

Fabrication of porous thick films using room‐temperature aerosol deposition

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Abstract

A novel technique for the rapid room‐temperature deposition of porous ceramic, glass, or metal thick films using the aerosol deposition (AD) method is presented. The process is based on the co-deposition of the desired film material and a second water-soluble constituent, resulting in a ceramic-ceramic composite. Following the subsequent removal of water‐soluble end member, a network of pores is retained. To demonstrate the process, porous $BaTiO₃$ thick films were fabricated through codeposition with NaCl. Microstructural images show the clear development of a porous structure, which was found to enhance the dielectric properties over dense thick films, possibly related to the lower extent of internal residual stress. This simple but highly effective porous structure fabrication can be applied to any film and substrate material stable in water and is promising for the application of AD‐processed films in gas sensors, solid oxide fuel cells, and humidity sensors.

KEYWORDS

ceramic matrix composites, dielectric materials/properties, porous materials, sensors

1 | **INTRODUCTION**

The aerosol deposition (AD) method¹ has gained significant interest as it facilitates the rapid fabrication of ceramic films on different ceramic, metallic, glass, and polymeric substrates at room temperature. The AD is a type of low‐temperature spray deposition technique, where submicron particles are aerosolized and carried through a specifically designed nozzle using a carrier gas to impact on the substrate. It is argued that the deposition process involves particle fracture and impact consolidation without any significant rise of local temperature.¹ Due to the impact consolidation mechanisms, AD‐processed films exhibit nanograined microstructure with relatively high density.² In addition, AD-processed films possess high internal residual stress, on the order of ~GPa, related to the deposition process. $3-7$

Dense ceramic films with enhanced functional properties as well as mechanical stability are useful for numerous applications, such as energy harvesters, sensors, microelectronics.8,9 However, for some specific applications the optimized properties are realized by the presence of controlled porosity in the microstructure. In fact, fabrication and understanding of electromechanical behavior in porous bulk ceramic are a significant area of academic and industrial interest.¹⁰⁻¹⁴ Additionally, ceramic films with porous microstructure are also essential for numerous practical applications. For instance, the gas-sensing properties and humidity sensing efficiency are profoundly affected by the density of the functional ceramic films.15,16 In addition, solid‐oxide fuel cells also requires a porous electrode layer for both the cathode and anode to facilitate efficient operation.¹⁷ For these reasons, a number lated to the deposition process.³⁻⁷ of previous investigations have focused on developing porous intervalsed on the deposition of previous investigations have focused on developing porous intervalsed in the set of the se

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films using the AD method.^{18,19} Ryu et al¹⁹ used a β-tricalcium phosphate/TiO₂ composite and an acid leaching step to create a porous structure, demonstrating enhanced photocatalytic activity of the porous $TiO₂$ film. It has also been found that adding a small amount of polymer to the ceramic matrix and subsequent high-temperature heating of the as-deposited film can reduce the internal residual stress and induce porosity in the structure.²⁰ Recently, a Japanese patent was filed that mentioned the fabrication of porous AD films for dye‐sensitized solar cell using nanoparticles of water‐soluble materials. 21 In this work, however, we demonstrate a simple way to prepare AD-processed porous structure without requiring any heat-treatment or acidic chemicals. Importantly, this technique can be applied to any water‐stable substrate and film material, such as ceramics, metals, and glasses, which opens the possibilities for application in numerous technologies and engineered structures. To demonstrate the facile green fabrication route, we used water‐soluble NaCl powder and $BaTiO₃$ to prepare a ceramic-ceramic composite. The microstructure and relative dielectric permittivity of an AD-processed dense BaTiO₃ film of \sim 16 µm thickness was compared with that of an AD-processed porous BaTiO₃ film.

2 | **EXPERIMENTAL PROCEDURE**

Commercially available $BaTiO₃$ (Helsa-automotive GmbH & Co. KG) and NaCl powder were used in this work. NaCl powder was milled using cyclohexane to optimize the median particle size, $d_{50} \approx 1.2$ µm for the deposition. As-received $BaTiO₃$ powder was milled using a rolling mill to obtain the median particle size $d_{50} \approx 1$ µm. The NaCl and BaTiO₃ powders were dry mixed with a ratio of 70 vol% NaCl and 30 vol% BaTiO₃. The NaCl/BaTiO₃ composite powder was codeposited on a stainless steel substrate (SUS 304) using the AD process.⁷ Details of the AD process parameters can be found in Table 1. Following deposition, the NaCl/BaTiO₃ composite film was washed using distilled water in an ultrasonic bath for 5 minutes. The washed sample was air dried

for approximately 12 hours at 100°C before measurements. The cross-section of the sample was prepared using sequential grinding, polishing, and additional fine polishing with colloidal silica suspension for 90 minutes. Microstructures were observed using a field-emission scanning electron microscope (FE‐SEM, JSM‐7600F). The microstructure was analyzed to obtain an estimation of the fraction of porous area in the film using $ImageL^{22}$ The temperature-dependent dielectric permittivity over the range from room temperature to 300°C was measured using an automated system whereby an impedance analyzer Keysight Model E4980AL and a furnace (LE 4/11 3216, Nabertherm GmbH) were controlled by a LabView program. During testing, the SUS304 substrate acted as the bottom electrode, while a top Pt (area of 5×4 mm) electrode was sputtered on the opposite side of the film. The sample was electrically contacted with the 4‐point measurement technique using Pt wires, which were electrically shielded by Inconel tubing to minimize external parasitic signals.

3 | **RESULTS AND DISCUSSION**

The cross-sectional images of the as-processed dense $BaTiO₃$ and porous $BaTiO₃$ films, that is, after the removal of NaCl, are shown in Figure 1A,B, respectively. A significant difference in the microstructure is visible, most notably an increase in the number and size of the visible pores through the thickness of the film. The observed pores also appear elongated parallel to the substrate surface. This elongation is possibly related to the impact consolidation mechanisms of AD. As porosity can be observed through the full thickness of the $BaTiO₃ film$, it is expected that the porous network fully penetrates the film. However, it is important to note that how much NaCl is fully embedded in the BT matrix and cannot be removed with the washing process remains unclear. It is likely that the resulting porous film is a combination of 0‐3 and 3‐3 connectivity, where additional studies are required to accurately determine the ratio of each. It should be mentioned here that the deposition parameters and particle morphology of the BaTiO₃ powder was the same for both cases. Additional SEM image (Figure S1) reveals that a size reduction of the starting ceramic particles took place during the co-deposition of BaTiO₃/NaCl powder. Moreover, the AD process‐induced crystallite size reduction was also confirmed for both the dense and porous film (Figure S4). These observations further confirmed the impact consolidation process in the $BaTiO₃/NaCl$ codeposited porous film. Additionally, our previous study showed that NaCl itself can be deposited using AD process where impact consolidation phenomenon occurred.²³

In order to determine the pore content, the cross‐sectional microstructure of the dense and porous BT film was analyzed

FIGURE 1 Cross‐sectional micrographs of a dense (A) and a porous (B) BaTiO₃ film deposited with AD. Analyzed area fraction of a dense (C) and a porous film (D). A calculated porous area fraction of 1.7% and 11.8% were obtained, respectively [Color figure can be viewed at wileyonlinelibrary.com]

(Figure 1C,D). From this analysis of the microstructure, a porosity of 1.7% \pm 1% and 11.8% \pm 2.7% was estimated for dense and porous AD films, respectively. It should be mentioned here that the ceramic specimen with a density of ≤90% of theoretical density can be considered to exhibit open porosity, that is, interconnected pores.^{24,25} In our case, the estimated porosity of approximately 12% further indicates the occurrence of open porosity. An average pore size (feret diameter) of 0.10 ± 0.05 µm (176 pores) and 0.14 ± 0.07 µm (498 pores) for dense and porous BT films were estimated. It should be highlighted that although average pore size of the porous BT is not significantly different from the dense BT film, the number of pores is almost four times greater and also they are more homogeneously distributed. It is important to note that although the average pore size is ~ 0.1 µm the pore size is not homogenous, that is, a number of pores larger than the average size is clearly visible. For a better analysis of porous structure, it will be ideal to investigate using micro‐ CT or spectroscopic ellipsometry. Nevertheless, our analysis gives a semi‐quantitative estimation of the extent of porosity in the film. It should be noted here that, despite the use of 70 vol% NaCl, the estimated porosity using a microstructure image is only approximately 12%. This is possibly related to the difference in deposition efficiency of NaCl and BaTiO₃. It is reasonable that for a given carrier gas flow rate NaCl and BT will have different impact velocities due to the difference in density of NaCl (2.16 $g/cm³$) and BaTiO₃ (6.02 g) cm³). It is considered that for the deposition of AD film, a window for particle impact velocity of 150-500 m/s is required.² Therefore, variation in impact velocities can affect the particle deposition efficiency. Another possibility is that

the dry mixing of the constituent particles was not sufficient to homogenously distribute the NaCl and BaTiO₃. Wet mixing of NaCl and BT using cyclohexane could be beneficial to improve the homogeneity.

AD‐deposited BT ceramic films are of significant interest for humidity sensing applications.^{15,16} The efficiency of the humidity sensor prepared by AD-processed film can be significantly improved by the porous microstructure. The porous structure obtained using a simple method in our work can be helpful to explore further humidity sensing properties of other material systems. The temperature‐dependent dielectric permittivity of as‐processed and heat‐treated BT films, both dense and porous, is shown in Figure 2. The porous BT film displayed a room‐temperature dielectric permittivity value nearly twice that of the dense film. This enhanced permittivity is possibly related to the lower internal stress in the porous film. Previous reports on AD‐processed film have shown that the porous films as well as ceramic/polymer composite films exhibit lower internal stresses than the regular processed AD $film.²⁶⁻²⁸$ In addition, although we have not observed any significant difference in the grain size as well as in the crystallite size of dense and porous $BaTiO₃$ film (Figures S1-S4), it is known that the AD‐processed film exhibits inhomogeneous grain size. Therefore, it is possible that the presence of NaCl, that is, co-deposition of BaTiO₃/NaCl shifted the BaTiO₃ grain size distribution toward larger grains and resulted in an increase in permittivity. It should be mentioned here that the AD‐processed dielectric ceramic films intrinsically show lower dielectric permittivity than their bulk counterpart and is possibly related to the fine-grained microstructure.^{29,30} In addition, previous studies on the stress‐dependent dielectric

FIGURE 2 Temperature‐dependent dielectric permittivity of the as‐processed (1st heating cycle) and dried (2nd heating cycle) (A) porous BaTiO₃ and (B) dense BaTiO₃ measured at 1 kHz. Frequencydependent room-temperature $(\sim 20^{\circ}C)$ dielectric permittivity of the porous and dense film after heat treatment up to 300°C is shown as the inset in (A) and (B), respectively [Color figure can be viewed at wileyonlinelibrary.com]

permittivity of $BaTiO₃$ have shown an increase in the Curie temperature and a more diffuse phase transition.³¹ The observed dielectric anomaly at approximately 100°C in the as‐processed porous BT film is likely related to water incorporation, which could have occurred during the washing process to remove NaCl. No such anomaly was observed for the second heating cycle, indicating that the water was removed. A similar minor dielectric peak at 100°C was also observed in the dense as‐processed film, likely also related to water incorporation through, for example, humidity. Interestingly, the permittivity value for the porous BT film is higher than the regular dense BT film of similar thickness even after heat treatment, indicating that the higher permittivity exhibited in the porous BT film is not solely related to the water content. The frequency‐dependent dielectric permittivity of the thermally annealed porous $BaTiO₃$ film is shown in inset of Figure 2A. It can be seen that within the broad frequency range the room‐temperature permittivity value does not change significantly.

4 | **CONCLUSIONS**

We developed a simple fabrication method for porous ceramic thick films, which can also be applied to other non–water-soluble film and substrate materials. This costeffective and rapid method involves the co-deposition of a water-soluble and a non-water soluble end member, resulting in a ceramic‐ceramic composite. After removal of the water-soluble end member, a network of pores is retained, which can have significant influence on various industrial applications. The results of $BaTiO₃$ films deposited on steel were presented, where a porosity of approximately 12% were found to increase the relative permittivity.

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SUPPORTING INFORMATION

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