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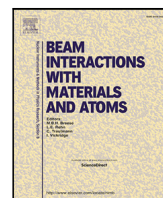
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## Increasing the rate capability for the cryogenic stopping cell of the FRS Ion Catcher

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### ABSTRACT

At the FRS Ion Catcher (FRS-IC), projectile and fission fragments are produced at relativistic energies, separated in-flight, energy-bunched, slowed down, and thermalized in the ultra-pure helium gas-filled cryogenic stopping cell (CSC). Thermalized nuclei are extracted from the CSC using a combination of DC and RF electric fields and gas flow. This CSC also serves as the prototype for the CSC of the Super-FRS, where exotic nuclei will be produced at unprecedented rates making it possible to go towards the extremes of the nuclear chart. Therefore, it is essential to efficiently extract thermalized exotic nuclei from the CSC under high beam rate conditions, in order to use the rare exotic nuclei, which come as cocktail beams. The dependence of the extraction efficiency on the intensity of the impinging beam into the CSC was studied with a primary beam of  $^{238}\text{U}$  and its fragments. Tests were done with two different versions of the DC electrode structure inside the cryogenic chamber, the standard 1 m long and a short 0.5 m long DC electrode systems. In contrast to the rate capability of  $10^4$  ions/s with the long DC electrode system, results show no extraction efficiency loss up to the rate of  $2 \times 10^5$  ions/s with the new short DC electrode. This order of magnitude increase of the rate capability paves the way for new experiments at the FRS-IC, including studies of exotic nuclei with in-cell multi-nucleon transfer reactions. The results further validate the design concept of the CSC of the Super-FRS, which was developed to effectively manage beams of even higher intensities.

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## 1. Introduction

With the FRS Ion Catcher (FRS-IC) [1,2], high-precision experiments of thermalized exotic nuclei are performed at the final focus of the symmetric branch of the in-flight fragment separator (FRS) [3] at the GSI Helmholtz Center for Heavy Ion Research, Darmstadt, Germany. The FRS-IC consists of a gas-filled Cryogenic Stopping Cell (CSC) [4, 5], a Radio Frequency Quadrupole (RFQ) beamline, and a Multiple-Reflection Time-Of-Flight Mass Spectrometer (MR-TOF-MS) [6–8]. The CSC also serves as the prototype for the next-generation CSC [9] of the Super-FRS [10]. Exotic nuclei produced at relativistic energies by projectile fragmentation and fission are separated in-flight by the FRS. These nuclei are stopped in the CSC by the ultra-pure helium gas at cryogenic temperatures and are then transported via the RFQ beamline to the MR-TOF-MS for high-precision direct mass measurements.

As a universal method to convert fast exotic beams to low-energy and low-emittance beams for precision experiments with stored ions, e.g., mass measurements and decay and laser spectroscopy [11], gas-filled stopping cells have been widely used to slow down and thermalize exotic nuclei produced by fusion-evaporation, in-flight fragmentation and fission [12–17]. One of the challenges of this approach is the operation with high beam intensities, as space-charge and plasma effects can deteriorate the efficiency [18–23]. The CSC of the FRS-IC is operated at cryogenic temperatures to achieve high cleanliness of the stopping gas. Strong DC push fields are created by a DC-cage in the CSC for fast ion extraction. The DC-cage consists of ring electrodes (e.g., a short DC-cage in Fig. 1) with different voltages applied to form the DC push fields. At the end of the DC-cage, an RF carpet is used to guide the ions out of the CSC via the small hole in the middle of the RF carpet. The RF carpet with small electrode spacing (i.e., 0.25 mm) provides a strong repelling force and allows to reach the highest buffer gas density (i.e., stopping efficiency).

The ability to handle incoming beams of high intensity without deteriorating ion extraction efficiency (i.e., high rate capability) opens up possibilities for new experiments, where the nuclear reactions take place in the stopping volume of the CSC. Examples of such experiments include in-cell multi-nucleon transfer (MNT) reactions [24] and spontaneous fission [2,25,26] studies, where an ionization rate density of  $10^7$   $\text{He}_3^+e^-$  pairs/ $\text{cm}^3/\text{s}$  (considering the volume of the DC-cage of  $2.7 \times 10^4$   $\text{cm}^3$ ) is generated by the stopping of spontaneous fission fragments and MNT fragments. A new dedicated DC-cage has been developed [27] for the high-rate experiments above to surpass the limitations of a standard DC-cage. The rate capability of both systems has been studied experimentally, and the results are presented in this paper.

## 2. Experiment

Two experiments (i.e., Experiment I and Experiment II) have been performed with a  $^{238}\text{U}$  primary beam to study the rate capability of the CSC at the FRS-IC in 2016 and 2021 with the experimental setup described in detail in Refs. [1,4,5,28]. In past investigations [29], beam pulses with very short duration on the millisecond scale have been used to simulate high-rate DC beams. In the experiments presented here, more realistic experimental conditions with a spill length of a few seconds were used. In both experiments, the optimum range of the ions for efficient stopping in the CSC was tuned by varying the homogeneous degrader installed in front of the CSC. Thus the ratio of stopped ions to injected ions was maximized. The overall efficiency of the thermalization and extraction process, given by the product of stopping efficiency and extraction efficiency, was measured for different beam intensities. The beam intensities were measured with a plastic scintillator mounted in front of the CSC. The stopping efficiencies were determined from a measurement of the range distribution and the known areal density of the stopping cell. The overall efficiencies were determined by counting the ions extracted from the CSC with the MR-TOF-MS. The extraction

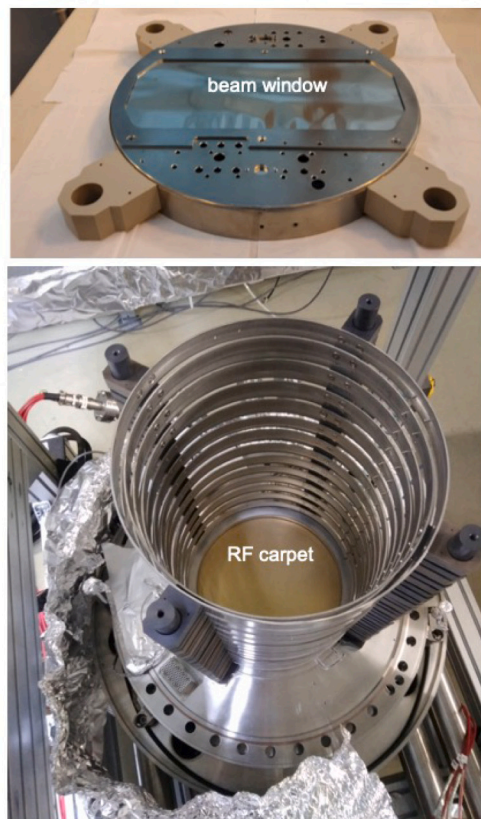


Fig. 1. Photo of the short DC-cage installed on the flange of the CSC. The DC-cage consists of 27 ring electrodes with a pitch (i.e., the central distance between the neighboring electrodes) of 2 cm. The “golden” RF carpet and the entrance electrode (with a beam window) installed on the two ends of the DC-cage are shown as well.

efficiencies could then be calculated as the ratio of overall efficiency to stopping efficiency.

In Experiment I, the extraction efficiencies were investigated for different rates of the  $^{238}\text{U}$  primary beam at 300 MeV/u with a spill length of 1 s. Thermalized  $^{238}\text{U}$  ions were extracted from the CSC and measured with the MR-TOF-MS. As uranium is one of the most reactive elements, it tends to form molecules from reactions with contaminants contained in the helium gas. The extraction efficiencies were calculated from the total count rates of all observed forms (i.e.,  $^{238}\text{U}^{2+}$ ,  $^{238}\text{UO}^{2+}$ ,  $^{238}\text{UOH}^{2+}$ , and  $^{238}\text{UO}_2^{2+}$ ) identified via high precision mass measurements with the MR-TOF-MS. In this experiment, the long DC electrode structure was used in the CSC (i.e., long DC-cage), which has a stopping volume with a length of 105.4 cm and a diameter of 25 cm. The CSC was operated with a helium areal density of  $3.16 \pm 0.35$   $\text{mg}/\text{cm}^2$  (corresponding to a pressure of  $59 \pm 6$  mbar at a temperature of 94 K) and a DC push field of 20.0 V/cm. Three different values of the repelling RF voltage (i.e.,  $94 V_{pp}$ ,  $40 V_{pp}$ , and  $28 V_{pp}$ ) were applied to the RF carpet. This assists in verifying that the decrease in extraction efficiency is attributable to space-charge effects within the bulk of the stopping volume rather than an insufficient repelling force exerted by the RF carpet, which could impact the ion motion in that region.

A short DC electrode structure (i.e., short DC-cage shown in Fig. 1) with a length of 48.2 cm and a diameter of 26.7 cm was used in Experiment II. This short DC-cage shortens the extraction path and allows applying a higher DC push field in the CSC. In addition, the pitch (i.e., the central distance between the neighboring electrodes) of the short DC-cage are reduced to half of the longer one used in previous experiments and the diameter is slightly increased; together these increase the effective radius of the stopping volume by 15% and

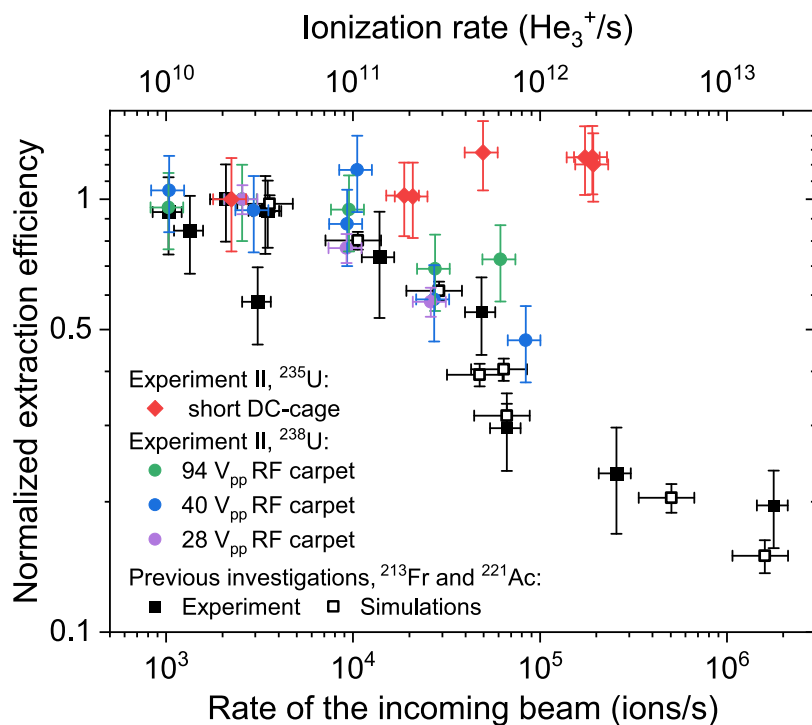


Fig. 2. Rate capability achieved with the long DC-cage (filled squares and circles) and the short DC-cage (filled diamonds). Simulations (open squares) done for previous investigations with the long DC-cage agree well with experimental results (filled squares). The corresponding ionization rate is given in helium trimer ions  $\text{He}_3^+$  per second.  $\text{He}_3^+$  ions are generated from the ionization of the helium gas when stopping the ions.  $\text{He}_3^+$  is the main charge carrier under the conditions of the CSC.

thus the effective area by 30%. This further increases the rate capability of the system. The extraction efficiencies were investigated with a  $^{235}\text{U}$  secondary beam produced by a  $^{238}\text{U}$  primary beam at different intensities with a spill length of 5 s and 12 s.  $^{235}\text{U}$  ions were produced via  $^{238}\text{U}$  projectile fragmentation at 1000 MeV/u in a beryllium target with an areal density of  $0.664 \text{ g/cm}^2$ . The target was followed by a  $0.223 \text{ g/cm}^2$  Nb stripper to reach the highest charge state at this energy.  $^{235}\text{U}$  ions were separated in flight using twofold magnetic rigidity analysis and a  $2 \text{ g/cm}^2$  Al wedge degrader located at the central focal plane of the FRS. The identification of the ions was performed using the standard particle detectors of the FRS. After further slowing down in the degrader at the final focal plane, the ions were injected into the CSC. The CSC was operated with a helium areal density of  $1.12 \pm 0.12 \text{ mg/cm}^2$  (corresponding to a pressure of  $36 \pm 4 \text{ mbar}$  at a temperature of 75 K) and a DC push field of  $30.4 \text{ V/cm}$ . The RF carpet was operated with 100% transmission efficiency. In Experiment II, extraction efficiencies were calculated from the count rates of  $^{235}\text{UO}^{2+}$  measured with the MR-TOF-MS. No other molecular forms besides  $^{235}\text{UO}^{2+}$  were observed.

### 3. Results and discussion

Fig. 2 shows a compilation of the results of past investigations done in 2014 [29] and new measurements performed in the present work. In addition, the corresponding ionization rate is given in helium trimer ions  $\text{He}_3^+$  per second. To eliminate effects from the stopping in the CSC and transport from the CSC to the MR-TOF-MS, the extraction efficiencies are normalized to a rate at which the CSC has the full extraction efficiency. For Experiment I, data points of the three different repelling RF voltages were normalized to the extraction efficiencies measured at beam intensities of about  $2.5 \times 10^3$  ions/s, respectively. The normalization of data from Experiment II was done with the extraction efficiency measured at the beam intensity of  $2.2 \times 10^3$  ions/s. The total efficiency for extraction and transmission of the ions from the CSC to the MR-TOF-MS and their detection amounts to 0.69% and 0.85% for Experiment I and Experiment II, respectively.

The rate capabilities were found to be independent of the repelling RF voltage applied to the RF carpet. As shown (by filled circles) in Fig. 2, the decreasing trend of the extraction efficiency is independent of the repelling RF voltage applied to the RF carpet. As seen from the figure, the new measurements (filled blue and green circles) performed in Experiment I with the long DC-cage agree with the simulation results (open squares) and the former experimental data with short beam spills (filled squares). Up to an incoming beam rate of about  $10^4$  ions/s of  $^{238}\text{U}$  injected into the CSC, the extraction efficiency stays constant. However, the extraction efficiency decreases at higher rates. The agreement between pulsed and DC beam and the simulation further supports the correct understanding of the system by space-charge effects. With increasing the beam rate, these effects cause a severe deflection of the thermalized ions towards the DC electrodes, thus only ions stopped in the region close to the RF carpet can be efficiently extracted.

In contrast to the long DC-cage, the extraction efficiency is significantly improved with the short DC-cage, and there is no loss in extraction efficiency up to an incoming beam rate of  $2 \times 10^5$  ions/s as shown with the filled diamonds in Fig. 2. Simulations show the rate limit can reach  $10^7 - 10^8$  ions/s [27]. However, higher beam intensities could not be tested as the radiation limit of the experimental cave was reached. The improvement is due to (i) the smaller pitch design that reduces the near-field distortions (confirmed by simulations) and allows efficient transport of the ions stopped closer to the DC electrode, (ii) the larger diameter of the DC electrodes that enlarges the stopping volume of the CSC in the radial direction, (iii) the higher DC push field that leads to faster removal of He ion–electron pairs and (iv) the shorter DC-cage that brings the stopping volume closer to the RF carpet (as can be seen from the Fig. 1 in Ref. [29]). The short DC-cage design (i.e., the smaller pitch and the larger diameter of the DC electrode) increases the stopping volume in the radial direction, which is crucial for efficient stopping and extracting the energetic fission and MNT fragments produced inside the CSC.

The results of Experiment I validate the simulation model used to project the rate capability of the next-generation CSC for the Super-FRS [9]. Compared to the present CSC with the standard (long) DC-cage, the next-generation CSC will exhibit notable enhancements in

terms of two times shorter ion paths and three times stronger electric fields. Additionally, multiple RF carpets will cover a larger area relative to the stopping volume. According to the simulations, these advancements combined will further reduce ion losses caused by space-charge effects, enabling the next-generation CSC to meet the required rate capability of  $10^7$  ions/s. A configuration of the present CSC with the short DC-cage is aligned closely with the design concepts of the next-generation CSC. Therefore, the successful use of the short DC-cage in Experiment II surpassing the rate capability of the long DC-cage by more than an order of magnitude provides additional support for the selected design concepts.

#### 4. Conclusions and outlook

The rate capability of the CSC at the FRS-IC has been studied with the  $^{238}\text{U}$  primary beam and its projectile fragments with a spill length scale of seconds. With the standard long DC-cage, the extraction efficiency decreases for a beam rate higher than  $10^4$  ions/s. In contrast, no extraction efficiency loss is observed up to a rate of  $2 \times 10^5$  ions/s with the newly developed short DC-cage. This new rate capability is achieved by employing a shorter and wider DC electrode structure, which has better tolerance of the space-charge effects. This paves the way for exotic nuclei studies at the FRS-IC with in-cell multi-nucleon transfer reactions. The new results not only provide experimental confirmation of the advantages of the CSC with the short DC-cage, but also complete the validation of the simulation model and justify its use for the next-generation CSC [9] of the Super-FRS at FAIR.

#### CRedit authorship contribution statement

**J.W. Zhao:** Writing – original draft, Formal analysis, Conceptualization. **D. Amanbayev:** Writing – review & editing, Formal analysis, Visualization. **T. Dickel:** Writing – review & editing, Conceptualization, Methodology, Supervision. **I. Miskun:** Resources, Investigation. **W.R. Plaß:** Writing – review & editing, Conceptualization, Supervision. **N. Tortorelli:** Visualization, Validation. **S. Ayet San Andrés:** Writing – review & editing, Validation, Investigation. **S. Beck:** Investigation. **J. Bergmann:** Investigation. **Z. Brencic:** Writing – review & editing, Investigation. **P. Constantin:** Writing – review & editing, Visualization, Funding acquisition. **H. Geissel:** Investigation. **F. Greiner:** Investigation. **L. Gröf:** Investigation. **C. Hornung:** Validation, Investigation. **N. Kuzminchuk:** Investigation. **G. Kripkó-Koncz:** Investigation. **I. Mardor:** Validation, Investigation. **I. Pohjalainen:** Validation, Investigation. **C. Scheidenberger:** Supervision, Investigation, Funding acquisition. **P.G. Thirolf:** Writing – review & editing, Funding acquisition. **S. Bagchi:** Writing – review & editing, Investigation. **E. Haettner:** Writing – review & editing, Validation, Investigation. **E. Kazantseva:** Investigation. **D. Kostyleva:** Investigation. **A. Oberstedt:** Validation, Investigation. **S. Pietri:** Validation, Investigation. **M.P. Reiter:** Resources, Validation, Investigation. **Y.K. Tanaka:** Investigation. **M. Wada:** Investigation. **D.L. Balabanski:** Investigation. **D. Benyamin:** Investigation. **M.N. Harakeh:** Writing – review & editing, Investigation. **N. Hubbard:** Investigation. **N. Kalantar-Nayestanaki:** Writing – review & editing, Validation, Investigation. **A. Mollaebrahimi:** Writing – review & editing, Validation, Investigation. **I. Mukha:** Validation, Investigation. **M. Narang:** Validation, Investigation. **T. Niwase:** Writing – review & editing, Investigation. **Z. Patyk:** Writing – review & editing, Funding acquisition. **S. Purushothaman:** Investigation. **A. Rotaru:** Investigation. **A. Spătaru:** Investigation. **G. Stanic:** Investigation. **M. Vencelj:** Investigation. **H. Weick:** Investigation. **J. Yu:** Validation, Investigation.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

#### Data availability

Data will be made available on request.

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