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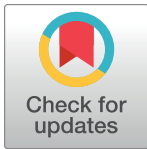
Meenal Datta, McCarthy Kennedy, Saeed Siri, Laura Via, James W. Baish, Lei Xu, Veronique Dartois, Clifton Barry, and Rakesh Jain

RESEARCH ARTICLE

Mathematical model of oxygen, nutrient, and drug transport in tuberculosis granulomas

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Abstract

Physiological abnormalities in pulmonary granulomas—pathological hallmarks of tuberculosis (TB)—compromise the transport of oxygen, nutrients, and drugs. In prior studies, we demonstrated mathematically and experimentally that hypoxia and necrosis emerge in the granuloma microenvironment (GME) as a direct result of limited oxygen availability. Building on our initial model of avascular oxygen diffusion, here we explore additional aspects of oxygen transport, including the roles of granuloma vasculature, transcapillary transport, plasma dilution, and interstitial convection, followed by cellular metabolism. Approximate analytical solutions are provided for oxygen and glucose concentration, interstitial fluid velocity, interstitial fluid pressure, and the thickness of the convective zone. These predictions are in agreement with prior experimental results from rabbit TB granulomas and from rat carcinoma models, which share similar transport limitations. Additional drug delivery predictions for anti-TB-agents (rifampicin and clofazimine) strikingly match recent spatially-resolved experimental results from a mouse model of TB. Finally, an approach to improve molecular transport in granulomas by modulating interstitial hydraulic conductivity is tested *in silico*.

Author summary

Treatment failure in infectious diseases such as tuberculosis is often the result of inadequate drug delivery to the site of infection. In the case of tuberculosis, that site is most commonly a pulmonary granuloma—an abnormal mass of immune cells that forms in the lung in response to the body's attempt to confine and constrain the infection-causing bacteria. Within the granuloma interior, blood vessels are non-functional or absent, and the tissue is dense and fibrous. These physiological abnormalities hinder not only drug delivery, but also oxygen and nutrient availability to the immune cells fighting off the infection.

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Here, we mathematically examine the basis and scope of the poor delivery of oxygen, glucose, and tuberculosis-fighting drugs in granulomas. Our simulations agree with experimental results from animal models of this disease and reveal potential strategies to overcome physiological barriers to drug delivery in granulomas.

Introduction

Tuberculosis (TB) afflicts roughly one-third of the global population and causes approximately 1.5 million deaths annually [1]. Its treatment often requires a lengthy drug therapy, in part because the dormant *Mycobacterium tuberculosis* bacilli hide within the core of hardened cellular masses in lungs called granulomas that offer a significant barrier to the transport of nutrients and therapeutic drugs. It is, thus, important to understand the flux of small molecules within granulomas, so that strategies might be devised to overcome transport limitations and hence improve treatment outcomes.

In order to reach the granuloma-contained bacilli, drugs must travel via the circulatory system to the lesion site, exit the granuloma vasculature (i.e., transvascular transport), and traverse the granuloma interior (i.e., interstitial transport) before encountering its target (i.e., cellular metabolism) [2]. A related area of study wherein the path of circulating agents to and through abnormal masses has been thoroughly explored is the field of tumor transport [3,4]. Indeed, TB granulomas and cancerous solid tumors are morphologically similar, resulting in similar transport limitations that have implications for therapeutic delivery and efficacy. As we have previously reported, a shared characteristic of these two cellular structures is an abnormal vasculature that is non-uniformly distributed within the tissue, resulting in avascular, diffusion-dominated regions, and thus, poor oxygen and drug delivery [5].

Within tumors, transvascular transport is compromised by the poorly formed and leaky tumor vasculature [6]. This negatively impacts interstitial transport, exacerbated further by a lack of functional lymphatics, which in normal physiological settings serve a crucial role in homeostatic fluid balance within tissues [7]. Impaired drainage by non-functional lymph vessels combined with abnormal, hyper-permeable blood vessels, results in an overall reduced pressure difference between the blood vessel and the interstitium [7], which is the driving force for transcapillary plasma exchange. This increases the interstitial fluid pressure (IFP), thereby reducing the effectiveness of the convective delivery of oxygen, nutrients, and drugs from the blood vessels within the core of the tumors, and hence providing a considerable barrier to effective delivery of anti-tumor agents. Although an absence of lymph vessels has not been confirmed within TB granuloma masses, we posit here that a similar IFP rise occurs within TB granulomas, as we have previously shown that granuloma blood vessels are structurally and functionally abnormal in the same manner as tumor blood vessels—and can even be “normalized” using the same targeted pharmacological approaches as for cancer [5].

The rise in IFP toward the core causes a radially outward convective flow of interstitial fluid velocity (IFV) oozing out at the periphery, thwarting the inward diffusion of drugs and nutrients [8,9]. Interstitial diffusion, particularly of macromolecules, is further impeded by a dense cellular matrix. This has motivated many studies of tumor transport so that impediments to anti-cancer therapies can be understood and strategies developed to overcome them [10–14]. Although IFP and IFV have not yet been directly measured within granulomas as they have been in tumors, we posit that a similar phenomenon occurs in TB, as we have found that other aspects including vasculature and hypoxia have been found to be analogous between the two lesion types in our prior experimental work [5].

The observable physiological abnormalities motivate a better understanding of the disease etiology and the underlying physicochemical properties that result in granuloma transport limitations. We first addressed this via a mathematical analysis of interstitial *diffusion* to quantitatively describe the emergence of hypoxic and necrotic granuloma regions as a direct result of limited oxygen availability [15]. We now build upon these findings to include both *convection and diffusion* in the variably perfused regions in the granuloma microenvironment (GME). Because of the morphological similarities between tumors and granulomas, the substantial tumor transport modeling and experimental literature was leveraged to guide this approach; thus, results are shown for both abnormal masses.

Materials and methods

The description here is limited to the physiological basis (Fig 1) and main equations. The complete model derivation, assumptions, boundary conditions, parameter values, analytical solutions, and additional findings are provided in S1 Text. Results were plotted in Figs 2–7 for IFP (from Eq S30), IFV (from Eq S33), and chemical species concentrations (from Eq S14) from the main equations described below in Model Formulation and Assumptions and in S1 Text, using the built-in function “NDSolve” in Mathematica (Wolfram Research Inc., Champaign, IL).

Model formulation and assumptions

We assume here that the transcapillary exchange of oxygen is limited to an outer thoroughly vascularized shell [5,15]. The rest of the GME is considered as completely avascular, thus allowing the assumptions of: 1) no extravasation, and 2) only diffusive (and no convective) transport therein (Fig 1). (In reality, the blood microvessel density declines more gradually [5], instead of an abrupt transition between well-perfused and inner regions assumed in our shell-core model; see S1 Fig). The main equations governing the figures shown in the Results are as follows (see S1 Text for the governing equations and derivation).

Transport of oxygen and other small molecules in an idealized, spherical, vascularized granuloma can be written as a one-dimensional (radial) mass balance in the interstitial space (equivalent to Eq S11 in S1 Text)

$$\underbrace{\frac{\partial C_j}{\partial t}}_{\text{Accumulation}} + \underbrace{v_r \frac{\partial C_j}{\partial r}}_{\text{Convection}} - \underbrace{D_j^e \left(\frac{2}{r} \frac{\partial C_j}{\partial r} + \frac{\partial^2 C_j}{\partial r^2} \right)}_{\text{Diffusion}} = - \underbrace{\frac{k C_j}{1 + K C_j}}_{\text{Reaction}} + \underbrace{L_p a_v (p_{v,e} - p_i) (C_{j,b} - C_j)}_{\text{Extravasation and Dilution}} \quad (\text{Eq1})$$

Where, for any chemical species *j* (e.g., oxygen, a nutrient, or a drug), its concentration is *C_j*, which varies with respect to time (*t*) and radial location (*r*) within the idealized granuloma (Fig 1). Compared to our prior computational model (which only considered diffusion and reaction), we now include convection, extravasation, and dilution terms which we describe in detail here. On the left-hand side: 1) the accumulation term becomes 0 assuming steady-state (i.e., no accumulation of oxygen in the GME), and 2) the convection (second term on the left; *v_r* is the radial interstitial fluid velocity) and diffusion (third term on the left; *D_j^e* is the effective diffusion coefficient of species *j* in the interstitial fluid) terms account for interstitial transport of species *j*. On the right-hand side: 3) the reaction term is assumed to follow Michaelis-Menten kinetics of cellular consumption (e.g., of oxygen, where *k* is the first-order rate constant for species consumption and *K* is the inverse of the half-saturation Michaelis-Menten constant) [15], while 4) the last term includes transvascular transport (i.e., extravasation) and plasma dilution (where *L_p* is the hydraulic conductivity of the membrane-like blood vessel wall, *a_v* is the volumetric vessel surface area in the tissue, *p_{v,e}* is the effective vessel pressure, *p_i* is the

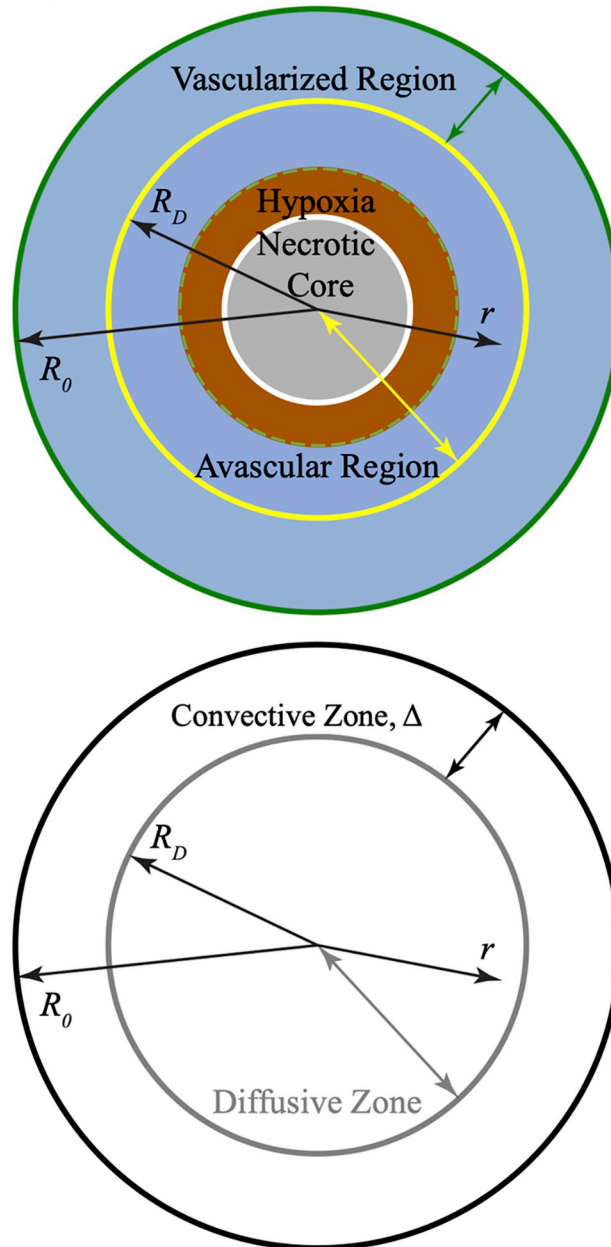


Fig 1. Physiological basis for compartmentalized transport models in TB granulomas. Schematic depicting regions and consequences of compromised oxygen transport in idealized spherical granulomas, including 1) a vascularized region where convection dominates and plasma filtration from blood vessels occurs, and 2) an inner region lacking blood vessels where diffusion dominates, and hypoxia and necrosis result. (Adapted from [15]).

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interstitial fluid pressure, and $C_{j,b}$ is the bulk concentration of the species j in plasma). In dimensionless form (dimensionless terms defined in Eq S12 in S1 Text), the steady-state mass balance (in terms of dimensionless species concentration f over dimensionless radial distance ξ) reduces to (equivalent to Eq S14 in S1 Text)

$$\frac{d^2f}{d\xi^2} - \left\{ (Pe_{R_0})v - \frac{2}{\xi} \right\} \frac{df}{d\xi} - \phi^2 \left(\frac{f}{1 + \chi f} \right) + (\alpha^2 \omega) \varrho (1 - f) = 0 \tag{EqII}$$

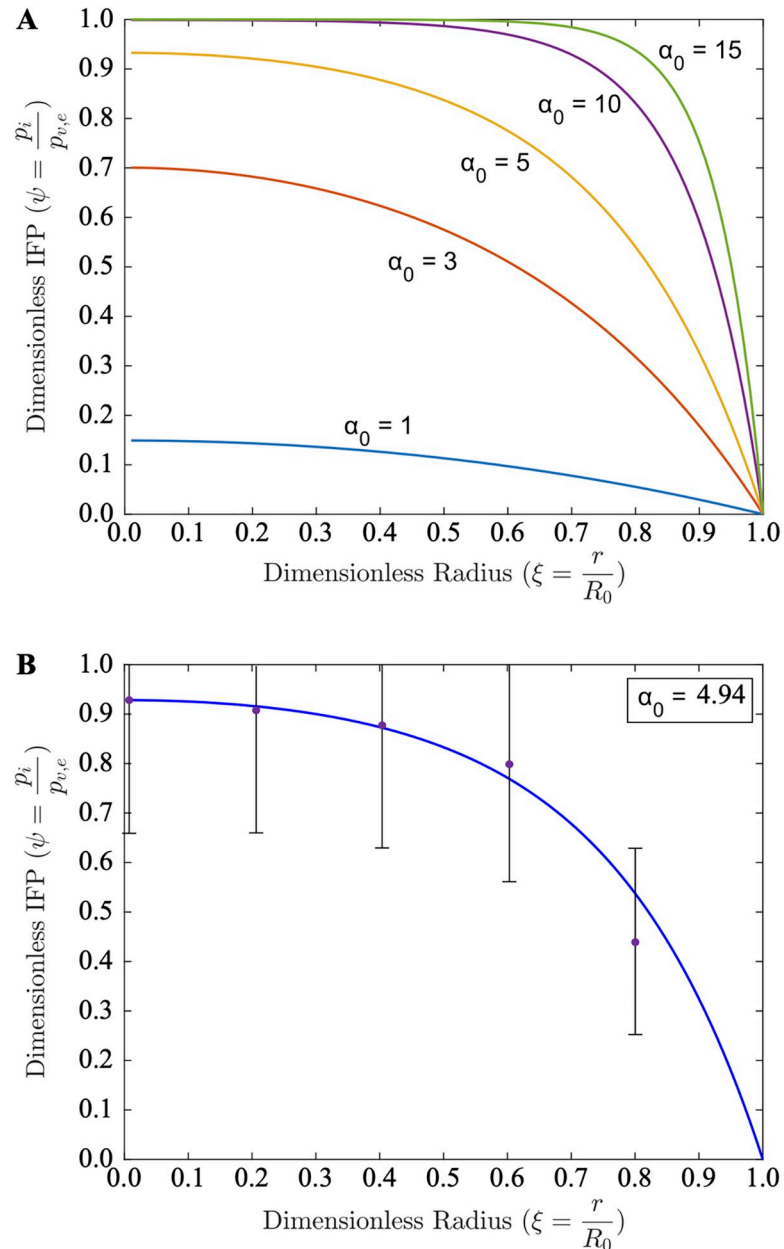


Fig 2. Granuloma IFP estimates and comparisons to tumor data. (A) Predicted dimensionless IFP profiles within granulomas from the uniform perfusion case for varying values of dimensionless granuloma size, $\alpha_0 = 1-15$. (B) Fitting the theoretical IFP estimates (Eq III with a fitted modulus $\alpha_0^2 = 24.4$ [9], see S1 Text) to experimentally measured tumor IFP data (from human neuroblastoma tumor models grown in immunosuppressed rats, ~2 cm in diameter [9]) demonstrates the applicability of the uniform perfusion model to physiological IFP levels with a single fitted parameter.

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where Pe is the Péclet number, i.e., the ratio of convective to diffusive transport, v is the dimensionless radial interstitial velocity, ϕ^2 is the Thiele modulus, i.e., the ratio of reaction to diffusion rates, χ is the dimensionless Michaelis-Menten kinetic factor, α is the dimensionless modulus (i.e., granuloma size), ω is the dimensionless diffusion rate, and ρ is the relative extravasation/dilution rate.

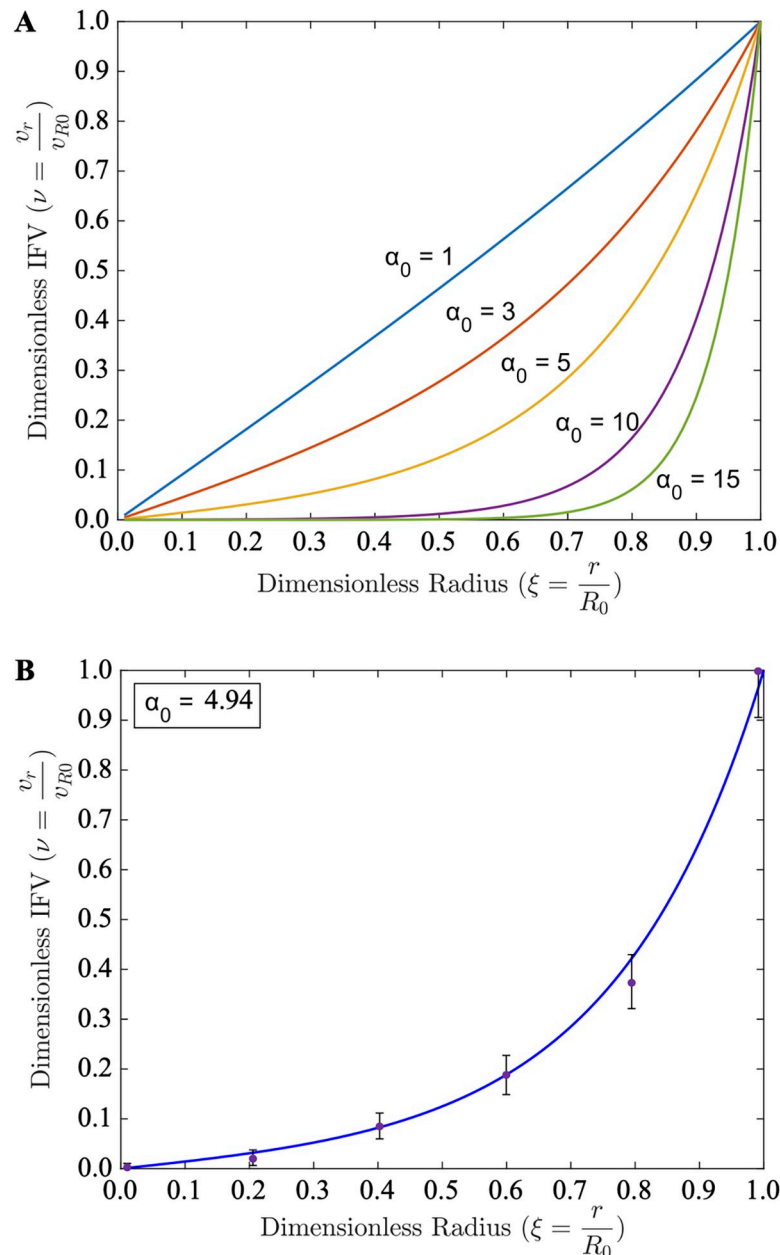


Fig 3. Granuloma IFV estimates and comparisons to tumor data. (A) Predicted dimensionless IFV profiles within granulomas from the uniform perfusion case for varying values of dimensionless granuloma size, $\alpha_0 = 1$ –15. (B) Fitting the theoretical IFV estimates (Eq IV with a fitted modulus $\alpha_0^* = 24.4$ [9], see S1 Text) to experimentally measured tumor IFV data [9] demonstrates the applicability of the uniform perfusion model to physiological IFV levels with a single fitted parameter.

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Explicit expressions for interstitial fluid pressure and velocity derive from the steady-state continuity equation, subject to suitable assumptions and boundary conditions (Eq S14 and S21) as described in the S1 Text. Upon testing multiple perfusion distribution scenarios (S1–S3 Figs), the idealized case of uniform perfusion was selected as the final form used here, given the striking similarity of its analytical solutions to the physiological reality of non-uniform perfusion (S3 Fig). In dimensionless forms, the radial IFP and IFV are, respectively (equivalent to

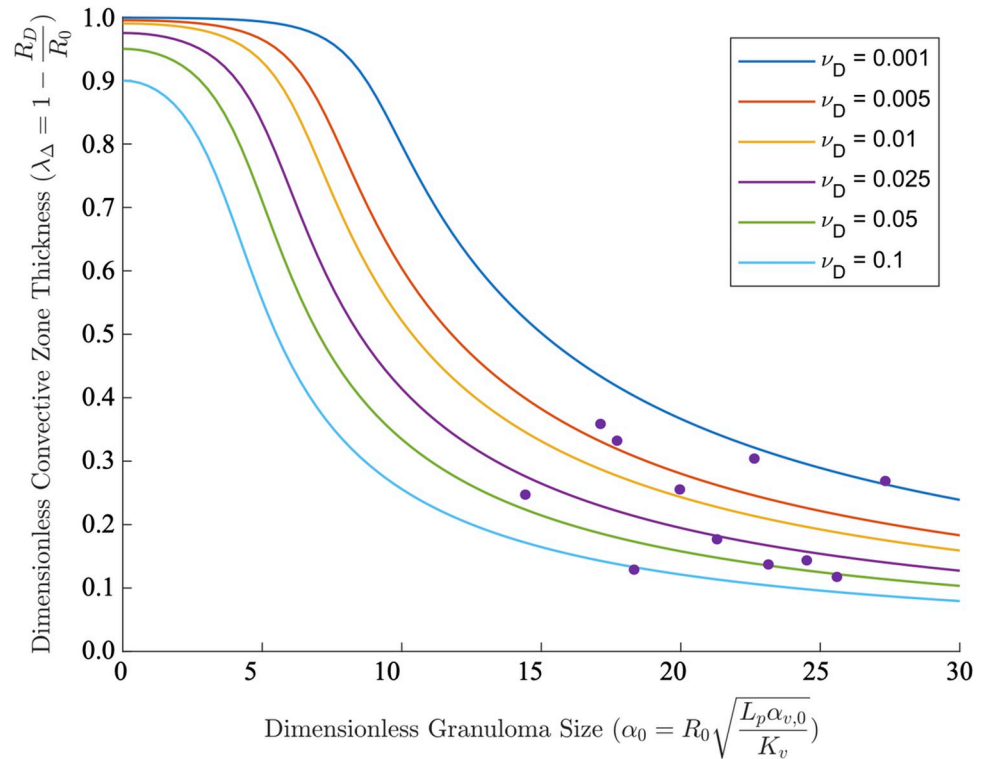


Fig 4. Granuloma convective zone thickness estimates and comparisons to experimental granuloma data. Dimensionless convective zone thickness, λ_{Δ} (lines), as a function of dimensionless granuloma size ($0 < \alpha_0 < 30$) for varying values of dimensionless limiting perfusion velocity, ν_D / ν_{D0} (as defined in the S1 Text), in comparison to experimental data from rabbit TB granulomas [15] (gray dots).

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Eqs S30 and S33 in S1 Text)

$$\psi = 1 - \varrho = 1 - \frac{1 \sinh(\alpha_0 \xi)}{\xi \sinh(\alpha_0)} \tag{EqIII}$$

$$v = \left(\frac{1}{\alpha_0 \coth \alpha_0 - 1} \right) \frac{1}{\xi^2} \left\{ \frac{(\alpha_0 \xi) \cosh(\alpha_0 \xi)}{\sinh \alpha_0} - \frac{\sinh(\alpha_0 \xi)}{\sinh \alpha_0} \right\} \tag{EqIV}$$

where ψ is dimensionless IFP, v is dimensionless IFV, and α_0 is the dimensionless form of the outer granuloma radius (i.e., maximum dimensionless modulus).

Experimental data and parameter values

To the best of our knowledge, although IFP and IFV are well-studied in cancerous tumors, they have thus far not been theoretically investigated nor experimentally measured in TB granulomas. This means that any corroboration of the theoretical results must depend on corresponding experimental results for tumors. We predict TB granuloma pressure and velocity profiles in the Results, hypothesizing that granuloma properties are similar to those of tumors (Eq S39 and Eq S41 in S1 Text) based on our previous observations of morphological and functional similarities between cancerous tumors and TB granulomas in experiments [5]. Using tumor parameter values, the dimensionless granuloma size (i.e., the modulus α) should be in the range of $\alpha_0 = 1-15$ in our simulations, as a common granuloma diameter in the rabbit

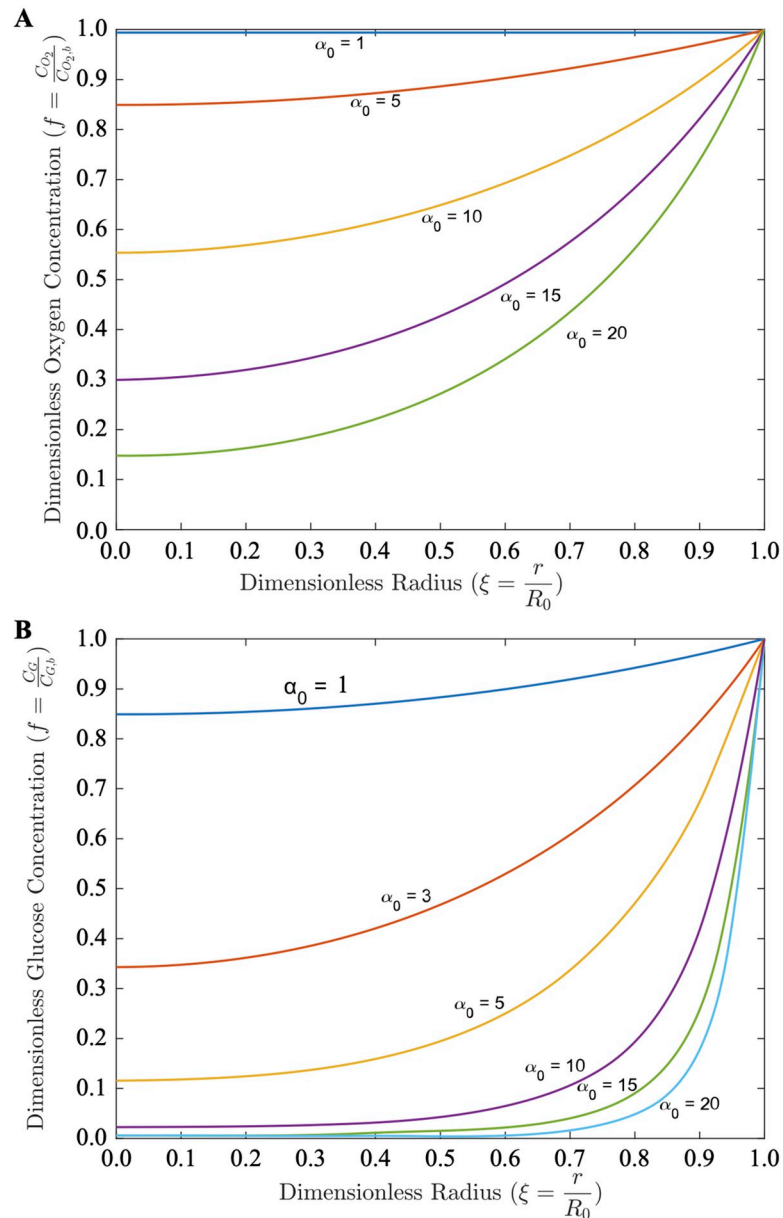


Fig 5. Granuloma oxygen and glucose profile estimates. Dimensionless concentration, f , of oxygen (A) and glucose (B) as a function of dimensionless granuloma radius, ξ , for increasing values of dimensionless granuloma size (the modulus α_0).

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model is $2R_0 = 0.5\text{--}5$ mm (although they can coalesce into larger lesions) [5,16]. We compare these simulations to IFP/IFV data from tumor models [9]. The oxygen consumption Michaelis-Menten parameters are utilized based on our previous work in rabbit TB granulomas [15]. Drug delivery data from mouse models of TB [17] are compared to our simulations, with estimated tissue diffusion coefficients informed by anti-TB drug uptake in rats [18]. All parameters are summarized in **S1 Table** and all raw and predicted drug delivery data and calculated mean square error (MSE) values are in **S2 Table**.

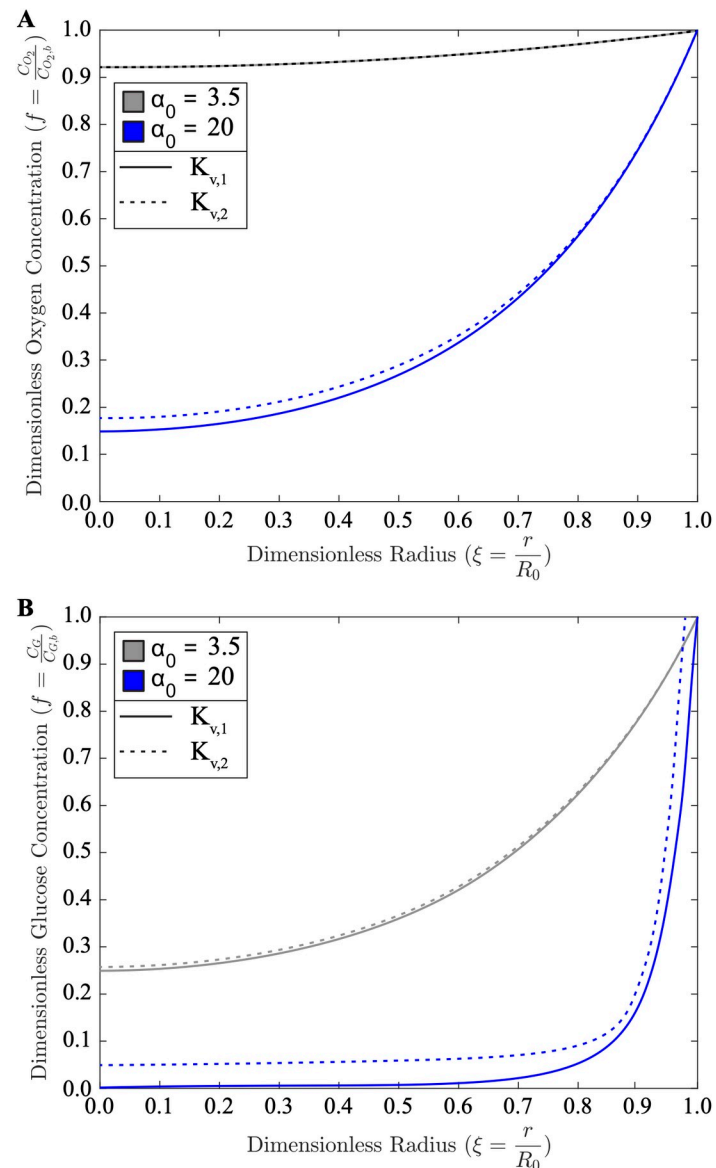


Fig 6. Effect of tissue hydraulic conductivity on oxygen and glucose delivery. (A) Oxygen and (B) glucose concentration profiles for base case parameter values (Eq S39, see S1 Text) of tissue hydraulic conductivity K_v , increased by a factor of 10 for small ($\alpha_0 = 3.5$) and large ($\alpha_0 = 20$) granulomas.

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Results

Interstitial Fluid Pressure and Velocity Radial Profiles

We and others have experimentally and theoretically investigated the interstitial fluid pressure (IFP) in tumors [8,19–26]. We hypothesize here that there is an analogous IFP rise within TB granulomas, which has not yet been experimentally investigated. Theoretical IFP (Fig 2A) and IFV (Fig 3A) profiles are shown for varying values of the modulus α . IFP rises with distance into the granuloma, while effusive IFV follows an opposite trend and decreases towards the interior of the granuloma. We theorize in analogy to tumors [8] that i) the plasma that leaks out of the abnormal blood vessels as previously described [5] causes this rise in the IFP towards

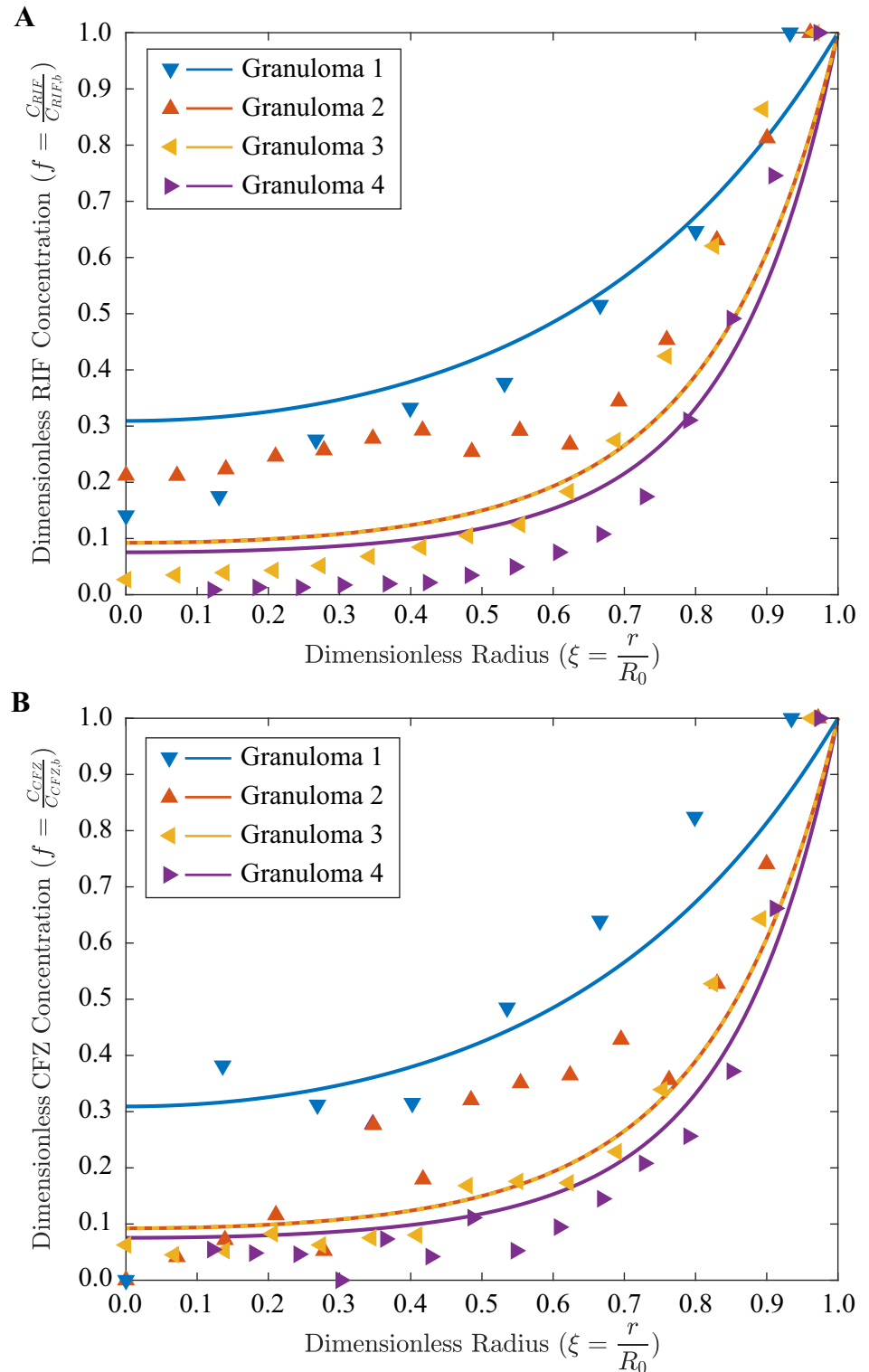


Fig 7. Estimates of drug delivery and comparisons to rifampicin and clofazimine distribution data in experimental granulomas. Dimensionless concentration (lines), f , of rifampicin (A; RIF) and clofazimine (B; CFZ) as a function of dimensionless granuloma radius, ξ , for increasing values of dimensionless granuloma size (the modulus α_0) in comparison to experimental data from mouse TB granulomas [17] (dots). The mean squared error (MSE, see Eq S44) between the theoretical and experimental results for rifampicin and clofazimine are 0.012 and 0.010, respectively (see S2 Table for all raw data, predicted data, and MSE values).

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the granuloma core and ii) this is exacerbated by a paucity of functional lymph vessels. As IFP rises, the pressure drop declines until it eventually becomes zero. This is given by the Starling equation that accounts for the plasma flux across the microvessel walls between i) the effective vessel pressure ($p_{v,e} \equiv p_v - \sigma_s(\pi_v - \pi_i)$), where p_v is the vascular pressure (mmHg), π_v and π_i are the vascular and interstitial osmotic pressures (mmHg), respectively, and σ_s is the Staverman reflection coefficient) and ii) the IFP (p_i , mmHg). This is especially apparent for larger granulomas (Fig 2A, $\alpha_0 > 10$), where the IFP approaches the effective vessel pressure rapidly with increasing distance towards the core.

As a result of the reducing pressure differential, the effusive (or filtration) flux of plasma, ϕ_B , from the blood vessels (bearing oxygen, nutrients, and drugs) declines in the inward radial direction eventually becoming zero. Consequently, at this point, there is no further source for oxygen as well as other nutrients or small molecules/drugs, so that beyond this point the radial flux of these entities is entirely by their diffusion along with any interstitial (albeit compromised) fluid convection. Thus, IFV drops and stagnates in the core; this is especially apparent for large granulomas (Fig 3A, $\alpha_0 > 10$) where the IFV drops to zero rapidly with increasing distance into the granuloma. At the periphery of the granuloma ($r \rightarrow R_0$) we may infer that, as in tumors [8], the IFV is directed outwards, which would further impede transport in the GME.

Model comparisons to experimental IFP/IFV measurements

DiResta et al. measured IFP and IFV in human neuroblastoma tumor models in rats [9]. Our predictive models of IFP (Fig 2B) and IFV (Fig 3B) align well with these experimental measurements (despite large error bars from the *in-situ* measurements) using a fitted value of $\alpha_0 = 4.95$, analogous to S3 Fig. Thus, the simple analytical solution for the uniform perfusion case is strikingly accurate in predicting *in vivo* IFP/IFV levels, even in large lesions that are presumably non-uniformly perfused and likely contain hypoxic and necrotic regions.

Convective zone thickness

As depicted schematically in Fig 1, convection dominates in the vascularized, well-perfused outer rim of the GME, i.e., the region closest to the normal lung parenchyma. We can estimate the thickness of this rim ($\Delta = R_0 - R_D$, Fig 1) by assuming that within this shell, the pressure gradient becomes small enough that convective velocity approaches 0, representing the turning point at which diffusion dominates (i.e., this can be defined as the limited perfusion velocity; see S1 Text). Utilizing this assumption in Eq IV (equivalent to Eq S33 from the S1 Text), the dimensionless thickness of the convection zone, λ_Δ , is obtained and plotted vs. granuloma size for varying limited perfusion velocities (Fig 4). For small granulomas ($\alpha_0 < 5$), the majority of the GME is predicted to be well-vascularized; this aligns with experimental observations [5,16]. For $5 < \alpha_0 < 10$, the convective zone thickness drastically declines with increasing granuloma size until, at $\alpha_0 > 10$, it plateaus. This indicates that for large granulomas, the convection zone occupies less than half of the total mass thickness and the thickness of the convection zone becomes independent of total granuloma size. Utilizing our previously collected data for convective zone thickness from the rabbit TB model [15], in conjunction with theoretical parameter estimates from tumors (Eq S39 in S1 Text), we observe good agreement between our predicted and experimental results.

Oxygen and glucose concentration profiles

Expanding our previous modeling of avascular granulomas limited to diffusive transport combined with cellular consumption [15], our current model predicts oxygen concentration profiles while accounting for transcapillary exchange, plasma dilution, and interstitial convection

and diffusion (Fig 5A). As expected, oxygen concentration drops quickly with distance into the granuloma core with increasing granuloma size. For $\alpha_0 > 10$, oxygen is predicted to be fully consumed rapidly within the GME; in reality, we know from prior measurements that necrosis emerges due to cell death at oxygen levels nearing—but not reaching—anoxia [5,16]. Similar profiles result from the modeling of glucose transport (Fig 5B)—a slightly larger chemical species with poorer diffusivity (S1 Table) than molecular oxygen—resulting in more rapid consumption of this nutrient particularly for $\alpha_0 > 10$, wherein the central GME is predicted to be devoid of glucose.

Overcoming interstitial transport barriers

The effect of tissue hydraulic conductivity on oxygen transport can be observed via *in silico* perturbation, whereby the simulated dimensionless oxygen concentration profile within the GME is shown for when the estimated base case parameter of tissue hydraulic conductivity K_v (Eq S39 in S1 Text) is increased by a factor of 10 for small ($\alpha_0 = 3.5$) and large ($\alpha_0 = 20$) granulomas (Fig 6A). For both small and large granulomas, increasing hydraulic conductivity does not significantly affect oxygen concentration. However, in the large granuloma, the base value hydraulic conductivity value results in the glucose concentration dropping quickly to zero around a dimensionless radius value of 0.5 (Fig 6B). This implies that this nutrient is theoretically absent from the central GME under base tissue hydraulic conductivity. Significantly increasing tissue hydraulic conductivity (e.g., by drug treatment), results in glucose not being fully consumed before reaching the granuloma core. Indeed, a paucity of glucose is no longer predicted to emerge even in this very large simulated granuloma with the improvement in hydraulic conductivity, which suggests improved glucose distribution in the granuloma core.

Model comparisons to experimental drug delivery measurements in granulomas

Finally, this model can be applied not only to oxygen and nutrient delivery, but to anti-TB drug delivery as well. In a recent study [17], Kokesch-Himmelreich et al. measured drug delivery of rifampicin (RIF; molecular weight = 823 g/mol), clofazimine (CFZ; molecular weight = 473 g/mol), and other antibacterial agents using the spatially-resolved matrix-assisted laser desorption/ionization mass spectrometry imaging (MALDI-MSI) method in murine TB granulomas. We extracted and non-dimensionalized the spatially-resolved drug delivery data for RIF and CFZ in four granulomas (all $R_0 < 0.5$ mm, $\alpha_0 < 5$), from this paper [17]. Strikingly, our simple mass transport model accurately predicts the delivery of these two anti-TB agents, with low MSE values of ~ 0.01 for both drugs (Fig 7 and S2 Table).

Discussion

A detailed understanding of the drug transport barriers within granulomas can illuminate causes underlying the necessary prolonged treatment for TB, and suggest approaches to alleviate these physiological abnormalities of the GME that hinder transport. Thus, analogous modeling approaches from cancer research are applied here, based on the structural and morphological similarities between TB granulomas and tumors [5] despite the obvious differences between the two disease etiologies. Indeed, common modeling approaches for tumors that have been explored in TB granulomas by us and others include reaction-diffusion [15,27], continuum [28,29], agent-based [30–32], and multiscale [33–35] models, and vascular network/angiogenesis models from tumors [36,37] are likely to be applied to TB granulomas in the future. The approximate analytical solution we obtained previously [15], for the case of diffusion-limited reaction, was able to predict the size of hypoxic and necrotic regions in good

agreement with our experimental results from the rabbit TB model. Here, we extended our mathematical framework to include the effect of convective transport within the GME as a result of its abnormal vasculature, and to determine its impact on oxygen, nutrient, and drug delivery.

Model features, findings, and limitations

Transport phenomena including pressure rise, velocity profile, and interstitial diffusion, are dependent on the structural properties of the GME. We assume that the TB granuloma structure is similar to that of a tumor [21], which is comprised of three regions [5,15]: 1) the vascular region, limited to the periphery and devoid of functional lymphatic vessels; 2) the cellular region containing the cells; and 3) the interstitial (extra-cellular) space that contains an extra-cellular matrix network that imparts mechanical rigidity, bathed in interstitial fluid. We have shown previously that granuloma vessels are structurally and functionally abnormal, leading to inhomogeneous transport [5]. In tumors, this aberrant vasculature compromises transvascular and interstitial convection due to high vessel permeability and an increase in IFP from plasma leakage and a lack of functional lymphatics. Together, these effects result in an outward convective interstitial velocity that opposes inward transport. By assuming that the GME recapitulates these transvascular and interstitial transport limitations seen in tumors based on our prior experimental evidence [5], the objective of our modeling effort was to predict these parameters and to indicate fruitful directions for future experimental investigations.

We provide here a comprehensive theoretical model of oxygen transport and reaction within a granuloma (or a tumor) that accounts for non-uniform vasculature, transcapillary exchange, plasma dilution, and interstitial convection and diffusion. Three limiting models of vasculature distribution were considered simultaneously for the first time: a model of uniform MVD distribution, a shell-core model, and a non-uniform MVD distribution model. Based on our analyses for IFP and IFV, we can conclude that the simpler case of uniform MVD distribution is adequate for predicting species transport and reaction. In contrast to earlier tumor IFP/IFV models [8,19], our model accounts for plasma dilution (which is often excluded in the literature as negligible). Our mass balance formulation accounts for plasma extravasation from blood vessels not only as a source for oxygen, nutrients, and drugs, but as a diluent as well. Indeed, our model of interstitial transport was found to be in accord with tumor experiments. Predictions of convective zone thickness were found to be in agreement with experimental data from granulomas. The model was also utilized to theoretically investigate the effect of enhanced tissue hydraulic conductivity for overcoming transport barriers. Finally, our model accurately predicted the delivery of two anti-TB agents—rifampicin (first-line therapy) and clofazimine (second-line therapy)—with surprisingly good agreement given the simplicity of the mathematics describing the underlying transport phenomena.

In short, this model sheds light on the limitations of oxygen, nutrient, and drug transport within granulomas and tumors, and how such barriers might be overcome. For example, it predicts an IFP rise towards the granuloma core as a result of the known abnormal vasculature. This in turn results in a reduced or even stagnated IFV, compromising interstitial convective transport and thus depriving the granuloma core—where the bacilli hide—of oxygen, nutrients, and drugs. Our model predicts an absence of glucose in the granuloma core; this warrants experimental confirmation. The persistent bacteria in the hypoxic and necrotic core are able to utilize alternative carbon sources (e.g., lactate) [38]; thus, these metabolic alterations may present targetable vulnerabilities for therapeutic strategies. Modulating the interstitial hydraulic conductivity, e.g., with an agent targeting the interstitial components (such as losartan, a widely-prescribed, safe and inexpensive anti-hypertensive drug [39]), could prove to be an

effective host-directed therapeutic strategy to modulate the GME and improve drug delivery and efficacy.

There are some limitations to the model. As described in detail in [S1 Text](#), the non-uniform and/or shell-core models of perfusion better represent the physiological reality of blood vessel distribution in granulomas than the uniform perfusion model. However, the simpler limiting case of uniform perfusion advantageously allows for analytical solutions that 1) do not require artificially defining regions where convection or diffusion dominate, 2) are in good agreement when fitted with the non-uniform perfusion numerical solutions, and, most importantly, 3) accurately predict IFP/IFV experimental data. We also ignore cell membrane transport as a factor in the mass balance equation; however, we account for the cellular reaction of the species (i.e., oxygen consumption). Because we do not have experimental parameter measurements for TB granulomas (e.g., membrane and interstitial hydraulic conductivities) we apply tumor parameter values to the model given the similarities between granulomas and tumors, based on our previous experimental and computational observations regarding shared morphological and functional characteristics of these diseased masses (including vascular density, architecture, and perfusion) [5,15]. We also do not consider variable oxygen/nutrient/drug uptake rates by different types of immune cells, e.g., macrophages vs. T cells, which we have recently demonstrated experimentally can contribute to heterogeneous drug distribution within the GME [40]. Finally, because we do not consider the transport of large molecules here, we ignore any retardation factor. Indeed, because anti-TB agents often bind to proteins such as albumin [41], it may become necessary to model the unbound vs. bound drug fractions in future considerations.

Future directions

To the best of our knowledge, we provide here the first consideration of convective transport in the GME, and initial predictions for IFP and IFV profiles and their associated consequences in TB granulomas. To further support these findings, it should be experimentally confirmed whether—as in tumors—TB granulomas lack functional lymphatics. It should be noted that the first predictions of tumor IFP/IFV [8] preceded, yet accurately predicted, the first experimental measurements of these parameters by a number of years [42–47]. We posit that future IFP/IFV measurements in TB granulomas will similarly confirm our predictions here. Continued comparison of tumors and TB granulomas via modeling may reveal novel similarities and differences between these two types of masses, particularly with regards to immune state and function. Furthermore, our findings support future testing of host-directed therapies that can modulate the GME to overcome transport barriers and improve treatment outcomes for this virulent and deadly disease. Indeed, following recent efforts by others to computationally optimize the implementation of multiple antibiotic treatments [48], future modeling efforts should provide rational basis for multi-drug dosing and scheduling.

Supporting information

S1 Text. Supporting Information. S1. Species mass balance in granulomas and tumors. S2. Interstitial fluid pressure and velocity profiles. S2.1. Shell-core model of non-uniform perfusion in granulomas. S2.2. Uniform perfusion case. S2.3. Non-uniform perfusion case. S3. Comparison of interstitial perfusion for varying vascular distribution. S3.1. Predictions with the shell-core model. S3.2. Predictions with the uniform vasculature model. S3.3 Comparisons with the non-uniform vessel distribution. S4. Overcoming transport barriers. S5. Convective zone thickness. S6. Mean squared error. Abbreviations, symbols, and terminology. (DOCX)

S1 Table. Parameter values for the mathematical model of transport in TB granulomas. (DOCX)

S2 Table. Experimental (Exp.), modeled (Mod.), and differences (Diff) between experimental and modeled data for drug delivery in TB granulomas for CFZ and RIF delivery, with MSE calculated on a per granuloma basis. (DOCX)

S1 Fig. Granuloma microvascular density and non-uniform perfusion estimates. Comparison of experimental microvessel density (MVD; dots) in rabbit granulomas [5] versus fitting (lines) via Eq S34 (see S1 Text) for the following parameters: $\beta = 1/2$; $R_0 = 3$ mm $L_p = 2.8 \times 10^{-7}$ cm \cdot mmHg $^{-1}\cdot$ s $^{-1}$, $K_v = 4.13 \times 10^{-8}$ cm $^2\cdot$ mmHg $^{-1}\cdot$ s $^{-1}$, $N_{v,0} = 1,000$, and $a_{v,0} = 200$ cm $^2\cdot$ cm $^{-3}$. (TIFF)

S2 Fig. Granuloma IFP estimates from the shell-core model. Predicted dimensionless (A) IFP and (B) IFP profiles within granulomas for different moduli α_0 and for the shell-core perfusion model, with $\xi_D = 0.5$. (TIFF)

S3 Fig. Granuloma IFP estimate comparisons from non-uniform, shell-core, and uniform perfusion models. Predicted dimensionless IFP rise within granulomas for the uniform (Eq III), shell-core (Eq S25, see S1 Text), and non-uniform perfusion (Eq S35) models for case of $\alpha_0 = 6$, with an additional fitted uniform perfusion case for $\alpha_0 = 4.1$. (TIFF)

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Mathematical Model of Oxygen, Nutrient, and Drug Transport in Tuberculosis

Granulomas

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S1. Species Mass Balance in Granulomas and Tumors

A blood-borne molecular nutrient or drug species undergoes the following sequential transport steps (1, 2) within a granuloma or a tumor: 1) extravasation across the capillary wall; 2) transport through the interstitial space via convection and diffusion; 3) transport across a cell membrane; and 4) metabolic reaction within the cell. We neglect the cell membrane transfer resistance here, but account for the cellular reaction of a species. Further, for larger molecules such as monoclonal antibodies or proteins, not considered here, there is specific or non-specific binding (3).

We adopt a coarse-grained continuum approach, and start with the molar form of unsteady-state mass balance of species j (oxygen, nutrient, or a drug) within the granuloma or tumor (4), i.e.,

$$\frac{\partial C_j}{\partial t} + \nabla \cdot \mathbf{N}_j = R_j \quad (\text{Eq.S1})$$

where R_j is the volumetric source term for species j . The flux of a species j , in general, contains both convective and diffusive terms, which for dilute solutions is of the form (4)

$$\mathbf{N}_j = \boldsymbol{\nu} C_j - D_j^e \nabla C_j \quad (\text{Eq.S2})$$

19 The effective diffusivity D_j^e of a molecule in the interstitial region may be estimated from
 20 its molecular diffusion coefficient D_j via the relation $D_j^e = (\varepsilon/\tau)D_j$ (5), where ε is the
 21 volume fraction (or void fraction) of interstitial space among the cells, and τ is the so-
 22 called tortuosity factor, accounting for the tortuous diffusion paths. This is based on the
 23 assumption that the transport is limited to the interstitial domain. This is not true for
 24 molecules such as oxygen, which might well diffuse through the cellular region as well.
 25 Further, the tortuosity factor in turn can be related to the interstitial volume fraction. For
 26 example, the random pore model suggests $\tau = 1/\varepsilon$. More generally, $\tau = 1/\varepsilon^q$, where, q
 27 = 0.5 refers to the so-called Bruggeman exponent. Other factors besides the structure,
 28 e.g., partition coefficient, or solubility, can also affect the effective diffusion coefficient of
 29 a molecule (1, 6). Finally, since we are not considering large molecules, we ignore any
 30 retardation factor (1).

31 Combining the last two relations and carrying out the indicated differential operation

$$\frac{\partial C_j}{\partial t} + \boldsymbol{v} \cdot \nabla C_j + C_j \nabla \cdot \boldsymbol{v} - D_j^e \nabla^2 C_j = R_j \quad (\text{Eq.S3})$$

32 The convective term itself is, thus, comprised of two parts: 1) the usual *convective* term
 33 $\boldsymbol{v} \cdot \nabla C_j$, and 2) the *dilution* term $C_j \nabla \cdot \boldsymbol{v}$ containing the divergence of fluid velocity, $\nabla \cdot \boldsymbol{v}$.
 34 For transport in incompressible fluids (liquids), the second term is typically zero, since
 35 from the equation of continuity $\nabla \cdot \boldsymbol{v} = 0$ (4). However, for a granuloma or a tumor
 36 comprising of blood and lymphatic vessels that provide a net source/sink term for the
 37 fluid, the equation of continuity, i.e., overall mass balance, instead takes the form (3, 5)

$$\nabla \cdot \boldsymbol{v} = \varphi_B(\mathbf{r}) - \varphi_L(\mathbf{r}) \quad (\text{Eq.S4})$$

38 where $\varphi_B(\mathbf{r})$ (s^{-1}) is the position (\mathbf{r}) dependent interstitial fluid source term i.e., the net
 39 volumetric rate of plasma extravasated by blood vessels per unit volume of the granuloma
 40 or tumor, while $\varphi_L(\mathbf{r})$ is the corresponding term for the drainage of the interstitial fluid by
 41 lymphatics. In biological tissues these terms represent the rate of plasma flow from blood
 42 vessels into the interstitial space, and from interstitial space into the lymph vessels,
 43 respectively (see Reference (5) for schematic representations).

44 The distribution of these vessels is well-known to vary with location \mathbf{r} , within the tumor
 45 (3), and has also been shown to similarly vary within granulomas (8). In the case of the
 46 diffusion-limited region (denoted by subscript D), where there is a complete absence of
 47 such vessels, Eq.S4 reduces to the common form of the equation of continuity, $\nabla \cdot \boldsymbol{\nu} = 0$.

48 Combining the last two relations, the mass balance in granulomas or tumors takes the
 49 form

$$\frac{\partial C_j}{\partial t} + \boldsymbol{\nu} \cdot \nabla C_j - D_j^e \nabla^2 C_j = R_j - C_j(\varphi_B - \varphi_L) \quad (\text{Eq.S5})$$

50 Further, in the above, the net rate of the species “source” term R_j within the tissue is a
 51 sum of two terms: 1) that due to reaction, and 2) that due to the fluid source term

$$R_j = -\frac{kC_j}{1 + KC_j} + \varphi_B C_{j,b} \quad (\text{Eq.S6})$$

52 where the metabolic reaction rate term is assumed of the Michaelis-Menten (MM) form,
 53 as is common for many cellular reactions, with a negative sign denoting “consumption,”
 54 rather than generation, while the source term of species j from the blood vessels is $\varphi_B C_{j,b}$,
 55 where $C_{j,b}$ is the concentration of the species j in the bulk plasma. The MM kinetics
 56 appropriately reduce to first-order when $KC_j \ll 1$, with a pseudo-first order rate constant

57 k , while it reduces to zero-order for the case when $KC_j \gg 1$, when kinetic rate is equal to
 58 k/K (9). In terms of the more traditional form, the MM kinetics are written as: $r_j =$
 59 $V_{max}C_j/(K_M + C_j)$, where the MM parameters, $V_{max} = k/K$, and the MM constant, $K_M =$
 60 $1/K$. In our recent publication (9), further, only the first term in Eq.S6 was included, as
 61 applicable to the diffusion-dominated quiescent inner region where there are no blood
 62 vessels. This assumption is relaxed here.

63 Combining the last two relations

$$\frac{\partial C_j}{\partial t} + \boldsymbol{v} \cdot \nabla C_j - D_j^e \nabla^2 C_j = -\frac{kC_j}{1 + KC_j} + \varphi_B(C_{j,b} - C_j) + \varphi_L C_j \quad (\text{Eq.S7})$$

64 which in one-dimensional (radial) form

$$\frac{\partial C_j}{\partial t} + v_r \frac{\partial C_j}{\partial r} - D_j^e \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial C_j}{\partial r} \right) = -\frac{kC_j}{1 + KC_j} + \varphi_B(C_{j,b} - C_j) + \varphi_L C_j \quad (\text{Eq.S8})$$

65 This formulation is a bit different from the corresponding mass balance equations in the
 66 literature, because it accounts for the effect of extravasation not only as a source for
 67 species j but also as a diluent, latter by virtue of the use of equation of continuity, Eq.S4.

68 In solid tumors, further, there are few functional lymph vessels, and so that $\varphi_L \rightarrow 0$ (1).
 69 Even if this were not completely true, certainly $\varphi_B \gg \varphi_L$, as blood vessels are leakier in
 70 tumors, so that φ_L may be neglected. We make the same assumption here for TB
 71 granulomas. Further, carrying out the indicated differentiation in the Laplacian term, the
 72 species mass balance reduces to

$$\frac{\partial C_j}{\partial t} + v_r \frac{\partial C_j}{\partial r} - D_j^e \left(\frac{2}{r} \frac{\partial C_j}{\partial r} + \frac{\partial^2 C_j}{\partial r^2} \right) = -\frac{kC_j}{1 + KC_j} + \varphi_B(C_{j,b} - C_j) \quad (\text{Eq.S9})$$

73 The plasma flux across the microvessel walls is further given by the Starling equation (3,
74 5)

$$\varphi_B \equiv \frac{J_v}{V} = L_p a_v \{(p_v - p_i) - \sigma_S(\pi_v - \pi_i)\} = L_p a_v (p_{v,e} - p_i) \quad (\text{Eq.S10})$$

75 where J_v/V is the volumetric flow rate out of the vasculature per unit volume of tissue, L_p
76 is the membrane hydraulic conductivity of vessels ($\text{cm}^4/\text{s}\cdot\text{mmHg}$) within the granuloma,
77 $a_v(r)$ is the surface area of the vessels/volume of tissue (cm^2/cm^3), i.e., S/V , which varies
78 with location r , owing to the heterogeneous nature of blood vessel distribution in
79 granulomas or tumors. For example, $a_v = N_v(\pi d_v)l_v$, where $N_v(r)$ is the number density
80 of microvessels/volume, and d_v and l_v are their average diameter and length.

81 Further, p_v and p_i are the vascular and interstitial pressures (mmHg), respectively, while
82 π_v and π_i are the corresponding osmotic pressures (mmHg), and σ_S is the Staverman
83 reflection coefficient. In other words, the driving force is the hydrostatic pressure
84 difference minus the osmotic pressure difference between the inside of the vessels and
85 the interstitial space in tissue. For a single solute, for instance, the osmotic pressure, $\pi =$
86 $-(RT/\bar{V}_j)\ln a_j$, i.e., it depends on the species activity or concentration. Further, in Eq.S10,
87 we have defined an effective vessel pressure, $p_{v,e} \equiv p_v - \sigma_S(\pi_v - \pi_i)$.

88 Combining the last two equations

$$\begin{aligned} \underbrace{\frac{\partial C_j}{\partial t}}_{\text{Accumulation}} + \underbrace{v_r \frac{\partial C_j}{\partial r}}_{\text{Convection}} - \underbrace{D_j^e \left(\frac{2}{r} \frac{\partial C_j}{\partial r} + \frac{\partial^2 C_j}{\partial r^2} \right)}_{\text{Diffusion}} \\ = - \underbrace{\frac{kC_j}{1 + KC_j}}_{\text{Reaction}} + \underbrace{L_p a_v (p_{v,e} - p_i) (C_{j,b} - C_j)}_{\text{Extravasation and Dilution}} \end{aligned} \quad (\text{Eq.S11})$$

89 where the different transport (convection and diffusion), accumulation, and source
 90 (reaction and extravasation) terms are as indicated. This may be compared to the mass
 91 balance equation of our previous work (9), that assumes: 1) that the flux is by diffusion
 92 only (i.e., $v_r = 0$, or no convection), and 2) that the last term on the right, accounting for
 93 transcapillary extravasation and plasma dilution, is zero as there are no blood vessels in
 94 the diffusion-limited region. In other words, it involves only diffusion and reaction, as in a
 95 conventional catalyst particle, the convection and the fluid source term being assumed
 96 zero.

97 For this, we next non-dimensionalize this mass balance equation using the following
 98 dimensionless variables

$$\xi \equiv \frac{r}{R_0}; \psi \equiv \frac{p_i}{p_{v,e}}; \varrho \equiv 1 - \frac{p_i}{p_{v,e}}; f \equiv \frac{C_j}{C_{j,b}}; v \equiv \frac{v_r}{v_{R_0}}; Pe_{R_0} \equiv \frac{v_{R_0} R_0}{D_j^e};$$

$$\phi \equiv R_0 \sqrt{\frac{k}{D_j^e}}; \alpha(\xi) \equiv R_0 \sqrt{\frac{L_p a_v(\xi)}{K_v}}; \chi \equiv K C_{j,b}; \tau \equiv \left(\frac{D_j^e}{R_0^2}\right) t; \omega \equiv \frac{K_v p_{v,e}}{D_j^e};$$
(Eq.S12)

99 It is noteworthy that for given membrane and tissue properties, the modulus $\alpha \propto R_0$, since
 100 the square root term is independent of granuloma/tumor size, i.e., a bigger modulus
 101 means a larger granuloma/tumor. In other words, the modulus α may be roughly
 102 considered as dimensionless radius of granuloma/tumor.

103 In dimensionless form, the mass balance, thus, the unsteady-state mass balance for
 104 species j is

$$\frac{\partial f}{\partial \tau} + (Pe_{R_0})v \frac{\partial f}{\partial \xi} - \left(\frac{2}{\xi} \frac{\partial f}{\partial \xi} + \frac{\partial^2 f}{\partial \xi^2} \right) = -\phi^2 \frac{f}{1 + \chi f} + (\alpha^2 \omega) \varrho (1 - f) \quad (\text{Eq.S13})$$

105 Besides the dimensionless concentration, $f(\xi)$, this equation involves the convection
 106 term on the left that is a function of ξ via the dimensionless velocity $v(\xi)$, as well as the
 107 extravasation term, i.e., the last term on the right, also a function of ξ via the
 108 dimensionless pressure difference $\varrho(\xi)$. Thus, other relations are needed for $v(\xi)$ and
 109 $\varrho(\xi)$, as discussed next.

110 For the steady-state case, the species mass balance reduces to

$$\frac{d^2 f}{d\xi^2} - \left\{ (Pe_{R_0})v - \frac{2}{\xi} \right\} \frac{df}{d\xi} - \phi^2 \left(\frac{f}{1 + \chi f} \right) + (\alpha^2 \omega) \varrho(1 - f) = 0 \quad (\text{Eq.S14})$$

111 subject to the boundary conditions

$$\begin{aligned} \text{B.C. 1:} \quad & \text{at } \xi = 1 \quad f = 1 \\ \text{B.C. 2:} \quad & \text{at } \xi = 0 \quad \frac{df}{d\xi} = 0 \end{aligned}$$

112 The expressions for the dimensionless interstitial velocity $v(\xi)$ and the volumetric effusion
 113 term, $\Omega(\xi) \equiv \alpha^2 \omega \varrho(\xi)$, are developed in the next section.

114 **S2. Interstitial Fluid Pressure and Velocity Profiles**

115 We and others have experimentally and theoretically investigated the interstitial fluid
 116 pressure (IFP) in tumors (1, 3, 7, 10-15). It is hypothesized that there is an analogous IFP
 117 rise within TB granulomas, not yet experimentally investigated, as modeled below (5).

118

119 The steady-state equation of continuity, or fluid mass balance, Eq.S4 provides $\nabla \cdot \boldsymbol{v} =$
 120 $\varphi_B(\mathbf{r}) - \varphi_L(\mathbf{r})$, which is combined with the constitutive equation for viscous flow in porous
 121 media, namely D'Arcy's law, $\boldsymbol{v} = -(B_0/\mu)\nabla p_i$, normally written in the tumor literature as
 122 (15)

$$\boldsymbol{v} = -K_v \nabla p_i \quad (\text{Eq.S15})$$

123 where $K_v \equiv (B_0/\mu)$, is the so-called hydraulic conductivity of the tumor or granuloma,
 124 while B_0 is the D'Arcy permeability, to provide

$$-K_v \nabla^2 p_i = \varphi_B - \varphi_L \quad (\text{Eq.S16})$$

125 Using the Laplacian for a one-dimensional transport in a spherical shaped granuloma,
 126 Eq.S16 reduces to

$$-K_v \frac{1}{r^2} \frac{d}{dr} \left(r^2 \frac{dp_i}{dr} \right) = \varphi_B - \varphi_L \quad (\text{Eq.S17})$$

127 Assuming as above, that either $\varphi_L \rightarrow 0$, or that $\varphi_B \gg \varphi_L$, for the TB granulomas and
 128 combining Eqns. (Eq.S10) and (Eq.S17)

$$-K_v \frac{1}{r^2} \frac{d}{dr} \left(r^2 \frac{dp_i}{dr} \right) - L_p a_v (p_{v,e} - p_i) = 0 \quad (\text{Eq.S18})$$

129 where recall that $a_v = a_v(\xi)$. This can be written in the dimensionless form

$$\frac{1}{\xi^2} \frac{d}{d\xi} \left(\xi^2 \frac{d\varrho}{d\xi} \right) - \alpha^2 \varrho = 0 \quad (\text{Eq.S19})$$

130 where recall that the dimensionless interstitial pressure *difference*, $\varrho \equiv (p_{v,e} - p_i)/p_{v,e} =$
 131 $1 - \psi$, and the dimensionless interstitial pressure, $\psi \equiv p_i/p_{v,e}$.

132 In general, as indicated above, the microvessel surface area per unit volume also varies
 133 with location, i.e., $a_v = a_v(\xi)$, so that the parameter $\alpha = \alpha(\xi)$. We consider three different
 134 cases for the vasculature architecture as described below:

- 135 1) the case of uniform perfusion throughout the granuloma/tumor, wherein $a_v =$
 136 $a_{v,0} = \text{constant}$, i.e., independent of ξ ;
- 137 2) the case of non-uniform perfusion described via step change (3), wherein the
 138 diffusion-limited hypoxic core has no vessels ($a_v = 0$), while the outer shell of

139 the granuloma/tumor is fully vascularized ($a_v = a_{v,0}$), i.e., the shell-core model,

140 and

141 3) the case of non-uniform perfusion with a realistic variation in microvessel

142 density (MVD) distribution, $N_v = N_v(\xi)$.

143 The first two cases allow analytical solution for the IFP and IFV, while the last requires a

144 numerical solution. We consider below the more general Case 2 first, from which Case 1

145 derives as a limiting case.

146 **S2.1. Shell-Core Model of Non-uniform Perfusion in Granulomas**

147 Adapting the approach of Baxter and Jain (1990) for tumors to granulomas, it is assumed

148 here that in the region $R_D < r < R_0$, $a_v = a_{v,0}$, while in the region $r < R_D$, $a_v = 0$. Thus,

149 the modulus $\alpha = \alpha_0$ in the shell region, defined as

$$\alpha_0 \equiv R_0 \sqrt{\frac{L_p a_{v,0}}{K_v}} \quad (\text{Eq.S20})$$

150 which represents a ratio of the interstitial resistance to vascular resistance to IF flow.

151 The momentum balance equation is subject to the following boundary conditions (16):

$$\text{BC 1: at } \xi = 1, \quad \varrho = 1, \text{ i.e., } \psi = 0 \text{ (or } p_i = 0),$$

$$\text{BC 2: at } \xi = \xi_D, \quad \frac{d\varrho}{d\xi} = 0; \quad \varrho = \varrho_D. \quad (\text{Eq.S21})$$

152 where the first boundary condition specifies that the pressure at the periphery, $p_i = 0$,

153 while the second represents no flow, or pressure gradient, along with continuity of

154 pressure at the diffusion-limited core radius R_D .

155 The general solution to Eq.S19, which is of the same form as that for molecular diffusion

156 and first order reaction in granuloma (9), is

$$\varrho = \frac{C_1}{\xi} \cosh(\alpha_0 \xi) + \frac{C_2}{\xi} \sinh(\alpha_0 \xi) \quad (\text{Eq.S22})$$

157 which upon differentiating provides

$$\frac{d\varrho}{d\xi} = \frac{C_1}{\xi^2} \{\alpha_0 \xi \sinh(\alpha_0 \xi) - \cosh(\alpha_0 \xi)\} + \frac{C_2}{\xi^2} \{\alpha_0 \xi \cosh(\alpha_0 \xi) - \sinh(\alpha_0 \xi)\} \quad (\text{Eq.S23})$$

158 Using B.C. 2 in Eq.S23 while using B.C. 1 in Eq.S22, and solving the resulting two
 159 equations simultaneously for the two unknown constants of integration C_1 and C_2 , followed
 160 by some simplification, provides

$$C_1 = -\frac{\sinh(\alpha_0 \xi_D) - \alpha_0 \xi_D \cosh(\alpha_0 \xi_D)}{\sinh[\alpha_0(1 - \xi_D)] + \alpha_0 \xi_D \cosh[\alpha_0(1 - \xi_D)]} \quad (\text{Eq.S24})$$

$$C_2 = -\frac{\alpha_0 \xi_D \sinh(\alpha_0 \xi_D) - \cosh(\alpha_0 \xi_D)}{\sinh[\alpha_0(1 - \xi_D)] + \alpha_0 \xi_D \cosh[\alpha_0(1 - \xi_D)]}$$

161 Using these in Eq.S22 and simplifying further, the dimensionless pressure differential (16)

$$\varrho(\xi) = \frac{1}{\xi} \left\{ \frac{\sinh[\alpha_0(\xi - \xi_D)] + \alpha_0 \xi_D \cosh[\alpha_0(\xi - \xi_D)]}{\sinh[\alpha_0(1 - \xi_D)] + \alpha_0 \xi_D \cosh[\alpha_0(1 - \xi_D)]} \right\} \quad (\text{Eq.S25})$$

162 where we have used the identities, $\sinh(u - v) = \sinh u \cosh v - \cosh u \sinh v$ and
 163 $\cosh(u - v) = \cosh u \cosh v - \sinh u \sinh v$. These results are applicable to the shell
 164 region, i.e., for $\xi_D \leq \xi \leq 1$. The dimensionless pressure differential in the non-
 165 vascularized core of the particle is obtained by setting $\xi = \xi_D$ in Eq.S25.

166 Further, taking the derivative of the dimensionless pressure gradient, and combining it
 167 with the 1-dimensional Darcy's law $v_r = -K_v(dp_i/dr) = K_v p_{v,e}/R_0(d\varrho/d\xi)$, provides the
 168 velocity profile within a granuloma

$$v_r = \frac{K_v p_{v,e}}{R_0} \frac{1}{\xi^2} \left\{ \frac{\alpha_0(\xi - \xi_D) \cosh[\alpha_0(\xi - \xi_D)] - (1 - \alpha_0^2 \xi_D \xi) \sinh[\alpha_0(\xi - \xi_D)]}{\sinh[\alpha_0(1 - \xi_D)] + \alpha_0 \xi_D \cosh[\alpha_0(1 - \xi_D)]} \right\} \quad (\text{Eq.S26})$$

169 which when evaluated at the granuloma surface ($\xi = 1$), yields the efflux velocity at the
 170 surface

$$v_{R_0} = \left(\frac{K_v p_{v,e}}{R_0} \right) \left\{ \frac{\alpha_0(1 - \xi_D) \cosh[\alpha_0(1 - \xi_D)] - (1 - \alpha_0^2 \xi_D) \sinh[\alpha_0(1 - \xi_D)]}{\sinh[\alpha_0(1 - \xi_D)] + \alpha_0 \xi_D \cosh[\alpha_0(1 - \xi_D)]} \right\} \quad (\text{Eq.S27})$$

171 The surface effusion velocity could alternately be determined as follows. From the Gauss-
 172 Ostrogradskii divergence theorem (4), $\int^V (\nabla \cdot \boldsymbol{v}) dV = \int^S (\boldsymbol{v} \cdot \boldsymbol{n}) dS$, and using Eq.S4 for
 173 the divergence of velocity in this, along with Eq.S10 for the volumetric efflux φ_B , there
 174 results

$$v_{R_0} = \left(\frac{K_v p_{v,e}}{R_0} \right) \int_{\xi_D}^1 (\alpha^2 \varrho) \xi^2 d\xi \quad (\text{Eq.S28})$$

175 Finally, assuming $\alpha = \alpha_0$, using Eq.S25 for ϱ and integrating, Eq.S27 results.

176 From Eq.S26 and Eq.S27, the dimensionless velocity, $v \equiv v_r / v_{R_0}$,

$$v = \frac{1}{\xi^2} \left\{ \frac{\alpha_0(\xi - \xi_D) \cosh[\alpha_0(\xi - \xi_D)] - (1 - \alpha_0^2 \xi_D \xi) \sinh[\alpha_0(\xi - \xi_D)]}{\alpha_0(1 - \xi_D) \cosh[\alpha_0(1 - \xi_D)] - (1 - \alpha_0^2 \xi_D) \sinh[\alpha_0(1 - \xi_D)]} \right\} \quad (\text{Eq.S29})$$

177 The above algebraic relations for the dimensionless pressure difference ϱ , Eq.S25, and
 178 the dimensionless IF velocity v , Eq.S29, can be utilized in the steady-state species j mass
 179 balance differential equation, Eq.S14. In other words, Eq.S14, Eq.S25, and Eq.S29
 180 together form a set of differential-algebraic equations that can be solved simultaneously
 181 numerically to compute the concentration profile of a molecule within a granuloma. We
 182 have already solved the concentration profile, Eq.S14, for the case of no convective flow
 183 ($v = 0$) as well as no source term ($\Omega = 0$), where we also provided analytical solutions for
 184 the two limiting cases of first- and zero-order kinetics (9). Our analysis here extends our

185 initial results to the more general case to include both convective transport ($v \neq 0$) as well
 186 as a source term ($\Omega \neq 0$).

187 **S2.2. Uniform Perfusion Case**

188 For the case when there is no hypoxic core, $\xi_D \rightarrow 0$, i.e., the granuloma is uniformly
 189 perfused throughout, then the corresponding relations may be obtained by simply setting
 190 $\xi_D = 0$ in the above. Thus, from Eq.S25, the dimensionless pressure rise within the
 191 granuloma for the case of uniform perfusion (5)

$$\psi = 1 - \varrho = 1 - \frac{1}{\xi} \frac{\sinh(\alpha_0 \xi)}{\sinh(\alpha_0)} \quad (\text{Eq.S30})$$

192 The radial velocity profile from Eq.S26

$$v_r = \left(\frac{K_v p_{v,e}}{R_0} \right) \frac{1}{\xi^2} \left\{ \frac{(\alpha_0 \xi) \cosh(\alpha_0 \xi)}{\sinh \alpha_0} - \frac{\sinh(\alpha_0 \xi)}{\sinh \alpha_0} \right\} \quad (\text{Eq.S31})$$

193 while the efflux velocity at the granuloma surface, from Eq.S27 with $\xi_D = 0$

$$v_{R_0} = \left(\frac{K_v p_{v,e}}{R_0} \right) (\alpha_0 \coth \alpha_0 - 1) \quad (\text{Eq.S32})$$

194 so that the dimensionless velocity profile takes the form (5)

$$v = \left(\frac{1}{\alpha_0 \coth \alpha_0 - 1} \right) \frac{1}{\xi^2} \left\{ \frac{(\alpha_0 \xi) \cosh(\alpha_0 \xi)}{\sinh \alpha_0} - \frac{\sinh(\alpha_0 \xi)}{\sinh \alpha_0} \right\} \quad (\text{Eq.S33})$$

195 These simpler alternate relations for the volumetric fluid effusion and the dimensionless
 196 IFV applicable for the case of uniform vasculature can next be utilized in the species j
 197 mass balance, Eq.S14, to obtain concentration profile within a granuloma or a tumor.

198 **S2.3. Non-uniform Perfusion Case**

199 In the above shell-core model, we considered the case where the granuloma/tumor was
 200 assumed to be fully vascularized outside of the hypoxic core, while there was no perfusion

201 within it. This is not physically realistic, as the microvessel density (MVD) distribution does
 202 not change so abruptly, but rather more gradually. In fact, the MVD distribution in a
 203 granuloma has been measured by us (8), as shown in **Figure S1**.

204 Clearly the blood vessels are restricted to the granuloma periphery and tend to be absent
 205 from the central region, as we found previously (8), but this change happens gradually.
 206 In fact, it might be argued that the MVD distribution appears to follow the pressure
 207 difference distribution, i.e., the extravasation driving force, $\varrho = 1 - \psi$. As a result, in
 208 analogy with Eq.S30, we might simply assume the MVD distribution

$$\frac{N_v(\xi)}{N_{v,0}} = \frac{a_v(\xi)}{a_{v,0}} = \frac{\alpha(\xi)}{\alpha_0} = \frac{1 \sinh(\beta\alpha_0\xi)}{\xi \sinh(\beta\alpha_0)} \quad (\text{Eq.S34})$$

209 Where $\beta \sim 1/2$ is a fitted constant. This would be used in both momentum balance,
 210 Eq.S19, and mass balance, Eq.S14.

211 It is apparent from **Figure S1** that the agreement is good. There might, in fact, be
 212 physiological reasons for this. Thus, we might surmise that functional blood vessels are
 213 not present beyond the point where $p_i \rightarrow p_{v,e}$, since the plasma can no longer flow out of
 214 the blood vessels. Clearly, in this case, analytical solution for the pressure profile is not
 215 possible, and Eq.S19 must be solved numerically, which, when combined with Eq.S34,
 216 may be written as

$$\left(\frac{2}{\xi} \frac{d\varrho}{d\xi} + \frac{d^2\varrho}{d\xi^2} \right) - \alpha_0^2 \left\{ \frac{1 \sinh(\beta\alpha_0\xi)}{\xi \sinh(\beta\alpha_0)} \right\} \varrho = 0 \quad (\text{Eq.S35})$$

217 A numerical solution of this provides the pressure differential profile within the granuloma.

218 This is next related to the velocity profile via

$$v = \frac{1}{v_{R_0}} \left(\frac{K_v p_{v,e}}{R_0} \right) \left(\frac{d\rho}{d\xi} \right) \quad (\text{Eq.S36})$$

219 where from Eq.S28 and Eq.S34

$$v_{R_0} = \left(\frac{K_v p_{v,e}}{R_0} \right) \alpha_0^2 \int_0^1 \left\{ \frac{\sinh(\beta \alpha_0 \xi)}{\sinh(\beta \alpha_0)} \right\}^2 \rho d\xi \quad (\text{Eq.S37})$$

220 where ρ is obtained from a solution to Eq.S35.

221 Alternately, we can write the dimensionless velocity as

$$v = \left(\frac{d\rho}{d\xi} \right) / \left(\frac{d\rho}{d\xi} \right)_{\xi=1} \quad (\text{Eq.S38})$$

222 The last two ODEs, for ρ (Eq.S35) and for v (Eq.S36 or Eq.S38), along with Eq.S14, the
 223 ODE representing the mass balance of species j , represent a system of three differential
 224 equations that need to be solved simultaneously in order to numerically obtain the
 225 pressure difference, velocity, and species j concentration profiles within the granuloma or
 226 the tumor. This is then the most general case considered here, wherein few simplifying
 227 assumptions have been made.

228 **S3. Comparison of Interstitial Perfusion for Varying Vascular Distribution**

229 Because IFP and IFV have not yet been measured experimentally in granuloma vessels,
 230 we first predict these profiles assuming that granulomas and tumors share certain
 231 physiological parameters. Thus, in combination with oxygen consumption parameters
 232 values from our previous work (9), we use the following parameter values (provided from
 233 tumors (1, 3, 5, 12-14)):

$$L_p = 2.8 \times 10^{-7} \text{ cm} \cdot \text{mmHg}^{-1} \cdot \text{s}^{-1}; \quad a_{v,0} = 200 \text{ cm}^2 \cdot \text{cm}^{-3}; K_v = 4.13 \times 10^{-8} \text{ cm}^2 \cdot \text{mmHg}^{-1} \cdot \text{s}^{-1} \quad (\text{Eq.S39})$$

234 Assuming, that these values are a good first estimate for granulomas as well,

235
$$\sqrt{\frac{L_p a_{v,0}}{K_v}} = \sqrt{\frac{2.8 \times 10^{-7} \times 200}{4.13 \times 10^{-8}}} = 36.82 \text{ cm}^{-1}$$

236 Thus, for $2R_0 = 0.5 - 5 \text{ mm}$, a common size of granulomas observed in rabbits (though
 237 they can be larger if multiple lesions coalesce) (8, 17), this provides the range of the
 238 modulus $\alpha_0 = 1 - 15$, which would hence be of the primary interest for granulomas.

239 **S3.1. Predictions with the Shell Core Model ($\xi_D > 0$)**

240 We provide figures (**Figure S2**) of dimensionless pressure rise and velocity profile
 241 (Eq.S7) for the case of $\xi_D = 0.5$ and different values of α_0 based on the use of Eqs.
 242 (Eq.S25) – (Eq.S29). These expressions are applicable to the shell region, i.e., for $\xi_D \leq$
 243 $\xi \leq 1$. For the hypoxic core, the dimensionless pressure differential is obtained by setting
 244 $\xi = \xi_D$ in Eq.S25, providing

$$\psi_0 = 1 - \varrho_0 = 1 - \frac{\alpha_0}{\sinh[\alpha_0(1 - \xi_D)] + \alpha_0 \xi_D \cosh[\alpha_0(1 - \xi_D)]} \quad (\text{Eq.S40})$$

245 As **Figure S2A** shows, the pressure rises sharply in the shell and then levels out at the
 246 value indicated by Eq.S40. In fact, for $\alpha_0 > 10$, the interstitial pressure in the particle core
 247 attains the value in the effective vascular pressure.

248 **Figure S2B** plots the resulting effusion velocity as a function of radial distance in the shell.
 249 The velocity in the core is zero, due to the absence of any pressure gradient therein. It is
 250 interesting that for small modulus α_0 , the velocity profile has a slight convexity to it. In
 251 fact, it is possible that the small α_0 values ($0 < \alpha_0 < 5$) are inconsistent with the
 252 assumptions inherent in the shell-core model, as for small α_0 , the hypoxic core is unlikely
 253 to exist.

254 **S3.2. Predictions with the Uniform Vasculature Model ($\xi_D \rightarrow 0$)**

255 The case of uniform vasculature is actually consistent with smaller values of the modulus
256 α_0 ($0 < \alpha_0 < 5$), which recall is rather a dimensionless particle radius. Nonetheless, the
257 computations for the case of uniform vasculature are provided in for the pressure rise
258 (**Figure 2**) and the velocity profile (**Figure 3**) for a variety of the values of the modulus α_0 .

259 It is evident that the maximum pressure rises at a given value of α_0 is higher for the case
260 of uniform perfusion rather than for the case of shell perfusion. The velocity profiles
261 (**Figure 3**) are also more reasonable for smaller values of α_0 than that in **Figure S2B**
262 based on assuming perfusion limited to a shell.

263 On the other hand, for the case of larger modulus α_0 ($\alpha_0 > 7$), the difference in the
264 predictions of the two models are small. In summary, we can surmise that for smaller
265 values of the modulus α_0 (smaller particles), the uniform perfusion model is a better
266 approximation, while for the case of larger particle sizes and α_0 , the shell-core model is
267 more physically realistic, but even the uniform perfusion model is adequate. In short, the
268 simpler uniform perfusion model is adequate in general.

269 It is further seen from **Figures 2** and **3** that when flow resistance of the interstitial space
270 is smaller (large K_v) than the flow resistance of the vessel walls, or when the granuloma
271 particle size is small, i.e., when $\alpha_0 \leq 1$, the pressure rise within the granuloma is small,
272 and the convective velocity of the plasma leaving the vessels is linear all the way to the
273 particle center, so that the entire granuloma is well-perfused and there is no hypoxic ring
274 or necrotic core, i.e., transport of a solute is not limited by diffusion.

275 On the other hand, when flow resistance of the interstitial space is higher (smaller K_v)
276 than the flow resistance of the vessel walls, or when the granuloma particle size is large,
277 $\alpha_0 \gg 1$, and the IFP rise is rapid, and within a short distance Δ of the particle surface, $\psi \rightarrow$
278 1 or $p_i \rightarrow p_{v,e}$. Further, in this case, the convective velocity of the plasma $v_r \rightarrow 0$ for $\xi <$
279 ξ_D , after which convective transport of oxygen/solute comes to a halt, so that the oxygen
280 and other nutrients must diffuse thereafter, resulting in a hypoxic ring, as well as a necrotic
281 core inside the granuloma. Thus, Swabb et al. (1974) concluded that for small molecules,
282 e.g., oxygen, glucose, and amino acids, the transport via diffusive mechanism is
283 dominant. On the other hand, larger molecules such as antibodies are largely dependent
284 on convective transport.

285 **S3.3. Comparisons with the Non-uniform Vessel Distribution**

286 The uniform and shell-core model microvessel distributions discussed above are two
287 limiting cases of a more realistic and gradual vessel distribution of the kind discussed
288 above. We next explore how the predictions of pressure rise, e.g., for this case are in
289 comparison to the above two limiting distributions.

290 Based on the numerical integration of Eq.S35, **Figure S3** provides a comparison of the
291 pressure rise for the case of a particle with MVD distribution as described by Eq.S34 for
292 the case of $\alpha_0 = 6$, which is rather an intermediate value in the range of interest ($0 < \alpha_0 <$
293 15). The case of uniformly distributed vessels Eq.S30 overpredicts the pressure rise in
294 comparison, while the shell-core distribution can provide a reasonable estimate provided
295 the thickness of the well-perused shell is used as a fitted parameter. Thus, in **Figure S3**,
296 the value of $\xi_D = 0.48$ provides a good approximation. For that matter, the simple uniform

297 distribution model can also provide a good estimate of the pressure profile, provided the
298 modulus α_0 is used as a fitted parameter. Thus, the use of $\alpha_0 = 4.1$ provides a pressure
299 rise profile (dotted line) that adequately mimics that resulting from the case of non-
300 uniformly distributed vessels (Eq.S35). In summary, the uniform MVD distribution model
301 would be adequate in most cases for a prediction of the pressure rise, and consequently,
302 the effusion velocity distribution while it has the advantage of simple explicit expressions.

303 **S4. Overcoming Transport Barriers**

304 To theoretically investigate the effect of improving delivery (e.g., of oxygen, nutrients, or
305 drugs) by improving the tissue hydraulic conductivity of the tumors or granulomas, we
306 retain as the base case the parameters used above, namely, those in Eq.S39, along with
307 the following typical values:

$$p_{v,e} = 20 \text{ mmHg}; R_0 = 2.5\text{mm}; k = 0.01 \text{ s}^{-1}; D_j^e = 1 \times 10^{-6} \text{ cm}^2 \text{ s}^{-1} \quad (\text{Eq.S41})$$

308 The first-order rate constant and the effective diffusion coefficient are typical of nutrient
309 of the size of glucose (18), rather than a smaller molecule such as oxygen. Larger
310 molecules (>50,000 Da), e.g., antibodies, are also of interest where a diffusion retardation
311 factor (14) may be needed to describe diffusion in the interstitial space.

312 Further, as discussed above, the simpler explicit expressions describing the IFP and IFV
313 within a granuloma or tumor for the case of uniform MVD distribution are adequate.
314 Consequently, even though the other cases discussed above, namely, the abrupt shell-
315 core model, or the more gradually declining MVD distribution described by the fitted
316 model, may be more realistic, in what follows, we will simply adopt the uniform MVD

317 distribution model (Eq.S30 and Eq.S33) for use in the steady-state species mass balance
318 relation, Eq.S14.

319 **Figure 5B** provides the simulated species distribution profile within a tumor or a
320 granuloma based on the above parameters: 1) as the base case for the hydraulic
321 conductivity provided in Eq.S39 ($K_v = 4.13 \times 10^{-8} \text{ cm}^2 \cdot \text{mmHg}^{-1} \cdot \text{s}^{-1}$) and 2) the case of
322 improved hydraulic conductivity by a factor of 10. For the parameters adopted, this means
323 the following dimensionless parameters: a Thiele modulus, $\phi = 25$; the modulus
324 characteristic of the vessel to tissue hydraulic conductivity, $\alpha_0 = 9.2$; and the parameter
325 $\omega = 0.83$. Additionally, for the base case, the surface effusion velocity from Eq.S32, $v_{R_0} =$
326 $0.27 \mu\text{m} \cdot \text{s}^{-1}$, so that the Peclet number at the surface, $Pe_{R_0} = 6.78$.

327 The hydraulic conductivity K_v can, in fact, be described in terms of tissue structural
328 parameters (15). For example (5), by visualizing a porous medium as a bundle of
329 capillaries of radius a , and using the Poiseuille equation for laminar capillary flow, $K_v =$
330 $(\varepsilon/\tau)(a^2/8\mu)$, where μ is the interstitial fluid viscosity. Other factors affecting hydraulic
331 conductivity have been discussed (1).

332 **S5. Convective Zone Thickness**

333 The convective zone thickness Δ of the outer well-perfused rim, where the dimensionless
334 concentration $f \rightarrow 1$, can be estimated from a numerical solution of the mass balance
335 equation. We are interested in approximately determining the thickness of this zone,
336 where convective transport dominates. It is necessary to select a criterion for this, e.g., at
337 a location when the pressure gradient becomes small enough so that convective velocity
338 $\rightarrow 0$ (at the edge of the diffusive, non-vascularized zone, R_D , **Figure 1**), before diffusion

339 becomes the dominant mode of transport. For this, a reasonable estimated Peclet number
 340 can be assumed, e.g., $Pe_D \ll 1$. Then from the definition of the Peclet number, one can
 341 obtain the corresponding velocity, i.e.,

$$v_D = Pe_D \left(\frac{D_{O_2}^e}{R_0} \right) \quad (\text{Eq.S42})$$

342 For example, for the case of oxygen, with $D_{O_2}^e = 2.5 \times 10^{-5} \text{ cm}^2/\text{s}$, and $R_0 = 0.25 \text{ cm}$, and
 343 assuming $Pe_D = 0.01$, the limiting perfusion velocity, $v_D = 1 \times 10^{-6} \text{ cm/s}$. Thus, the
 344 dimensionless, limiting perfusion velocity for determining the thickness Δ , $v_D \equiv v_D/v_{R_0} =$
 345 $1 \times 10^{-6}/1.36 \times 10^{-5} = 0.073$.

346 In other words, from Eq.S33 for the uniform MVD distribution case, we can determine the
 347 corresponding dimensionless convective zone thickness $\lambda_\Delta = 1 - \xi_D$, where $\xi_D \equiv R_D/R_0$,
 348 for an assumed of say $v_D \approx 0.001 - 0.1$, i.e., by solving the following

$$v_D - \left(\frac{1}{\alpha_0 \coth \alpha_0 - 1} \right) \left\{ \frac{\alpha_0 \cosh(\alpha_0 \xi_D)}{\xi_D \sinh(\alpha_0)} - \frac{1 \sinh(\alpha_0 \xi_D)}{\xi_D^2 \sinh(\alpha_0)} \right\} = 0 \quad (\text{Eq.S43})$$

349

350 **S6. Mean Squared Error (MSE)**

351 The agreement between the experimental drug delivery data and the predicted values
 352 from the model can be assessed via the MSE metric, which is reported for each
 353 granuloma and drug in **S2 Table.docx**. We calculate MSE as (Eq. S44)

$$MSE = \frac{1}{n} \sum_{i=1}^n (Y - Y')^2 \quad (\text{Eq.S44})$$

354 Where Y represents actual experimental values each measured at i^{th} observed values, Y'
 355 represents the predicted values, i is and n is the total number of data points for each
 356 granuloma. A lower MSE indicates a better fit of model predictions to observed data.

357 **Abbreviations, symbols, and terminology**
 358

Abbreviations:

B.C.	Boundary condition
CFZ	Clofazamine
Da	Dalton
GME	Granuloma microenvironment
HDT	Host-directed therapy
IFP	Interstitial fluid pressure
IFV	Interstitial fluid velocity
MM	Michaelis-Menten
MSE	Mean squared error
MVD	Microvascular density
RIF	Rifampicin
ODE	Ordinary differential equation
TME	Tumor microenvironment

Roman Symbols:

a_v	surface area of the vessels/volume of tissue (cm^2/cm^3)
B_0	D'Arcy permeability (cm^{-2})
$C_{1,2}$	Constants of integration
C_j	Concentration of chemical species j (i.e., where j is oxygen, a nutrient [e.g., glucose], or a drug) (mol/L)
C_G	concentration of glucose (mol/cm^3)
$C_{G,b}$	constant bulk concentration of glucose in the perfused region (mol/L)
C_{O_2}	concentration of oxygen (mol/cm^3)
$C_{O_2,b}$	constant bulk concentration of oxygen in the perfused region (mol/L)
$D_{CFZ,RIF}$	effective diffusion coefficient of CFZ and RIF in the interstitial fluid (mm^2/s)
D_j^e	the effective diffusion coefficient of chemical species j in the interstitial fluid (mm^2/s)
d_v	average microvessel diameter (mm)
f	dimensionless concentration of oxygen
J_v	vascular volumetric flow rate (mm^3/s)
k	first-order rate constant for oxygen consumption (s^{-1})
K	inverse of the half-saturation Michaelis-Menten constant (L/mol)
K_M	half-saturation constant of the Michaelis-Menten equation (mol/L)
K_v	hydraulic conductivity coefficient (mm/s)
L_p	membrane hydraulic conductivity of blood vessels ($\text{mm}^4/\text{s}\text{-mmHg}$)
l_v	average microvessel length (mm)
n	number of drug delivery points gathered experimentally per granuloma
N_v	microvessel density (number of microvessels/ mm^2)
p_i	interstitial fluid pressure (mmHg)
$p_{v,e}$	effective vessel pressure (mmHg)

Pe_r	Péclet number for radial transport
Pe_{R_0}	Péclet number at the granuloma-lung interface (at $r = R_0$)
Pe_Δ	Péclet number below which diffusion dominates
q	Bruggeman exponent
r	radial position in the granuloma (mm)
Δr	radial thickness over which the shell-balance is performed (mm)
R_0	radius of the granuloma (mm)
R_D	radius of diffusive region (mm)
R_j	volumetric source term for chemical species j
v_r	radial interstitial fluid velocity (mm/s)
v_Δ	radial velocity associated with Pe_Δ (mm/s)
V	granuloma/tumor volume (mm ³)
V_{max}	maximum rate of respiration (mol/mm ³ s)
Y	experimental (observed) value of normalized drug delivery in a TB granuloma
Y'	modeled (predicted) value of normalized drug delivery in a TB granuloma

Greek Symbols:

α_0	dimensionless modulus (i.e., granuloma/tumor size)
χ	dimensionless Michaelis-Menten kinetic factor
Δ	thickness of well-perfused layer (mm)
ε	volume fraction
ϕ	Thiele modulus
φ_B	volumetric rate of oxygen delivery from the vasculature into the tissue (mm ³ /s)
φ_L	volumetric flow rate of plasma to the lymph vessels (mm ³ /s)
κ	ratio of the first-order rate constant for oxygen consumption to the half-saturation constant of the Michaelis-Menten equation (mol/Ls)
λ_Δ	dimensionless well-perfused layer thickness
π_i	interstitial oncotic pressure (mmHg)
π_v	vessel oncotic pressure (mmHg)
ϱ	dimensionless pressure difference
σ_S	solute (Staverman) reflection coefficient
τ	tortuosity factor
ν	dimensionless IFV
ξ	dimensionless radial depth
ψ	dimensionless IFP

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