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# Self-heating and Memory Effects in RF Power Amplifiers Explained Through Electro-Thermal Modeling

Wei Wei, Ole Kiel Jensen, Jan H. Mikkelsen

**Abstract**—Self-heating has already been proven to be one of the key sources to memory effects in RF power amplifiers (PAs). However, mechanisms behind the generation of memory effects, as caused by self-heating have not been well documented. On basis of transistor physical properties this paper proposes a simple electro-thermal model and shows how self-heating can generate different types of memory effects, such as bandwidth dependent intermodulation components and hysteresis loops. In addition, it is shown that self-heating can result in generation of new spectral components even in an otherwise linear PA. A time domain modeling framework is implemented to investigate memory effects generated by self-heating and simulation results are shown to agree with theoretical analysis.

**Index Terms**—Memory effect, self-heating, power amplifier, intermodulation, hysteresis,

## I. INTRODUCTION

Memory effects observed in typical RF PAs normally originate from 3 sources: self-heating [1], electron trapping [2] and baseband effects [1], [3]. Usually, these sources affect the performance of PAs simultaneously, which makes an understanding of the impact of each source difficult. Consequently, PAs with memory effects are normally analyzed and modeled behaviorally on the basis of measured data. For instance, Volterra series [4] represents a typical behavioral modeling approach. However, a behavioral modeling approach does not offer any physical explanation and understanding of the mechanism behind the memory effects.

As a memory source self-heating has been observed to affect intermodulation distortion [1], [5]. In a system with memory, the intermodulation depends not only on signal magnitudes but also on signal bandwidth [6]. This paper shows that bandwidth-dependent intermodulation can be caused by self-heating and clearly explains the physical mechanism behind. The occurrence of AM/AM hysteresis loops is another typical result of memory effects [7]. So far no link between self-heating and AM/AM hysteresis loops has been established in the literature. By adding a simple electro-thermal model this paper forms the link and shows how self-heating can result in AM/AM hysteresis.

Thorough understanding of the generation of memory effects can improve characterization and modeling of PAs. To achieve this, physical properties of transistors need to be investigated. On the basis of these physical properties, this

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paper explains the mechanism by which self-heating generates bandwidth-dependent output spectral components, AM/AM hysteresis loop opening and dynamic AM/AM and AM/PM behavior. Especially, for the first time, it is detailed how self-heating can be a source to generate AM/AM hysteresis loops and why the loop opening is bandwidth-dependent. The underlying physical reason for these memory effects is the interaction between RF signals and slow thermal responses.

This paper is organized as follows. The electro-thermal response of a class-A PA is discussed in section II, and how an electro-thermal response can generate memory effects is discussed in section III. Conclusions are finally given in section VI.

## II. ELECTRO-THERMAL RESPONSE IN PAs

The electro-thermal response observed in PAs can be described by means of a feedback loop [8], as illustrated in Fig. 1 where the transistor is simply modelled as a linear but temperature dependent transconductance..

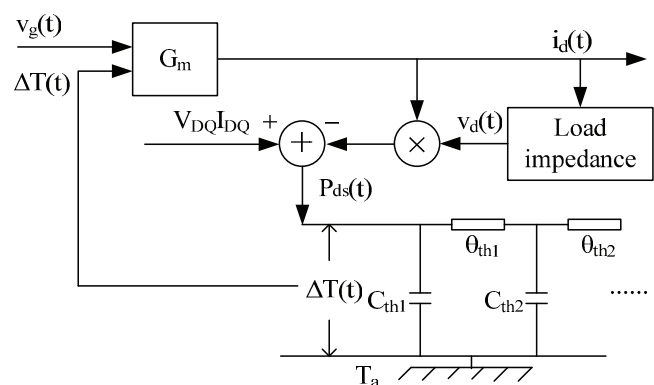


Fig. 1. Interaction between RF signals and thermal response in a FET based PA.  $v_g(t)$  denotes the gate voltage,  $G_m$  the transconductance,  $i_d$  and  $v_d$  denote the RF components of the drain current and voltage,  $I_{DQ}$  and  $V_{DQ}$  represent the drain bias current and voltage,  $C_{th}$  and  $\theta_{th}$  terms denote thermal capacitance and resistance.  $T_a$ ,  $P_{ds}$  and  $\Delta T$  denotes the ambient temperature, power dissipation and the temperature change respectively.

During operation, both bias and RF signals result in thermal power dissipation. As a consequence, both bias and RF signals affect the FET temperature ( $T_{FET}$ ). A changing  $T_{FET}$  affects  $G_m$ , that is, higher  $T_{FET}$  normally results in lower  $G_m$  following a roughly linear relation between  $G_m$  and  $T_{FET}$  [9]. By affecting  $G_m$ ,  $T_{FET}$  indirectly interacts with RF signals,

which gives rise to the electro-thermal response in a PA. In the following discussion, a simplified linear relation between  $G_m$  and  $T_{\text{FET}}$  is assumed:  $G_m = G_{ma} - \gamma\Delta T$ , where  $G_{ma}$  is the gate transconductance at the ambient temperature and  $\gamma$  is a positive coefficient.

Since  $P_{ds}$  is time-varying, the same will be the case for  $T_{\text{FET}}$ . If a PA is excited by an RF signal with a periodic envelope,  $T_{\text{FET}}$  can be expressed as

$$T_{\text{FET}}(t) = T_a + T_0 + \sum_{n=1}^N T_n \cos(n\omega_{th}t + \phi_n), \quad (1)$$

where  $T_0$  is the DC component of  $\Delta T(t)$ ,  $\omega_{th} = \frac{2\pi}{T_e}$  and  $T_e$  is the period of the signal envelope. The thermal time constant is normally in the range of  $\mu\text{s}$ . Therefore the temperature change within an RF-period is negligible.

Under two-tone excitation, the drain current can thus be expressed as

$$i_d = \{G_{ma} - \gamma[T_0 + \sum_{n=1}^N T_n \cos(n(\omega_{th})t + \phi_n)]\} \cdot V_g(\cos \omega_1 t + \cos \omega_2 t), \quad (2)$$

where  $V_g$  is the input amplitude of each tone. The power dissipation has spectral components from DC to RF frequencies. Due to the low-pass property of thermal circuits, only DC and baseband components can contribute to  $T_{\text{FET}}$  variations. Therefore, under two-tone excitation  $\omega_{th} = \omega_2 - \omega_1$ . In the simplified case of  $N=1$ , based on Eq. (2) the drain current is found to be

$$\begin{aligned} i_d &= (G_{ma} - \gamma T_0)V_g \cos \omega_1 t - \frac{1}{2}\gamma T_1 V_g \cos(\omega_1 - \phi_1) \\ & (G_{ma} - \gamma T_0)V_g \cos \omega_2 t - \frac{1}{2}\gamma T_1 V_g \cos(\omega_2 + \phi_1) \\ & - \frac{1}{2}\gamma T_1 V_g \cos(n(2\omega_1 - \omega_2)t - \phi_1) \\ & - \frac{1}{2}\gamma T_1 V_g \cos(n(2\omega_2 - \omega_1)t + \phi_1). \end{aligned} \quad (3)$$

From Eq. (3) it is shown that the mixing of the two tones and the thermal response causes amplitude and phase distortion of the two tones (first two lines) and also generates 3rd order intermodulation products (last two lines). Both magnitudes and phases of the generated intermodulation products are bandwidth dependent since  $T_n$  terms are bandwidth dependent. Secondly, Eq. (2) shows the appearance of AM/AM hysteresis loops. For simplicity, if only  $T_1$  is considered and harmonic terms of  $T_n$  are neglected, the input envelope and  $G_m$  under this simplified condition are shown in Fig. 2. At the rising and falling edges of the input envelope, all  $G_m$  curves are symmetrical while  $\phi_n = (2n+1)\pi/2$ , but asymmetrical while  $\phi_n \neq (2n+1)\pi/2$ . Obviously, asymmetry of  $G_m$  results in asymmetry of output envelopes.

The  $T_1$  term makes  $G_m$  change periodically at  $\omega_{th}$ . Similarly, a  $T_n$  term makes  $G_m$  change periodically at  $n\omega_{th}$  if  $n\omega_{th}$  is below the cut-off frequency of the thermal circuit. Variation of  $G_m$  causes distortions to signals.

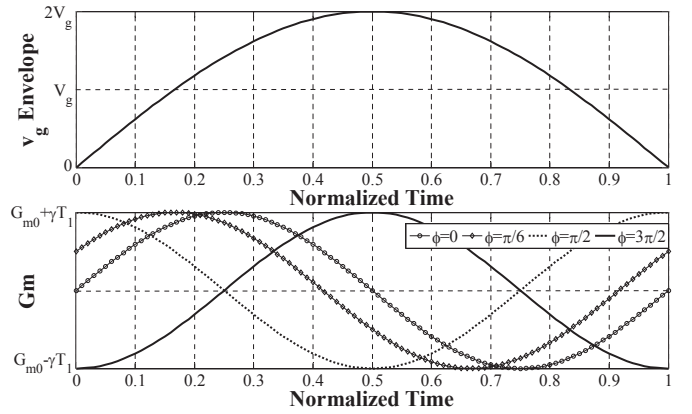


Fig. 2. Calculated input envelope and periodically changing transconductance of a class-A PA under two-tone excitation. The moment at which the envelope is zero is assigned to be zero on the time axis, and the time is normalized to  $\frac{2\pi}{\omega_2 - \omega_1}$ .

### III. MEMORY EFFECTS DUE TO ELECTRO-THERMAL RESPONSE

To investigate memory effects, a class-A PA model is implemented in Matlab Simulink with the modeling framework in Fig. 1. This model is implemented on the basis of a 20-finger FET. The gate width of each finger is  $50\mu\text{m}$  and the parameters of each finger are described by [9]. For this FET, the parameters at  $T_a = 325\text{ K}$  and  $V_{GQ} = -4.5\text{ V}$  are  $G_{ma} \approx 0.12\text{ S}$  and  $\gamma \approx 0.0002\text{ S/K}$ . With this FET the simulation is based on the following parameters:  $G_{ma} = 0.12\text{ S}$ ,  $\gamma = 0.0002\text{ S/K}$ ,  $V_{DQ}I_{DQ} = 6\text{ W}$ , load impedance =  $50\ \Omega$ ,  $\theta_{th} = 40\text{ K/W}$ ,  $C_{th} = 1.25 \times 10^{-6}\text{ J/K}$ .

Two-tone signals and stepped signals are introduced to excite the PA. The centre frequency of the RF signal during the simulation is 1 GHz.

#### A. $T_{\text{FET}}$ under Two Tone Excitation

Fig. 3 shows that under two tone excitation,  $\Delta T$  changes periodically at the period of  $2\pi/(\omega_2 - \omega_1)$ , and  $T_n$  harmonics appear. However, under single tone excitation,  $\Delta T$  is a constant value.

It is interesting to see that both the magnitude and phase of  $\Delta T$  depend on the difference frequency,  $\omega_2 - \omega_1$ . This is due to the low-pass properties of the thermal circuit. Fig. 4 shows the frequency response of the thermal impedance, where  $Z_{th} = \theta_{th}/(j\omega_{th}C_{th} + 1)$  denotes the thermal impedance.

#### B. Intermodulation Generated by Self-heating

Intermodulation products under two tone test appear in output signals, which is shown to agree with Eq. (2). Magnitudes of these components depend on the difference frequency of the two tones, as is shown in Fig. 5.

Demonstrated in Fig. 4 and 5, both magnitudes of IMD3 and  $Z_{th}$  decrease as the difference frequency increases. The underlying physical reason is that a higher magnitude of  $Z_{th}$  cause higher magnitudes of  $T_n$  terms, and hence higher magnitudes of intermodulation components, as illustrated by Eq. (2).

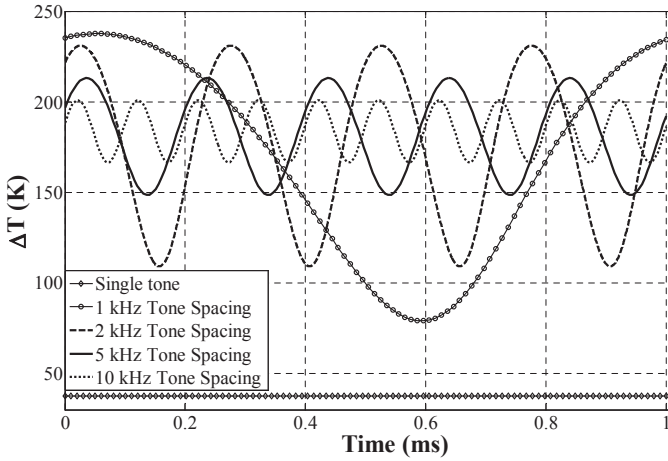


Fig. 3. Simulation results of  $\Delta T$  due to self-heating in a Class-A PA at  $V_g = 2$  V.

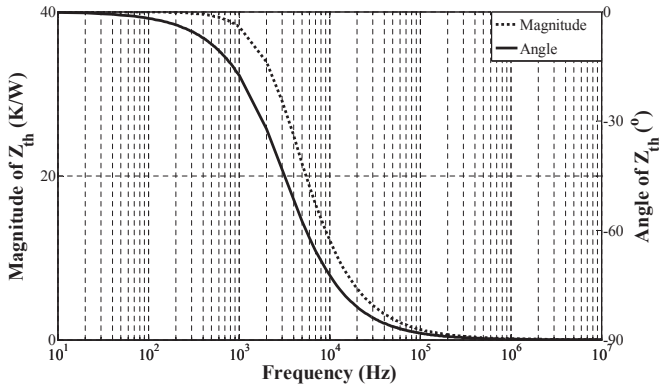


Fig. 4. Calculated thermal impedance of the FET with  $\theta_{th} = 40$  K/W and  $C_{th} = 1.25 \times 10^{-6}$  J/K.

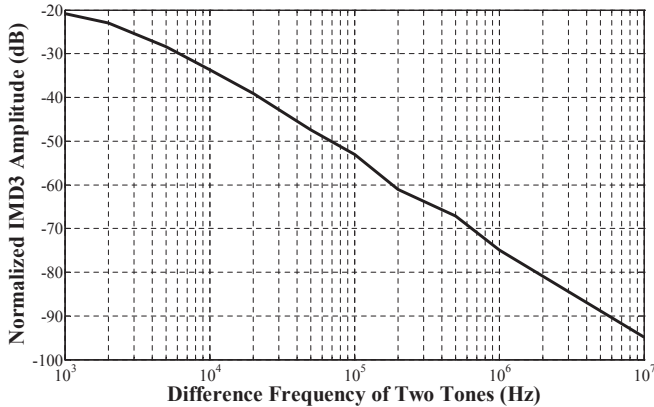


Fig. 5. Simulated IMD3 magnitude vs. difference frequency at  $V_g = 2$  V. IMD3 magnitudes are normalized to the magnitude of the fundamental tones.

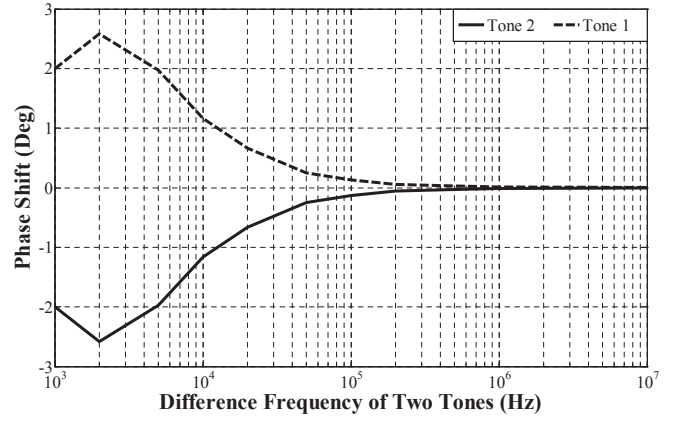


Fig. 6. Simulated phase shift due to self-heating vs. difference frequency of two tones at  $V_g = 2$  V.

### C. Phase Variation

The phase shift of the two output tones is also bandwidth-dependent, as shown in Fig. 6. When the difference frequency is outside the pass band of the thermal circuit, self-heating cannot cause phase variation to the two output tones.

### D. AM/AM Characteristic

Fig. 7 shows output envelopes and  $\Delta T$ . The asymmetry of the output envelopes is due to the asymmetry of  $T_{FET}$ . Fig. 8 shows AM/AM hysteresis loops. In these 2 figures, the  $v_g$  envelope is normalized to  $2V_g$ , and  $i_d$  envelopes are normalized to their maximum values, that is, 0.41 A, 0.38 A, 0.34 A, 0.33 A. The difference frequencies of the two tones are 1 kHz, 2 kHz, 10 kHz, 50 kHz, respectively.

The size of an AM/AM hysteresis loop depends on both magnitude and angle of  $Z_{th}$ , and then the loop-opening is also bandwidth-dependent, as is shown in Fig. 8.

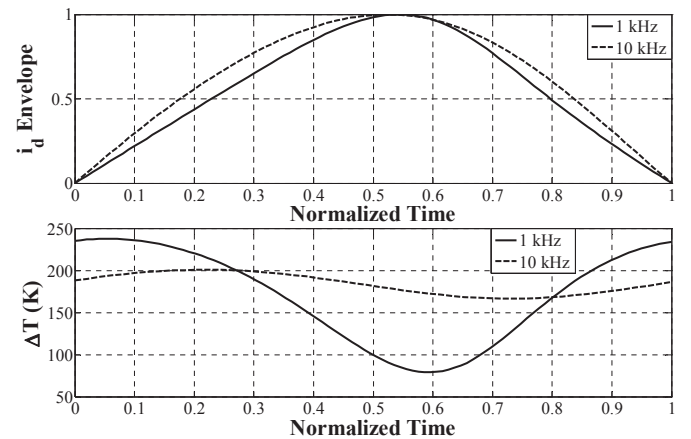


Fig. 7. Simulation results of output envelopes and  $\Delta T$  in a half of the envelope period at  $V_g = 2$  V. For each tone spacing, time starts at a zero point of the envelope and normalized to  $\frac{2\pi}{\omega_2 - \omega_1}$ .

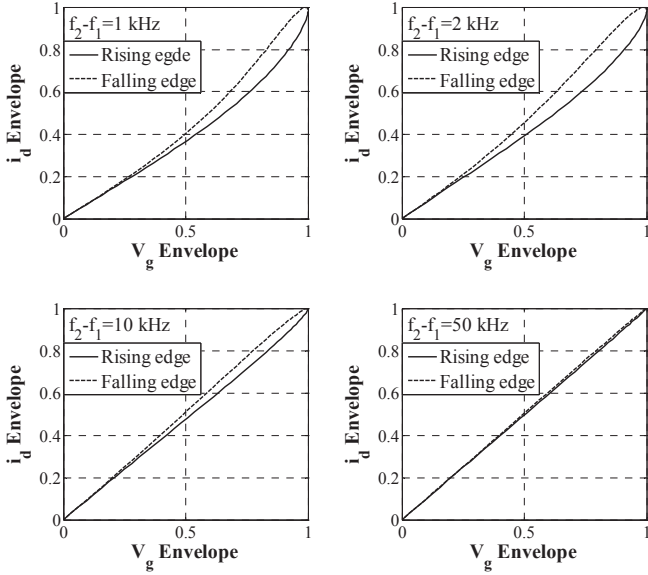


Fig. 8. Simulation results of AM/AM hysteresis loop opening caused by self-heating at  $V_g = 2$  V. Input and output envelopes are normalized to their maximum values respectively.

#### E. Response to Stepped RF signal

Fig. 9 shows that under step single-tone excitation, at the rising edges of the input envelope, the output envelope rises exponentially while  $T_{\text{FET}}$  drops exponentially. In addition, at the falling edges of the input envelope, the output envelope drops exponentially while  $T_{\text{FET}}$  rises exponentially.

The step response of the output envelope is due to the thermal response of the FET. Due to this step response, the output signal magnitude depends not only on the present input but also on the previous input.

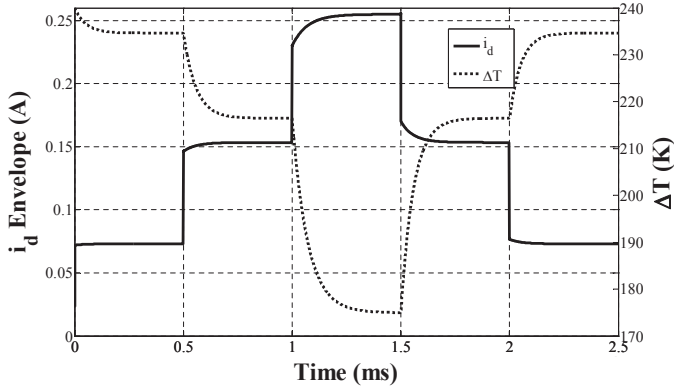


Fig. 9. Simulation results of output envelope and  $\Delta T$  under step single-tone excitation.  $V_g$  starts at 0 V, steps to 1 V at 0 ms, to 2 V at 0.5 ms, to 3 V at 1 ms, to 2 V at 1.5 ms and to 1 V at 2 ms.

## IV. CONCLUSION

On the basis of physical properties of FETs, this paper explains how self-heating can cause memory effects in an RF

PA. Thermal properties of FETs have low pass characteristics. Under two-tone excitation, while the difference frequency is lower than the cut-off frequency of the low-pass thermal circuit, the FET temperature and hence the transconductance changes periodically at the difference frequency. This periodically changing transconductance generates new spectral components, causes AM/AM hysteresis loop opening, and introduces magnitude and phase variation to output signals. All these effects are bandwidth dependent and disappear while the difference frequency is outside the pass band of the thermal circuit. Under stepped single-tone excitation, the thermal response causes an exponential increase and decrease of the output envelope.

Simple mathematics is formulated to describe the mechanism by which self-heating generates memory effects. As an outcome of the theoretical analysis, a time domain modeling framework is proposed and implemented. Simulation results are shown to agree with the theoretical analysis.

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