

1 **Ceramic enamels as new back contacts for Cu(In,Ga)Se₂ based photovoltaic tile**

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6
7 **Abstract**

8 In this work, we investigated the properties of silver and gold enamels as potential back
9 contacts for Cu(In,Ga)Se₂ (CIGS) solar cells. The enamels were deposited on ceramic
10 tiles by non-vacuum printing techniques. Thus, we are proposing a development of
11 integrated photovoltaic tile for the first time. We also explained the CIGS synthesis
12 procedure using co-precipitation of selenites precursors. To deposit the precursor
13 powders on the substrate, a doctor blade method is applied. The interface morphology
14 between ceramic tile, back contact, and CIGS absorber was studied as a critical factor
15 for the final solar cell performance. The thermal treatment effect on the back contact
16 properties was also reported.

17 Excellent compatibility between CIGS and gold layer was observed, keeping thickness
18 and chemical composition adequate for photovoltaic applications. The band gap energy
19 confirms assembly effectiveness. Unsatisfied results of silver diffusion towards CIGS
20 absorber were obtained when silver enamels were used.

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1. Introduction

Thin film technology is a desired alternative for preparing photovoltaic devices because of an enormous saving of costly materials and simplification of the manufacturing process. The low-cost potential of this technology is rooted by means of cheaper substrate applications, effective uses of raw materials and thinner coatings (ranging from 1.5 to 3 μm)^{1, 2}. In this sense, ceramic tiles emerge as good alternatives for substrate by reducing production costs and giving benefits to the final products. An advantage is a possibility to use higher temperature treatments, keeping intact material thermal stability. The photovoltaic (PV) incorporation in building constructions as an energy source by replacing of conventional building materials (as roof, skylights, or facades) makes them very attractive for so called Building Integrated Photovoltaics (BIPV)^{3, 4}. In addition, these systems can provide large areas of photovoltaic modules based on diverse absorbers.

Cu(In,Ga)Se₂ (CIGS) is an attractive absorber for thin film solar cells due to its unique optical and electrical properties⁵⁻⁷. CIGS technology has recorded 21.7% of efficiencies⁸. The typical CIGS solar cell is constituted for soda-lime glass substrate (3 mm), sputtered molybdenum back contact (800 nm), CIGS absorber layer (2 μm), chemical bath deposited CdS buffer layer (10-60 nm), sputtered zinc oxide (i:ZnO) or/and indium tin oxide (ITO) as window layer⁹. The use of vacuum-based technique for thin film deposition is a main handicap of this technology^{10, 11}. Covering at room temperature and atmospheric pressures stand out as an attractive alternative for the absorber layers¹²⁻¹⁷. Methods as doctor blade, spin coating, and dip-coating are very suitable for that purpose, being cost-effective ways of preparation. In this connection, the doctor blade technique is very desirable from an industrial point of view for large-scale production due to its simplicity and availability at many factories (e.g ceramic tile

47 industrial units)^{10, 18}. The doctor blade, also known as tape casting, is a processing
48 method for producing of thin films on large area surfaces with no waste of materials and
49 good layer uniformity. Commonly, this method involves spreading through a moving
50 blade onto a stationary substrate. There are three different type of doctor blade coating
51 devices in use: a knife, a rectangular frame and a spiral film applicator¹⁹. The gap size
52 of the blade governs the layer thickness. The micrometric precision of blade regulation
53 is the main inconvenient of this way of deposition that leads difficult precise depth
54 control. However, controlling coating parameters that influence to the film formation as
55 surface energy of the substrate, surface tension of the fluid, coating or blade speed, fluid
56 viscosity, density, and surface temperatures could solve this problem ^{20, 21}.

57 The soda-lime glass is probably the most used substrate in CIGS solar cell ²². Polymers
58 and metals are also investigated as alternative options ²³⁻²⁶. Polymers have appropriate
59 chemical inertness and do not react with selenium during the thermal treatment ²³. In
60 addition, these materials have a smoother surface and humidity barrier. However, they
61 have low thermal stability to withstand thermal selenization treatment.

62 In contrast, metals have better thermal stability than polymers, but a barrier layer is
63 required to block impurities that can diffuse toward the absorber layer. Concerning these
64 drawbacks, the ceramics are good alternative substrates. The principal selection criteria
65 that ceramics must fulfill are: compatible thermal expansion coefficient (CTE) ($\sim 7 \cdot 10^{-6}$
66 K^{-1}), excellent thermal ($T > 600 \text{ }^\circ\text{C}$) and chemical resistivity and being suitable for
67 industrial uses in terms of costs and facilities. The CTE of ceramics is similar to the
68 CTE of CIGS ($8-11 \cdot 10^{-6} \text{ K}^{-1}$) ²³ and is relatively cheap product. Thus, ceramic tiles for
69 substrates offer new possibilities for solar cells and its integration in urban areas
70 (BIPV).

71 Commonly, the back contact layer is made of metal. Its fabrication is well studied part of
72 materials engineering field. The main requirements for a good back contact for CIGS
73 solar cells are: inertness, smooth surface, good electrical properties (low contact
74 resistance), good thermal stability and cost, and it should act as diffusion barrier. The
75 surface morphology plays a key role in the final electrical properties. The back contact
76 executed as a barrier acts as impurities diffusion membrane between the substrate and
77 the absorber²³. Variety of metal/ CIGS contacts have been investigated, including (Cu,
78 Ni, Al, Mo, Pt)²⁷⁻²⁹, Ag³⁰, Au³¹ and others (W, Cr, Ta, Nb, V, Ti, Mn)^{32, 33} with limited
79 success. The most applied metal is molybdenum (Mo). Despite of that, Mo deposition
80 also presents certain problems related to bad substrate adhesion and fast metal
81 oxidation³³⁻³⁶. The back contacts used for high- efficiency devices, is typically deposited
82 by direct current (dc) sputtering^{37, 38}, evaporation^{39, 40} or chemical vapour deposition
83 (CVD)⁴¹ that increase the final value of the cell.

84 Although CIGS semiconductor has been studied for several decades, rather limited
85 information has been reported in literature on metal morphology effects on the back
86 contact resistance.

87 The paper reports a development of new back contacts for CIGS solar cells. Substrate
88 made by common porcelain stoneware ceramic tile is used. The tile was previously
89 covered with industrial glazes containing gold or silver in its compositions. The glaze,
90 situated between the CIGS absorber and the substrate, provides chemical stability,
91 inertness and roughness reduction. The glass nature of the enamels simulates flat
92 surface with no porosity. The metal (gold or silver) content allows it to operate as a
93 metal back contact. Non-vacuum, solution-based, and large-scale way of deposition,
94 called ink printing, of the enamels for reducing materials and costs is suggested. In
95 addition, simple way of preparation using co-precipitation route for the CIGS absorber

96 is also reported. The developed powders were deposited on the substrate by doctor
97 blade technique. The morphological properties in the interface ceramic tile/ back
98 contact/CIGS were investigated as crucial aspect for the final solar cell performance.
99 Band gap energy was measured for the optimal sample testing the assembly
100 effectiveness.

101

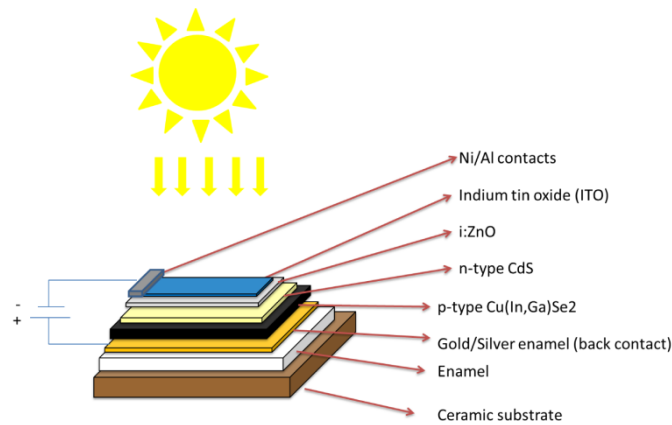
102 **2. Experimental details**

103 **2.1 Support preparation**

104 Porcelain stoneware substrates (5 mm thickness) were made by industrial method of
105 preparation using kaolinitic clay, feldspar and feldspathic sand. The pastes (with
106 average chemical composition (oxide weights %): 60-70 SiO₂, 18-20Al₂O₃, 1.5-3 K₂O,
107 3.5- 4.5 Na₂O, 1-2 others oxides, were prepared by pressing and further sintering in a
108 conventional kiln.

109 Industrial frit developed for the enamel applied in the solar cell contains the following
110 average composition (oxide weights %): 55-65 SiO₂, 10-30 Al₂O₃, 0.5-5 Na₂O-K₂O, 13
111 -17 MgO-CaO, 10-20 others. The frits were applied in order to ensure low porosity,
112 impermeability and to provide chemical stability and roughness reduction simulating
113 thereby glass surface.

114 The gold dye over the frit was deposited by ink-jet printing in non-vacuum conditions
115 for obtaining gold conductive enamel with a thickness ~ 200 nm. The same procedure
116 was applied for the silver enamel (~ 2.50 μm thickness), but the silver dye was
117 deposited by screen printing technique. These coating methodology, ink-jet and screen-
118 printing, were selected to determine their effectiveness. They achieved different layer
119 depths and morphologies that may influence to the device properties. On Figure 1
120 schematic design of the photovoltaic ceramic tile is shown.



121

122 **Figure 1.** Schematic layout of a Cu(InGa)Se₂-based photovoltaic ceramic tile.

123

124 2.2 CIGS synthesis and deposition

125 CuIn_{0.7}Ga_{0.3}Se₂ solid solution was synthesized using co-precipitation route of metal
 126 selenite precursors, keeping atomic ratio of Cu/(In + Ga) = 0.92 and Ga/(In+Ga) = 0.3¹,
 127 ⁴². The resulting CIGS powder was further mixed with triethanolamine (TEA, 99%,
 128 Riedel-de Haën) and ethanol (C₂H₅OH, 99.9%, Sharlau) to form slurry that was
 129 deposited on ceramic substrate by manual knife doctor blade method. The slurry
 130 viscosity and the blade gap mainly govern the thickness precision.

131 The obtained layer was pre-heated on a hot plate at 400°C for 2 min to remove partially
 132 the solvent and to encourage further precursor decomposition. Finally, the CIGS films
 133 were selenized under reducing atmosphere (5% H₂/ 95% N₂) in a tubular furnace. The
 134 applied thermal cycle corresponds to heating velocity rate of 20 °C/min up to maximum
 135 temperature of: 200 °C (sample A); 350 °C (sample B); 450 °C (sample C); 500 °C
 136 (sample D) and 550 °C (sample E). Free cooling and no soaking time were applied.

137

138 2.3 Characterization techniques

139 Crystal structure of powders and films was monitored by X-ray diffraction (XRD) using
 140 a D4 Endeavor, Bruker-AXS equipped with a Cu K α radiation source. Data were

141 collected by step-scanning from 10° to 80° with step size of 0.05° 2θ and 1 s counting
142 time per step.

143 The particle sizes were quantitatively evaluated from the XRD data using the Debye-
144 Scherrer equation⁴³,

$$145 \quad D = \frac{k\lambda}{\beta \cos \theta} \quad (1)$$

146 where k is Scherrer constant (0.89), λ the X-ray wavelength (0.15405 nm), β the peak
147 width of half-maximum, and θ is the Bragg diffraction angle.

148 Scanning Electron Microscopy (SEM) model JEOL 7001F attached with an energy
149 dispersive X-ray analysis (EDX) was employed to study the morphology and elemental
150 composition of the films. The layer thickness was determined from cross section
151 micrographs. The glaze surfaces were studied by Atomic Force Microscope (AFM) with
152 a JSPM-5200 JEOL Scanning Probe Microscope operating in contact approach.
153 Adhesion between back contact layers and support was measured using laboratory test
154 method by applying and removing tape and scratching of the surface. This method is
155 used to establish whether the adhesion of a coating to a substrate is at a generally
156 adequate level. The films electrical resistance was measured using a digital multimeter
157 (Volt-Ohm meter).

158 Optical properties and band gap energy of the CIGS layer was conducted by UV-Vis-
159 NIR spectroscopy in the wavelength range 200-1200 nm (step size 1 nm) using Cary
160 500 Scan Varian spectrophotometer. The absorption spectra were obtained applying
161 BaSO₄ integrating sphere as a white reference material.

162

163 **3. Results and Discussion**

164 **3.1 Ceramic substrate**

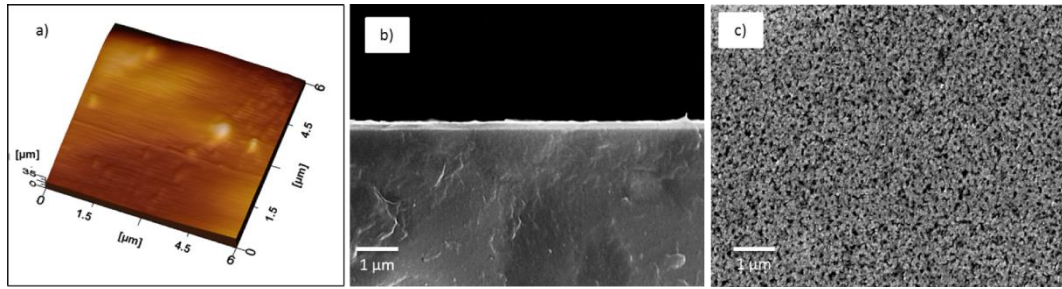
165 Physical characteristics of the ceramic body were analyzed. The obtained tiles density
166 was 2.056 g/cm^3 after thermal treatment at $1200 \text{ }^\circ\text{C}$ (data not shown). The vitrification
167 plot displayed linear contraction of 7.56% and water absorption of 0.98% at $1165 \text{ }^\circ\text{C}$.
168 These values remained constant even at $1190 \text{ }^\circ\text{C}$, where the water absorption decreases
169 up to 0% (data not shown).

170

171 **3.2 Gold enamel**

172 Figure 2(a) displays AFM images of the Au enamel layer. Rather smooth and regular
173 surface of polycrystalline gold enamel is observed. The average roughness is about 3
174 nm, very suitable for layer applications. There are some isolated grains disperse on the
175 surface, but this fact does not harm layer functionality. The gold cover is dense and
176 well-adhered to the ceramic substrate (Fig. 2b). The estimated, from the cross-section
177 micrograph, layer thickness is $\sim 200 \text{ nm}$ (Fig. 2b). Homogeneous grain distribution of
178 particles with 50 nm average dimensions (Fig. 2c) suggests excellent coating properties.
179 Figure 3 displays the X-ray diffraction pattern of Au layer before CIGS deposition. The
180 sample reveals various diffraction peaks related to SiO_2 (quartz, JCPDS card, file No
181 01-083-2471) at 27.1° (2θ) and SiO_2 (cristobalite, JCPDS card, file No 01-076-0939) at
182 21.8° and 35.8° (2θ). The reflections indexed with (1,1,1), (2,0,0), (2,2,0) and (3,1,1)
183 belong to Au (JCPDS card, file No 01-1172). The SiO_2 compounds in the pattern are
184 coming from the glaze layer below. This demonstrates that the Au layer is very thin that
185 may affect to the device properties.

186



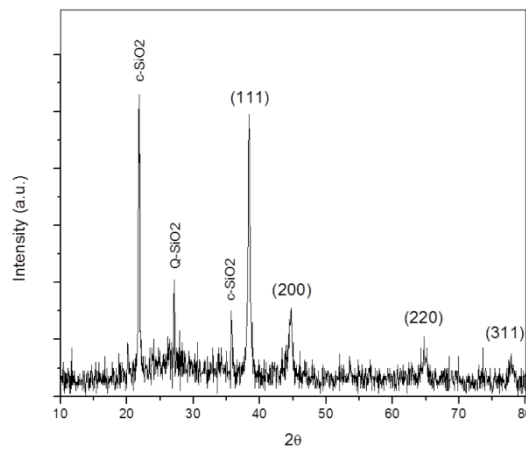
187

188 **Figure 2.** Surface morphology of Au thin film: a) AFM surface image; b) SEM cross-
 189 section micrograph of Au layer and c) SEM micrograph of Au surface.

190

191 The Au particle sizes were quantitatively evaluated from the XRD data (Fig. 3) using
 192 the Debye-Scherrer equation (1). From the (1,1,1), (2,0,0) and (2,2,0) d-spacing's
 193 crystallite dimensions were calculated. The particles measure from 20 nm to 50 nm. The
 194 result fits well with the microscope observations (Fig. 2c).

195



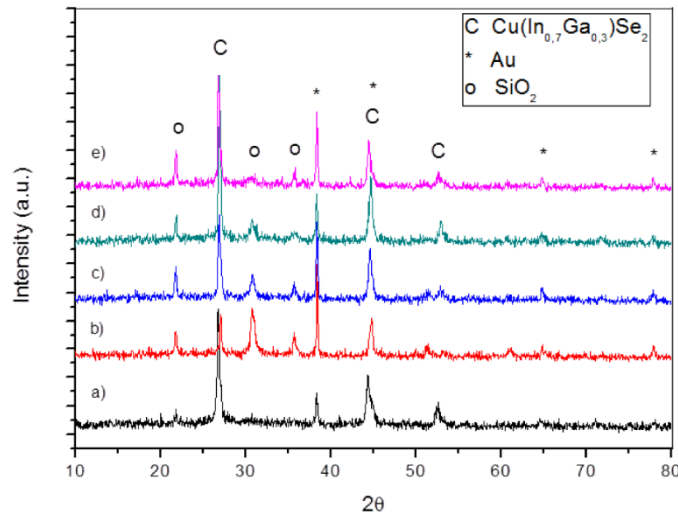
196

197 **Figure 3.** X-ray diffraction pattern of Au layer before CIGS deposition.

198

199 X-ray diffractograms of samples A, B, C, D and E after CIGS thermal treatment are
 200 shown in Figure 4. The main diffraction peaks could be assigned to $\text{CuIn}_{0.7}\text{Ga}_{0.3}\text{Se}_2$
 201 crystalline phase (JCPDS card, file No 35-1102). It can be notice that reflection
 202 intensities increase with temperature changes from 200° to 550 °C. Additional peaks at

203 $2\theta = 38.3, 64.9, 44.6$ and 77° are also found. These reflections could be associated to Au
 204 (JCPDS card, file No 01-1172). Diffraction peaks at $2\theta = 21.8, 30.8$ and 35.7°
 205 corresponds to SiO_2 (JCDPS card, file No 76-0939) and are coming from the glaze. No
 206 secondary phases during the CIGS formation are detected.
 207



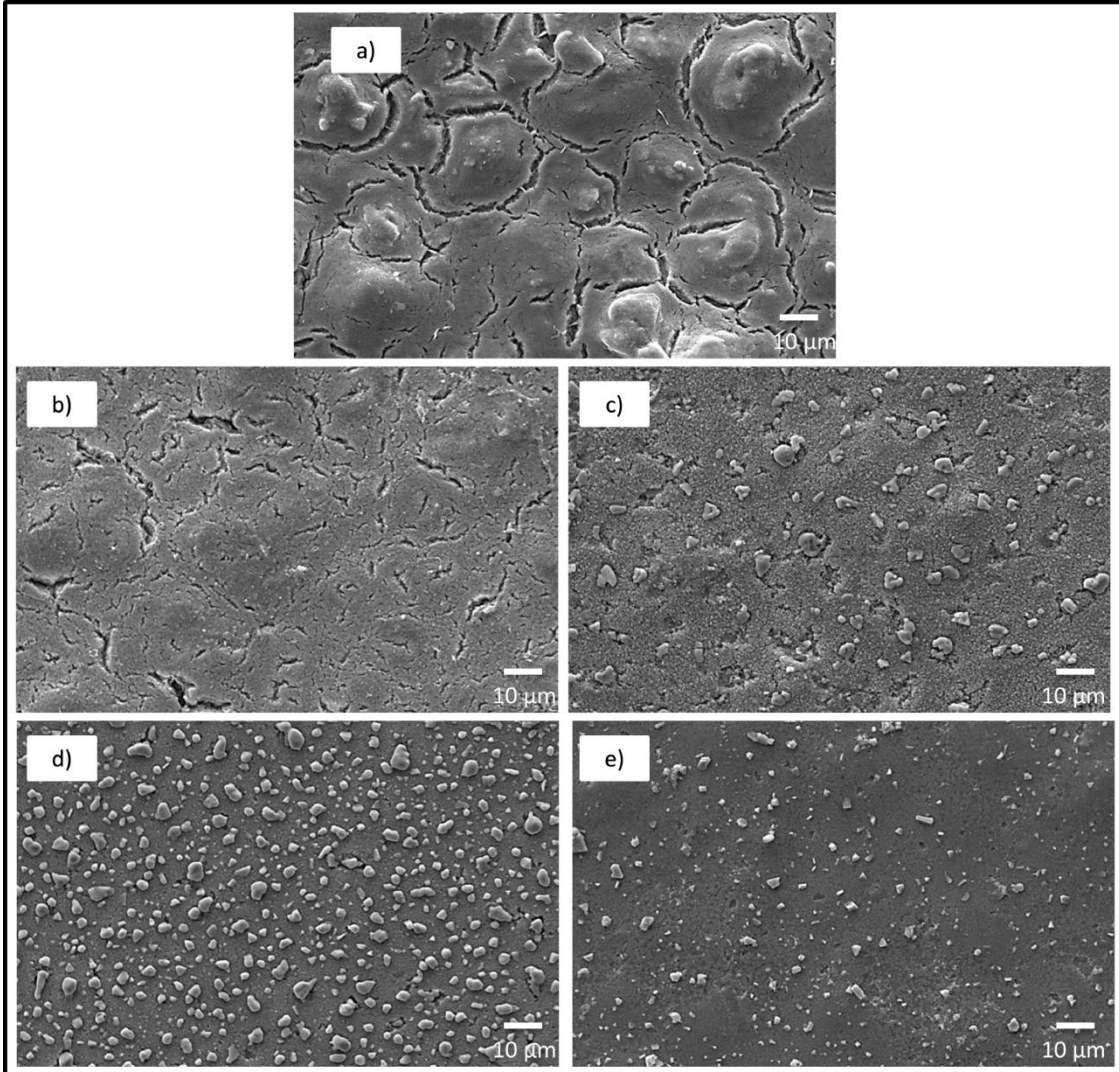
208
 209 **Figure 4.** XRD of CIGS films after thermal treatment at: a) 200 °C, b) 350 °C, c) 450
 210 °C, d) 500 °C and e) 550 °C.

211
 212 Figure 5 shows surface SEM images of CIGS films selenized at different temperatures.
 213 The film crystallinity rise with temperature according to XRD results (Fig. 4). Surface
 214 (Fig. 5a and 5b) and cross-section view (Fig. 6a and 6b) of the films obtained at low
 215 temperatures shows cracks and pinholes. This result suggests unstuck to the substrate
 216 coating. In order to improve the layer, higher temperatures were applied. After
 217 treatment, the samples (Fig. 5c, 5d and 5e) show granular surface morphology that
 218 decreases with sintering procedure. Finally, well-sintered dense coating with some
 219 surface crystals at 500°C (Fig. 5d) is detected. The gold layer thickness decrease from
 220 300 nm (for sample heated at 200°C) to 160 nm (for sample at 550°C) due to precursor's
 221 decomposition during calcination (Fig. 6). The sample calcined at 500°C displays lack

222 of surface defects, good adhesion to the ceramic substrate and dense and microstructure.

223 As a result, it was selected among other samples as optimum.

224



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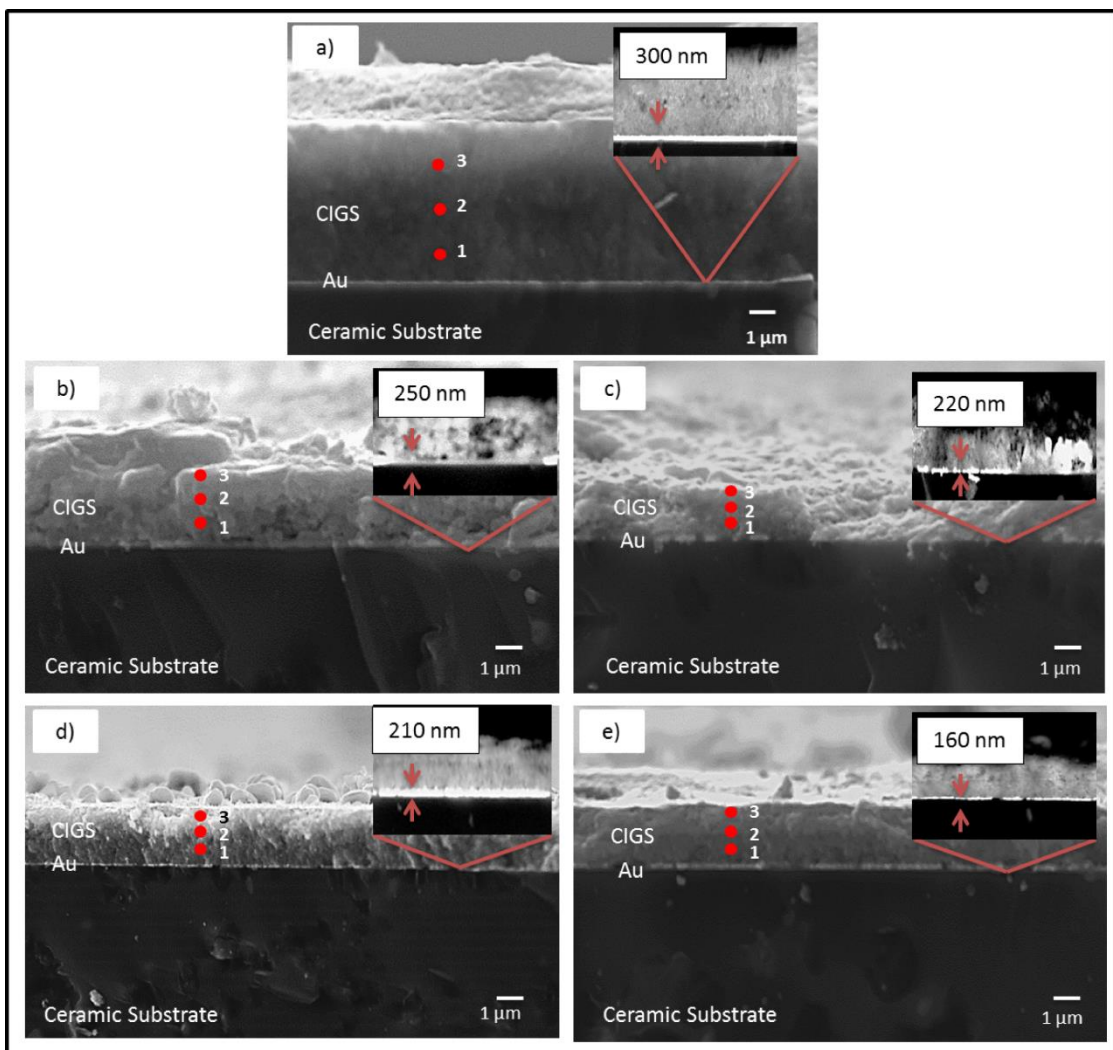
226 **Figure 5.** Surface micrographs of samples treated at: a) 200 °C, b) 350 °C, c) 450 °C, d)
227 500 °C and e) 550 °C.

228

229 The film elemental composition was determined by energy-dispersive X-ray analysis
230 (EDX). Dotted lines in Figure 6 indicate the semi-quantitative analysis (atomic %) of
231 CIGS stoichiometry. The elemental concentration is indicated with dots along the
232 depth in three different areas: bottom (1), middle (2) and top (3). The results in Table 1

233 prove a slight Au diffusion towards the CIGS absorber for samples (b), (c), (d) and (e).
234 When temperatures up the Au diffusion increase and layer thickness decrease (Fig. 6 a-
235 e). Nevertheless, the Au diffusion does not have an influence on the optical properties of
236 the CIGS absorber and on the electrical resistance of the back contact. The Au layer still
237 had electrical conductivity that was checked by Multimeter. The optical response is
238 discussed hereafter.

239



240

241 **Figure 6.** Cross-sections micrographs of samples treated at: a) 200 °C, b) 350 °C, c) 450
242 °C, d) 500 °C and e) 550 °C.

243

244 The CIGS sample heated at 500°C presents homogeneous chemical composition (Table
 245 1 sample d). The extra Cu amount is according to the initial stoichiometry. At lower
 246 temperatures (samples a, b and c) selenium losses are detected. Unexpected more
 247 heterogeneous composition for sample (e) is observed despite of the applied higher
 248 temperature.

249

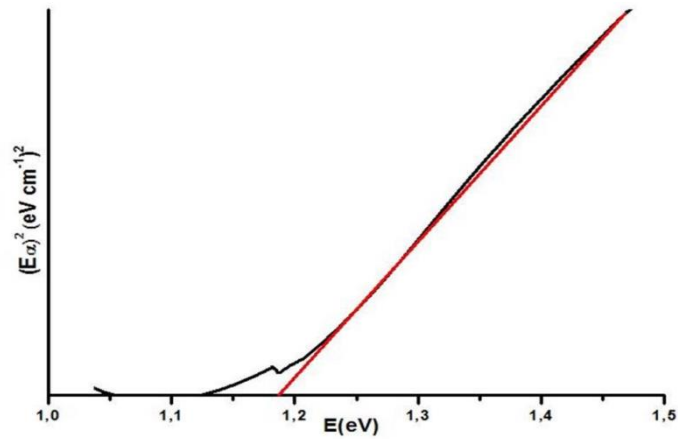
250 **Table 1.** EDX analysis (at %) and metal ratio of sample treated at: a) 200 °C, b) 350 °C,
 251 c) 450 °C, d) 500 °C and e) 550 °C.

Sample	Point of analysis	Cu	In	Ga	Se	Au	Cu/In+Ga	Ga/In+Ga
a)	1	29.82	19.85	7.60	42.73	-	1.08	0.27
	2	28.40	19.76	8.17	43.67	-	1.01	0.29
	3	29.67	19.66	8.95	41.72	-	1.03	0.31
b)	1	22.95	49.06	11.68	15.38	0.93	0.37	0.19
	2	15.06	62.98	13.88	8.08	-	0.19	0.18
	3	13.05	65.82	12.63	8.50	-	0.16	0.16
c)	1	30.63	31.87	12.44	21.04	4.02	0.69	0.28
	2	41.78	19.53	6.60	30.08	2.01	1.59	0.25
	3	32.86	22.72	8.23	34.95	1.24	1.06	0.26
d)	1	22.45	17.51	5.27	51.42	3.35	0.98	0.23
	2	24.48	16.70	5.78	52.05	0.99	1.08	0.26
	3	25.86	17.46	6.31	49.44	0.93	1.08	0.27
e)	1	34.43	19.68	3.89	35.23	6.77	1.46	0.16
	2	33.48	21.07	4.51	37.03	3.91	1.30	0.17
	3	24.71	21.10	15.51	37.49	1.19	0.67	0.42

252

253 Band gap energy was measured only for sample “d” selected as optimum. Figure 7
 254 shows band gap of approximately 1.18 eV that fits with the value corresponding to
 255 $\text{Cu}(\text{In}_{1-x}\text{Ga}_x)\text{Se}_2$ solid solution⁴⁴. The result indicates that the detected gold diffusion
 256 does not concern the optical properties of the final device.

257



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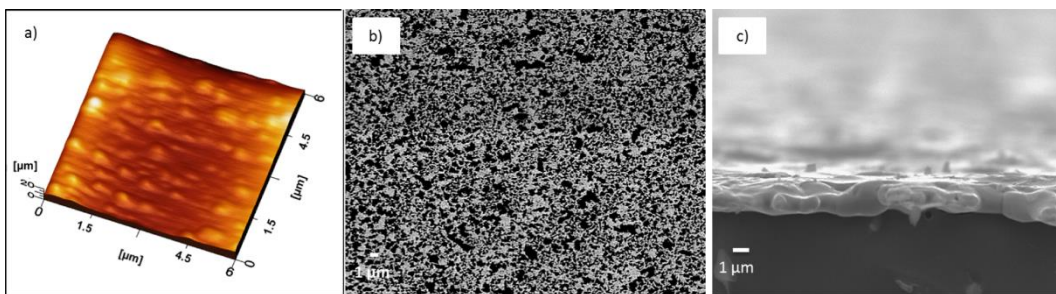
259 **Figure 7.** Plot of $(\alpha hv)^2$ as function of energy for CIGS sample “d”.

260

261 3.2.1 Silver enamel

262 Figure 8 (a) display AFM images of the Ag glazed layer. Polycrystalline silver glaze
 263 with heterogeneous and roughness surface is observed. The average roughness is about
 264 14 nm, suitable for layer applications. However, different embedded grains on the
 265 surface are detected.

266



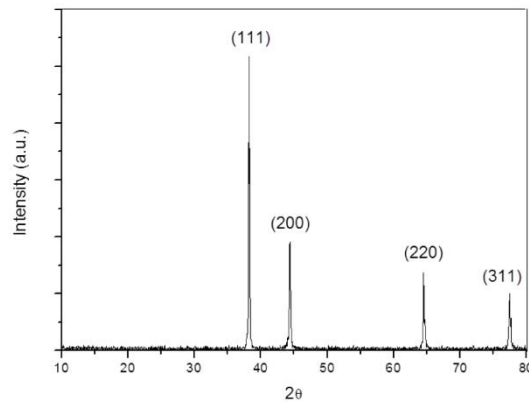
267

268 **Figure 8.** Surface morphology of Ag thin film: a) AFM surface image; b) SEM
 269 micrograph of Ag surface and c) SEM micrograph of cross-section of Ag layer.

270

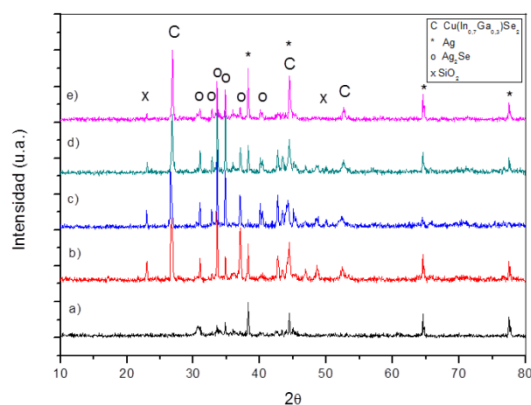
271 Well-adhered to the ceramic substrate silver layer is assumed from Figure 8b and 8c.
 272 Layer thickness $\geq 2 \mu\text{m}$ is deduced from the cross-section image in Figure 8c.
 273 Heterogeneous grain distribution with sizes from 3nm to 500 nm is detected. To

274 confirm the particle dimensions, X-ray diffraction of the Ag layer before CIGS
275 deposition was done (Fig. 9). The calculation using equation (1) of (1,1,1), (2,0,0) and
276 (2,2,0) exposes crystal sizes corresponding to 176 nm, 88 nm and 196 nm that are
277 agreed with the range (3-500 nm) discussed before.
278



279
280 **Figure 9.** XRD pattern of Ag layer before CIGS deposition.

281
282 X-ray diffraction spectra of CIGS films treated at different condition are exposed in
283 Figure 10. It can be emphasized that CIGS compound crystallizes even at 350°C (Fig.
284 10b). The main reflections could be assigned to the $\text{CuIn}_{0.7}\text{Ga}_{0.3}\text{Se}_2$ (JCPDS card, file
285 No 35-1102). Peaks intensities increase with temperature (Fig. 10b-e). Reflections at 2θ
286 = 38.2, 44.4, 64.6 and 77.5° are related to Ag (JCPDS card, file No 01-087-0718).
287 Secondary phase of Ag_2Se compound ($2\theta = 30.99, 32.78, 33.56, 34.82, 37.04$ and
288 42.73°) (JCPDS card, file No 00-020-1063) is also distinguished. This result concludes
289 that Ag diffuse towards the absorber layer (Table 2). Diffraction peaks at $2\theta = 21.8,$
290 30.8 and 35.7° is assigned to SiO_2 (JCPDS card, file No 76-0939).
291



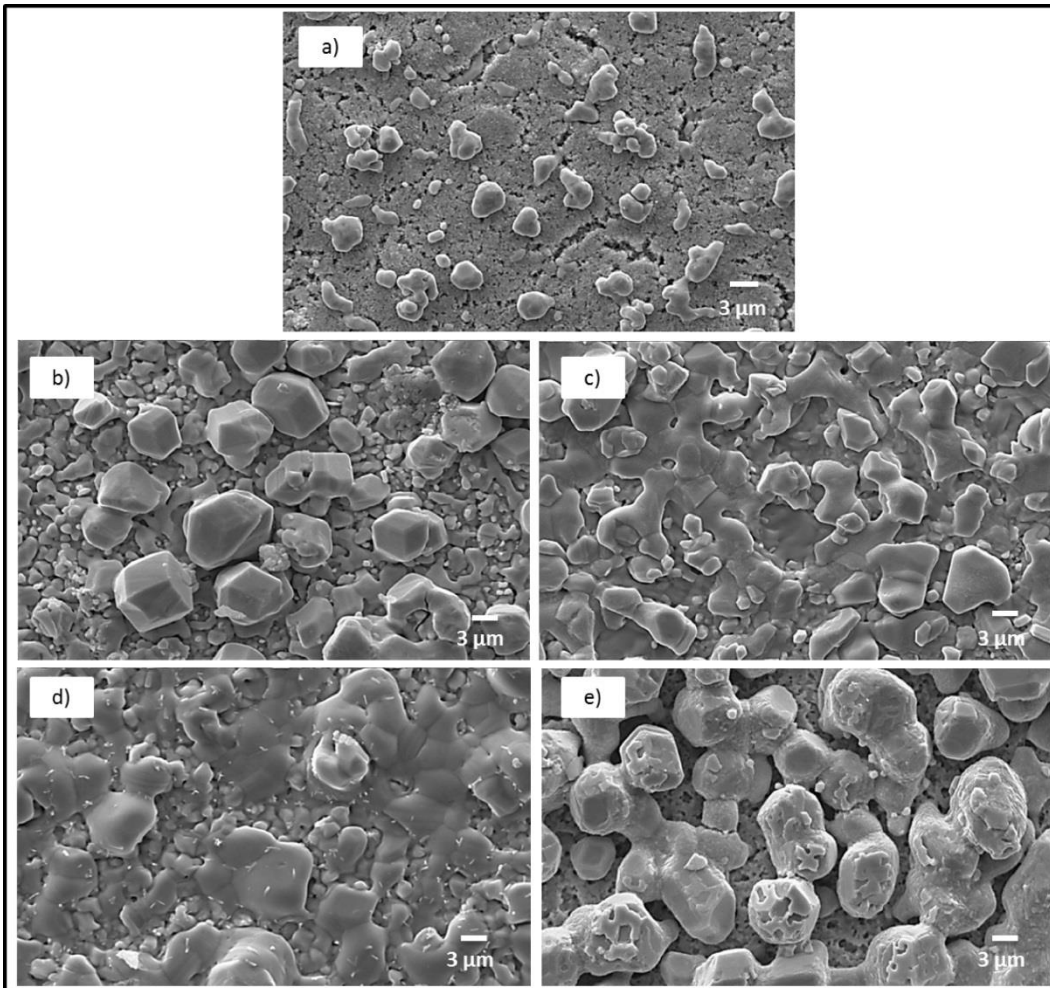
292

293 **Figure 10.** XRD of films treated at temperatures: a) 200 °C, b) 350 °C, c) 450 °C, d) 500
 294 °C and e) 550 °C.

295

296 SEM surface images of CIGS films treated at different temperatures are exposed in
 297 Figure 11. Granular surface morphology and increasing with temperature grains can be
 298 observed. Sintering processes at higher temperatures are deduced (Fig. 11 c and d). The
 299 cross-section micrographs on Figure 12 show unstuck to the substrate coatings for all
 300 temperatures. This result could be ascribed to the way of deposition (e.g screen
 301 printing). Holes and irregular morphology for all samples is remarked. The layer's
 302 elemental composition (Table 2) confirms silver diffusion and heterogeneities. The
 303 silver enamel is unstable under thermal treatment. The layer results non-ohmic. Any
 304 further characterizations for the Ag system were avoided.

305

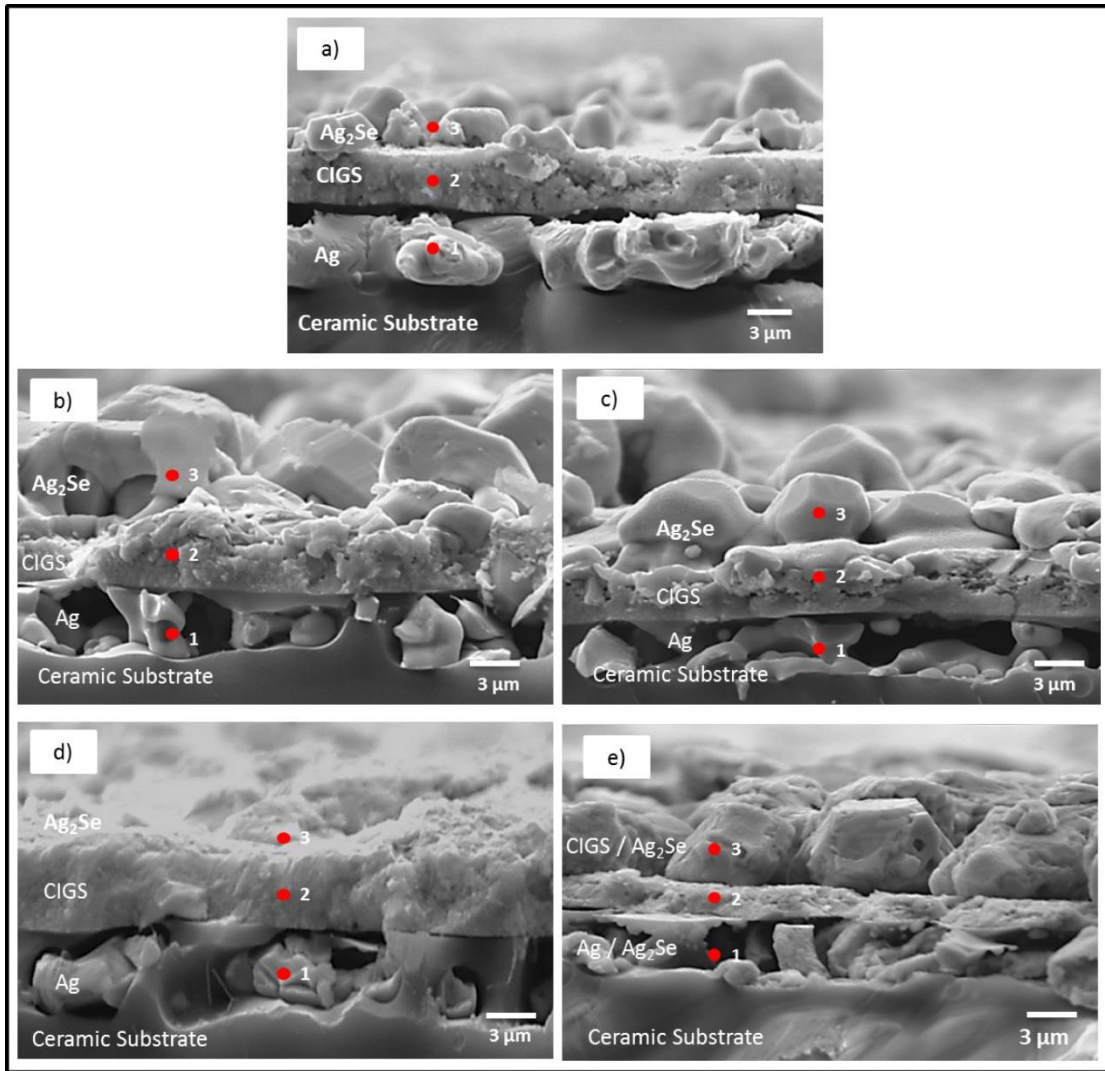


306

307 **Figure 11.** SEM surface images of samples heated at: a) 200 °C, b) 350 °C, c) 450 °C, d)

308 500 °C and e) 550 °C.

309



310

311 **Figure 12.** SEM cross-section images of samples heated at: a) 200 °C, b) 350 °C, c) 450
 312 °C, d) 500 °C and e) 550 °C.

313

314 **Table 2.** EDX analysis (atomic %) and metal ratio of sample heated at: a) 200 °C, b)
 315 350 °C, c) 450 °C, d) 500 °C and e) 550 °C.

Sample	Point of analysis	Cu (at%)	In (at%)	Ga (at%)	Se (at%)	Ag (at%)	Cu/In+Ga	Ga/In+Ga
a)	1	-	-	-	-	100	-	-
	2	20.25	10.87	4.49	17.03	47.36	1.32	0.29
	3	-	-	-	27.31	72.69	-	-
b)	1	-	-	-	30.22	69.78	-	-
	2	22.49	13.26	2.08	30.67	31.5	1.46	0.14
	3	-	-	-	32.8	67.2	-	-
c)	1	-	-	-	27.74	72.26	-	-
	2	7.35	4.5	1.11	37.16	49.88	1.31	0.19
	3	-	-	-	30.05	69.95	-	-

	1	-	-	-	10.76	89.24	-	-
d)	2	16.05	15.69	3.76	45.9	18.6	0.83	0.20
	3	-	-	-	30.30	69.70	-	-
	1	-	-	-	28.51	71.49	-	-
e)	2	12.74	12.47	6.89	43.72	24.18	0.66	0.35
	3	20.52	17.93	1.19	45.58	14.78	1.07	0.10

316

317 **4. Conclusions**

318 Gold and silver enamels were developed as potential back contacts for CIGS solar cells.

319 The enamels were successfully deposited on ceramic substrates making integrated
 320 photovoltaic tiles for the first time. The substrates evidence lack of porosity, mechanical
 321 and chemical resistance, and low linear contraction. Different methods of enamel
 322 deposition, ink-jet and screen-printing, were applied. The ink-jet proves better
 323 effectiveness than screen-printing.

324 Non-vacuum routes for CIGS synthesis (co-precipitation) and deposition (doctor blade)
 325 were used. The co-precipitation of selenite precursors results very successful obtaining
 326 $\text{CuIn}_{0.7}\text{Ga}_{0.3}\text{Se}_2$ solid solution. Doctor blade technique achieved well-adhered, dense,
 327 and homogeneous layers with adequate thickness.

328 Excellent compatibility between CIGS and gold coating was obtained keeping layer
 329 width and chemical composition adequate for photovoltaic applications. The band gap
 330 measurement confirms the assembly effectiveness.

331 In contrast, silver diffusion leading coating separation was achieved for the silver glaze.
 332 The Ag layer results non-ohmic and therefore the back contact unusable.

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