

# **On Robust Fault Detection for Precision Mechatronics**

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# **On Robust Fault Detection for Precision Mechatronics**

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# 1 Background

Rising market demands for computer chips necessitate the continuous operation of high-tech production equipment. Downtime due to unexpected faults has impact on uptime having negative financial consequences. To minimize down-time, industry is shifting towards predictive maintenance tools by exploiting fault diagnosis systems [1]. This work focuses on solving the *fault detection* (FD) system design problem for uncertain closed-loop systems, which builds the core for diagnostic systems.

# 2 Problem formulation

Consider the uncertain closed-loop controlled system with augmented FD system in Fig. 1. The FD system design consists of two steps; 1) the design of  $(M_u(s), N_u(s)) \in \mathscr{RH}_{\infty}$ and subsequently 2) the design of  $R(s) \in \mathscr{RH}_{\infty}$ . While  $M_u$ and  $N_u$  focus on minimizing the impact of r for the case without uncertainty, i.e.,  $\Delta = 0$ , the post-filter R aims at maximizing the sensitivity to faults f and minimize the effect of uncertainty  $\Delta$  and disturbances d into the residual  $\varepsilon$ . Provided that the residual dynamics is described by

$$\boldsymbol{\varepsilon} = \boldsymbol{R}(s)T_{\tilde{\boldsymbol{\varepsilon}},rd}(s,\Delta) \begin{bmatrix} r\\ d \end{bmatrix} + \boldsymbol{R}(s)T_{\tilde{\boldsymbol{\varepsilon}}f}(s,\Delta)f, \tag{1}$$

the optimization problem is to find post-filter R(s) in (1) such that  $||R(s)T_{\tilde{e},rd}(s,\Delta)||_{\infty} \leq \gamma$  for all  $\Delta \in \mathbf{\Delta}$ , and perfor-



**Figure 1:** General uncertain closed-loop FD configuration, with  $G_u(s, \Delta)$  the uncertain plant model of the prototype wafer stage that was used for synthesis.

mance index  $J_{-\infty}(R)$  is maximized, that is,

$$\sup_{R(s)\in\mathscr{RH}_{\infty}} J_{-/\infty}(R) = \sup_{R(s)\in\mathscr{RH}_{\infty}} \frac{\|R(s)T_{\tilde{\mathcal{E}}f}(s,\Delta)\|_{-}}{\|R(s)T_{\tilde{\mathcal{E}},rd}(s,\Delta)\|_{\infty}}.$$
 (2)

# **3** Approach

The multiobjective optimization problem in (2) is solved in two steps. First, filters  $M_u(s)$  and  $N_u(s)$  are obtained by applying a left coprime factorization to the nominal plant, i.e.,  $G_u(s,0) = M_u^{-1}(s)N_u(s)$ . Second, a worst-case overbound of uncertain disturbance transfer function matrix  $T_{\bar{\varepsilon},rd}(s,\Delta)$ is found. This allows to solve problem (2) with a single Riccati equation, giving the optimal post-filter R(s) in view of (2) [2].

# 4 Results and Outlook

The approach is experimentally validated on a prototype wafer stage as shown in Fig. 1. It is shown that the residual signal only exceeds the detection threshold  $\gamma$  if a fault is present in the system, while being robust to the effects of model uncertainty and disturbances, as is shown in Fig. 2. A next step is to extend this solution to optimally solve the *fault detection and isolation* problem.



**Figure 2:** Time response of a residual in (—) together with the detection threshold  $\gamma$  shown in (—). The faults are shown in (—) and (…). Indeed, the residual remains within the bound if no fault is acting on the system.

#### References

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