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Green Chemistry for Stainless Steel Corrosion

2 Resistance: Life Cycle Assessment (LCA) of

3 Citric Acid versus Nitric Acid Passivation

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9 Abstract

- 10 Corrosion is a significant problem in many industries, and when using stainless steel,
- passivation is undertaken to improve corrosion resistance.
- 12 Traditionally, nitric acid is used within the passivation step, however, this has some
- detrimental environmental and human health impacts during its production and use.
- 14 Reducing this impact is critical, and because of its toxicity, associated occupational risk and
- special disposal requirements, end-users of passivated stainless steels are exploring
- 16 alternative passivation methods. However, it is also critical to understand the impact of any
- alternatives. Sustainable processing and manufacture embodies many elements, including;
- waste reduction, resource efficiency measures, energy reduction and the application of
- 19 'green' or renewable chemicals. In order to ensure the most effective system is utilised the
- 20 impact, or potential impact of the system must be measured and options compared. The
- 21 comparative environmental credentials of bio-based chemicals can be assessed using tools
- 22 such as Life Cycle Assessment (LCA).

- 23 This paper is the first paper to evaluate the environmental impact of passivation using nitric
- 24 and citric acid. It uses attributional Life Cycle Assessment (ALCA) to assess the
- 25 environmental benefits and dis-benefits of using citric acid produced biologically via
- fermentation, to replace nitric acid, whilst keeping the same level of corrosion resistance.
- 27 The work is anticipatory in nature as the process is not yet undertaken on a commercial
- basis. The results therefore feed into future manufacturing and design.
- 29 Citric and nitric acids were compared using three different solutions: 4% and 10% citric acid
- 30 solutions, and a 10% nitric acid solution (the conventional case). The results show that a
- 31 scenario using a 4% citric acid solution is environmentally preferable to nitric acid across all
- impact categories assessed. However, a 10% citric acid solution used on low chromium and
- 33 nickel steel was only environmentally preferable for 50% of the environmental impact
- categories assessed due to increased electrical energy demand for that scenario.
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Highlights

- Citric acid is environmentally preferable to nitric acid for stainless steel passivation
- Extent is dependent on passivation bath conditions for comparable performance
- Life cycle approach is key to understanding nuances of environmental impact for
- 40 stainless steel passivation

41 Key words

- 42 Stainless steel, passivation, environmental impact, life cycle assessment, LCA
- 43 1.0 Introduction
- 44 Sustainability has become an increasingly important element in materials manufacture,
- leading to focus on process energy reduction and the application of green chemistry and
- other eco-design principles. The term 'green chemistry' gained traction during the 1990's
- culminating in formal recognition through the publication of the 12 principles of green

48 chemistry [1]. The guiding element to this being 'benign by design'. The principles provide a 49 toolkit for employing ideas embedded in industrial ecology [2]. The Environmental Protection 50 Agency (EPA) definition of green chemistry is 'the design of chemical products and 51 processes that reduce or eliminate the use or generation of hazardous substances. Green 52 chemistry applies across the life cycle of a chemical product, including its design, 53 manufacture, use, and ultimate disposal' [3]. 54 Metrics for green chemistry include the *Efactor* defined as the amount of waste produced per 55 kilogram (product) [4], reaction mass efficiency or carbon efficiency [5]], and Cfactor which is 56 the mass ratio of CO₂ to product mass [6], however, it does not distinguish between fossil and biogenic CO₂ emissions. 57 58 Given that the overarching aim of green chemistry employs life cycle thinking and a 59 consideration for the whole chemical product system, techniques like Life Cycle Assessment 60 (LCA) are often used to quantitatively assess the potential environmental impacts of bio-61 based/renewable solvents or resource efficiency measures [7, 8]. LCA evaluates environmental impact of a chemical process from raw materials production all the way 62 through to end-of-life [9]. It is a comparative assessment method, meaning that is can be 63 usefully applied to compare 'green' and conventional production methods. Unlike the green 64 65 chemistry metrics, LCA also enables the comparison of production processes across a number of different environmental impact categories. ISO standards 14040 and 14044 set 66 67 out procedures and methodologies for carrying out an LCA study [10, 11]. LCA has four main components: goal and scope definition, life cycle inventory (LCI), life cycle impact 68 69 assessment (LCIA), and interpretation [10]. The goal and scope definition describes the 70 product or process under assessment and details the purpose of the study. In the life cycle inventory step data is collected to then be analysed in the impact assessment stage. 71 72 There are a number of challenges in applying LCA to green chemistry and biotechnology. At 73 design or process development stages, LCA is often seen as too complex when evaluating different materials, processing or solvent options – particularly where there is high 74

uncertainty on what the process may look like at scale. Another challenge is the availability of industrial production data for many biologically derived chemicals and solvents. In order to overcome some of these issues, key parameters for LCA of green chemicals have previously been identified in [12]. Never the less, LCA still remains an important assessment tool in determining comparative impact for bio-based chemicals across a range of environmental impact criteria. Passivation of stainless steel is an important process to improve corrosion resistance. For example, within the space industry stainless steels are used in spacecraft and ground support structures where corrosion risk is high, including the storage and handling of certain liquids and wastes, propulsion systems, and components and fasteners exposed to harsh or demanding environments [13]. The effects of corrosion can have substantial economic and safety impacts, and lead to prolonged periods of asset downtime. The passivation process removes anodic surface contaminants (e.g. iron compounds) via chemical dissolution and leads to the formation of a passive oxide layer. The most commonly used acid to do this is nitric acid. Nitric acid is produced via ammonia oxidation. The process emits nitrous oxides (NO_x) and ammonia (NH₃) [14]. Nitric acid is highly corrosive and toxic on inhalation, and whilst it does feature on the EPA's safer chemical choice list for its application as a processing aid and additive, it is recognised as having some hazard profile issues and is not necessarily a low level of hazard concern for all human health and environmental endpoints [15]. Because of its toxicity, associated occupational risk and special disposal requirements, end-users of passivated stainless steel such as NASA and the European Space Agency (ESA) have been evaluating the performance of alternative acids, namely citric acid, as a potential replacement for nitric acid for passivation [13]. Citric acid is a common metabolite of plants and animals, also present in the juice of citrus fruits and pineapple. Its biological source and biodegradability make it a renewable and less toxic alternative to nitric acid. The acid is predominately used for soft drinks, confectionary,

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medicinal citrates, with smaller quantities used in dying and engraving [16]. On an industrial scale it is predominately produced via fermentation of *Aspergillus* or *Candida*.

Despite the introduction of citric acid products such as CitriSurf® for stainless steel passivation, to date there has lacked rigorous evaluation of chemical performance as a passivation medium, and comparative assessment of its environmental impact compared with nitric acid. The goal of this work is to compare nitric and citric acid production across a range of environmental impact categories to understand whether biologically produced citric acid can offer a greener, more environmentally friendly alternative to nitric acid passivation whilst reaching comparable performance levels.

2.0 Methods

This study is to contrasts the currently applied nitric acid passivation process with the most suitable citric acid passivation process for selected types of pristine and welded stainless steels.

The process evaluated in this LCA study is based on a laboratory-scale method for stainless steel passivation. Primary data was collected based on processing methods employed by ESR Technology Limited. Secondary sources include databases such as Ecoinvent 3.4 [17] and published literature, which is referenced accordingly in section 2.2. LCA software package Simapro 8 is used for the study.

The LCA evaluates a range of environmental impact categories as part of life cycle impact assessment, based on the ILCD recommended midpoint impact assessment categories [18]. The full range of midpoint categories are reported: climate change, ozone depletion, human toxicity (cancer and non-cancer), particulate matter, lonizing radiation HH, lonizing radiation E (interim), photochemical ozone formation, acidification, terrestrial eutrophication,

freshwater eutrophication, marine eutrophication, freshwater ecotoxicity, land use, water resource depletion, mineral, fossil and renewable resource depletion.

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2.1 Functional Unit and System Boundaries

Within LCA it is common for the environmental impacts to be calculated for the same given service - the functional unit. The functional unit used for this study is per 2000 cm2 of stainless steel surface passivated. This equates to the average surface area exposed during one passivation process run in the ESR Technology laboratory. Surface area could be used as a functional unit as it is assumed that each passivation process yielded a comparable passivation performance. This equivalence was the basis of the ESR and ESA research into the passivation processes - needing a functionally equivalent output on an area basis. Cut-off rules (relating to environmental significance of certain materials and energy flows) were not formally applied to the study; however, some inputs to the process were omitted for both citric and nitric acid passivation. This includes some laboratory disposables used in the cleaning of the stainless steel samples, such as disposable knitted polyester cloths and pH testing paper. This is due to an inability to model these inputs to a reasonable level of accuracy. Also omitted from this work are inputs relating to bagging and storage of samples, as the conditions for doing this are assumed to be the same for each acid assessment. The input of the stainless steel into the passivation process is outside the system boundary of this work. This was done to ensure focus on the passivation process itself, as for nitric or citric acid the input of stainless steel is assumed to be the same. The system boundary is given in Figure 1. This includes all activities associated with the cleaning, acid bath passivation, and subsequent washing and drying of samples. Impacts are allocated 100% to the functional unit. There are 3 stainless steels evaluated: AISI 410, PH17-7, and AISI 302. This was done in

order to take into account the different processing conditions required for different types of

stainless steel based on chromium content. AISI 410 is Martensitic with a lower alloy content (~12.5% chromium, 0% nickel content). AISI 302 contains ~18% chromium, 9% nickel, and PH17-7 contains ~17% chromium, 7% nickel.

The three passivation scenarios were evaluated: 50% nitric acid heated to 55°C and held at temperature for 30 minutes (for AISI 302/PH 17-7 and AISI 410 stainless steels); 4% citric acid heated to 60°C and held at temperature for 1 hour (AISI 302/PH 17-7 stainless steels); and 10% citric acid heated to 80°C and held at temperature for 3 hours (AISI 410 stainless steel only – accounting for lower alloying content).

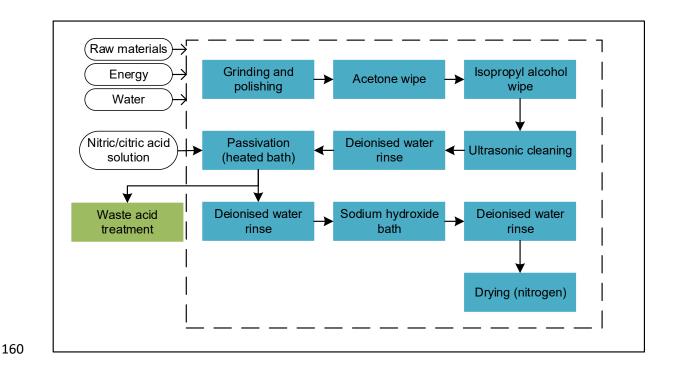


Figure 1. Process flow based flow for stainless steel passivation at laboratory scale (dotted line indicates process steps, full line indicates system boundaries

2.2 Data collection and modelling

The LCI was modelled based on primary data from ESR. Material inputs were modelled using Ecoinvent 3.4, and are shown in Table 1. An outline of the process is shown in figure

1. The abrasive paper used to polish the samples in the first process step was modelled based on a 3M abrasive paper specification. The acetone wipes used to clean the samples (3 samples per wipe) excluded the knitted polyester wipe used to apply the acetone. The same omission was applied to the application of isopropyl alcohol with a polyester wipe. The model for the Lenium® cleaning solution was based on its MSDS data sheet [19]. The two major components of the solution n-propyl bromide and 2-propanol were modelled using production data from Ecoinvent (Simpro inputs available in Supplementary Material). For the passivation process direct electricity demand was modelled based on primary data from ESR. The 3.5l acid bath containing solutions of 4%, 10% w/w citric acid and 50% w/w nitric acid was modelled using data from Ecoinvent. Subsequent neutralisation with sodium hydroxide, rinsing with deionised water and drying with gaseous nitrogen was also all modelled using data from Ecoinvent. Heating of the sodium hydroxide solution to 70°C on a laboratory hot plate was modelled using energy meter data at the University of Bath. The bagging and storing of samples is not included in the scope of the study. Electricity production is modelled using the Digest of United Kingdom Energy Statistics (DUKES) [20]. This assumes a 2015 UK energy mix and assumes a mix broken down in the following way: 22% coal, 30% natural gas, 21% nuclear, and remaining proportion from renewables. Within the LCA model, acid waste is treated differently depending on whether it is citric or nitric acid. Spent nitric acid from the passivation bath (which is assumed to be emptied after every six samples) is treated by waste solvent incineration. Spent citric acid, emptied from the passivation bath at the same frequency as the nitric acid, is treated as effluent to waste water treatment. Within the main LCIA, waste treatment is included as a sub-process within the passivation step.

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Waste management is also modelled separately in EcoSolvent [20] to evaluate each acid under different waste management scenarios: incineration and waste water treatment.

Again, this assumes the passivation bath is emptied after each six sample batch.

The model assumes a large waste-solvent incineration plant, where the co-products of the incineration plant are steam and electricity. Waste water treatment is calculated as a function of the waste water composition. The model provides generic and site-specific data ranges for mechanical-biological treatment, reverse osmosis and extraction. It is adapted to fit the chemical properties of nitric and citric acid.

Table 1. Inventory for 2000 cm2 passivation of stainless steel

Item	Process input	Comment	
Grit paper	6 pieces	Based on 3M grit paper 12.5%	
		silicon carbide, 87.5% paper	
		backing	
Acetone	30 ml	Primary data (ESR)	
Isopropyl alcohol	30 ml	Primary data (ESR)	
Lenium® solution	0.15 kg	Primary data (ESR) based on 85%	
		n-propyl bromide and 10% 2	
		propanol	
Ultrasonic cleaning bath	1.92 kWh	Primary data (ESR) based on 85%	
		n-propyl bromide and 10% 2	
		propanol	
Deionised water	5.2 kg	Primary data (ESR)	
Passivation	_		
50% nitric acid			
Nitric acid	1.75kg	Primary data (ESR)	
Bath heating	0.21 kWh	Primary data (ESR)	
Fume hood operation	0.93 MJ	Calculated based on Caltech fume	
·		hood energy calculator:	
		http://fumehoodcalculator.lbl.gov/	
4% citric acid			
Citric acid	0.14kg	Primary data (ESR)	
Bath heating	0.52 kWh	Primary data (ESR)	
Fume hood operation	1.8 MJ	Calculated based on Caltech fume	
		hood energy calculator:	
		http://fumehoodcalculator.lbl.gov/	
10% citric acid			
Citric acid	0.35kg	Primary data (ESR)	

Bath heating	3.3 kWh	Primary data (ESR)
Fume hood operation	5.6 MJ	Calculated based on Caltech fume hood energy calculator: http://fumehoodcalculator.lbl.gov/
Sodium hydroxide solution	21	Primary data (ESR)

2.3 Assumptions and Limitations

There are a number of assumptions and limitations associated with the LCA study. The process is based on laboratory scale stainless steel passivation, therefore may not be indicative of passivation at industrial scale. The production of steel is not included within the scope of the LCA to allow direct comparison between passivation acids (with the production of citric and nitric acid included in the scope of the study). Some laboratory consumables are omitted from the study, such as polyester wipes used for initial degreasing of the samples, as it has proved difficult to obtain inventory data to accurately represent these. These form only a very small part of the study and are their omission is therefore thought to have minimal impact on the results. As per standard LCA practice, the production of laboratory equipment is also not included within the scope of the assessment.

In the LCA study it is assumed that nitric and citric acid undergo different waste treatment options. Nitric acid is treated via waste solvent incineration, and citric acid via waste water treatment. There is uncertainty as to what would be the case at an industrial scale, and

3.0 Results and Discussion

3.1 Contribution analysis

The contribution of each processing step to the overall environmental impact of the whole passivation process was assessed using the ILCD recommended midpoint impact assessment categories. In this analysis everything is analysed as a percentage contribution

therefore waste treatment was also modelled separately in Ecosolvent.

229 of the individual process. This indicates within each option which impact has the most significant contribution. 230 231 The contribution results assess the following 3 scenarios for the passivation bath step: 50% nitric acid heated to 55°C and held at temperature for 30 minutes (AISI 302/PH 232 17-7 and AISI 410 stainless steels) 233 4% citric acid heated to 60°C and held at temperature for 1 hour (AISI 302/PH 17-7 234 235 stainless steel) 10% citric acid heated to 80°C and held at temperature for 3 hours (AISI 410 236 237 stainless steel) 238 239 Impact relating to acid usage and waste disposal is included as part of the passivation step. 240 Figure 2Figure 2 shows the contribution to total impact for the 4% citric acid scenario. Major 241 contributors to climate change impact (kg CO₂eq) are the ultrasonic cleaning step (55%) and 242 the passivation step (19%). Within both of these stages the main contribution to impact is from process energy use – the operation of the cleaning bath or the passivation bath. 243 Further impact categories show a similar trend with ultrasonic cleaning and passivation step 244 245 dominating.

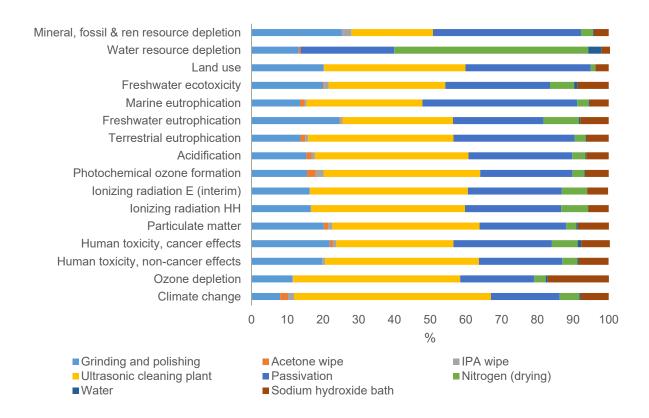


Figure 2 Contribution analysis for AISI 302/PH 17-7 4% citric acid

The passivation step is far more dominant for the 50% nitric acid scenario (Figure 3Figure 3). Here contribution to climate change impact is 83% of the total score. Passivation dominates other environmental impact categories. The dominance of the passivation step relates to the production of nitric acid. Nitric acid in Ecoinvent via the Ostwald process is dominated by ammonia production.

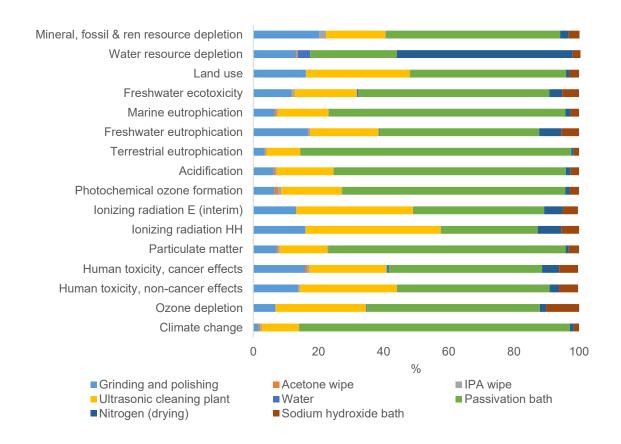


Figure 3 Contribution analysis for AISI 302/PH 17-7 and AISI 410 50% nitric acid

The 10% citric acid scenario is used for the AISI 410 steel type only (figure 5). This has a far lower chromium and nickel alloy content (12.5% chromium, 0% nickel). Here the passivation step dominates impact for the majority of impact categories assessed. For climate change it contributes to 51% of overall impact. For freshwater ecotoxicity it contributes 56%, and for human toxicity (cancer and non-cancer) it contributes 55%. Sub-processes leading to the significant contribution of the passivation bath step to total impact are energy demand (bath operation) and production of citric acid. In this case citric acid is assumed to be produced via the fermentation of microorganism *Aspergillus niger*. Fermentation data is provided by a European citric acid producer, but the dataset aggregated by Ecoinvent to protect process confidentiality. Due to the contribution of the citric acid, further exploration undertaken in this area showed that although the process is widely known there is no published disaggregated data available on this. However, based on analysis of ecoinvent proxies (and previous

evaluation by [22]) indicate that the impacts in citric acid production result predominantly from the feedstock and any energy used in associated fermentation.

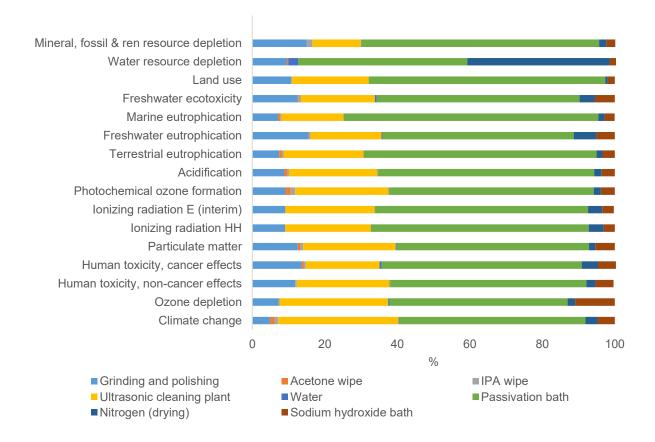


Figure 4 Contribution analysis for AISI 410 10% citric acid

3.2 Comparisons

All three passivation scenarios can be compared against each other (figure 5). All impacts are compared with nitric acid as the reference, which is shown as 100% impact. Therefore, effectively the two citric acid options are compared to nitric acid as the base case.

Comparing the 4% citric acid scenario used for AISI 302 and PH17-7 stainless steels against the 50% nitric acid scenario used for all steels, the 4% scenario performs better across all ILCD impact categories. For 8 out of the 16 ILCD impact categories for the 10% citric acid scenario (AISI 410 stainless steel) has a higher environmental impact than the 50% nitric

acid scenario. This is due to the production of electricity required to heat the passivation bath for three hours. Options to reduce this would include using a higher penetration renewable technology for the heating, or heating in a more efficient way, if possible.

The comparisons made here show that despite the increased toxicity and environmental impact from use of nitric acid as opposed to bio-based citric acid to passivate stainless steel, where the process requires longer heating periods (10% citric acid scenario) and hence higher process energy inputs this reduces some of the environmental gains made through use of bio-based chemicals. The findings here highlight why multi-impact category assessment methods like LCA are valuable for assessing green manufacturing alternatives.

Table 2 shows the characterised data in terms of absolute total values. The same data as in Figure 5 is shown here, but not in terms of a percentage of the largest impact in each category. Therefore, here one can compare the impact across the scenarios all the scenarios in absolute terms for each scenario.

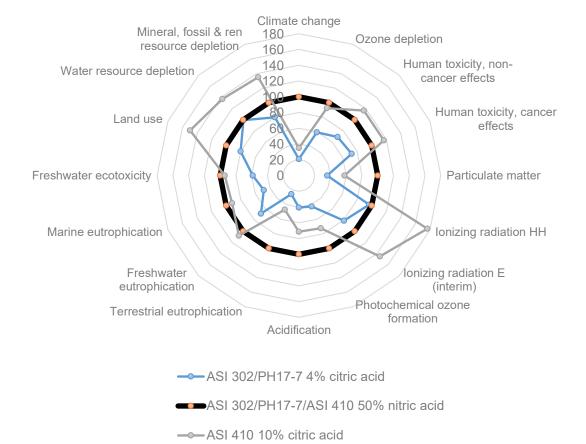


Figure 5. Comparison of each acid passivation scenario across all ILCD Recommended impact categories (nitric acid = 100%)

Table 12. Breakdown of individual ILCD impact scores for each passivation scenario

Impact category	Unit	AISI 302/PH17-7 4% citric acid	AISI 302/PH17- 7/AISI 410 50% nitric acid	AISI 410 10% citric acid
Climate change	kg CO2 eq	2.42E+00	1.15E+01	4.02E+00
Ozone depletion Human toxicity, non-cancer	kg CFC-11 eq	4.92E-07	8.29E-07	7.67E-07
effects	CTUh	8.39E-07	1.21E-06	1.41E-06
Human toxicity, cancer effects	CTUh	1.26E-07	1.74E-07	2.03E-07
Particulate matter	kg PM2.5 eq	1.89E-03	5.27E-03	3.04E-03
lonizing radiation HH	kBq U235 eq	8.75E-01	9.07E-01	1.60E+00
Ionizing radiation E (interim)	CTUe kg NMVOC	2.42E-06	2.99E-06	4.34E-06
Photochemical ozone formation	eq	8.46E-03	1.99E-02	1.44E-02
Acidification	molc H+ eq	2.04E-02	5.02E-02	3.58E-02
Terrestrial eutrophication	molc N eq	3.40E-02	1.34E-01	6.27E-02
Freshwater eutrophication	kg P eq	1.17E-03	1.71E-03	1.85E-03
Marine eutrophication	kg N eq	3.73E-03	7.73E-03	7.10E-03
Freshwater ecotoxicity	CTUe	1.89E+01	3.22E+01	3.03E+01
Land use	kg C deficit	1.03E+01	1.28E+01	1.91E+01
Water resource depletion Mineral, fossil & ren resource	m3 water eq	2.25E-02	2.26E-02	3.11E-02
depletion	kg Sb eq	1.80E-04	2.25E-04	3.04E-04

3.3 Acid waste treatment

Aside from potentially different processing conditions for citric (4%, 10% scenarios) and nitric acid during the stainless steel passivation process, the methods for acid disposal also differ. Nitric acid is highly corrosive and a strong oxidiser meaning that the 50% nitric acid solution within the passivation bath will require special handling. It is likely that it would be disposed of via a formal solvent disposal route as opposed to an industrial waste water treatment system. Within the LCA model itself the nitric acid is assumed to be incinerated, whereas the citric acid is treated via waste water treatment. For transparency, the disposal methods are compared using Ecosolvent, which is a life cycle assessment tool developed by ETH Zurich to quantify impacts relating to waste solvent treatment [20]. The tool models a hazardous waste solvent incineration plant, and an industrial waste water treatment plant. Coproducts from the incineration plant are steam and electricity, with environmental credits granted for these.

Ecosolvent holds data for 26 solvents based on their elemental composition, heat of vaporisation, and heating value. The model for these was adapted for nitric and citric acid using their chemical property information. The incineration model calculates inventory data for solvent combustion as a function of chemical composition. The model is based on data for a Swiss incineration plant with a capacity of 35,000 tonnes per year. Results from each waste scenario are reported in terms of their global warming potential For the incineration scenario (figure 6), incineration energy recovery for all 3 scenarios is not enough to counter direct emissions from the process. Per functional unit impact from solvent production is far higher for nitric acid than for both citric acid scenarios. GWP totals for 10%, 4% citric acid and 50% nitric acid were 3.23, 2.37 and 7.52 kg CO₂eg respectively. Impact from treatment at a waste water treatment plant (figure 7), despite not including any energy recovery, is environmentally favourable for all acid passivation scenarios. Impact is separated between solvent production, electricity and ancillaries in mechanical-biological treatment and associated emissions (MBTP), sludge treatment, and waste water treatment (WWTP). Impacts relating to reverse osmosis and extraction are zero. The relative GWP for 10%, 4% citric acid and 50% nitric acid scenarios is 1.79, 0.72, and 5.5 kg CO₂eq. The results from modelling of waste treatment show that for both waste treatment options nitric acid has the higher GWP potential compared with both 4% and 10% citric acid scenarios. However, much of this additional impact comes from nitric acid production

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(particularly for waste water treatment), rather than the waste disposal method selected.

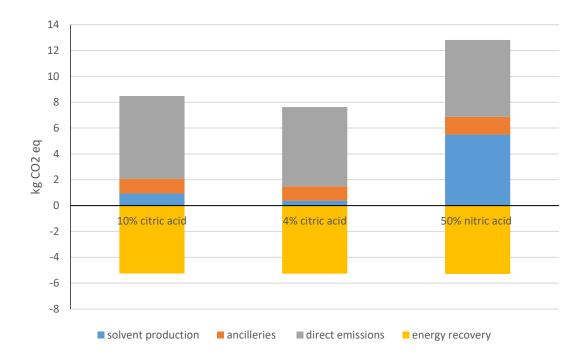


Figure 6 Waste solvent treatment - Incineration. Global Warming Potential (GWP) per functional unit

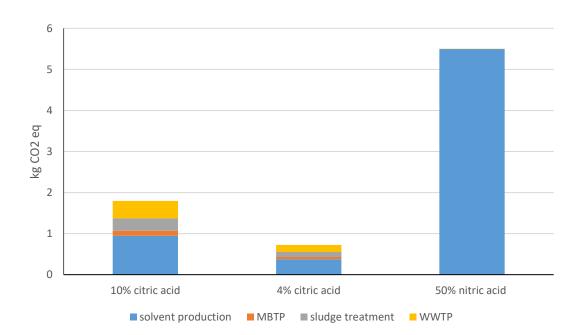


Figure 7 Waste solvent treatment. Waste water treatment plant. Global Warming Potential (GWP) per functional unit

4.0 Conclusions

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The use of green chemicals in manufacture and materials treatment processes, increases sustainability and helps to avoid difficult scale-up issues relating to chemical health and safety implications. Bio-based, renewable chemicals have the potential to be safer and have lower environmental impacts associated with both production and disposal stages of their life cycle than many conventional chemicals and solvents. However that is not always the case, and using Life cycle assessment (LCA) is a useful quantitative method for determining the comparative benefits or dis-benefits when selecting certain 'green' chemicals. When treating stainless steel for corrosion resistance, there is increasing interest in passivating them using citric acid as opposed to nitric acid. Nitric acid is highly corrosive and toxic on inhalation, requiring heightened EHS criteria. This paper provides the first LCA of the potential benefits of citric acid over nitric acid as a passivation technique. This is based on the required conditions for passivation in order to generate the same corrosion resistance performance. The LCA results show that the 4% citric acid scenario using AISI 302 and PH17-7 stainless steels, is environmentally preferable to 50% nitric acid across all ILCD recommended environmental impact categories. However, for the lower chromium and nickel content stainless steel AISI 410, the environmental benefits of moving to citric acid are less pronounced with only 50% of the ILCD impact categories assessed having a lower impact score than the nitric acid case. Impact associated with ionising radiation, resource depletion, and human toxicity were higher for the 10% citric acid scenario than for the nitric acid scenario. This is due to the increased time required within the heated passivation bath for the 10% citric acid scenario over the 4% citric acid, and 50% nitric acid scenarios. This work demonstrates the importance of LCA as a method for evaluating processes which contain 'green' or bio-based chemicals. Evaluation across a number of different impact categories reveals a more nuanced picture of comparative environmental impact than that

given through use of singular assessment metrics. This is despite modelling approach having been carried out at a laboratory scale and lead to potential misalignment with actual processing at industrial scale. Process energy provision during passivation has been shown to strongly influence the scale of environmental gains made by switching to a 'greener' acid alternative.

Acknowledgements

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Data availability

Primary data was provided by ESR Technology Limited. The raw data required to reproduce these findings is available in the Supplementary Material. Processed data produced using Simapro 8 and Ecosolvent is presented within the body of this paper.

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