

BLIND OCEAN ACOUSTIC TOMOGRAPHY: EXPERIMENTAL RESULTS ON THE INTIFANTE'00 DATA SET

S.M. Jesus^a, C. Soares^a, J. Onofre^b and P. Picco^c

^a *SiPLAB-FCT, Universidade do Algarve, PT-8000 Faro, Portugal*

^b *Instituto Hidrográfico, PT-1296 Lisboa, Portugal*

^c *ENEA, Marine Environment Research Centre CP 224, I-19100 La Spezia, Italy.*

Summary:

Blind Ocean Acoustic Tomography (BOAT) is an ocean remote exploration concept similar to acoustic tomography but where both the emitted signal waveform and the source position are unknown. BOAT consists of a minimal environmental model of the area, a broadband matched-field processor and a genetic algorithm search procedure. This paper presents the results obtained with BOAT on part of the data set acquired during the INTIFANTE'00 sea trial, where an acoustic source was towed along both range independent and range dependent paths, with source-receiver ranges varying from 500 m up to 5.5 km and water depths varying from 70 to 120 m. The results obtained on several hours of data, show that source range and depth can be used as focalizing parameters, together with the Bartlett power to indicate model fitness. Using this three parameters it becomes clear when the environment is “in focus” and when it is “out of focus” leading to reliable estimates of the geometric and environmental parameters under estimation.

1 Introduction

Ocean Acoustic Tomography (OAT) explores the tight relation between ocean physical properties and sound propagation. This relation is such, that transmitting a sound wave between two points allows, under certain circumstances, to determine the mean temperature profile over the distance separating the two points. Among the circumstances that may condition OAT are the ability of the source emitted signal to temporally resolve the multipath structure of the acoustic channel, the *a priori* knowledge of other environmental parameters (like for instance geoaoustic properties), the precise knowledge of the source - receiver relative position, both in depth and range, and finally the knowledge of the source emitted signal waveform itself.

If some (or all) of those parameters are not precisely known, the situation is similar to that encountered in communication theory, when both the message and the transmission channel are unknown and need to be simultaneously estimated - that is blind deconvolution. In ocean acoustic tomography, simultaneous estimation of the environmental properties that describe the channel of propagation and the acoustic source position, without knowing the source emitted waveform, is called “Blind Ocean Acoustic Tomography (BOAT)”. In practice BOAT simply starts from an *a priori* baseline model of the area with all parameters unknown, but the bathymetry. When a signal is received at the array, a few frequencies are selected without precise knowledge either of the transmitted

signal itself or the source position. A broadband conventional Bartlett processor is used to incoherently combine various frequencies and provide an objective function to be optimised with a genetic search algorithm. The procedure described so far is, in all respects, similar to *acoustic focalization*, as proposed in [1] and used for generic parameter estimation in [2], for geoacoustic inversion in [3, 4], and for source localization in [5, 6, 7]. One risk inherent to focalization with a high number of free parameters, is that the final model estimate might represent an acoustic equivalent model but an environmentally different model from the true model, leading to erroneous environmental parameter estimates. The objective of this paper is to show some real data examples where, using an extended band of frequencies and three “model fit indicators” lead to credible environmental model estimates.

In this paper, the results obtained on a real data set acquired during the INTIFANTE’00 sea trial, off the coast of Portugal, near Setúbal, have shown that the ensemble of source range, source depth and Bartlett power can be safely used as indicators for determining if the model is adequate, giving expectable results regarding water column temperature evolution through time and space. Those results were obtained both with a fixed and a moving source over range independent and range dependent bathymetries. The source emitted signals were either deterministic linear frequency modulated (LFM) chirps or continuous pseudorandom noise sequences.

2 The INTIFANTE’00 sea trial and baseline models

The INTIFANTE’00 sea trial was primarily designed for testing shallow water tomography and source localization techniques. An

overall description of the sea trial can be found in [8]. This paper concentrates on two events in particular: event II, along a range-independent(RI) track, towards NW from the receiving vertical line array (VLA), and event 5, along a range-dependent(RD) track, to the NE of the VLA. Both events are depicted on figure 1. The bathymetry used for the computer model was obtained from direct depth sounding over a 200 m wide path along the acoustic propagation lines, as shown on the colour coded background of figure 1. Figure 2 shows source range versus time as estimated from GPS data, for event 2 (a) and for event 5 (b). The geoacoustic properties were drawn from generic geological knowledge of the area where it was assumed that the NW-RI track had a quite regular bottom, covered by fine sand, and the NE-RD track was largely range-dependent with a background of fine sand and patches of mud, gravel and rock. There were no *in situ* tests or other acoustic measurements in the area previous or after the experiment that could be used as additional background information.

2.1 The baseline model

An important first step in tomographic inversion is the choice of an environmental model able to represent the mean characteristics of the media where the signal is propagating. Such model will be called the baseline model and generally includes all the a priori information available for the problem at hand. In our case there will be two of such models: one for the RI track and the other for the RD track. They basically consist of an ocean layer overlying a sediment layer and a bottom half space assumed to be range independent. Since for the application at hand little environment information is available all the parameters will be assumed equal for the two models apart from the bathymetry. For a sake of simplic-

ity figure 3 shows the baseline model only for RD-track, knowing that the only difference for the RI-track is that the bathymetry will be constant with a water depth equal to 119 m. For the purpose of inversion the forward model parameters were divided into four parameter subsets: geometric, sediment, bottom, and water sound speed. The geometric parameters included source range, source depth, receiver depth and bathymetry (in the RD case). The water column sound speed, shown in figure 3, is the mean temperature profile measured at the VLA thermistor sensors (see environmental description in [8]).

2.2 Ocean sound speed modelling

Another important problem when inverting acoustic data for tomographic purposes, is the difficulty associated with the representation of the sound speed field in time, depth and range, by a finite set of invariant parameters. The classical solution for this problem, known as data regularization, consists on the expansion of the temperature, or equivalently the sound speed field¹, on a basis of functions representative of the data set to be estimated. A well known method for obtaining such basis functions, is to calculate the Empirical Orthogonal Functions (EOF) from the eigenfunctions of the data correlation matrix. The EOFs were obtained using a singular value decomposition (SVD) of a data matrix \mathbf{C} with columns

$$\underline{C}_i = \underline{c}_i - \bar{c}, \quad (1)$$

where \underline{c}_i are the real profiles available, and \bar{c} is the average profile. The SVD is known to be

$$\mathbf{C} = \mathbf{U}\mathbf{D}\mathbf{V}, \quad (2)$$

where \mathbf{D} is a diagonal matrix with the singular values, and \mathbf{U} is a matrix with orthogonal

¹if the salinity profile is known.

columns, which are used as the EOFs. The sound-speed profile is obtained by

$$\underline{C}_{EOF} = \bar{c} + \sum_{n=1}^N \alpha_n \underline{U}_n, \quad (3)$$

where N is the number of EOFs to be combined, judged to accurately represent the sound speed field for the problem at hand. Generally, a criteria based on the total energy contained on the first N EOFs is used. The 14 sound speed profiles obtained from the XBT measurements (see \mathbf{X} signs in figure 1) served as database for the computation of the EOFs. The criteria used to select the number of relevant EOFs was

$$\hat{N} = \min_N \left\{ \frac{\sum_{n=1}^N \lambda_n^2}{\sum_{m=1}^M \lambda_m^2} > 0.8 \right\} \quad (4)$$

where the λ_n are the singular values obtained by the SVD, M is the total number of singular values, provided that $\lambda_1 \geq \lambda_2 \geq \dots \geq \lambda_M$. For this data set, criteria (4) yielded $N = 2$, i.e. the first two EOFs are sufficient to model the sound speed with enough accuracy (see figure 4). The coefficients α_n , which are the coefficients of the linear combination of EOFs, are now part of the search space, i.e., they are searched as free parameters.

3 Inversion results

Multiple environmental and geometrical parameter optimization is often a computationally cumbersome task. The first approach to the problem is to try to obtain as much *a priori* information as possible for the environmental parameters in the baseline model, in order to set an interval of variation as narrow as possible into the focalization process. The search intervals for the baseline model described above have been set according to the values shown in Table 1. The forward computation model used was the normal mode code

CSNAP[9]. The optimization technique for reducing the number of forward computations was based on a genetic algorithm (GA) and the GA implementation used was proposed by Fassbender [10].

Symbol	Unit	Search int./Steps		
α_1	m/s	-20	20	64
α_2	m/s	-20	20	64
sr	km	0.5	5.5	128
sd	m	10	100	64
rd	m	85	95	32
θ	rad	-0.03	0.045	32
c_{sed}	m/s	1520	1700	64
h_{sed}	m	1	15	32
Δc_{bot}^\dagger	m/s	20	200	32

Table 1: Focalization parameters and search intervals: EOF1 (α_1), EOF2 (α_2), source range (sr), source depth (sd), receiver depth (rd), VLA tilt (θ), compressional sediment speed (c_{sed}), sediment thickness (h_{sed}) and bottom compressional speed variation (Δc_{bot}). † where Δc_{bot} is assumed to lay in the interval $[\hat{c}_{sed} + 20, c_{sed} + 200]$.

In order to cover a search space of the order of 10^{15} , the GA optimizer was set with a population size of 90 individuals and 50 iterations. Three independent populations were run for each case. The mutation and the crossover probability were respectively set to 0.008 and 0.7. In particular, a new technique that was found to drastically optimize the search is to use the final solution at a given time point in the initialization of the solving procedure of the next time point.

Let us assume that at time t_i the best individual of the last population is $b(t_i)$. The GA is initialized at time t_{i+1} such that 30% of the individuals of the initial population are uniformly distributed within a 10% variation interval of the coordinates of $b(t_i)$. The other 70% are randomly distributed in whole search space, as it is usually done, in order to maintain a high degree of diversity. With this procedure the number of iterations has been

decreased at each time point except for the first one. In practice it is verified that the model fit drops at the beginning of each time point when compared with its value at the end of the previous time point, denoting that a misadjustment has been introduced in the data. However, after that initial fitness drop, rapid convergence is obtained leading to parameter values settling down to their "right" values, or at least those that give the highest fit. The objective function used in this study, was based on the incoherent Bartlett processor in a frequency band selected according to the received signal spectrum.

3.1 The NW-RI track

At the beginning of the run the source was moving away from the VLA location giving the opportunity to test inversion methods with a moving source, which is known to be an always challenging exercise for matched-field algorithms. The source was emitting a series of LFM signals which frequency range, duration and repetition rate is described in [8], and is not repeated here since that information was neither explicitly or implicitly used in the present study in order to ensure passive tomography constraints. For each time point estimate three consecutive snapshots were isolated, Fourier transformed and averaged. From the resulting spectra 7 discrete frequencies 50 Hz apart in the band 300-600 Hz were extracted for computing the incoherent Bartlett processor.

The focalization results are shown in figure 5, plots (a) to (j) and the reconstructed sound speed field is shown in plot (k). These results call for the following comments: first, is that the model fit to the data is excellent with a mean Bartlett power of 0.8, only dropping below that value at the end of the run. Source range is perfectly in agreement with the GPS estimated values and, although there

are no complete source depth recordings, the estimated values do agree with cable scope estimates taking into account ship speed, source weight and cable payout. Note that even the small ship acceleration at the beginning of the run is perfectly reproduced with a consequent and logical decrease on the source depth from about 80 to 73 m. Receiver depth and tilt are consistent with the values monitored by the VLA sensors (see report [11]). Bottom properties are consistent with those historically found in that area, that correspond to a thin (2 - 4 m) sediment layer of fine sand or mud, although it may be doubtful that it can be clearly “acoustically seen” at those frequencies. The sound speed inversion result shown in plot (k) represents about 2h 15min of data which is clearly a short time interval but denotes a slight rise of the thermocline in agreement with the data observed at the VLA thermistors (see [8]) and in phase with a tidal prediction for that day. Note that during this inversion the source was moving, so the depth-time plot can also be seen as a depth-variable range-average plot, depending if the temperature field is assumed range stationary or time stationary, respectively.

3.2 The NE-RD track

Although a range-independent propagation environment is a view of the reality that allows nice theoretical analytical developments, it is, in most cases only a simplified view that does not represent the large majority of the real world situations. In this section the data gathered during event 5, along the NE leg, when the source was at about 5 km range and then approaching the receiver is used to downslope propagate from approximately 70 m water depth to the VLA located in 120 m water depth (see figure 1). This is the most interesting yet, most difficult, case that attempts to represent a realistic situation of

an unknown sound source emitting a PRN sequence at undetermined range and depth, moving over a range dependent environment. The frequency band was the same as that used for the event 2. The results of the inversion are shown in figure 6.

This run is a good example on how the three indicators - source range, source depth and Bartlett power - can be used to validate environmental model estimates. At the beginning of the run, until Julian time 290.96, the Bartlett power varies between 0.4 and 0.8, source range changes rapidly and most of the other parameters have highly variable values and some are on, or near, the bounds of their search intervals. So in these initial period, sound speed estimated values are can not be considered as valid. At Julian time 290.96, source range suddenly picks up at 4 km range and steadily follows the approaching of the source to the VLA up to time 291 at about 2 km source range. During that interval most of the parameters, but the EOF coefficient 1, follow stable and credible values well within their respective intervals and are therefore mostly credible. The first EOF coefficient suffers a strong, and to date unexplained, change at 290.98 right in the middle of that smooth path. After Julian time 291, when the source has reached the closest point of approach to the VLA, the “focus” is again suddenly lost with strong variations on all parameters: drop of the Bartlett power from 0.8 to 0.3, a sudden range variation from 1 to 3.5 km and a drop of 10 m on source depth. It was found that time 291 coincides with the low-tide change producing a 1.5 m rise on the array accompanied of strong variations on array tilt, as measured on the depth sensors and tiltmeters on the VLA (see report [11]). The model regains “focus” after 15 min with smooth parameter estimates and high Bartlett power values. Among all obtained values within validated intervals

source range and depth were clearly in agreement with the expected values, sound speed in the sediment and bottom are reasonably well estimated to have mean values of 1580 and 1700 m/s, with a higher uncertainty in the last one, and finally array depth and array tilt are in good agreement with the pressure and tilt sensors colocated with the VLA. After focalization the sound speed evolution through time was reconstructed - plot (k) - showing a highly perturbed estimate due successive focus and lost of focus throughout time.

4 Conclusions

One of the basic principles of OAT is that both source(s) and receiver(s) are under control - that is, the emitted source signal and the source-receiver geometry is known at all times during the observation window. In passive tomography the control of the source needs to be relaxed in order to be able to take advantage of possible sources of opportunity passing within acoustic range from the receiver(s). Although passive tomography is very appealing for the ease of application, its practical implementation is extremely challenging and its full feasibility remains to be proved. BOAT represents a step towards a full demonstration of passive tomography.

This study reports the inversion results obtained on part of the data gathered during the INTIFANTE'00 sea trial, where a towed sound source emitting LFM's and noise sequences was used. The challenge is represented by the fact that during the various runs a priori knowledge about the source is progressively relaxed leading to a situation close to that encountered in passive tomography. In a first data set it was proved that a moving source at an unknown location emitting a deterministic unknown signal over a range-independent environment can be used for ocean tomography when the environ-

ment and the source position is progressively adapted through time. Estimates of the various environmental and geometrical parameters are consistent with expected values. In a second data set the same source was moving towards the array emitting a PRN signal over a range-dependent environment, representing a scenario close to a possible real passive tomography scenario. It was shown that also in this close-to-real scenario, both geometrical and environmental parameters were consistently estimated over time resulting in a high model fit indicating a potential for accurate inversion estimates. BOAT was proved to represent the tool of choice for accounting for the unknown geometrical and environmental parameters, inherent to passive tomography feasibility.

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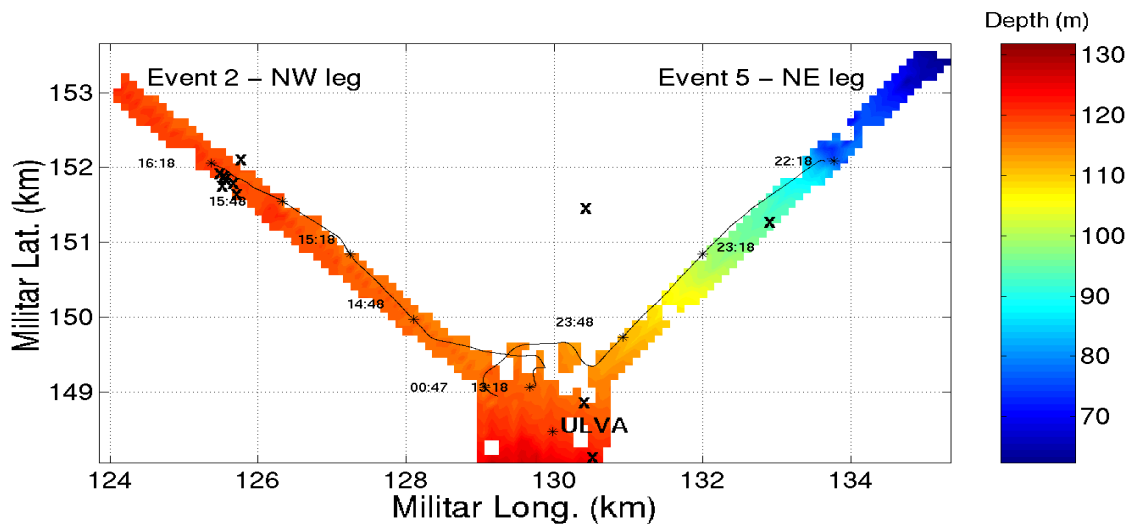


Figure 1: *INTIFANTE’00* sea trial site bathymetry with XBT locations (marked \times) and acoustic tracks for events 2 and 5.

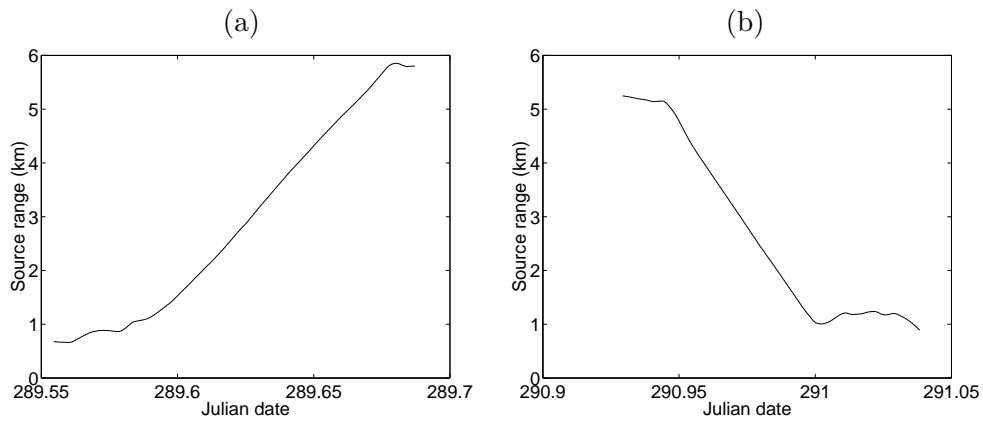


Figure 2: *Source - VLA receiver range vs. time for the NW-RI track (a) and the NE-RD track (b).*

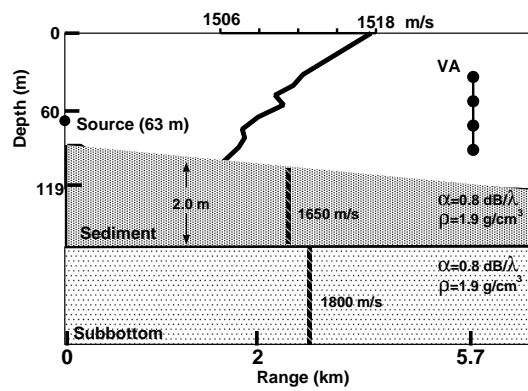


Figure 3: *Baseline environmental model for the NE range-dependent track.*

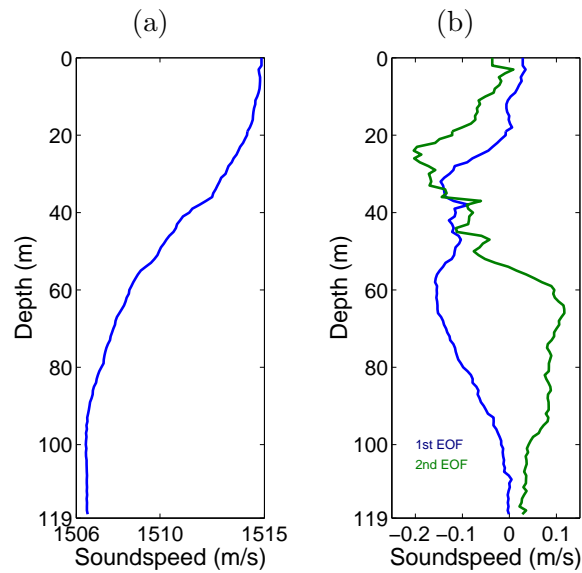


Figure 4: *XBT based data used for ocean sound speed estimation: mean sound speed profile (a) and empirical orthonormal functions (EOFs) (b).*

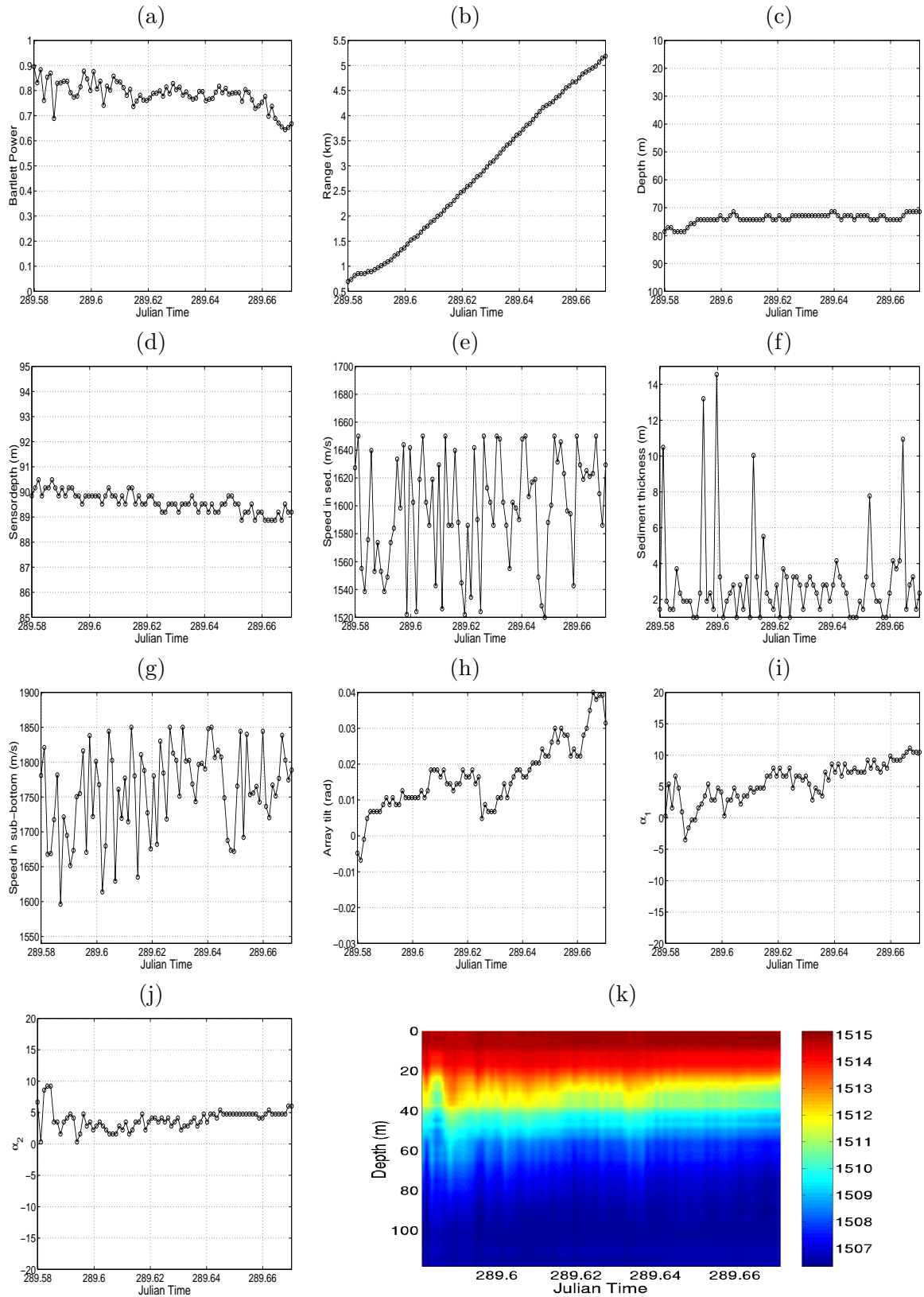


Figure 5: Focalization results for Event 2: Bartlett power (a), source range (b), source depth (c), receiver depth (d), sediment compressional speed (e), sediment thickness (f), sub-bottom compressional speed (g), VLA tilt (h), EOF coefficient 1 (i), EOF coefficient 2 (j) and reconstructed sound speed (k).

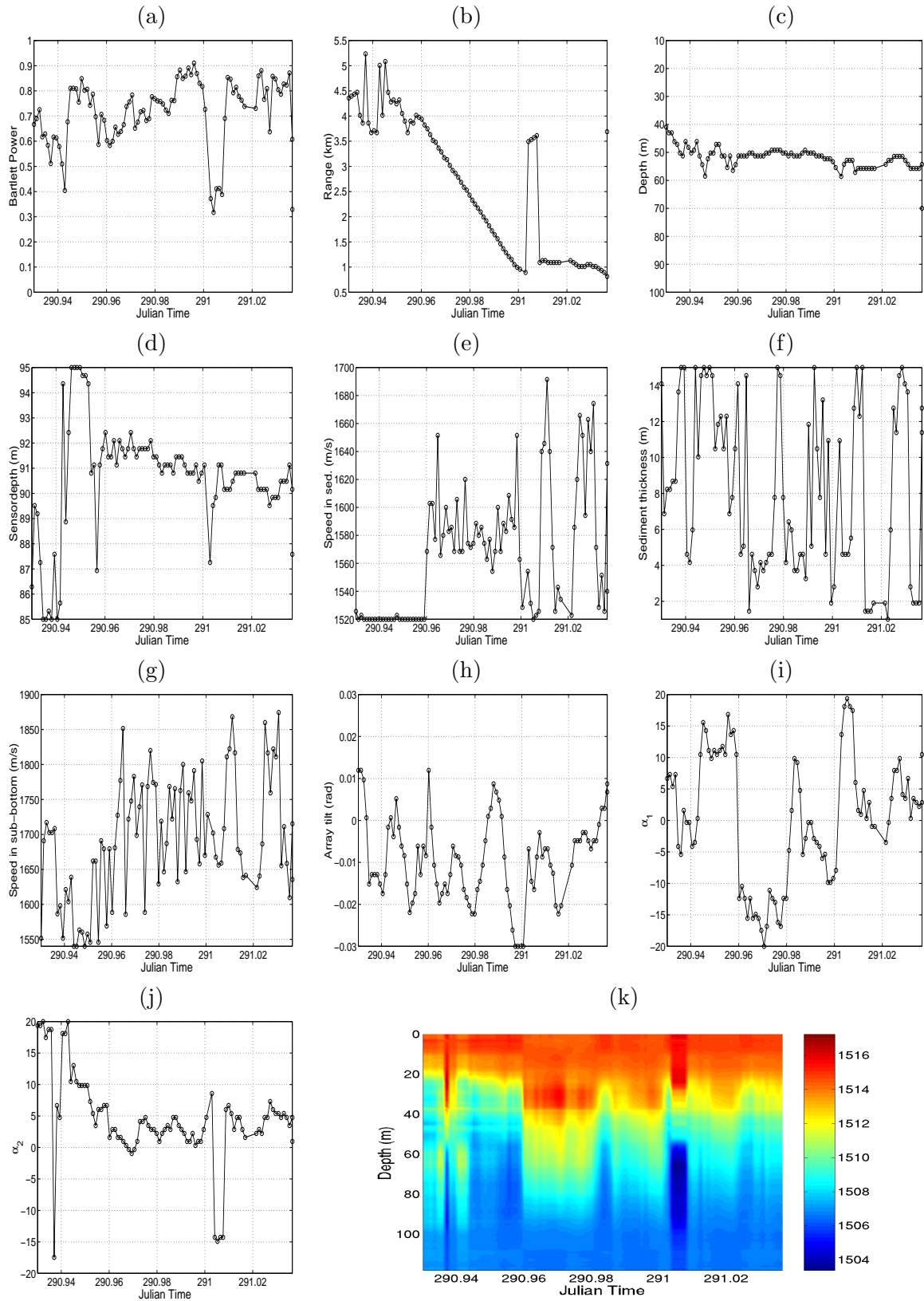


Figure 6: Focalization results for Event 5: Bartlett power (a), source range (b), source depth (c), receiver depth (d), sediment compressional speed (e), sediment thickness (f), sub-bottom compressional speed (g), VLA tilt (h), EOF coefficient 1 (i), EOF coefficient 2 (j) and reconstructed sound speed (k).