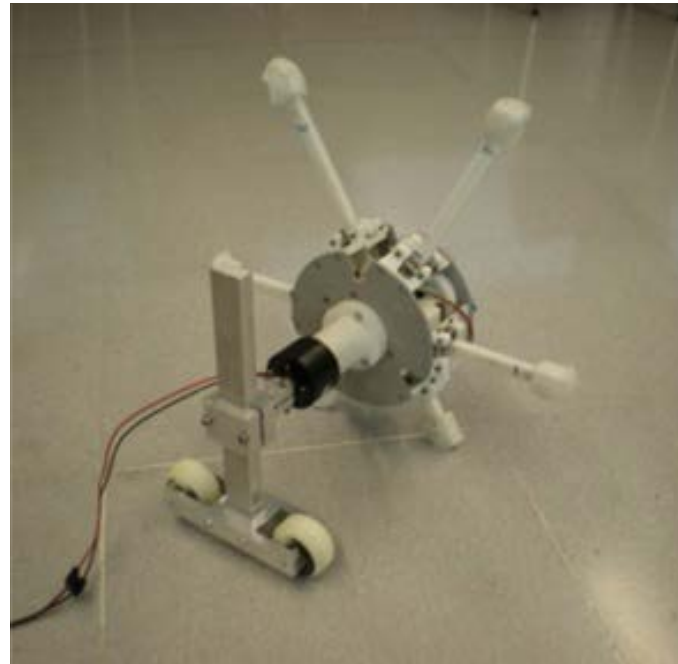


$$\omega_{ref}^1 = 120^\circ/s$$



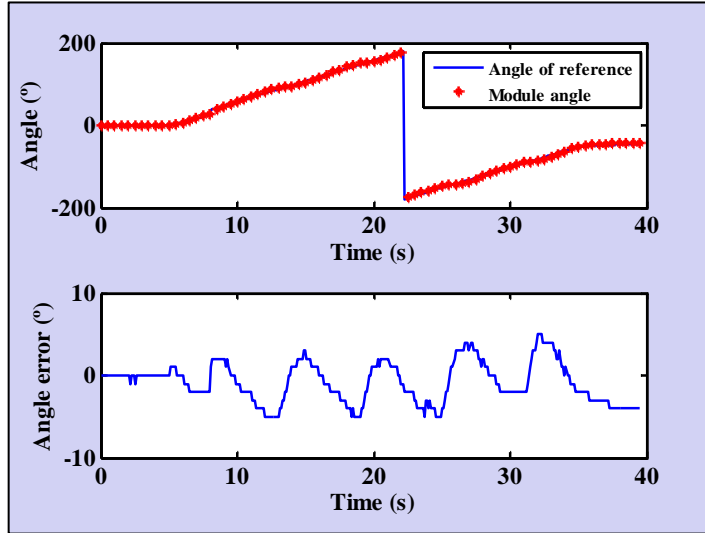


Experimental Results

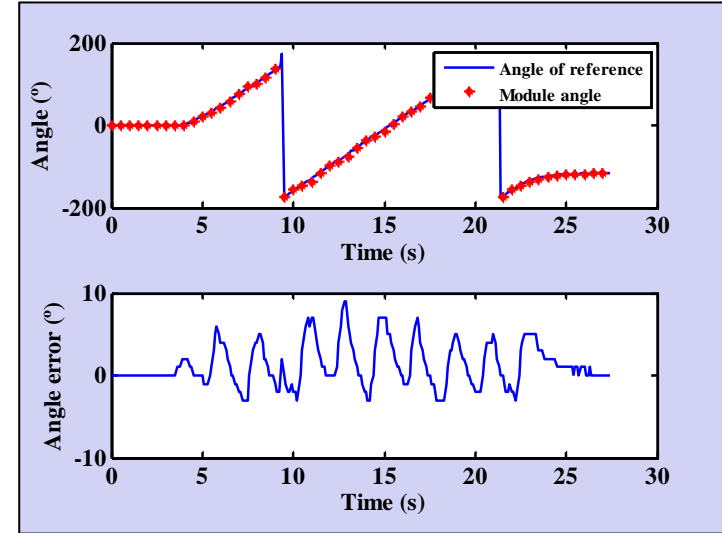


Experimental results

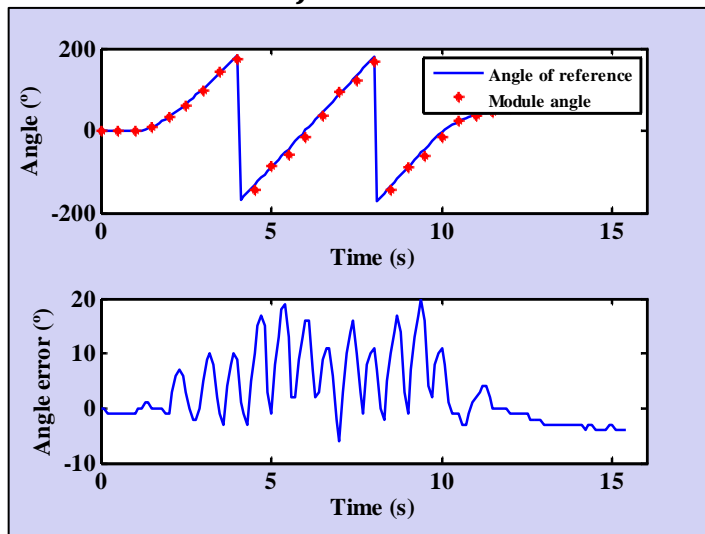
$$\omega_{ref}^1 = 10^\circ/s$$



$$\omega_{ref}^2 = 30^\circ/s$$



$$\omega_{ref}^3 = 90^\circ/s$$



- The module faithfully follows the reference.
- The maximum angle errors are smaller than 9 and 20 degrees respectively.
- The errors increase when moving faster since the movement of the module becomes sharper and less smooth.
- Results are very similar to those obtained in simulations,



Conclusions





Conclusions

- **A new concept of locomotion system for mobile robots has been proposed, designed and built.**



Conclusions

- A new concept of locomotion system for mobile robots has been proposed, designed and built.
- **A model of the module in SimMechanics™ has been programmed.**



Conclusions

- A new concept of locomotion system for mobile robots has been proposed, designed and built.
- A model of the module in SimMechanics™ has been programmed.
- **Simulations show that the model accurately reproduces the movement of the module.**



Conclusions

- A new concept of locomotion system for mobile robots has been proposed, designed and built.
- A model of the module in SimMechanics™ has been programmed.
- Simulations show that the model accurately reproduces the movement of the module.
- **The model is a very useful tool to test different control algorithms that could be implemented on the real robot.**



Conclusions

- A new concept of locomotion system for mobile robots has been proposed, designed and built.
- A model of the module in SimMechanics™ has been programmed.
- Simulations show that the model accurately reproduces the movement of the module.
- The model is a very useful tool to test different control algorithms that could be implemented on the real robot.
- **A control algorithm has been programmed and tested with the model.**

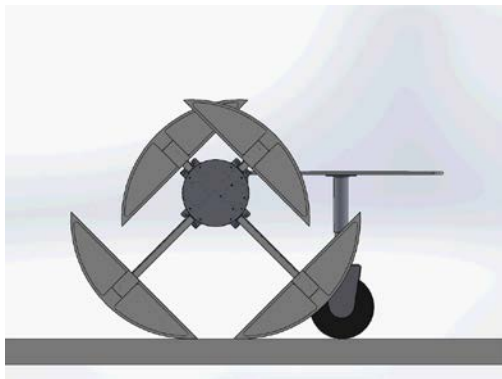
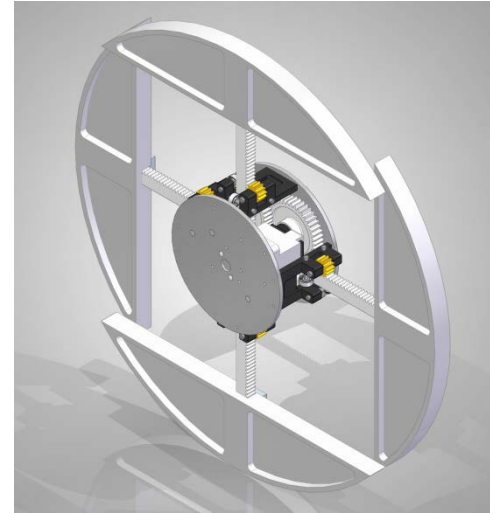
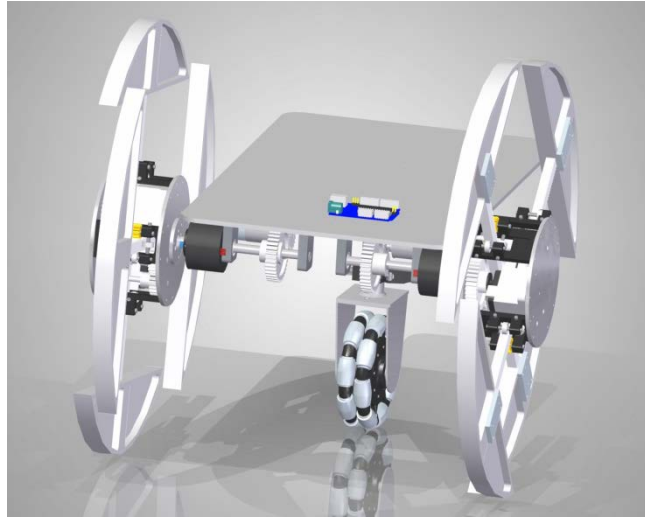


Conclusions

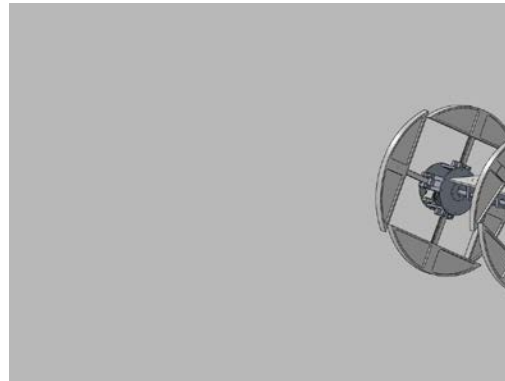
- A new concept of locomotion system for mobile robots has been proposed, designed and built.
- A model of the module in SimMechanics™ has been programmed .
- Simulations show that the model accurately reproduces the movement of the module.
- The model is a very useful tool to test different control algorithms that could be implemented on the real robot.
- A control algorithm has been programmed and tested with the model.
- **Experimental tests demonstrate the correct operation of the module when moving on a flat and smooth surface and without obstacles.**



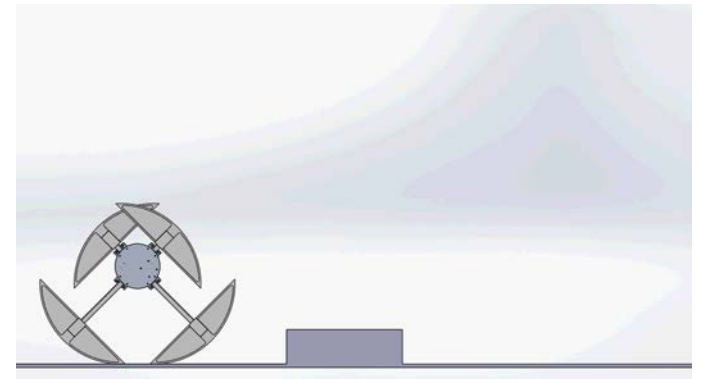
Conclusions



Legs



Wheels



Obstacle



Thank you for your attention

J. J. CASTILLO, J. A. CABRERA, M. JAIMEZ , F. VIDAL AND A. SIMÓN

Escuela de Ingenierías

C/ Doctor Ortiz Ramos s/n, 29071
Málaga, Spain

Tf. +34 951952369

Fax +34 951952605

E-mail: marianojt@uma.es

Web: webdeptos.uma.es/ingenieriamecanica

